

85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

October 22, 2024

City of Portsmouth Planning Department Attn: Peter Stith, Planning Manager 1 Junkins Avenue, Suite 3rd Floor Portsmouth, NH 03801

RE: Response Letter 3

635 Sagamore Ave, Portsmouth, NH

Tax Map 222, Lot 19 JBE Project No. 18134.1

Dear Mr. Stith,

We are in receipt of comments from Eric Weinrieb, P.E., Altus Engineering dated October 7, 2024 and Stefanie Casella, Portsmouth Planning Department, dated September 30, 2024. Review comments are listed below with our responses in bold. In addition to the comments listed below, we have also added a proposed radar speed sign near the intersection of Sagamore Avenue and Cliff Road as requested by Eric Eby. This sign is shown on Sheet H1 of the plan set and standard specifications for the sign have been added to Sheet D6.

ALTUS Comments:

GENERAL COMMENTS:

1.Based on the discussion at the October 1st TAC meeting, it is understood the Designer was going to expand the retaining wall and move it closer to buildings 3 and 4, making the wall higher, while preserving more of the natural vegetation. This will also provide more fill material for the absorption of the roof and perimeter drain runoff and additional soil for the proposed landscaping. In general, Altus supports this approach and will provide comment on the design when the revised plans and documents are submitted.

RESPONSE: We have extended the proposed retaining wall and moved the proposed plantings to the high side of it in order to preserve existing vegetation, provide more of a visual buffer, and provide additional soil beneath the proposed landscaping.

2. The Designer has eliminated the infiltration component from the large stormwater management device behind the Patten residence. Infiltration is being considered for the management of the runoff from buildings 3 and 4. As noted by the Designer, the infiltration basins are sitting on ledge and will have some modest downward infiltration into the ledge cracks. The majority of the runoff will travel laterally into the filled area. The subgrade backfill material is specified as "backfill material shall be suitable for both infiltration and deck supports." The Designer needs to provide further information

clarifying their intentions including material specifications, minimum thickness of said material and the layout of the underdrain from drip edge should be provided including key elevations. It is unclear if the pipe will abruptly stop at the edge of the stone reservoir or if it runs through the system similar to an effluent disposal system.

RESPONSE: We have specified on the "Infiltration stone underneath deck" detail on Sheet D5 that the backfill material beneath these infiltration practices shall be native material from elsewhere on site and shall be placed from pre-construction existing grade to bottom of stone, in the locations where the bottom of stone will be in a fill. As shown in plan view on Sheet C3, the perforated 6" HDPE underdrain shall continue through the stone underneath the deck and this has also been noted on the detail on Sheet D5. As noted, the top elevation of the underdrain shall be 3" below the top of stone.

3. The Designer is now specifying a "sand absorption area" for the perimeter drain collection/infiltration system. The Designer needs to provide details for this treatment device including bedding material, bedding preparation, inverts, surface treatment, maintenance requirements, soil absorption capacity, and down gradient material requirements. As drawn, it appears that the discharge pipes will be on the ground surface without adequate cover. The design should provide material specifications for the downgradient fill material and how the materials will interface.

RESPONSE: A detail for the stand absorption area has been added to Sheet D4. This detail specifies the depth of sand, a sieve specification for the sand material, and the specification for the berm, subgrade, and downgradient material. Additionally, we have noted on Sheet C3 that a 3' wide overflow spillway shall be added 3" above the top of sand, and that the foundation drain shall outlet at or above the spillway elevation so that water does not back up into the unit basements.

4. The Inspection and Maintenance Operations Manual needs to be amended to include the "sand absorption area."

RESPONSE: The operations & maintenance manual has been amended to include a section for the sand absorption areas.

5. The Designer should provide an explanation as to why all of the amoozemeter tests started at the exact same time and have the exact same results.

RESPONSE: This is not true. The results of the amoozemeter tests vary and they did not start at the same time. The '0.0 minutes' listed at the beginning of each test is relative to each time increment only for that specific test. Nine consecutive tests were performed (three in each of the three locations) and none were simultaneous.

6. The drainage study narrative should be updated to reflect the current design approach. RESPONSE: The drainage narrative has been updated to reflect the current design approach.



7. The drainage computations indicate that in the 10-year storm event, the peak elevation in the stone reservoir behind building 3 is elevation 67.08. The basement finished floor elevation is elevation 65.70 and the adjacent grade appears to be in the 65 range. It appears that pond will overflow. The Designer also needs to confirm the rate of infiltration, the analysis indicates that the rate is 0.3 inches per hour. The tests indicate that the rate is 0.15 inches per hour.

RESPONSE: We have revised the elevations in our drainage computations so that the top of the stone reservoir is 8" below the basement finished floor. Because these devices are in fill, a worst-case-scenario infiltration rate of 0.6 in/hr was conservatively assumed for the fill material and a factor of safety of two was applied in order to arrive at the infiltration rate of 0.3 in/hr to use for design. The section of the drainage narrative where it was stated simply that the infiltration rate of the material was assumed to be 0.3 in/hr has been revised for clarification.

8. The drainage computations indicate that in the 10-year storm event, the peak elevation in the stone reservoir behind building 4 is elevation 66.2. The finish grade contour 66 runs through the stone basin, thus it appears that pond will overflow. The Designer also needs to confirm the rate of infiltration, the analysis indicates that the rate is 0.3 inches per hour. The tests indicate that the rate is 0.15 inches per hour.

RESPONSE: We have revised the elevations in our drainage computations so that the top of the stone reservoir is 8" below the basement finished floor. The system is sloped but the grade of the stone reservoir immediately adjacent to the unit was modelled as the top of the stone reservoir because that is the location where there is the smallest separation from finished grade to existing grade, and therefore the smallest separation to ledge beneath the bottom of stone. The far end of the stone reservoir where the finished grade is lowest will fill up first.

Because these devices are in fill, a worst-case-scenario infiltration rate of 0.6 in/hr was conservatively assumed for the fill material and a factor of safety of two was applied in order to arrive at the infiltration rate of 0.3 in/hr to use for design. The section of the drainage narrative where it was stated simply that the infiltration rate of the material was assumed to be 0.3 in/hr has been revised for clarification.

9. As previously noted, and acknowledged by the Designer, the Tidewatch Condominium development closed drainage system along their access drive does not operate properly. Stormwater bypasses the culverts as the roadway and drainage system is not properly maintained. No action required.

RESPONSE: No response needed.

TAC Comments:

1. In reference to #9 response to TAC comments, will it be reduced from existing conditions or from construction conditions?

RESPONSE: Peak flow rates and runoff volumes will be reduced from existing conditions as required.

2. Please provide the height of all structures based on the definition found in the Zoning Ordinance.

RESPONSE: Building heights have been added to the architectural plans.



3.Limited common areas cannot be included in the condo agreement as there can be no division of land without a subdivision.

RESPONSE: LCA lines are no longer shown on the condominium site plan. They will be described in the condominium documents.

4. Altus needs final review and approval of the drainage scheme.

RESPONSE: See above responses to Altus comments.

5.Behind units 3 & 4, it seems like if the proposed boulder retaining wall was extended along the path of the proposed 60 contour, a number of existing trees could be saved and the additional plantings that are proposed could then be planted uphill of the wall. This would provide a sufficiently sloped and adequate 'back yard' and the fill soil for the wall would provide enough soil for the new shrubs and plantings to grow into a nice screen placed between the 64 and 60 contour.

RESPONSE: We have extended the proposed boulder retaining wall as shown in Sheet C3. Plantings have been moved to the uphill side of the retaining wall as shown on Sheet L2 and we are now maintaining more of a natural vegetated buffer.

6.A final dollar value based on as-built cost is needed for the developer to pay for the new drainage basin, water stub, and hydrant on Sagamore.

RESPONSE: Understood.

7. Water stub and hydrant have been installed. Remove from plans.

RESPONSE: The water stub and hydrant are now shown as existing rather than proposed features.

8. Tracer wire must be installed with HDPE water main.

RESPONSE: The water system trench detail on Sheet D2 has been revised to specify blue tracer wire above the water main.

9. Water main is small diameter HDPE pipe that can be bent. Bends and thrust blocks are not recommended.

RESPONSE: Bends and thrust blocks have been removed from the plan; instead, we are showing the water main to be deflected.

10.Each unit only gets one water service. Irrigation meter is a sub-meter after the domestic water meter.

RESPONSE: Irrigation services have been revised from the plans. We are still showing irrigation meters in the interior of each unit. A 1" HDPE water service for both potable water and irrigation to each unit has been provided

11. Private hydrant maintenance agreement and standard easement for leak detection and valve access will be required.

RESPONSE: A private hydrant maintenance agreement will be provided. See Note #17 on Sheet C2, and Note #15 on Sheet CS1 regarding the need for an easement. Such easement will be provided to and approved by the City Legal Department prior to construction.



Included with this response letter are the following:

- 1. One (1) Full Size Revised Plan Set.
- 2. Architectural Plans and Elevations (At end of plan set and separately).
- 3. One (1) Revised Drainage Analysis.
- 4. Updated Site Review Checklist.
- 5. One (1) Revised Stormwater Operations & Maintenance Manual.

If you have any questions or need any additional information, please feel free to contact our office. Thank you very much for your time.

Very truly yours,

JONES & BEACH ENGINEERS, INC.

Joseph A. Coronati

Vice President

cd:

Eric Weinrieb, P.E., Altus Engineering (via email and hand delivered) Stefanie Casella, Portsmouth Planning Department (via email) Michael Garrepy (via email)

JONES & BEACH



City of Portsmouth, New Hampshire Site Plan Application Checklist

This site plan application checklist is a tool designed to assist the applicant in the planning process and for preparing the application for Planning Board review. The checklist is required to be completed and uploaded to the Site Plan application in the City's online permitting system. A preapplication conference with a member of the planning department is strongly encouraged as additional project information may be required depending on the size and scope. The applicant is cautioned that this checklist is only a guide and is not intended to be a complete list of all site plan review requirements. Please refer to the Site Plan review regulations for full details.

Applicant Responsibilities (Section 2.5.2): Applicable fees are due upon application submittal along with required attachments. The application shall be complete as submitted and provide adequate information for evaluation of the proposed site development. <u>Waiver requests must be submitted in writing with appropriate justification</u>.

Name of Applicant: 635 Sagamore Development, LLC	_ Date Submitted:	3/18/24	
Application # (in City's online permitting): LU-22-209			
Site Address: 635 Sagamore Avenue		Map: _22:	2Lot: _19

	Application Requirements		
Ø	Required Items for Submittal	Item Location (e.g. Page or Plan Sheet/Note #)	Waiver Requested
X	Complete <u>application</u> form submitted via the City's web-based permitting program (2.5.2.1(2.5.2.3A)		N/A
X	All application documents, plans, supporting documentation and other materials uploaded to the application form in viewpoint in digital Portable Document Format (PDF). One hard copy of all plans and materials shall be submitted to the Planning Department by the published deadline. (2.5.2.8)		N/A

	Site Plan Review Application Required Information		
\square	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
X	Statement that lists and describes "green" building components and systems. (2.5.3.1B)	Included with Submissic	n
X	Existing and proposed gross floor area and dimensions of all buildings and statement of uses and floor area for each floor. (2.5.3.1C)	Architectural Plans	N/A
X	Tax map and lot number, and current zoning of all parcels under Site Plan Review. (2.5.3.1D)	Cover Sheet & Sheet C2	N/A

	Site Plan Review Application Required Information			
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested	
X	Owner's name, address, telephone number, and signature. Name, address, and telephone number of applicant if different from owner. (2.5.3.1E)	Cover Sheet	N/A	
X	Names and addresses (including Tax Map and Lot number and zoning districts) of all direct abutting property owners (including properties located across abutting streets) and holders of existing conservation, preservation or agricultural preservation restrictions affecting the subject property. (2.5.3.1F)	Cover Sheet	N/A	
X	Names, addresses and telephone numbers of all professionals involved in the site plan design. (2.5.3.1G)	Cover Sheet	N/A	
x	List of reference plans. (2.5.3.1H)	Cl	N/A	
х	List of names and contact information of all public or private utilities servicing the site. (2.5.3.11)	Cover Sheet	N/A	

Site Plan Specifications			
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
X	Full size plans shall not be larger than 22 inches by 34 inches with match lines as required, unless approved by the Planning Director (2.5.4.1A)	Required on all plan sheets	N/A
X	Scale: Not less than 1 inch = 60 feet and a graphic bar scale shall be included on all plans. (2.5.4.1B)	Required on all plan sheets	N/A
Х	GIS data should be referenced to the coordinate system New Hampshire State Plane, NAD83 (1996), with units in feet. (2.5.4.1C)	C1, Note #3	N/A
X	Plans shall be drawn to scale and stamped by a NH licensed civil engineer. (2.5.4.1D)	Required on all plan sheets	N/A
X	Wetlands shall be delineated by a NH certified wetlands scientist and so stamped. (2.5.4.1E)	None Observed, Wetland Delineation Report Include	N/A
X	Title (name of development project), north point, scale, legend. (2.5.4.2A)	C1	N/A
X	Date plans first submitted, date and explanation of revisions. (2.5.4.2B)	All Sheets	N/A
X	Individual plan sheet title that clearly describes the information that is displayed. (2.5.4.2C)	Required on all plan sheets	N/A
K	Source and date of data displayed on the plan. (2.5.4.2D)	Cı	N/A

	Site Plan Specifications – Required Exhibits and Data		
Ø	Required Items for Submittai	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
X	 Existing Conditions: (2.5.4.3A) Surveyed plan of site showing existing natural and built features; Existing building footprints and gross floor area; Existing parking areas and number of parking spaces provided; Zoning district boundaries; Existing, required, and proposed dimensional zoning requirements including building and open space coverage, yards and/or setbacks, and dwelling units per acre; Existing impervious and disturbed areas; Limits and type of existing vegetation; Wetland delineation, wetland function and value assessment (including vernal pools); SFHA, 100-year flood elevation line and BFE data, as required. 	C1	
X	 2. Buildings and Structures: (2.5.4.3B) Plan view: Use, size, dimensions, footings, overhangs, 1st fl. elevation; Elevations: Height, massing, placement, materials, lighting, façade treatments; Total Floor Area; Number of Usable Floors; Gross floor area by floor and use. 	Architectural Plans	
X	 Access and Circulation: (2.5.4.3C) Location/width of access ways within site; Location of curbing, right of ways, edge of pavement and sidewalks; Location, type, size and design of traffic signing (pavement markings); Names/layout of existing abutting streets; Driveway curb cuts for abutting prop. and public roads; If subdivision; Names of all roads, right of way lines and easements noted; AASHTO truck turning templates, description of minimum vehicle allowed being a WB-50 (unless otherwise approved by TAC). 	C2 T1-T2	
x	 4. Parking and Loading: (2.5.4.3D) Location of off street parking/loading areas, landscaped areas/buffers; Parking Calculations (# required and the # provided). 	C2, Note #3	
X	 Water Infrastructure: (2.5.4.3E) Size, type and location of water mains, shut-offs, hydrants & Engineering data; Location of wells and monitoring wells (include protective radii). 	C4	
X	Sewer Infrastructure: (2.5.4.3F) Size, type and location of sanitary sewage facilities & Engineering data, including any onsite temporary facilities during construction period.	C4 & P2	

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X	 7. Utilities: (2.5.4.3G) The size, type and location of all above & below ground utilities; Size type and location of generator pads, transformers and other fixtures. 	C4
X	8. Solid Waste Facilities: (2.5.4.3H)	C2, Note #22
	The size, type and location of solid waste facilities.	
X	 9. Storm water Management: (2.5.4.3I) The location, elevation and layout of all storm-water drainage. The location of onsite snow storage areas and/or proposed off-site snow removal provisions. Location and containment measures for any salt storage facilities Location of proposed temporary and permanent material storage locations and distance from wetlands, water bodies, and stormwater structures. 	Snow Storage - C2 Everything Else - C3
X	 10. Outdoor Lighting: (2.5.4.3J) Type and placement of all lighting (exterior of building, parking lot and any other areas of the site) and photometric plan. 	L2
X	11. Indicate where dark sky friendly lighting measures have been implemented. (10.1)	Everywhere
X	 12. Landscaping: (2.5.4.3K) Identify all undisturbed area, existing vegetation and that which is to be retained; Location of any irrigation system and water source. 	L1
X	 13. Contours and Elevation: (2.5.4.3L) Existing/Proposed contours (2 foot minimum) and finished grade elevations. 	C3
X	 14. Open Space: (2.5.4.3M) Type, extent and location of all existing/proposed open space. 	C2, Note #2
	15. All easements, deed restrictions and non-public rights of ways. (2.5.4.3N)	N/A
	 16. Character/Civic District (All following information shall be included): (2.5.4.3P) Applicable Building Height (10.5A21.20 & 10.5A43.30); Applicable Special Requirements (10.5A21.30); Proposed building form/type (10.5A43); Proposed community space (10.5A46). 	N/A
	 17. Special Flood Hazard Areas (2.5.4.3Q) The proposed development is consistent with the need to minimize flood damage; All public utilities and facilities are located and construction to minimize or eliminate flood damage; Adequate drainage is provided so as to reduce exposure to flood hazards. 	N/A

	Other Required Information		
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
Х	Traffic Impact Study or Trip Generation Report, as required. (3.2.1-2)	Included with Submission	
X	Indicate where Low Impact Development Design practices have been incorporated. (7.1)	С3	
X	Indicate whether the proposed development is located in a wellhead protection or aquifer protection area. Such determination shall be approved by the Director of the Dept. of Public Works. (7.3.1)	C2, Note #23	
X	Stormwater Management and Erosion Control Plan. (7.4)	Included with Submission	
X	Inspection and Maintenance Plan (7.6.5)	Included with Submission	

	Final Site Plan Approval Required Info	rmation	
Ø	Required Items for Submittal		/aiver uested
X	All local approvals, permits, easements and licenses required, including but not limited to: • Waivers; • Driveway permits; • Special exceptions; • Variances granted; • Easements; • Licenses. (2.5.3.2A)	C2, Note # 4 & 5	
X	 Exhibits, data, reports or studies that may have been required as part of the approval process, including but not limited to: Calculations relating to stormwater runoff; Information on composition and quantity of water demand and wastewater generated; Information on air, water or land pollutants to be discharged, including standards, quantity, treatment and/or controls; Estimates of traffic generation and counts pre- and post-construction; Estimates of noise generation; A Stormwater Management and Erosion Control Plan; Endangered species and archaeological / historical studies; Wetland and water body (coastal and inland) delineations; Environmental impact studies. 	Included with Submission	
X	A document from each of the required private utility service providers indicating approval of the proposed site plan and indicating an ability to provide all required private utilities to the site. (2.5.3.2D)	Pending	

Final Site Plan Approval Required Information Required Items for Submittal Item Location Waiver				
Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested		
A list of any required state and federal permit applications required for the project and the status of same. (2.5.3.2E)	C2, Note #5			
A note shall be provided on the Site Plan stating: "All conditions on this Plan shall remain in effect in perpetuity pursuant to the requirements of the Site Plan Review Regulations." (2.5.4.2E)	C2, Note #21	N/A		
For site plans that involve land designated as "Special Flood Hazard Areas" (SFHA) by the National Flood Insurance Program (NFIP) confirmation that all necessary permits have been received from those governmental agencies from which approval is required by Federal or State law, including Section 404 of the Federal Water Pollution Control Act Amendments of 1972, 33 U.S.C. 1334. (2.5.4.2F)	N/A			
Plan sheets submitted for recording shall include the following notes: a. "This Site Plan shall be recorded in the Rockingham County Registry of Deeds." b. "All improvements shown on this Site Plan shall be constructed and maintained in accordance with the Plan by the property owner and all future property owners. No changes shall be made to this Site Plan without the express approval of the Portsmouth Planning Director."	C2, Note #19 & 20	N/A		
	A list of any required state and federal permit applications required for the project and the status of same. (2.5.3.2E) A note shall be provided on the Site Plan stating: "All conditions on this Plan shall remain in effect in perpetuity pursuant to the requirements of the Site Plan Review Regulations." (2.5.4.2E) For site plans that involve land designated as "Special Flood Hazard Areas" (SFHA) by the National Flood Insurance Program (NFIP) confirmation that all necessary permits have been received from those governmental agencies from which approval is required by Federal or State law, including Section 404 of the Federal Water Pollution Control Act Amendments of 1972, 33 U.S.C. 1334. (2.5.4.2F) Plan sheets submitted for recording shall include the following notes: a. "This Site Plan shall be recorded in the Rockingham County Registry of Deeds." b. "All improvements shown on this Site Plan shall be constructed and maintained in accordance with the Plan by the property owner and all future property owners. No	Required Items for Submittal A list of any required state and federal permit applications required for the project and the status of same. (2.5.3.2E) A note shall be provided on the Site Plan stating: "All conditions on this Plan shall remain in effect in perpetuity pursuant to the requirements of the Site Plan Review Regulations." (2.5.4.2E) For site plans that involve land designated as "Special Flood Hazard Areas" (SFHA) by the National Flood Insurance Program (NFIP) confirmation that all necessary permits have been received from those governmental agencies from which approval is required by Federal or State law, including Section 404 of the Federal Water Pollution Control Act Amendments of 1972, 33 U.S.C. 1334. (2.5.4.2F) Plan sheets submitted for recording shall include the following notes: a. "This Site Plan shall be recorded in the Rockingham County Registry of Deeds." b. "All improvements shown on this Site Plan shall be constructed and maintained in accordance with the Plan by the property owner and all future property owners. No changes shall be made to this Site Plan without the express		

Applicant's Signature:	9/5/2024 Date:	
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Sagamore A... Save

Letter of Authorization

635 Sagamore Development, LLC, owner of property located at 635 Sagamore Avenue in Portsmouth, NH, known as Tax Map 222, Lot 19, do hereby authorize Jones & Beach Engineers, Inc. ("JBE"), Garrepy Planning Consultants, LLC ("GPC"), and Hoefle, Phoenix, Gormley & Roberts, PLLC ("HPGR") to act on its behalf concerning the previously mentioned property.

I hereby appoint JBE, GPC and HPGR as agents to act on behalf of 635 Sagamore Development, LLC in the Planning Board and Zoning Board application process, to include any required signatures.

635 Sagamore Development, LLC

Timothy J. Black, Duly Authorized

January 5, 2022 Date

Book: 6332 Page: 1158

Return to:

E # 21060614 09/24/2021 09:32:59 AM Book 6332 Page 1158 Page 1 of 2

Register of Deeds, Rockingham County

LCHIP ROA585829 TRANSFER TAX R0109828 RECORDING

SURCHARGE

25.00 5.807.00 14.00

WARRANTY DEED

KNOW ALL BY THESE PRESENTS, that I, WILLIAM A. HINES, married person, TRUSTEE OF THE WILLIAM A. HINES FAMILY REVOCABLE TRUST a/k/a The Hines Family Revocable Trust of 2006, of 635 Sagamore Avenue, Portsmouth, New Hampshire 03801, for consideration paid. hereby grant to 635 SAGAMORE DEVELOPMENT, LLC, a New Hampshire limited liability company with a mailing address of 3612 Lafayette Road, Dept. 4, Portsmouth, New Hampshire 03801 with WARRANTY COVENANTS, the following described premises:

A certain tract of land with the buildings thereon, situate on Sagamore Avenue in said Portsmouth, more particularly described as follows:

Beginning at a point on Sagamore Avenue at land now or formerly of Arnold, thence running Westerly by said Arnold land three hundred (300) feet, more or less, to land now or formerly of W.W. and D.M. Johnston; thence turning and running Northwesterly by said Johnston land one hundred and twentyfour (124) feet; thence turning and running Northerly also by said Johnston land one hundred sixtytwo (162) feet to land now or formerly of C.W. Walker; thence turning and running Easterly by said Walker land four hundred nineteen (419) feet to Sagamore Avenue; thence turning and running Easterly one hundred forty (140) feet; thence turning and running along said Sagamore Avenue thirty (30) feet to land of one Smith; thence turning and running Westerly one hundred forty (140) feet; thence turning and running Southerly ninety (90) feet; thence turning and running Easterly one hundred forty (140) feet to Sagamore Avenue; the last three bounds being land of Smith; thence turning running Southerly by said Sagamore Avenue one hundred sixty (160) feet to the point of beginning.

EXCEPTING AND RESERVING to the said William A. Hines and his wife Bonnie Hines a life estate in the above-described property permitting them to reside in the existing residential apartment on the property for the remainder of William A. Hines natural life, plus one year unless Bonne Hines shall have predeceased.

Meaning and intending to convey the same premises conveyed to the Grantor by deed of William A. Hines dated February 11, 2008 and recorded in the Rockingham County Registry of Deeds at Book 4885, Page 1538.

BY SIGNING BELOW, William A. Hines and Bonnie Hines release all homestead rights to the Premises.

Book: 6332 Page: 1159

TRUSTEE CERTIFICATE

I, William A. Hines, Trustee of the William A. Hines Family Revocable Trust A/K/A The Hines Family Revocable Trust of 2006, hereby covenant that said Trust is duly organized under the laws of the State of New Hampshire; that I am the sole trustee pursuant to said Declaration of Trust; that said Trust is still in full force and effect; that I have the power thereunder to convey as aforesaid; and that, in making this conveyance, I have, in all respects, acted pursuant to the authority vested in and granted to me therein and no purchaser or third party shall be bound to inquire whether the Trustee has said power or are properly exercising said power or to see to the application of any trust assets paid to the Trustee for a conveyance thereof.

Signed this 3rd day of September, 2021.

William A. Hines, Trustee of the William A. Hines Family Revocable Trust A/K/A The Hines Family Revocable Trust of 2006

Bonnic Hines

STATE OF NEW HAMPSHIRE COUNTY OF ROCKINGHAM

On this, the 3rd day of September, 2021, before me, the undersigned Officer, personally appeared William A. Hines, Trustee of the William A. Hines Family Revocable Trust A/K/A The Hines Family Revocable Trust of 2006, known to me, or satisfactorily proven, to be the person whose name is subscribed to the foregoing instrument, and acknowledged that he executed the same for the purposes set forth therein.

Justice of the Peace/Notary Public
My commission expires:

AMMINITAL.

COMMISSION EXPIRES

COMMISSION

STATE OF NEW HAMPSHIRE COUNTY OF ROCKINGHAM

On this, the 3rd day of September, 2021, before me, the undersigned Officer, personally appeared Bonnie Hines, known to me, or satisfactorily proven, to be the person whose name is subscribed to the foregoing instrument, and acknowledged that she executed the same for the purposes set forth the resignation.

ustice of the Peace/Notary Public

My commission expires:

< Sagamore A... Save □

Letter of Authorization

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635 Sagamore Development, LLC

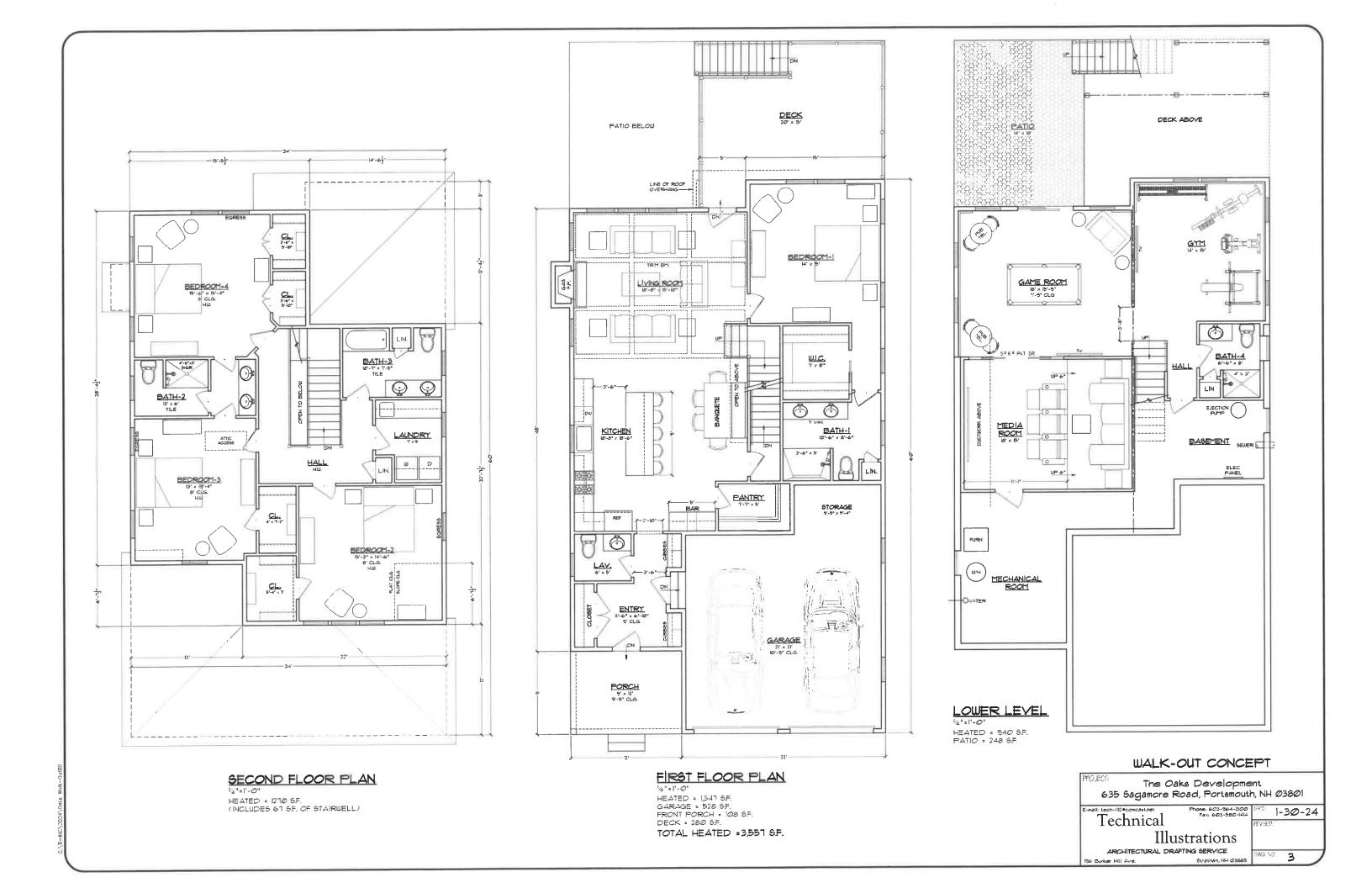
Timothy J. Black Duly Authorized

January 5, 2022 Date

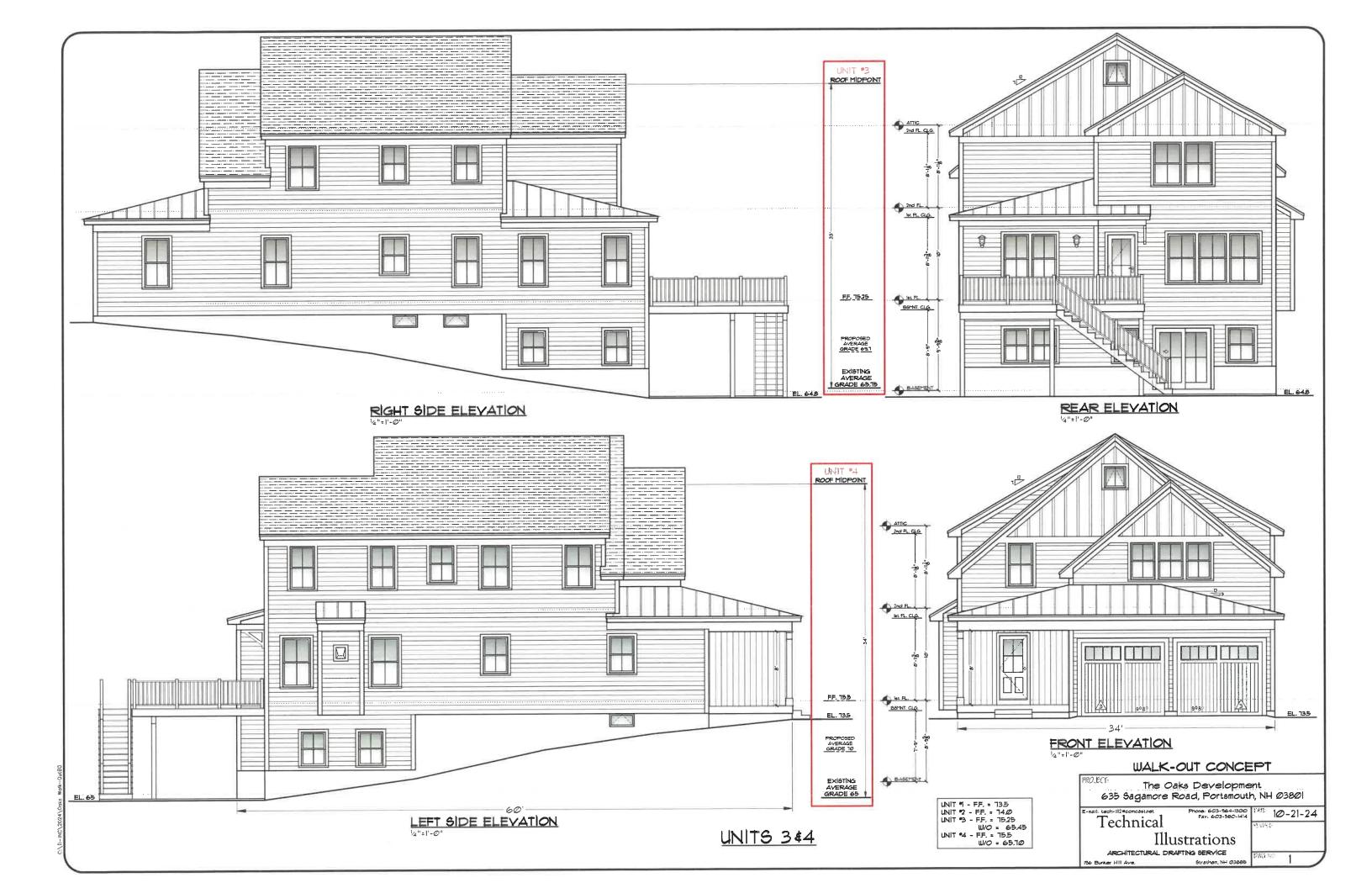














85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

STORMWATER MANAGEMENT OPERATIONS AND MAINTENANCE MANUAL

Luster Cluster 635 Sagamore Ave. Portsmouth, NH 03801 Tax Map 222, Lot 19

Prepared for:

635 Sagamore Development LLC 3612 Lafayette Rd., Dept 4 Portsmouth, NH 03801

Prepared by:

Jones & Beach Engineers, Inc.
85 Portsmouth Avenue
P.O. Box 219
Stratham, NH 03885
(603) 772-4746
March 18, 2024
Revised April 15, 2024
Revised August 8, 2024
Revised October 14, 2024
JBE Project No. 18134.1

Inspection and Maintenance of Facilities and Property

A. Maintenance of Common Facilities or Property

1. The Condominium Association, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Association, future owners and assigns shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form and shall submit an Operations and Maintenance report on a yearly basis to the Portsmouth Planning Department.

B. General Inspection and Maintenance Requirements

- 1. Permanent stormwater and sediment and erosion control facilities to be maintained on the site include, but are not limited to, the following:
 - a. Roadway and driveways
 - b. Vegetation and landscaping
 - c. Sediment Forebay
 - d. Bioretention system
 - e. Catch Basins & Yard Drains
 - f. Stone Drip Edges
 - g. Stone Underneath Decks
 - h. Culverts
 - i. Rip-Rap Outlet Protection Aprons
 - i. Sand Absorption Areas
- 2. Maintenance of permanent measures shall follow the following schedule:
 - a. Normal winter roadway maintenance including plowing and snow removal. Road sweeping at the end of every winter, preferably before the start of the spring rain season.
 - b. **Annual inspection** of the site for erosion, destabilization, settling, and sloughing. Any needed repairs are to be conducted immediately. **Annual inspection** of site's vegetation and landscaping. Any areas that are bare shall be reseeded and mulched with hay or, if the case is extreme, loamed and seeded or sodded to ensure adequate vegetative cover. Landscape specimens shall be replaced in kind, if they are found to be dead or dying.
 - c. Cleaning Criteria for all Sedimentation Forebays: Sediment shall be removed from the sedimentation chamber (forebay) when it accumulates to a depth of more than 12 inches (30 cm) or 10 percent of the pretreatment volume. The sedimentation forebay shall be cleaned of vegetation if persistent standing water and wetland vegetation becomes dominant. The cleaning interval is once every year. A dry sedimentation forebay is the optimal condition while in practice this condition is rarely achieved. The sedimentation chamber, forebay, and treatment cell outlet devices shall be cleaned when drawdown



chamber, forebay, and treatment cell outlet devices shall be cleaned when drawdown times exceed 60 to 72 hours. Materials can be removed with heavy construction equipment; however, this equipment shall not track on the wetland surface. Revegetate disturbed areas as necessary. Removed sediments shall be dewatered (if necessary) and disposed of in an acceptable manner.

d. Bioretention Systems:

- Visually inspect monthly and repair erosion. Use small stones to stabilize erosion along drainage paths.
- Check the pH once a year if grass is not surviving. Apply an alkaline product, such as limestone, if needed.
- Re-seed any bare areas by hand as needed.
- Immediately after the completion of cell construction, water grass for 14 consecutive days unless there is sufficient natural rainfall.
- Once a month (more frequently in the summer), the land owner or Association shall visually inspect vegetation for disease or pest problems and treat as required.
- During times of extended drought, look for physical features of stress. Water in the early morning as needed.
- Weed regularly, if needed.
- After rainstorms, inspect the cell and make sure that drainage paths are clear and that ponding water dissipates over 4-6 hours. (Water may pond for longer times during the winter and early spring.)
- Twice annually, inspect the outlet control structures to ensure that they are not clogged and correct any clogging found as needed.
- Any debris and sediment accumulations shall be removed from the outlet structures, overflow risers, and emergency spillways and disposed of properly.
- Inspect outlet structure for deterioration and or clogging.
- If erosion is evident on the berm or emergency spillway, stabilize the affected area by seeding. Trees must not be allowed to grow in these areas.
- KEEP IN MIND, THE BIORETENTION CELL IS NOT A POND. IT SHALL NOT PROVIDE A BREEDING GROUND FOR MOSQUITOES. MOSQUITOES NEED AT LEAST FOUR (4) DAYS OF STANDING WATER TO DEVELOP AS LARVA.
- e. Annual inspection of catch basins and yard drains to determine if they need to be cleaned. Catch basins and yard drains are to be cleaned if the depth of deposits is greater than one-half the depth from the basin bottom to the invert of the lowest pipe or opening into or out of the basin. If a catch basin or yard drain significantly exceeds the one-half depth standard during the inspection, then it shall be cleaned more frequently. If woody debris or trash accumulates in the catch basin or yard drain, then it shall be cleaned on a weekly basis. The catch basin or yard drain can be cleaned either manually or by specially designed equipment including, but not limited to, bucket loaders and vacuum pumps. Before any materials can be disposed, it is necessary to perform a detailed chemical analysis to determine if the materials meet the EPA criteria for hazardous waste. This will help determine

how the materials shall be stored, treated, and disposed. Grease hoods are to be wiped clean and the rags disposed of properly. Debris obscuring the grate inlet shall also be removed.

f. Stone drip edges:

Units 3 & 4 feature stone drip edges to collect roof runoff into a pipe in order to direct it into the stone areas underneath the unit decks. These practices shall be lined and are not intended for infiltration. The following course of action will help assure that the roof drip edges are maintained to preserve its effectiveness.

In the spring and fall, visually inspect the area around the edges and repair any erosion. Use small stones to stabilize erosion along drainage paths. Inspect stone area to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation shall not be allowed to become established in stone areas, and/or any debris removed from the void spaces between the stones

g. Stone underneath decks:

Units 3 and 4 feature stone areas underneath their associated rear decks for infiltration of roof runoff. The following guidelines will help ensure proper functioning of the system.

In the spring and fall, visually inspect the area around the edges and repair any erosion. Use small stones to stabilize erosion along drainage paths. Inspect stone area to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation shall not be allowed to become established in stone areas, and/or any debris removed from the void spaces between the stones.

- h. **Inspection** of culvert inlets and outlets at least **once per month** during the rainy season (March to November). Any debris is to be removed and disposed of properly.
 - i. Rock riprap shall be **inspected annually** in order to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation must not be allowed to become established in riprap areas, and/or any debris removed from the void spaces between the rocks. If the riprap is adjacent to a stream or other waterbody, the water shall be kept clear of obstructions, debris, and sediment deposits

j. There are two sand absorption areas intended to infiltrate foundation drain effluent to the extent practicable. One is located approximately 34'-45' past the end of the shared driveway near the southeast property line of the site in order to handle foundation drain effluent for Units 1 and 2. The other is located between the backyards of Units 3 and 4 in order to handle foundation drain effluent for Units 3 and 4. The foundation drain outfalls shall be **inspected monthly** and more frequently during autumn in order to ensure that there is no debris or leaf buildup. Any debris or leaves that is either clogging or appears that it may clog the outlets must be removed **immediately** and disposed of properly.

During these inspections, additionally check for sediment buildup and standing water in the small ponding areas for these devices. If more than 1" of standing water is persistently present in these systems, contact a professional engineer to evaluate the issue. Remedies may range from cleaning the overflow spillway to replacing the sand media.

See attached sample forms as a guideline.

Any inquiries in regards to the design, function, and/or maintenance of any one of the abovementioned facilities or tasks shall be directed to the project engineer:

Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885

T#: (603) 772-4746 F#: (603) 772-0227



Commitment to maintenance requirements

I agree to complete and/or observe all of the required maintenance practices and their respective schedules as outlined above.		
Signature		
	_	
Print Name		
Title	-	
Date	-	

Annual Operations and Maintenance Report

The Condominium Association, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Association, future owners and assigns shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form and shall submit an Operations and Maintenance report on a yearly basis to the Portsmouth Planning Department.

Construction Activity	Date of Inspection	Who Inspected	Findings of Inspector
Roadway and Driveways			
Vegetation and Landscaping			
Sediment Forebay			
Bioretention Pond			
Catch Basins & Yard Drains			

Unit 3 Stone Drip Edge		
Unit 4 Stone Drip Edge		
'		
Stone underneath unit 3 deck		
Stone underneath unit 4 deck		
Culverts		
Rip Rap Outlet Protection		
Units 1&2 Foundation		
drain outfall sand absorption area		

Units 3&4 Foundation drain outfall sand absorption area		
Swale		
Other (please note):		

Regular Inspection and Maintenance Guidance for Bioretention Systems / Tree Filters

Maintenance of bioretention systems and tree filters can typically be performed as part of standard landscaping. Regular inspection and maintenance is critical to the effective operation of bioretention systems and tree filters to insure they remain clear of leaves and debris and free draining. This page provides guidance on maintenance activities that are typically required for these systems, along with the suggested frequency for each activity. Individual systems may have more, or less, frequent maintenance needs, depending on a variety of factors including the occurrence of large storm events, overly wet or dry (I.E., drought), regional hydrologic conditions, and the upstream land use.

ACTIVITIES

The most common maintenance activity is the removal of leaves from the system and bypass structure. Visual inspections are routine for system maintenance. This includes looking for standing water, accumulated leaves, holes in the soil media, signs of plant distress, and debris and sediment accumulation in the system. Mulch and/or vegetation coverage is integral to the performance of the system, including infiltration rate and nutrient uptake. Vegetation care is important to system productivity and health.

ACTIVITY	FREQUENCY	
A record should be kept of the time to drain for the system completely after a storm event. The system should drain completely within 72 hours.		
Check to insure the filter surface remains well draining after storm event. Remedy: If filter bed is clogged, draining poorly, or standing water covers more than 15% of the surface 48 hours after a precipitation event, then remove top	After every major storm in the first few months, then biannually.	
few inches of discolored material. Till or rake remaining material as needed.		
Check inlets and outlets for leaves and debris. Remedy: Rake in and around the system to clear it of debris. Also, clear the inlet and overflow if obstructed.		
Check for animal burrows and short circuiting in the system Remedy: Soil erosion from short circuiting or animal boroughs should be repaired when they occur. The holes should be filled and lightly compacted.	Quarterly initially, biannually, frequency adjusted as needed after 3 inspections	
Check to insure the filter bed does not contain more than 2 inches accumulated material		
Remedy: Remove sediment as necessary. If 2 inches or more of filter bed has been removed, replace media with either mulch or a (50% sand, 20% woodchips, 20% compost, 10% soil) mixture.		
During extended periods without rainfall, inspect plants for signs of distress. Remedy: Plants should be watered until established (typical only for first few months) or as needed thereafter.		
Inspect inlets and outlets to ensure good condition and no evidence of deterioration. Check to see if high-flow bypass is functioning. Remedy: Repair or replace any damaged structural parts, inlets, outlets, sidewalls.	Annually	
Check for robust vegetation coverage throughout the system. Remedy: If at least 50% vegetation coverage is not established after 2 years, reinforcement planting should be performed.		
Check for dead or dying plants, and general long term plant health. Remedy: This vegetation should be cut and removed from the system. If woody vegetation is present, care should be taken to remove dead or decaying plant Material. Separation of Herbaceous vegetation rootstock should occur when overcrowding is observed.	As needed	

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CHECKLIST FOR INSPECTION OF BIORETENTION SYSTEM / TREE FILTERS

1	oca	tı	\sim	n	
4	JUUG	ы	u	ı	

Inspector:

Date:

Time:

Site Conditions:

Date Since Last Rain Event:

Inspection Items		tory (S) or actory (U)	Comments/Corrective Action
1. Initial Inspection After Planting and Mulching			
Plants are stable, roots not exposed	S	U	
Surface is at design level, typically 4" below overpass	S	U	
Overflow bypass / inlet (if available) is functional	s	U	
2. Debris Cleanup (2 times a year minimum, Spring & Fall)		8. N . L.L	
Litter, leaves, and dead vegetation removed from the system	S	U]
Prune perennial vegetation	s	U	
3. Standing Water (1 time a year, After large storm events)	ST WILL		
No evidence of standing water after 72 hours	s	U	
4. Short Circuiting & Erosion (1 time a year, After large storm	n events)		
No evidence of animal burrows or other holes	S	U	
No evidence of erosion	S	U]
5. Drought Conditions (As needed)			
Water plants as needed	U]	
Dead or dying plants			1
6. Overflow Bypass / Inlet Inspection (1 time a year, After lar	ge storm ev	ents)	
No evidence of blockage or accumulated leaves	S	U	1
Good condition, no need for repair	s	U	1
7. Vegetation Coverage (once a year)			
50% coverage established throughout system by first year	s	U	
Robust coverage by year 2 or later	s	U	
8. Mulch Depth (if applicable)(once every 2 years)		15 1 1 1 No.	
Mulch at original design depth after tilling or replacement	s	U	
9. Vegetation Health (once every 3 years)	111 11 1		
Dead or decaying plants removed from the system	s	U	
10. Tree Pruning (once every 3 years)			
Prune dead, diseased, or crossing branches	s	Ü	
Corrective Action Needed			Due Date
1.			
2.			
3.			

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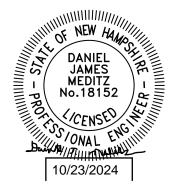
DRAINAGE ANALYSIS

SEDIMENT AND EROSION CONTROL PLAN

"Luster Cluster" 635 Sagamore Ave. Portsmouth, NH 03801 Tax Map 222, Lot 19

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March 14, 2024
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JBE Project No. 18134.1

EXECUTIVE SUMMARY

635 Sagamore Development LLC proposes to demolish an existing commercial development and construct a 4-unit multi-family residential site on the subject parcel located at 635 Sagamore Ave. in Portsmouth, NH. In the existing condition, the subject parcel is home to two buildings and a paved parking area that used to comprise the "Luster King," a former auto detailing business that has since closed.

A drainage analysis of the entire site as well as offsite contributing watershed area was conducted for the purpose of estimating the peak rate of stormwater runoff and to subsequently design adequate drainage structures. Two models were compiled, one for the area in its existing (pre-construction) condition, and a second for its proposed (post-construction) condition. The analysis was conducted using data for the 2 Year – 24 Hour (3.70"), 10 Year – 24 Hour (5.61"), 25 Year – 24 Hour (7.12"), and 50 Year – 24 Hour (8.53") storm events using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment. This data was taken from the Extreme Precipitation Tables developed by the Northeast Regional Climate Center (NRCC), and the values have been increased by 15% due to the project being within the Coastal/Great Bay Region. A summary of the existing and proposed conditions peak rates of runoff toward the three analysis points and toward the existing drainage ditch on the Tidewatch Condominium property (Reach 1R) in units of cubic feet per second (cfs) is as follows:

Analysis Point	2 Y	ear	10 Year		25 Year		50 Year	
	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Analysis Point #1	1.36	1.03	2.38	1.83	3.19	2.46	3.95	3.05
Analysis Point #2	0.09	0.06	0.20	0.13	0.29	0.19	0.37	0.24
Analysis Point #3	2.79	2.40	5.63	4.12	8.00	5.49	10.27	7.72
Analysis Point #4	1.08	0.81	2.18	1.63	3.10	2.32	3.97	2.97

A similar summary of the existing and proposed peak volumes in units of acre-feet is as follows:

Analysis Point	2 Y	ear	10 Y	'ear	25 Y	Year	50 Y	Year
	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Analysis Point #1	0.100	0.076	0.177	0.135	0.241	0.185	0.301	0.231
Analysis Point #2	0.007	0.005	0.014	0.009	0.021	0.014	0.027	0.018
Analysis Point #3	0.240	0.208	0.477	0.405	0.681	0.577	0.879	0.744
Analysis Point #4	0.084	0.064	0.167	0.126	0.238	0.179	0.307	0.230

Peak flows and volumes are being reduced in the post-construction condition toward all analysis points during all analyzed storm events. The subject parcel is located in the Single Residence A (SRA) Zoning District. The subject parcel currently consists of the aforementioned former commercial site which is proposed to be demolished. Despite impervious surface existing on the subject parcel now, the proposed development results in an increase in impervious surface on the subject parcel. The addition of the proposed impervious surfaces causes an increase in the curve number (C_n) and a decrease in the time of concentration (T_c) , and if a stormwater management system were not implemented, the net result of this would be a potential increase in peak rates of runoff from the site. In order to avoid this potential, a stormwater management system has been designed, consisting of a bioretention system with a sediment forebay for pre-treatment of runoff, stone drip edges, and stone underneath decks as well as sand absorption areas for foundation drain effluent. Due to the use of these

stormwater management features, the peak flow and volume of runoff will be reduced toward all analysis points during all analyzed storm events in the proposed condition as compared to the existing condition, and the treatment requirements of the City of Portsmouth are met. Additionally, the NHDES Alteration of Terrain Bureau's groundwater recharge volume and channel protection requirements are met with the proposed development. Although some runoff from the front of the site proposed to drain into the Sagamore Avenue right of way and into a new catch basin without on-site treatment, the catch basin was presumably designed for the impervious surface being directed toward it from the Luster King development that currently exists. We are decreasing the amount of impervious surface as well as the peak flow rate and volume of runoff being directed toward this catch basin compared to what it was designed for. Therefore, if there is a treatment system at the outfall of the closed drainage network, then it will continue to function as designed for the runoff being directed to it from the proposed development. The stormwater management system as designed meets all requirements of the City of Portsmouth stormwater regulations per Section 7.1 and 7.4-7.6 of the Site Plan Review Regulations.

The use of Best Management Practices per the NHDES <u>Stormwater Manual</u> have been applied to the design of this stormwater management system and will be observed during all stages of construction. All land disturbed during construction will be stabilized within thirty days of groundbreaking and abutting property owners will suffer minimal adversity resultant to this development.

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1.0 RAINFALL CHARACTERISTICS

This drainage report includes an existing conditions analysis of the area involved in the proposed development, as well as a proposed condition, or post-construction analysis, of the same area. These analyses were accomplished using the USDA SCS TR-20 Method within the HydroCAD 10.20-3c Stormwater Modeling System. The curve numbers were developed using the SCS TR-55 Runoff Curve numbers for Urban Areas. A Type III SCS 24-hour rainfall distribution was utilized in analyzing the data for the 2 Year – 24 Hour (3.70"), 10 Year – 24 Hour (5.61"), 25 Year – 24 Hour (7.12"), and 50 Year – 24 Hour (8.53") storm events. This data was taken from the Extreme Precipitation Tables developed by the Northeast Regional Climate Center (NRCC), and the values have been increased by 15% due to the project being within the Coastal/Great Bay Region.

The peak rates and volume of runoff will be reduced from the existing condition, thereby minimizing any potential for a negative impact on abutting properties. This is accomplished through treatment of stormwater runoff and attenuation of peak flows and volumes resulting from storm events.

2.0 EXISTING CONDITIONS ANALYSIS

In the existing condition, the site consists of two commercial buildings as well as a shed and a paved parking area that comprise the former Luster King auto detailing business, which has since closed. Most of the area behind the existing commercial development is wooded with light underbrush and large ledge outcrops. There is some lawn space around the existing developed area as well.

The existing topography and roof ridges divide the subject parcel and offsite contributing watershed areas into four subcatchments, draining toward three analysis points. Subcatchment 1 represents the front of the subject parcel as well as a stretch of the northbound lane of Sagamore Avenue and some offsite contributing watershed. This subcatchment is entirely developed in the existing condition, and it drains directly into the Sagamore Ave. right of way, down a flow path modelled as Reach 3R. Reach 3R ends at Analysis Point 1, a specific point along the Sagamore Avenue right of way. The reason why Analysis Point 1 was located at the specific place where it was is explained later in this report.

Runoff that reaches Analysis Point 1 from the subject parcel then follows the curb lines of Sagamore Avenue and of the Tidewatch Condominium Roadway, modelled as Reaches 4R and 5R, toward an existing water collection point on the side of the Tidewatch Condominium Roadway where it appears that a significant amount of runoff puddles in the existing condition, modelled as Analysis Point 3.

A new catch basin has been installed just to the south of the intersection of Sagamore Avenue and the Tidewatch Condominium roadway as part of the ongoing Sagamore Avenue roadway improvements. This catch basin captures all runoff directed toward Analysis Point 1 immediately downstream of Reach 3R. Therefore, Analysis Point 1 was placed at the location of the newly installed catch basin. The addition of this catch basin prevents water from the Sagamore Avenue right of way up to the top of the hill to the south of the subject parcel from draining down the Tidewatch Condominium roadway, and therefore it will somewhat mitigate the existing drainage issue. However, because this catch basin was not yet installed at the time that the design of the proposed project began, we are modelling the hydrology of the site as it was before the catch basin was installed for the purposes of the existing conditions analysis. This is consistent with Env-Wq 1503.12(d), which requires that the existing conditions for a project site be modelled as the site was 10 years ago. In the proposed conditions analysis, we are modelling the site hydrology as is with the catch basin having been installed.

Subcatchment 2S represents a small section of the developed portion of the property to the north of an existing high point which drains on to abutting Tax Map 222, Lot 20, modelled as Analysis Point 2. It is very important that peak flows and volumes draining toward Analysis Points 1 and 2 are reduced in the post-construction condition, as these two analysis points represent a highway and a house lot, respectively. Runoff directed toward Analysis Point 2 is directed through Reach 2R, a flow path through Tax Map 222 Lot 20, toward aforementioned Reach 3R, from where the runoff then collects at AP1 before following Reaches 4R and 5R toward Analysis Point 3. In effect, the runoff directed toward AP1 includes the runoff directed toward AP2, and the runoff directed toward AP3 includes the runoff directed toward both AP1 and AP2 in the existing condition.

The largest subcatchment is Subcatchment 3S. Subcatchment 3S is roughly the western quarter of the property and it consists primarily of woodland with large ledge outcrops. Subcatchment 3S drains toward an existing drainage ditch alongside and below the grade of the Tidewatch Condominium private roadway, which is curbed so that no runoff from the roadway itself enters the ditch. This drainage ditch is modelled as a Tc segment for the subcatchment and it drains toward Analysis Point 3. Analysis Point 3 is an existing water collection point along the Tidewatch Condominium Road. In theory, water that collects here eventually infiltrates or overflows, but from on-site observations, there is erosion and puddling which is evidence that runoff mostly stops in this spot. Therefore, it is modelled as an analysis point with no overflow. This point receives the runoff from 3S as well as the runoff from AP1 and AP2 upstream.

Finally, a section of both developed and undeveloped land in the western end of the property, modelled as Subcatchment 4S, drains into abutting woodland on the Tidewatch Condominium property and ultimately toward a catch basin adjacent to the Tidewatch Condominium mailhouse that is modelled as Analysis Point 4.

Existing soil types were determined through a Site Specific Soil Survey conducted by a Certified Soil Scientist. The pervious soils are categorized into Hydrologic Soil Group (HSG) B while the impervious areas of the subject parcel are categorized as Urban Land (SSS Symbol 699). The pervious sections of the property are represented as Chatfield-Hollis-Rock Outcrop complex and Chatfield Variant (moderately well drained). Although these soils are categorized as HSG B currently, it is our understanding that the "Ksat Values for New Hampshire Soils," Special Publication No. 5 sponsored by the Society of Soil Scientists of Northern New England (SSSNNE) is in the process of being updated and there are plans to reclassify Chatfield as a HSG C soil. For this reason, Dave Desfosses of the Portsmouth Department of Public Works has requested that we model the entire site and all offsite contributing watershed areas as HSG C. We asked the project soil scientist, who confirmed that this is an acceptable approach in his professional opinion as well. Therefore, we have modelled the entire site and all offsite areas as HSG C.

According to "Ksat Values for New Hampshire Soils," Special Publication No. 5 sponsored by the Society of Soil Scientists of Northern New England (SSSNNE), Chatfield, Chatfield Variant, and Hollis soils all have identical saturated hydraulic conductivities, ranging from 0.6 to 6.0 inches/hour within both the B and C horizons.

To further determine the appropriate Ksat to use for design, infiltration testing was performed on site using a Compact Constant Head Permeameter (CCHP, also known as an amoozemeter) on July 2, 2024. Three (3) pits were dug using a shovel in the soil and three (3) infiltration tests were performed in each pit. The first pit was dug in the front of the site in order to evaluate the feasibility of adding a

new infiltration practice here. The second pit was dug in the footprint of the proposed bioretention system. The third and final pit was dug in the vicinity of Unit #4.

Standard size auger holes, 4 cm in diameter were dug within each pit to the depth of the bottom of each respective practice to obtain an accurate permeability reading below the bottom of the proposed systems. Water was then discharged through the soil and the drop in water level on the tube in which the water was stored before being discharged was recorded at several time intervals. The comparison between the drop in water level and the elapsed time from the start of the test was used to calculate the Ksat value. For example, if the water level dropped 3 cm after 5 minutes and 5 cm after 10 minutes, this was recorded and used as data to calculate the Ksat using the formulas listed in the data spreadsheets in the appendix of this report. The Ksat values from each time increment were then averaged to determine the mean Ksat, and lowest mean Ksat from each area was divided by a factor of safety of two in order to determine the saturated hydraulic conductivity to use for design purposes.

It should be noted that the CCHP was observed to drain very rapidly on these holes and it was difficult to achieve a steady state. The device was consistently draining while still attempting to fill the auger holes with water. When the test could finally be started, the first one or two increments on each test needed to be discarded from the results because they were much larger than the following increments after the soils were saturated and the infiltration rate stabilized. The saturated hydraulic conductivity that was determined at each test site was ultimately much higher than anticipated, but logically it makes sense as the substrate was observed to consist of coarse sand with many stones.

The results of the permeability testing are as summarized below:

Test	Ksat (in/hr)
Front of site – Test #1	27.33
Front of site – Test #2	30.85
Front of site – Test #3	22.26
Front of site – Low Ksat	22.26
Bioretention – Test #1	14.84
Bioretention – Test #2	33.41
Bioretention – Test #3	65.74
Bioretention – Low Ksat	14.84
Unit 4 – Test #1	30.64
Unit 4 – Test #2	25.41
Unit 4 – Test #3	37.31
Unit 4 – Low Ksat	25.41

A further breakdown of the data used to arrive at the final Ksat values is included in the appendix of this report. Applying a factor of safety of two, this comes out to a saturated hydraulic conductivity of 11.1 in/hr to use for the front of the site, 7.4 in/hr to use for the bioretention system, and 12.71 in/hr to use for the infiltration practices around the back two units. It was later determined that, because the bioretention system is in a cut, has a clay core berm, and is surrounded by ledge outcrops, infiltration could not be modelled on this device anyway. Because the infiltration practices are in a fill, a design infiltration rate of 0.6 in/hr was assumed as a worst-case scenario for the fill material. A factor of safety of two was applied and an infiltration rate of 0.3 in/hr was used for design.

3.0 PROPOSED CONDITIONS ANALYSIS

The addition of the proposed impervious surfaces causes an increase in the curve number (C_n) and a decrease in the time of concentration (T_c) , and if a stormwater management system were not implemented, the net result of this would be a potential increase in peak rates of runoff from the site. A stormwater management system was designed in order to avoid this potential. The proposed development, consisting of the aforementioned four (4) residential units with associated paved roadway and driveways as well as stormwater management features divide the subject parcel into seventeen (17) subcatchments. Subcatchments 1S-4S drain directly toward Analysis Points 1-4, respectively, as previously outlined. However, because a new catch basin will now intercept the flow that reaches the Sagamore Avenue right of way (Analysis Point 1) from the subject parcel, analysis point 3 is no longer modelled downstream of analysis point 1.

Subcatchment 5S has been removed from the drainage analysis as it was the subcatchment associated with a stormwater pond that has since been removed from the drainage design. Subcatchments 6S-9S drain through catch basins into a closed drainage system which outlets toward a bioretention pond modelled as Pond 1P. The bioretention pond is designed to treat the water quality volume of runoff directed to it and otherwise attenuate stormwater so that the peak rate of runoff at the analysis point is lower post-development than it is in the existing condition. The bioretention pond will have a sediment forebay for pre-treatment. Any discharge from Pond 1P follows a path through Subcatchment 3S represented as Reach 7R, toward Reach 8R, an existing roadside ditch on the Tidewatch condominium property leading to Analysis Point 3.

Subcatchments 11S and 12S consist of lawn and roof areas that drain toward yard drains 1 and 2, respectively. The runoff that is caught by these yard drains additionally enters the previously described closed drainage system that outlets toward Pond 1P.

Subcatchments 13S and 14S represent roof and deck areas on Units 3-4 which are routed toward infiltration stone underneath these units back decks. These devices are modelled as Ponds 3P and 4P.

Subcatchments 15S and 16S represent roof areas on Units 3 and 4 which drain into stone drip edges adjacent to the inside facing walls on these units. The stone drip edges, modelled as Ponds 5P and 6P, will be lined and underdrained for the sole purpose of directing this roof water into the aforementioned stone areas underneath the back decks of these units (3P and 4P) in order to meet the City's pollutant removal requirements.

Subcatchments 17S and 18S represent roof areas on Units 3 and 4 which drain into stone drip edges adjacent to the outside facing walls on these units. Although these stone drip edges, modelled as Ponds 7P and 8P, are useless for infiltration due to the presence of a perimeter drain beneath them, they will prevent the grassed slope adjacent to the units from eroding due to inundation with roof runoff. The stone drip edges will be lined and underdrained, and the underdrains for Ponds 7P and 8P will outlet toward Reaches 9R and 10R, which themselves carry water toward 1P and AP4, respectively.

Finally, Subcatchment 19S represents the grassed and roof area that drains directly toward Pond 1P without passing through the closed drainage system in the proposed condition.

As a result of the implementation of this stormwater management system, peak flows and runoff volumes are reduced toward all four analysis points during all analyzed storm events in the proposed condition as compared with the existing condition. The NHDES Alteration of Terrain Bureau allows

an increase in runoff volume of up to 0.1 acre-feet during the 2-year 24-hour storm event. We are decreasing runoff volumes and therefore this would be approvable by the AOT Bureau if the project needed an AOT permit (which it does not as the area of disturbance is below 100,000 SF).

Furthermore, the project as designed exceeds the AOT Bureau's groundwater recharge volume requirement. A GRV worksheet is contained within the appendix of this report in order to illustrate this. Therefore, we have designed the drainage system to avoid adverse impacts to abutting infrastructure and the requirement per Section 7.1 of the Site Plan Review Regulations to "design practices to the maximum extent practical (MEP) to reduce stormwater runoff volumes, maintain predevelopment site hydrology, and protect water quality in receiving waters" is met. Rain gardens (also known as bioretention systems) are recommended as a Low Impact Development practice in this same section of the regulations. We are using bioretention systems to treat and attenuate runoff from paved areas of the subject parcel in the proposed condition.

According to the NH Stormwater Manual, bioretention systems provide a pollutant removal efficiency of 90% for TSS and 65% for nitrogen, and drip edges provide a removal efficiency of 90% for TSS and 55% for nitrogen. While drip edges cannot be used for infiltration in this case as the units will have foundation drains, stone underneath a deck is assumed to provide similar stormwater treatment to a stone drip edge. The City of Portsmouth Site Plan Review Regulations stipulate that stormwater BMPs shall be designed for 80% TSS removal and 50% nitrogen removal of stormwater runoff from post-construction impervious surfaces. This plan meets the pollutant removal requirement for runoff directed toward Analysis Points 3 and 4 in the post-construction condition. A breakdown of pollutant removal efficiencies for the runoff that passes through the bioretention ponds, stone infiltration areas, or no treatment BMP and reaches Analysis Points 3 and 4 from the subject parcel is contained within the appendix of this report in order to demonstrate this.

No impervious surface is directed toward Analysis Point 2 post-construction. Presumably, the flow directed toward the new catch basin along the gutter line of Sagamore Avenue from the existing Luster King development was accounted for in the design of the City's closed drainage network. Because the amount of impervious surface being directed toward Analysis Point 1 is being decreased post-construction, we presume that whatever stormwater management the City had proposed for the runoff downstream of the new catch basin will continue to function as intended post-construction. Therefore, no on-site treatment BMPs are proposed for the impervious surface directed toward Analysis Point 1 post-construction, and the impervious surface directed toward analysis point 1 post-construction is excluded from the pollutant removal calculations. Even if we did propose a treatment BMP for the runoff directed toward the Sagamore Avenue right of way, what would result is a point discharge of stormwater from an outlet pipe or weir directly toward pavement, which is not advisable. Therefore, this water *cannot* be treated on site, which will not be a problem assuming that the City designed an appropriate BMP for the runoff directed toward its catch basin from the Luster King site.

5.0 CONCLUSION

This proposed site development will have minimal adverse effect on abutting infrastructures, properties, and downstream wetlands by way of stormwater runoff or siltation. Appropriate steps will be taken to eliminate erosion and sedimentation; this will be accomplished through the construction of a drainage system consisting of site grading, catch basins, yard drains, a bioretention system, lined stone drip edges, infiltration stone underneath decks, and temporary erosion control measures including but not limited to silt fence and the use of a stabilized construction entrance. Best Management Practices developed by the State of New Hampshire have been utilized in the design of

this system and their application will be enforced throughout the construction process. Peak rates and volumes of runoff from the site will be reduced toward all analysis points during all analyzed storm events.

This project disturbs less than 100,000 S.F. and does <u>not</u> require a NHDES Alteration of Terrain Permit.

Respectfully Submitted,

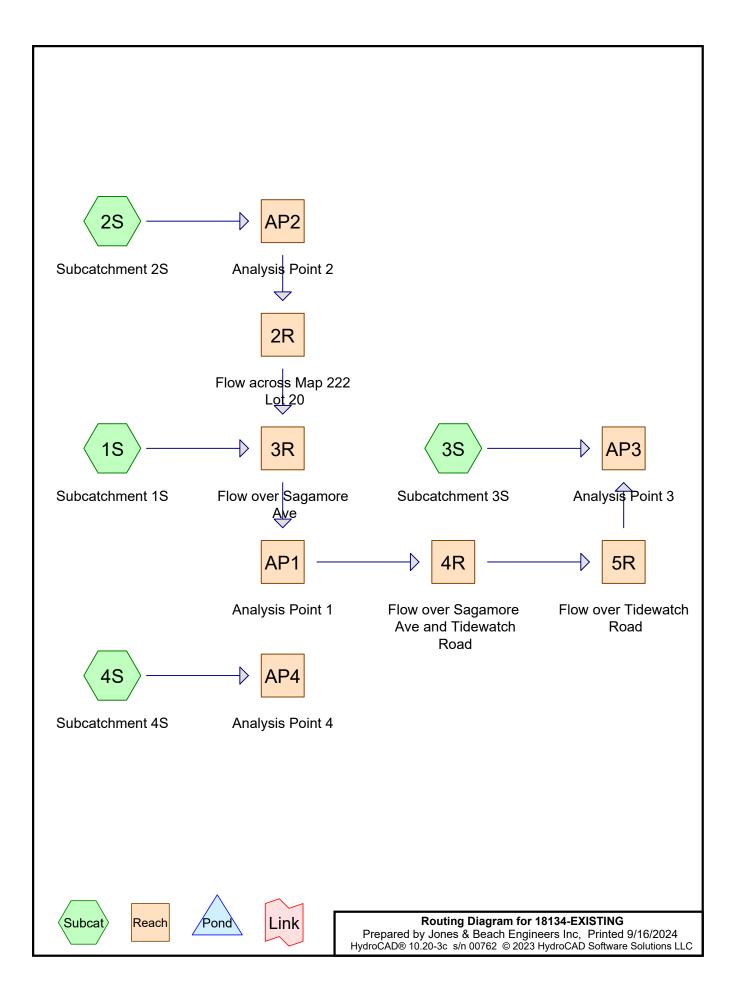
JONES & BEACH ENGINEERS, INC.

Daniel Meditz, P.E Lead Design Engineer

APPENDIX I

EXISTING CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Complete 10 YEAR Summary 25 YEAR Complete 50 YEAR



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Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.621	74	>75% Grass cover, Good, HSG C (1S, 2S, 3S, 4S)
0.123	96	Ledge, HSG C (3S, 4S)
0.230	98	Paved parking, HSG C (1S, 4S)
0.129	98	Roofs, HSG C (1S, 3S, 4S)
1.415	70	Woods, Good, HSG C (1S, 2S, 3S, 4S)
2.518	76	TOTAL AREA

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
2.518	HSG C	1S, 2S, 3S, 4S
0.000	HSG D	
0.000	Other	
2.518		TOTAL AREA

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1SRunoff Area=20,592 sf 54.90% Impervious Runoff Depth>2.36"
Flow Length=187' Tc=6.0 min CN=87 Runoff=1.28 cfs 0.093 af

Subcatchment2S: Subcatchment2S Runoff Area=2,614 sf 0.00% Impervious Runoff Depth>1.38" Flow Length=20' Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.09 cfs 0.007 af

Subcatchment3S: Subcatchment3SRunoff Area=58,629 sf 0.32% Impervious Runoff Depth>1.25"

Flow Length=447' Tc=11.9 min CN=72 Runoff=1.53 cfs 0.140 af

Subcatchment4S: Subcatchment4SRunoff Area=27,837 sf 14.82% Impervious Runoff Depth>1.58"
Flow Length=216' Tc=7.8 min CN=77 Runoff=1.08 cfs 0.084 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.02' Max Vel=0.63 fps Inflow=0.09 cfs 0.007 af n=0.030 L=81.0' S=0.0494 '/' Capacity=88.18 cfs Outflow=0.09 cfs 0.007 af

Reach 3R: Flow over Sagamore AveAvg. Flow Depth=0.14' Max Vel=2.71 fps Inflow=1.36 cfs 0.100 af n=0.016 L=101.0' S=0.0297'/' Capacity=39.77 cfs Outflow=1.36 cfs 0.100 af

Reach 4R: Flow over Sagamore Ave and Avg. Flow Depth=0.14' Max Vel=2.85 fps Inflow=1.36 cfs 0.100 af n=0.016 L=145.0' S=0.0345 '/' Capacity=42.85 cfs Outflow=1.35 cfs 0.100 af

Reach 5R: Flow over Tidewatch Road Avg. Flow Depth=0.12' Max Vel=3.38 fps Inflow=1.35 cfs 0.100 af n=0.016 L=253.0' S=0.0553 '/' Capacity=54.28 cfs Outflow=1.31 cfs 0.100 af

Reach AP1: Analysis Point 1 Inflow=1.36 cfs 0.100 af

Outflow=1.36 cfs 0.100 af

Reach AP2: Analysis Point 2 Inflow=0.09 cfs 0.007 af Outflow=0.09 cfs 0.007 af

Reach AP3: Analysis Point 3 Inflow=2.79 cfs 0.240 af Outflow=2.79 cfs 0.240 af

Reach AP4: Analysis Point 4 Inflow=1.08 cfs 0.084 af

Outflow=1.08 cfs 0.084 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.324 af Average Runoff Depth = 1.55" 85.76% Pervious = 2.159 ac 14.24% Impervious = 0.359 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S Runoff Area=20,592 sf 54.90% Impervious Runoff Depth>4.14"

Flow Length=187' Tc=6.0 min CN=87 Runoff=2.19 cfs 0.163 af

Subcatchment2S: Subcatchment2S Runoff Area=2,614 sf 0.00% Impervious Runoff Depth>2.86"

Flow Length=20' Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.20 cfs 0.014 af

Subcatchment3S: Subcatchment3S Runoff Area=58,629 sf 0.32% Impervious Runoff Depth>2.67"

Flow Length=447' Tc=11.9 min CN=72 Runoff=3.44 cfs 0.300 af

Subcatchment4S: Subcatchment4S Runoff Area=27,837 sf 14.82% Impervious Runoff Depth>3.14"

Flow Length=216' Tc=7.8 min CN=77 Runoff=2.18 cfs 0.167 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.03' Max Vel=0.80 fps Inflow=0.20 cfs 0.014 af

n=0.030 L=81.0' S=0.0494 '/' Capacity=88.18 cfs Outflow=0.19 cfs 0.014 af

Reach 3R: Flow over Sagamore Ave

Avg. Flow Depth=0.17' Max Vel=3.12 fps Inflow=2.38 cfs 0.177 af

n=0.016 L=101.0' S=0.0297'/' Capacity=39.77 cfs Outflow=2.38 cfs 0.177 af

Reach 4R: Flow over Sagamore Ave and Avg. Flow Depth=0.17' Max Vel=3.29 fps Inflow=2.38 cfs 0.177 af

 $n = 0.016 \quad L = 145.0' \quad S = 0.0345 \; \text{'/'} \quad Capacity = 42.85 \; \text{cfs} \quad Outflow = 2.37 \; \text{cfs} \quad 0.177 \; \text{af}$

Reach 5R: Flow over Tidewatch Road Avg. Flow Depth=0.15' Max Vel=3.88 fps Inflow=2.37 cfs 0.177 af

n=0.016 L=253.0' S=0.0553'/' Capacity=54.28 cfs Outflow=2.31 cfs 0.177 af

Reach AP1: Analysis Point 1 Inflow=2.38 cfs 0.177 af

Outflow=2.38 cfs 0.177 af

Reach AP2: Analysis Point 2 Inflow=0.20 cfs 0.014 af

Outflow=0.20 cfs 0.014 af

Reach AP3: Analysis Point 3 Inflow=5.63 cfs 0.477 af

Outflow=5.63 cfs 0.477 af

Reach AP4: Analysis Point 4 Inflow=2.18 cfs 0.167 af

Outflow=2.18 cfs 0.167 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.644 af Average Runoff Depth = 3.07" 85.76% Pervious = 2.159 ac 14.24% Impervious = 0.359 ac

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 2.19 cfs @ 12.09 hrs, Volume=

0.163 af, Depth> 4.14"

Routed to Reach 3R: Flow over Sagamore Ave

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

_	Α	rea (sf)	CN E	Description						
		2,869	98 F	98 Roofs, HSG C						
		8,436	98 F	Paved park	ing, HSG C					
		9,256	74 >	·75% Gras	s cover, Go	ood, HSG C				
		31	70 V	Voods, Go	od, HSG C					
		20,592	87 V	Veighted A	verage					
		9,287		•	vious Area					
		11,305	5	4.90% Imp	ervious Ar	ea				
	Тс	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	2.5	46	0.1090	0.31		Sheet Flow,				
						Grass: Short n= 0.150 P2= 3.70"				
	0.1	4	0.0670	1.26		Sheet Flow,				
						Smooth surfaces n= 0.011 P2= 3.70"				
	0.1	41	0.0670	5.25		Shallow Concentrated Flow,				
						Paved Kv= 20.3 fps				
	0.4	96	0.0360	3.85		Shallow Concentrated Flow,				
_						Paved Kv= 20.3 fps				
	3.1	187	Total, I	ncreased t	o minimum	Tc = 6.0 min				

,

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.20 cfs @ 12.09 hrs, Volume=

0.014 af, Depth> 2.86"

Routed to Reach AP2: Analysis Point 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Aı	rea (sf)	CN	Description						
		2,495	74	>75% Gras	s cover, Go	ood, HSG C				
_		119	70	Woods, Go	od, HSG C					
		2,614	74	Weighted A	verage					
		2,614		100.00% P	ervious Are	a				
	Tc	Length	Slope	,	Capacity	Description				
_	(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)					
	1.3	20	0.1000	0.25		Sheet Flow,				
_						Grass: Short	n= 0.150	P2= 3.70"		

1.3 20 Total, Increased to minimum Tc = 6.0 min

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Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 3.44 cfs @ 12.17 hrs, Volume=

0.300 af, Depth> 2.67"

Routed to Reach AP3: Analysis Point 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Area (sf)	CN E	escription		
	187	98 F	Roofs, HSC	G C	
	9,391	74 >	75% Gras	s cover, Go	ood, HSG C
	46,312	70 V	Voods, Go	od, HSG C	
*	2,739	96 L	edge, HS0	G C	
	58,629	72 V	Veighted A	verage	
	58,442	9	9.68% Per	rvious Area	
	187	0	.32% Impe	ervious Are	a
Тс		Slope	Velocity		Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.6	50	0.0415	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
0.7	62	0.0968	1.56		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.7	54	0.0741	1.36		Shallow Concentrated Flow,
4.0	400	0.4000	4.50		Woodland Kv= 5.0 fps
1.3	122	0.1000	1.58		Shallow Concentrated Flow,
0.0	450	0.0400	4 55	40.00	Woodland Kv= 5.0 fps
0.6	159	0.0189	4.55	18.20	Trap/Vee/Rect Channel Flow,
					Bot.W=1.00' D=1.00' Z= 3.0 '/' Top.W=7.00'
44.0	4.4-	T ()			n= 0.030 Short grass
11.9	447	Total			

, iotai

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 2.18 cfs @ 12.11 hrs, Volume= 0.167 af, Depth> 3.14"

Routed to Reach AP4: Analysis Point 4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Area (sf)	CN	Description					
	2,555	98	Roofs, HSG C					
	1,571	98	Paved parking, HSG C					
	5,912	74	75% Grass cover, Good, HSG C					
	15,194	70	Voods, Good, HSG C					
*	2,605	96	Ledge, HSG C					
	27,837	77	Weighted Average					
	23,711		85.18% Pervious Area					
	4,126		14.82% Impervious Area					

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.9	14	0.0210	0.13		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	4.2	36	0.1280	0.14		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	0.5	50	0.1280	1.79		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	1.0	87	0.0800	1.41		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.2	29	0.2860	2.67		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	7.8	216	Total			

Summary for Reach 2R: Flow across Map 222 Lot 20

Inflow Area = 0.060 ac, 0.00% Impervious, Inflow Depth > 2.86" for 10 Yr 24 Hr +15% event

Inflow = 0.20 cfs @ 12.09 hrs, Volume= 0.014 af

Outflow = 0.19 cfs @ 12.11 hrs, Volume= 0.014 af, Atten= 3%, Lag= 1.2 min

Routed to Reach 3R: Flow over Sagamore Ave

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.80 fps, Min. Travel Time= 1.7 min Avg. Velocity = 0.31 fps, Avg. Travel Time= 4.4 min

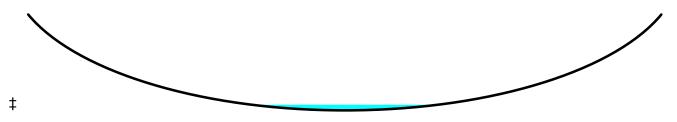
Peak Storage= 19 cf @ 12.11 hrs

Average Depth at Peak Storage= 0.03', Surface Width= 12.14' Bank-Full Depth= 0.50' Flow Area= 16.7 sf, Capacity= 88.18 cfs

50.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight

Length= 81.0' Slope= 0.0494 '/'

Inlet Invert= 66.00', Outlet Invert= 62.00'



Summary for Reach 3R: Flow over Sagamore Ave

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[62] Hint: Exceeded Reach 2R OUTLET depth by 2.14' @ 12.10 hrs

[64] Warning: Exceeded Reach 2R outlet bank by 1.67' @ 12.10 hrs

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 4.00" for 10 Yr 24 Hr +15% event

Inflow = 2.38 cfs @ 12.09 hrs, Volume= 0.177 af

Outflow = 2.38 cfs @ 12.10 hrs, Volume= 0.177 af, Atten= 0%, Lag= 0.4 min

Routed to Reach AP1: Analysis Point 1

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.12 fps, Min. Travel Time= 0.5 min

Avg. Velocity = 1.23 fps, Avg. Travel Time= 1.4 min

Peak Storage= 77 cf @ 12.10 hrs

Average Depth at Peak Storage= 0.17', Surface Width= 8.78' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 39.77 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= $50.0\ 0.5$ '/ Top Width= 25.25' Length= 101.0' Slope= 0.0297'/ Inlet Invert= 64.00', Outlet Invert= 61.00'

‡

Summary for Reach 4R: Flow over Sagamore Ave and Tidewatch Road

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 4.00" for 10 Yr 24 Hr +15% event

Inflow = 2.38 cfs @ 12.10 hrs, Volume= 0.177 af

Outflow = 2.37 cfs @ 12.11 hrs, Volume= 0.177 af, Atten= 1%, Lag= 0.6 min

Routed to Reach 5R: Flow over Tidewatch Road

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.29 fps, Min. Travel Time= 0.7 min Avg. Velocity = 1.30 fps, Avg. Travel Time= 1.9 min

Peak Storage= 104 cf @ 12.11 hrs

Average Depth at Peak Storage= 0.17', Surface Width= 8.52' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 42.85 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 145.0' Slope= 0.0345 '/'

Inlet Invert= 61.00', Outlet Invert= 56.00'

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Summary for Reach 5R: Flow over Tidewatch Road

[61] Hint: Exceeded Reach 4R outlet invert by 0.15' @ 12.10 hrs

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 3.99" for 10 Yr 24 Hr +15% event

Inflow = 2.37 cfs @ 12.11 hrs, Volume= 0.177 af

Outflow = 2.31 cfs @ 12.12 hrs, Volume= 0.177 af, Atten= 2%, Lag= 0.9 min

Routed to Reach AP3: Analysis Point 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.88 fps, Min. Travel Time= 1.1 min Avg. Velocity = 1.56 fps, Avg. Travel Time= 2.7 min

Peak Storage= 150 cf @ 12.12 hrs

Average Depth at Peak Storage= 0.15', Surface Width= 7.74' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 54.28 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 253.0' Slope= 0.0553 '/'

‡

Inlet Invert= 56.00', Outlet Invert= 42.00'

Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 4.00" for 10 Yr 24 Hr +15% event

Inflow = 2.38 cfs @ 12.10 hrs, Volume= 0.177 af

Outflow = 2.38 cfs @ 12.10 hrs, Volume= 0.177 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 4R: Flow over Sagamore Ave and Tidewatch Road

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.060 ac, 0.00% Impervious, Inflow Depth > 2.86" for 10 Yr 24 Hr +15% event

Inflow = 0.20 cfs @ 12.09 hrs, Volume= 0.014 af

Outflow = 0.20 cfs @ 12.09 hrs, Volume= 0.014 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 2R: Flow across Map 222 Lot 20

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.879 ac, 14.04% Impervious, Inflow Depth > 3.05" for 10 Yr 24 Hr +15% event

Inflow = 5.63 cfs @ 12.15 hrs, Volume= 0.477 af

Outflow = 5.63 cfs @ 12.15 hrs, Volume= 0.477 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.639 ac, 14.82% Impervious, Inflow Depth > 3.14" for 10 Yr 24 Hr +15% event

Inflow = 2.18 cfs @ 12.11 hrs, Volume= 0.167 af

Outflow = 2.18 cfs @ 12.11 hrs, Volume= 0.167 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S Runoff Area=20,592 sf 54.90% Impervious Runoff Depth>5.59"

Flow Length=187' Tc=6.0 min CN=87 Runoff=2.91 cfs 0.220 af

Subcatchment2S: Subcatchment2S Runoff Area=2,614 sf 0.00% Impervious Runoff Depth>4.14"

Flow Length=20' Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.29 cfs 0.021 af

Subcatchment3S: Subcatchment3S Runoff Area=58,629 sf 0.32% Impervious Runoff Depth>3.92"

Flow Length=447' Tc=11.9 min CN=72 Runoff=5.08 cfs 0.440 af

Subcatchment4S: Subcatchment4S Runoff Area=27,837 sf 14.82% Impervious Runoff Depth>4.47"

Flow Length=216' Tc=7.8 min CN=77 Runoff=3.10 cfs 0.238 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.04' Max Vel=0.90 fps Inflow=0.29 cfs 0.021 af

n=0.030 L=81.0' S=0.0494'/' Capacity=88.18 cfs Outflow=0.28 cfs 0.021 af

Reach 3R: Flow over Sagamore Ave Avg. Flow Depth=0.19' Max Vel=3.35 fps Inflow=3.19 cfs 0.241 af

n=0.016 L=101.0' S=0.0297'/' Capacity=39.77 cfs Outflow=3.19 cfs 0.241 af

Reach 4R: Flow over Sagamore Ave and Avg. Flow Depth=0.19' Max Vel=3.54 fps Inflow=3.19 cfs 0.241 af

 $n = 0.016 \quad L = 145.0' \quad S = 0.0345 \; \text{'/'} \quad Capacity = 42.85 \; \text{cfs} \quad Outflow = 3.18 \; \text{cfs} \quad 0.241 \; \text{af}$

Reach 5R: Flow over Tidewatch Road Avg. Flow Depth=0.17' Max Vel=4.19 fps Inflow=3.18 cfs 0.241 af

n=0.016 L=253.0' S=0.0553'/' Capacity=54.28 cfs Outflow=3.11 cfs 0.241 af

Reach AP1: Analysis Point 1 Inflow=3.19 cfs 0.241 af

Outflow=3.19 cfs 0.241 af

Reach AP2: Analysis Point 2 Inflow=0.29 cfs 0.021 af

Outflow=0.29 cfs 0.021 af

Reach AP3: Analysis Point 3 Inflow=8.00 cfs 0.681 af

Outflow=8.00 cfs 0.681 af

Reach AP4: Analysis Point 4 Inflow=3.10 cfs 0.238 af

Outflow=3.10 cfs 0.238 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.919 af Average Runoff Depth = 4.38" 85.76% Pervious = 2.159 ac 14.24% Impervious = 0.359 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S Runoff Area=20,592 sf 54.90% Impervious Runoff Depth>6.96"

Flow Length=187' Tc=6.0 min CN=87 Runoff=3.58 cfs 0.274 af

Subcatchment2S: Subcatchment2S Runoff Area=2,614 sf 0.00% Impervious Runoff Depth>5.40"

Flow Length=20' Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.37 cfs 0.027 af

Subcatchment3S: Subcatchment3S Runoff Area=58,629 sf 0.32% Impervious Runoff Depth>5.15"

Flow Length=447' Tc=11.9 min CN=72 Runoff=6.66 cfs 0.578 af

Subcatchment4S: Subcatchment4S Runoff Area=27,837 sf 14.82% Impervious Runoff Depth>5.76"

Flow Length=216' Tc=7.8 min CN=77 Runoff=3.97 cfs 0.307 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.04' Max Vel=0.98 fps Inflow=0.37 cfs 0.027 af

n=0.030 L=81.0' S=0.0494 '/' Capacity=88.18 cfs Outflow=0.36 cfs 0.027 af

Reach 3R: Flow over Sagamore Ave Avg. Flow Depth=0.21' Max Vel=3.54 fps Inflow=3.94 cfs 0.301 af

n=0.016 L=101.0' S=0.0297'/' Capacity=39.77 cfs Outflow=3.95 cfs 0.301 af

Reach 4R: Flow over Sagamore Ave and Avg. Flow Depth=0.20' Max Vel=3.74 fps Inflow=3.95 cfs 0.301 af

 $n = 0.016 \quad L = 145.0' \quad S = 0.0345 \; \text{'/'} \quad Capacity = 42.85 \; \text{cfs} \quad Outflow = 3.93 \; \text{cfs} \quad 0.301 \; \text{af}$

Reach 5R: Flow over Tidewatch Road Avg. Flow Depth=0.19' Max Vel=4.42 fps Inflow=3.93 cfs 0.301 af

n=0.016 L=253.0' S=0.0553 '/' Capacity=54.28 cfs Outflow=3.86 cfs 0.301 af

Reach AP1: Analysis Point 1 Inflow=3.95 cfs 0.301 af

Outflow=3.95 cfs 0.301 af

Reach AP2: Analysis Point 2 Inflow=0.37 cfs 0.027 af

Outflow=0.37 cfs 0.027 af

Reach AP3: Analysis Point 3 Inflow=10.27 cfs 0.879 af

Outflow=10.27 cfs 0.879 af

Reach AP4: Analysis Point 4 Inflow=3.97 cfs 0.307 af

Outflow=3.97 cfs 0.307 af

Total Runoff Area = 2.518 ac Runoff Volume = 1.186 af Average Runoff Depth = 5.65" 85.76% Pervious = 2.159 ac 14.24% Impervious = 0.359 ac

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 3.58 cfs @ 12.09 hrs, Volume= 0.274 af, Depth> 6.96"

Routed to Reach 3R: Flow over Sagamore Ave

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Α	rea (sf)	CN I	Description		
		2,869	98 I	Roofs, HSC	G C	
		8,436	98 I	Paved park	ing, HSG C	
		9,256	74 >	>75% Ġras	s cover, Go	ood, HSG C
_		31	70 \	Noods, Go	od, HSG C	
		20,592	87 \	Weighted A	verage	
		9,287	4	15.10% Pei	rvious Area	ľ
		11,305	į	54.90% lmp	pervious Ar	ea
	Тс	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.5	46	0.1090	0.31		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.1	4	0.0670	1.26		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.70"
	0.1	41	0.0670	5.25		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
	0.4	96	0.0360	3.85		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
	2.4	107	Total	laaraaaad t	a mainimatum	To = 6.0 min

3.1 187 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af, Depth> 5.40"

Routed to Reach AP2 : Analysis Point 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Α	rea (sf)	CN	Description						
		2,495	74	>75% Gras	s cover, Go	ood, HSG C				
		119	70	Woods, Go	od, HSG C					
		2,614	74	Weighted A	verage					
		2,614		100.00% P	ervious Are	a				
	Тс	Length	Slope	,	Capacity	Description				
_	(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)					
	1.3	20	0.1000	0.25		Sheet Flow,				
_						Grass: Short	n= 0.150	P2= 3.70"		

1.3 20 Total, Increased to minimum Tc = 6.0 min

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Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 6.66 cfs @ 12.17 hrs, Volume= 0.578 af, Depth> 5.15"

Routed to Reach AP3: Analysis Point 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Α	rea (sf)	CN E	escription		
		187		Roofs, HSC		
		9,391				ood, HSG C
*		46,312		,	od, HSG C	
_		2,739		edge, HS0		
		58,629		Veighted A		
		58,442			vious Area	
		187	0	.32% Impe	ervious Are	a
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Boompaon
_	8.6	50	0.0415	0.10	(0.0)	Sheet Flow,
	0.0	50	0.0410	0.10		Woods: Light underbrush n= 0.400 P2= 3.70"
	0.7	62	0.0968	1.56		Shallow Concentrated Flow,
	0.7	02	0.0000	1.00		Woodland Kv= 5.0 fps
	0.7	54	0.0741	1.36		Shallow Concentrated Flow,
	0	٠.	0.01			Woodland Kv= 5.0 fps
	1.3	122	0.1000	1.58		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.6	159	0.0189	4.55	18.20	Trap/Vee/Rect Channel Flow,
						Bot.W=1.00' D=1.00' Z= 3.0 '/' Top.W=7.00'
						n= 0.030 Short grass
	11 9	447	Total			<u> </u>

11.9 447 Total

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 3.97 cfs @ 12.11 hrs, Volume= 0.307 af, Depth> 5.76"

Routed to Reach AP4: Analysis Point 4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Area (sf)	CN	Description					
	2,555	98	Roofs, HSG C					
	1,571	98	Paved parking, HSG C					
	5,912	74	75% Grass cover, Good, HSG C					
	15,194	70	Voods, Good, HSG C					
*	2,605	96	Ledge, HSG C					
	27,837	77	Weighted Average					
	23,711		85.18% Pervious Area					
	4,126		14.82% Impervious Area					

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.9	14	0.0210	0.13		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	4.2	36	0.1280	0.14		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	0.5	50	0.1280	1.79		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	1.0	87	0.0800	1.41		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.2	29	0.2860	2.67		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	7.8	216	Total	·		

Summary for Reach 2R: Flow across Map 222 Lot 20

Inflow Area = 0.060 ac, 0.00% Impervious, Inflow Depth > 5.40" for 50 Yr 24 Hr +15% event

Inflow = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af

Outflow = 0.36 cfs @ 12.11 hrs, Volume= 0.027 af, Atten= 2%, Lag= 1.0 min

Routed to Reach 3R: Flow over Sagamore Ave

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.98 fps, Min. Travel Time= 1.4 min Avg. Velocity = 0.35 fps, Avg. Travel Time= 3.9 min

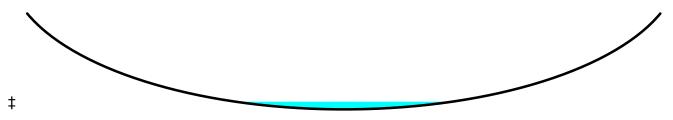
Peak Storage= 30 cf @ 12.11 hrs

Average Depth at Peak Storage= 0.04', Surface Width= 14.09' Bank-Full Depth= 0.50' Flow Area= 16.7 sf, Capacity= 88.18 cfs

50.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight

Length= 81.0' Slope= 0.0494 '/'

Inlet Invert= 66.00', Outlet Invert= 62.00'



Summary for Reach 3R: Flow over Sagamore Ave

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[62] Hint: Exceeded Reach 2R OUTLET depth by 2.17' @ 12.10 hrs

[64] Warning: Exceeded Reach 2R outlet bank by 1.71' @ 12.10 hrs

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 6.78" for 50 Yr 24 Hr +15% event

Inflow = 3.94 cfs @ 12.09 hrs, Volume= 0.301 af

Outflow = 3.95 cfs @ 12.10 hrs, Volume= 0.301 af, Atten= 0%, Lag= 0.4 min

Routed to Reach AP1: Analysis Point 1

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.54 fps, Min. Travel Time= 0.5 min

Avg. Velocity = 1.38 fps, Avg. Travel Time= 1.2 min

Peak Storage= 113 cf @ 12.10 hrs

Average Depth at Peak Storage= 0.21', Surface Width= 10.62' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 39.77 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25' Length= 101.0' Slope= 0.0297 '/'

Inlet Invert= 64.00', Outlet Invert= 61.00'

‡

Summary for Reach 4R: Flow over Sagamore Ave and Tidewatch Road

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 6.78" for 50 Yr 24 Hr +15% event

Inflow = 3.95 cfs @ 12.10 hrs, Volume= 0.301 af

Outflow = 3.93 cfs @ 12.10 hrs, Volume= 0.301 af, Atten= 0%, Lag= 0.5 min

Routed to Reach 5R: Flow over Tidewatch Road

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.74 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.46 fps, Avg. Travel Time= 1.7 min

Peak Storage= 153 cf @ 12.10 hrs

Average Depth at Peak Storage= 0.20', Surface Width= 10.31' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 42.85 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 145.0' Slope= 0.0345 '/'

Inlet Invert= 61.00', Outlet Invert= 56.00'

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Summary for Reach 5R: Flow over Tidewatch Road

[61] Hint: Exceeded Reach 4R outlet invert by 0.18' @ 12.10 hrs

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 6.78" for 50 Yr 24 Hr +15% event

Inflow = 3.93 cfs @ 12.10 hrs, Volume= 0.301 af

Outflow = 3.86 cfs @ 12.12 hrs, Volume= 0.301 af, Atten= 2%, Lag= 0.8 min

Routed to Reach AP3: Analysis Point 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 4.42 fps, Min. Travel Time= 1.0 min Avg. Velocity = 1.74 fps, Avg. Travel Time= 2.4 min

Peak Storage= 220 cf @ 12.12 hrs

Average Depth at Peak Storage= 0.19', Surface Width= 9.38' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 54.28 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 253.0' Slope= 0.0553 '/'

Inlet Invert= 56.00', Outlet Invert= 42.00'

‡

Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 6.78" for 50 Yr 24 Hr +15% event

Inflow = 3.95 cfs @ 12.10 hrs, Volume= 0.301 af

Outflow = 3.95 cfs @ 12.10 hrs, Volume= 0.301 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 4R: Flow over Sagamore Ave and Tidewatch Road

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.060 ac, 0.00% Impervious, Inflow Depth > 5.40" for 50 Yr 24 Hr +15% event

Inflow = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af

Outflow = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 2R: Flow across Map 222 Lot 20

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.879 ac, 14.04% Impervious, Inflow Depth > 5.61" for 50 Yr 24 Hr +15% event

Inflow = 10.27 cfs @ 12.15 hrs, Volume= 0.879 af

Outflow = 10.27 cfs @ 12.15 hrs, Volume= 0.879 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.639 ac, 14.82% Impervious, Inflow Depth > 5.76" for 50 Yr 24 Hr +15% event

Inflow = 3.97 cfs @ 12.11 hrs, Volume= 0.307 af

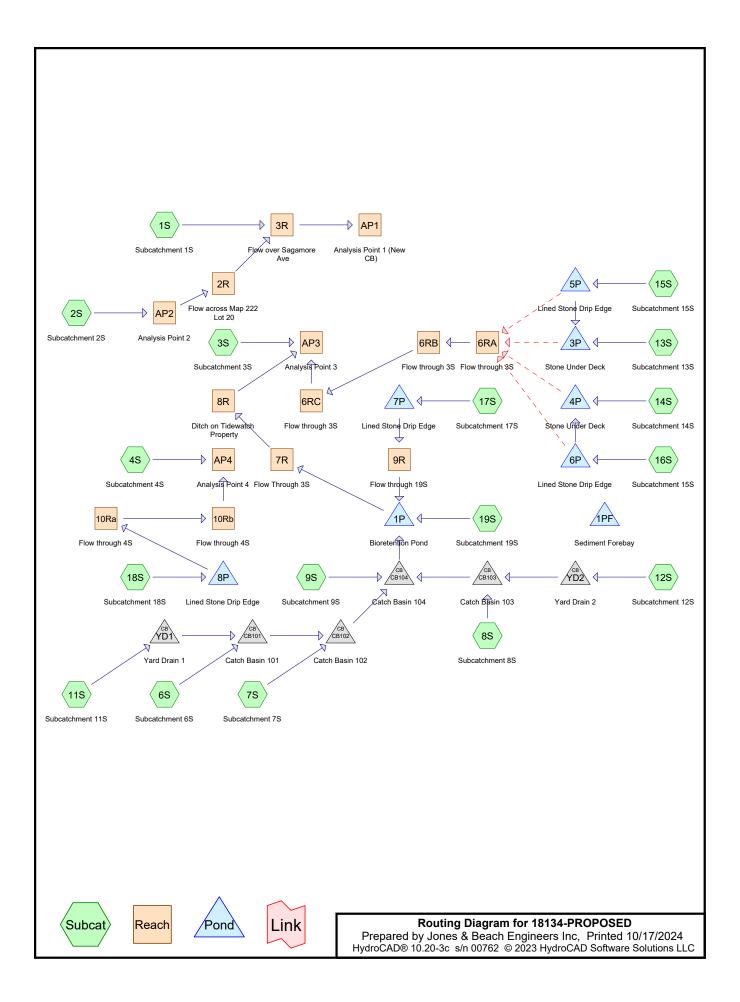
Outflow = 3.97 cfs @ 12.11 hrs, Volume= 0.307 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

APPENDIX II

PROPOSED CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Complete 10 YEAR Summary 25 YEAR Complete 50 YEAR



18134-PROPOSED

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Area Listing (all nodes)

Area	CN	Description	
(acres)		(subcatchment-numbers)	
1.067	74	>75% Grass cover, Good, HSG C (1S, 2S, 3S, 4S, 11S, 12S, 19S)	
0.071	96	Ledge, HSG C (3S, 4S)	
0.287	98	Paved parking, HSG C (1S, 6S, 7S, 8S, 9S, 11S, 19S)	
0.241	98	Roofs, HSG C (1S, 4S, 8S, 11S, 12S, 13S, 14S, 15S, 16S, 17S, 18S, 19S)	
0.017	98	Water Surface, 0% imp, HSG C (15S, 16S, 17S, 18S)	
0.835	70	Woods, Good, HSG C (3S, 4S)	
2.518	78	TOTAL AREA	

18134-PROPOSED

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Soil Listing (all nodes)

Area	Soil	Subcatchment
 (acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
2.518	HSG C	1S, 2S, 3S, 4S, 6S, 7S, 8S, 9S, 11S, 12S, 13S, 14S, 15S, 16S, 17S, 18S, 19S
0.000	HSG D	
0.000	Other	
2.518		TOTAL AREA

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=16,321 sf 51.36% Impervious Runoff Depth>2.27" Flow Length=186' Tc=6.0 min CN=86 Runoff=0.98 cfs 0.071 af
Subcatchment2S: Subcatchment2S Flow Length=20'	Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>1.38" Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.06 cfs 0.005 af
Subcatchment3S: Subcatchment3S	Runoff Area=44,463 sf 0.00% Impervious Runoff Depth>1.25" low Length=447' Tc=11.9 min CN=72 Runoff=1.16 cfs 0.106 af
Subcatchment4S: Subcatchment4S	Runoff Area=20,212 sf 5.43% Impervious Runoff Depth>1.51" Flow Length=216' Tc=7.8 min CN=76 Runoff=0.75 cfs 0.058 af
Subcatchment6S: Subcatchment6S	Runoff Area=1,084 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af
Subcatchment7S: Subcatchment7S	Runoff Area=954 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.08 cfs 0.006 af
Subcatchment8S: Subcatchment8S	Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.24 cfs 0.020 af
Subcatchment9S: Subcatchment9S	Runoff Area=325 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.03 cfs 0.002 af
Subcatchment11S: Subcatchment11S Flow Length=77'	Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>2.27" Slope=0.0396 '/' Tc=6.0 min CN=86 Runoff=0.27 cfs 0.020 af
Subcatchment12S: Subcatchment12S Flow Length=50'	Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>1.95" Slope=0.0320 '/' Tc=6.0 min CN=82 Runoff=0.19 cfs 0.014 af
Subcatchment13S: Subcatchment13S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment14S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment15S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment16S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment17S: Subcatchment17S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment18S: Subcatchment18S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af

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Subcatchment19S: Subcatchment19SRunoff Area=9,042 sf 12.11% Impervious Runoff Depth>1.58"

Flow Length=58' Tc=6.0 min CN=77 Runoff=0.37 cfs 0.027 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.02' Max Vel=0.56 fps Inflow=0.06 cfs 0.005 af n=0.030 L=81.0' S=0.0494 '/' Capacity=88.18 cfs Outflow=0.06 cfs 0.005 af

Reach 3R: Flow over Sagamore AveAvg. Flow Depth=0.12' Max Vel=2.94 fps Inflow=1.03 cfs 0.076 af n=0.016 L=45.0' S=0.0444 '/' Capacity=48.65 cfs Outflow=1.03 cfs 0.076 af

Reach 6RA: Flow through 3SAvg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af n=0.030 L=35.0' S=0.3429 '/' Capacity=464.76 cfs Outflow=0.00 cfs 0.000 af

Reach 6RB: Flow through 3SAvg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af n=0.030 L=39.0' S=0.1026 '/' Capacity=127.08 cfs Outflow=0.00 cfs 0.000 af

Reach 6RC: Flow through 3SAvg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af n=0.030 L=45.0' S=0.2667 '/' Capacity=409.88 cfs Outflow=0.00 cfs 0.000 af

Reach 7R: Flow Through 3SAvg. Flow Depth=0.12' Max Vel=3.30 fps Inflow=1.30 cfs 0.102 af n=0.030 L=220.0' S=0.0909 '/' Capacity=66.79 cfs Outflow=1.30 cfs 0.101 af

Reach 8R: Ditch on Tidewatch Property Avg. Flow Depth=0.30' Max Vel=2.28 fps Inflow=1.30 cfs 0.101 af n=0.030 L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=1.28 cfs 0.101 af

Reach 9R: Flow through 19SAvg. Flow Depth=0.03' Max Vel=0.61 fps Inflow=0.06 cfs 0.005 af n=0.030 L=39.0' S=0.0205 '/' Capacity=16.36 cfs Outflow=0.06 cfs 0.005 af

Reach 10Ra: Flow through 4SAvg. Flow Depth=0.00' Max Vel=0.83 fps Inflow=0.06 cfs 0.005 af n=0.030 L=18.0' S=0.3333 '/' Capacity=199.20 cfs Outflow=0.06 cfs 0.005 af

Reach 10Rb: Flow through 4SAvg. Flow Depth=0.00' Max Vel=0.70 fps Inflow=0.06 cfs 0.005 af n=0.030 L=51.0' S=0.2353 '/' Capacity=167.36 cfs Outflow=0.06 cfs 0.005 af

Reach AP1: Analysis Point 1 (New CB)

Inflow=1.03 cfs 0.076 af
Outflow=1.03 cfs 0.076 af

Reach AP2: Analysis Point 2 Inflow=0.06 cfs 0.005 af Outflow=0.06 cfs 0.005 af

Reach AP3: Analysis Point 3 Inflow=2.40 cfs 0.208 af
Outflow=2.40 cfs 0.208 af

Reach AP4: Analysis Point 4 Inflow=0.81 cfs 0.064 af
Outflow=0.81 cfs 0.064 af

Pond 1P: Bioretention Pond

Peak Elev=60.50' Storage=72 cf Inflow=1.33 cfs 0.102 af

Outflow=1.30 cfs 0.102 af

Pond 1PF: Sediment Forebay Peak Elev=0.00' Storage=0 cf

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Pond 3P: Stone Under Deck Peak Elev=63.57' Storage=0.005 af Inflow=0.11 cfs 0.009 af

Discarded=0.01 cfs 0.007 af Secondary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.007 af

Pond 4P: Stone Under Deck Peak Elev=63.19' Storage=0.002 af Inflow=0.11 cfs 0.009 af

Discarded=0.04 cfs 0.009 af Secondary=0.00 cfs 0.000 af Outflow=0.04 cfs 0.009 af

Pond 5P: Lined Stone Drip Edge Peak Elev=66.05' Storage=0.000 af Inflow=0.06 cfs 0.005 af

Primary=0.06 cfs 0.005 af Secondary=0.00 cfs 0.000 af Outflow=0.06 cfs 0.005 af

Pond 6P: Lined Stone Drip Edge Peak Elev=66.05' Storage=0.000 af Inflow=0.06 cfs 0.005 af

Primary=0.06 cfs 0.005 af Secondary=0.00 cfs 0.000 af Outflow=0.06 cfs 0.005 af

Pond 7P: Lined Stone Drip Edge Peak Elev=64.16' Storage=0.000 af Inflow=0.06 cfs 0.005 af

Outflow=0.06 cfs 0.005 af

Pond 8P: Lined Stone Drip Edge Peak Elev=64.66' Storage=0.000 af Inflow=0.06 cfs 0.005 af

Outflow=0.06 cfs 0.005 af

Pond CB101: Catch Basin 101 Peak Elev=66.97' Inflow=0.36 cfs 0.027 af

12.0" Round Culvert n=0.012 L=14.0' S=0.0071'/' Outflow=0.36 cfs 0.027 af

Pond CB102: Catch Basin 102 Peak Elev=66.80' Inflow=0.44 cfs 0.033 af

12.0" Round Culvert n=0.012 L=84.0' S=0.0060 '/' Outflow=0.44 cfs 0.033 af

Pond CB103: Catch Basin 103 Peak Elev=67.97' Inflow=0.43 cfs 0.034 af

12.0" Round Culvert n=0.012 L=42.0' S=0.0071'/' Outflow=0.43 cfs 0.034 af

Pond CB104: Catch Basin 104 Peak Elev=66.37' Inflow=0.90 cfs 0.069 af

12.0" Round Culvert n=0.012 L=31.0' S=0.0065 '/' Outflow=0.90 cfs 0.069 af

Pond YD1: Yard Drain 1 Peak Elev=67.64' Inflow=0.27 cfs 0.020 af

8.0" Round Culvert n=0.012 L=15.0' S=0.0247 '/' Outflow=0.27 cfs 0.020 af

Pond YD2: Yard Drain 2 Peak Elev=68.48' Inflow=0.19 cfs 0.014 af

8.0" Round Culvert n=0.012 L=13.0' S=0.0208 '/' Outflow=0.19 cfs 0.014 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.365 af Average Runoff Depth = 1.74" 79.02% Pervious = 1.990 ac 20.98% Impervious = 0.528 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=16,321 sf 51.36% Impervious Runoff Depth>4.04" Flow Length=186' Tc=6.0 min CN=86 Runoff=1.70 cfs 0.126 af
Subcatchment2S: Subcatchment2S Flow Length=20'	Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>2.86" Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.13 cfs 0.009 af
Subcatchment3S: Subcatchment3S	Runoff Area=44,463 sf 0.00% Impervious Runoff Depth>2.67" low Length=447' Tc=11.9 min CN=72 Runoff=2.61 cfs 0.227 af
Subcatchment4S: Subcatchment4S	Runoff Area=20,212 sf 5.43% Impervious Runoff Depth>3.04" Flow Length=216' Tc=7.8 min CN=76 Runoff=1.54 cfs 0.118 af
Subcatchment6S: Subcatchment6S	Runoff Area=1,084 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.13 cfs 0.011 af
Subcatchment7S: Subcatchment7S	Runoff Area=954 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.12 cfs 0.010 af
Subcatchment8S: Subcatchment8S	Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.37 cfs 0.031 af
Subcatchment9S: Subcatchment9S	Runoff Area=325 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.04 cfs 0.003 af
Subcatchment11S: Subcatchment11S Flow Length=77'	Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>4.04" Slope=0.0396 '/' Tc=6.0 min CN=86 Runoff=0.48 cfs 0.035 af
Subcatchment12S: Subcatchment12S Flow Length=50'	Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>3.63" Slope=0.0320 '/' Tc=6.0 min CN=82 Runoff=0.35 cfs 0.026 af
Subcatchment13S: Subcatchment13S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment14S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment15S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af
Subcatchment16S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af
Subcatchment17S: Subcatchment17S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af
Subcatchment18S: Subcatchment18S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af

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Subcatchment19S: Subcatchment19SRunoff Area=9,042 sf 12.11% Impervious Runoff Depth>3.14"

Flow Length=58' Tc=6.0 min CN=77 Runoff=0.75 cfs 0.054 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.02' Max Vel=0.70 fps Inflow=0.13 cfs 0.009 af n=0.030 L=81.0' S=0.0494 '/' Capacity=88.18 cfs Outflow=0.13 cfs 0.009 af

Reach 3R: Flow over Sagamore Ave Avg. Flow Depth=0.15' Max Vel=3.39 fps Inflow=1.82 cfs 0.135 af n=0.016 L=45.0' S=0.0444 '/' Capacity=48.65 cfs Outflow=1.83 cfs 0.135 af

Reach 6RA: Flow through 3SAvg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af n=0.030 L=35.0' S=0.3429 '/' Capacity=464.76 cfs Outflow=0.00 cfs 0.000 af

Reach 6RB: Flow through 3SAvg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af n=0.030 L=39.0' S=0.1026 '/' Capacity=127.08 cfs Outflow=0.00 cfs 0.000 af

Reach 6RC: Flow through 3SAvg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af n=0.030 L=45.0' S=0.2667 '/' Capacity=409.88 cfs Outflow=0.00 cfs 0.000 af

Reach 7R: Flow Through 3SAvg. Flow Depth=0.13' Max Vel=3.52 fps Inflow=1.53 cfs 0.178 af n=0.030 L=220.0' S=0.0909 '/' Capacity=66.79 cfs Outflow=1.53 cfs 0.178 af

Reach 8R: Ditch on Tidewatch Property Avg. Flow Depth=0.32' Max Vel=2.40 fps Inflow=1.53 cfs 0.178 af n=0.030 L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=1.53 cfs 0.178 af

Reach 9R: Flow through 19SAvg. Flow Depth=0.04' Max Vel=0.71 fps Inflow=0.09 cfs 0.008 af n=0.030 L=39.0' S=0.0205 '/' Capacity=16.36 cfs Outflow=0.09 cfs 0.008 af

Reach 10Ra: Flow through 4SAvg. Flow Depth=0.01' Max Vel=0.89 fps Inflow=0.09 cfs 0.008 af n=0.030 L=18.0' S=0.3333 '/' Capacity=199.20 cfs Outflow=0.09 cfs 0.008 af

Reach 10Rb: Flow through 4SAvg. Flow Depth=0.01' Max Vel=0.80 fps Inflow=0.09 cfs 0.008 af n=0.030 L=51.0' S=0.2353 '/' Capacity=167.36 cfs Outflow=0.09 cfs 0.008 af

Reach AP1: Analysis Point 1 (New CB)

Inflow=1.83 cfs 0.135 af
Outflow=1.83 cfs 0.135 af

Reach AP2: Analysis Point 2 Inflow=0.13 cfs 0.009 af Outflow=0.13 cfs 0.009 af

Reach AP3: Analysis Point 3 Inflow=4.12 cfs 0.405 af
Outflow=4.12 cfs 0.405 af

Reach AP4: Analysis Point 4 Inflow=1.63 cfs 0.126 af
Outflow=1.63 cfs 0.126 af

Pond 1P: Bioretention Pond

Peak Elev=61.22' Storage=411 cf Inflow=2.33 cfs 0.179 af

Outflow=1.53 cfs 0.178 af

Pond 1PF: Sediment Forebay Peak Elev=0.00' Storage=0 cf

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Pond 3P: Stone Under Deck Peak Elev=64.72' Storage=0.008 af Inflow=0.17 cfs 0.014 af Discarded=0.01 cfs 0.010 af Secondary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.010 af

Pond 4P: Stone Under Deck Peak Elev=63.65' Storage=0.003 af Inflow=0.17 cfs 0.014 af

Discarded=0.06 cfs 0.014 af Secondary=0.00 cfs 0.000 af Outflow=0.06 cfs 0.014 af

Pond 5P: Lined Stone Drip Edge Peak Elev=66.07' Storage=0.000 af Inflow=0.10 cfs 0.008 af

Primary=0.10 cfs 0.008 af Secondary=0.00 cfs 0.000 af Outflow=0.10 cfs 0.008 af

Pond 6P: Lined Stone Drip Edge Peak Elev=66.07' Storage=0.000 af Inflow=0.10 cfs 0.008 af

Primary=0.10 cfs 0.008 af Secondary=0.00 cfs 0.000 af Outflow=0.10 cfs 0.008 af

Pond 7P: Lined Stone Drip Edge Peak Elev=64.21' Storage=0.000 af Inflow=0.10 cfs 0.008 af

Outflow=0.09 cfs 0.008 af

Pond 8P: Lined Stone Drip Edge Peak Elev=64.71' Storage=0.000 af Inflow=0.10 cfs 0.008 af

Outflow=0.09 cfs 0.008 af

Pond CB101: Catch Basin 101 Peak Elev=67.13' Inflow=0.61 cfs 0.046 af

12.0" Round Culvert n=0.012 L=14.0' S=0.0071 '/' Outflow=0.61 cfs 0.046 af

Pond CB102: Catch Basin 102 Peak Elev=66.96' Inflow=0.73 cfs 0.056 af

12.0" Round Culvert n=0.012 L=84.0' S=0.0060 '/' Outflow=0.73 cfs 0.056 af

Pond CB103: Catch Basin 103 Peak Elev=68.09' Inflow=0.73 cfs 0.057 af

12.0" Round Culvert n=0.012 L=42.0' S=0.0071'/' Outflow=0.73 cfs 0.057 af

Pond CB104: Catch Basin 104 Peak Elev=66.58' Inflow=1.49 cfs 0.116 af

12.0" Round Culvert n=0.012 L=31.0' S=0.0065 '/' Outflow=1.49 cfs 0.116 af

Pond YD1: Yard Drain 1 Peak Elev=67.77' Inflow=0.48 cfs 0.035 af

8.0" Round Culvert n=0.012 L=15.0' S=0.0247 '/' Outflow=0.48 cfs 0.035 af

Pond YD2: Yard Drain 2 Peak Elev=68.59' Inflow=0.35 cfs 0.026 af

8.0" Round Culvert n=0.012 L=13.0' S=0.0208 '/' Outflow=0.35 cfs 0.026 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.695 af Average Runoff Depth = 3.31" 79.02% Pervious = 1.990 ac 20.98% Impervious = 0.528 ac

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff 1.70 cfs @ 12.09 hrs, Volume= 0.126 af, Depth> 4.04"

Routed to Reach 3R: Flow over Sagamore Ave

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

_	Α	rea (sf)	CN	Description						
		6,930	98	98 Paved parking, HSG C						
		7,938	74	>75% Ġras	s cover, Go	ood, HSG C				
		1,453								
16,321 86 Weighted Average										
		7,938		48.64% Pe	rvious Area					
		8,383	;	51.36% Imp	pervious Ar	ea				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	2.5	50	0.1250	0.33		Sheet Flow,				
						Grass: Short n= 0.150 P2= 3.70"				
	0.0	6	0.1250	2.47		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.3	30	0.0670	1.81		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.4	100	0.0360	3.85		Shallow Concentrated Flow,				
_						Paved Kv= 20.3 fps				
	3.2	186	Total,	Increased t	to minimum	Tc = 6.0 min				

Summary for Subcatchment 2S: Subcatchment 2S

Runoff 0.13 cfs @ 12.09 hrs, Volume= 0.009 af, Depth> 2.86"

Routed to Reach AP2 : Analysis Point 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Aı	rea (sf)	CN	Description						
		1,728	74	74 >75% Grass cover, Good, HSG C						
		1,728		100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	Description				
	1.3	20	0.1000	0.25		Sheet Flow,				
_						Grass: Short	n= 0.150	P2= 3.70"		
	4.0	00	T . 4 . 1	1		T				

1.3 20 Total, Increased to minimum Tc = 6.0 min Prepared by Jones & Beach Engineers Inc HydroCAD® 10.20-3c s/n 00762 © 2023 HydroCAD Software Solutions LLC Printed 10/17/2024

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Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 2.61 cfs @ 12.17 hrs, Volume= 0.227 af, Depth> 2.67"

Routed to Reach AP3: Analysis Point 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Α	rea (sf)	CN D	escription							
		14,740									
		28,306		•	•						
*		1,417	96 L	edge, HSC	3 C						
		44,463		Veighted A							
		44,463	1	00.00% Pe	ervious Are	a					
	_		01		0 "	D					
/	Tc	Length	Slope	•	Capacity	Description					
<u>(r</u>	nin)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	8.6	50	0.0415	0.10		Sheet Flow,					
						Woods: Light underbrush n= 0.400 P2= 3.70"					
	0.7	62	0.0968	1.56		Shallow Concentrated Flow,					
						Woodland Kv= 5.0 fps					
	0.7	54	0.0741	1.36		Shallow Concentrated Flow,					
						Woodland Kv= 5.0 fps					
	1.3	122	0.1000	1.58		Shallow Concentrated Flow,					
						Woodland Kv= 5.0 fps					
	0.6	159	0.0189	4.55	18.20	Trap/Vee/Rect Channel Flow,					
						Bot.W=1.00' D=1.00' Z= 3.0 '/' Top.W=7.00'					
						n= 0.030 Short grass					
1	11.9	447	Total								

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 1.54 cfs @ 12.11 hrs, Volume= 0.118 af, Depth> 3.04"

Routed to Reach AP4: Analysis Point 4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Area (sf)	CN	Description			
	9,377	74	75% Grass cover, Good, HSG C			
	8,075	70	Woods, Good, HSG C			
	1,097	98	Roofs, HSG C			
*	1,663	96	Ledge, HSG C			
	20,212	76	Weighted Average			
	19,115	· · · · · · · · · · · · · · · · · · ·				
	1,097		5.43% Impervious Area			

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.9	14	0.0210	0.13		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	4.2	36	0.1280	0.14		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	0.5	50	0.1280	1.79		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	1.0	87	0.0800	1.41		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.2	29	0.2860	2.67		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	7.8	216	Total			

Summary for Subcatchment 6S: Subcatchment 6S

Runoff = 0.13 cfs @ 12.09 hrs, Volume=

0.011 af, Depth> 5.37"

Routed to Pond CB101: Catch Basin 101

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

_	Α	rea (sf)	CN I	Description					
		1,084	98 I	Paved parking, HSG C					
		1,084	•	100.00% Impervious Area					
	To	Longth	Slope	Volocity	Canacity	Description			
	(min)	Length (feet)	(ft/ft)	(ft/sec)	(cfs)	Description			
_	6.0			,	, ,	Direct Entry.			

Summary for Subcatchment 7S: Subcatchment 7S

Runoff = 0.12 cfs @ 12.09 hrs, Volume=

0.010 af, Depth> 5.37"

Routed to Pond CB102: Catch Basin 102

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN [CN Description					
	954	98 F	98 Paved parking, HSG C					
	954	1	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

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Summary for Subcatchment 8S: Subcatchment 8S

Runoff = 0.37 cfs @ 12.09 hrs, Volume=

0.031 af, Depth> 5.37"

Routed to Pond CB103: Catch Basin 103

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN	Description		
	2,554	98	Paved park	ing, HSG C	
	457	98	Roofs, HSC	S Č	
	3,011	98	Weighted A	verage	
	3,011		100.00% Im	npervious A	Area
Тс	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/fi	(ft/sec)	(cfs)	
6.0					Direct Entry,

Summary for Subcatchment 9S: Subcatchment 9S

Runoff = 0.04 cfs @ 12.09 hrs, Volume=

0.003 af, Depth> 5.37"

Routed to Pond CB104: Catch Basin 104

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN [Description					
	325	98 F	Paved parking, HSG C					
	325	1	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

Summary for Subcatchment 11S: Subcatchment 11S

Runoff = 0.48 cfs @ 12.09 hrs, Volume= 0.035 af, Depth> 4.04"

Routed to Pond YD1: Yard Drain 1

Area (sf)	CN	Description				
1,998	98	Roofs, HSG C				
2,312	74	>75% Grass cover, Good, HSG C				
261	98	Paved parking, HSG C				
4,571	86	Weighted Average				
2,312		50.58% Pervious Area				
2,259		49.42% Impervious Area				

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	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	4.0	50	0.0396	0.21		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.3	27	0.0396	1.39		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	4.0	77	T.4.1 L			T. 0.0 mile

4.3 77 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 12S: Subcatchment 12S

Runoff 0.35 cfs @ 12.09 hrs, Volume= 0.026 af, Depth> 3.63"

Routed to Pond YD2: Yard Drain 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN I	Description						
	1,318	98 I	Roofs, HSG	G C					
	2,416	74 :	>75% Gras	s cover, Go	ood, HSG C				
	3,734	82 \	Weighted A	verage					
	2,416	(64.70% Per	vious Area					
	1,318	;	35.30% Imp	ervious Ar	ea				
Tc	Length	Slope	•	Capacity	Description				
(min)_	(feet)	(ft/ft)	(ft/sec)	(cfs)					
4.3	50	0.0320	0.19		Sheet Flow,				
					Grass: Short	n= 0.150	P2= 3.70"		
4.3	50	Total,	Increased t	o minimum	Tc = 6.0 min			•	

Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 13S: Subcatchment 13S

0.07 cfs @ 12.09 hrs, Volume=

0.006 af, Depth> 5.37"

Routed to Pond 3P: Stone Under Deck

A	rea (sf)	CN [Description		
	560	98 F	Roofs, HSG	G C	
	560	1	00.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

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Summary for Subcatchment 14S: Subcatchment 14S

Runoff = 0.07 cfs @ 12.09 hrs, Volume=

0.006 af, Depth> 5.37"

Routed to Pond 4P: Stone Under Deck

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

_	Α	rea (sf)	CN [Description					
		560	98 F	Roofs, HSG C					
		560	•	100.00% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	6.0	-				Direct Entry,			

Summary for Subcatchment 15S: Subcatchment 15S

Runoff = 0.10 cfs @ 12.09 hrs, Volume=

0.008 af, Depth> 5.37"

Routed to Pond 5P: Lined Stone Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN	Description				
	590	98	Roofs, HSC	G C			
	189	98	Water Surfa	ace, 0% im	np, HSG C		
	779	98	Weighted A	verage			
	189		24.26% Pervious Area				
	590		75.74% lmp	pervious Ar	rea		
Tc	Length	Slope	,	Capacity	·		
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)			
6.0					Direct Entry,		

Summary for Subcatchment 16S: Subcatchment 15S

Runoff = 0.10 cfs @ 12.09 hrs, Volume= 0.

0.008 af, Depth> 5.37"

Routed to Pond 6P: Lined Stone Drip Edge

 Area (sf)	CN	Description				
590	98	Roofs, HSG C				
 189	98	Water Surface, 0% imp, HSG C				
 779	98	Weighted Average				
189		24.26% Pervious Area				
590		75.74% Impervious Area				

Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

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Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	•	
6.0					Direct Entry,	

Summary for Subcatchment 17S: Subcatchment 17S

0.10 cfs @ 12.09 hrs, Volume=

0.008 af, Depth> 5.37"

Routed to Pond 7P: Lined Stone Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Area (sf)	CN	Description						
	590	98	Roofs, HSC	G C					
	189	98	Water Surfa	ace, 0% imp	np, HSG C				
	779	98	Weighted A	verage					
	189		24.26% Pe	rvious Area	a				
	590		75.74% lm	pervious Ar	rea				
_									
To	9	Slope	,	Capacity	·				
(min) (feet)	(ft/ft	(ft/sec)	(cfs)					
6.0)				Direct Entry,				

Direct Entry,

Summary for Subcatchment 18S: Subcatchment 18S

Runoff 0.10 cfs @ 12.09 hrs, Volume= 0.008 af, Depth> 5.37"

Routed to Pond 8P: Lined Stone Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN	Description					
_	590	98	Roofs, HSC	S C				
	189	98	Water Surfa	ace, 0% imp	ıp, HSG C			
	779	98	Weighted A	verage				
	189		24.26% Pei	rvious Area	a			
	590		75.74% lmp	pervious Ar	rea			
Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	Description			
6.0					Direct Entry,			

Summary for Subcatchment 19S: Subcatchment 19S

Runoff 0.75 cfs @ 12.09 hrs, Volume= 0.054 af, Depth> 3.14"

Routed to Pond 1P: Bioretention Pond

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A	rea (sf)	CN D	escription		
	7,947	74 >75% Grass cover, Go			ood, HSG C
	695	98 F	Roofs, HSG	G C	
	400	98 F	aved park	ing, HSG C	
	9,042	77 V	Veighted A	verage	
	7,947	8	7.89% Per	vious Area	l
	1,095	1	2.11% Imp	pervious Ar	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.5	43	0.0930	0.29		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
0.4	7	0.3333	0.33		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
0.0	8	0.3333	4.04		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
2.9	58	Total, I	ncreased t	o minimum	n Tc = 6.0 min

Summary for Reach 2R: Flow across Map 222 Lot 20

Inflow Area = 0.040 ac, 0.00% Impervious, Inflow Depth > 2.86" for 10 Yr 24 Hr +15% event

Inflow = 0.13 cfs @ 12.09 hrs, Volume= 0.009 af

Outflow = 0.13 cfs @ 12.12 hrs, Volume= 0.009 af, Atten= 4%, Lag= 1.4 min

Routed to Reach 3R: Flow over Sagamore Ave

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.70 fps, Min. Travel Time= 1.9 min Avg. Velocity = 0.28 fps, Avg. Travel Time= 4.8 min

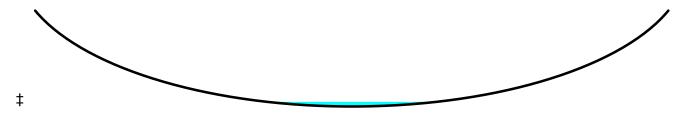
Peak Storage= 14 cf @ 12.12 hrs

Average Depth at Peak Storage= 0.02', Surface Width= 11.00' Bank-Full Depth= 0.50' Flow Area= 16.7 sf, Capacity= 88.18 cfs

50.00' x 0.50' deep Parabolic Channel, n= 0.030 Short grass

Length= 81.0' Slope= 0.0494 '/'

Inlet Invert= 66.00', Outlet Invert= 62.00'



Summary for Reach 3R: Flow over Sagamore Ave

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[62] Hint: Exceeded Reach 2R OUTLET depth by 1.12' @ 12.10 hrs

[64] Warning: Exceeded Reach 2R outlet bank by 0.65' @ 12.09 hrs

Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

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Inflow Area = 0.414 ac, 46.45% Impervious, Inflow Depth > 3.92" for 10 Yr 24 Hr +15% event

Inflow = 1.82 cfs @ 12.09 hrs, Volume= 0.135 af

Outflow = 1.83 cfs @ 12.09 hrs, Volume= 0.135 af, Atten= 0%, Lag= 0.2 min

Routed to Reach AP1: Analysis Point 1 (New CB)

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.39 fps, Min. Travel Time= 0.2 min Avg. Velocity = 1.35 fps, Avg. Travel Time= 0.6 min

Peak Storage= 24 cf @ 12.09 hrs

Average Depth at Peak Storage= 0.15', Surface Width= 7.37' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 48.65 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough

Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 45.0' Slope= 0.0444 '/'

‡

Inlet Invert= 63.00', Outlet Invert= 61.00'

Summary for Reach 6RA: Flow through 3S

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 6RB: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 0.50' Flow Area= 33.3 sf, Capacity= 464.76 cfs

100.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight

Length= 35.0' Slope= 0.3429 '/'

Inlet Invert= 66.00', Outlet Invert= 54.00'



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Summary for Reach 6RB: Flow through 3S

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 6RC: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 0.50' Flow Area= 16.7 sf, Capacity= 127.08 cfs

50.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight

Length= 39.0' Slope= 0.1026 '/'

Inlet Invert= 54.00', Outlet Invert= 50.00'



Summary for Reach 6RC: Flow through 3S

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routed to Reach AP3: Analysis Point 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 0.50' Flow Area= 33.3 sf, Capacity= 409.88 cfs

100.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight

Length= 45.0' Slope= 0.2667 '/'

Inlet Invert= 50.00', Outlet Invert= 38.00'



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Summary for Reach 7R: Flow Through 3S

Inflow Area = 0.539 ac, 45.26% Impervious, Inflow Depth > 3.97" for 10 Yr 24 Hr +15% event

Inflow 1.53 cfs @ 12.19 hrs, Volume= 0.178 af

1.53 cfs @ 12.20 hrs, Volume= 0.178 af, Atten= 0%, Lag= 0.7 min Outflow

Routed to Reach 8R: Ditch on Tidewatch Property

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.52 fps, Min. Travel Time= 1.0 min Avg. Velocity = 1.07 fps, Avg. Travel Time= 3.4 min

Peak Storage= 96 cf @ 12.20 hrs

Average Depth at Peak Storage= 0.13', Surface Width= 3.77' Bank-Full Depth= 1.00' Flow Area= 6.0 sf, Capacity= 66.79 cfs

3.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 3.0 '/' Top Width= 9.00'

Length= 220.0' Slope= 0.0909 '/'

Inlet Invert= 58.00', Outlet Invert= 38.00'



Summary for Reach 8R: Ditch on Tidewatch Property

[90] Warning: Qout>Qin may require smaller dt or Finer Routing [62] Hint: Exceeded Reach 7R OUTLET depth by 0.20' @ 12.20 hrs

0.539 ac, 45.26% Impervious, Inflow Depth > 3.96" for 10 Yr 24 Hr +15% event Inflow Area =

1.53 cfs @ 12.20 hrs, Volume= Inflow 0.178 af

1.53 cfs @ 12.21 hrs, Volume= 0.178 af, Atten= 0%, Lag= 0.8 min Outflow

Routed to Reach AP3: Analysis Point 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 2.40 fps, Min. Travel Time= 1.1 min

Avg. Velocity = 0.86 fps, Avg. Travel Time= 3.1 min

Peak Storage= 102 cf @ 12.21 hrs

Average Depth at Peak Storage= 0.32', Surface Width= 2.94'

Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.18 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 3.0 '/' Top Width= 7.00'

Length= 159.0' Slope= 0.0189 '/'

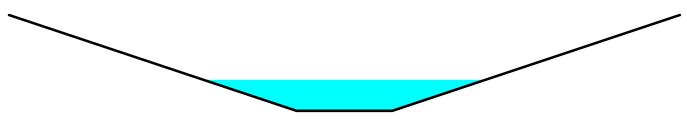
Inlet Invert= 38.00', Outlet Invert= 35.00'

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Summary for Reach 9R: Flow through 19S

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 5.35" for 10 Yr 24 Hr +15% event

Inflow = 0.09 cfs @ 12.10 hrs, Volume= 0.008 af

Outflow = 0.09 cfs @ 12.12 hrs, Volume= 0.008 af, Atten= 1%, Lag= 0.6 min

Routed to Pond 1P: Bioretention Pond

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.71 fps, Min. Travel Time= 0.9 min

Avg. Velocity = 0.23 fps, Avg. Travel Time= 2.8 min

Peak Storage= 5 cf @ 12.12 hrs

Average Depth at Peak Storage= 0.04', Surface Width= 4.10' Bank-Full Depth= 0.50' Flow Area= 5.3 sf, Capacity= 16.36 cfs

3.00' x 0.50' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 15.0 '/' Top Width= 18.00'

Length= 39.0' Slope= 0.0205 '/'

Inlet Invert= 63.80', Outlet Invert= 63.00'



Summary for Reach 10Ra: Flow through 4S

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 5.35" for 10 Yr 24 Hr +15% event

Inflow = 0.09 cfs @ 12.10 hrs, Volume= 0.008 af

Outflow = 0.09 cfs @ 12.11 hrs, Volume= 0.008 af, Atten= 0%, Lag= 0.2 min

Routed to Reach 10Rb: Flow through 4S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.89 fps, Min. Travel Time= 0.3 min

Avg. Velocity = 0.83 fps, Avg. Travel Time= 0.4 min

Peak Storage= 2 cf @ 12.11 hrs

Average Depth at Peak Storage= 0.01', Surface Width= 20.11'

Bank-Full Depth= 0.50' Flow Area= 12.5 sf, Capacity= 199.20 cfs

Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

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20.00' x 0.50' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 10.0 '/' Top Width= 30.00' Length= 18.0' Slope= 0.3333 '/' Inlet Invert= 64.00', Outlet Invert= 58.00'



Summary for Reach 10Rb: Flow through 4S

[61] Hint: Exceeded Reach 10Ra outlet invert by 0.01' @ 12.10 hrs

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 5.35" for 10 Yr 24 Hr +15% event

Inflow = 0.09 cfs @ 12.11 hrs, Volume= 0.008 af

Outflow = 0.09 cfs @ 12.12 hrs, Volume= 0.008 af, Atten= 1%, Lag= 0.7 min

Routed to Reach AP4: Analysis Point 4

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.80 fps, Min. Travel Time= 1.1 min Avg. Velocity = 0.70 fps, Avg. Travel Time= 1.2 min

Peak Storage= 6 cf @ 12.12 hrs

Average Depth at Peak Storage= 0.01', Surface Width= 20.12' Bank-Full Depth= 0.50' Flow Area= 12.5 sf, Capacity= 167.36 cfs

20.00' x 0.50' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 10.0 '/' Top Width= 30.00'

Length= 51.0' Slope= 0.2353 '/'

Inlet Invert= 58.00', Outlet Invert= 46.00'



Summary for Reach AP1: Analysis Point 1 (New CB)

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.414 ac, 46.45% Impervious, Inflow Depth > 3.92" for 10 Yr 24 Hr +15% event

Inflow = 1.83 cfs @ 12.09 hrs, Volume= 0.135 af

Outflow = 1.83 cfs @ 12.09 hrs, Volume= 0.135 af, Atten= 0%, Lag= 0.0 min

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.040 ac. 0.00% Impervious, Inflow Depth > 2.86" for 10 Yr 24 Hr +15% event

Inflow = 0.13 cfs @ 12.09 hrs, Volume= 0.009 af

Outflow = 0.13 cfs @ 12.09 hrs, Volume= 0.009 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 2R: Flow across Map 222 Lot 20

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.560 ac, 15.65% Impervious, Inflow Depth > 3.12" for 10 Yr 24 Hr +15% event

Inflow = 4.12 cfs @ 12.17 hrs, Volume= 0.405 af

Outflow = 4.12 cfs @ 12.17 hrs, Volume= 0.405 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.482 ac, 8.04% Impervious, Inflow Depth > 3.13" for 10 Yr 24 Hr +15% event

Inflow = 1.63 cfs @ 12.11 hrs, Volume= 0.126 af

Outflow = 1.63 cfs @ 12.11 hrs, Volume= 0.126 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Bioretention Pond

Inflow Area = 0.539 ac, 45.26% Impervious, Inflow Depth > 3.97" for 10 Yr 24 Hr +15% event

Inflow = 2.33 cfs @ 12.09 hrs, Volume= 0.179 af

Outflow = 1.53 cfs @ 12.19 hrs, Volume= 0.178 af, Atten= 34%, Lag= 6.0 min

Primary = 1.53 cfs @ 12.19 hrs, Volume= 0.178 af

Routed to Reach 7R: Flow Through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 61.22' @ 12.19 hrs Surf.Area= 845 sf Storage= 411 cf

Plug-Flow detention time= 3.9 min calculated for 0.178 af (100% of inflow)

Center-of-Mass det. time= 2.6 min (792.5 - 789.9)

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Volume	Inve	ert Avail.	Storage	Storage	Description		
#1	58.0	9'	2,583 cf	Custon	n Stage Data (Irreç	gular)Listed below	(Recalc)
Elevatio		Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
58.0)9	117	48.0	0.0	0	0	117
58.1	10	117	48.0	40.0	0	0	117
59.0)9	117	48.0	40.0	46	47	165
59.1	10	117	48.0	15.0	0	47	165
60.5	59	117	48.0	15.0	26	73	237
60.6		117	48.0	100.0	1	74	237
61.0		764	120.0	100.0	157	232	1,201
62.0		1,157	143.0	100.0	954	1,185	1,700
63.0		1,618	164.0	100.0	1,381	2,566	2,235
63.0)1	1,618	164.0	100.0	16	2,583	2,237
Device	Routing	Inv	ert Outle	et Device	es		
#1	Primary	58.3			d Culvert		
			Inlet	/ Outlet	P, projecting, no he Invert= 58.35' / 58.0 ow Area= 0.79 sf		
#2	Device 1	58.3		•		600 Limited to we	ir flow at low heads
#3	Device 1	61.8			Orifice/Grate C= ir flow at low heads		

Primary OutFlow Max=1.53 cfs @ 12.19 hrs HW=61.22' TW=58.13' (Dynamic Tailwater)

-1=Culvert (Passes 1.53 cfs of 4.59 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 1.53 cfs @ 7.79 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 1PF: Sediment Forebay

[43] Hint: Has no inflow (Outflow=Zero)

Volume	Invert	Avail.	Storage	Storage	Description	
#1	61.00'		272 cf	Custom	Stage Data (Pri	smatic)Listed below (Recalc)
Elevation (feet)		.Area sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)	
61.00		9		0	0	
62.00		119		64	64	
63.00		297		208	272	

Summary for Pond 3P: Stone Under Deck

Ledge surface modelled 24" below original grade based on TP 13 (Bedrock found from 24" to 36". High existing contour within footprint of stone is 63.0 and therefore ledge surface modelled at 61.0

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Inflow Area = 0.031 ac, 85.88% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event

Inflow = 0.17 cfs @ 12.09 hrs, Volume= 0.014 af

Outflow = 0.01 cfs @ 13.77 hrs, Volume= 0.010 af, Atten= 94%, Lag= 100.5 min

Discarded = 0.01 cfs @ 13.77 hrs, Volume= 0.010 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach 6RA: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 64.72' @ 13.77 hrs Surf.Area= 0.006 ac Storage= 0.008 af

Plug-Flow detention time= 299.4 min calculated for 0.010 af (72% of inflow)

Center-of-Mass det. time= 208.6 min (955.0 - 746.4)

Volume	Invert	Avail.Storage	Storage Description
#1	61.73'	0.009 af	14.00'W x 20.00'L x 3.31'H Prismatoid
			0.021 af Overall x 40.0% Voids

Device	Routing	Invert	Outlet Devices	
#0	Secondary	65.04'	Automatic Storage Overflow (Discharged with	out head)
#1	Discarded	61.73'	0.300 in/hr Exfiltration over Surface area	
			Conductivity to Groundwater Elevation = 61.00'	Phase-In= 0.10'

Discarded OutFlow Max=0.01 cfs @ 13.77 hrs HW=64.72' (Free Discharge) **1=Exfiltration** (Controls 0.01 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=61.73' TW=66.00' (Dynamic Tailwater)

Summary for Pond 4P: Stone Under Deck

Ledge surface modelled 20" below original grade based on TP 12 (Bedrock ranging from 20" to 28". High existing grade within footprint of practice is 64.0 and therefore ledge surface modelled at 62.33

Inflow Area = 0.031 ac, 85.88% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event Inflow 0.17 cfs @ 12.09 hrs, Volume= 0.014 af Outflow 0.06 cfs @ 12.32 hrs, Volume= 0.014 af, Atten= 61%, Lag= 13.8 min Discarded = 0.06 cfs @ 12.32 hrs, Volume= 0.014 af 0.00 hrs, Volume= Secondary = 0.00 cfs @ 0.000 af Routed to Reach 6RA: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 63.65' @ 12.32 hrs Surf.Area= 0.006 ac Storage= 0.003 af

Plug-Flow detention time= 35.4 min calculated for 0.014 af (99% of inflow) Center-of-Mass det. time= 30.3 min (776.2 - 745.9)

Volume	Invert	Avail.Storage	Storage Description
#1	62.37'	0.006 af	14.00'W x 20.00'L x 2.41'H Prismatoid
			0.015 af Overall x 40.0% Voids

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Device	Routing	Invert	Outlet Devices	
#0	Secondary	64.78'	Automatic Storage Overflow (Discharged without head)	
#1	Discarded	62.37'	0.300 in/hr Exfiltration over Surface area	
			Conductivity to Groundwater Elevation = 62.33' Phase-In= 0.10'	

Discarded OutFlow Max=0.06 cfs @ 12.32 hrs HW=63.64' (Free Discharge) T-1=Exfiltration (Controls 0.06 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=62.37' TW=66.00' (Dynamic Tailwater)

Summary for Pond 5P: Lined Stone Drip Edge

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event 0.10 cfs @ 12.09 hrs, Volume= Inflow 0.008 af Outflow 0.10 cfs @ 12.09 hrs, Volume= 0.008 af, Atten= 0%, Lag= 0.5 min 0.10 cfs @ 12.09 hrs, Volume= 0.008 af Primary = Routed to Pond 3P: Stone Under Deck 0.00 hrs, Volume= Secondary = 0.00 cfs @ 0.000 af Routed to Reach 6RA: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.07' @ 12.09 hrs Surf.Area= 0.003 ac Storage= 0.000 af

Plug-Flow detention time= 1.4 min calculated for 0.008 af (100% of inflow) Center-of-Mass det. time= 1.1 min (746.9 - 745.7)

Volume	Invert	Avail.Storag	ge Storage Description
#1	66.00'	0.001	af 2.00'W x 63.00'L x 1.01'H Prismatoid 0.003 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#0	Secondary	67.01'	Automatic Storage Overflow (Discharged without head)
#1	Primary	66.00'	6.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#2	Secondary	67.00'	63.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Primary OutFlow Max=0.09 cfs @ 12.09 hrs HW=66.07' TW=63.58' (Dynamic Tailwater) 1=Orifice/Grate (Weir Controls 0.09 cfs @ 0.86 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=66.00' TW=66.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 6P: Lined Stone Drip Edge

[44] Hint: Outlet device #1 is below defined storage

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event

Inflow = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af

Outflow = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af, Atten= 0%, Lag= 0.5 min

Primary = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af

Routed to Pond 4P : Stone Under Deck

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach 6RA: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.07' @ 12.09 hrs Surf.Area= 0.003 ac Storage= 0.000 af

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 0.3 min (746.1 - 745.7)

Volume	Invert	Avail.Storage	Storage Description
#1	66.01'	0.001 af	2.00'W x 63.00'L x 1.01'H Prismatoid
			0.003 af Overall x 40.0% Voids

Device	Routing	Invert	Outlet Devices
#1	Primary	66.00'	6.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#2	Secondary	67.00'	63.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Primary OutFlow Max=0.09 cfs @ 12.09 hrs HW=66.07' TW=63.33' (Dynamic Tailwater) 1=Orifice/Grate (Weir Controls 0.09 cfs @ 0.86 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=66.01' TW=66.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 7P: Lined Stone Drip Edge

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event

Inflow = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af

Outflow = 0.09 cfs @ 12.10 hrs, Volume= 0.008 af, Atten= 1%, Lag= 1.1 min

Primary = 0.09 cfs @ 12.10 hrs, Volume= 0.008 af

Routed to Reach 9R: Flow through 19S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 64.21' @ 12.10 hrs Surf.Area= 0.003 ac Storage= 0.000 af

Plug-Flow detention time= 6.6 min calculated for 0.008 af (100% of inflow) Center-of-Mass det. time= 4.8 min (750.6 - 745.7)

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Volume	Invert	Avail.Stora	age Storage Description
#1	64.00'	0.001	af 2.00'W x 63.00'L x 1.01'H Prismatoid 0.003 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#1	Primary	64.00'	6.0" Round Culvert L= 4.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 64.00' / 63.80' S= 0.0500 '/' Cc= 0.900 n= 0.012, Flow Area= 0.20 sf
#2	Device 1	64.00'	6.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Primary	65.00'	63.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Primary OutFlow Max=0.09 cfs @ 12.10 hrs HW=64.21' TW=63.84' (Dynamic Tailwater)

-1=Culvert (Inlet Controls 0.09 cfs @ 1.22 fps)

2=Orifice/Grate (Passes 0.09 cfs of 0.43 cfs potential flow)

-3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 8P: Lined Stone Drip Edge

0.018 ac, 75.74% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event Inflow Area =

Inflow 0.10 cfs @ 12.09 hrs, Volume= 0.008 af

0.09 cfs @ 12.10 hrs, Volume= Outflow 0.008 af, Atten= 1%, Lag= 1.1 min

Primary = 0.09 cfs @ 12.10 hrs, Volume= 0.008 af

Routed to Reach 10ra: Flow through 4S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 64.71' @ 12.10 hrs Surf.Area= 0.003 ac Storage= 0.000 af

Plug-Flow detention time= 6.6 min calculated for 0.008 af (100% of inflow) Center-of-Mass det. time= 4.8 min (750.6 - 745.7)

Volume	Invert	Avail.Stora	age Storage Description
#1	64.50'	0.001	af 2.00'W x 63.00'L x 1.01'H Prismatoid 0.003 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#1	Primary	64.50'	6.0" Round Culvert L= 4.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 64.50' / 64.00' S= 0.1250 '/' Cc= 0.900 n= 0.012, Flow Area= 0.20 sf
#2 #3	Device 1 Primary	64.50' 65.50'	6.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads 63.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

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Primary OutFlow Max=0.09 cfs @ 12.10 hrs HW=64.71' TW=64.01' (Dynamic Tailwater)

-1=Culvert (Inlet Controls 0.09 cfs @ 1.22 fps)

2=Orifice/Grate (Passes 0.09 cfs of 0.43 cfs potential flow)

-3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond CB101: Catch Basin 101

Inflow Area = 0.130 ac, 59.12% Impervious, Inflow Depth > 4.29" for 10 Yr 24 Hr +15% event

Inflow = 0.61 cfs @ 12.09 hrs, Volume= 0.046 af

Outflow = 0.61 cfs @ 12.09 hrs, Volume= 0.046 af, Atten= 0%, Lag= 0.0 min

Primary = 0.61 cfs @ 12.09 hrs, Volume= 0.046 af

Routed to Pond CB102: Catch Basin 102

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 67.13' @ 12.09 hrs

Flood Elev= 70.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	66.60'	12.0" Round Culvert
			L= 14.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 66.60' / 66.50' S= 0.0071 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.60 cfs @ 12.09 hrs HW=67.12' TW=66.95' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.60 cfs @ 2.12 fps)

Summary for Pond CB102: Catch Basin 102

Inflow Area = 0.152 ac, 65.02% Impervious, Inflow Depth > 4.45" for 10 Yr 24 Hr +15% event

Inflow = 0.73 cfs @ 12.09 hrs, Volume= 0.056 af

Outflow = 0.73 cfs @ 12.09 hrs, Volume= 0.056 af, Atten= 0%, Lag= 0.0 min

Primary = 0.73 cfs @ 12.09 hrs, Volume= 0.056 af

Routed to Pond CB104: Catch Basin 104

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 66.96' @ 12.09 hrs

Flood Elev= 70.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	66.40'	12.0" Round Culvert
			L= 84.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 66.40' / 65.90' S= 0.0060 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.71 cfs @ 12.09 hrs HW=66.95' TW=66.57' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.71 cfs @ 2.31 fps)

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Summary for Pond CB103: Catch Basin 103

Inflow Area = 0.155 ac, 64.18% Impervious, Inflow Depth > 4.40" for 10 Yr 24 Hr +15% event

Inflow 0.73 cfs @ 12.09 hrs. Volume= 0.057 af

0.73 cfs @ 12.09 hrs, Volume= Outflow 0.057 af, Atten= 0%, Lag= 0.0 min

0.73 cfs @ 12.09 hrs, Volume= Primary = 0.057 af

Routed to Pond CB104: Catch Basin 104

Routing by Dvn-Stor-Ind method. Time Span= 0.00-24.00 hrs. dt= 0.05 hrs / 3

Peak Elev= 68.09' @ 12.09 hrs

Flood Elev= 72.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	67.60'	12.0" Round Culvert
			L= 42.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 67.60' / 67.30' S= 0.0071 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.71 cfs @ 12.09 hrs HW=68.09' TW=66.57' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.71 cfs @ 1.87 fps)

Summary for Pond CB104: Catch Basin 104

Inflow Area = 0.314 ac, 65.44% Impervious, Inflow Depth > 4.45" for 10 Yr 24 Hr +15% event

1.49 cfs @ 12.09 hrs, Volume= Inflow = 0.116 af

1.49 cfs @ 12.09 hrs, Volume= 1.49 cfs @ 12.09 hrs, Volume= Outflow 0.116 af, Atten= 0%, Lag= 0.0 min

Primary 0.116 af

Routed to Pond 1P: Bioretention Pond

Routing by Dvn-Stor-Ind method. Time Span= 0.00-24.00 hrs. dt= 0.05 hrs / 3

Peak Elev= 66.58' @ 12.09 hrs

Flood Elev= 71.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	65.80'	12.0" Round Culvert
	·		L= 31.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 65.80' / 65.60' S= 0.0065 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=1.46 cfs @ 12.09 hrs HW=66.57' TW=61.02' (Dynamic Tailwater) **1=Culvert** (Barrel Controls 1.46 cfs @ 3.10 fps)

Summary for Pond YD1: Yard Drain 1

Inflow Area = 0.105 ac, 49.42% Impervious, Inflow Depth > 4.04" for 10 Yr 24 Hr +15% event

Inflow 0.48 cfs @ 12.09 hrs, Volume= 0.035 af

0.48 cfs @ 12.09 hrs, Volume= Outflow 0.035 af, Atten= 0%, Lag= 0.0 min

0.48 cfs @ 12.09 hrs, Volume= 0.035 af Primary

Routed to Pond CB101: Catch Basin 101

Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

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Peak Elev= 67.77' @ 12.09 hrs Flood Elev= 69.30'

Device	Routing	Invert	Outlet Devices
	Primary		8.0" Round Culvert L= 15.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 67.30' / 66.93' S= 0.0247 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.47 cfs @ 12.09 hrs HW=67.76' TW=67.12' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.47 cfs @ 1.82 fps)

Summary for Pond YD2: Yard Drain 2

Inflow Area = 0.086 ac, 35.30% Impervious, Inflow Depth > 3.63" for 10 Yr 24 Hr +15% event

Inflow = 0.35 cfs @ 12.09 hrs, Volume= 0.026 af

Outflow = 0.35 cfs @ 12.09 hrs, Volume= 0.026 af, Atten= 0%, Lag= 0.0 min

Primary = 0.35 cfs @ 12.09 hrs, Volume= 0.026 af

Routed to Pond CB103: Catch Basin 103

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 68.59' @ 12.09 hrs Flood Elev= 70.20'

Device Routing Invert Outlet Devices

#1 Primary

68.20' 8.0" Round Culvert

L= 13.0' CPP, projecting, no headwall, Ke= 0.900
Inlet / Outlet Invert= 68.20' / 67.93' S= 0.0208 '/' Cc= 0.900

n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.35 cfs @ 12.09 hrs HW=68.58' TW=68.09' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.35 cfs @ 1.67 fps)

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

•	
Subcatchment1S: Subcatchment1S	Runoff Area=16,321 sf 51.36% Impervious Runoff Depth>5.48" Flow Length=186' Tc=6.0 min CN=86 Runoff=2.27 cfs 0.171 af
Subcatchment2S: Subcatchment2S Flow Length=20'	Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>4.14" Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.19 cfs 0.014 af
Subcatchment3S: Subcatchment3S	Runoff Area=44,463 sf 0.00% Impervious Runoff Depth>3.92" Flow Length=447' Tc=11.9 min CN=72 Runoff=3.85 cfs 0.334 af
Subcatchment4S: Subcatchment4S	Runoff Area=20,212 sf 5.43% Impervious Runoff Depth>4.36" Flow Length=216' Tc=7.8 min CN=76 Runoff=2.20 cfs 0.169 af
Subcatchment6S: Subcatchment6S	Runoff Area=1,084 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.17 cfs 0.014 af
Subcatchment7S: Subcatchment7S	Runoff Area=954 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.013 af
Subcatchment8S: Subcatchment8S	Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.47 cfs 0.040 af
Subcatchment9S: Subcatchment9S	Runoff Area=325 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment11S: Subcatchment11S Flow Length=77'	Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>5.48" Slope=0.0396 '/' Tc=6.0 min CN=86 Runoff=0.64 cfs 0.048 af
Subcatchment12S: Subcatchment12S Flow Length=50'	Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>5.02" Slope=0.0320 '/' Tc=6.0 min CN=82 Runoff=0.49 cfs 0.036 af
Subcatchment13S: Subcatchment13S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af
Subcatchment14S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af
Subcatchment15S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.12 cfs 0.010 af
Subcatchment16S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.12 cfs 0.010 af
Subcatchment17S: Subcatchment17S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.12 cfs 0.010 af
Subcatchment18S: Subcatchment18S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.12 cfs 0.010 af

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Subcatchment19S: Subcatchment19SRunoff Area=9,042 sf 12.11% Impervious Runoff Depth>4.47"

Flow Length=58' Tc=6.0 min CN=77 Runoff=1.06 cfs 0.077 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.03' Max Vel=0.79 fps Inflow=0.19 cfs 0.014 af n=0.030 L=81.0' S=0.0494 '/' Capacity=88.18 cfs Outflow=0.18 cfs 0.014 af

Reach 3R: Flow over Sagamore Ave Avg. Flow Depth=0.16' Max Vel=3.65 fps Inflow=2.45 cfs 0.185 af n=0.016 L=45.0' S=0.0444 '/' Capacity=48.65 cfs Outflow=2.46 cfs 0.185 af

Reach 6RA: Flow through 3SAvg. Flow Depth=0.01' Max Vel=0.96 fps Inflow=0.06 cfs 0.002 af n=0.030 L=35.0' S=0.3429 '/' Capacity=464.76 cfs Outflow=0.07 cfs 0.002 af

Reach 6RB: Flow through 3SAvg. Flow Depth=0.02' Max Vel=0.74 fps Inflow=0.07 cfs 0.002 af n=0.030 L=39.0' S=0.1026 '/' Capacity=127.08 cfs Outflow=0.07 cfs 0.002 af

Reach 6RC: Flow through 3SAvg. Flow Depth=0.01' Max Vel=0.85 fps Inflow=0.07 cfs 0.002 af n=0.030 L=45.0' S=0.2667 '/' Capacity=409.88 cfs Outflow=0.06 cfs 0.002 af

Reach 7R: Flow Through 3SAvg. Flow Depth=0.14' Max Vel=3.63 fps Inflow=1.67 cfs 0.242 af n=0.030 L=220.0' S=0.0909 '/' Capacity=66.79 cfs Outflow=1.67 cfs 0.241 af

Reach 8R: Ditch on Tidewatch Property Avg. Flow Depth=0.34' Max Vel=2.46 fps Inflow=1.67 cfs 0.241 af n=0.030 L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=1.67 cfs 0.241 af

Reach 9R: Flow through 19SAvg. Flow Depth=0.04' Max Vel=0.77 fps Inflow=0.12 cfs 0.010 af n=0.030 L=39.0' S=0.0205 '/' Capacity=16.36 cfs Outflow=0.12 cfs 0.010 af

Reach 10Ra: Flow through 4SAvg. Flow Depth=0.01' Max Vel=1.00 fps Inflow=0.12 cfs 0.010 af n=0.030 L=18.0' S=0.3333 '/' Capacity=199.20 cfs Outflow=0.12 cfs 0.010 af

Reach 10Rb: Flow through 4SAvg. Flow Depth=0.01' Max Vel=0.90 fps Inflow=0.12 cfs 0.010 af n=0.030 L=51.0' S=0.2353 '/' Capacity=167.36 cfs Outflow=0.12 cfs 0.010 af

Reach AP1: Analysis Point 1 (New CB)

Inflow=2.46 cfs 0.185 af
Outflow=2.46 cfs 0.185 af

Reach AP2: Analysis Point 2 Inflow=0.19 cfs 0.014 af
Outflow=0.19 cfs 0.014 af

Reach AP3: Analysis Point 3 Inflow=5.49 cfs 0.577 af
Outflow=5.49 cfs 0.577 af

Reach AP4: Analysis Point 4 Inflow=2.32 cfs 0.179 af
Outflow=2.32 cfs 0.179 af

Pond 1P: Bioretention Pond

Peak Elev=61.73' Storage=886 cf Inflow=3.14 cfs 0.242 af

Outflow=1.67 cfs 0.242 af

Pond 1PF: Sediment Forebay Peak Elev=0.00' Storage=0 cf

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Pond 3P: Stone Under Deck Peak Elev=65.04' Storage=0.009 af Inflow=0.21 cfs 0.018 af Discarded=0.01 cfs 0.011 af Secondary=0.06 cfs 0.002 af Outflow=0.07 cfs 0.013 af

Discarded the title that are established to the title the title are

Pond 4P: Stone Under Deck
Peak Elev=64.00' Storage=0.004 af Inflow=0.21 cfs 0.018 af
Discarded=0.08 cfs 0.017 af Secondary=0.00 cfs 0.000 af Outflow=0.08 cfs 0.017 af

Pond 5P: Lined Stone Drip Edge Peak Elev=66.08' Storage=0.000 af Inflow=0.12 cfs 0.010 af

Primary=0.12 cfs 0.010 af Secondary=0.00 cfs 0.000 af Outflow=0.12 cfs 0.010 af

Pond 6P: Lined Stone Drip Edge Peak Elev=66.08' Storage=0.000 af Inflow=0.12 cfs 0.010 af

Primary=0.12 cfs 0.010 af Secondary=0.00 cfs 0.000 af Outflow=0.12 cfs 0.010 af

Pond 7P: Lined Stone Drip Edge Peak Elev=64.24' Storage=0.000 af Inflow=0.12 cfs 0.010 af

Outflow=0.12 cfs 0.010 af

Pond 8P: Lined Stone Drip Edge Peak Elev=64.74' Storage=0.000 af Inflow=0.12 cfs 0.010 af

Outflow=0.12 cfs 0.010 af

Pond CB101: Catch Basin 101 Peak Elev=67.25' Inflow=0.81 cfs 0.062 af

12.0" Round Culvert n=0.012 L=14.0' S=0.0071 '/' Outflow=0.81 cfs 0.062 af

Pond CB102: Catch Basin 102 Peak Elev=67.09' Inflow=0.96 cfs 0.075 af

12.0" Round Culvert n=0.012 L=84.0' S=0.0060 '/' Outflow=0.96 cfs 0.075 af

Pond CB103: Catch Basin 103 Peak Elev=68.18' Inflow=0.96 cfs 0.076 af

12.0" Round Culvert n=0.012 L=42.0' S=0.0071'/' Outflow=0.96 cfs 0.076 af

Pond CB104: Catch Basin 104 Peak Elev=66.74' Inflow=1.96 cfs 0.154 af

12.0" Round Culvert n=0.012 L=31.0' S=0.0065 '/' Outflow=1.96 cfs 0.154 af

Pond YD1: Yard Drain 1 Peak Elev=67.86' Inflow=0.64 cfs 0.048 af

8.0" Round Culvert n=0.012 L=15.0' S=0.0247 '/' Outflow=0.64 cfs 0.048 af

Pond YD2: Yard Drain 2 Peak Elev=68.67' Inflow=0.49 cfs 0.036 af

8.0" Round Culvert n=0.012 L=13.0' S=0.0208 '/' Outflow=0.49 cfs 0.036 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.975 af Average Runoff Depth = 4.64" 79.02% Pervious = 1.990 ac 20.98% Impervious = 0.528 ac

Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S Runoff Area=16,321 sf 51.36% Impervious Runoff Depth>6.84" Flow Length=186' Tc=6.0 min CN=86 Runoff=2.81 cfs 0.214 af Subcatchment2S: Subcatchment2S Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>5.40" Flow Length=20' Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.24 cfs 0.018 af Runoff Area=44,463 sf 0.00% Impervious Runoff Depth>5.15" Subcatchment3S: Subcatchment3S Flow Length=447' Tc=11.9 min CN=72 Runoff=5.05 cfs 0.438 af Runoff Area=20,212 sf 5.43% Impervious Runoff Depth>5.64" Subcatchment4S: Subcatchment4S Flow Length=216' Tc=7.8 min CN=76 Runoff=2.83 cfs 0.218 af Runoff Area=1,084 sf 100.00% Impervious Runoff Depth>8.28" Subcatchment6S: Subcatchment6S Tc=6.0 min CN=98 Runoff=0.20 cfs 0.017 af Subcatchment7S: Subcatchment7S Runoff Area=954 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.18 cfs 0.015 af Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>8.28" Subcatchment8S: Subcatchment8S Tc=6.0 min CN=98 Runoff=0.57 cfs 0.048 af Subcatchment9S: Subcatchment9S Runoff Area=325 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af Subcatchment11S: Subcatchment11S Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>6.84" Slope=0.0396 '/' Tc=6.0 min CN=86 Runoff=0.79 cfs 0.060 af Flow Length=77' Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>6.36" Subcatchment12S: Subcatchment12S Slope=0.0320 '/' Tc=6.0 min CN=82 Runoff=0.61 cfs 0.045 af Flow Length=50' Subcatchment13S: Subcatchment13S Runoff Area=560 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.11 cfs 0.009 af Subcatchment14S: Subcatchment14S Runoff Area=560 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.11 cfs 0.009 af Subcatchment15S: Subcatchment15S Runoff Area=779 sf 75.74% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af Subcatchment16S: Subcatchment15S Runoff Area=779 sf 75.74% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af Runoff Area=779 sf 75.74% Impervious Runoff Depth>8.28" Subcatchment17S: Subcatchment17S Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af Subcatchment18S: Subcatchment18S Runoff Area=779 sf 75.74% Impervious Runoff Depth>8.28"

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Subcatchment19S: Subcatchment19SRunoff Area=9,042 sf 12.11% Impervious Runoff Depth>5.76"

Flow Length=58' Tc=6.0 min CN=77 Runoff=1.36 cfs 0.100 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.03' Max Vel=0.86 fps Inflow=0.24 cfs 0.018 af n=0.030 L=81.0' S=0.0494 '/' Capacity=88.18 cfs Outflow=0.24 cfs 0.018 af

Reach 3R: Flow over Sagamore AveAvg. Flow Depth=0.18' Max Vel=3.85 fps Inflow=3.04 cfs 0.231 af n=0.016 L=45.0' S=0.0444 '/' Capacity=48.65 cfs Outflow=3.05 cfs 0.231 af

Reach 6RA: Flow through 3SAvg. Flow Depth=0.01' Max Vel=1.21 fps Inflow=0.17 cfs 0.004 af n=0.030 L=35.0' S=0.3429 '/' Capacity=464.76 cfs Outflow=0.16 cfs 0.004 af

Reach 6RB: Flow through 3SAvg. Flow Depth=0.02' Max Vel=0.97 fps Inflow=0.16 cfs 0.004 af n=0.030 L=39.0' S=0.1026 '/' Capacity=127.08 cfs Outflow=0.15 cfs 0.004 af

Reach 6RC: Flow through 3SAvg. Flow Depth=0.01' Max Vel=1.12 fps Inflow=0.15 cfs 0.004 af n=0.030 L=45.0' S=0.2667 '/' Capacity=409.88 cfs Outflow=0.16 cfs 0.004 af

Reach 7R: Flow Through 3SAvg. Flow Depth=0.18' Max Vel=4.33 fps Inflow=2.75 cfs 0.302 af n=0.030 L=220.0' S=0.0909 '/' Capacity=66.79 cfs Outflow=2.82 cfs 0.302 af

Reach 8R: Ditch on Tidewatch Property Avg. Flow Depth=0.43' Max Vel=2.81 fps Inflow=2.82 cfs 0.302 af n=0.030 L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=2.78 cfs 0.302 af

Reach 9R: Flow through 19SAvg. Flow Depth=0.05' Max Vel=0.82 fps Inflow=0.14 cfs 0.012 af n=0.030 L=39.0' S=0.0205 '/' Capacity=16.36 cfs Outflow=0.14 cfs 0.012 af

Reach 10Ra: Flow through 4SAvg. Flow Depth=0.01' Max Vel=1.08 fps Inflow=0.14 cfs 0.012 af n=0.030 L=18.0' S=0.3333 '/' Capacity=199.20 cfs Outflow=0.14 cfs 0.012 af

Reach 10Rb: Flow through 4SAvg. Flow Depth=0.01' Max Vel=0.96 fps Inflow=0.14 cfs 0.012 af n=0.030 L=51.0' S=0.2353 '/' Capacity=167.36 cfs Outflow=0.14 cfs 0.012 af

Reach AP1: Analysis Point 1 (New CB)

Inflow=3.05 cfs 0.231 af
Outflow=3.05 cfs 0.231 af

Reach AP2: Analysis Point 2 Inflow=0.24 cfs 0.018 af
Outflow=0.24 cfs 0.018 af

Reach AP3: Analysis Point 3 Inflow=7.72 cfs 0.744 af
Outflow=7.72 cfs 0.744 af

Reach AP4: Analysis Point 4 Inflow=2.97 cfs 0.230 af Outflow=2.97 cfs 0.230 af

Pond 1P: Bioretention Pond

Peak Elev=61.96' Storage=1,144 cf Inflow=3.90 cfs 0.302 af

Outflow=2.75 cfs 0.302 af

Pond 1PF: Sediment Forebay Peak Elev=0.00' Storage=0 cf

Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

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Pond 3P: Stone Under Deck

Peak Elev=65.04' Storage=0.009 af Inflow=0.25 cfs 0.021 af

Discarded=0.01 cfs 0.012 af Secondary=0.17 cfs 0.004 af Outflow=0.18 cfs 0.016 af

Pond 4P: Stone Under Deck Peak Elev=64.34' Storage=0.005 af Inflow=0.25 cfs 0.021 af

Discarded=0.10 cfs 0.021 af Secondary=0.00 cfs 0.000 af Outflow=0.10 cfs 0.021 af

Pond 5P: Lined Stone Drip Edge Peak Elev=66.09' Storage=0.000 af Inflow=0.15 cfs 0.012 af

Primary=0.15 cfs 0.012 af Secondary=0.00 cfs 0.000 af Outflow=0.15 cfs 0.012 af

Pond 6P: Lined Stone Drip Edge Peak Elev=66.09' Storage=0.000 af Inflow=0.15 cfs 0.012 af

Primary=0.15 cfs 0.012 af Secondary=0.00 cfs 0.000 af Outflow=0.15 cfs 0.012 af

Pond 7P: Lined Stone Drip Edge Peak Elev=64.26' Storage=0.000 af Inflow=0.15 cfs 0.012 af

Outflow=0.14 cfs 0.012 af

Pond 8P: Lined Stone Drip Edge Peak Elev=64.76' Storage=0.000 af Inflow=0.15 cfs 0.012 af

Outflow=0.14 cfs 0.012 af

Pond CB101: Catch Basin 101 Peak Elev=67.39' Inflow=0.99 cfs 0.077 af

12.0" Round Culvert n=0.012 L=14.0' S=0.0071 '/' Outflow=0.99 cfs 0.077 af

Pond CB102: Catch Basin 102 Peak Elev=67.24' Inflow=1.17 cfs 0.092 af

12.0" Round Culvert n=0.012 L=84.0' S=0.0060 '/' Outflow=1.17 cfs 0.092 af

Pond CB103: Catch Basin 103 Peak Elev=68.25' Inflow=1.17 cfs 0.093 af

12.0" Round Culvert n=0.012 L=42.0' S=0.0071'/' Outflow=1.17 cfs 0.093 af

Pond CB104: Catch Basin 104 Peak Elev=66.94' Inflow=2.40 cfs 0.190 af

12.0" Round Culvert n=0.012 L=31.0' S=0.0065 '/' Outflow=2.40 cfs 0.190 af

Pond YD1: Yard Drain 1 Peak Elev=67.98' Inflow=0.79 cfs 0.060 af

8.0" Round Culvert n=0.012 L=15.0' S=0.0247 '/' Outflow=0.79 cfs 0.060 af

Pond YD2: Yard Drain 2 Peak Elev=68.75' Inflow=0.61 cfs 0.045 af

8.0" Round Culvert n=0.012 L=13.0' S=0.0208 '/' Outflow=0.61 cfs 0.045 af

Total Runoff Area = 2.518 ac Runoff Volume = 1.245 af Average Runoff Depth = 5.93" 79.02% Pervious = 1.990 ac 20.98% Impervious = 0.528 ac

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 2.81 cfs @ 12.09 hrs, Volume=

0.214 af, Depth> 6.84"

Routed to Reach 3R: Flow over Sagamore Ave

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Д	rea (sf)	CN I	Description						
		6,930	98 I	98 Paved parking, HSG C						
		7,938	74	74 >75% Grass cover, Good, HSG C						
		1,453	98	Roofs, HSC	G C					
		16,321	86 \	Weighted A	verage					
		7,938	4	48.64% Pe	rvious Area					
		8,383	!	51.36% Imp	pervious Ar	ea				
	Тс	Length	Slope		Capacity	Description				
((min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	2.5	50	0.1250	0.33		Sheet Flow,				
						Grass: Short n= 0.150 P2= 3.70"				
	0.0	6	0.1250	2.47		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.3	30	0.0670	1.81		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.4	100	0.0360	3.85		Shallow Concentrated Flow,				
						Paved Kv= 20.3 fps				
	3.2	186	Total,	Increased t	to minimum	Tc = 6.0 min				

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.24 cfs @ 12.09 hrs, Volume=

0.018 af, Depth> 5.40"

Routed to Reach AP2 : Analysis Point 2

	Aı	rea (sf)	CN	CN Description						
		1,728	74	74 >75% Grass cover, Good, HSG C						
		1,728		100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	Description				
	1.3	20	0.1000	0.25		Sheet Flow,				
_						Grass: Short	n= 0.150	P2= 3.70"		
	1.3	20	Total,	Total, Increased to minimum Tc = 6.0 min						

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Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 5.05 cfs @ 12.17 hrs, Volume= 0.438 af, Depth> 5.15"

Routed to Reach AP3: Analysis Point 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Α	rea (sf)	CN D	escription		
		14,740			•	ood, HSG C
		28,306		•	od, HSG C	
*		1,417	96 L	edge, HSC	G C	
		44,463	72 V	Veighted A	verage	
		44,463	1	00.00% Pe	ervious Are	a
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	8.6	50	0.0415	0.10		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	0.7	62	0.0968	1.56		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.7	54	0.0741	1.36		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	1.3	122	0.1000	1.58		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.6	159	0.0189	4.55	18.20	Trap/Vee/Rect Channel Flow,
						Bot.W=1.00' D=1.00' Z= 3.0 '/' Top.W=7.00'
						n= 0.030 Short grass
	11.9	447	Total			

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 2.83 cfs @ 12.11 hrs, Volume= 0.218 af, Depth> 5.64"

Routed to Reach AP4: Analysis Point 4

	Area (sf)	CN	Description			
	9,377	74	75% Grass cover, Good, HSG C			
	8,075	70	Woods, Good, HSG C			
	1,097	98	Roofs, HSG C			
*	1,663	96	Ledge, HSG C			
	20,212	12 76 Weighted Average				
	19,115		94.57% Pervious Area			
	1,097		5.43% Impervious Area			

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	1.9		0.0210	0.13		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	4.2	36	0.1280	0.14		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	0.5	50	0.1280	1.79		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	1.0	87	0.0800	1.41		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.2	29	0.2860	2.67		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	7.8	216	Total			

Summary for Subcatchment 6S: Subcatchment 6S

Runoff = 0.20 cfs @ 12.09 hrs, Volume=

0.017 af, Depth> 8.28"

Routed to Pond CB101: Catch Basin 101

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

_	Α	rea (sf)	CN I	Description					
		1,084	98 I	Paved parking, HSG C					
		1,084	•	100.00% Impervious Area					
	To	Longth	Slope	Volocity	Canacity	Description			
	(min)	Length (feet)	(ft/ft)	(ft/sec)	(cfs)	Description			
_	6.0				, ,	Direct Entry.			

Summary for Subcatchment 7S: Subcatchment 7S

Runoff = 0.18 cfs @ 12.09 hrs, Volume=

0.015 af, Depth> 8.28"

Routed to Pond CB102: Catch Basin 102

A	rea (sf)	CN [Description						
	954	98 F	98 Paved parking, HSG C						
	954	1	00.00% In	npervious A	Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
6.0					Direct Entry,				

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Summary for Subcatchment 8S: Subcatchment 8S

Runoff = 0.57 cfs @ 12.09 hrs, Volume=

0.048 af, Depth> 8.28"

Routed to Pond CB103: Catch Basin 103

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description					
	2,554	98	Paved parking, HSG C					
	457	98	Roofs, HSG	C				
	3,011	98	Weighted A	verage				
	3,011		100.00% Im	pervious A	Area			
_								
Tc	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
6.0					Direct Entry,			

Summary for Subcatchment 9S: Subcatchment 9S

Runoff = 0.06 cfs @ 12.09 hrs, Volume=

0.005 af, Depth> 8.28"

Routed to Pond CB104: Catch Basin 104

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN [Description					
	325	98 F	B Paved parking, HSG C					
	325	1	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

Summary for Subcatchment 11S: Subcatchment 11S

Runoff = 0.79 cfs @ 12.09 hrs, Volume= 0.060 af, Depth> 6.84"

Routed to Pond YD1: Yard Drain 1

Area (sf)	CN	Description						
1,998	98	Roofs, HSG C						
2,312	74	>75% Grass cover, Good, HSG C						
261	98	Paved parking, HSG C						
4,571	86	Weighted Average						
2,312		50.58% Pervious Area						
2,259		49.42% Impervious Area						

Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

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	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	4.0	50	0.0396	0.21		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.3	27	0.0396	1.39		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	4.0					T 00 :

4.3 77 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 12S: Subcatchment 12S

Runoff 0.61 cfs @ 12.09 hrs, Volume= 0.045 af, Depth> 6.36"

Routed to Pond YD2: Yard Drain 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN [Description						
	1,318	98 F	Roofs, HSG	G C					
	2,416	74 >	>75% Gras	s cover, Go	ood, HSG C				
	3,734	82 \	Weighted A	verage					
	2,416	6	64.70% Per	vious Area					
	1,318	3	35.30% Imp	ervious Ar	ea				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
4.3	50	0.0320	0.19		Sheet Flow,				
					Grass: Short	n= 0.150	P2= 3.70"		
4.3	50	Total,	Increased t	o minimum	Tc = 6.0 min				

Summary for Subcatchment 13S: Subcatchment 13S

0.11 cfs @ 12.09 hrs, Volume= 0.009 af, Depth> 8.28"

Routed to Pond 3P: Stone Under Deck

A	rea (sf)	CN [Description		
	560	98 F	Roofs, HSC	G C	
	560	1	00.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

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Summary for Subcatchment 14S: Subcatchment 14S

Runoff = 0.11 cfs @ 12.09 hrs, Volume=

0.009 af, Depth> 8.28"

Routed to Pond 4P: Stone Under Deck

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Area (s	f)	CN	Description		
	56	60	98	Roofs, HSG	G C	
	56	0		100.00% In	npervious A	Area
T (mir	c Lenç	_	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.	0					Direct Entry,

Summary for Subcatchment 15S: Subcatchment 15S

Runoff = 0.15 cfs @ 12.09 hrs, Volume=

0.012 af, Depth> 8.28"

Routed to Pond 5P: Lined Stone Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description						
	590	98	Roofs, HSG C						
	189	98	Water Surfa	ace, 0% imp	ip, HSG C				
	779	98	Veighted Average						
	189		24.26% Pervious Area						
	590		75.74% lmp	pervious Ar	rea				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	,	(cfs)	2000p				
6.0					Direct Entry,				

Summary for Subcatchment 16S: Subcatchment 15S

Runoff = 0.15 cfs @ 12.09 hrs, Volume=

0.012 af, Depth> 8.28"

Routed to Pond 6P: Lined Stone Drip Edge

Area (sf) Cl	N	Description				
5	90 9	98	Roofs, HSG C				
1	89 9	8	Water Surface, 0% imp, HSG C				
7	79 9	98	Weighted Average				
1	89		24.26% Pervious Area				
5	90		75.74% Impervious Area				

Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

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		_	•	•	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
-	6.0		·		·	Direct Entry,

Summary for Subcatchment 17S: Subcatchment 17S

0.012 af, Depth> 8.28" 0.15 cfs @ 12.09 hrs, Volume=

Routed to Pond 7P: Lined Stone Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description							
	590	98	Roofs, HSC	Roofs, HSG C						
	189	98	Water Surfa	ace, 0% imp	p, HSG C					
	779	98	Weighted A	Veighted Average						
	189		24.26% Pervious Area							
	590		75.74% lmp	pervious Ar	rea					
Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	Description					
6.0	(1001)	(12/12)	(14,000)	(0.0)	Direct Entry,					

Direct Entry,

Summary for Subcatchment 18S: Subcatchment 18S

Runoff 0.15 cfs @ 12.09 hrs, Volume= 0.012 af, Depth> 8.28"

Routed to Pond 8P: Lined Stone Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description							
_	590	98	Roofs, HSG C							
	189	98	Water Surface, 0% imp, HSG C							
	779	98	B Weighted Average							
	189	24.26% Pervious Area								
	590		75.74% Impervious Area							
Tc (min)	Length (feet)	Slope (ft/ft	,	Capacity (cfs)	Description					
6.0					Direct Entry,					

Direct Entry,

Summary for Subcatchment 19S: Subcatchment 19S

1.36 cfs @ 12.09 hrs, Volume= Runoff 0.100 af, Depth> 5.76"

Routed to Pond 1P: Bioretention Pond

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A	rea (sf)	CN D	escription					
	7,947	74 >75% Grass cover, Good, HSG C						
	695	98 Roofs, HSG C						
	400	98 Paved parking, HSG C						
	9,042	77 Weighted Average						
	7,947	87.89% Pervious Area						
	1,095	12.11% Impervious Area						
·								
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
2.5	43	0.0930	0.29		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.70"			
0.4	7	0.3333	0.33		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.70"			
0.0	8	0.3333	4.04		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
2.9	58	Total, I	ncreased t	o minimum	n Tc = 6.0 min			

Summary for Reach 2R: Flow across Map 222 Lot 20

Inflow Area = 0.040 ac, 0.00% Impervious, Inflow Depth > 5.40" for 50 Yr 24 Hr +15% event

Inflow = 0.24 cfs @ 12.09 hrs, Volume= 0.018 af

Outflow = 0.24 cfs @ 12.11 hrs, Volume= 0.018 af, Atten= 2%, Lag= 1.1 min

Routed to Reach 3R: Flow over Sagamore Ave

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.86 fps, Min. Travel Time= 1.6 min Avg. Velocity = 0.31 fps, Avg. Travel Time= 4.3 min

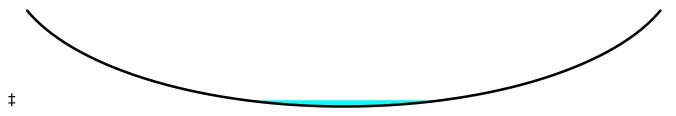
Peak Storage= 23 cf @ 12.11 hrs

Average Depth at Peak Storage= 0.03', Surface Width= 12.77' Bank-Full Depth= 0.50' Flow Area= 16.7 sf, Capacity= 88.18 cfs

50.00' x 0.50' deep Parabolic Channel, n= 0.030 Short grass

Length= 81.0' Slope= 0.0494 '/'

Inlet Invert= 66.00', Outlet Invert= 62.00'



Summary for Reach 3R: Flow over Sagamore Ave

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[62] Hint: Exceeded Reach 2R OUTLET depth by 1.14' @ 12.10 hrs

[64] Warning: Exceeded Reach 2R outlet bank by 0.68' @ 12.09 hrs

Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

18134-PROPOSED

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Inflow Area = 0.414 ac, 46.45% Impervious, Inflow Depth > 6.70" for 50 Yr 24 Hr +15% event

Inflow = 3.04 cfs @ 12.09 hrs, Volume= 0.231 af

Outflow = 3.05 cfs @ 12.09 hrs, Volume= 0.231 af, Atten= 0%, Lag= 0.2 min

Routed to Reach AP1: Analysis Point 1 (New CB)

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.85 fps, Min. Travel Time= 0.2 min Avg. Velocity = 1.51 fps, Avg. Travel Time= 0.5 min

Peak Storage= 36 cf @ 12.09 hrs

Average Depth at Peak Storage= 0.18', Surface Width= 8.94' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 48.65 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough

Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 45.0' Slope= 0.0444 '/'

‡

Inlet Invert= 63.00', Outlet Invert= 61.00'

Summary for Reach 6RA: Flow through 3S

Inflow = 0.17 cfs @ 12.21 hrs, Volume= 0.004 af

Outflow = 0.16 cfs @ 12.22 hrs, Volume= 0.004 af, Atten= 2%, Lag= 0.4 min

Routed to Reach 6RB: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 1.21 fps, Min. Travel Time= 0.5 min

Avg. Velocity = 0.71 fps, Avg. Travel Time= 0.8 min

Peak Storage= 5 cf @ 12.22 hrs

Average Depth at Peak Storage= 0.01', Surface Width= 15.86'

Bank-Full Depth= 0.50' Flow Area= 33.3 sf, Capacity= 464.76 cfs

100.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight

Length= 35.0' Slope= 0.3429 '/'

Inlet Invert= 66.00', Outlet Invert= 54.00'



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Summary for Reach 6RB: Flow through 3S

[62] Hint: Exceeded Reach 6RA OUTLET depth by 0.01' @ 12.25 hrs

Inflow = 0.16 cfs @ 12.22 hrs, Volume= 0.004 af

Outflow = 0.15 cfs @ 12.24 hrs, Volume= 0.004 af, Atten= 5%, Lag= 1.3 min

Routed to Reach 6RC: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.97 fps, Min. Travel Time= 0.7 min

Avg. Velocity = 0.46 fps, Avg. Travel Time= 1.4 min

Peak Storage= 6 cf @ 12.24 hrs

Average Depth at Peak Storage= 0.02', Surface Width= 10.59'

Bank-Full Depth= 0.50' Flow Area= 16.7 sf, Capacity= 127.08 cfs

50.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight

Length= 39.0' Slope= 0.1026 '/'

Inlet Invert= 54.00', Outlet Invert= 50.00'



Summary for Reach 6RC: Flow through 3S

[90] Warning: Qout>Qin may require smaller dt or Finer Routing [61] Hint: Exceeded Reach 6RB outlet invert by 0.01' @ 12.25 hrs

Inflow = 0.15 cfs @ 12.24 hrs, Volume= 0.004 af

Outflow = 0.16 cfs @ 12.25 hrs, Volume= 0.004 af, Atten= 0%, Lag= 0.7 min

Routed to Reach AP3: Analysis Point 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 1.12 fps, Min. Travel Time= 0.7 min

Avg. Velocity = 0.63 fps, Avg. Travel Time= 1.2 min

Peak Storage= 6 cf @ 12.25 hrs

Average Depth at Peak Storage= 0.01', Surface Width= 16.23'

Bank-Full Depth= 0.50' Flow Area= 33.3 sf. Capacity= 409.88 cfs

100.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight

Length= 45.0' Slope= 0.2667 '/'

Inlet Invert= 50.00', Outlet Invert= 38.00'

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Summary for Reach 7R: Flow Through 3S

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

Inflow Area = 0.539 ac, 45.26% Impervious, Inflow Depth > 6.72" for 50 Yr 24 Hr +15% event

Inflow = 2.75 cfs @ 12.18 hrs, Volume= 0.302 af

Outflow = 2.82 cfs @ 12.20 hrs, Volume= 0.302 af, Atten= 0%, Lag= 1.2 min

Routed to Reach 8R: Ditch on Tidewatch Property

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 4.33 fps, Min. Travel Time= 0.8 min Avg. Velocity = 1.26 fps, Avg. Travel Time= 2.9 min

Peak Storage= 143 cf @ 12.20 hrs

Average Depth at Peak Storage= 0.18', Surface Width= 4.10' Bank-Full Depth= 1.00' Flow Area= 6.0 sf, Capacity= 66.79 cfs

3.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 3.0 '/' Top Width= 9.00'

Length= 220.0' Slope= 0.0909 '/'

Inlet Invert= 58.00', Outlet Invert= 38.00'



Summary for Reach 8R: Ditch on Tidewatch Property

[62] Hint: Exceeded Reach 7R OUTLET depth by 0.25' @ 12.20 hrs

Inflow Area = 0.539 ac, 45.26% Impervious, Inflow Depth > 6.71" for 50 Yr 24 Hr +15% event

Inflow = 2.82 cfs @ 12.20 hrs, Volume= 0.302 af

Outflow = 2.78 cfs @ 12.21 hrs, Volume= 0.302 af, Atten= 1%, Lag= 0.7 min

Routed to Reach AP3: Analysis Point 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 2.81 fps, Min. Travel Time= 0.9 min

Avg. Velocity = 1.01 fps, Avg. Travel Time= 2.6 min

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Peak Storage= 157 cf @ 12.21 hrs

Average Depth at Peak Storage= 0.43', Surface Width= 3.59' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.18 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value = 3.0 '/' Top Width = 7.00'

Length= 159.0' Slope= 0.0189 '/'

Inlet Invert= 38.00', Outlet Invert= 35.00'



Summary for Reach 9R: Flow through 19S

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 8.27" for 50 Yr 24 Hr +15% event

Inflow = 0.14 cfs @ 12.10 hrs, Volume= 0.012 af

Outflow = 0.14 cfs @ 12.11 hrs, Volume= 0.012 af, Atten= 1%, Lag= 0.6 min

Routed to Pond 1P: Bioretention Pond

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.82 fps, Min. Travel Time= 0.8 min Avg. Velocity = 0.25 fps, Avg. Travel Time= 2.6 min

Peak Storage= 7 cf @ 12.11 hrs

Average Depth at Peak Storage= 0.05', Surface Width= 4.41' Bank-Full Depth= 0.50' Flow Area= 5.3 sf, Capacity= 16.36 cfs

3.00' x 0.50' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 15.0 '/' Top Width= 18.00'

Length= 39.0' Slope= 0.0205 '/'

Inlet Invert= 63.80', Outlet Invert= 63.00'



Summary for Reach 10Ra: Flow through 4S

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 8.27" for 50 Yr 24 Hr +15% event

Inflow = 0.14 cfs @ 12.10 hrs, Volume= 0.012 af

Outflow = 0.14 cfs @ 12.10 hrs, Volume= 0.012 af, Atten= 1%, Lag= 0.2 min

Routed to Reach 10Rb: Flow through 4S

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 1.08 fps, Min. Travel Time= 0.3 min

Avg. Velocity = 0.84 fps, Avg. Travel Time= 0.4 min

Peak Storage= 2 cf @ 12.10 hrs

Average Depth at Peak Storage= 0.01', Surface Width= 20.13'

Bank-Full Depth= 0.50' Flow Area= 12.5 sf, Capacity= 199.20 cfs

20.00' x 0.50' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 10.0 '/' Top Width= 30.00'

Length= 18.0' Slope= 0.3333 '/'

Inlet Invert= 64.00', Outlet Invert= 58.00'



Summary for Reach 10Rb: Flow through 4S

[61] Hint: Exceeded Reach 10Ra outlet invert by 0.01' @ 12.10 hrs

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 8.27" for 50 Yr 24 Hr +15% event

Inflow = 0.14 cfs @ 12.10 hrs, Volume= 0.012 af

Outflow = 0.14 cfs @ 12.11 hrs, Volume= 0.012 af, Atten= 1%, Lag= 0.6 min

Routed to Reach AP4: Analysis Point 4

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.96 fps, Min. Travel Time= 0.9 min

Avg. Velocity = 0.70 fps, Avg. Travel Time= 1.2 min

Peak Storage= 8 cf @ 12.11 hrs

Average Depth at Peak Storage= 0.01', Surface Width= 20.15'

Bank-Full Depth= 0.50' Flow Area= 12.5 sf, Capacity= 167.36 cfs

20.00' x 0.50' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 10.0 '/' Top Width= 30.00'

Length= 51.0' Slope= 0.2353 '/'

Inlet Invert= 58.00', Outlet Invert= 46.00'



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Summary for Reach AP1: Analysis Point 1 (New CB)

[40] Hint: Not Described (Outflow=Inflow)

0.414 ac, 46.45% Impervious, Inflow Depth > 6.70" for 50 Yr 24 Hr +15% event Inflow Area =

Inflow 3.05 cfs @ 12.09 hrs, Volume= 0.231 af

Outflow 3.05 cfs @ 12.09 hrs, Volume= 0.231 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

0.040 ac, 0.00% Impervious, Inflow Depth > 5.40" for 50 Yr 24 Hr +15% event Inflow Area =

Inflow 0.24 cfs @ 12.09 hrs, Volume= 0.018 af

0.24 cfs @ 12.09 hrs, Volume= 0.018 af, Atten= 0%, Lag= 0.0 min Outflow

Routed to Reach 2R: Flow across Map 222 Lot 20

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

1.560 ac, 15.65% Impervious, Inflow Depth > 5.72" for 50 Yr 24 Hr +15% event Inflow Area =

Inflow 7.72 cfs @ 12.19 hrs, Volume= 0.744 af

7.72 cfs @ 12.19 hrs, Volume= Outflow 0.744 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

0.482 ac, 8.04% Impervious, Inflow Depth > 5.73" for 50 Yr 24 Hr +15% event Inflow Area =

Inflow 2.97 cfs @ 12.11 hrs, Volume= 0.230 af

Outflow 2.97 cfs @ 12.11 hrs, Volume= 0.230 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Bioretention Pond

0.539 ac, 45.26% Impervious, Inflow Depth > 6.73" for 50 Yr 24 Hr +15% event Inflow Area =

3.90 cfs @ 12.09 hrs, Volume= Inflow 0.302 af

2.75 cfs @ 12.18 hrs, Volume= 2.75 cfs @ 12.18 hrs, Volume= 0.302 af, Atten= 30%, Lag= 5.3 min Outflow =

0.302 af Primary

Routed to Reach 7R: Flow Through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Volume

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Peak Elev= 61.96' @ 12.18 hrs Surf.Area= 1,141 sf Storage= 1,144 cf

Plug-Flow detention time= 4.4 min calculated for 0.302 af (100% of inflow)

Avail.Storage Storage Description

Center-of-Mass det. time= 3.6 min (783.1 - 779.5)

Invert

TOTALLIO		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		- c.c.a.g.c	Bocompaion		
#1	58.0	9'	2,583 cf	Custom	n Stage Data (Irreg	ular)Listed below (I	Recalc)
Elevatio		Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
58.0)9	117	48.0	0.0	0	0	117
58.1	10	117	48.0	40.0	0	0	117
59.0)9	117	48.0	40.0	46	47	165
59.1	10	117	48.0	15.0	0	47	165
60.5	59	117	48.0	15.0	26	73	237
60.6	30	117	48.0	100.0	1	74	237
61.0	00	764	120.0	100.0	157	232	1,201
62.0	00	1,157	143.0	100.0	954	1,185	1,700
63.0	00	1,618	164.0	100.0	1,381	2,566	2,235
63.0)1	1,618	164.0	100.0	16	2,583	2,237
Device	Routing	lnv	vert Outle	et Device	es		
#1	Primary	58.	.35' 12.0	" Round	d Culvert		
	•		L= 2	0.0' CPI	P, projecting, no he	adwall, Ke= 0.900	
			Inlet	/ Outlet I	nvert= 58.35' / 58.0	0' S= 0.0175 '/' C	Cc= 0.900
			n= 0	.012, Flo	ow Area= 0.79 sf		
#2	Device 1	58.	.35' 6.0"	Vert. Or	ifice/Grate C= 0.6	600 Limited to weir	flow at low heads
#3	Device 1	61.			Orifice/Grate C= 0 ir flow at low heads		

Primary OutFlow Max=2.69 cfs @ 12.18 hrs HW=61.96' TW=58.18' (Dynamic Tailwater)

1=Culvert (Passes 2.69 cfs of 5.26 cfs potential flow)

2=Orifice/Grate (Orifice Controls 1.73 cfs @ 8.82 fps)

-3=Orifice/Grate (Weir Controls 0.95 cfs @ 1.29 fps)

Summary for Pond 1PF: Sediment Forebay

[43] Hint: Has no inflow (Outflow=Zero)

Volume	Invert	Avail.Storage	Storage	Description	
#1	61.00'	272 cf	Custon	n Stage Data (Pri	smatic)Listed below (Recalc)
Elevation (feet)	Surf.A (sq		c.Store ic-feet)	Cum.Store (cubic-feet)	
61.00	-	9	0	0	
62.00	1	119	64	64	
63.00	2	297	208	272	

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Summary for Pond 3P: Stone Under Deck

Ledge surface modelled 24" below original grade based on TP 13 (Bedrock found from 24" to 36". High existing contour within footprint of stone is 63.0 and therefore ledge surface modelled at 61.0

Inflow Area =	0.031 ac, 85.88% Impervious, Inflow	Depth > 8.28" for 50 Yr 24 Hr +15% event		
Inflow =	0.25 cfs @ 12.09 hrs, Volume=	0.021 af		
Outflow =	0.18 cfs @ 12.21 hrs, Volume=	0.016 af, Atten= 30%, Lag= 7.2 min		
Discarded =	0.01 cfs @ 12.15 hrs, Volume=	0.012 af		
Secondary =	0.17 cfs @ 12.21 hrs, Volume=	0.004 af		
Routed to Reach 6RA : Flow through 3S				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 65.04' @ 12.15 hrs Surf.Area= 0.006 ac Storage= 0.009 af

Plug-Flow detention time= 232.7 min calculated for 0.016 af (76% of inflow) Center-of-Mass det. time= 148.6 min (889.2 - 740.6)

Volume	Invert	Avail.Storage	Storage Description
#1	61.73'	0.009 af	14.00'W x 20.00'L x 3.31'H Prismatoid 0.021 af Overall x 40.0% Voids
Device	Routing	Invert Ou	utlet Devices
#0	Secondary	65.04' A ı	utomatic Storage Overflow (Discharged without head)
#1	Discarded	61.73' 0. 3	300 in/hr Exfiltration over Surface area
		Co	onductivity to Groundwater Elevation = 61.00' Phase-In= 0.10'

Discarded OutFlow Max=0.01 cfs @ 12.15 hrs HW=65.04' (Free Discharge) **1=Exfiltration** (Controls 0.01 cfs)

Secondary OutFlow Max=0.00 cfs @ 12.21 hrs HW=65.04' TW=66.01' (Dynamic Tailwater)

Summary for Pond 4P: Stone Under Deck

Ledge surface modelled 20" below original grade based on TP 12 (Bedrock ranging from 20" to 28". High existing grade within footprint of practice is 64.0 and therefore ledge surface modelled at 62.33

Inflow Area =	0.031 ac, 85.88% Impervious, Inflow	Depth > 8.28" for 50 Yr 24 Hr +15% event			
Inflow =	0.25 cfs @ 12.09 hrs, Volume=	0.021 af			
Outflow =	0.10 cfs @ 12.32 hrs, Volume=	0.021 af, Atten= 61%, Lag= 13.8 min			
Discarded =	0.10 cfs @ 12.32 hrs, Volume=	0.021 af			
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af			
Routed to Reach 6RA : Flow through 3S					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 64.34' @ 12.32 hrs Surf.Area= 0.006 ac Storage= 0.005 af

Plug-Flow detention time= 35.1 min calculated for 0.021 af (99% of inflow) Center-of-Mass det. time= 30.7 min (771.0 - 740.2)

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Volume	Invert	Avail.Storage	Storage Description
#1	62.37'	0.006 af	14.00'W x 20.00'L x 2.41'H Prismatoid 0.015 af Overall x 40.0% Voids
Device	Routing	Invert O	utlet Devices
#0	Secondary	64.78' A ı	utomatic Storage Overflow (Discharged without head)
#1	Discarded	62.37' 0. 3	300 in/hr Exfiltration over Surface area
		Co	onductivity to Groundwater Elevation = 62.33' Phase-In= 0.10'

Discarded OutFlow Max=0.10 cfs @ 12.32 hrs HW=64.33' (Free Discharge) **1=Exfiltration** (Controls 0.10 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=62.37' TW=66.00' (Dynamic Tailwater)

Summary for Pond 5P: Lined Stone Drip Edge

0.018 ac, 75.74% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr +15% event Inflow Area = Inflow = 0.15 cfs @ 12.09 hrs, Volume= 0.012 af 0.15 cfs @ 12.09 hrs, Volume= Outflow 0.012 af, Atten= 0%, Lag= 0.4 min 0.15 cfs @ 12.09 hrs, Volume= 0.012 af Primary Routed to Pond 3P : Stone Under Deck 0.00 cfs @ 0.00 hrs, Volume= Secondary = 0.000 af Routed to Reach 6RA: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.09' @ 12.09 hrs Surf.Area= 0.003 ac Storage= 0.000 af

Plug-Flow detention time= 1.3 min calculated for 0.012 af (100% of inflow) Center-of-Mass det. time= 1.0 min (741.0 - 740.0)

Volume	Invert	Avail.Stora	ge Storage Description
#1	66.00'	0.001	af 2.00'W x 63.00'L x 1.01'H Prismatoid 0.003 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#0	Secondary	67.01'	Automatic Storage Overflow (Discharged without head)
#1	Primary	66.00'	6.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#2	Secondary	67.00'	63.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Primary OutFlow Max=0.14 cfs @ 12.09 hrs HW=66.09' TW=64.75' (Dynamic Tailwater) 1=Orifice/Grate (Weir Controls 0.14 cfs @ 0.99 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=66.00' TW=66.00' (Dynamic Tailwater)

2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 6P: Lined Stone Drip Edge

[44] Hint: Outlet device #1 is below defined storage

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr +15% event

Inflow = 0.15 cfs @ 12.09 hrs, Volume= 0.012 af

Outflow = 0.15 cfs @ 12.09 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.4 min

Primary = 0.15 cfs @ 12.09 hrs, Volume= 0.012 af

Routed to Pond 4P : Stone Under Deck

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach 6RA: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.09' @ 12.09 hrs Surf.Area= 0.003 ac Storage= 0.000 af

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 0.4 min (740.4 - 740.0)

Volume	Invert	Avail.Storage	Storage Description
#1	66.01'	0.001 af	2.00'W x 63.00'L x 1.01'H Prismatoid
			0.003 af Overall x 40.0% Voids

Device	Routing	Invert	Outlet Devices
#1	Primary	66.00'	6.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#2	Secondary	67.00'	63.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3 30 3 31 3 32

Primary OutFlow Max=0.14 cfs @ 12.09 hrs HW=66.09' TW=63.85' (Dynamic Tailwater) 1=Orifice/Grate (Weir Controls 0.14 cfs @ 0.99 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=66.01' TW=66.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 7P: Lined Stone Drip Edge

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr +15% event

Inflow = 0.15 cfs @ 12.09 hrs, Volume= 0.012 af

Outflow = 0.14 cfs @ 12.10 hrs, Volume= 0.012 af, Atten= 1%, Lag= 0.9 min

Primary = 0.14 cfs @ 12.10 hrs, Volume= 0.012 af

Routed to Reach 9R: Flow through 19S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 64.26' @ 12.10 hrs Surf.Area= 0.003 ac Storage= 0.000 af

Plug-Flow detention time= 5.5 min calculated for 0.012 af (100% of inflow) Center-of-Mass det. time= 4.0 min (744.0 - 740.0)

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Volume	Invert	Avail.Stora	age Storage Description
#1	64.00'	0.001	af 2.00'W x 63.00'L x 1.01'H Prismatoid
			0.003 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#1	Primary	64.00'	6.0" Round Culvert
	•		L= 4.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 64.00' / 63.80' S= 0.0500 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.20 sf
#2	Device 1	64.00'	6.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Primary	65.00'	63.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Primary OutFlow Max=0.14 cfs @ 12.10 hrs HW=64.26' TW=63.85' (Dynamic Tailwater)

-1=Culvert (Inlet Controls 0.14 cfs @ 1.38 fps)

2=Orifice/Grate (Passes 0.14 cfs of 0.48 cfs potential flow)

-3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 8P: Lined Stone Drip Edge

0.018 ac, 75.74% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr +15% event Inflow Area =

Inflow 0.012 af 0.15 cfs @ 12.09 hrs, Volume=

0.14 cfs @ 12.10 hrs, Volume= Outflow 0.012 af, Atten= 1%, Lag= 0.9 min

Primary = 0.14 cfs @ 12.10 hrs, Volume= 0.012 af

Routed to Reach 10ra: Flow through 4S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 64.76' @ 12.10 hrs Surf.Area= 0.003 ac Storage= 0.000 af

Plug-Flow detention time= 5.5 min calculated for 0.012 af (100% of inflow) Center-of-Mass det. time= 4.0 min (744.0 - 740.0)

Volume	Invert	Avail.Stora	age Storage Description
#1	64.50'	0.001	af 2.00'W x 63.00'L x 1.01'H Prismatoid 0.003 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#1	Primary	64.50'	6.0" Round Culvert L= 4.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 64.50' / 64.00' S= 0.1250 '/' Cc= 0.900 n= 0.012, Flow Area= 0.20 sf
#2 #3	Device 1 Primary	64.50' 65.50'	6.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads 63.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

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Primary OutFlow Max=0.14 cfs @ 12.10 hrs HW=64.76' TW=64.01' (Dynamic Tailwater)

_1=Culvert (Inlet Controls 0.14 cfs @ 1.38 fps)

2=Orifice/Grate (Passes 0.14 cfs of 0.48 cfs potential flow)

-3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond CB101: Catch Basin 101

Inflow Area = 0.130 ac, 59.12% Impervious, Inflow Depth > 7.12" for 50 Yr 24 Hr +15% event

Inflow = 0.99 cfs @ 12.09 hrs, Volume= 0.077 af

Outflow = 0.99 cfs @ 12.09 hrs, Volume= 0.077 af, Atten= 0%, Lag= 0.0 min

Primary = 0.99 cfs @ 12.09 hrs, Volume= 0.077 af

Routed to Pond CB102: Catch Basin 102

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 67.39' @ 12.09 hrs

Flood Elev= 70.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	66.60'	12.0" Round Culvert
			L= 14.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 66.60' / 66.50' S= 0.0071 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.97 cfs @ 12.09 hrs HW=67.37' TW=67.22' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.97 cfs @ 1.49 fps)

Summary for Pond CB102: Catch Basin 102

Inflow Area = 0.152 ac, 65.02% Impervious, Inflow Depth > 7.29" for 50 Yr 24 Hr +15% event

Inflow = 1.17 cfs @ 12.09 hrs, Volume= 0.092 af

Outflow = 1.17 cfs @ 12.09 hrs, Volume= 0.092 af, Atten= 0%, Lag= 0.0 min

Primary = 1.17 cfs @ 12.09 hrs, Volume= 0.092 af

Routed to Pond CB104: Catch Basin 104

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 67.24' @ 12.09 hrs

Flood Elev= 70.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	66.40'	12.0" Round Culvert
			L= 84.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 66.40' / 65.90' S= 0.0060 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=1.14 cfs @ 12.09 hrs HW=67.22' TW=66.92' (Dynamic Tailwater) 1=Culvert (Outlet Controls 1.14 cfs @ 2.26 fps)

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Summary for Pond CB103: Catch Basin 103

Inflow Area = 0.155 ac, 64.18% Impervious, Inflow Depth > 7.22" for 50 Yr 24 Hr +15% event

Inflow 1.17 cfs @ 12.09 hrs. Volume= 0.093 af

1.17 cfs @ 12.09 hrs, Volume= Outflow 0.093 af, Atten= 0%, Lag= 0.0 min

1.17 cfs @ 12.09 hrs, Volume= Primary 0.093 af

Routed to Pond CB104: Catch Basin 104

Routing by Dvn-Stor-Ind method. Time Span= 0.00-24.00 hrs. dt= 0.05 hrs / 3

Peak Elev= 68.25' @ 12.09 hrs

Flood Elev= 72.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	67.60'	12.0" Round Culvert
			L= 42.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 67.60' / 67.30' S= 0.0071 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=1.14 cfs @ 12.09 hrs HW=68.24' TW=66.92' (Dynamic Tailwater) 1=Culvert (Inlet Controls 1.14 cfs @ 2.15 fps)

Summary for Pond CB104: Catch Basin 104

Inflow Area = 0.314 ac, 65.44% Impervious, Inflow Depth > 7.28" for 50 Yr 24 Hr +15% event

2.40 cfs @ 12.09 hrs. Volume= Inflow = 0.190 af

2.40 cfs @ 12.09 hrs, Volume= 2.40 cfs @ 12.09 hrs, Volume= Outflow 0.190 af, Atten= 0%, Lag= 0.0 min

Primary 0.190 af

Routed to Pond 1P: Bioretention Pond

Routing by Dvn-Stor-Ind method. Time Span= 0.00-24.00 hrs. dt= 0.05 hrs / 3

Peak Elev= 66.94' @ 12.09 hrs

Flood Elev= 71.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	65.80'	12.0" Round Culvert
	-		L= 31.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 65.80' / 65.60' S= 0.0065 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=2.34 cfs @ 12.09 hrs HW=66.92' TW=61.64' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 2.34 cfs @ 2.98 fps)

Summary for Pond YD1: Yard Drain 1

Inflow Area = 0.105 ac, 49.42% Impervious, Inflow Depth > 6.84" for 50 Yr 24 Hr +15% event

Inflow 0.79 cfs @ 12.09 hrs, Volume= 0.060 af

0.79 cfs @ 12.09 hrs, Volume= Outflow 0.060 af, Atten= 0%, Lag= 0.0 min

0.79 cfs @ 12.09 hrs, Volume= 0.060 af Primary

Routed to Pond CB101: Catch Basin 101

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

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Peak Elev= 67.98' @ 12.09 hrs Flood Elev= 69.30'

Device	Routing	Invert	Outlet Devices
#1	Primary	67.30'	8.0" Round Culvert
			L= 15.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 67.30' / 66.93' S= 0.0247 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.77 cfs @ 12.09 hrs HW=67.97' TW=67.37' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.77 cfs @ 2.19 fps)

Summary for Pond YD2: Yard Drain 2

Inflow Area = 0.086 ac, 35.30% Impervious, Inflow Depth > 6.36" for 50 Yr 24 Hr +15% event

Inflow = 0.61 cfs @ 12.09 hrs, Volume= 0.045 af

Outflow = 0.61 cfs @ 12.09 hrs, Volume= 0.045 af, Atten= 0%, Lag= 0.0 min

Primary = 0.61 cfs @ 12.09 hrs, Volume= 0.045 af

Routed to Pond CB103: Catch Basin 103

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 68.75' @ 12.09 hrs

Flood Elev= 70.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	68.20'	8.0" Round Culvert
	-		L= 13.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 68.20' / 67.93' S= 0.0208 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.59 cfs @ 12.09 hrs HW=68.74' TW=68.24' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.59 cfs @ 1.97 fps)

APPENDIX III

Test Pit Logs



GOVE ENVIRONMENTAL SERVICES, INC. TEST PIT DATA

Project 635 Sagamore Ave

Client 635 Sagamore Development LLC

GES Project No. GES 2021307

MM/DD/YY Staff 3-18-2022 JPG

Test Pit No. 1

ESHWT: n/a

Termination @ 15"

Refusal: 15" SCS Soil: Hollis

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0-5" **NONE FSL** GR 10YR 3/2 FR **NONE** 5-15" 10YR 5/6 **FSL** GR FR

Test Pit No. 2

ESHWT: n/a

Termination @ 25"

Refusal: 25" SCS Soil: Chatfield

Obs. Water: none

Redox; Quantity/Contrast Depth Color Texture Structure Consistence 0-5" 10YR 3/2 **FSL** GR FR **NONE** 5-25" **FSL** GR FR **NONE** 10YR 5/6

Test Pit No. 3

ESHWT: n/a

Termination @ 25"

Refusal: 25" SCS Soil: Chatfield

Obs. Water: none

Depth Color **Texture** Structure Consistence Redox; Quantity/Contrast 0-6" 10YR 3/2 **FSL** GR FR **NONE** NONE 6-25" **FSL** GR FR 10YR 5/6

Test Pit No. 4

ESHWT: n/a

Termination @ 15"

Refusal: 15" Obs. Water: none SCS Soil:

Hollis

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0–15" 10YR 3/2 FSL GR FR NONE

Test Pit No. 5

ESHWT: 30"

Termination @ 36"

Refusal: 36" SCS Soil: Chatfield variant

Obs. Water: none

Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-8"	10YR 3/2	FSL	GR	FR	NONE
8-30"	10YR 4/6	FSL	GR	FR	NONE
30-36"	2.5Y 5/3	FSL	GR	FR	10% Distinct

Test Pit No. 6

ESHWT: n/a

Termination @ 12"

Refusal: 12" SCS Soil: Hollis

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0–12" 10YR 3/2 FSL GR FR NONE

Test Pit No. 7

ESHWT: n/a

Termination @ 27"

Refusal: 27" SCS Soil: Chatfield

Obs. Water: none

Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0–4"	10YR 3/2	FSL	GR	FR	NONE
4–27"	10YR 5/6	FSL	GR	FR	NONE

Test Pit No. 8

ESHWT: 35"

Termination @ 40"

Refusal: 40" SCS Soil: Chatfield variant Obs. Water: none

Texture Structure Consistence Depth Color Redox; Quantity/Contrast 0-6" 10YR 3/2 FSL GR FR **NONE** 6-35" **NONE** 10YR 5/6 **FSL** GR FR 35-40" 2.5Y 5/3 **FSL** OM FI 10% Distinct

Test Pit No. 9

ESHWT: n/a

Termination @ 27"

Refusal: 27" SCS Soil: Chatfield

Obs. Water: none

Structure Redox; Quantity/Contrast Depth Color Texture Consistence 0-4" 10YR 3/2 **FSL** GR FR **NONE** 4-27" 10YR 5/6 **FSL** GR FR **NONE**

Test Pit No. 10

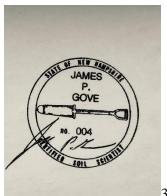
ESHWT: 35

Termination @ 62"

Refusal: 62" SCS Soil: Scituate

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0-10" 10YR 3/2 **FSL** GR FR NONE 10-35" **FSL** GR FR **NONE** 10YR 5/6 35-62" 2.5Y 5/3 **FSL** PL FΙ 10%, Distinct



Legend:

FSL = fine sandy loam GR = granular PL = platy FI = firm



GOVE ENVIRONMENTAL SERVICES, INC.

TEST PIT DATA

Project 635 Sagamore Ave., Portsmouth NH Client 635 Sagamore Development LLC

GES Project No. 2021308

MM/DD/YY Staff 07-24-2024 James Gove, CSS#004

Witnessed by: David Desfosses, City of Portsmouth

Test Pit No.11Soils Series:UdorthentsESHWT::noneLandscape:PavedTermination @32"Slope:B

Refusal: 32" Parent Material: Fill over till
Obs. Water: None Hydrologic Soil Group: Impervious

Horizon Color (Munsell) Texture Structure-Consistence-Redox Fill 1, 0-8" 10YR4/4 fine sandy loam massive-friable-none

Fill 1, 0-8" 10YR4/4 fine sandy loam massive-friable-none Fill 2, 8-19" 10YR2/1 ground pavement massive-firm-none Bw 18-32" 10YR5/6 fine sandy loam granular-friable-none

Test Pit No.12Soils Series:ChatfieldESHWT::noneLandscape:HillsideTermination @28"Slope:C

Refusal: 28" Parent Material: Bedrock Till

Obs. Water: None Hydrologic Soil Group: B

Horizon Color (Munsell) Texture Structure-Consistence-Redox

A 0-6" 10YR3/2 fine sandy loam granular-friable-none Bw 6-28" 10YR5/6 fine sandy loam granular-friable-none

Bedrock ranges from 20" to 28" in test pit.

Test Pit No.13Soils Series:ChatfieldESHWT::noneLandscape:HillsideTermination @36"Slope:C

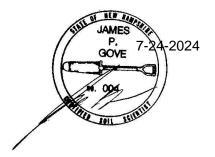
Refusal: 36" Parent Material: Bedrock Till

Obs. Water: None Hydrologic Soil Group: B

Horizon Color (Munsell) Texture Structure-Consistence-Redox fine sandy loam granular-friable-none A 0-6" 10YR3/2 Bw 6-24" 10YR4/6 fine sandy loam granular-friable-none C 24-36" fine sandy loam granular-friable-none 2.5Y5/3

Bedrock ranges from 24" to 36" in test pit.

Note: Site should be calculated as HSG C, due to the limited infiltration in thin soil layers above the bedrock.



Test Pit Data: 635 Sagamore Ave. 7-24-2024 —Page 4 of 4

APPENDIX IV

Site Specific Soil Survey Report and Map



GOVE ENVIRONMENTAL SERVICES, INC

SITE-SPECIFIC SOIL SURVEY REPORT
For
635 Sagamore Avenue, Portsmouth, NH
By
GES, Inc.
Project # 2021308
Date: 02-20-2024

1. MAPPING STANDARDS

Site-Specific Soil Mapping Standards for New Hampshire and Vermont. SSSNNE Special Publication No. 3, Version 7.0, July, 2021.

This map product is within the technical standards of the National Cooperative Soil Survey. It is a special purpose product, intended for infiltration requirements by the NH DES Alteration of Terrain Bureau. The soil map was produced by a professional soil scientist and is not a product of the USDA Natural Resources Conservation Service. This report accompanies the soil map.

The site-specific soil map (SSSM) was produced 2-20-2024; prepared by JP Gove, CSS #004, GES, Inc.

Soils were identified with the New Hampshire State-wide Numerical Soils Legend, USDA NRCS, Durham, NH. Issue # 10, January 2011.

Hydrologic Soil Group was determined using SSSNNE Special Publication No. 5, Ksat Values for New Hampshire Soils, September 2009.

High Intensity Soil Map symbols, based upon SSSNNE Special Publication 1, December 2017, were added to the Soil Legend.

Scale of soil map: Approximately 1" = 20'.

Contours Interval: 2 feet

2. LANDFORMS & EXISTING CONDITIONS:

The site is located on sloping hillside that is bedrock controlled. Rock outcrops are numerous. At the top of the hill, adjacent Sagamore Avenue, is an existing commercial building and paved areas. Behind the impervious areas to the south, the hillside slopes downward. The area is forested in white pines. There are no wetlands on the site.

3. <u>DATE SOIL MAP PRODUCED</u>

Date(s) of on-site field work: 3-18-2022

Date(s) of test pits: 3-18-2922

Test pits recorded by: JP Gove, CSS # 004

4. GEOGRAPHIC LOCATION AND SIZE OF SITE

City or town where soil mapping was conducted: Portsmouth, NH

Location: Tax Map 222 Lot 19

Size of area: Approximately 2 acres

Was the map for the entire lot? Yes

If no, where was the mapping conducted on the parcel: n/a

5. PURPOSE OF THE SOIL MAP

Was the map prepared to meet the requirement of Alteration of Terrain? No

If no, what was the purpose of the map? City of Portsmouth requirements

Who was the map prepared for? Jones & Beach Engineers, Inc.



6. SOIL IDENTIFICATION LEGEND

Map	Unit Sym	ibol Map Unit N	lame		HISS Symb	ool	Hydrol	ogic Soil Group		
41	Chatfi	eld-Hollis-Rock C	outcrop complex		228		В			
289	Chatfi	eld Variant (mod	erately well drai	ned)	327 B			3		
699	Urban	Land			n/a		Imperv	rious		
SLOP	E PHASE:									
0-8%		В	8-15%	С		15-25%	,)	D		
25%-	50%	E	50%+	F						

7. NARRATIVE MAP UNIT DESCRIPTIONS

SITE-SPECIFIC MAP UNIT: 41

CORRELATED SOIL SERIES: Chatfield-Hollis-Rock Outcrop complex

LANDSCAPE SETTING: Sloping to very steep hillside.

CHARACTERISTIC SURFACE FEATURES: Numerous rock outcrops

DRAINAGE CLASS: Well drained

PARENT MATERIAL: Glacial Till

NATURE OF DISSIMILAR INCLUSIONS: With a complex, several similar soils are present. While the major soil is the moderately deep Chatfield, the shallow Hollis and the exposed ledge of the Rock Outcrop, are large minor components. Chatfield is 50%, Hollis is 25%, and Rock Outcrop is 25%. A few deeper soil areas are present in hollow in the bedrock.

ESTIMATED PERCENTAGE OF DISSIMILAR INCLUSIONS: less than 5%.

SOIL PROFILE DESCRIPTIONS- horizon designation, depth, soil texture, Munsell color notation, Munsell color of redox features, soil structure, soil consistence, estimated coarse fragments, estimated seasonal high water table (ESHWT), observed water table (OBSWT), kind of water table (perched, apparent, or both), depth to lithic or paralithic contact:

Test Pit No. 3

ESHWT: n/a

Termination @ 25"

Refusal: 25"

Obs. Water: none

SCS Soil: Chatfield

Structure Consistence Redox; Quantity/Contrast Depth Color Texture 0-6" 10YR 3/2 FSL GR FR **NONE** 6-25" 10YR 5/6 **FSL** GR FR **NONE**

No OBSWT, no ESHWT, lithic contact at 25", 20% rock fragments.

Test Pit No. 1

ESHWT: n/a

Termination @ 15"

Refusal: 15" SCS Soil: Hollis

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0-5" 10YR 3/2 FSL GR FR **NONE** 5-15" 10YR 5/6 **FSL** GR FR NONE

No OBSWT, no ESHWT, lithic contact at 15", 20% rock fragments.

SITE-SPECIFIC MAP UNIT: 289

CORRELATED SOIL SERIES: Chatfield Variant (moderately well drained)



LANDSCAPE SETTING: At the top of the slope, a slightly deeper soil area on the northwest corner of the site.

CHARACTERISTIC SURFACE FEATURES: Fewer outcrops than the rest of the site.

DRAINAGE CLASS: Moderately well drained.

PARENT MATERIAL: Glacial till.

NATURE OF DISSIMILAR INCLUSIONS: Scituate soils with a hard pan above the bedrock,

ESTIMATED PERCENTAGE OF DISSIMILAR INCLUSIONS: 5%

SOIL PROFILE DESCRIPTIONS- horizon designation, depth, soil texture, Munsell color notation, Munsell color of redox features, soil structure, soil consistence, estimated coarse fragments, estimated seasonal high water table (ESHWT), observed water table (OBSWT), kind of water table (perched, apparent, or both), depth to lithic or paralithic contact:

Test Pit No. 5

ESHWT: 30"

Termination @ 36"

Refusal: 36"

SCS Soil: Chatfield variant

Obs. Water: none

Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-8"	10YR 3/2	FSL	GR	FR	NONE
8-30"	10YR 4/6	FSL	GR	FR	NONE
30-36"	2.5Y 5/3	FSL	GR	FR	10% Distinct

ESHWT is 30", no OBSWT, lithic contact at 36", 20% rock fragments.

SITE-SPECIFIC MAP UNIT: 699

CORRELATED SOIL SERIES: Urban land

LANDSCAPE SETTING: Top of slope adjacent to Sagamore Avenue.

CHARACTERISTIC SURFACE FEATURES: Impervious.

DRAINAGE CLASS: N/A

PARENT MATERIAL: N/A

NATURE OF DISSIMILAR INCLUSIONS: N/A

ESTIMATED PERCENTAGE OF DISSIMILAR INCLUSIONS: N/A

SOIL PROFILE DESCRIPTIONS- horizon designation, depth, soil texture, Munsell color notation, Munsell color of redox features, soil structure, soil consistence, estimated coarse fragments, estimated seasonal high water table (ESHWT), observed water table (OBSWT), kind of water table (perched, apparent, or both), depth to lithic or paralithic contact:

N/A ---- Pavement and buildings.



8. RESPONSIBLE SOIL SCIENTIST

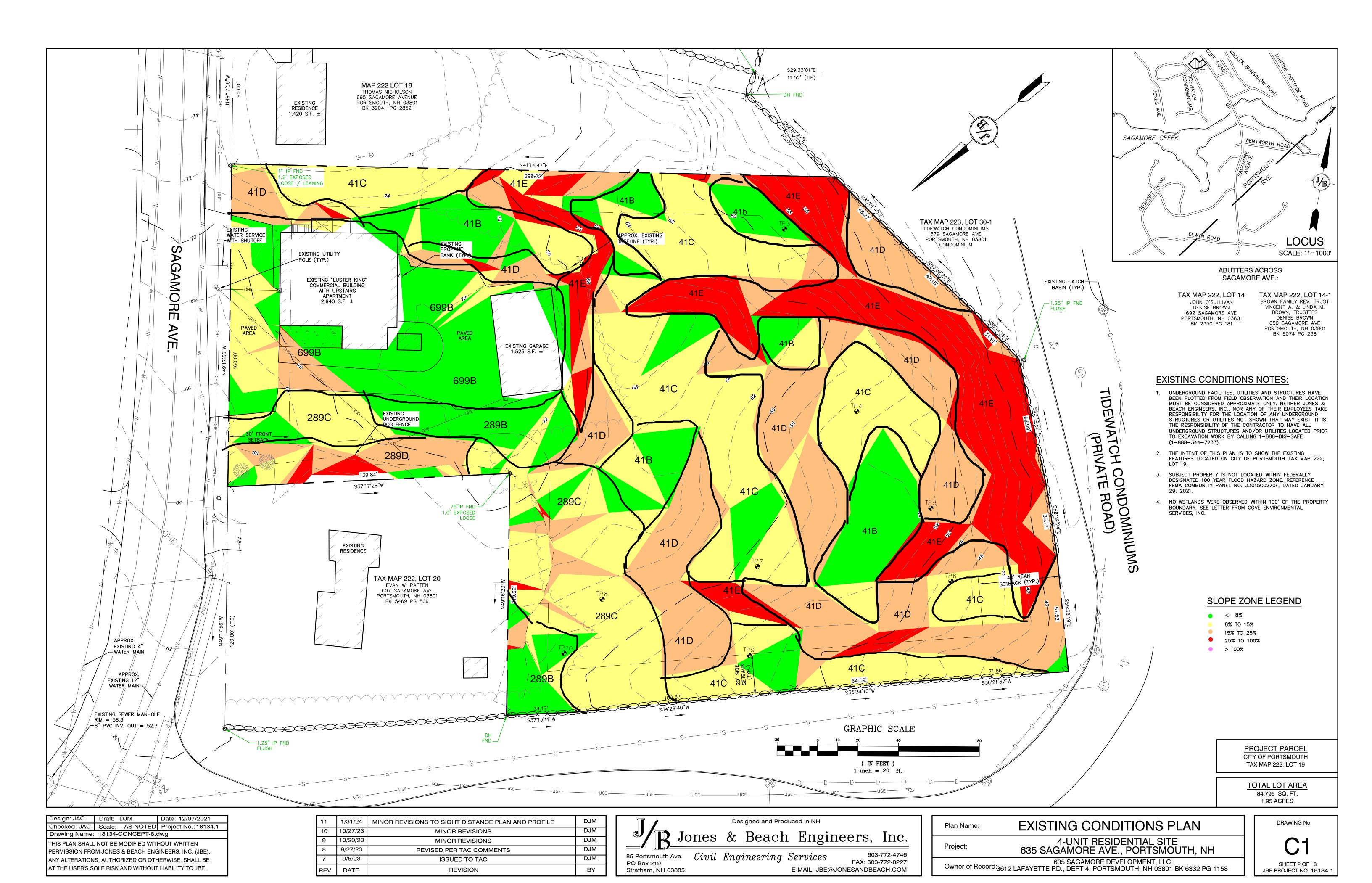
Name: James Gove

Certified Soil Scientist Number: 004

9. OTHER DISTINGUISHING FEATURES OF SITE

Is the site in a natural condition? Yes, with exception of existing development.

info@gesinc.biz



APPENDIX V

NRCS Soil Map



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons



Soil Map Unit Points

Special Point Features

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

+ Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot

Other

Special Line Features

Water Features

Δ

Streams and Canals

Transportation

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Rockingham County, New Hampshire Survey Area Data: Version 26, Aug 22, 2023

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Jun 19, 2020—Sep 20, 2020

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

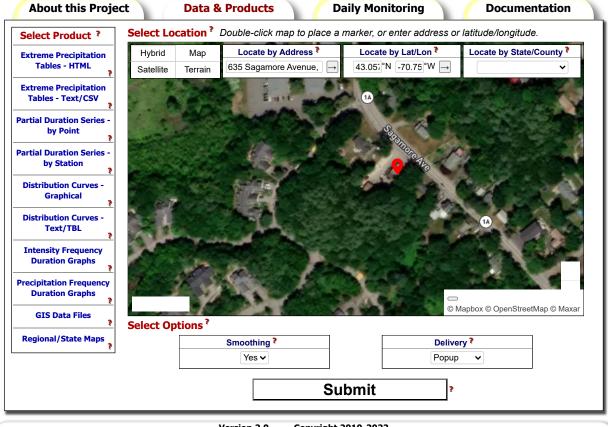
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
140B	Chatfield-Hollis-Canton complex, 0 to 8 percent slopes, rocky	0.7	30.5%
140D	Chatfield-Hollis-Canton complex, 15 to 35 percent slopes, rocky	1.6	69.5%
Totals for Area of Interest		2.3	100.0%

APPENDIX VI

Extreme Precipitation Estimates

Extreme Precipitation in New York & New England

An Interactive Web Tool for Extreme Precipitation Analysis



Version 2.0 Copyright 2010-2022
This project is a joint collaboration between:
Northeast Regional Climate Center (NRCC)
Natural Resources Conservation Service (NRCS)

SDA ONRCS
Contact: precip@cornell.edu

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Metadata for Point

Smoothing Yes

State Location

Latitude 43.058 degrees North Longitude 70.753 degrees West

Elevation 10 feet

Date/Time Wed Feb 21 2024 09:41:54 GMT-0500 (Eastern Standard

Time)

+15% due to location in Coastal/Great Bay Region

2yr: 3.22*1.15 = 3.70 in 10yr: 4.88*1.15 = 5.16 in 25yr: 6.19*1.15 = 7.12 in

50yr: 7.42*1.15 = 8.53 in

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day
1yr	0.26	0.40	0.50	0.65	0.82	1.04	1yr	0.70	0.98	1.21	1.56	2.03	2.67	2.94	1yr	2.36	2.82	3.24	3.96	4.57
2yr	0.32	0.50	0.62	0.82	1.03	1.30	2yr	0.89	1.18	1.52	1.94	2.49	3.22	3.58	2yr	2.85	3.45	3.95	4.70	5.35
5yr	0.37	0.58	0.73	0.98	1.25	1.61	5yr	1.08	1.47	1.89	2.44	3.15	4.08	4.60	5yr	3.61	4.42	5.07	5.96	6.73
10yr	0.41	0.65	0.82	1.12	1.46	1.90	10yr	1.26	1.73	2.24	2.90	3.76	4.88	5.55	10yr	4.32	5.34	6.12	7.14	8.01
25yr	0.48	0.76	0.97	1.34	1.78	2.35	25yr	1.54	2.15	2.79	3.65	4.76	6.19	7.13	25yr	5.48	6.86	7.85	9.07	10.09
50yr	0.54	0.86	1.11	1.55	2.08	2.77	50yr	1.80	2.54	3.31	4.35	5.69	7.42	8.62	50yr	6.57	8.29	9.48	10.87	12.02
100yr	0.60	0.97	1.25	1.78	2.43	3.28	100yr	2.10	2.99	3.93	5.19	6.80	8.89	10.42	100yr	7.87	10.02	11.46	13.04	14.33
200yr	0.68	1.11	1.44	2.06	2.85	3.86	200yr	2.46	3.54	4.65	6.17	8.12	10.65	12.60	200yr	9.43	12.12	13.85	15.64	17.09
500yr	0.81	1.33	1.73	2.51	3.51	4.80	500yr	3.03	4.41	5.81	7.76	10.28	13.54	16.21	500yr	11.98	15.59	17.81	19.90	21.58

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day
1yr	0.23	0.36	0.44	0.59	0.72	0.88	1yr	0.62	0.86	0.93	1.33	1.69	2.26	2.51	1yr	2.00	2.41	2.88	3.20	3.93
2yr	0.32	0.49	0.60	0.81	1.00	1.19	2yr	0.86	1.16	1.37	1.82	2.33	3.07	3.47	2yr	2.72	3.33	3.84	4.56	5.11
5yr	0.35	0.54	0.67	0.92	1.17	1.40	5yr	1.01	1.37	1.61	2.11	2.73	3.80	4.21	5yr	3.36	4.05	4.74	5.56	6.27
10yr	0.39	0.59	0.74	1.03	1.33	1.60	10yr	1.15	1.57	1.81	2.38	3.05	4.39	4.88	10yr	3.88	4.70	5.48	6.45	7.23
25yr	0.44	0.67	0.83	1.19	1.57	1.90	25yr	1.35	1.86	2.10	2.74	3.52	4.77	5.92	25yr	4.22	5.70	6.70	7.85	8.73
50yr	0.48	0.73	0.92	1.32	1.77	2.17	50yr	1.53	2.12	2.35	3.06	3.91	5.40	6.84	50yr	4.78	6.58	7.79	9.11	10.08
100yr	0.54	0.81	1.02	1.47	2.02	2.47	100yr	1.74	2.42	2.63	3.39	4.33	6.08	7.90	100yr	5.38	7.60	9.07	10.60	11.64
200yr	0.59	0.89	1.13	1.64	2.29	2.82	200yr	1.97	2.75	2.94	3.75	4.76	6.83	9.12	200yr	6.05	8.77	10.54	12.34	13.47
500yr	0.69	1.02	1.32	1.92	2.72	3.37	500yr	2.35	3.29	3.42	4.28	5.41	7.97	11.03	500yr	7.06	10.61	12.87	15.13	16.32

Upper Confidence Limits

5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day
0.29	0.44	0.54	0.72	0.89	1.08	1yr	0.77	1.06	1.26	1.74	2.20	2.99	3.18	1yr	2.64	3.05	3.59	4.38	5.06
0.34	0.52	0.64	0.87	1.07	1.27	2yr	0.92	1.24	1.48	1.96	2.51	3.43	3.72	2yr	3.03	3.57	4.10	4.86	5.64
0.40	0.62	0.77	1.05	1.34	1.63	5yr	1.16	1.59	1.89	2.54	3.25	4.36	4.98	5yr	3.85	4.79	5.40	6.40	7.18
0.47	0.72	0.89	1.25	1.61	1.98	10yr	1.39	1.94	2.29	3.11	3.96	5.36	6.22	10yr	4.74	5.98	6.84	7.87	8.78
0.58	0.88	1.09	1.56	2.06	2.58	25yr	1.77	2.52	2.96	4.08	5.17	7.77	8.36	25yr	6.87	8.04	9.18	10.37	11.44
0.67	1.03	1.28	1.84	2.48	3.15	50yr	2.14	3.08	3.61	5.01	6.35	9.71	10.48	50yr	8.60	10.08	11.48	12.76	14.00
0.80	1.20	1.51	2.17	2.98	3.83	100yr	2.57	3.75	4.39	6.18	7.80	12.14	13.13	100yr	10.74	12.62	14.35	15.74	17.13
0.93	1.40	1.78	2.57	3.58	4.69	200yr	3.09	4.58	5.36	7.61	9.60	15.22	16.46	200yr	13.47	15.83	17.96	19.40	20.96
1.16	1.72	2.22	3.22	4.58	6.09	500yr	3.95	5.95	6.96	10.07	12.65	20.54	22.22	500yr	18.18	21.36	24.18	25.57	27.38
	0.29 0.34 0.40 0.47 0.58 0.67 0.80	0.29 0.44 0.34 0.52 0.40 0.62 0.47 0.72 0.58 0.88 0.67 1.03 0.80 1.20 0.93 1.40	0.29 0.44 0.54 0.34 0.52 0.64 0.40 0.62 0.77 0.47 0.72 0.89 0.58 0.88 1.09 0.67 1.03 1.28 0.80 1.20 1.51 0.93 1.40 1.78	0.29 0.44 0.54 0.72 0.34 0.52 0.64 0.87 0.40 0.62 0.77 1.05 0.47 0.72 0.89 1.25 0.58 0.88 1.09 1.56 0.67 1.03 1.28 1.84 0.80 1.20 1.51 2.17 0.93 1.40 1.78 2.57	0.29 0.44 0.54 0.72 0.89 0.34 0.52 0.64 0.87 1.07 0.40 0.62 0.77 1.05 1.34 0.47 0.72 0.89 1.25 1.61 0.58 0.88 1.09 1.56 2.06 0.67 1.03 1.28 1.84 2.48 0.80 1.20 1.51 2.17 2.98 0.93 1.40 1.78 2.57 3.58	0.29 0.44 0.54 0.72 0.89 1.08 0.34 0.52 0.64 0.87 1.07 1.27 0.40 0.62 0.77 1.05 1.34 1.63 0.47 0.72 0.89 1.25 1.61 1.98 0.58 0.88 1.09 1.56 2.06 2.58 0.67 1.03 1.28 1.84 2.48 3.15 0.80 1.20 1.51 2.17 2.98 3.83 0.93 1.40 1.78 2.57 3.58 4.69	0.29 0.44 0.54 0.72 0.89 1.08 1yr 0.34 0.52 0.64 0.87 1.07 1.27 2yr 0.40 0.62 0.77 1.05 1.34 1.63 5yr 0.47 0.72 0.89 1.25 1.61 1.98 10yr 0.58 0.88 1.09 1.56 2.06 2.58 25yr 0.67 1.03 1.28 1.84 2.48 3.15 50yr 0.80 1.20 1.51 2.17 2.98 3.83 100yr 0.93 1.40 1.78 2.57 3.58 4.69 200yr	0.29 0.44 0.54 0.72 0.89 1.08 1yr 0.77 0.34 0.52 0.64 0.87 1.07 1.27 2yr 0.92 0.40 0.62 0.77 1.05 1.34 1.63 5yr 1.16 0.47 0.72 0.89 1.25 1.61 1.98 10yr 1.39 0.58 0.88 1.09 1.56 2.06 2.58 25yr 1.77 0.67 1.03 1.28 1.84 2.48 3.15 50yr 2.14 0.80 1.20 1.51 2.17 2.98 3.83 100yr 2.57 0.93 1.40 1.78 2.57 3.58 4.69 200yr 3.09	0.29 0.44 0.54 0.72 0.89 1.08 lyr 0.77 1.06 0.34 0.52 0.64 0.87 1.07 1.27 2yr 0.92 1.24 0.40 0.62 0.77 1.05 1.34 1.63 5yr 1.16 1.59 0.47 0.72 0.89 1.25 1.61 1.98 10yr 1.39 1.94 0.58 0.88 1.09 1.56 2.06 2.58 25yr 1.77 2.52 0.67 1.03 1.28 1.84 2.48 3.15 50yr 2.14 3.08 0.80 1.20 1.51 2.17 2.98 3.83 100yr 2.57 3.75 0.93 1.40 1.78 2.57 3.58 4.69 200yr 3.09 4.58	0.29 0.44 0.54 0.72 0.89 1.08 1yr 0.77 1.06 1.26 0.34 0.52 0.64 0.87 1.07 1.27 2yr 0.92 1.24 1.48 0.40 0.62 0.77 1.05 1.34 1.63 5yr 1.16 1.59 1.89 0.47 0.72 0.89 1.25 1.61 1.98 10yr 1.39 1.94 2.29 0.58 0.88 1.09 1.56 2.06 2.58 25yr 1.77 2.52 2.96 0.67 1.03 1.28 1.84 2.48 3.15 50yr 2.14 3.08 3.61 0.80 1.20 1.51 2.17 2.98 3.83 100yr 2.57 3.75 4.39 0.93 1.40 1.78 2.57 3.58 4.69 200yr 3.09 4.58 5.36	0.29 0.44 0.54 0.72 0.89 1.08 lyr 0.77 1.06 1.26 1.74 0.34 0.52 0.64 0.87 1.07 1.27 2yr 0.92 1.24 1.48 1.96 0.40 0.62 0.77 1.05 1.34 1.63 5yr 1.16 1.59 1.89 2.54 0.47 0.72 0.89 1.25 1.61 1.98 10yr 1.39 1.94 2.29 3.11 0.58 0.88 1.09 1.56 2.06 2.58 25yr 1.77 2.52 2.96 4.08 0.67 1.03 1.28 1.84 2.48 3.15 50yr 2.14 3.08 3.61 5.01 0.80 1.20 1.51 2.17 2.98 3.83 100yr 2.57 3.75 4.39 6.18 0.93 1.40 1.78 2.57 3.58 4.69 200yr 3.09 4.58 <th< td=""><td>0.29 0.44 0.54 0.72 0.89 1.08 lyr 0.77 1.06 1.26 1.74 2.20 0.34 0.52 0.64 0.87 1.07 1.27 2yr 0.92 1.24 1.48 1.96 2.51 0.40 0.62 0.77 1.05 1.34 1.63 5yr 1.16 1.59 1.89 2.54 3.25 0.47 0.72 0.89 1.25 1.61 1.98 10yr 1.39 1.94 2.29 3.11 3.96 0.58 0.88 1.09 1.56 2.06 2.58 25yr 1.77 2.52 2.96 4.08 5.17 0.67 1.03 1.28 1.84 2.48 3.15 50yr 2.14 3.08 3.61 5.01 6.35 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APPENDIX VII

Rip Rap Calculations

RIP RAP CALCULATIONS

"Luster Cluster" 635 Sagamore Ave. Portsmouth, NH

Jones & Beach Engineers, Inc.

P.O. Box 219 Stratham, NH 03885 3/14/2024 REVISED 4/19/2024 REVISED 8/8/2024 REVISED 9/16/2024

Rip Rap equations were obtained from the *Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire.*Aprons are sized for the 10-Year storm event.

TAILWATER < HALF THE D_o

 $L_a = (1.8 \text{ x Q}) / D_0^{3/2} + (7 \text{ x D}_o)$

 $W = L_a + (3 \times D_o)$ or defined channel width

$$d_{50} = (0.02 \text{ x } Q^{4/3}) / (T_w \text{ x } D_0)$$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	d ₅₀ -Median Stone
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	Rip Rap
(Sta. No.)	T_{w}	Q	D_{o}	L _a (feet)	W (feet)	d50 (feet)
1P Outlet Pipe	0.39	1.67	1	10.0	13	0.10

TAILWATER > HALF THE D_o

 $L_a = (3.0 \text{ x Q}) / D_0^{3/2} + (7 \text{ x D}_o)$

 $W = (0.4 \text{ x L}_a) + (3 \text{ x D}_o)$ or defined channel width

$$d_{50} = (0.02 \text{ x } Q^{4/3}) / (T_w \text{ x } D_0)$$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	d ₅₀ -Median Stone
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	Rip Rap
(Sta. No.)	$T_{ m w}$	Q	D_{o}	L_a (feet)	W (feet)	d50 (feet)
CB104 Outlet Pipe	0.59	1.96	1	12.9	8	0.08

d_{50} Size =	0.25	Feet	3	Inches	
% of Weight Smaller	Size of Stone (Inches)				
Than the Given d ₅₀ Size		From		To	
100%		5		6	
85%		4		5	
50%		3		5	
15%		1		2	

Table 7-24 Recommended Rip Rap Gradation Ranges						
d_{50} Size =	0.5	Feet	6	Inches		
% of Weight Smaller	Size of Stone (Inches)					
Than the Given d ₅₀ Size		From		To		
100%		9		12		
85%		8		11		
50%		6		9		
15%		2		3		

APPENDIX VIII

BMP Worksheets



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name: Bioretention Pond (1P)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

Yes	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.0)7(a).
0.54 ac	A = Area draining to the practice	
0.24 ac	A _I = Impervious area draining to the practice	
0.45 decimal	I = Percent impervious area draining to the practice, in decimal form	
0.46 unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
0.25 ac-in	WQV= 1" x Rv x A	
895 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
224 cf	25% x WQV (check calc for sediment forebay volume)	
671 cf	75% x WQV (check calc for surface sand filter volume)	
Sediment Forebay	_	
272 cf	V _{SED} = Sediment forebay volume, if used for pretreatment	<u>></u> 25%WQV
Calculate time to dra	in if system IS NOT underdrained:	
sf	A _{SA} = Surface area of the practice	
iph	Ksat _{DESIGN} = Design infiltration rate ¹	
	If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?	
Yes/No	(Use the calculations below)	
- hours	$T_{DRAIN} = Drain time = V / (A_{SA} * I_{DESIGN})$	<u><</u> 72-hrs
Calculate time to dra	in if system IS underdrained:	
61.78 ft	E _{WQV} = Elevation of WQV (attach stage-storage table)	
1.69 cfs	Q_{WQV} = Discharge at the E_{WQV} (attach stage-discharge table)	
0.29 hours	$T_{DRAIN} = Drain time = 2WQV/Q_{WQV}$	<u><</u> 72-hrs
0.29 hours 59.10 feet	T_{DRAIN} = Drain time = $2WQV/Q_{WQV}$ E_{FC} = Elevation of the bottom of the filter course material ²	< 72-hrs
		≤ 72-hrs
59.10 feet	E _{FC} = Elevation of the bottom of the filter course material ²	
59.10 feet 58.35 feet	E_{FC} = Elevation of the bottom of the filter course material ² E_{UD} = Invert elevation of the underdrain (UD), if applicable	pit)
59.10 feet 58.35 feet 58.08 feet	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p	pit)
59.10 feet 58.35 feet 58.08 feet 57.67 feet	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test	pit) t pit)
59.10 feet 58.35 feet 58.08 feet 57.67 feet 0.75 feet	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test E_{ROCK} = Depth to UD from the bottom of the filter course	oit) t pit) <u>></u> 1'
59.10 feet 58.35 feet 58.08 feet 57.67 feet 0.75 feet 1.43 feet	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test points E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test E_{ROCK} = Depth to UD from the bottom of the filter course $E_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course	pit) t pit) ≥ 1' ≥ 1'
59.10 feet 58.35 feet 58.08 feet 57.67 feet 0.75 feet 1.43 feet 1.02 feet	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test of the Error Elevation of bedrock (if none found, enter the lowest elevation of the test of the Error Elevation of bedrock (if none found, enter the lowest elevation of the test of the Elevation of the UD from the bottom of the filter course $D_{FC \text{ to } SHWT}$ = Depth to bedrock from the bottom of the filter course $D_{FC \text{ to } SHWT}$ = Depth to SHWT from the bottom of the filter course	pit) t pit) ≥ 1' ≥ 1'
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59.10 feet 58.35 feet 58.08 feet 57.67 feet 0.75 feet 1.43 feet 1.02 feet 61.96 ft 63.00 ft YES If a surface sand filte	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test particles E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test particles E_{ROCK} = Depth to UD from the bottom of the filter course $E_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from t	oit) t pit) ≥ 1' ≥ 1' ≥ 1'
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If a biorete	ntion a	rea i	is proposed:	
YES	ac		Drainage Area no larger than 5 ac?	← yes
905	cf		V = Volume of storage ³ (attach a stage-storage table)	<u>></u> WQV
18.0	inches		D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet	<u> </u>	D4	Note what sheet in the plan set contains the filter course specification	
3.0	1:1		Pond side slopes	<u>> 3</u> :1
Sheet		D4	Note what sheet in the plan set contains the planting plans and surface cover	
If porous p	avemen	ıt is	proposed:	
			Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acres		A _{SA} = Surface area of the pervious pavement	
	:1		Ratio of the contributing area to the pervious surface area	≤ 5:1
	inches		D _{FC} = Filter course thickness	12", or 18" if within GPA
Sheet			Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

- 1. Rate of the limiting layer (either the filter course or the underlying soil). Ksat_{design} includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
- 2. See lines 34, 40 and 48 for required depths of filter media.
- 3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:			

60.64

156

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Stage-Area-Storage for Pond 1P: Bioretention Pond

Elevation	Surface	Storage	Elevation	Surface	Storage	
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)	
58.09	117		60.69	213	89	
		0				
58.14	117	2	60.74	279	101	
58.19	117	5	60.79	354	117	
58.24	117	7	60.84	437	137	
58.29	117	9	60.89	530	161	
58.34	117	12	60.94	631	190	
				741	224	
58.39	117	14	60.99			
58.44	117	16	61.04	778	262	
Bottom of 58.49	117	19	61.09	796	302	
58 5 <u>4</u>	117	21	61.14	814	342	
filter 58.59	117	23	61.19	832	383	
course = 58.64	117	26	61.24	851	425	
59.1 58.69	117	28	61.29	870	468	
F0.74						
Vol. below 58.74	117	30	61.34	889	512	Volume below
= 47 cf 58.79	117	33	61.39	908	557	E(WQV) = Volume
30.04	117	35	61.44	927	603	•
58.89	117	37	61.49	946	650	of stone voids +
58.94	117	40	61.54	966	698	Required WQV =
58.99	117	42	61.59	986	746	•
			61.64			47+895 = 942 cf
59.04	117	44		1,006	796	
59.09	117	47	61.69	1,026	847	E(MOV) 04.70 l
59.14	117	48	61.74	1,047	899	E(WQV) = 61.78 by
59.19	117	49	61.79	1,068	952	interpolation
59.24	117	49	61.84	1,089	1,006	interpolation
59.29	117	50	61.89	1,110	1,061	
59.34	117	51	61.94	1,131	1,117	Overflow el. = 61.8
						Vol. below = 952 cf
59.39	117	52	61.99	1,153	1,174	
59.44	117	53	62.04	1,174	1,232	Storage volume
59.49	117	54	62.09	1,195	1,291	provided = 952-47 =
59.54	117	55	62.14	1,217	1,352	•
59.59	117	56	62.19	1,239	1,413	905 cf > 895 cf
59.64	117	56	62.24	1,261	1,475	
59.69	117	57	62.29	1,283	1,539	
59.74		58	62.34			
	117			1,305	1,604	
59.79	117	59	62.39	1,328	1,669	
59.84	117	60	62.44	1,350	1,736	
59.89	117	61	62.49	1,373	1,805	
59.94	117	62	62.54	1,396	1,874	
59.99	117	63	62.59	1,420	1,944	
60.04	117	63	62.64	1,443	2,016	
60.09	117		62.69	1,467	2,088	
		64				
60.14	117	65	62.74	1,491	2,162	
60.19	117	66	62.79	1,515	2,238	
60.24	117	67	62.84	1,539	2,314	
60.29	117	68	62.89	1,564	2,391	
60.34	117	69	62.94	1,588	2,470	
60.39	117	70	62.99	1,613	2,550	
			02.33	1,013	2,550	
60.44	117	70				
60.49	117	71				
60.54	117	72				
60.59	117	73				
60 64	156	80				

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Stage-Discharge for Pond 1P: Bioretention Pond

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	
58.09	0.00	60.69	1.37	
58.14	0.00	60.74	1.38	
58.19	0.00	60.79	1.40	
58.24	0.00	60.84	1.41	
58.29	0.00	60.89	1.43	
58.34	0.00	60.94	1.45	
58.39	0.01	60.99	1.46	
58.44	0.02	61.04	1.48	
58.49	0.06	61.09	1.49	
58.54	0.10	61.14	1.51	
58.59	0.16	61.19	1.52	
58.64	0.22	61.24	1.54	
58.69	0.28	61.29	1.55	
58.74	0.35	61.34	1.56	
58.79	0.41	61.39	1.58	
58.84	0.47	61.44	1.59	
58.89	0.51 0.55	61.49 61.54	1.61 1.62	
58.94 58.99	0.55	61.59	1.62	
59.04	0.63	61.64	1.65	
59.09	0.66	61.69	1.66	
59.14	0.69	61.74	1.68	E(WQV) = 61.78
59.19	0.73	61.79	1.69	Q(WQV) = 1.69 cfs
59.24	0.76	61.84	1.83	Д(11 Д1)
59.29	0.79	61.89	2.13	
59.34	0.81	61.94	2.54	
59.39	0.84	61.99	3.02	
59.44	0.87	62.04	3.57	
59.49	0.89	62.09	4.17	
59.54	0.92	62.14	4.83	
59.59	0.94	62.19	5.46	
59.64 59.69	0.96	62.24	5.50	
59.69 59.74	0.99 1.01	62.29 62.34	5.54 5.58	
59.79	1.03	62.39	5.62	
59.84	1.05	62.44	5.66	
59.89	1.07	62.49	5.70	
59.94	1.09	62.54	5.74	
59.99	1.11	62.59	5.77	
60.04	1.13	62.64	5.81	
60.09	1.15	62.69	5.85	
60.14	1.17	62.74	5.89	
60.19	1.19	62.79	5.93	
60.24	1.21	62.84	5.96	
60.29	1.23	62.89	6.00	
60.34	1.25	62.94	6.04	
60.39 60.44	1.26	62.99	6.07	
60.44	1.28 1.30			
60.54	1.30			
60.59	1.33			
60.64	1.35			



GROUNDWATER RECHARGE VOLULME (GRV) CALCULATION (Env-Wq 1507.04)

	ac	Area of HSG A soil that was replaced by impervious cover	0.40"
0.12	ac	Area of HSG B soil that was replaced by impervious cover	0.25"
	ac	Area of HSG C soil that was replaced by impervious cover	0.10"
	ac	Area of HSG D soil or impervious cover that was replaced by impervious cover	0.0"
0.25	inches	Rd = Weighted groundwater recharge depth	
0.031	ac-in	GRV = AI * Rd	
113	cf	GRV conversion (ac-in x 43,560 sf/ac x 1ft/12")	

Provide calculations below showing that the project meets the groundwater recharge requirements (Env-Wq 1507.04):

Stone Beneath Unit 3 deck: (14 ft * 20 ft * 2.4 ft)*0.4 = 269 cf
Stone Beneath Unit 4 deck: (14 ft * 20 ft *3.3 ft)*0.4 = 370 cf
269+370 = 639 cf > 113 cf

APPENDIX IX

Pollutant Removal Calculations

POLLUTANT REMOVAL CALCULATIONS

BMP	Drip Edge	Bioretention	None	Total	Required
Acres Impervious	0.053	0.244	0.039	0.335	
TSS Removal (%)	90%	90%	0%	80%	80%
TN Removal (%)	55%	65%	0%	67%	50%

Calculations are based on post-construction impervious surfaces directed toward AP3 and AP4. Post-construction impervious surfaces directed toward AP1 are handled offsite via the City's drainage system, and the amount of impervious surface directed toward AP1 is being decreased post-construction.

Stone underneath decks are assumed to provide similar treatment to a stone drip edge.

TSS removal of 80% provided meets 80% requirement

TN removal of 67% provided exceeds 50% requirement

Pollutant Ro	emoval Efficiencies for Best M for Use in Pollutant Loading		Accepting Ana			
BMP Type	ВМР		Lit. Ref.	TSS	TN	TP
	Wet Pond		B, F	70%	35%	45%
01	Wet Extended Detention Pond		A, B	80%	55%	68%
Stormwater Ponds	Micropool Extended Detention Pond	TBA				
	Multiple Pond System	TBA				
	Pocket Pond	TBA				
	Shallow Wetland		A, B, F, I	80%	55%	45%
Stormwater	Extended Detention Wetland		A, B, F, I	80%	55%	45%
Wetlands	Pond/Wetland System	TBA				
	Gravel Wetland		Н	95%	85%	64%
	Infiltration Trench (≥75 ft from surface water)		B, D, I	90%	55%	60%
	Infiltration Trench (<75 ft from surface water)		B, D, I	90%	10%	60%
Infiltration Practices	Infiltration Basin (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%
	Infiltration Basin (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%
	Dry Wells			90%	55%	60%
	Drip Edges			90%	55%	60%
	Aboveground or Underground Sand Filter that infiltrates WQV (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%
	Aboveground or Underground Sand Filter that infiltrates WQV (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%
	Aboveground or Underground Sand Filter with underdrain		A, I, F, G, H	85%	10%	45%
Filtering	Tree Box Filter	TBA				
Practices	Bioretention System		I, G, H	90%	<mark>65%</mark>	<mark>65%</mark>
	Permeable Pavement that infiltrates WQV (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%
	Permeable Pavement that infiltrates WQV (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%
	Permeable Pavement with underdrain		Use TN and TP values for sand filter w/ underdrain and outlet pipe	90%	10%	45%

Pollutant R	Values Accepted for Loading Analyses					
BMP Type	ВМР	Notes	Lit. Ref.	TSS	TN	TP
Treatment Swales	Flow Through Treatment Swale	TBA				
Vegetated Buffers	Vegetated Buffers		A, B, I	73%	40%	45%
	Sediment Forebay	TBA				
	Vegetated Filter Strip		A, B, I	73%	40%	45%
	Vegetated Swale		A, B, C, F, H, I	65%	20%	25%
Pre-	Flow-Through Device - Hydrodynamic Separator		A, B, G, H	35%	10%	5%
Treatment Practices	Flow-Through Device - ADS Underground Multichamber Water Quality Unit (WQU)		G, H	72%	10%	9%
	Other Flow-Through Devices	TBA				
	Off-line Deep Sump Catch Basin		J, K, L, M	15%	5%	5%

APPENDIX X

Infiltration Testing Data

Front of Site - Test #1

	Height	Constant	Tim	ie	Outflow	Rate (K _{sat})	
	cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
	0						
Ī	6.2	105	0.5	0.008333	78120.0	82.4947	32.4782
	9.9	105	1	0.016667	62370.0	65.8627	25.9302
	13.5	105	1.5	0.025	56700.0	59.8752	23.5729

 Mean
 27.3271

 σ (Std. Dev.)
 3.7674

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 22.3 iph (Test #3)

With factor of safety of two = 11.15 iph

Constant	105 cm^2	
Glover Coefficient:	0.001056 1/cm ²	2

Front of Site - Test #2

	Height	Constant	Tim	ne	Outflow	Rate (K _{sat})	
	cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
	0						
1	6.7	105	0.5	0.008333	84420.0	89.1475	35.0974
	11.2	105	1	0.016667	70560.0	74.5114	29.3352
	16.1	105	1.5	0.025	67620.0	71.4067	28.1129

 Mean
 30.8485

 σ (Std. Dev.)
 3.0456

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Me

Lowest Mean Ksat = 22.3 iph (Test #3) With factor of safety of two = 11.15 iph

Front of Site - Test #3

	Height	Constant	Tim	ne	Outflow	Rate (K _{sat})	
	cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
	0						
Ī	4.8	105	0.5	0.008333	60480.0	63.8669	25.1444
	8.3	105	1	0.016667	52290.0	55.2182	21.7395
	11.4	105	1.5	0.025	47880.0	50.5613	19.9060

 Mean
 22.2633

 σ (Std. Dev.)
 2.1704

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksa

Lowest Mean Ksat = 22.3 iph (Test #3) With factor of safety of two = 11.15 iph

Constant	105 cm^2
Glover Coefficient:	0.001056 1/cm ²

Bioretention - Test #1

Height	Constant	Tim	ie	Outflow	Rate (K _{sat})
cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
0						
2.9	105	0.5	0.008333	36540.0	38.5862	15.1914
5.7	105	1	0.016667	35910.0	37.9210	14.9295
8	105	1.5	0.025	33600.0	35.4816	13.9691
10.65	105	2	0.033333	33547.5	35.4262	13.9473
14.7	105	2.5	0.041667	37044.0	39.1185	15.4010
17.9	105	3	0.05	37590.0	39.6950	15.6280

 Mean
 14.8444

 σ (Std. Dev.)
 0.6611

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest

Lowest Mean Ksat = 14.8 iph (Test #1) With factor of safety of two = 7.4 iph

Constant	105 cm^2
Glover Coefficient:	0.001056 1/cm ²

Bioretention - Test #2

	Height	Constant	Tim	ne	Outflow	Rate (K _{sat})	
	cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
	0						
Ī	6.8	105	0.5	0.008333	85680.0	90.4781	35.6213
	13	105	1	0.016667	81900.0	86.4864	34.0498
	17.5	105	1.5	0.025	73500.0	77.6160	30.5575

 Mean
 33.4095

 σ (Std. Dev.)
 2.1163

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 14.8 iph (Test #1)

With factor of safety of two = 7.4 iph

Constant	105 (cm^2
Glover Coefficient:	0.001056	1/cm ²

Bioretention - Test #3

Height	Constant	Tim	e Outflow		Rate (K _{sat})	
cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
0						
12.6	105	0.5	0.008333	158760.0	167.6506	66.0042
25	105	1	0.016667	157500.0	166.3200	65.4803

 Mean
 65.7422

 σ (Std. Dev.)
 0.2619

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 14.8 iph (Test #1)

With factor of safety of two = 7.4 iph

Unit 4 - Test #1

Height	Constant	Tim	ne	Outflow	Rate ((K _{sat})
cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
0						
6.5	105	0.5	0.008333	81900.0	86.4864	34.0498
11.7	105	1	0.016667	73710.0	77.8378	30.6448
15.6	105	1.5	0.025	65520.0	69.1891	27.2398

 Mean
 30.6448

 σ (Std. Dev.)
 2.7802

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 25.4 iph (Test #2)

With factor of safety of two = 12.7 iph

Unit 4 - Test #2

Height	Constant	Tim	ne	Outflow	Rate (K _{sat})
cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
0						
5.6	105	0.5	0.008333	70560.0	74.5114	29.3352
9.5	105	1	0.016667	59850.0	63.2016	24.8825
12.6	105	1.5	0.025	52920.0	55.8835	22.0014

 Mean
 25.4064

 σ (Std. Dev.)
 3.0168

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 25.4 iph (Test #2)

With factor of safety of two = 12.7 iph

Unit 4 - Test #3

	Height	Constant	Tim	ne	Outflow	Rate (K _{sat})
	cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
	0						
Ī	8.4	105	0.5	0.008333	105840.0	111.7670	44.0028
	13.6	105	1	0.016667	85680.0	90.4781	35.6213
	18.5	105	1.5	0.025	77700.0	82.0512	32.3036

 Mean
 37.3092

 σ (Std. Dev.)
 4.9230

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 25.4 iph (Test #2)

With factor of safety of two = 12.7 iph

Project #: Test Pit #: Permeameter Test #: Date:

Outflow Chamber(s) Used (circle one):

Associated Conversion Factor:

Soil Map Unit Series:

Location:

Horizon: B/C (circle one)

Test hole profile:

Set-Up Calculation

Hole Depth (cm): **Distance From Bottom of Bubble:**

Tube to Soil Surface (cm): **Desired Water Depth In Hole (cm):**

= CHT Tube Setting (cm):

Small ("1 on") $(=20.0cm^2)$

Both ("2 on") (= 105.0 cm^2)

Unit

Α	В				D	E	F
Drop In Water	Outflow Chamber	Clock Time	Elapse	d Time	Outflow (Q)	Saturated Hydraulic	
Level				С	(4)	Conductivity (Ksat)	
(cm)	(C.F.)	(hr : min)	(min)	(min/hr	(cm³/hr)	(cm/hr)	(in/hr)
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)					4		
					M		
					Mean Ksat		

Calculation Formulas:

D = (AxB)/C

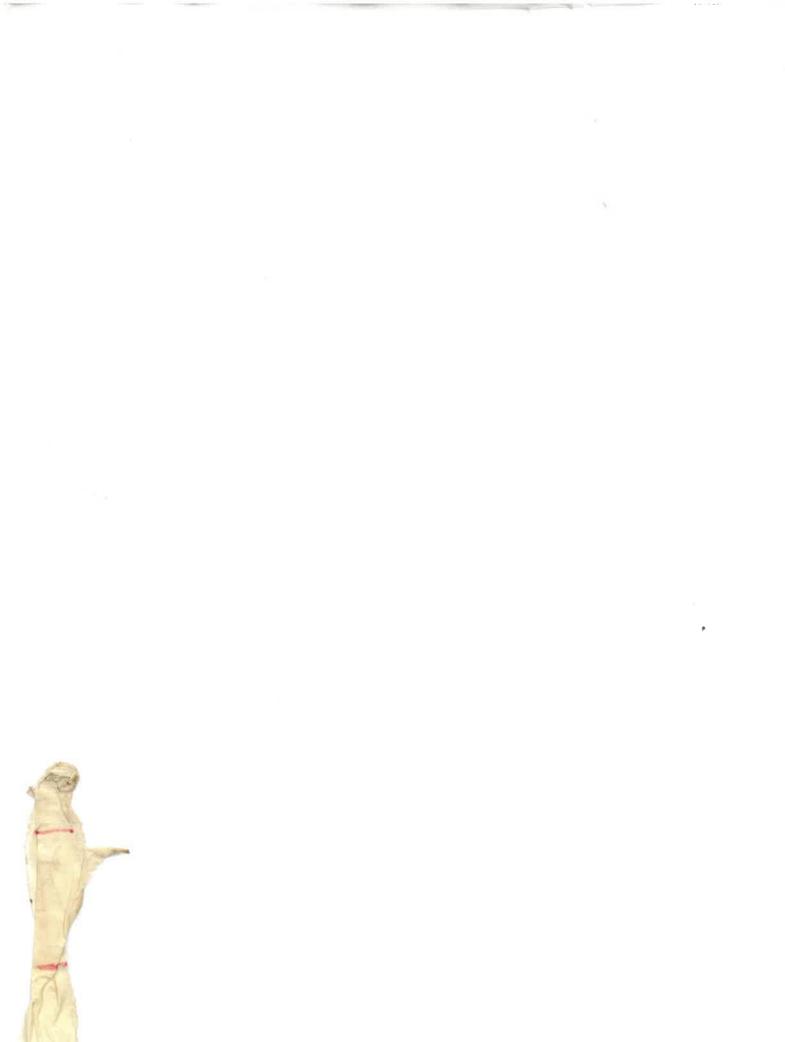
 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr



Project #:

Test Pit #:

Front

Permeameter Test #:

Date: Location: 7/2/24

Soil Map Unit Series:

Horizon:

B/C

(circle one)

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Test hole profile:

Unit

8"

6

Set-Up Calculation
Hole De

Hole Depth (cm):

Distance From Bottom of Bubble:

Tube to Soil Surface (cm):

Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on")

 $(= 20.0 cm^2)$

Both ("2 on") (= 105.0 cm^2)

<-- "B

Α	В				D	E	F
Drop in Water Level	Outflow Chamber	Clock Time	Elapsed Time C		Outflow (Q)	Saturated Hydraulic Conductiv	ity (Ksat)
(cm)	(C.F.)	(hr : min)	(min)	(min/hr)	(cm³/hr)	(cm/hr)	(in/hr)
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)							
	1100				Mean Ksat		

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr

F:\Forms, Apps, Regs\Templates\Amoozemeter\Amoozemeter Data Sheet.xlsx

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Project #: 181341

Test Pit #: 4 F(0x)

Permeameter Test #: 3

Date: 7/2/24

Location: 635 569

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Soil Map Unit Series:
Horizon: B / C (circle one)

Set-Up Calculation

Hole Depth (cm):

Distance From Bottom of Bubble:

Tube to Soil Surface (cm):

Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

Test hole profile:

Unit

9

"

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on") (= 20.0cm²) Both ("2 on") (= 105.0 cm^2)

<-- "B"

Α	В				D	E	F
Drop In Water	Outflow Chamber	Clock Time	Liapseu Time		Outflow (Q)	Saturated Hydraulic	
Level				С	(4)	Conductivity (Ksat)	
(cm)	(C.F.)	(hr : min)	(min)	(min/hr	(cm³/hr)	(cm/hr)	(in/hr)
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)							
					Mean Ksat		

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr





Project #:	18134.)	
Test Pit #:	BiO/eletia	
Permeamete	r Test #:	
Date:	7/2/24	
Location:	635 500	
Soil Map Uni	t Series:	

B/C

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Set-Up Calculation

(circle one)

Hole Depth (cm):

Distance From Bottom of Bubble:

Tube to Soil Surface (cm):

Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

Test hole profile:

Unit

9
"

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on") (= 20.0cm²) Both ("2 on") (= 105.0 cm^2)

<-- "B

Α	В				D	E	F	
Drop In Water	Outflow Chamber	Clock Time	Liapsed Time		Outflow (Q)	Saturated Hydraulic		
Level				С	(4)	Conductiv	ity (Ksat)	
(cm)	(C.F.)	(hr : min)	(min)	(min/hr	(cm ³ /hr)	(cm/hr)	(in/hr)	
Example:	20	10:17	15	0.25	392	0.4139	0.1629	
Start (0)								
							·	
					Mean Ksat		-	

Calculation Formulas:

D = (AxB)/C

Horizon:

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr



Project #: Test Pit #:	18134 1 Bio 1886	192					
Permeamete	Permeameter Test #:						
Date:	7/2/1	1					
Location:	635 54	.9					
Soil Map Unit Series:							
Horizon:	B/C	(circle one)					

Outflow Chamber(s) Used (circle one):

Associated Conversion Factor:

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Test hole profile:

Set-Up Calculation

Hole Depth (cm):

Distance From Bottom of Bubble: Tube to Soil Surface (cm): Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

setting (cm):

Small ("1 on") (= 20.0cm²) Both ("2 on") (= 105.0 cm^2)

<-- "B

Unit

Α	В				D	Е	F
Drop In Water Level	Outflow Chamber	Clock Time	Elapse	d Time	Outflow (Q)	Saturated Hydraulic Conductiv	ity (Ksat)
(cm)	(C.F.)	(hr : min)	(min)	(min/hr)	(cm³/hr)	(cm/hr)	(in/hr)
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)							
					Mean Ksat		

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr



Project #: Test Pit #: Permeameter Test #: Date: Location:

Soil Map Unit Series:

Horizon: B/C (circle one)

Set-Up Calculation Hole Depth (cm): **Distance From Bottom of Bubble:** Tube to Soil Surface (cm): Desired Water Depth In Hole (cm): **CHT Tube Setting (cm):**

Test hole profile: Unit

Outflow Chamber(s) Used (circle one): Associated Conversion Factor:

Small ("1 on") $(=20.0cm^2)$

Both ("2 on") $(= 105.0 \text{ cm}^2)$

Α	В				D	E	F	
Drop In Water	Outflow Chamber	Clock Time	Elapsed Time		Outflow	Saturated Hydraulic	1	
Level				С	(Q)	Conductivity (ity (Ksat)	
(cm)	(C.F.)	(hr : min)	(min)	(min/hr	(cm³/hr)	(cm/hr)	(in/hr)	
Example:	20	10:17	15	0.25	392	0.4139	0.1629	
Start (0)					332	0.4155	0.1029	
.5								
ART								
25				-				
				٨	lean Ksat			

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from ${\rm cm}^3/{\rm hr}$ to ${\rm cm/hr}$

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr

 $F: \label{lem:first} F: \lab$

Project #:	18134	1
Test Pit #:	Unit	4
Permeamet	er Test #:	
Date:	7/2/20	21
Location:	635 Sa	9
Soil Map Ur	nit Series:	
Horizon:	B/C	(circle one)

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Set-Up Calculation

Hole Depth (cm):
Distance From Bottom of Bubble:
Tube to Soil Surface (cm):
Desired Water Depth In Hole (cm):
= CHT Tube Setting (cm):

Test hole	profile:
	Unit
	6 "

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on") (= 20.0cm²) Both ("2 on") (= 105.0 cm^2)

<-- "B'

Α	В				D	E	F
Drop In Water	Outflow Chamber	Clock Time	Elapsed Time		Outflow (Q)	Saturated Hydraulic	
Level				С	(4)	Conductivi	ity (Ksat)
(cm)	(C.F.)	(hr : min)	(min)	(min/hr	(cm³/hr)	(cm/hr)	(in/hr)
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)							
					Mean Ksat		

Calculation Formulas:

D = (AxB)/C

E = D x 0.001056

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr



Project #: Test Pit #: Permeamete Date: Location: Soil Map Un	7/2/2014 635 Say	JONES& ENGINEER	SEAC RS IN
-		Tost	hala profila
Horizon:	B/C (circle one)	rest	hole profile:
			Unit
	Set-Up Calculation		i n
	Hole Depth	(cm):	110
	Distance From Bottom of Bu	ıbble:	**
	Tube to Soil Surface	(cm):	

Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

Outflow Chamber(s) Used (circle one): Small ("1 on") Both ("2 on") $(= 20.0 \text{cm}^2)$ (= 105.0 cm²) Associated Conversion Factor:

Unit

Α	В				D	E	F
Drop In Water Level	Outflow Chamber			Elapsed Time		Saturated Hydraulic Conductivity (Ksat)	
(cm)	(C.F.)		(cm³/hr)	(cm/hr)	(in/hr)		
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)							
	A STATE OF THE PARTY OF THE PAR				Mean Ksat		

Calculation Formulas:

D = (AxB)/C

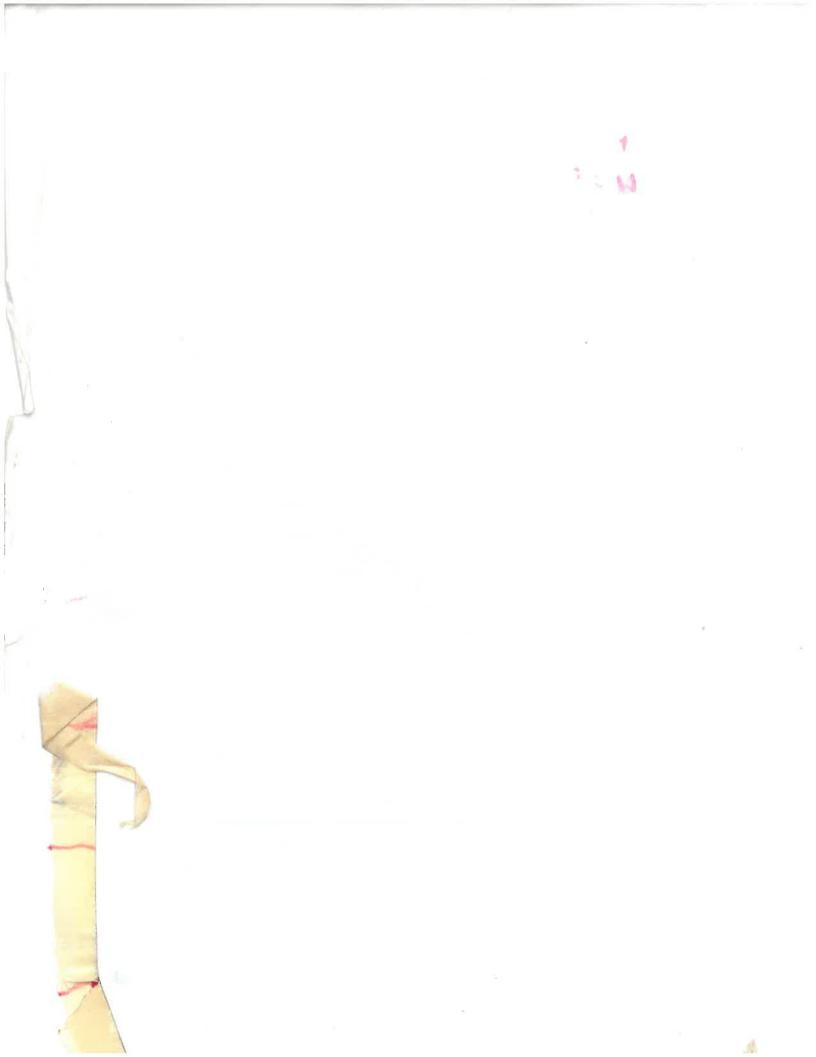
 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr



AMOOZEMETER DATA SHEET

Project #:	18134.1
Test Pit #:	1/1/1 4
Permeamete	er Test #: 3
Date:	7/2/29
Location:	635 509

JONES & BEACH ENGINEERS INC.

Soil Map Unit Series:

Horizon: B / C (circle one)

Test hole profile:
Unit

Set-Up Calculation

Hole Depth (cm):
Distance From Bottom of Bubble:
Tube to Soil Surface (cm):
Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

Both ("2 on") (= 105.0 cm^2)

<-- "B"

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on") (= 20.0cm²)

Mean Ksat

Α	В				D	E	F
Drop In Water Level	Outflow Chamber	Clock Time	Elapse	d Time	Outflow (Q)	Saturated Hydraulic Conductivity (Ksat)	
(cm)	(C.F.)	(hr : min)	(min)	C (min/hr)	(cm³/hr)	(cm/hr) (in/h	
Example:	20	10:17	15	-	392	0.4139	0.1629
Start (0)							

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr



APPENDIX XI

Stormwater Operations and Maintenance Manual



85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

STORMWATER MANAGEMENT OPERATIONS AND MAINTENANCE MANUAL

Luster Cluster 635 Sagamore Ave. Portsmouth, NH 03801 Tax Map 222, Lot 19

Prepared for:

635 Sagamore Development LLC 3612 Lafayette Rd., Dept 4 Portsmouth, NH 03801

Prepared by:

Jones & Beach Engineers, Inc.
85 Portsmouth Avenue
P.O. Box 219
Stratham, NH 03885
(603) 772-4746
March 18, 2024
Revised April 15, 2024
Revised August 8, 2024
Revised October 22, 2024
JBE Project No. 18134.1

Inspection and Maintenance of Facilities and Property

A. Maintenance of Common Facilities or Property

1. The Condominium Association, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Association, future owners and assigns shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form and shall submit an Operations and Maintenance report on a yearly basis to the Portsmouth Planning Department.

B. General Inspection and Maintenance Requirements

- 1. Permanent stormwater and sediment and erosion control facilities to be maintained on the site include, but are not limited to, the following:
 - a. Roadway and driveways
 - b. Vegetation and landscaping
 - c. Sediment Forebay
 - d. Bioretention system
 - e. Catch Basins & Yard Drains
 - f. Stone Drip Edges
 - g. Stone Underneath Decks
 - h. Culverts
 - i. Rip-Rap Outlet Protection Aprons
 - j. Sand Absorption Areas
- 2. Maintenance of permanent measures shall follow the following schedule:
 - a. Normal winter roadway maintenance including plowing and snow removal. Road sweeping at the end of every winter, preferably before the start of the spring rain season.
 - b. **Annual inspection** of the site for erosion, destabilization, settling, and sloughing. Any needed repairs are to be conducted immediately. **Annual inspection** of site's vegetation and landscaping. Any areas that are bare shall be reseeded and mulched with hay or, if the case is extreme, loamed and seeded or sodded to ensure adequate vegetative cover. Landscape specimens shall be replaced in kind, if they are found to be dead or dying.
 - c. Cleaning Criteria for all Sedimentation Forebays: Sediment shall be removed from the sedimentation chamber (forebay) when it accumulates to a depth of more than 12 inches (30 cm) or 10 percent of the pretreatment volume. The sedimentation forebay shall be cleaned of vegetation if persistent standing water and wetland vegetation becomes dominant. The cleaning interval is once every year. A dry sedimentation forebay is the optimal condition while in practice this condition is rarely achieved. The sedimentation chamber, forebay, and treatment cell outlet devices shall be cleaned when drawdown



times exceed 60 to 72 hours. Materials can be removed with heavy construction equipment; however, this equipment shall not track on the wetland surface. Revegetate disturbed areas as necessary. Removed sediments shall be dewatered (if necessary) and disposed of in an acceptable manner.

d. Bioretention Systems:

- Visually inspect monthly and repair erosion. Use small stones to stabilize erosion along drainage paths.
- Check the pH once a year if grass is not surviving. Apply an alkaline product, such as limestone, if needed.
- Re-seed any bare areas by hand as needed.
- Immediately after the completion of cell construction, water grass for 14 consecutive days unless there is sufficient natural rainfall.
- Once a month (more frequently in the summer), the land owner or Association shall visually inspect vegetation for disease or pest problems and treat as required.
- During times of extended drought, look for physical features of stress. Water in the early morning as needed.
- Weed regularly, if needed.
- After rainstorms, inspect the cell and make sure that drainage paths are clear and that ponding water dissipates over 4-6 hours. (Water may pond for longer times during the winter and early spring.)
- Twice annually, inspect the outlet control structures to ensure that they are not clogged and correct any clogging found as needed.
- Any debris and sediment accumulations shall be removed from the outlet structures, overflow risers, and emergency spillways and disposed of properly.
- Inspect outlet structure for deterioration and or clogging.
- If erosion is evident on the berm or emergency spillway, stabilize the affected area by seeding. Trees must not be allowed to grow in these areas.
- KEEP IN MIND, THE BIORETENTION CELL IS NOT A POND. IT SHALL NOT PROVIDE A BREEDING GROUND FOR MOSQUITOES. MOSQUITOES NEED AT LEAST FOUR (4) DAYS OF STANDING WATER TO DEVELOP AS LARVA.
- e. Annual inspection of catch basins and yard drains to determine if they need to be cleaned. Catch basins and yard drains are to be cleaned if the depth of deposits is greater than one-half the depth from the basin bottom to the invert of the lowest pipe or opening into or out of the basin. If a catch basin or yard drain significantly exceeds the one-half depth standard during the inspection, then it shall be cleaned more frequently. If woody debris or trash accumulates in the catch basin or yard drain, then it shall be cleaned on a weekly basis. The catch basin or yard drain can be cleaned either manually or by specially designed equipment including, but not limited to, bucket loaders and vacuum pumps. Before any materials can be disposed, it is necessary to perform a detailed chemical analysis to determine if the materials meet the EPA criteria for hazardous waste. This will help determine how the materials shall be stored, treated, and disposed. Grease hoods are to be



wiped clean and the rags disposed of properly. Debris obscuring the grate inlet shall also be removed.

f. Stone drip edges:

Units 3 & 4 feature stone drip edges to collect roof runoff into a pipe in order to direct it into the stone areas underneath the unit decks. These practices shall be lined and are not intended for infiltration. The following course of action will help assure that the roof drip edges are maintained to preserve its effectiveness.

In the spring and fall, visually inspect the area around the edges and repair any erosion. Use small stones to stabilize erosion along drainage paths. Inspect stone area to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation shall not be allowed to become established in stone areas, and/or any debris removed from the void spaces between the stones

g. Stone underneath decks:

Units 3 and 4 feature stone areas underneath their associated rear decks for infiltration of roof runoff. The following guidelines will help ensure proper functioning of the system.

In the spring and fall, visually inspect the area around the edges and repair any erosion. Use small stones to stabilize erosion along drainage paths. Inspect stone area to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation shall not be allowed to become established in stone areas, and/or any debris removed from the void spaces between the stones.

- h. **Inspection** of culvert inlets and outlets at least **once per month** during the rainy season (March to November). Any debris is to be removed and disposed of properly.
 - i. Rock riprap shall be **inspected annually** in order to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation must not be allowed to become established in riprap areas, and/or any debris removed from the void spaces between the rocks. If the riprap is adjacent to a stream or other waterbody, the water shall be kept clear of obstructions, debris, and sediment deposits



j. There are two sand absorption areas intended to infiltrate foundation drain effluent to the extent practicable. One is located approximately 34'-45' past the end of the shared driveway near the southeast property line of the site in order to handle foundation drain effluent for Units 1 and 2. The other is located between the backyards of Units 3 and 4 in order to handle foundation drain effluent for Units 3 and 4. The foundation drain outfalls shall be **inspected monthly** and more frequently during autumn in order to ensure that there is no debris or leaf buildup. Any debris or leaves that is either clogging or appears that it may clog the outlets must be removed **immediately** and disposed of properly.

During these inspections, additionally check for sediment buildup and standing water in the small ponding areas for these devices. If more than 1" of standing water is persistently present in these systems, contact a professional engineer to evaluate the issue. Remedies may range from cleaning the overflow spillway to replacing the sand media.

See attached sample forms as a guideline.

Any inquiries in regards to the design, function, and/or maintenance of any one of the above-mentioned facilities or tasks shall be directed to the project engineer:

Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885

T#: (603) 772-4746 F#: (603) 772-0227



Commitment to maintenance requirements

I agree to complete and/or observe all of the required schedules as outlined above.	maintenance practices and their respective
Signature	-
Print Name	_
	_
Title	
Date	_

Annual Operations and Maintenance Report

The Condominium Association, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Association, future owners and assigns shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form and shall submit an Operations and Maintenance report on a yearly basis to the Portsmouth Planning Department.

Construction Activity	Date of Inspection	Who Inspected	Findings of Inspector
Roadway and Driveways			
Vegetation and Landscaping			
Sediment Forebay			
Bioretention Pond			
Catch Basins & Yard Drains			



Unit 3 Stone Drip Edge		
Unit 4 Stone Drip Edge		
Stone underneath unit 3		
deck		
Stone underneath unit 4		
deck		
Culverts		
Rip Rap Outlet Protection		
Units 1&2 Foundation		
drain outfall sand absorption area		
-		



Units 3&4 Foundation drain outfall sand absorption area			
Swale			
Other (please note):			

Regular Inspection and Maintenance Guidance for Bioretention Systems / Tree Filters

Maintenance of bioretention systems and tree filters can typically be performed as part of standard landscaping. Regular inspection and maintenance is critical to the effective operation of bioretention systems and tree filters to insure they remain clear of leaves and debris and free draining. This page provides guidance on maintenance activities that are typically required for these systems, along with the suggested frequency for each activity. Individual systems may have more, or less, frequent maintenance needs, depending on a variety of factors including the occurrence of large storm events, overly wet or dry (I.E., drought), regional hydrologic conditions, and the upstream land use.

ACTIVITIES

The most common maintenance activity is the removal of leaves from the system and bypass structure. Visual inspections are routine for system maintenance. This includes looking for standing water, accumulated leaves, holes in the soil media, signs of plant distress, and debris and sediment accumulation in the system. Mulch and/or vegetation coverage is integral to the performance of the system, including infiltration rate and nutrient uptake. Vegetation care is important to system productivity and health.

ACTIVITY	FREQUENCY	
A record should be kept of the time to drain for the system completely after a storm event. The system should drain completely within 72 hours.		
Check to insure the filter surface remains well draining after storm event. Remedy: If filter bed is clogged, draining poorly, or standing water covers more than 15% of the surface 48 hours after a precipitation event, then remove top few inches of discolored material. Till or rake remaining material as needed.	After every major storm in the first few months, then biannually.	
Check inlets and outlets for leaves and debris. Remedy: Rake in and around the system to clear it of debris. Also, clear the inlet and overflow if obstructed.		
Check for animal burrows and short circuiting in the system Remedy: Soil erosion from short circuiting or animal boroughs should be repaired when they occur. The holes should be filled and lightly compacted.	Quarterly initially, biannually,	
Check to insure the filter bed does not contain more than 2 inches accumulated material Remedy: Remove sediment as necessary. If 2 inches or more of filter bed has been removed, replace media with either mulch or a (50% sand, 20% woodchips, 20% compost, 10% soil) mixture.	frequency adjusted as needed after 3 inspections	
During extended periods without rainfall, inspect plants for signs of distress. Remedy: Plants should be watered until established (typical only for first few months) or as needed thereafter.		
Inspect inlets and outlets to ensure good condition and no evidence of deterioration. Check to see if high-flow bypass is functioning. Remedy: Repair or replace any damaged structural parts, inlets, outlets, sidewalls.	Annually	
Check for robust vegetation coverage throughout the system. Remedy : If at least 50% vegetation coverage is not established after 2 years, reinforcement planting should be performed.		
Check for dead or dying plants, and general long term plant health. Remedy : This vegetation should be cut and removed from the system. If woody vegetation is present, care should be taken to remove dead or decaying plant Material. Separation of Herbaceous vegetation rootstock should occur when overcrowding is observed.	As needed	

1/15/2011, University of New Hampshire Stormwater Center

CHECKLIST FOR INSPECTION OF BIORETENTION SYSTEM / TREE FILTERS Location: Inspector: Date: Time: Site Conditions: Date Since Last Rain Event: Inspection Items Satisfactory (S) or Unsatisfactory (U) Comments/Corrective Action

Inspection Items	Satisfact Unsatisfa	ory (S) or actory (U)	Comments/Corrective Action
1. Initial Inspection After Planting and Mulching			
Plants are stable, roots not exposed	S	U]
Surface is at design level, typically 4" below overpass	S	U	
Overflow bypass / inlet (if available) is functional	s	U	<u></u>
2. Debris Cleanup (2 times a year minimum, Spring & Fall)			
Litter, leaves, and dead vegetation removed from the system	S	U	7
Prune perennial vegetation	S	U	T
3. Standing Water (1 time a year, After large storm events)			
No evidence of standing water after 72 hours	S	U	
4. Short Circuiting & Erosion (1 time a year, After large storn	n events)		
No evidence of animal burrows or other holes	S	U	
No evidence of erosion	s	U	
5. Drought Conditions (As needed)			
Water plants as needed	S	U]
Dead or dying plants			
6. Overflow Bypass / Inlet Inspection (1 time a year, After lar	ge storm eve	ents)	
No evidence of blockage or accumulated leaves	S	U	
Good condition, no need for repair	S	U	
7. Vegetation Coverage (once a year)			
50% coverage established throughout system by first year	s	U	
Robust coverage by year 2 or later	s	U	
8. Mulch Depth (if applicable)(once every 2 years)			
Mulch at original design depth after tilling or replacement	s	U	
9. Vegetation Health (once every 3 years)			
Dead or decaying plants removed from the system	s	U	
10. Tree Pruning (once every 3 years)			
Prune dead, diseased, or crossing branches	S	U	
Corrective Action Needed			Due Date
1.			
2.			
3.			

1/15/2011, University of New Hampshire Stormwater Center

APPENDIX XII

Pre- and Post-Construction Watershed Plans



Checked: PSL Scale: AS NOTED Project No.: 18134.1

Drawing Name: 18134-WATERSHED.dwg

THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN
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ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE
AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



	4	10/17/24	REVISED PER ALTUS AND TAC COMMENTS	DJM			
	3	9/16/24	REVISED PER ALTUS AND TAC COMMENTS	DJM			
	2	8/16/24	REVISED PER CITY REVIEW ENGINEER COMMENTS				
	1	4/19/24	REVISED PER TAC COMMENTS	DJM			
	0	3/8/24	ISSUED FOR REVIEW	DJM			
	REV.	DATE	REVISION	BY			

Bones & Beach Engineers, Inc.

85 Rortsmouth Ave. Civil Engineering Somvious 603-772-4746

85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885

E-MAIL: JBE@JONESANDBEACH.COM

Plan Name:	EXISTING WATERSHED PLAN
Project:	"LUSTER CLUSTER" 635 SAGAMORE AVE., PORTSMOUTH, NH
Owner of Record:	635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

DRAWING No.

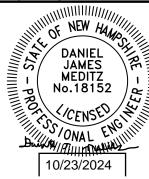
W1

SHEET 1 OF 2

JBE PROJECT NO. 18134.1



Design: DJM Draft: DJM Date: 2/26/2024
Checked: PSL Scale: AS NOTED Project No.: 18134.1
Drawing Name: 18134-WATERSHED.dwg
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DJM REVISED PER ALTUS AND TAC COMMENTS 9/16/24 REVISED PER CITY REVIEW ENGINEER COMMENTS DJM 8/16/24 DJM 4/19/24 REVISED PER TAC COMMENTS DJM 3/8/24 ISSUED FOR REVIEW REVISION BY REV. DATE

Bones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services

PO Box 219
Stratham, NH 03885

Civil Engineering Services

E-MAIL: JBE@JONESANDBEACH.COM

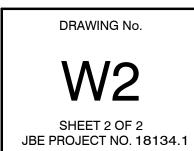
Plan Name: PROPOSED WATERSHED PLAN

"LUSTER CLUSTER"

635 SAGAMORE AVE., PORTSMOUTH, NH

635 SAGAMORE DEVELOPMENT LLC

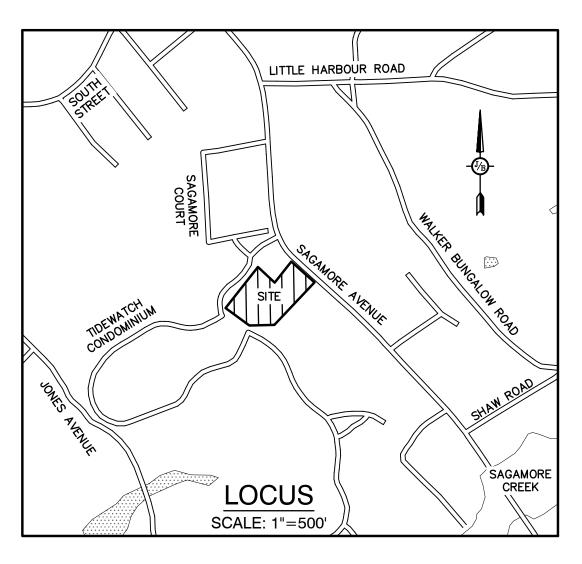
Owner of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158



GENERAL LEGEND **EASEMENT** MAJOR CONTOUR MINOR CONTOUR VERTICAL GRANITE CURB UNDERDRAIN THRUST BLOCK IRON PIPE/IRON ROD DRILL HOLE IRON ROD/DRILL HOLE STONE/GRANITE BOUND 100x0 SPOT GRADE x 100.00 PAVEMENT SPOT GRADE CURB SPOT GRADE BENCHMARK (TBM) DOUBLE POST SIGN SINGLE POST SIGN TEST PIT TREES AND BUSHES UTILITY POLE DRAIN MANHOLE SEWER MANHOLE HYDRANT WATER GATE VALVE WATER SHUT OFF REDUCER SINGLE GRATE CATCH BASIN TRANSFORMER CULVERT W/FLARED END SECTION CULVERT W/STRAIGHT HEADWALL STONE CHECK DAM DRAINAGE FLOW DIRECTION PAVEMENT HATCH STABILIZED CONSTRUCTION **ENTRANCE** CONCRETE **GRAVEL** SNOW STORAGE RETAINING WALL

SINGLE FAMILY CONDOMINIUM "LUSTER CLUSTER" TAX MAP 222, LOT 19 635 SAGAMORE AVE., PORTSMOUTH, NH





CIVIL ENGINEER / SURVEYOR

JONES & BEACH ENGINEERS, INC. 85 PORTSMOUTH AVENUE PO BOX 219 STRATHAM, NH 03885 (603) 772-4746 CONTACT: JOSEPH CORONATI EMAIL: JCORONATI@JONESANDBEACH.COM

TRAFFIC ENGINEER

STEPHEN G. PERNAW & COMPANY, INC. P.O. BOX 1721 CONCORD, NH 03302 (603) 731-8500 CONTACT: STEPHEN PERNAW

SOILS CONSULTANT

GOVE ENVIRONMENTAL SERVICES, INC. 8 CONTINENTAL DRIVE, BLDG 2, UNIT H EXETER, NH 03833-7507 (603) 418-7260 CONTACT: JAMES GOVE EMAIL: JGOVE@GESINC.BIZ

LANDSCAPE DESIGNER

LM LAND DESIGN, LLC 11 SOUTH ROAD BRENTWOOD, NH 03833 (603) 770-7728 **CONTACT: LISE MCNAUGHTON**

WATER

CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS WATER DIVISION 680 PEVERLY HILL ROAD PORTSMOUTH, NH 03801 (603) 427-1530

SEWER

Stratham, NH 03885

CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS **SEWER DIVISION** 680 PEVERLY HILL ROAD PORTSMOUTH, NH 03801 (603) 766-1421

LIGHTING DESIGN

EXPOSURE LIGHTING 501 ISLINGTON STREET, UNIT 1A PORTSMOUTH, NH 03801 **CONTACT: KEN SWEENEY**

EVERSOURCE 1700 LAFAYETTE ROAD PORTSMOUTH, NH 03801 (800) 662-7764

TELEPHONE

CONSOLIDATED COMMUNICATIONS 1575 GREENLAND ROAD GREENLAND, NH 03840 (800) 427-5525

CABLE TV

E-MAIL: JBE@JONESANDBEACH.COM

COMCAST COMMUNICATION CORPORATION 334-B CALEF HIGHWAY EPPING, NH 03042-2325 (603) 679-5695

SHEET INDEX

COVER SHEET

EXISTING CONDITIONS PLAN

DEMOLITION PLAN

SITE PLAN

CONDOMINIUM SITE PLAN

GRADING AND DRAINAGE PLAN

UTILITY PLAN

LIGHTING PLAN

LANDSCAPE PLAN

DRIVEWAY PLAN AND PROFILE

SEWER PLAN AND PROFILE

HIGHWAY ACCESS PLAN

TRUCK TURNING PLAN

DETAIL SHEET D1-D5

TC-600 RADAR SPEED SIGN SPECIFICATIONS

E1 **EROSION AND SEDIMENT CONTROL DETAILS**

ARCHITECTURAL PLANS

PROJECT PARCEL CITY OF PORTSMOUTH TAX MAP 222, LOT 19

TOTAL LOT AREA 84,795 SQ. FT.

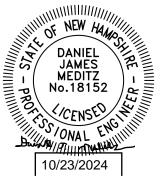
1.95 ACRES

CITY OF PORTSMOUTH PLANNING BOARD

CHAIRPERSON

DATE

Design: DJM Draft: KDR Date: 2/26/2024 Checked: JAC | Scale: AS NOTED | Project No.: 18134.1 Drawing Name: 18134.1-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



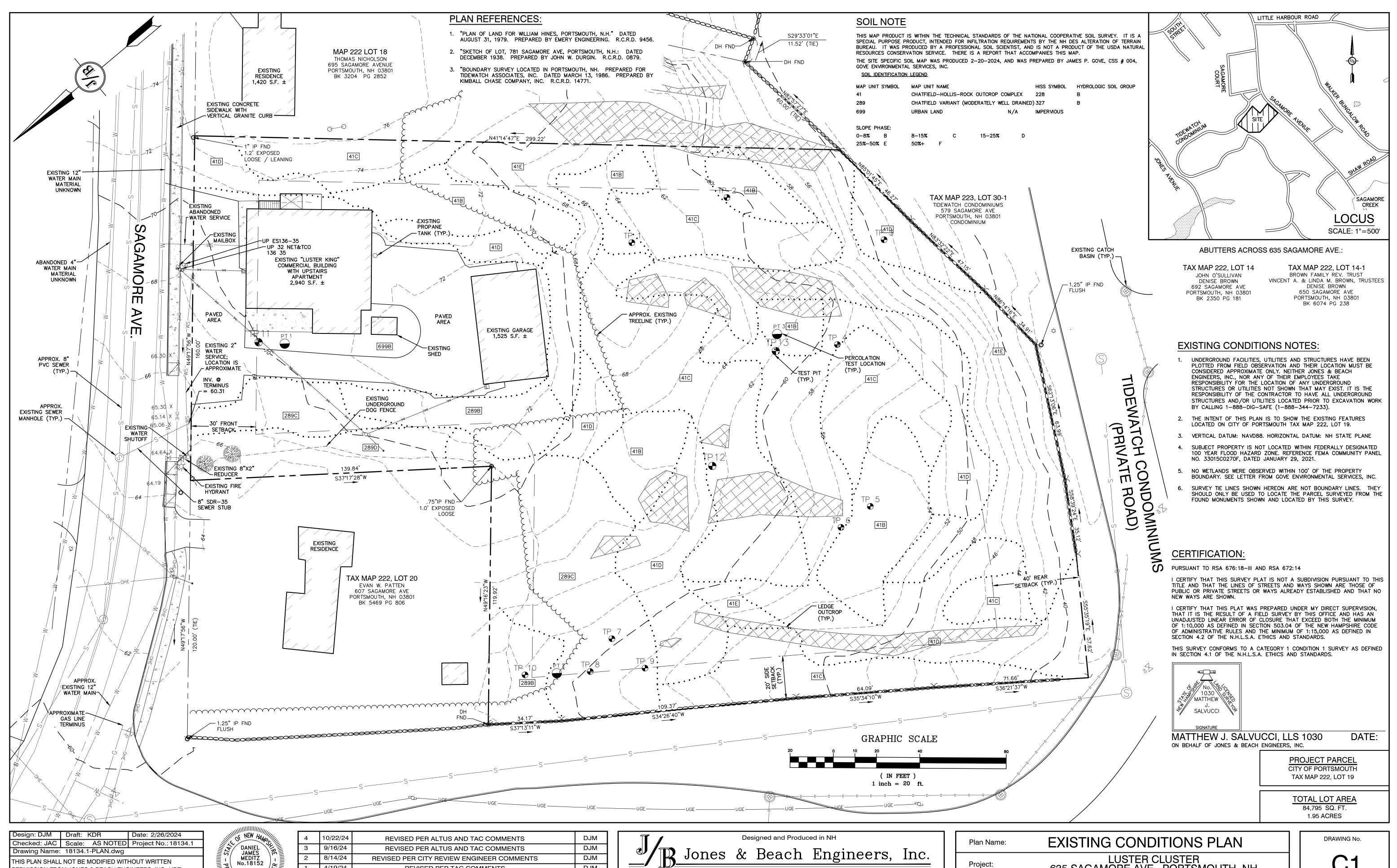
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3	9/16/24	REVISED PER ALTUS AND TAC COMMENTS				
2	8/14/24	REVISED PER CITY REVIEW ENGINEER COMMENTS	DJM			
1	4/19/24	REVISED PER TAC COMMENTS	DJM			
0	3/18/24	ISSUED FOR REVIEW	KDR			
REV.	DATE	REVISION	BY			

Designed and Produced in NH Jones & Beach Engineers, Inc. 603-772-4746 85 Portsmouth Ave. Civil Engineering Services PO Box 219

COVER SHEET Plan Name: LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH Project: 635 SAGAMORE DEVELOPMENT LLC

Owner of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

DRAWING No. JBE PROJECT NO. 18134.1



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4/19/24 **REVISED PER TAC COMMENTS** DJM KDR 3/18/24 **ISSUED FOR REVIEW REVISION** DATE BY REV.

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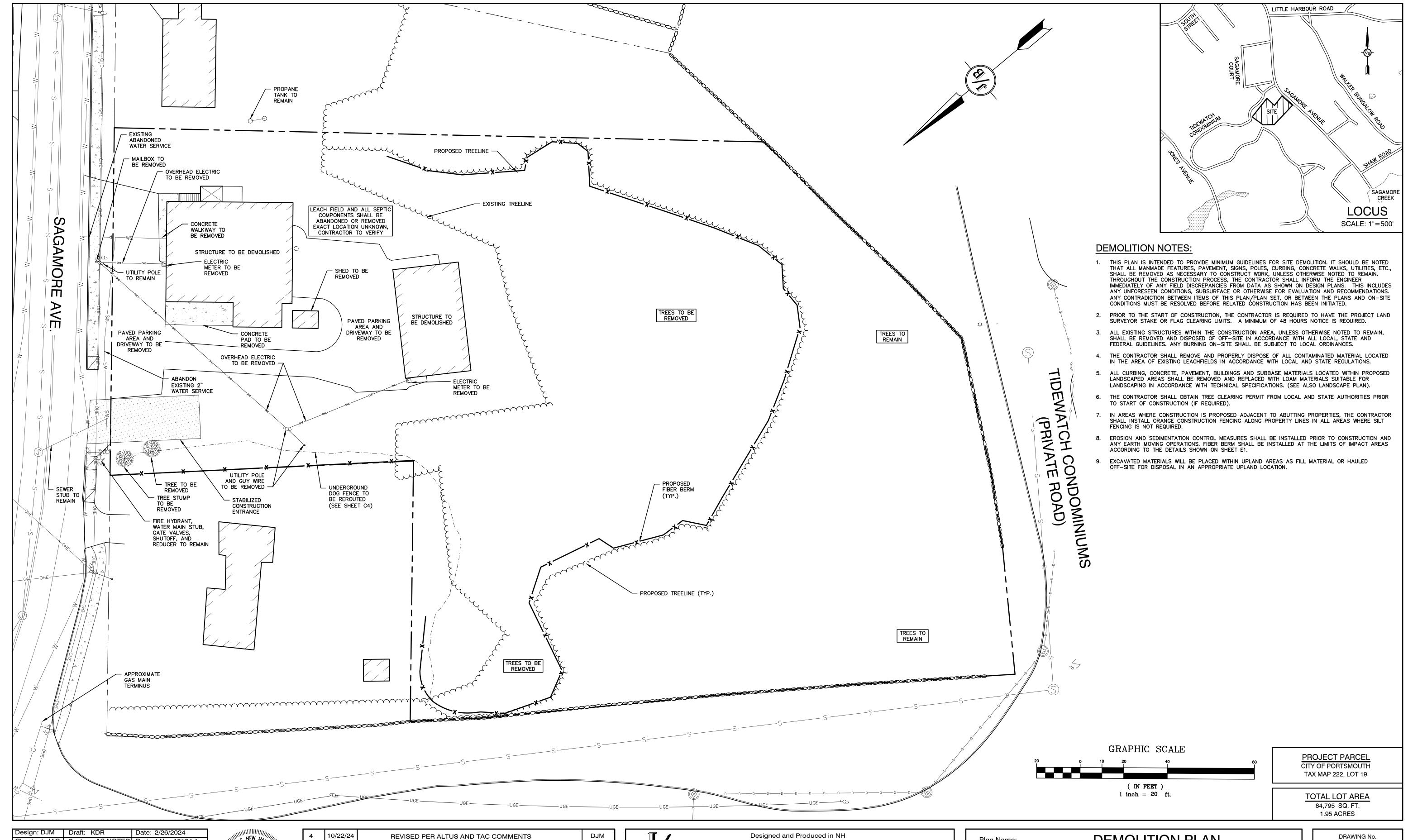
FAX: 603-772-0227

E-MAIL: JBE@JONESANDBEACH.COM

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH 635 SAGAMORE DEVELOPMENT LLC

Owner of Record:3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

SHEET 2 OF 21 JBE PROJECT NO. 18134.1



Design: DJM Draft: KDR Date: 2/26/2024

Checked: JAC Scale: AS NOTED Project No.: 18134.1

Drawing Name: 18134.1-PLAN.dwg

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DANIEL JAMES MEDITZ No.18152

CENSE ONAL ENGINEER TO 10/23/2024

4 10/22/24 REVISED PER ALTUS AND TAC COMMENTS DJM
3 9/16/24 REVISED PER ALTUS AND TAC COMMENTS DJM
2 8/14/24 REVISED PER CITY REVIEW ENGINEER COMMENTS DJM
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0 3/18/24 ISSUED FOR REVIEW KDR
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Civil Engineering Services

603-772-4746

E-MAIL: JBE@JONESANDBEACH.COM

Plan Name: DEMOLITION PLAN

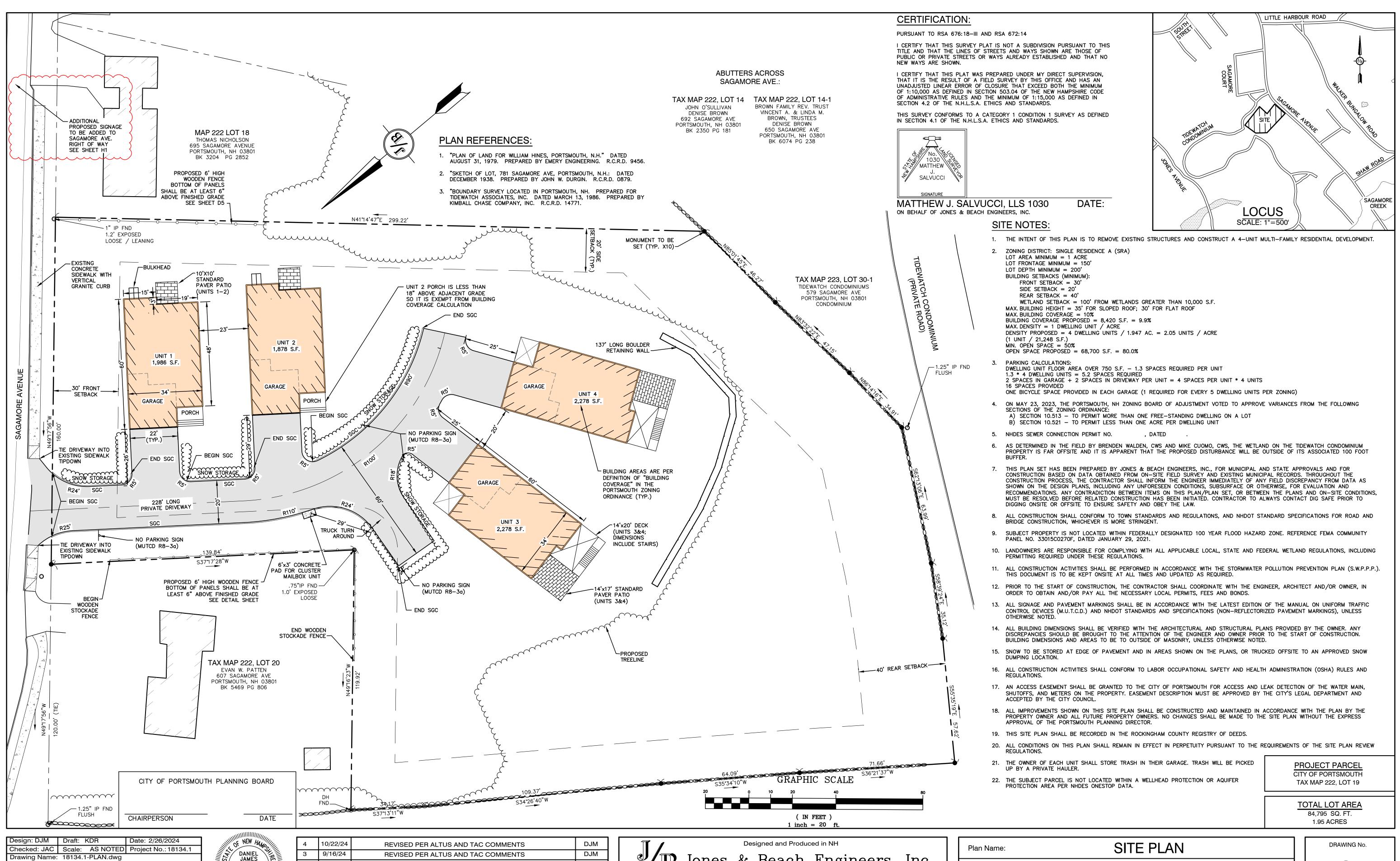
LUSTER CLUSTER
635 SAGAMORE AVE., PORTSMOUTH, NH

635 SAGAMORE AVE., PORTSMOUTH, NH

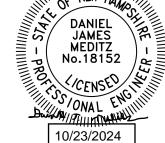
635 SAGAMORE DEVELOPMENT LLC

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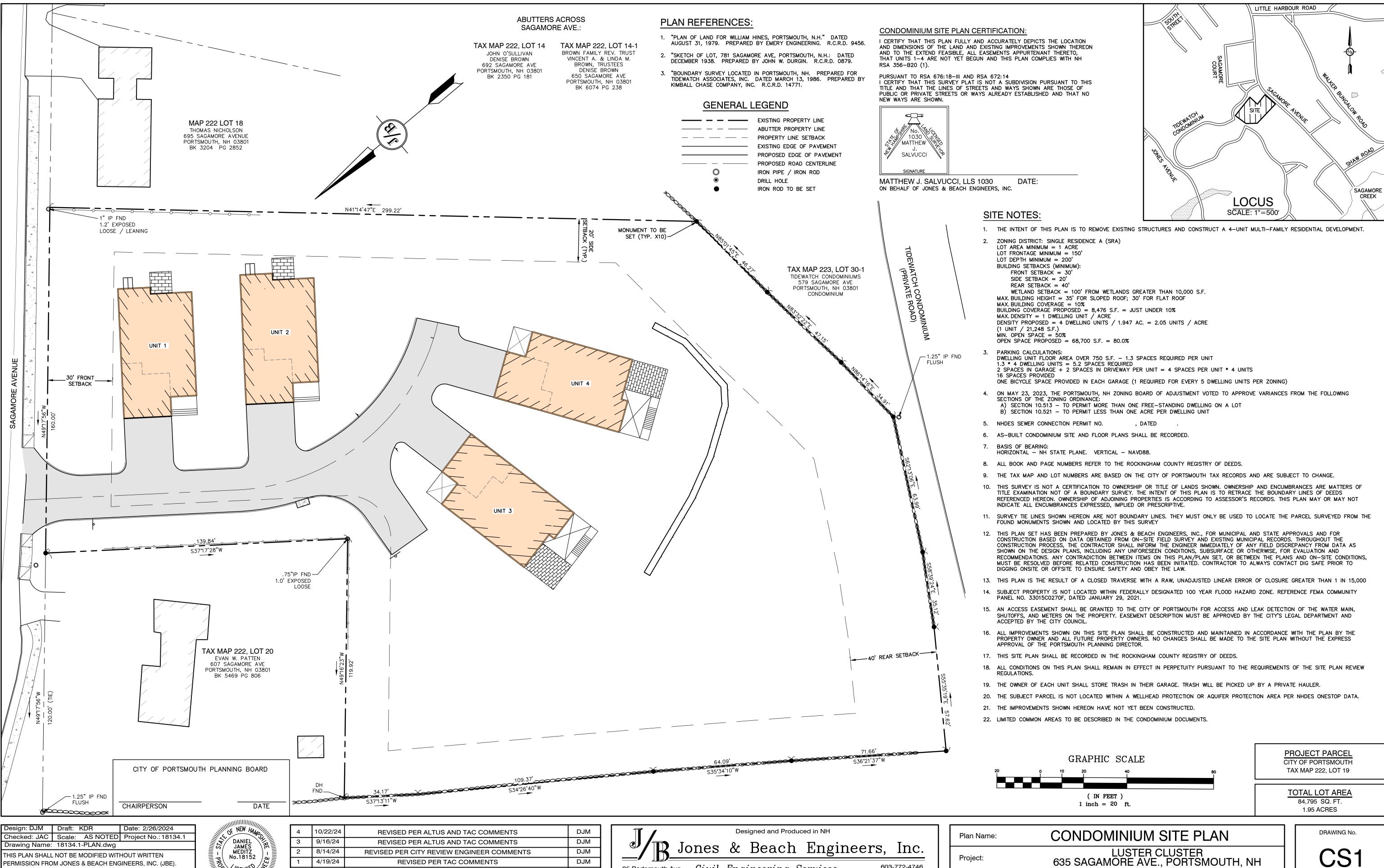
8/14/24 REVISED PER CITY REVIEW ENGINEER COMMENTS DJM 4/19/24 DJM **REVISED PER TAC COMMENTS** KDR 3/18/24 ISSUED FOR REVIEW DATE **REVISION** BY REV.

85 Portsmouth Ave. Civil Engineering Services 603-772-4746 FAX: 603-772-0227 PO Box 219 E-MAIL: JBE@JONESANDBEACH.COM Stratham, NH 03885

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH Project:

635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

JBE PROJECT NO. 18134.1



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Project:

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603-772-4746

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No.18152

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4/19/24

3/18/24

DATE

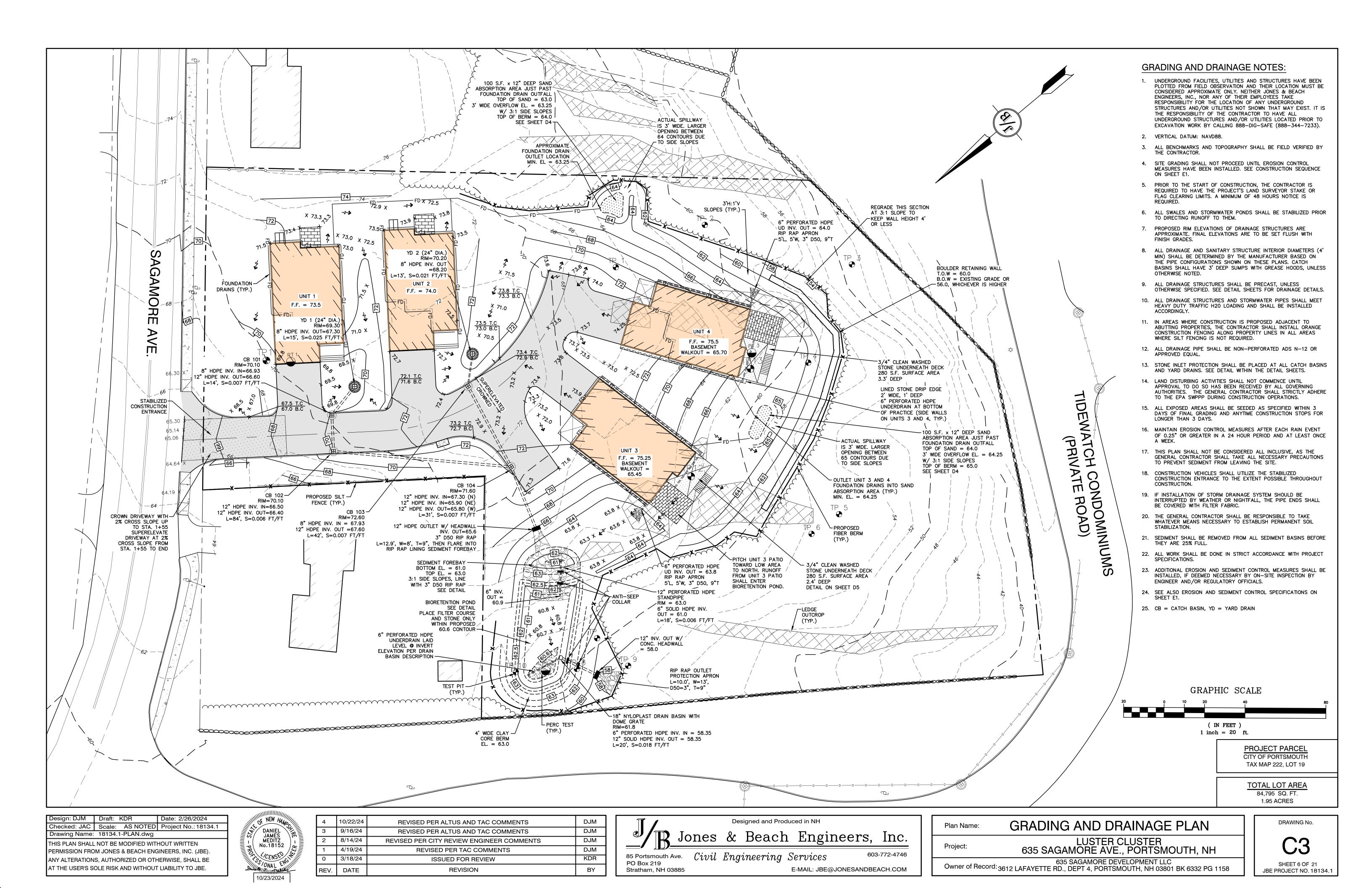
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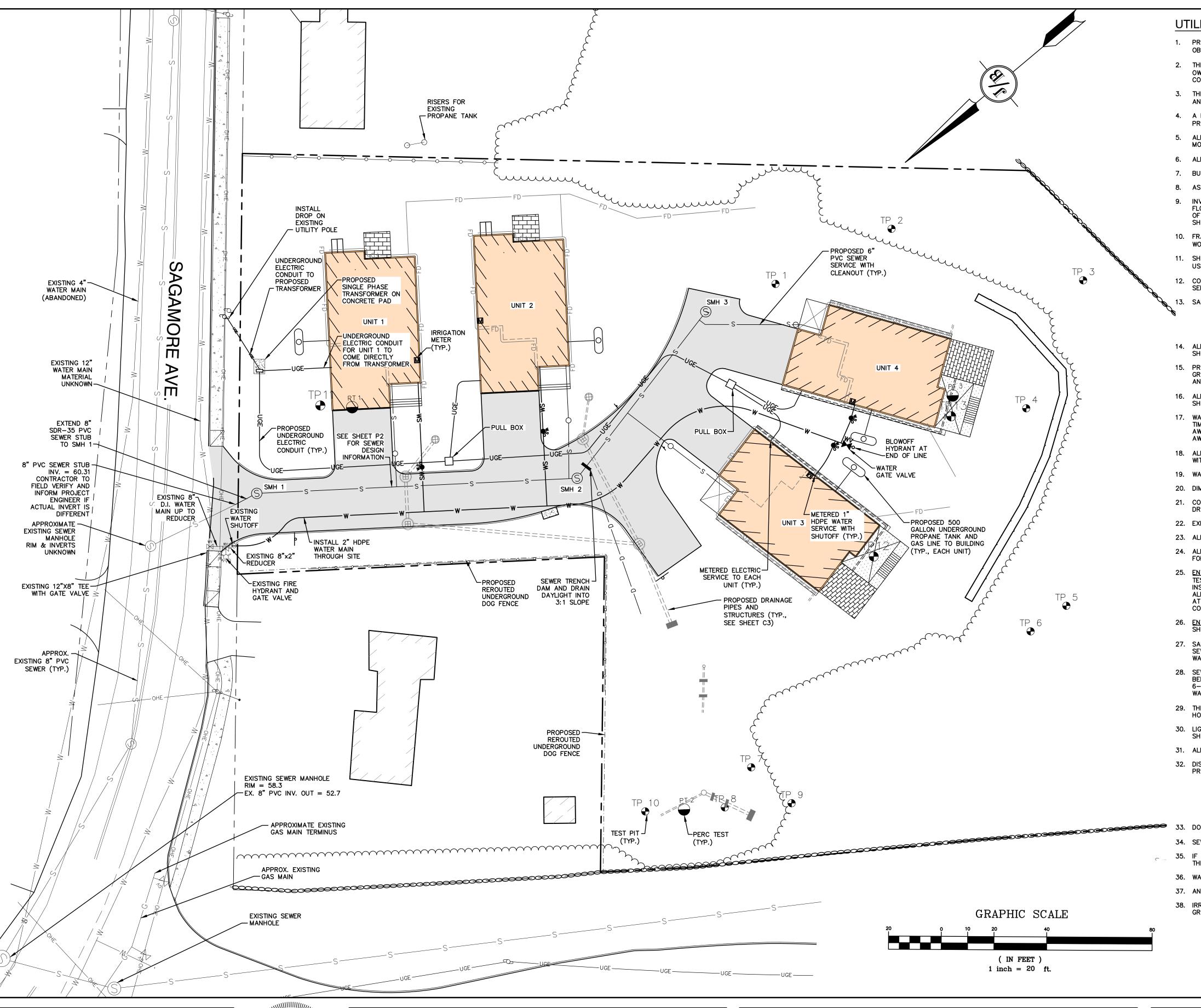
REVISED PER TAC COMMENTS

ISSUED FOR REVIEW

REVISION

JBE PROJECT NO. 18134.1





UTILITY NOTES:

- PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR SHALL COORDINATE WITH THE ENGINEER, ARCHITECT AND/OR OWNER, IN ORDER TO OBTAIN AND/OR PAY ALL THE NECESSARY LOCAL PERMITS, CONNECTION FEES AND BONDS.
- 2. THE CONTRACTOR SHALL PROVIDE A MINIMUM NOTICE OF FOURTEEN (14) DAYS TO ALL CORPORATIONS, COMPANIES AND/OR LOCAL AUTHORITIES OWNING OR HAVING A JURISDICTION OVER UTILITIES RUNNING TO, THROUGH OR ACROSS PROJECT AREAS PRIOR TO DEMOLITION AND/OR
- 3. THE LOCATION, SIZE, DEPTH AND SPECIFICATIONS FOR CONSTRUCTION OF PROPOSED PRIVATE UTILITY SERVICES SHALL BE TO THE STANDARDS AND REQUIREMENTS OF THE RESPECTIVE UTILITY COMPANY (ELECTRIC, TELEPHONE, CABLE TELEVISION, WATER, AND SEWER).
- 4. A PRECONSTRUCTION MEETING SHALL BE HELD WITH THE OWNER, ENGINEER, ARCHITECT, CONTRACTOR, LOCAL OFFICIALS, AND ALL PROJECT-RELATED UTILITY COMPANIES (PUBLIC AND PRIVATE) PRIOR TO START OF CONSTRUCTION.
- ALL CONSTRUCTION SHALL CONFORM TO THE CITY STANDARDS AND REGULATIONS, AND NHDES STANDARDS AND SPECIFICATIONS, WHICHEVER ARE MORE STRINGENT, UNLESS OTHERWISE SPECIFIED.
- 6. ALL CONSTRUCTION ACTIVITIES SHALL CONFORM TO LABOR OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA) RULES AND REGULATIONS.
- 7. BUILDINGS TO BE SERVICED BY UNDERGROUND UTILITIES UNLESS OTHERWISE NOTED.
- 8. AS-BUILT PLANS SHALL BE SUBMITTED TO DEPARTMENT OF PUBLIC WORKS.
- 9. INVERTS AND SHELVES: MANHOLES SHALL HAVE A BRICK PAVED SHELF AND INVERT, CONSTRUCTED TO CONFORM TO THE SIZE OF PIPE AND FLOW AT CHANGES IN DIRECTION. THE INVERTS SHALL BE LAID OUT IN CURVES OF THE LONGEST RADIUS POSSIBLE TANGENT TO THE CENTER LINE OF THE SEWER PIPES. SHELVES SHALL BE CONSTRUCTED TO THE ELEVATION OF THE THROUGH CHANNEL UNDERLAYMENT OF INVERT, AND SHELF
- 10. FRAMES AND COVERS: MANHOLE FRAMES AND COVERS SHALL BE OF HEAVY DUTY DESIGN AND PROVIDE A 30 INCH DIA, CLEAR OPENING. THE WORD "SEWER" SHALL BE CAST INTO THE CENTER OF THE UPPER FACE OF EACH COVER WITH RAISED, 3" LETTERS.
- 11. SHALLOW MANHOLE: IN LIEU OF A CONE SECTION, WHEN MANHOLE DEPTH IS LESS THAN 6 FEET, A REINFORCED CONCRETE SLAB COVER MAY BE USED HAVING AN ECCENTRIC ENTRANCE OPENING AND CAPABLE OF SUPPORTING H20 LOADS. (THIS APPLIES TO SMH 1)
- 12. CONTRACTOR SHALL PLACE 2" WIDE METAL WIRE IMPREGNATED RED PLASTIC WARNING TAPE OVER ENTIRE LENGTH OF ALL GRAVITY SEWERS,
- SANITARY SEWER FLOW CALCULATIONS:
 - 4 FOUR BEDROOM UNITS. ASSUME 5 PEOPLE IN 4-BEDROOM UNITS PER METCALF & EDDY TABLE 3-2: 61 GPD/PERSON IN 5 PERSON HOUSE
 - (61 GPD * 5 PEOPLE * 4) = 1,220 GPD.
 - 1,000 GPD ADDITIONAL ESTIMATED WATER USE FOR IRRIGATION
- 14. ALL SANITARY STRUCTURE INTERIOR DIAMETERS (4' MIN) SHALL BE DETERMINED BY THE MANUFACTURER BASED ON THE PIPE CONFIGURATIONS SHOWN ON THESE PLANS.
- 15. PROPOSED RIM ELEVATIONS OF DRAINAGE AND SANITARY MANHOLES ARE APPROXIMATE. FINAL ELEVATIONS ARE TO BE SET FLUSH WITH FINISH GRADES. ADJUST ALL OTHER RIM ELEVATIONS OF MANHOLES, WATER GATES, AND OTHER UTILITIES TO FINISH GRADE AS SHOWN ON THE GRADING
- 16. ALL WATER MAINS AND SERVICE PIPES SHALL HAVE A MINIMUM 12" VERTICAL AND 24" HORIZONTAL SEPARATION TO MANHOLES, OR CONTRACTOR SHALL INSTALL BOARD INSULATION FOR FREEZING PROTECTION.
- 17. WATER MAINS SHALL BE HYDROSTATICALLY PRESSURE TESTED FOR LEAKAGE PRIOR TO ACCEPTANCE. WATERMAINS SHALL BE TESTED AT 1.5 TIMES THE WORKING PRESSURE OR 150 PSI, WHICH EVER IS GREATER. TESTING SHALL BE CONDUCTED IN ACCORDANCE WITH SECTION 4 OF AWWA STANDARD C 600. WATERMAINS SHALL BE DISINFECTED AFTER THE ACCEPTANCE OF THE PRESSURE AND LEAKAGE TESTS ACCORDING TO
- 18. ALL WATER AND SANITARY LEADS TO BUILDING(S) SHALL END 5' OUTSIDE THE BUILDING LIMITS AS SHOWN ON PLANS AND SHALL BE PROVIDED WITH A TEMPORARY PLUG AND WITNESS AT END.
- 19. WATER LINE TO BE DEFLECTED IN LIEU OF THRUST BLOCKS AT BENDS.
- 20. DIMENSIONS ARE SHOWN TO CENTERLINE OF PIPE OR FITTING.
- 21. CONTRACTOR TO FURNISH SHOP DRAWINGS FOR UTILITY RELATED ITEMS TO ENSURE CONFORMANCE WITH THE PLANS AND SPECIFICATIONS. SHOP DRAWINGS SHOULD BE SENT IN TRIPLICATE TO THE DESIGN ENGINEER FOR REVIEW AND APPROVAL PRIOR TO INSTALLATION.
- 22. EXISTING UTILITIES SHALL BE DIGSAFED BEFORE CONSTRUCTION.
- 23. ALL WATER LINES SHALL HAVE TESTABLE BACKFLOW PREVENTERS AT THE ENTRANCE TO EACH BUILDING.
- 24. ALL GRAVITY SEWER PIPE, MANHOLES, AND FORCE MAINS SHALL BE TESTED ACCORDING TO NHDES STANDARDS OF DESIGN AND CONSTRUCTION FOR SEWAGE AND WASTEWATER TREATMENT FACILITIES, CHAPTER ENV-WQ 700. ADOPTED ON 10-15-14.
- 25. ENV-WQ 704.06 GRAVITY SEWER PIPE TESTING: GRAVITY SEWERS SHALL BE TESTED FOR WATER TIGHTNESS BY USE OF LOW-PRESSURE AIR TESTS CONFORMING WITH ASTM F1417-92(2005) OR UNI-BELL PVC PIPE ASSOCIATION UNI-B-6. LINES SHALL BE CLEANED AND VISUALLY INSPECTED AND TRUE TO LINE AND GRADĖ. DEFLECTION TESTS SHALL TAKE PLACE AFTER 30 DAYS FOLLOWING INSTALLATION AND THE MAXIMUM ALLOWABLE DEFLECTION OF FLEXIBLE SEWER PIPE SHALL BE 5% OF AVERAGE INSIDE DIAMETER. A RIGID BALL OR MANDREL WITH A DIAMETER OF AT LEAST 95% OF THE AVERAGE INSIDE PIPE DIAMETER SHALL BE USED FOR TESTING PIPE DEFLECTION. THE DEFLECTION TEST SHALL BE CONDUCTED WITHOUT MECHANICAL PULLING DEVICES.
- 26. ENV-WQ 704.17 SEWER MANHOLE TESTING: SHALL BE TESTED FOR LEAKAGE USING A VACUUM TEST PRIOR TO BACKFILLING AND PLACEMENT OF
- 27. SANITARY SEWER LINES SHALL BE LOCATED AT LEAST TEN (10) FEET HORIZONTALLY FROM AN EXISTING OR PROPOSED WATER LINE. WHEN A SEWER LINE CROSSES UNDER A WATER LINE, THE SEWER PIPE JOINTS SHALL BE LOCATED AT LEAST 6 FEET HORIZONTALLY FROM THE WATERMAIN. THE SEWER LINE SHALL ALSO MAINTAIN A VERTICAL SEPARATION OF NOT LESS THAN 18 INCHES.
- 28. SEWERS SHALL BE BURIED TO A MINIMUM DEPTH OF 6 FEET BELOW GRADE IN ALL ROADWAY LOCATIONS, AND TO A MINIMUM DEPTH OF 4 FEET BELOW GRADE IN ALL CROSS-COUNTRY LOCATIONS. PROVIDE TWO-INCHES OF R-10 FOAM BOARD INSULATION 2-FOOT WIDE TO BE INSTALLED 6-INCHES OVER SEWER PIPE IN AREAS WHERE DEPTH IS NOT ACHIEVED. A WAIVER FROM THE DEPARTMENT OF ENVIRONMENTAL SERVICES WASTEWATER ENGINEERING BUREAU IS REQUIRED PRIOR TO INSTALLING SEWER AT LESS THAN MINIMUM COVER.
- 29. THE CONTRACTOR SHALL MINIMIZE THE DISRUPTIONS TO THE EXISTING SEWER FLOWS AND THOSE INTERRUPTIONS SHALL BE LIMITED TO FOUR (4) HOURS OR LESS AS DESIGNATED BY THE CITY SEWER DEPARTMENT.
- 30. LIGHTING CONDUIT SHALL BE SCHEDULE 40 PVC, AND SHALL BE INSTALLED IN CONFORMANCE WITH THE NATIONAL ELECTRIC CODE. CONTRACTOR SHALL PROVIDE EXCAVATION AND BACKFILL.
- 31. ALL TRENCHING, PIPE LAYING, AND BACKFILLING SHALL BE IN ACCORDANCE WITH FEDERAL OSHA REGULATIONS.
- 32. DISINFECTION OF WATER MAINS SHALL BE CARRIED OUT IN STRICT ACCORDANCE WITH AWWA STANDARD C651, LATEST EDITION. THE BASIC
 - PROCEDURE TO BE FOLLOWED FOR DISINFECTING WATER MAINS IS AS FOLLOWS: PREVENT CONTAMINATING MATERIALS FROM ENTERING THE WATER MAIN DURING STORAGE, CONSTRUCTION, OR REPAIR.
 - REMOVE, BY FLUSHING OR OTHER MEANS, THOSE MATERIALS THAT MAY HAVE ENTERED THE WATER MAINS. CHLORINATE ANY RESIDUAL CONTAMINATION THAT MAY REMAIN, AND FLUSH THE CHLORINATED WATER FROM THE MAIN. PROTECT THE EXISTING DISTRIBUTION SYSTEM FROM BACKFLOW DUE TO HYDROSTATIC PRESSURE TEST AND DISINFECTION PROCEDURES. DETERMINE THE BACTERIOLOGICAL QUALITY BY LABORATORY TEST AFTER DISINFECTION.
- MAKE FINAL CONNECTION OF THE APPROVED NEW WATER MAIN TO THE ACTIVE DISTRIBUTION SYSTEM 33. DOMESTIC SHUTOFFS & VALVES SHALL BE PAINTED BLUE.
- 34. SEWER TRENCH DAMS SHALL BE INSTALLED EVERY 75' ALONG GRAVITY SEWER PIPE.
- 35. IF IRRIGATION IS TO BE USED, THE PIPING SYSTEM SHALL BE REVIEWED AND APPROVED BY THE PORTSMOUTH CITY PLANNER, CITY ENGINEER, AND THE WATER DEPARTMENT PRIOR TO INSTALLATION.
- 36. WATER LINE TO BE CONSTRUCTED PER CITY OF PORTSMOUTH SPECIFICATIONS.
- 37. AN AS-BUILT PLAN OF THE WATER LINE IS TO BE PREPARED AND SUBMITTED TO THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS.
- 38. IRRIGATION METERS SHALL BE USED IF IRRIGATION IS DESIRED. IF USED, THEY SHALL BE ABOVE GROUND AND INSIDE OF A STRUCTURE, AND SHALL HAVE BACKFLOW ENCLOSURES.

PROJECT PARCEL CITY OF PORTSMOUTH TAX MAP 222, LOT 19

TOTAL LOT AREA 84,795 SQ. FT. 1.95 ACRES

Design: DJM | Draft: KDR Date: 2/26/2024 Checked: JAC | Scale: AS NOTED | Project No.: 18134.1 Drawing Name: 18134.1-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE T THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

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REV.	DATE	REVISION	BY

Designed and Produced in NH

PO Box 219

603-772-4746 85 Portsmouth Ave. Civil Engineering Services FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM Stratham, NH 03885

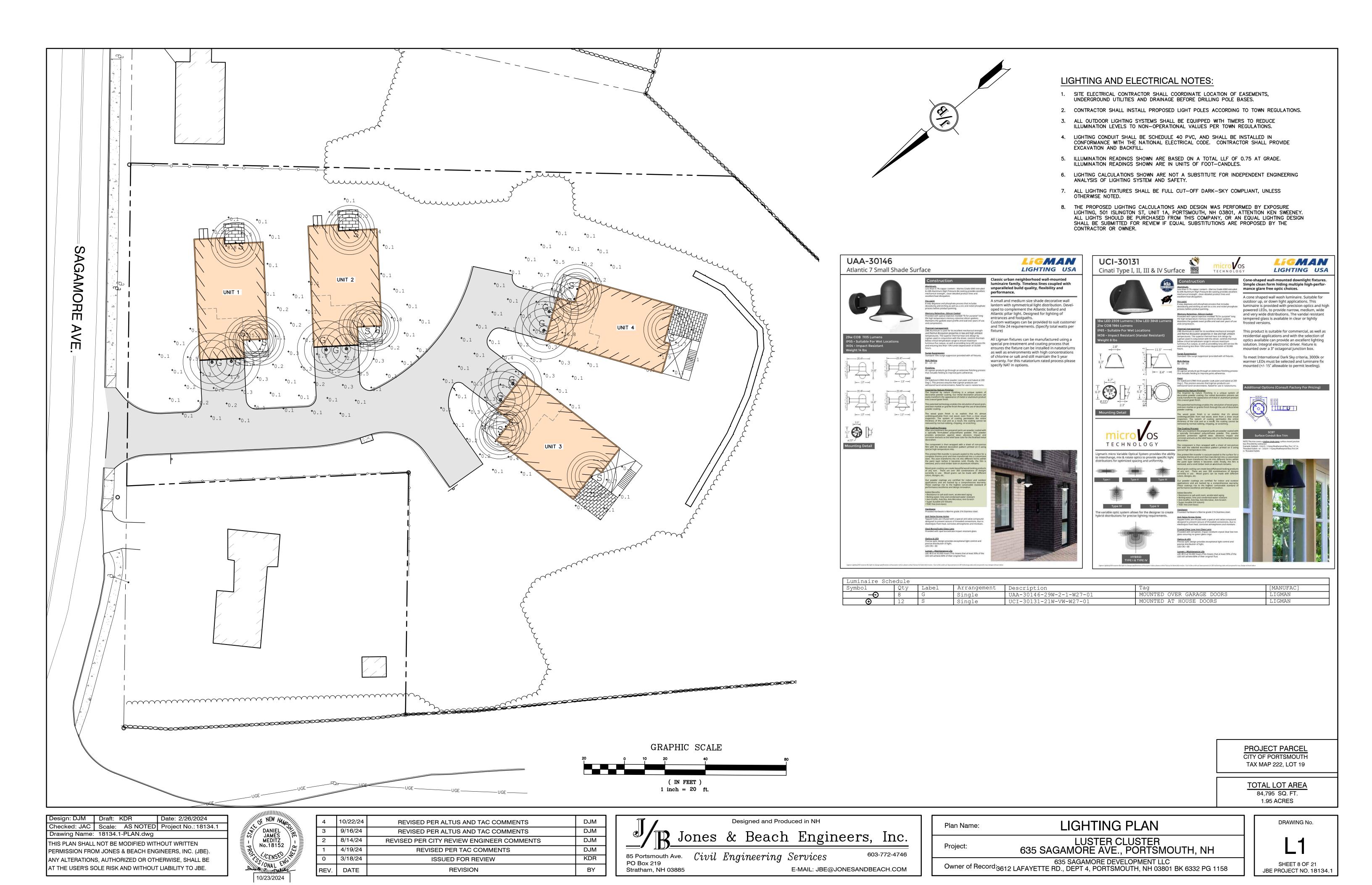
UTILITY PLAN Plan Name:

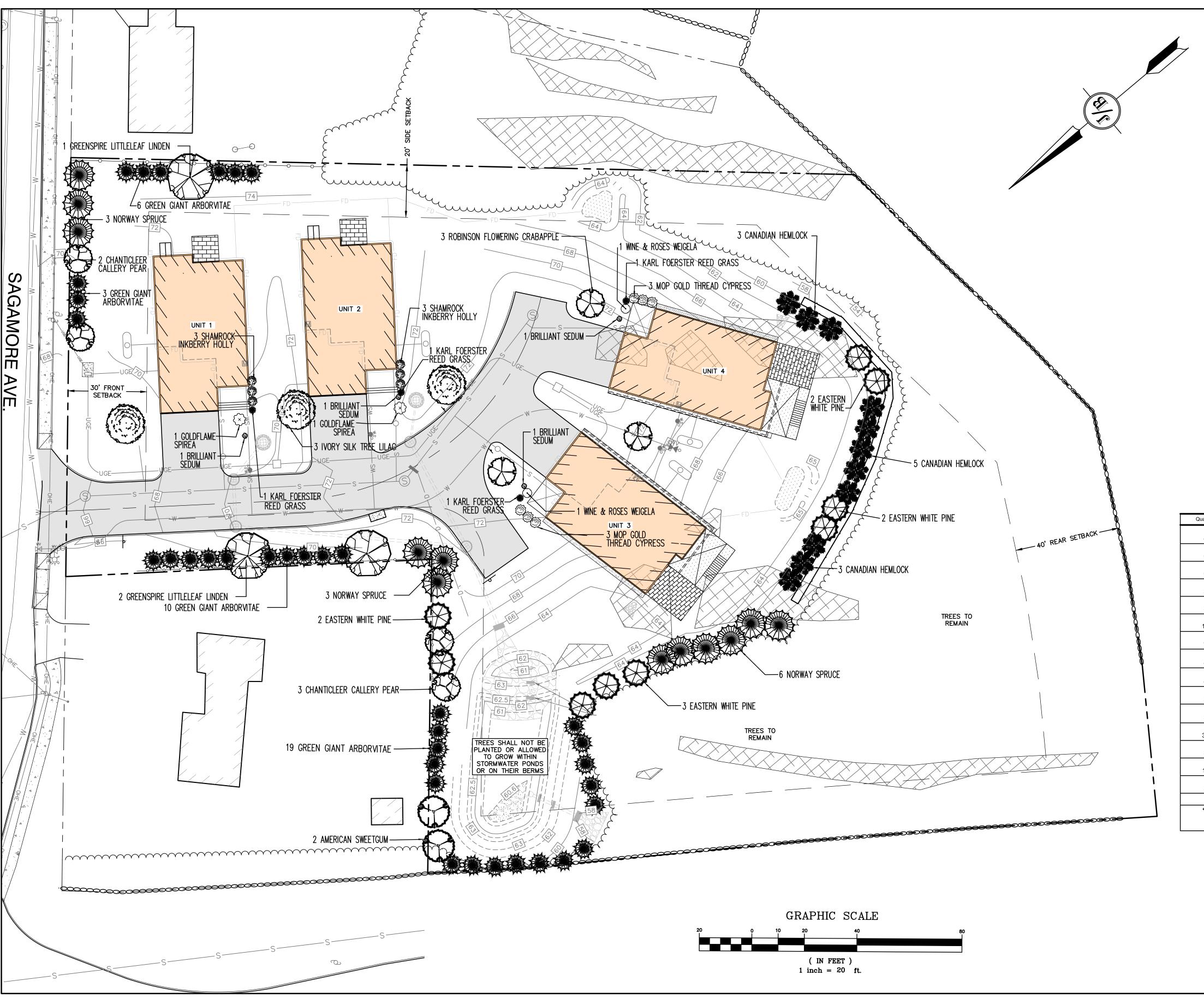
Project:

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH

635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158 JBE PROJECT NO. 18134.1

DRAWING No.





LANDSCAPE NOTES:

- 1. THE CONTRACTOR SHALL LOCATE AND VERIFY THE EXISTENCE OF ALL UTILITIES PRIOR TO STARTING WORK.
- THE CONTRACTOR SHALL SUPPLY ALL PLANT MATERIALS IN QUANTITIES SUFFICIENT TO COMPLETE THE PLANTINGS SHOWN ON THE
- ALL MATERIAL SHALL CONFORM TO THE GUIDELINES ESTABLISHED BY THE CURRENT AMERICAN STANDARD FOR NURSERY STOCK PUBLISHED BY THE AMERICAN ASSOCIATION OF NURSERYMEN.
- 4. PLANTS SHALL BE SUBJECT TO INSPECTION AND APPROVAL AT THE PLACE OF GROWTH, UPON DELIVERY OR AT THE JOB SITE WHILE WORK IS ON-GOING FOR CONFORMITY TO SPECIFIED QUALITY, SIZE AND VARIETY.
- PLANTS FURNISHED IN CONTAINERS SHALL HAVE THE ROOTS WELL ESTABLISHED IN THE SOIL MASS AND SHALL HAVE AT LEAST ONE (1) GROWING SEASON. ROOT-BOUND PLANTS OR INADEQUATELY SIZED CONTAINERS TO SUPPORT THE PLANT MAY BE DEEMED UNACCEPTABLE.
- 6. NO PLANT SHALL BE PUT IN THE GROUND BEFORE GRADING HAS BEEN COMPLETED.
- 7. ALL WORK AND PLANTS SHALL BE DONE, INSTALLED AND DETAILED IN STRICT ACCORDANCE WITH PROJECT SPECIFICATIONS.
- 8. ALL PLANTS SHALL BE WATERED THOROUGHLY TWICE DURING THE FIRST 24-HOUR PERIOD AFTER PLANTING. ALL PLANTS SHALL BE WATERED WEEKLY, OR MORE OFTEN IF NECESSARY, DURING THE FIRST GROWING SEASON.
- 9. ALL LANDSCAPE AREAS TO BE GRASS COMMON TO REGION, EXCEPT FOR INTERIOR LANDSCAPED ISLANDS OR WHERE OTHER PLANT MATERIAL IS SPECIFIED.
- 10. ALL TREES AND SHRUBS SHALL BE PLANTED IN MULCH BEDS WITH EDGE STRIPS TO SEPARATE TURF GRASS AREAS.
- 11. THE CONTRACTOR SHALL REMOVE WEEDS, ROCKS, CONSTRUCTION ITEMS, ETC. FROM ANY LANDSCAPE AREA SO DESIGNATED TO
- REMAIN, WHETHER ON OR OFF-SITE. GRASS SEED OR PINE BARK MULCH SHALL BE APPLIED AS DEPICTED ON PLANS.
- 12. EXISTING TREES TO REMAIN SHALL BE PROTECTED WITH TEMPORARY SNOW FENCING AT THE DRIPLINE OF THE TREE. THE CONTRACTOR SHALL NOT STORE VEHICLES OR MATERIALS WITHIN THE LANDSCAPED AREAS. ANY DAMAGE TO EXISTING TREES, SHRUBS OR LAWN SHALL BE REPAIRED BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.
- 13. ALL MULCH AREAS SHALL RECEIVE A 3" LAYER OF SHREDDED PINE BARK MULCH OVER A 10 MIL WEED MAT EQUAL TO 'WEEDBLOCK' BY EASY GARDENER OR DEWITT WEED BARRIER.
- 14. ALL LANDSCAPED AREAS SHALL HAVE SELECT MATERIALS REMOVED TO A DEPTH OF AT LEAST 9" BELOW FINISH GRADE. THE RESULTING VOID IS TO BE FILLED WITH A MINIMUM OF 9" HIGH-QUALITY SCREENED LOAM AMENDED WITH 3" OF AGED ORGANIC
- 15. THIS PLAN IS INTENDED FOR LANDSCAPING PURPOSES ONLY. REFER TO CIVIL/SITE DRAWINGS FOR OTHER SITE CONSTRUCTION INFORMATION.
- 16. IRRIGATION PIPING SYSTEM SHALL BE REVIEWED AND APPROVED BY OWNER AND ENGINEER PRIOR TO INSTALLATION.
- 17. WITH AUTHORIZATION OF THE PROJECT ENGINEER, PROPOSED TREES ALONG EDGE OF WOODED BUFFER SHALL BE PLACED WHEREVER NECESSARY IN ORDER TO COVER GAPS IN EXISTING WOODED BUFFER IN ORDER TO BLOCK VISIBILITY FROM TIDEWATCH CONDOMINIUM PROPERTY.
- 18. TREES SHALL NOT BE PLANTED ON BERMS OF STORMWATER PONDS.
- 19. ALL PLANTING SHALL ADHERE TO THE GENERAL REQUIREMENTS OUTLINED IN SECTION 6.3 AND THE PLANTING REQUIREMENTS

20. ALL PLANTING SHALL FOLLOW THE ANSI A300 PART 6 STANDARD PRACTICES FOR PLANTING AND TRANSPLANTING (AS AMENDED).

- OUTLINED IN SECTION 6.4 OF THE PORTSMOUTH SITE PLAN REVIEW REGULATIONS.
- 21. LEDGE SHALL BE REMOVED TO AT LEAST 3 FEET BELOW ALL PROPOSED PLANTINGS, OR PLANTS SHALL BE PLACED ON MOUNDS THAT IN A WAY THAT DOES NOT OBSTRUCT DRAINAGE FLOW TO AN ELEVATION AT LEAST 3 FEET ABOVE THE LEDGE SURFACE,

Quantity	Botanical Name	Common Name	Size	Growth Habits
4	Calamagrostis x acutiflora 'Karl Foerster'	KARL FOERSTER REED GRASS **	2 Gallon	5' tall narrow grass
6	Chamaecyparis pisifera 'Mop'	MOP GOLD THREAD CYPRESS **	5 Gallon	4'x5' spreading conifer shrub
6	Ilex glabra 'Shamrock'	SHAMROCK INKBERRY HOLLY **	5 Gallon	5'x4' evergreen shrub
2	Liquidambar styraciflua	AMERICAN SWEETGUM **	3" Caliper	60'x40' upright tree
3	Malus x 'Robinson'	ROBINSON FLOWERING CRABAPPLE **	2" Caliper	20'x20' spreading tree
12	Picea abies	NORWAY SPRUCE	8-9 Ft. Ht.	60'x30' conifer tree
9	Pinus strobus	EASTERN WHITE PINE	8-9 Ft. Ht.	60'x30' conifer tree
4	Pyrus calleryana 'Chanticleer'	CHANTICLEER CALLERY PEAR **	2.5" Caliper	30'x15' upright flowering tree
4	Sedum spectabile 'Brilliant'	BRILLIANT SEDUM **	1 Gallon	18" late season color perennial
2	Spiraea japonica 'Goldflame'	GOLDFLAME SPIREA **	5 Gallon	3'x4' flowering shrub
3	Syringa reticulata 'Ivory Silk'	IVORY SILK TREE LILAC	2" Caliper	30'x20' upright flowering tree
38	Thuja plicata 'Green Giant'	GREEN GIANT ARBORVITAE **	7-8 Ft. Ht.	30'x15' conifer tree
3	Tilia cordata 'Greenspire'	GREENSPIRE LITTLELEAF LINDEN **	3" Caliper	50'x35' upright tree
11	Tsuga canadensis	CANADIAN HEMLOCK	8-9 Ft. Ht.	60'x30' conifer tree
2	Weigela florida 'Alexandra'	WINE & ROSES WEIGELA	5 Gallon	4'x5' flowering shrub
**	Denotes plants that are tolerant of urban conditions including road salt, soil compaction, drought, heat, and air pollution.			

PROJECT PARCEL CITY OF PORTSMOUTH TAX MAP 222, LOT 19

TOTAL LOT AREA 84,795 SQ. FT. 1.95 ACRES

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LANDSCAPE PLAN Plan Name:

Project:

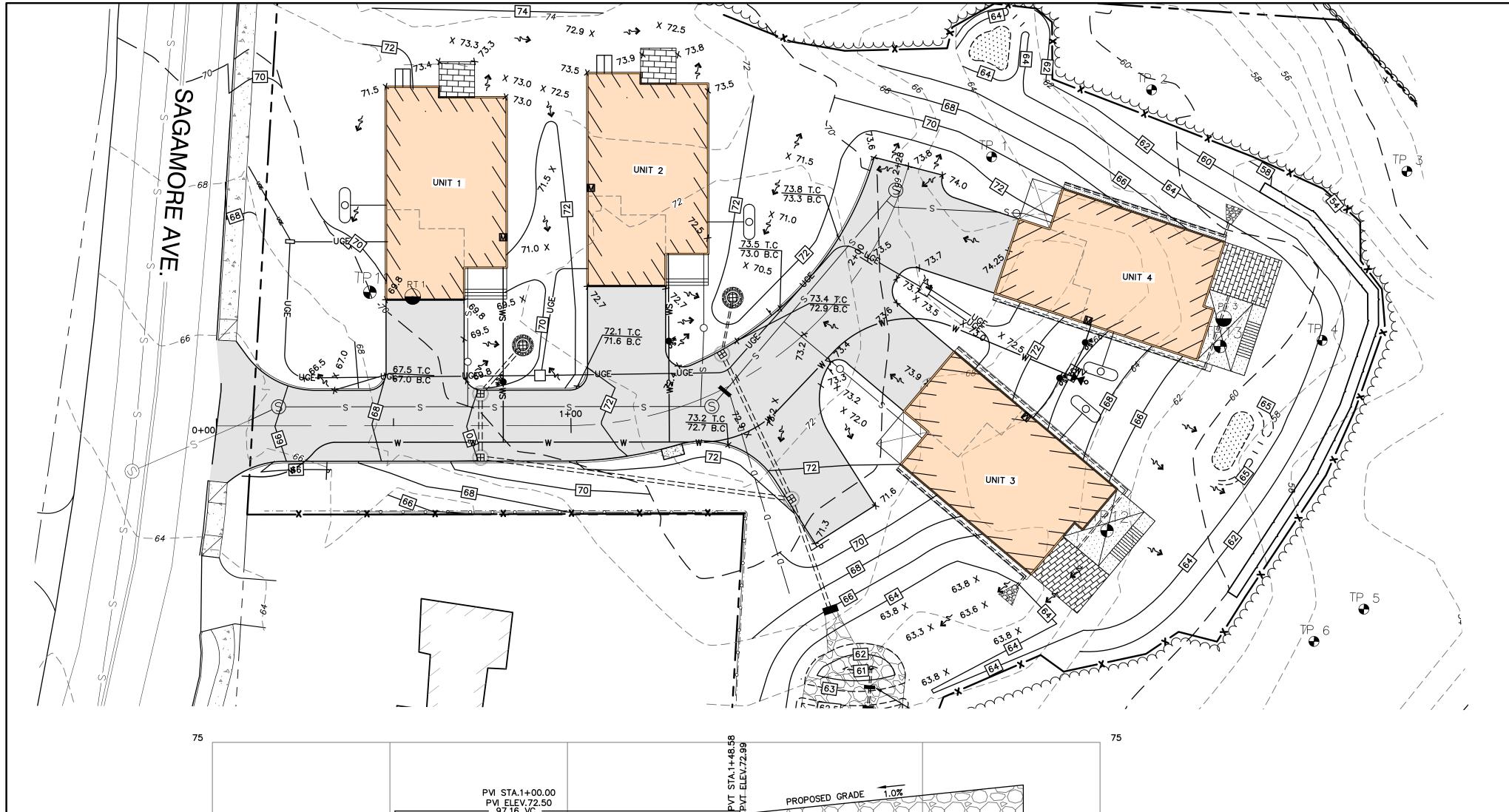
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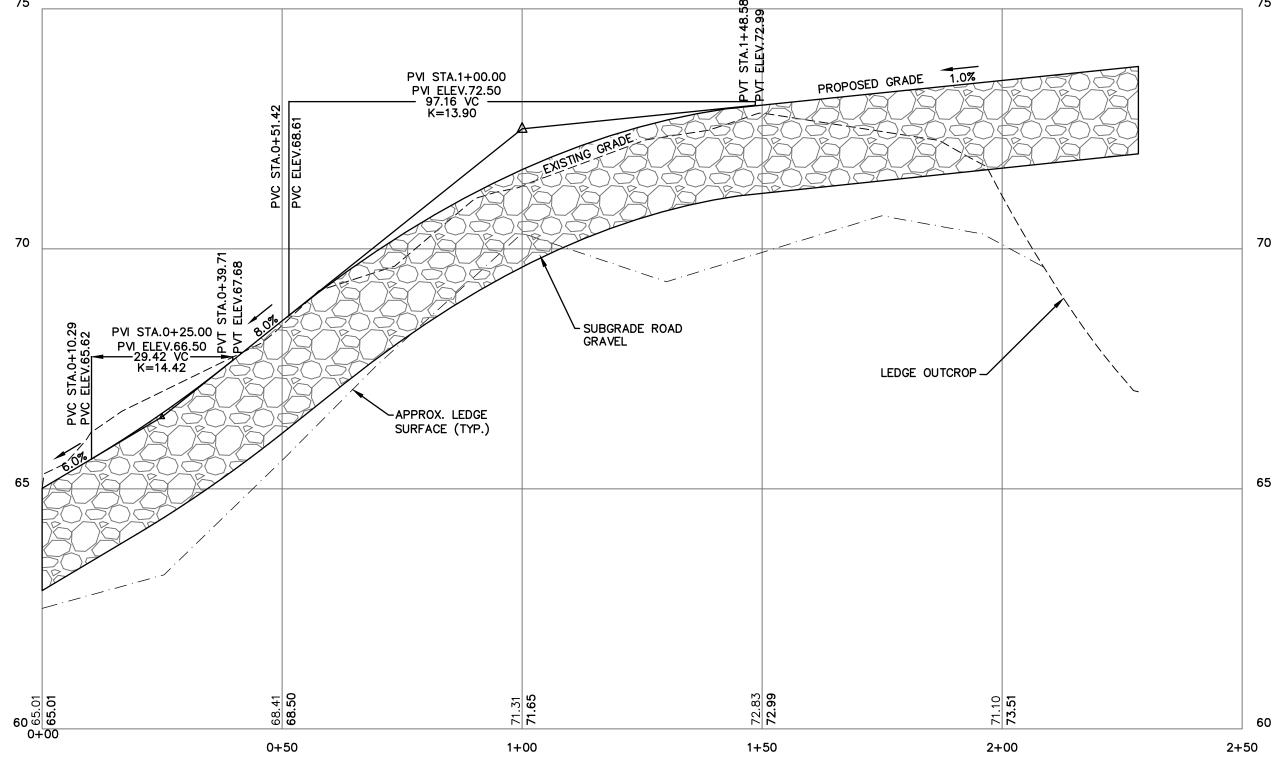
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SHEET 9 OF 21 JBE PROJECT NO. 18134.1

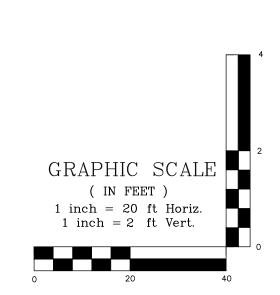
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NOTES:

- THIS SITE WILL REQUIRE A USEPA NPDES PERMIT FOR STORMWATER DISCHARGE FOR THE CONSTRUCTION SITE. THE CONSTRUCTION SITE OPERATOR SHALL DEVELOP AND IMPLEMENT A CONSTRUCTION STORM WATER POLLUTION PREVENTION PLAN (SWPPP), WHICH SHALL REMAIN ON SITE AND BE MADE ACCESSIBLE TO THE PUBLIC. THE CONSTRUCTION SITE OPERATOR SHALL SUBMIT A NOTICE OF INTENT (NOI) TO THE EPA REGIONAL OFFICE SEVEN DAYS PRIOR TO COMMENCEMENT OF ANY WORK ON SITE. EPA WILL POST THE NOI AT HTTP://CFPUB1.EPA.GOV/NPDES/STORMWATER/NOI/NOISEARCH.CFM. AUTHORIZATION IS GRANTED UNDER THE PERMIT ONCE THE NOI IS SHOWN IN "ACTIVE" STATUS ON THIS WEBSITE. A COMPLETED NOTICE OF TERMINATION SHALL BE SUBMITTED TO THE NPDES PERMITTING AUTHORITY WITHIN 30 DAYS AFTER EITHER OF THE FOLLOWING CONDITIONS HAVE BEEN MET:
- A. FINAL STABILIZATION HAS BEEN ACHIEVED ON ALL PORTIONS OF THE SITE FOR WHICH THE PERMITTEE IS RESPONSIBLE; OR
- B. ANOTHER OPERATOR/PERMITTEE HAS ASSUMED CONTROL OVER ALL AREAS OF THE SITE THAT HAVE NOT BEEN FINALLY STABILIZED. PROVIDE DPW WITH A COPY OF THE NOTICE OF TERMINATION (NOT).
- 2. ALL ROAD AND DRAINAGE WORK SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE STANDARD SPECIFICATIONS FOR THE CITY, AND NHDOT SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION, WHICHEVER IS MORE STRINGENT.
- 3. AS-BUILT PLANS TO BE SUBMITTED TO THE CITY PRIOR TO ACCEPTANCE OF THE ROADWAY.
- CONTRACTOR TO COORDINATE AND COMPLETE ALL WORK REQUIRED FOR THE RELOCATION AND/OR INSTALLATION OF ELECTRIC, CATV, TELEPHONE, PER UTILITY DESIGN AND STANDARDS. LOCATIONS SHOWN ARE APPROXIMATE. LOW PROFILE STRUCTURES SHALL BE USED TO THE GREATEST EXTENT POSSIBLE.
- 5. THIS PLAN HAS BEEN PREPARED BY JONES & BEACH ENGINEERS, INC. FOR MUNICIPAL AND STATE APPROVALS AND FOR CONSTRUCTION BASED ON DATA OBTAINED FROM ON—SITE FIELD SURVEY AND EXISTING MUNICIPAL RECORDS. THROUGHOUT THE CONSTRUCTION PROCESS, THE CONTRACTOR SHALL INFORM THE ENGINEER IMMEDIATELY OF ANY FIELD DISCREPANCY FROM DATA SHOWN ON THE DESIGN PLANS. THIS INCLUDES ANY UNFORESEEN CONDITIONS, SUBSURFACE OR OTHERWISE, FOR EVALUATION AND RECOMMENDATIONS. ANY CONTRADICTION BETWEEN ITEMS OF THIS PLAN/PLAN SET, OR BETWEEN THE PLANS AND ON—SITE CONDITIONS MUST BE RESOLVED BEFORE RELATED CONSTRUCTION HAS BEEN INITIATED.
- 6. SILTATION AND EROSION CONTROLS SHALL BE INSTALLED PRIOR TO CONSTRUCTION, SHALL BE MAINTAINED DURING CONSTRUCTION, AND SHALL REMAIN UNTIL SITE HAS BEEN STABILIZED WITH PERMANENT VEGETATION. SEE DETAIL SHEET E1 FOR ADDITIONAL NOTES ON EROSION CONTROL.
- 7. ALL DISTURBED AREAS NOT STABILIZED BY OCTOBER 15TH SHALL BE COVERED WITH AN EROSION CONTROL BLANKET. PRODUCT TO BE SPECIFIED BY THE ENGINEER.
- 8. FINAL DRAINAGE, GRADING AND EROSION PROTECTION MEASURES SHALL CONFORM TO REGULATIONS OF THE PUBLIC WORKS DEPARTMENT.
- 9. CONTRACTOR TO VERIFY EXISTING UTILITIES AND TO NOTIFY ENGINEER OF ANY DISCREPANCY IMMEDIATELY.
- 10. DRAINAGE INSPECTION AND MAINTENANCE SCHEDULE: SILT FENCING WILL BE INSPECTED DURING AND AFTER STORM EVENTS TO ENSURE THAT THE FENCE STILL HAS INTEGRITY AND IS NOT ALLOWING SEDIMENT TO PASS. SEDIMENT BUILD UP IN SWALES WILL BE REMOVED IF IT IS DEEPER THAN SIX INCHES, AND IS TO BE REMOVED FROM SUMPS BELOW THE INLET OF CULVERTS SEMIANNUALLY, AS WELL AS FROM CATCH BASINS. FOLLOWING MAJOR STORM EVENTS, THE STAGE DISCHARGE OUTLET STRUCTURES ARE TO BE INSPECTED AND ANY DEBRIS REMOVED FROM THE ORIFICE, TRASH TRACK AND EMERGENCY SPILL WAY. INFREQUENTLY, SEDIMENT MAY ALSO HAVE TO BE REMOVED FROM THE SUMP OF THE STRUCTURE.
- 11. ALL DRAINAGE INFRASTRUCTURE SHALL BE INSTALLED AND STABILIZED PRIOR TO DIRECTING ANY RUNOFF TO IT.
- 12. BIORETENTION PONDS REQUIRE TIMELY MAINTENANCE AND SHOULD BE INSPECTED AFTER EVERY MAJOR STORM EVENT, AS WELL AS FREQUENTLY DURING THE FIRST YEAR OF OPERATION, AND ANNUALLY THEREAFTER. EVERY FIVE YEARS, THE SERVICES OF A PROFESSIONAL ENGINEER SHOULD BE RETAINED TO PERFORM A THOROUGH INSPECTION OF THE BIORETENTION POND AND ITS INFRASTRUCTURE. ANY DEBRIS AND SEDIMENT ACCUMULATIONS SHOULD BE REMOVED FROM THE OUTLET STRUCTURE(S) AND EMERGENCY SPILLWAY(S) AND DISPOSED OF PROPERLY. BIORETENTION POND BERMS SHOULD BE MOWED AT LEAST ONCE ANNUALLY SO AS TO PREVENT THE ESTABLISHMENT OF WOODY VEGETATION. TREES SHOULD NEVER BE ALLOWED TO GROW ON A BIORETENTION POND BERM, AS THEY MAY DESTABILIZE THE STRUCTURE AND INCREASE THE POTENTIAL FOR FAILURE. AREAS SHOWING SIGNS OF EROSION OR THIN OR DYING VEGETATION SHOULD BE REPAIRED IMMEDIATELY BY WHATEVER MEANS NECESSARY, WITH THE EXCEPTION OF FERTILIZER. RODENT BORROWS SHOULD BE REPAIRED IMMEDIATELY AND THE ANIMALS SHOULD BE TRAPPED AND RELOCATED IF THE PROBLEM PERSISTS.
- 13. IN THOSE AREAS WHERE THE BERMS OF THE BIORETENTION SYSTEMS MUST BE CONSTRUCTED BY THE PLACEMENT OF FILL, THE ENTIRE EMBANKMENT AREA OF THE BIORETENTION PONDS SHALL BE EXCAVATED TO PROPOSED GRADE, STRIPPED OF ALL ORGANIC MATERIALS, COMPACTED TO AT LEAST 95% AND SCARIFIED PRIOR TO THE PLACEMENT OF THE EMBANKMENT MATERIAL. IN THE EVENT THE FOUNDATION MATERIAL EXPOSED DOES NOT ALLOW THE SPECIFIED COMPACTION, AN ADDITIONAL ONE FOOT (1') OF EXCAVATION AND THE PLACEMENT OF A ONE FOOT (1') THICK, TWELVE FOOT (12') WIDE PAD OF THE MATERIAL DESCRIBED IN THE NOTE BELOW, COMPACTED TO 95% OF ASTM D-1557 MAY BE NECESSARY. PLACEMENT AND COMPACTION SHOULD OCCUR AT A MOISTURE CONTENT OF OPTIMUM PLUS OR MINUS 3%, AND NO FROZEN OR ORGANIC MATERIAL SHOULD BE PLACED WITHIN FOR ANY REASON.
- 14. EMBANKMENT IS TO HAVE 3:1 SIDE SLOPES (MAX.) AND IS TO BE BROUGHT TO SPECIFIED GRADES PRIOR TO THE ADDITION OF LOAM (4" MINIMUM) SO AS TO ALLOW FOR THE COMPACTION OF THE STRUCTURE OVER TIME WHILE MAINTAINING THE PROPER BERM FLEXATION
- 15. COMPACTION TESTING SERVICES (I.E. NUCLEAR DENSITY TESTS) ARE TO BE PERFORMED BY AN INDEPENDENT GEOTECHNICAL ENGINEER RETAINED BY THE CONTRACTOR FOR ROADWAY CONSTRUCTION, AND ON THE FOUNDATION OF THE BERM AND ON EVERY



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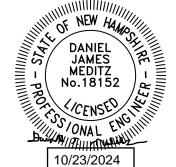
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Jones & Beach Engineers, Inc.

85 Portsmouth Ave. PO Box 219
Stratham, NH 03885

Civil Engineering Services

FAX: 603-772-4746
FAX: 603-772-0227
E-MAIL: JBE@JONESANDBEACH.COM

Plan Name:	DRIVEWAY PLAN AND PROFILE

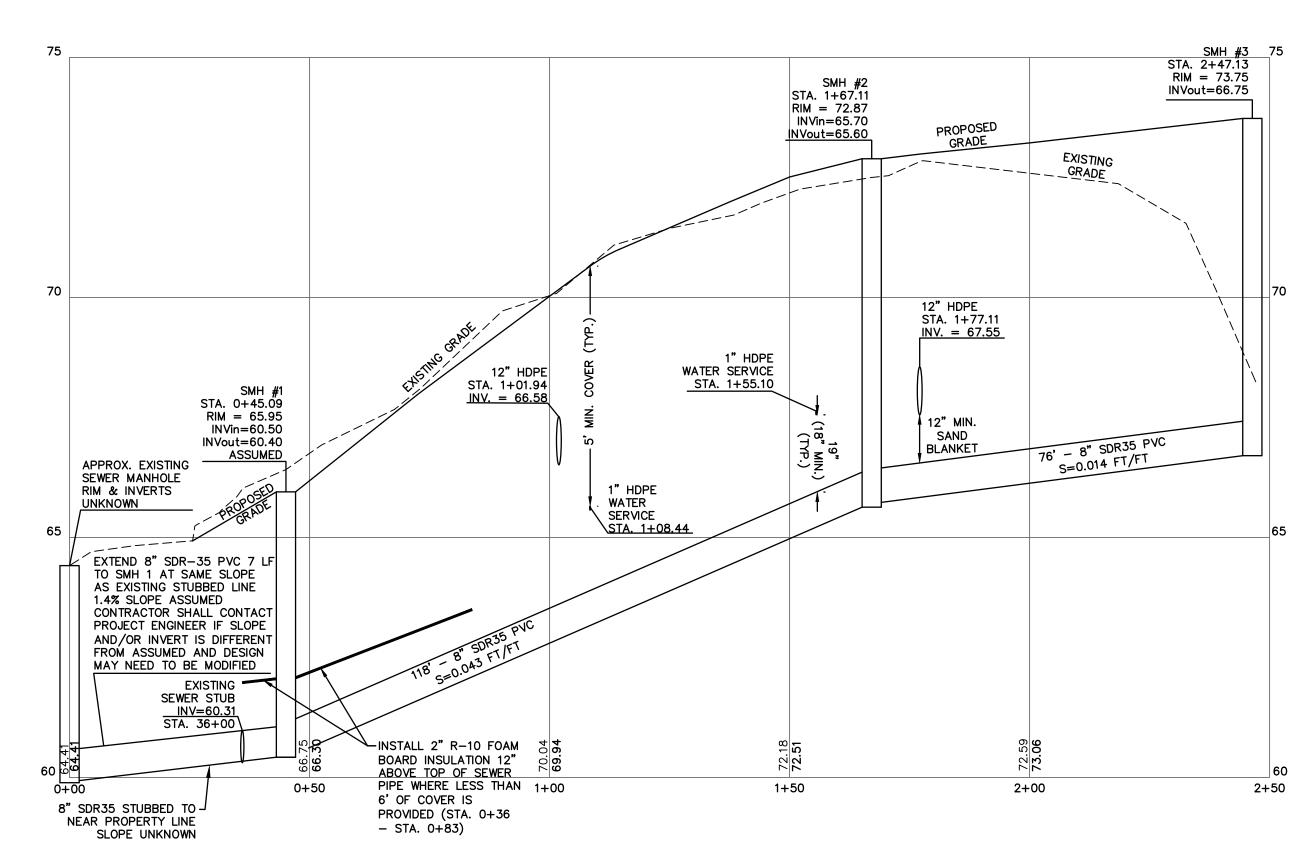
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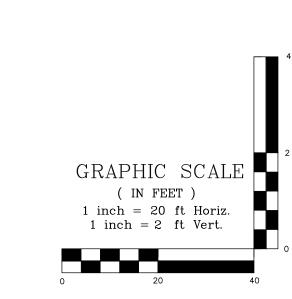
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SHEET 10 OF 21
JBE PROJECT NO. 18134.1



NOTES:

- 1. PROPOSED GRADES SHOWN HEREON ARE APPROXIMATE. REFER TO SHEETS C3 AND P1 FOR GRADING OF SITE AND DRIVEWAY. SET RIM ELEVATIONS OF SEWER STRUCTURES FLUSH WITH PROPOSED GRADE.
- 2. STATIONS REFER TO CENTERLINE OF SEWER STRUCTURE OR CROSSING DRAINAGE/WATER PIPE.
- CONTRACTOR TO CONFIRM ACTUAL EXISTING INVERT OF STUB IN THE FIELD AND NOTIFY ENGINEER IF IT IS MORE THAN 0.1'
 DIFFERENT FROM THE STATED INVERT.





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	1	4/19/24	REVISED PER TAC COMMENTS	DJM
	0	3/18/24	ISSUED FOR REVIEW	KDR
	REV.	DATE	REVISION	BY

Designed and Produced in NH

Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services 603-772-4746

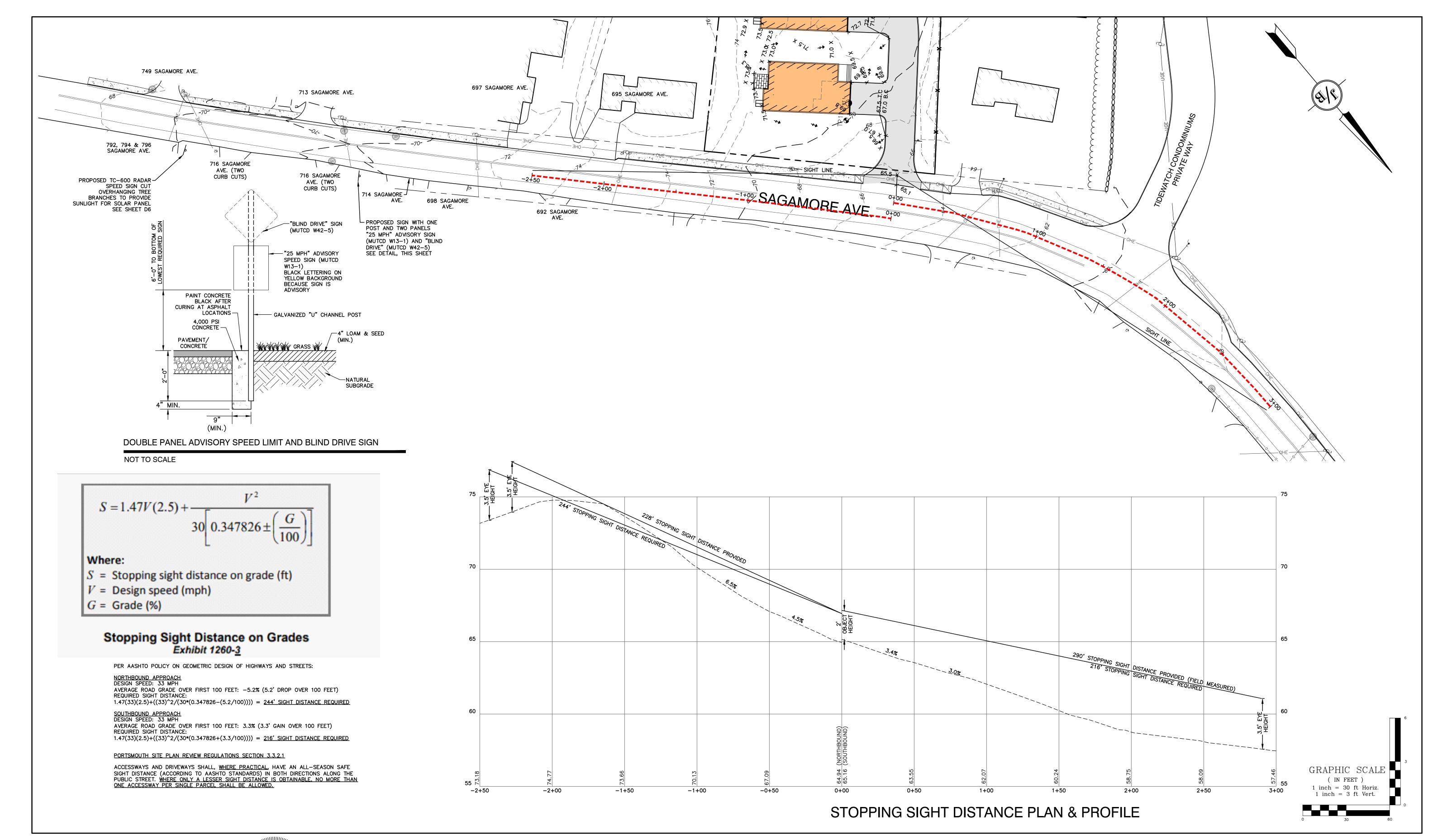
85 Portsmouth Ave. PO Box 219
Stratham, NH 03885

Civil Engineering Services

FAX: 603-772-4746
FAX: 603-772-0227
E-MAIL: JBE@JONESANDBEACH.COM

Plan Name:	SEWER PLAN AND PROFILE
Project:	LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH
Owner of Record	635 SAGAMORE DEVELOPMENT LLC ^{1:} 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

P2
SHEET 11 OF 21
JBE PROJECT NO. 18134.1



Design: DJM	Draft: KDR	Date: 2/26/2024			
Checked: JAC	Scale: AS NOTED	Project No.: 18134.1			
Drawing Name: 18134.1-PLAN.dwg					
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3	9/16/24	REVISED PER ALTUS AND TAC COMMENTS	DJM
2	8/14/24	REVISED PER CITY REVIEW ENGINEER COMMENTS	DJM
1	4/19/24	REVISED PER TAC COMMENTS	DJM
0	3/18/24	ISSUED FOR REVIEW	KDR
REV.	DATE	REVISION	BY

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Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services
PO Box 219

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Engineers, Inc.

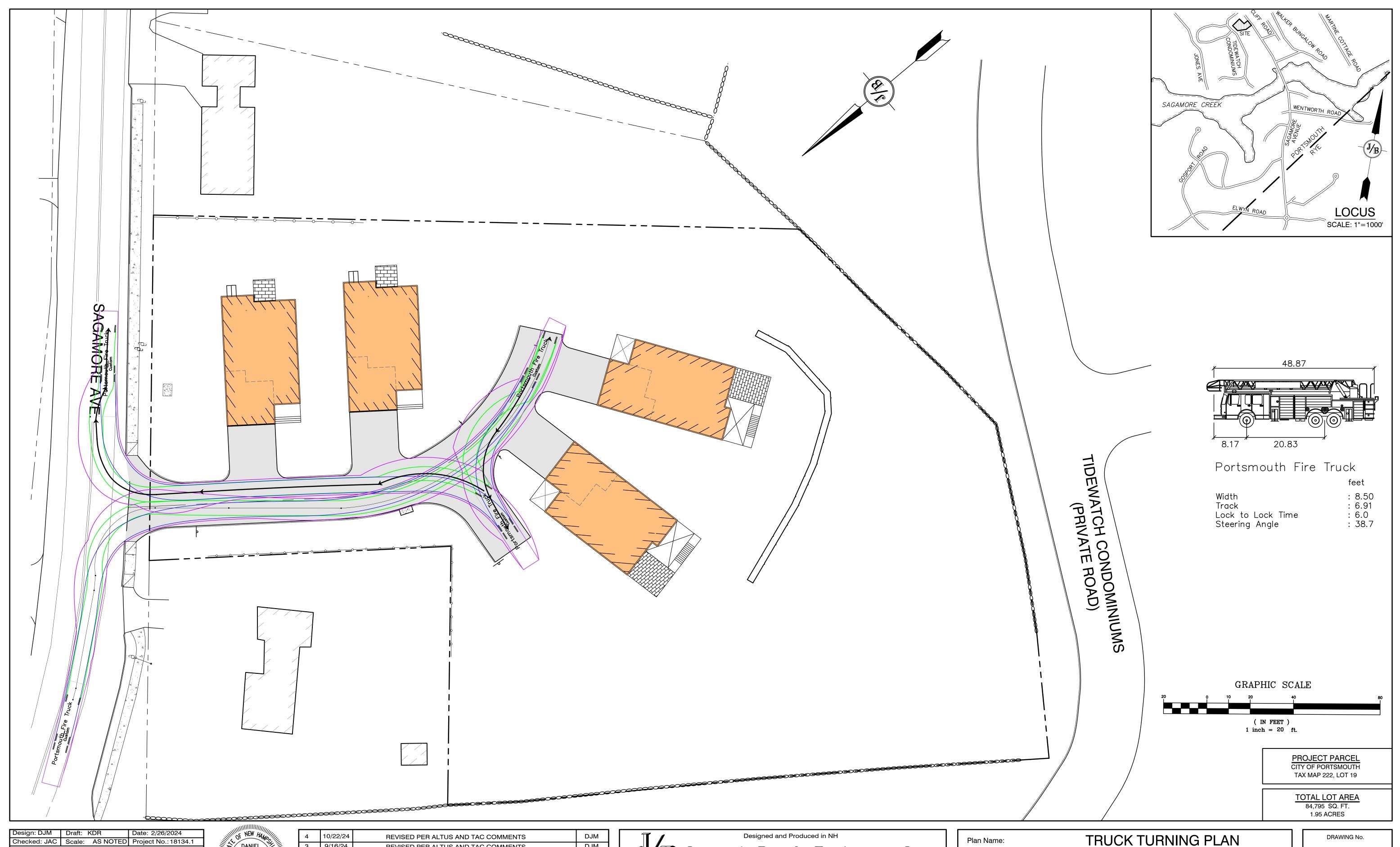
603-772-4746
FAX: 603-772-0227

Stratham, NH 03885

E-MAIL: JBE@JONESANDBEACH.COM

Plan Name:	HIGHWAY ACCESS PLAN	
Project:	LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH	
Owner of Record:	635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158	





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REV.	DATE	REVISION	BY

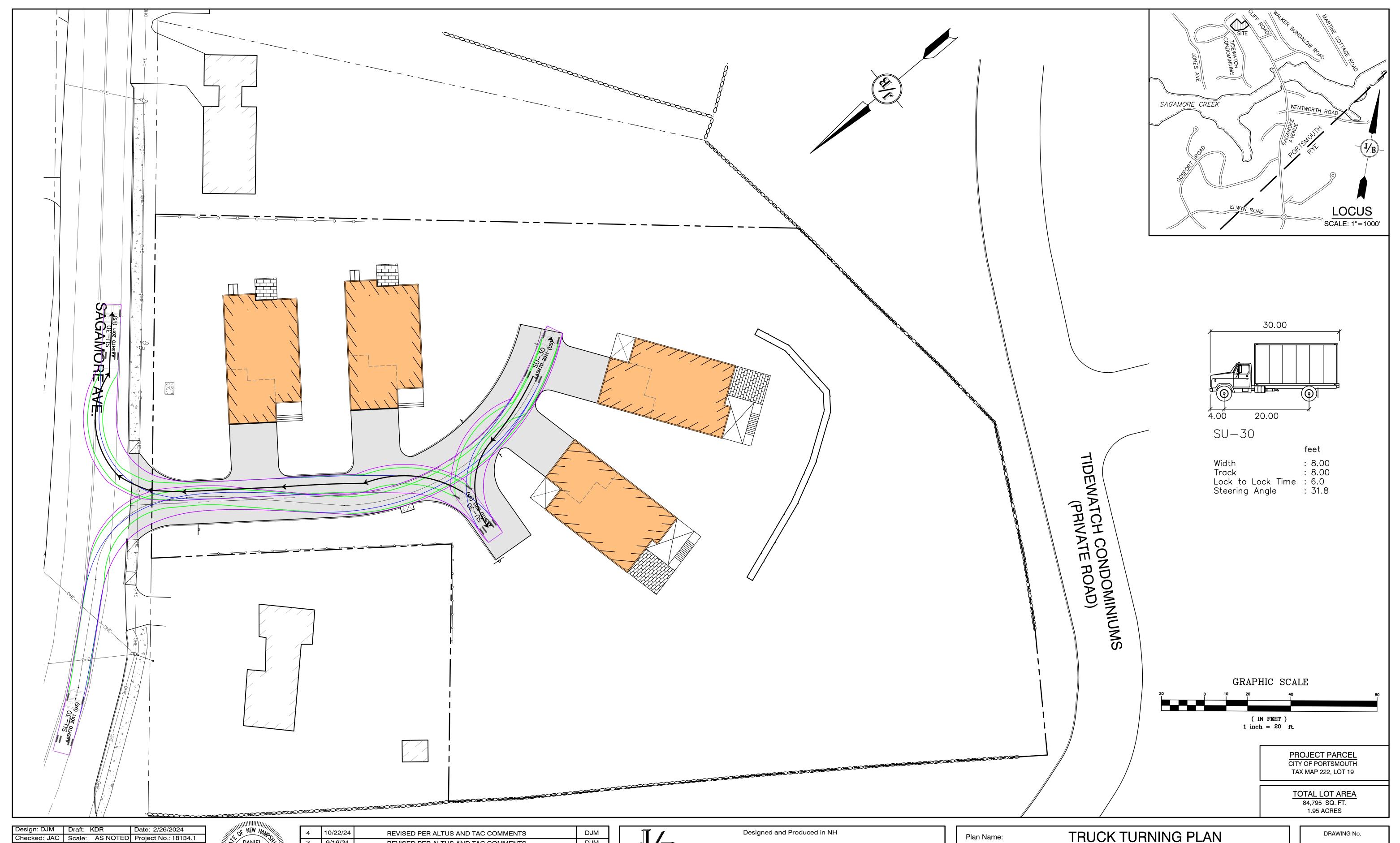
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PO Box 219
Stratham, NH 03885

E-MAIL: JBE@ 603-772-4746 FAX: 603-772-0227

E-MAIL: JBE@JONESANDBEACH.COM

	Plan Name:	TRUCK TURNING PLAN
	Project:	LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH
635 SAGAMORE DEVELOPMENT LLC Owner of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PC		635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

SHEET 13 OF 21 JBE PROJECT NO. 18134.1



Drawing Name: 18134.1-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



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0	3/18/24	ISSUED FOR REVIEW	KDR
REV.	DATE	REVISION	BY

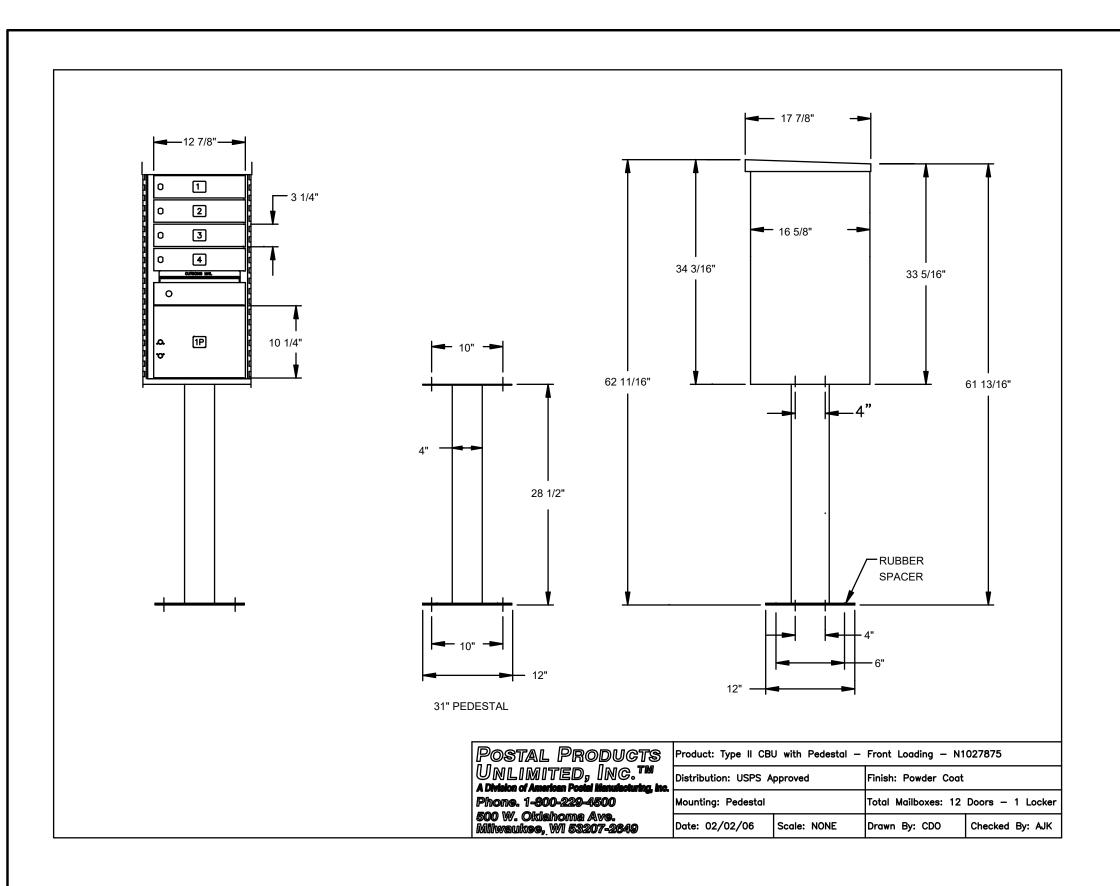
Jones & Beach Engineers, Inc.

Stratham, NH 03885

85 Portsmouth Ave. Civil Engineering Services
PO Box 219 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

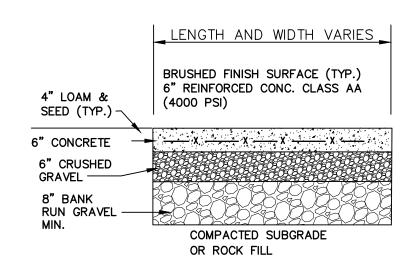
	Plan Name:	TRUCK TURNING PLAN
LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, N		LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH
l	Owner of Record:	635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

SHEET 14 OF 21 JBE PROJECT NO. 18134.1



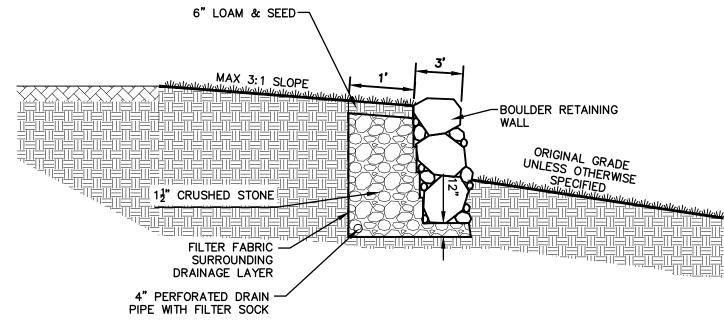
CLUSTER MAILBOX UNIT DETAIL

NOT TO SCALE



CONCRETE PAD DETAIL

NOT TO SCALE



OF NEW HAMP

DANIEL JAMES MEDITZ

No.18152

CENSED

10/23/2024

THE CONTRACTOR IS RESPONSIBLE FOR RETAINING THE SERVICES OF A STRUCTURAL ENGINEER LISENCED IN THE STATE OF NEW HAMPSHIRE TO DESIGN ANY WALL THAT HAS A HEIGHT OVER 4.0'. JONES & BEACH ENGINEERS, INC. DOES NOT ACCEPT ANY LIABILITY FOR THE STRUCTURAL DESIGN AND/OR INSTALLATION OF ANY RETAINING WALL OF ANY TYPE ABOVE THIS HEIGHT. THIS DETAIL IS INTENDED TO PROVIDE AN EXAMPLE OF THE RETAINING WALL FOR PLANNING PURPOSES ONLY AND IS SPECIFICALLY NOT INTENDED FOR USE BY THE CONTRACTOR IN ANY CONSTRUCTION-RELATED ACTIVITY FOR A WALL GREATER THAN 4.0' IN HEIGHT.

Date: 2/26/2024

BOULDER RETAINING WALL CROSS SECTION

Checked: JAC | Scale: AS NOTED | Project No.: 18134.1

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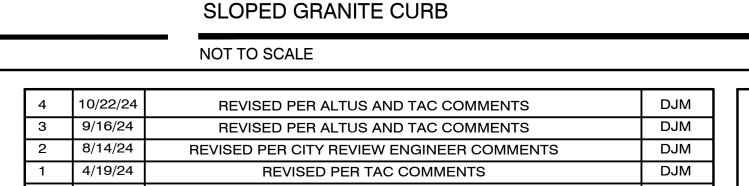
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Design: DJM Draft: KDR

Drawing Name: 18134.1-PLAN.dwg



-SAWCUT AND REMOVE EXIST. PAVEMENT.

ABUTTING PAVEMENT

KEYWAY

9009000000000

TO EXISTING PAVEMENT

KEYWAY DETAIL FOR CONNECTION

BINDER COURSE -

BASE COURSE-

NOT TO SCALE

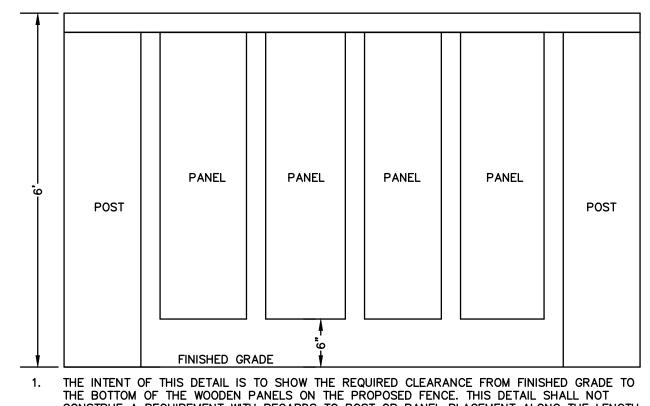
COAT EXPOSED EDGES OF EXISTING PVMT. WITH BIT. EMULSION PRIOR TO PLACING

—1" TOP COURSE

12" MIN. GRAVEL

—2" BINDER COURSE

√—6" CRUSHED GRAVEL

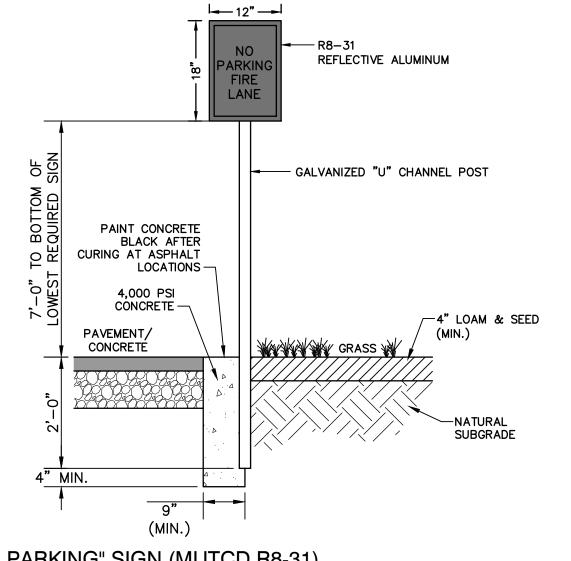


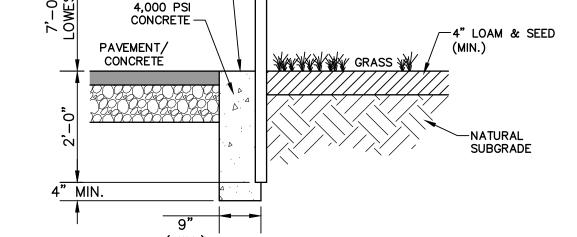
CONSTRUE A REQUIREMENT WITH REGARDS TO POST OR PANEL PLACEMENT ALONG THE LENGTH

6' HIGH WOODEN STOCKADE FENCE DETAIL

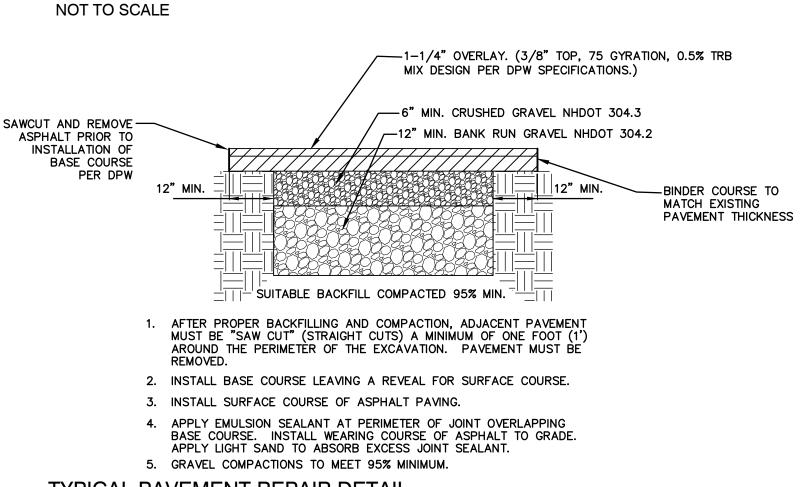
NOT TO SCALE

-PAVED FINISH SURFACE





"NO PARKING" SIGN (MUTCD R8-31)

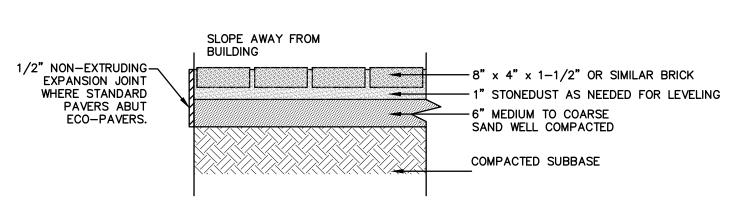


TYPICAL PAVEMENT REPAIR DETAIL

NOT TO SCALE

NHDOT ITEM 609.01 VERTICAL GRANITE CURB THE MAXIMUM ALLOWABLE CROSS SLOPE OF ACCESSIBLE ROUTE (SIDEWALK) AND CURB SHALL BE 1.5%. 2. THE MAXIMUM ALLOWABLE SLOPE OF ACCESSIBLE ROUTE EXCLUDING CURB RAMPS SHALL BE 5%. 3. THE MAXIMUM ALLOWABLE SLOPE OF ACCESSIBLE ROUTE (SIDEWALK) CURB RAMPS SHALL BE 8%. 4. À MINIMUM OF 4 FEET CLEAR SHALL BE MAINTAINED AT ANY PERMANENT OBSTACLE IN ACCESSIBLE ROUTE (i.e., HYDRANTS, UTLITY POLES, TREE WELLS, SIGNS, ETC.).
5. CURB TREATMENT VARIES, SEE PLANS FOR CURB TYPE. BASE OF RAMP SHALL BE GRADED TO PREVENT PONDING. ACCESSIBLE CURB RAMP (TYPE 'B')

NOT TO SCALE



7. SEE TYPICAL SECTION FOR RAMP CONSTRUCTION.

STANDARD BRICK PAVER

NOT TO SCALE

WEARING COURSE (NHDOT 9.5mm SUPERPAVE) -2.5" -3/4" HOT BIT PAVEMENT ///////// BINDER COURSE (NHDOT 19mm SUPERPAVE) 6" NHDOT ITEM 304.3 CRUSHED GRAVEL 95% MIN. COMPACTION INCLUDING RECLAIMED MATERIAL -12" - NHDOT ITEM 304.2 BANK RUN GRAVEL (MIN.) 95% MIN. COMPACTION 95% COMPACTED SUBGRADE OR ROCK FILL

TYPICAL BITUMINOUS PAVEMENT

635 SAGAMORE DEVELOPMENT LLC

NOT TO SCALE

DETAIL SHEET Plan Name: LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH Project:

Owner of Record;3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

DRAWING No. SHEET 15 OF 21 JBE PROJECT NO. 18134.1

Designed and Produced in NH 85 Portsmouth Ave. Civil Engineering Services 603-772-4746 KDR PO Box 219 E-MAIL: JBE@JONESANDBEACH.COM

3/18/24 **ISSUED FOR REVIEW** DULLAN THINMAN **REVISION** REV. DATE

GRAVEL SUBBASE

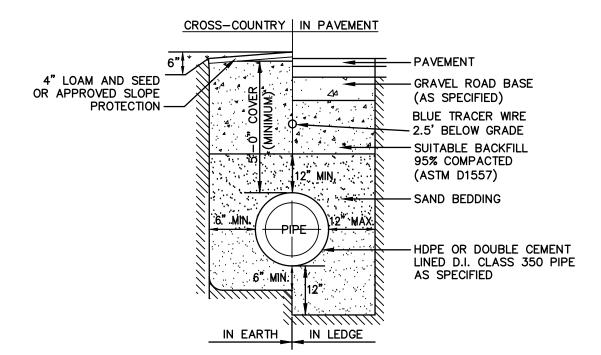
NOTES:

BY Stratham, NH 03885

1. EDGING TO BE PLACED PRIOR TO PLACING TOP SURFACE COURSE.

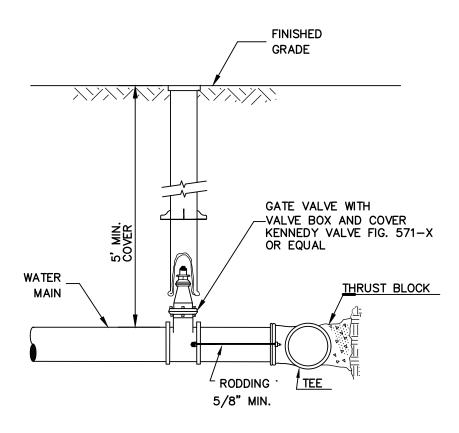
3. SALVAGE GRANITE CURBS ON-SITE AND RESET TO THE EXTENT POSSIBLE.

2. JOINTS BETWEEN STONES SHALL BE MORTARED.



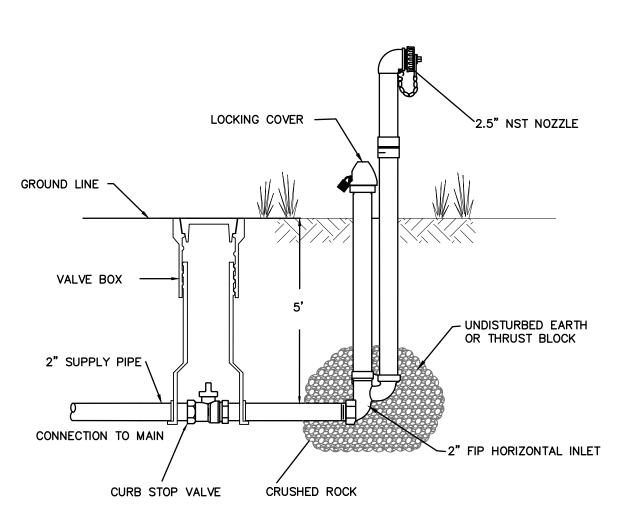
WATER SYSTEM TRENCH

NOT TO SCALE



BURIED GATE VALVE DETAIL

NOT TO SCALE

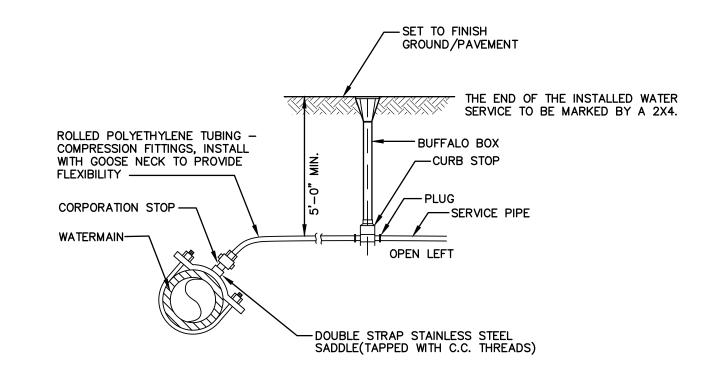


POST HYDRANTS SHALL BE NON-FREEZING, SELF DRAINING TYPE WITH A 5' BURY. THESE HYDRANTS WILL BE FURNISHED WITH A 2" FIP HORIZONTAL INLET, A NON-TURNING OPERATING ROD, AND SHALL OPEN LEFT. BRONZE OPERATING MECHANISM AND ALUMINUM PLUNGER. DESIGN, AND BE SERVICABLE FROM ABOVE GRADE WITH NO DIGGING. THE OUTLET SHALL ALSO BE BRONZE AND BE 2-1/2" NST. HYDRANTS SHALL BE LOCKABLE TO PREVENT UNAUTHORIZED USE AS MANUFACTURED BY KUPFERLE FOUNDRY CO., ST. LOUIS, MO, OR APPROVED EQUAL.

INLET PRESSURE (PSI)	FLOW RATE (GPM)		
75	675		
100	742		
125	800		
150	856		
•			

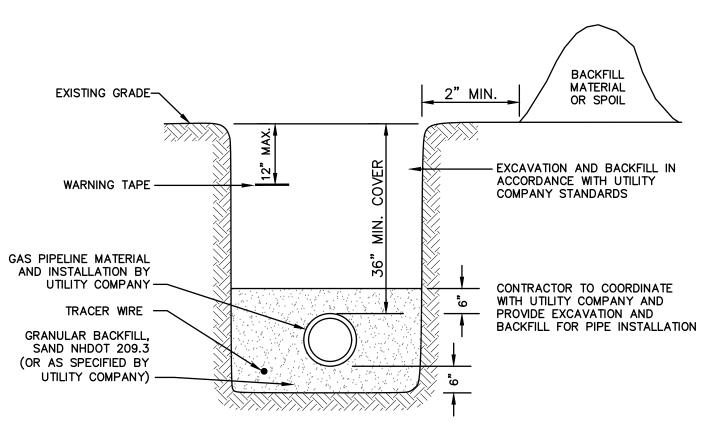
BLOW-OFF HYDRANT DETAIL

NOT TO SCALE



WATER SERVICE CONNECTION-POLYETHYLENE

NOT TO SCALE



GAS TRENCH

NOT TO SCALE

Stratham, NH 03885

SUBMITTALS SHOP DRAWINGS, INCLUDING SPECIFICATIONS, CATALOG CUTS, DATA SHEETS, DRAWINGS AND OTHER DESCRIPTIVE MATERIAL SHALL BE SUPPLIED TO THE ENGINEER FOR REVIEW PRIOR TO INSTALLATION. A CERTIFICATE OF COMPLIANCE FROM THE MANUFACTURER INDICATING CONFORMANCE WITH THE SPECIFIED REQUIREMENTS FOR DUCTILE IRON PIPE SHALL BE SUBMITTED TO THE ENGINEER FOR REVIEW AND APPROVAL.

<u>DELIVERY, HANDLING, AND STORAGE</u>
ALL PIPE AND APPURTENANCES ARE SUBJECT TO INSPECTION BY THE ENGINEER AT THE POINT OF DELIVERY. MATERIAL FOUND TO BE DEFECTIVE DUE TO MANUFACTURE OR DAMAGE IN SHIPMENT SHALL BE REJECTED OR RECORDED ON THE BILL OF LADING AND REMOVED FROM THE JOB SITE. ALL MATERIALS, IF STORED, SHALL BE KEPT SAFE FROM ANY POTENTIAL DAMAGE.

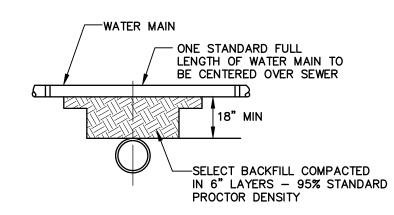
SAND BEDDING SAND BLANKET SHALL CONSIST OF CLEAN SAND THAT IS FREE FROM ORGANIC MATTER AND GRADED SO THAT 90-100% PASSES A 1/2" SIEVE AND NOT MORE THAN 15% WILL PASS A #200

BACKFILL SUITABLE MATERIAL FOR BACKFILL IN ROADS, ROAD SHOULDERS, AND WALKWAYS SHALL BE THE NATURAL MATERIAL REMOVED DURING THE COURSE OF TRENCH EXCAVATION, BUT SHALL EXCLUDE ANY DEBRIS, PAVEMENT, ORGANIC MATTER, LOAM, WET OR SOFT MUCK, PEAT, OR CLAY. BACKFILL MATERIAL SHALL BE PLACED IN 6" LIFTS AND SHALL BE COMPACTED TO 95% OF ASTM-1557 AT OPTIMUM MOISTURE CONTENT.

DUCTILE IRON PIPE-CLASS 52 JOINTS SHALL BE OF "PUSH-ON" TYPE UNLESS OTHERWISE SPECIFIED. PIPE SHALL HAVE A DOUBLE CEMENT LINING WITH SEAL COATING INSIDE AND BITUMINOUS COATING OUTSIDE THAT MEETS OR EXCEEDS THE REQUIREMENTS OF AWWA/ANSI C104/A21.4. GASKETS FOR DUCTILE IRON PIPE SHALL BE OIL-RESISTANT RUBBER WHICH MEETS OR EXCEEDS THE REQUIREMENTS OF AWWA/ANSI C111/A21.11. PIPE SHALL BE FURNISHED COMPLETE WITH ALL GASKETS AND

WATERMAIN TESTING
ALL WATER MAINS WILL BE CLEANED AND HYDROSTATICALLY TESTED AT A MINIMUM PRESSURE OF 150psi AT THE HIGHEST POINT ALONG THE TEST SECTION. THE HYDROSTATIC TEST SHALL BE CONDUCTED FOR A MINIMUM OF TWO HOURS DURING WHICH TEST PRESSURE SHALL NOT VARY MORE THAN ±5psi. LEAKAGE CALCULATIONS WILL BE COMPLETED IN ACCORDANCE WITH THE REQUIREMENTS OF THE AMERICAN WATER WORKS ASSOCIATION. DISINFECTION WILL BE REQUIRED PER THE SPECIFICATIONS OF ANSI/AWWA C651. WITHIN 24 HOURS OF DISINFECTION, ALL NEWLY INSTALLED MAINS SHALL BE FLUSHED.

- 1. CONTRACTOR TO INSTALL 2" RIGID INSULATION BETWEEN THE PROPOSED WATERMAIN(S) AND DRAINAGE LINES IN ALL AREAS WHERE SEPARATION IS TO BE IN 4' OR LESS.
- 2. ALL PIPE, FITTINGS, HYDRANTS, AND WORKMANSHIP SHALL BE INSPECTED AND APPROVED BY THE MUNICIPAL WATER/SEWER DEPARTMENT.
- 4. ALL CONSTRUCTION AND TESTING SHALL COMPLY WITH THE REGULATIONS OF THE MUNICIPAL, THE STATE, AND THE AMERICAN WATER WORKS ASSOCIATION.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING AND DETERMINING THE LOCATION, SIZE, AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO THE START OF CONSTRUCTION. THE ENGINEER SHALL BE NOTIFIED IN WRITING OF ANY UNFORESEEN UTILITY FOUND INTERFERING WITH THE PROPOSED CONSTRUCTION. ANY APPROPRIATE REMEDIAL ACTION MUST BE AGREED TO BY THE ENGINEER PRIOR TO THE COMMENCEMENT OF WORK. THE CONTRACTOR SHALL BE RESPONSIBLE FOR CONTACTING "DIG-SAFE" AT 1-888-344-7233 AT LEAST 72 HOURS BEFORE DIGGING.
- 6. ALL CONCRETE SHALL HAVE A COMPRESSIVE STRENGTH OF NOT LESS THAN 2000 PSI AFTER 28 DAYS.
- 7. CONTRACTOR TO INSTALL CORPORATION FITTINGS AT EACH CONNECTION TO THE WATER MAIN FOR TESTING PURPOSES. CORPORATIONS SHALL BE REMOVED AND PLUGGED AT THE COMPLETION OF TESTING.
- 8. CONTRACTOR TO OBSERVE ALL APPROPRIATE BEST MANAGEMENT PRACTICES.
- 9. ALL GATE VALVES TO BE MUELLER RESILIENT WEDGE (OPEN RIGHT).
- 10. ALL TEES TO BE ANCHOR TEES.
- 11. THE TERMINAL 36' OF ALL "DEAD END" WATERMAINS AND ALL BENDS AND TEES ARE TO BE FITTED WITH MECHANICAL RESTRAINING JOINTS, "MEGALUG" OR APPROVED EQUAL AND THRUST BLOCKS.
- 12. INSTALL THRUST BLOCKS AT ALL TEES, BENDS, AND FITTINGS.

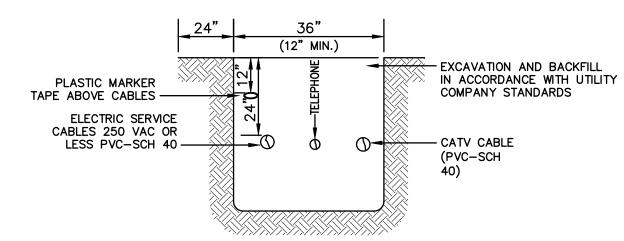


SEPARATION NOTES:

1. WATER MAINS SHALL BE LAID AT LEAST 10 FEET HORIZONTALLY FROM ANY EXISTING OR PROPOSED SEWERS. THE DISTANCE SHALL BE MEASURED EDGE TO EDGE. 2. WATER MAINS CROSSING SEWERS SHALL BE LAID TO PROVIDE A MINIMUM VERTICAL DISTANCE OF 18 INCHES BETWEEN PIPES. SEWER PIPE JOINTS SHALL BE LOCATED AT LEAST 6 FEET HORIZONTALLLY FROM THE WATER MAIN.

TYPICAL WATER / SEWER SEPARATION

NOT TO SCALE



NOTE: ALL UTILITIES SHALL BE REVIEWED AND APPROVED BY APPROPRIATE UTILITY COMPANY.

UTILITY TRENCH

NOT TO SCALE

DETAIL SHEET

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH

635 SAGAMORE DEVELOPMENT LLC

JBE PROJECT NO. 18134.1

DRAWING No.

WATER LINE TECHNICAL SPECIFICATIONS

Design: DJM Draft: KDR Checked: JAC | Scale: AS NOTED | Project No.: 18134.1 Drawing Name: 18134.1-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).

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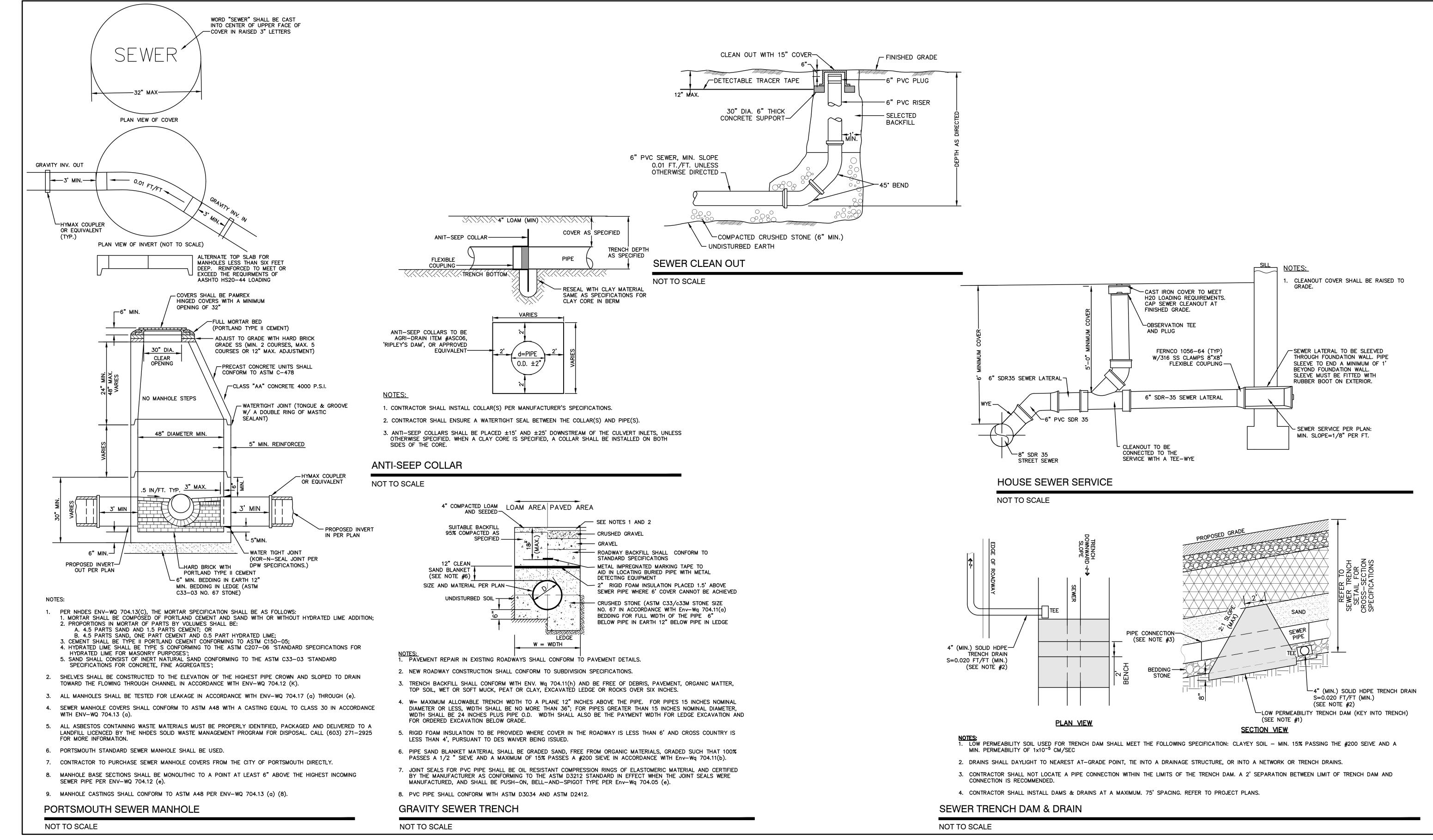


	4	10/22/24	REVISED PER ALTUS AND TAC COMMENTS	DJM		
	3	9/16/24	REVISED PER ALTUS AND TAC COMMENTS	DJM		
	2	8/14/24	REVISED PER CITY REVIEW ENGINEER COMMENTS			
	1	4/19/24	REVISED PER TAC COMMENTS	DJM		
	0	3/18/24	ISSUED FOR REVIEW	KDR		
	REV.	DATE	REVISION	BY		

Designed and Produced in NH Jones & Beach Engineers, Inc. 85 Portsmouth Ave. Civil Engineering Services 603-772-4746 PO Box 219

Plan Name:

Project:



Design: DJM Draft: KDR Date: 2/26/2024

Checked: JAC Scale: AS NOTED Project No.: 18134.1

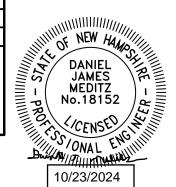
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B Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885

E-MAIL: JBE@JONESANDBEACH.COM

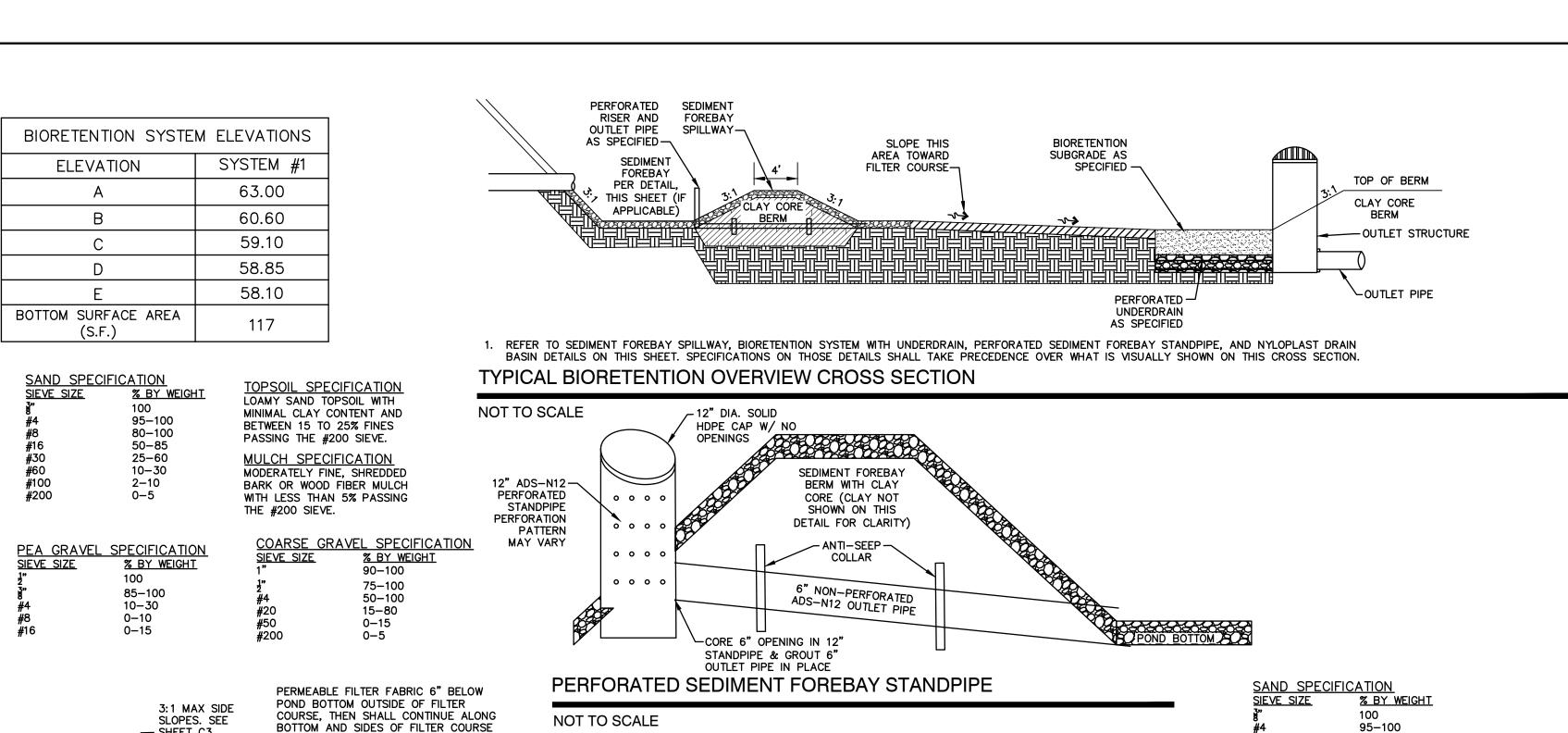
	Plan Name:	DETAIL SHEET
	Project:	LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH
Owner of Record:3612 L		635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

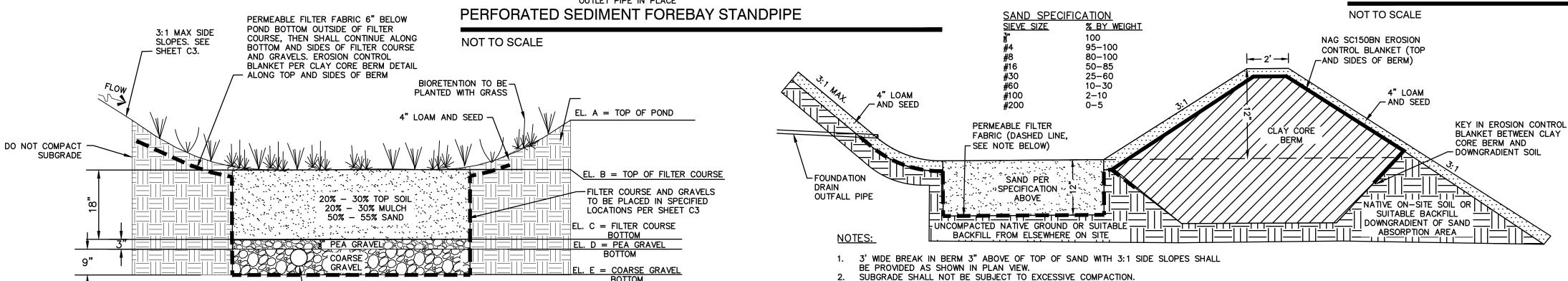
D3

SHEET 17 OF21

JBE PROJECT NO. 18134.1

DRAWING No.





<u>DESIGN CONSIDERATIONS</u>

DO NOT PLACE BIORETENTION SYSTEMS INTO SERVICE UNTIL THE BMP HAS BEEN SEEDED AND ITS CONTRIBUTING AREAS HAVE BEEN FULLY STABILIZED.

- DO NOT DISCHARGE SEDIMENT-LADEN WATERS FROM CONSTRUCTION ACTIVITIES (RUN-OFF, WATER FROM EXCAVATIONS) TO THE BIORETENTION AREA DURING ANY STAGE OF CONSTRUCTION.
- DO NOT TRAFFIC EXPOSED SOIL SURFACE WITH CONSTRUCTION EQUIPMENT. IF FEASIBLE, PERFORM EXCAVATIONS WITH EQUIPMENT OUTSIDE THE LIMITS OF THE INFILTRATION COMPONENTS OF THE SYSTEM.
- REMOVE LEDGE TO AT LEAST TWO FEET BELOW BOTTOM OF COARSE GRAVEL LAYER IF ENCOUNTERED.
- IN ADDITION TO DESIGN CRITERIA LISTED HERE, REFER TO GUIDELINES LISTED IN UNIVERSITY OF NEW HAMPSHIRE (UNH) STORMWATER CENTER BIORETENTION SOIL SPECIFICATION.
- THE EXISTING NATIVE SUBGRADE MATERIAL BENEATH THE FILTER COURSE AND GRAVEL LAYERS SHALL NOT BE COMPACTED OR SUBJECT TO EXCESSIVE CONSTRUCTION EQUIPMENT TRAFFIC PRIOR TO STONE PLACEMENT. IF SOIL MEDIA OR SUBGRADE IS OVER COMPACTED, DISTURBED, OR CONTAMINATED BY FOREIGN OR DELETERIOUS MATERIALS OR LIQUIDS, REMOVE THE SOIL MEDIA AND CONTAMINATION; RESTORE THE SUBGRADE AS DIRECTED BY ENGINEER AND REPLACE CONTAMINATED

MAINTENANCE REQUIREMENTS:

SOIL MEDIA WITH NEW SOIL MEDIA.

- SYSTEMS SHALL BE INSPECTED AT LEAST TWICE ANNUALLY, AND FOLLOWING ANY RAINFALL EVENT EXCEEDING 2.5 INCHES IN A 24 HOUR PERIOD, WITH MAINTENANCE OR REHABILITATION CONDUCTED AS
- PRETREATMENT MEASURES SHALL BE INSPECTED AT LEAST TWICE ANNUALLY, AND CLEANED OF ACCUMULATED SEDIMENT AS WARRANTED BY INSPECTION, BUT NO LESS THAN ONCE ANNUALLY.
- 3. TRASH AND DEBRIS SHALL BE REMOVED AT EACH INSPECTION.
- AT LEAST ONCE ANNUALLY, SYSTEM SHALL BE INSPECTED FOR DRAWDOWN TIME. IF BIORETENTION SYSTEM DOES NOT DRAIN WITHIN 72 HOURS FOLLOWING A RAINFALL EVENT, THEN A QUALIFIED PROFESSIONAL SHALL ASSESS THE CONDITION OF THE FACILITY TO DETERMINE MEASURES REQUIRED TO RESTORE FILTRATION FUNCTION, INCLUDING BUT NOT LIMITED TO REMOVAL OF ACCUMULATED SEDIMENTS OR RECONSTRUCTION OF THE FILTER MEDIA.
- VEGETATION SHALL BE INSPECTED AT LEAST ANNUALLY, AND MAINTAINED IN HEALTHY CONDITION, INCLUDING PRUNING, REMOVAL AND REPLACEMENT OF DEAD OR DISEASED VEGETATION, AND REMOVAL OF INVASIVE
- COMPACTION AND MATERIALS TESTING SERVICES SHALL BE PERFORMED BY AN INDEPENDENT GEOTECHNICAL ENGINEER RETAINED BY THE OWNER. BIORETENTION SYSTEM WITH UNDERDRAIN

NOT TO SCALE

RIP RAP -D50 = 3PROPEX GEOTEX WS-200ST GEOTEXTILE FABRIC OR APPROVED EQUAL AL HA HA HA HA H SPILLWAY SECTION $D50 = 3" \neg$ PERFORATED WATER FLOW RISER AND OUTLET PIPE)404040404040 AS SPECIFIED SEDIMENT **FOREBAY** CLAY CORE BERM POND AREA PROPEX GEOTEX WS-200S GEOTEXTILE FABRIC EXTEND RIP RAP 5' OR APPROVED EQUAL MIN. INTO POND AREA SPILLWAY PROFILE

GRADE OF SEDIMENT FOREBAY SPILLWAY IS EQUAL TO GRADE OF BERM OF POND IN THIS CASE.

NOT TO SCALE

BERM SHALL BE CONSTRUCTED WITH A CLAY CORE TO BE KEYED INTO ORIGINAL GRADE, AS WELL AS A FINE GEOTEXTILE, TO AVOID WATER SEEPAGE AND SOIL PIPING THROUGH THE EARTHEN DIVIDER. THE ENTIRE EMBANKMENT AREA OF THE POND AREAS SHALL BE EXCAVATED TO 2' BELOW ORIGINAL GRADE, STRIPPED OF ALL ORGANIC MATERIALS, COMPACTED TO AT LEAST 92% OF ASTM D-1557, AND SCARIFIED PRIOR TO THE PLACEMENT OF THE EMBANKMENT MATERIAL. PLACEMENT AND COMPACTION SHOULD OCCUR AT A MOISTURE CONTENT OF OPTIMUM PLUS OR MINUS 3%, AND NO FROZEN OR ORGANIC MATERIAL SHOULD BE PLACED FOR ANY REASON. CLAY CORE MATERIAL SHALL BE CLEAN SILTY-CLAY BORROW FREE OF ROOTS, ORGANIC MATTER, AND OTHER DELETERIOUS SUBSTANCES, AND SHALL CONTAIN NO ROCKS OR LUMPS OVER THREE INCHES (3") IN DIAMETER. THIS MATERIAL SHALL BE INSTALLED IN 6" LIFTS COMPACTED TO 92% OF ASTM D-1557, AND SHALL MEET THE FOLLOWING SPECIFICATIONS: 6" PASSING 100%, #4 SIEVE 95-100%, #40 SIEVE 60-90%, #100 SIEVE 40-60%, #200 SIEVE 25-45% (OF THE FRACTION PASSING THE #4 SIEVE). THE

PERMEABLE FILTER FABRIC SHALL BE PLACED BENEATH LOAM AND SEED ALONG SIDE SLOPES EXCEPT FOR BERM, AND ALONG BOTTOM AND SIDES OF SAND IN ABSORPTION

AREA. NAG SC150BN EROSION CONTROL BLANKET ALONG CLAY CORE BERM.

SAND ABSORPTION AREA

NOT TO SCALE

5. REMOVE LEDGE TO AT LEAST 2' OUTSIDE AND EBLOW LIMITS OF CLAY CORE. **CLAY CORE BERM**

SEDIMENT FOREBAY SPILLWAY

NOT TO SCALE

4" LOAM AND SEED ON SIDE

SEDIMENT FOREBAY SPILLWAY.

SLOPES AND TOP OF BERM RIP RAP COVER ONLY ON

BERM AROUND BACK OF

POND SHALL BE LOAMED.

GEOTEXTILE FABRIC (AMOCO 6" SAND FILTER TO BE PLACED #2006 OR EQUIVALENT) TO BE BELOW THE GEOTEXTILE FOR THE PLACED BETWEEN RIP RAP AND FULL EXTENT OF THE APRON (TYP.) SOIL (TYP.)-<u>SECTION A—A</u> SECTION A-A

- 8" - 30" DOME GRATES SHALL BE DUCTILE IRON PER ASTM A536

OF A PVC BODY TOP. SEE DRAWING NO. 7001-110-045.

4 - DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO

RESTRICTIONS. SEE DRAWING NO. 7001-110-065.

N-12 HP, & PVC SEWER (4" - 24").

RIM ELAVTION OF STRUCTURE

(5) ADAPTER ANGLES VARIABLE

0° - 360° ACCORDING TO PLANS

4" MIN ON 8"-24"

6" MIN ON 30"

REFERS TO THIS POINT

8" - 30" DOME GRATES HAVE NO LOAD RATING.

- DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN

8" & 10" DOME GRATES FIT ONTO THE DRAIN BASINS WITH THE USE

DETAILS. RISERS ARE NEEDED FOR BASINS OVER 84" DUE TO SHIPPING

ASTM D3212 FOR CORRUGATED HDPE (ADS N-12/HANCOR DUAL WALL),

MINIMUM ANGLE BETWEEN ADAPTERS SEE DRAWING NO. 7001-110-012.

(3) VARIABLE SUMP DEPTH

ACCORDING TO PLANS

(6" MIN. ON 8"-24", 10" MIN. ON 30"

BASED ON MANUFACTURING REQ.)

PIPE OUTLET TO

WELL-DEFINED CHANNEL

THE BACKFILL MATERIAL SHALL BE CRUSHED STONE

REQUIREMENTS OF CLASS I, CLASS II, OR CLASS III

INTLETS SHALL BE PLACED & COMPACTED UNIFORMLY

OR OTHER GRANULAR MATERIAL MEETING THE

BEDDING & BACKFILL FOR SURFACE DRAINAGE

MATERIAL AS DEFINED IN ASTM D2321.

IN ACCORDANCE WITH ASTM D2321.

- ADAPTERS CAN BE MOUNTED ON ANY ANGLE 0° TO 360°. TO DETERMINE

GRADE 70-50-05.

(1, 2) INTEGRATED DUCTILE IRON

MINIMUM PIPE BURIAL

DEPTH PER PIPE

MANUFACTURER

RECOMMENDATION

(MIN. MANUFACTURING

REQ. SAME AS MIN. SUMP)

WATERTIGHT JOINT -

24" DIA. NYLOPLAST DRAIN BASIN (YARD DRAIN & POND OUTLET STRUCTURE SPECIFICATION)

(CORRUGATED HDPE SHOWN)

(4) VARIOUS TYPES OF INLET & OUTLET ADAPTERS -

AVAILABLE: 4" - 30" FOR CORRUGATED HDPE

(ADS N-12/HANCOR DUAL WALL, ADS/HANCOR

(EX: SDR 35), PVC DWV (EX: SCH 40), PVC

C900/C905, CORRUGATED & RIBBED PVC

SINGLE WALL), N-12 HP, PVC SEWER

(3) VARIABLE INVERT HEIGHTS

AVAILABLE (ACCORDING TO

PLANS/TAKE OFF)

AS SHOWN

CLAY COMPONENT SHALL HAVE "A PLASTICITY INDEX OF AT LEAST 8 AND A HYDRAULIC CONDUCTIVITY

COMPACTION AND MATERIALS TESTING SERVICES SHALL BE PERFORMED BY AN INDEPENDENT

TOP OF BERM

CLAY CORE,

NOTE #3

-LIMIT OF FOUNDATION

EXCAVATION

SPECIFICATION PER

SLOPES TO BE STABILIZED WITH

NAG S150BN EROSION CONTROL

BLANKET OR

APPROVED EQUAL

GRATE TO MATCH BASIN O.D.

TABLE 7-24RECOMMENDED	RIP RAP GR	ADA	TION RANGES
THICKNESS OF RIP RAP = 0	.75 FEET		
d50 SIZE= 0.25	FEET	3	INCHES
% OF WEIGHT SMALLER THAN THE GIVEN d50 SIZE	SIZE OF FROM	STC	NE (INCHES) TO
100%	5		6
85%	4		5
50%	3		5
15%	1		2

- 1. THE SUBGRADE FOR THE GEOTEXTILE FABRIC AND RIP RAP SHALL BE PREPARED TO THE LINES AND GRADES SHOWN ON THE PLANS.
- 2. THE RIP RAP SHALL CONFORM TO THE SPECIFIED GRADATION.

PIPE OUTLET TO FLAT AREA

- 3. GEOTEXTILE FABRICS SHALL BE PROTECTED FROM PUNCTURE OR TEARING DURING THE PLACEMENT OF THE ROCK RIP. DAMAGED AREAS IN THE FABRIC SHALL BE REPAIRED BY PLACING A PIECE OF FABRIC OVER THE DAMAGED AREA OR BY COMPLETE REPLACEMENT OF THE FABRIC. ALL OVERLAPS REQUIRED FOR REPAIRS OR JOINING TWO PIECES OF FABRIC SHALL BE A MINIMUM OF 12 INCHES.
- 4. STONE FOR THE RIP RAP MAY BE PLACED BY EQUIPMENT AND SHALL BE CONSTRUCTED TO THE FULL LAYER THICKNESS IN ONE OPERATION AND IN SUCH A MANNER AS TO PREVENT SEGREGATION OF THE
- 5. OUTLETS TO A DEFINED CHANNEL SHALL HAVE 2:1 OR FLATTER SIDE SLOPES AND SHOULD BEGIN AT THE TOP OF THE CULVERT AND TAPER DOWN TO THE CHANNEL BOTTOM THROUGH THE LENGTH OF THE
- 6. <u>MAINTENANCE</u>; THE OUTLET PROTECTION SHOULD BE CHECKED AT LEAST ANNUALLY AND AFTER EVERY MAJOR STORM. IF THE RIP RAP HAS BEEN DISPLACED, UNDERMINED OR DAMAGED, IT SHOULD BE REPAIRED IMMEDIATELY. THE CHANNEL IMMEDIATELY BELOW THE OUTLET SHOULD BE CHECKED TO SEE THAT EROSION IS NOT OCCURRING. THE DOWNSTREAM CHANNEL SHOULD BE KEPT CLEAR OF OBSTRUCTIONS SUCH AS FALLEN TREES, DEBRIS, AND SEDIMENT THAT COULD CHANGE FLOW PATTERNS AND/OR TAILWATER DEPTHS ON THE PIPES. REPAIRS MUST BE CARRIED OUT IMMEDIATELY TO AVOID ADDITIONAL DAMAGE TO OUTLET PROTECTION.

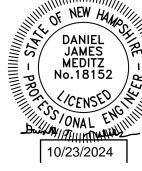
RIP RAP OUTLET PROTECTION APRON

NOT TO SCALE

Design: DJM | Draft: KDR Date: 2/26/2024 Checked: JAC | Scale: AS NOTED | Project No.: 18134.1 Drawing Name: 18134.1-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).

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─6" PERFORATED

HDPE UNDERDRAIN

(INVERT PER PLAN)

4	10/22/24	REVISED PER ALTUS AND TAC COMMENTS	DJM
3	9/16/24	REVISED PER ALTUS AND TAC COMMENTS	DJM
2	8/14/24	REVISED PER CITY REVIEW ENGINEER COMMENTS	DJM
1	4/19/24	REVISED PER TAC COMMENTS	DJM
0	3/18/24	ISSUED FOR REVIEW	KDR
REV.	DATE	REVISION	BY

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OF 10 TO THE -6 CM/SEC.

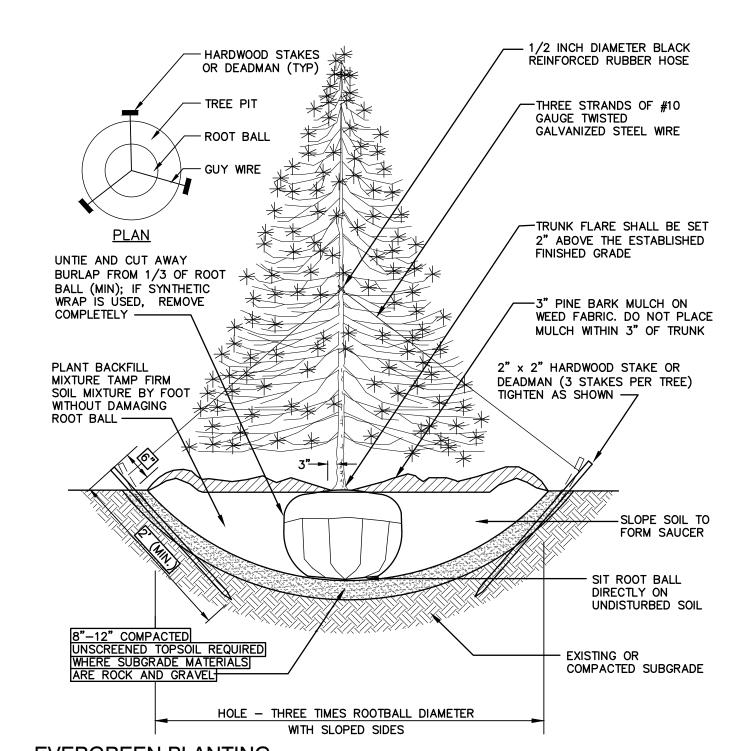
GEOTECHNICAL ENGINEER RETAINED BY THE OWNER.

Plan Name:	DETAIL SHEET
Project:	LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH
Owner of December	635 SAGAMORE DEVELOPMENT LLC

Owner of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

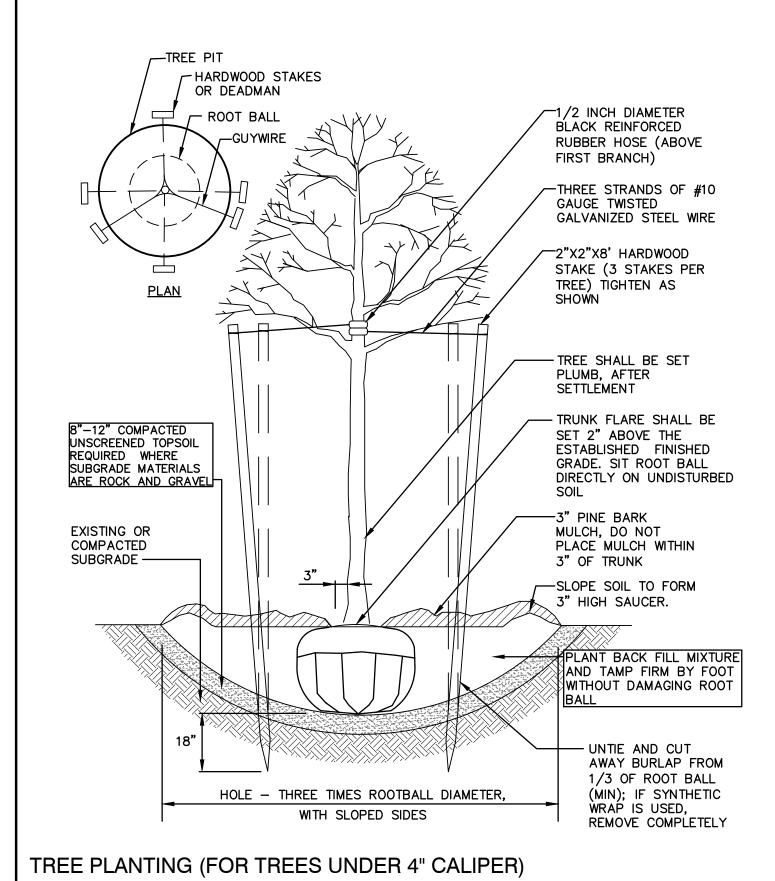
SHEET 18 OF 21 JBE PROJECT NO. 18134.1

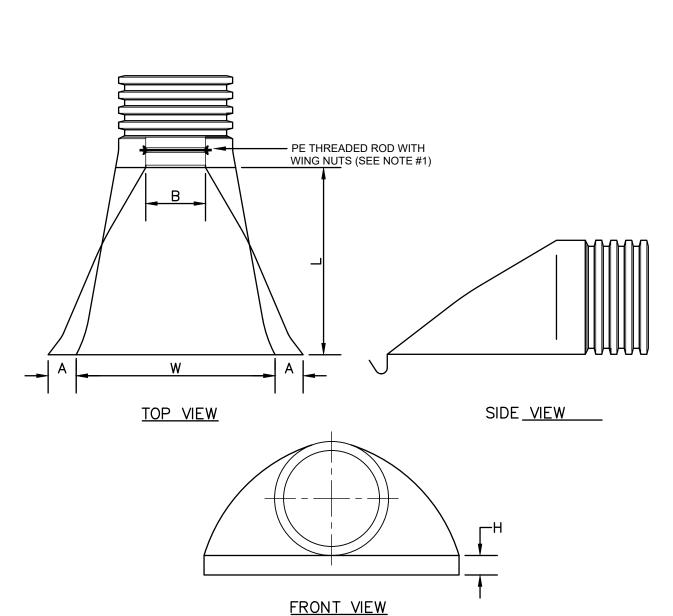
DRAWING No.



EVERGREEN PLANTING

NOT TO SCALE



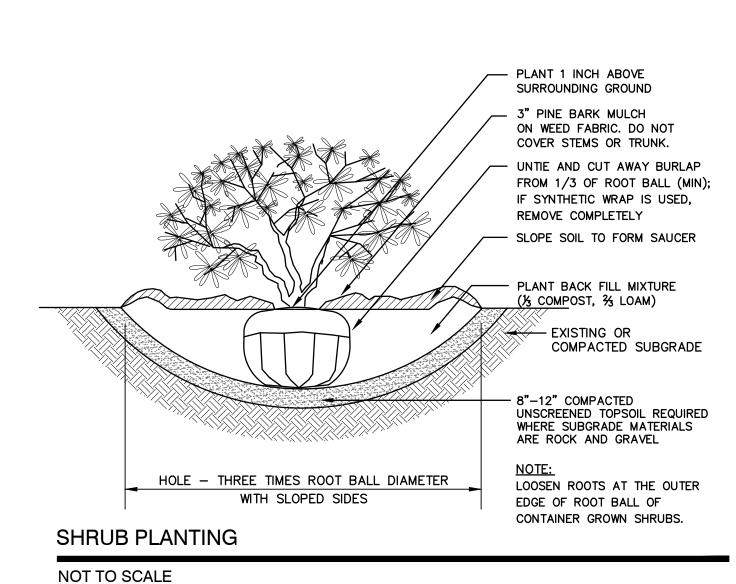


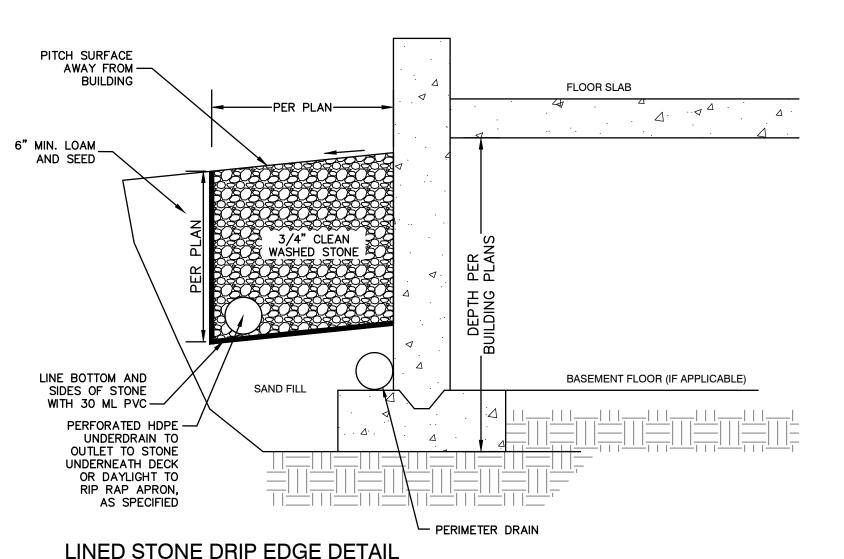
PART NO.	PIPE SIZE	Α	B (MAX)	Н	L	w
1210-NP	12"	6.5"	10"	6.5"	25"	29"
1510-NP	15"	6.5"	10"	6.5"	25"	29"
1810-NP	18"	7.5"	15"	6.5"	32"	35"
2410-NP	24"	7.5"	18"	6.5"	36"	45"
3010-NP	30"	10.5"	N/A	7.0"	53"	68"
3610-NP	36"	10.5"	N/A	7.0"	53"	68"

- 1. PE THREADED ROD WITH WING NUTS PROVIDED FOR END SECTIONS 12"-24". 30" AND 36" END SECTIONS TO BE WELDED PER MANUFACTURER'S RECOMMENDATIONS.
- 2. ALL DIMENSIONS ARE NOMINAL.

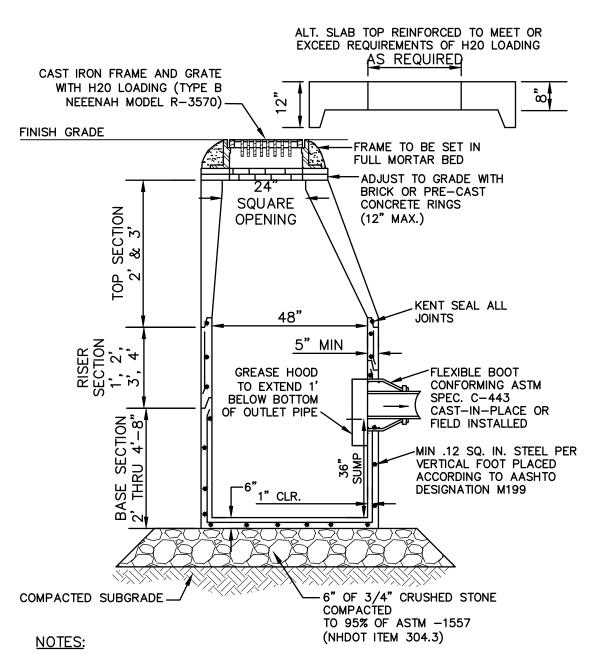
ADS N-12 FLARED END SECTION

NOT TO SCALE



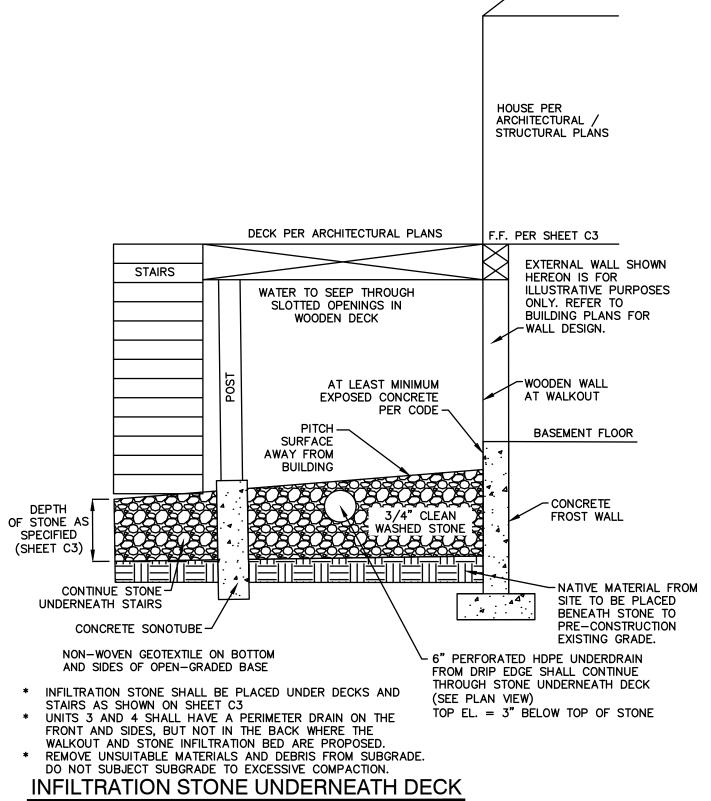


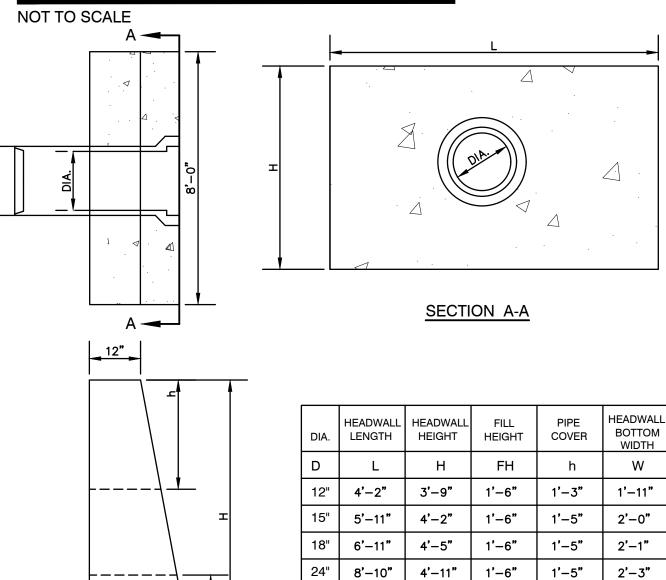
NOT TO SCALE



- 1. BASE SECTION SHALL BE MONOLITHIC WITH 48" INSIDE DIAMETER.
- 2. ALL SECTIONS SHALL BE DESIGNED FOR H20 LOADING.
- 3. CONCRETE SHALL BE COMPRESSIVE STRENGTH 4000 PSI, TYPE II CEMENT.
- 4. FRAMES AND GRATES SHALL BE HEAVY DUTY AND DESIGNED FOR H20 LOADING
- 5. PROVIDE "V" KNOCKOUTS FOR PIPES WITH 2" MAX. CLEARANCE TO OUTSIDE OF PIPE. MORTAR ALL PIPE CONNECTIONS SO AS TO BE WATERTIGHT.
- 6. JOINT SEALANT BETWEEN PRECAST SECTIONS SHALL BE BUTYL RUBBER.
- 7. STANDARD CATCH BASIN FRAME AND GRATE(S) SHALL BE SET IN FULL MORTAR BED. ADJUST TO GRADE WITH CLAY BRICK AND MORTAR (2 BRICK COURSES TYPICALLY, 5 BRICK COURSES MAXIMUM, BUT NO MORE THAN 12"), OR PRECAST CONCRETE 'DONUTS'.
- 8. CATCH BASINS SHALL HAVE A 36" MINIMUM SUMP AS SHOWN. CATCH BASIN

NOT TO SCALE





LONGITUDINAL SECTION

- NOTES: 1. ALL DIMENSIONS GIVEN IN FEET & INCHES.
- PROVIDE BELL END AT INLET HEADWALL, AND SPIGOT END AT OUTLET END HEADWALL. . CONCRETE: 5,000 PSI MINIMUM AFTER 28 DAYS. CEMENT TO BE TYPE III PER ASTM
- C-150. REINFORCING TO MEET OR EXCEED ASTM A-615 GRADE 60 DEFORMED BARS.
- 4. 1" THREADED INSERTS PROVED FOR FINAL ATTACHMENT IN FIELD BY OTHERS.

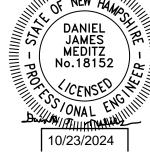
PRECAST CONCRETE HEADWALL

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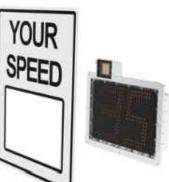
85 Portsmouth Ave. Civil Engineering Services 603-772-4746 PO Box 219 E-MAIL: JBE@JONESANDBEACH.COM Stratham, NH 03885

Plan Name:	DETAIL SHEET
Project:	LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH
Owner of Record;	635 SAGAMORE DEVELOPMENT LLC 612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

DRAWING No. **SHEET 19 OF 21** JBE PROJECT NO. 18134.1



TC-600 RADAR SPEED SIGN









- Speed Display Numbers: 13" tall speed display numbers; capable of showcasing 2 or 3 digits, with readability up to 600 feet
- Ideal Speed Range: Ideal for roads with traffic speeds ranging from 5 to 60 mph
- LED Configuration: Super bright amber LEDs in full matrix design; Life up to 100,000 hours
- Enhanced Visibility Design: Laser cut flat black mask enhances visibility of LED display when illuminated; Ensures completely dark display when LEDs are off
- Adjustable Display Brightness: Display brightness fully automatic or user adjustable

SPEED VIOLATOR ALERTS

- Standard Alerts: SPEED with 3 flash rate options; Enhanced font; SLOW DOWN; TOO FAST
- Alert Options: Display speed and word message alerts alternately or individually based on speed settings
- Speed Display Flash Rates: MUTCD flash (approx. 55-60 fpm); slow flash (approx. 90 fpm); fast flash (approx. 140 fpm)
- (not available with cellular signs)

YOUR SPEED FACEPLATE

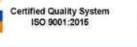
- Dimensions: 28"W x 33"H with 4" high lettering; Optional oversized 30"W x 36"H YOUR SPEED facept
- Available in white, yellow, fluorescent yellow/green, and safety orange

SOLAR POWER MODEL

- Operation: Operates 24/7 with solar power supply Power Supply: Two 12-volt,18 amp/hour AGM batteries (UL recognized); Provides up to 14 days of back-up
- operation on fully charged batteries Power Consumption: < 2.0 amps (24w) at maximum display
- intensity; Idle mode: < 1/2 watt
- Circuit Breaker: Multi-circuit; 3 x 10 amp fuses Battery Status Monitoring: Check battery charge levels and
- solar amperage via Wi-Fi or cellular Low battery cut-off feature provides intelligent battery management, optimizing the performance and longevity of
- the battery Charger and battery characteristics matched to operate
- within the sign's operating temperature range
- Solar Panel Output: 50 watt standard
- Solar Charger: Fully integrated charge controller that continuously monitors and logs data regarding solar output and battery charge status

- All power inputs are fused and reverse polarity protected
- All circuit boards are conformally coated for extra protection
- Automatic reset and watch-dog circuitry ensure the sign returns to normal operation without the need for user intervention

nfo@radarsign.com







AC POWER MODEL



Operation: Operates 24/7 with AC power supply

Power Consumption: < 2.0 amps (24w) at maximum display

Power Supply: Hard wire to 100 VAC-240 VAC

Circuit Breaker: Multi-circuit, 10 amp fuse

intensity; Idle mode: < 1/2 watt



- Type: K Band, single direction Doppler radar; FCC part 15 compliant; No license required
- Sensor Range: Detects vehicles up to 1200 feet
- Beam Width: 12 degrees, +/- 2 degrees
- Operating Frequency: 24.125 GHz, +/- 50 MHz
- Accuracy: +/- 1.0 mph Speed Detection Range: 5-127 mph; 8-198 kph
- RADAR SPEED SIGN HOUSING • Industrial Design: Single-piece cast aluminum housing; Seamless construction with no welding; Provides maximum protection from the
- elements and vandalism Thickness: Constructed from 0.1875" thick heavy-duty aluminum
- Compliance Standards: IP65 compliant; NEMA 4 level compliant
- Humidity Maximum: 100%; Non-sealed and ventilated
- Provides maximum protection from the elements and vandalism Dimensions: 18.5"H x 26.25" W x 5.0"D
- Mounting Bracket: Stainless steel mounting hardware included for poles up to 4.5" OD

WEIGHT & OPERATING TEMPERATURE

- TC-600 Solar Power Model: Weight 67 lbs.
- TC-600 AC Power Model: Weight 42 lbs. Operating temperature: -40°F to +160°F

STANDARD FEATURES ON ALL RADARSIGN MODELS

BASHPLATE™ WITH INTEGRATED LED REFLECTOR CONES

- Heavy duty aluminum shield over LED display to protect components from abuse or vandalism
- Radarsign's proprietary directional beam technology includes custom reflectors positioned around each LED. This unique design magnifies the intensity of the light, ensuring the highest quality viewable display with minimal energy usage.

POLYCARBONATE DISPLAY COVER

- .25" thick protective sheet covers entire display area
- Abrasion, graffiti and shatter resistant; Provides UV protection

- Radar speed sign emits it's own Wi-Fi signal, eliminating the need for an internet connection. Manage sign with smart phone, tablet, or laptop; Allows for quick, easy sign operation and data download from most web enabled devices.
- Connection range up to 300 feet from sign
- WPA2 encrypted security; Unique password protected
- OTA Software Updates (over-the-air): Allow the wireless delivery of software updates and upgrades directly to the radar sign
- Speed is 10x faster and has 10x the range of Bluetooth

STANDARD PROGRAMMING

- Setup Functions: Easy-to-navigate digital menu; No mechanical switches to operate
- Daily Timers: Allow up to 5 on/off timer settings per day, including 4 customizable timers in addition to the standard setting. Settings allow for lower speed limits for school zone times.
- Stealth Mode: This feature allows the display to be turned off while still allowing continuous traffic data collection. This ensures data monitoring even when the display is not active.
- Possum Switch™: In the event of a forceful attack, the sign can simulate inactivity or "play dead" for a duration of 30 minutes. This
- feature helps protect the sign from malicious tampering or damage. Maximum Speed Cutoff: Designed to prevent the sign from displaying excessively high speeds, this feature curbs any attempts at speeding towards or "racing" the sign. Users have the option to choose between flashing dashes or an LED display cutoff.

WARRANTY: 2 years on parts and labor including batteries; Exceptions: Does not cover malicious abuse, theft, or damage due to unauthorized modification.

OPTIONAL DATA REPORTING, MANAGEMENT AND SCHEDULING FEATURES

STREETSMART TRAFFIC DATA COLLECTION & REPORTING SOFTWARE: This feature comes with a lifetime license for a one-time charge, eliminating recurring fees. It is licensed per sign and allows the download, reporting, organization, and analysis of speed and traffic data recorded by the radar speed sign. Users can generate 35 charts and graphs with Excel™ macro. The Traffic Data Storage Capacity allows data storage for up to 5 million vehicles, retaining data for 12 months in the sign before overwriting the oldest data first.

CLOUD SERVICE: The built-in cellular modern allows cloud accessibility from anywhere with an internet connection. It enables remote management of sign settings for your entire network of signs. Additionally, it uploads daily traffic statistics to the Radarsign Cloud server (requires the purchase of a Streetsmart data license). This feature also provides alerts in case of low battery or interrupted connection.

ADVANCED SCHEDULER: Date-driven program enables the pre-programming of multiple years and schedules for radar speed signs. This functionality is particularly beneficial for scheduling in school zones or areas where events occur regularly.



Pole and Base Options

Radarsign offers a round aluminum or decorative black fluted aluminum pole for use with our radar speed signs. Our selection of pole bases includes square or or gonal aluminum bases, or a black decorative base for a more architectural look. All Radarsign pole bases have reakaway design that meets FHWA crash test guidelines.







Pole Style	Round aluminum	Round aluminum	Decorative black fluted
Pole OD (outside diameter)	4.5"	4.5"	4"
Pole Length	Choice of 12', 13', 14', 15', or 16'	Choice of 12', 13', 14', 15', or 16'	12'
Base Style	Square	Octagonal	Decorative black
Base Anchor Meth	Cement pad with concrete form kit or anchor bolt cage kit	Cement pad with concrete form kit or anchor bolt cage kit	2.5" x 2.5" sleeve in cemen

Installation Form Kits

Concrete Form Kit

The concrete form kit, customized for the aluminum pole bases with the round aluminum poles, makes base and pole installation easy. The kit includes a prefabricated concrete pole base form, four anchor bolts, a rebar base cap, and a rebar sample. (Not compatible with decorative black pole).





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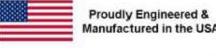
Anchor Bolt Cage Kit

The anchor bolt cage kit is a pre-fabricated form guide for pole footing installation. The kit includes an anchor bolt cage with hardware and (4) 18" x 3/4" J bolts.



Certified Quality System





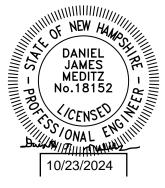
Manufactured in the USA 678-965-4814

1 of 1

Pole and Base Options MK0003 v22.01

Design: DJM Draft: KDR Date: 2/26/2024 Checked: JAC | Scale: AS NOTED | Project No.: 18134.1 Drawing Name: 18134.1-PLAN.dwg

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0	3/18/24	ISSUED FOR REVIEW	KDR
REV.	DATE	REVISION	BY

Designed and Produced in NH

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Plan Name: TC-600 RADAR SPEED SIGN SPECIFICATIONS

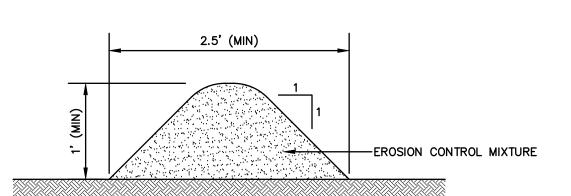
LUSTER CLUSTER Project: 635 SAGAMORE AVE., PORTSMOUTH, NH 635 SAGAMORE DEVELOPMENT LLC Owner of Record 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

D6 SHEET 20 OF 21 JBE PROJECT NO. 18134.1

DRAWING No.

TEMPORARY EROSION CONTROL NOTES

- THE SMALLEST PRACTICAL AREA OF LAND SHALL BE EXPOSED AT ANY ONE TIME. AT NO TIME SHALL AN AREA IN EXCESS OF 5
- EROSION, SEDIMENT AND DETENTION MEASURES SHALL BE INSTALLED AS SHOWN ON THE PLANS AND AT LOCATIONS AS REQUIRED, DIRECTED BY THE ENGINEER.
- 3. ALL DISTURBED AREAS (INCLUDING POND AREAS BELOW THE PROPOSED WATERLINE) SHALL BE RETURNED TO PROPOSED GRADES AND ELEVATIONS. DISTURBED AREAS SHALL BE LOAMED WITH A MINIMUM OF 6" OF SCREENED ORGANIC LOAM AND SEEDED WITH SEED MIXTURE 'C' AT A RATE NOT LESS THAN 1.10 POUNDS OF SEED PER 1,000 S.F. OF AREA (48 LBS. / ACRE).
- SILT FENCES AND OTHER BARRIERS SHALL BE INSPECTED EVERY SEVEN CALENDAR DAYS AND WITHIN 24 HOURS OF A RAINFALL OF 0.5" OR GREATER. ALL DAMAGED AREAS SHALL BE REPAIRED, AND SEDIMENT DEPOSITS SHALL PERIODICALLY BE REMOVED
- AFTER ALL DISTURBED AREAS HAVE BEEN STABILIZED, THE TEMPORARY EROSION CONTROL MEASURES SHALL BE REMOVED AND THE AREA DISTURBED BY THE REMOVAL SMOOTHED AND RE-VEGETATED.
- AREAS MUST BE SEEDED AND MULCHED OR OTHERWISE PERMANENTLY STABILIZED WITHIN 3 DAYS OF FINAL GRADING, OR TEMPORARILY STABILIZED WITHIN 14 DAYS OF THE INITIAL DISTURBANCE OF SOIL. ALL AREAS SHALL BE STABILIZED WITHIN 45
- ALL PROPOSED VEGETATED AREAS THAT DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED BY SEEDING AND INSTALLING NORTH AMERICAN GREEN S75 EROSION CONTROL BLANKETS (OR AN EQUIVALENT APPROVED IN WRITING BY THE ENGINEER) ON SLOPES GREATER THAN 3:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT EVENTS.
- ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15. OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS.
- AFTER OCTOBER 15th, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3" OF CRUSHED GRAVEL PER NHDOT ITEM 304.3.
- 10. AN AREA SHALL BE CONSIDERED STABLE IF ONE OF THE FOLLOWING HAS OCCURRED:
 - a. BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED;
 - b. A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED;
 - c. A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH STONE OR RIPRAP HAS BEEN INSTALLED; OR
 - d. EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.
- 11. FUGITIVE DUST CONTROL IS REQUIRED TO BE CONTROLLED IN ACCORDANCE WITH ENV-A 1000, AND THE PROJECT IS TO MEET THE REQUIREMENTS AND INTENT OF RSA 430:53 AND AGR 3800 RELATIVE TO INVASIVE SPECIES.



- 1. ORGANIC FILTER BERMS SHALL BE UTILIZED IN LIEU OF SILT FENCE.
- 2. THE EROSION CONTROL MIX USED IN THE FILTER BERMS SHALL BE A WELL-GRADED MIXTURE OF PARTICLE SIZES. MAY CONTAIN ROCKS LESS THAN 4" IN DIAMETER. STUMP GRINDINGS. SHREDDED OR COMPOSTED BARK, OR ACCEPTABEL MANUFACTURED PRODUCTS, AND SHALL BE FREE OF REFUSE, PHYSICAL CONTAMINANTS, AND MATERIAL TOXIC TO PLANT GROWTH, AND SHALL MEET THE FOLLOWING STANDARDS:
- a) THE ORGANIC CONTENT SHALL BE 25-65% OF DRY WEIGHT.
- b) PARTICLE SIZE BY WEIGHT SHALL BE 100% PASSING A 3" SCREEN, 90-100% PASSING A 1" SCREEN, 70-100& PASSING A 0.75" SCREEN, AND 30-75% PASSING A 0.25"
- c) THE ORGANIC PORTION SHALL BE FIBROUS AND ELONGATED. d) LARGE PORTIONS OF SILTS, CLAYS, OR FINE SANDS SHALL NOT BE INCLUDED IN THE
- e) SOLUBLE SALTS CONTENT SHALL BE >4.0mmhos/cm. f) THE pH SHALL BE BETWEEN 5.0 AND 8.0.
- 3. ORGANIC FILTER BERMS SHALL BE INSTALLED ALONG A RELATIVELY LEVEL CONTOUR. IT MAY BE NECESSARY TO CUT TALL GRASSES OR WOODY VEGETATION TO AVOID CREATING VOIDS AND BRIDGES THAT WOULD ENABLE FINES TO WASH UNDER THE BERM.
- 4. ON SLOPES LESS THAN 5%, OR AT THE BOTTOM OF SLOPES STEEPER THAN 3:1, UP TO 20' LONG, THE BERM SHALL BE A MINIMUM OF 12" HIGH (AS MEASURED ON THE UPHILL SIDE), AND A MINIMUM OF 36" WIDE. ON LONGER OR STEEPER SLOPES, THE BERM SHALL BE WIDER TO ACCOMMODATE THE POTENTIAL ADDITIONAL RUNOFF.
- 5. FROZEN GROUND, OUTCROPS OF BEDROCK, AND VERY ROOTED FORESTED AREAS PRESENT THE MOST PRACTICAL AND EFFECTIVE LOCATIONS FOR ORGANIC FILTER BERMS. OTHER BMP'S SHOULD BE USED AT LOW POINTS OF CONCENTRATED RUNOFF, BELOW CULVERT OUTLET APRONS, AROUND CATCH BASINS, AND AT THE BOTTOM OF STEEP PERIMETER SLOPES THAT HAVE A LARGE CONTRIBUTING AREA.
- 6. SEDIMENT SHALL BE REMOVED FROM BEHIND THE STRUCTURES WHEN IT HAS ACCUMULATED TO ONE HALF THE ORIGINAL HEIGHT OF THE STRUCTURE.

Date: 2/26/2024

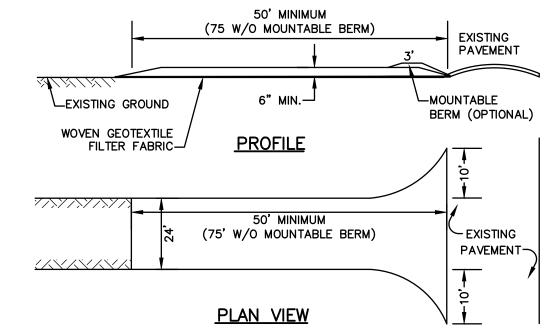
7. STRUCTURES MAY BE LEFT IN PLACE ONCE THE SITE IS STABILIZED.

ORGANIC FILTER BERM / FIBER BERM

NOT TO SCALE

Design: DJM | Draft: KDR

ACRES BE EXPOSED AT ANY ONE TIME BEFORE DISTURBED AREAS ARE STABILIZED.



- 1. STONE FOR STABILIZED CONSTRUCTION ENTRANCE SHALL BE 3 INCH STONE, RECLAIMED STONE, OR RECYCLED CONCRETE EQUIVALENT.
- 2. THE LENGTH OF THE STABILIZED ENTRANCE SHALL NOT BE LESS THAN 50 FEET, 75' WITHOUT A MOUNTABLE BERM, AND EXCEPT FOR A SINGLE RESIDENTIAL LOT WHERE A 30 FOOT MINIMUM LENGTH WOULD APPLY. 3. THICKNESS OF THE STONE FOR THE STABILIZED ENTRANCE SHALL NOT BE LESS THAN 6
- 4. THE WIDTH OF THE ENTRANCE SHALL NOT BE LESS THAN THE FULL WIDTH OF THE ENTRANCE WHERE INGRESS OR EGRESS OCCURS, OR 10 FEET, WHICHEVER IS GREATER.
- 5. GEOTEXTILE FILTER FABRIC SHALL BE PLACED OVER THE ENTIRE AREA PRIOR TO PLACING THE STONE. FILTER FABRIC IS NOT REQUIRED FOR A SINGLE FAMILY RESIDENTIAL LOT. 6. ALL SURFACE WATER THAT IS FLOWING TO OR DIVERTED TOWARD THE CONSTRUCTION ENTRANCE SHALL BE PIPED BENEATH THE ENTRANCE. IF PIPING IS IMPRACTICAL, A STONE BERM WITH 5:1 SLOPES THAT CAN BE CROSSED BY VEHICLES MAY BE SUBSTITUTED FOR
- 7. THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION THAT WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO THE PUBLIC RIGHT-OF-WAY. THIS MAY REQUIRE PERIODIC TOP DRESSING WITH ADDITIONAL STONE AS CONDITIONS DEMAND AND REPAIR AND/OR CLEAN OUT OF ANY MEASURES USED TO TRAP SEDIMENT. ALL SEDIMENT SPILLED, WASHED, OR TRACKED ONTO THE PUBLIC RIGHT-OF-WAY MUST BE REMOVED PROMPTLY.

STABILIZED CONSTRUCTION ENTRANCE

NOT TO SCALE

SEEDING SPECIFICATIONS

- GRADING AND SHAPING A. SLOPES SHALL NOT BE STEEPER THAN 2:1 WITHOUT APPROPRIATE EROSION CONTROL MEASURES AS
- SPECIFIED ON THE PLANS (3:1 SLOPES OR FLATTER ARE PREFERRED). B. WHERE MOWING WILL BE DONE, 3:1 SLOPES OR FLATTER ARE RECOMMENDED.

2. <u>SEEDBED PREPARATION</u>

- A. SURFACE AND SEEPAGE WATER SHOULD BE DRAINED OR DIVERTED FROM THE SITE TO PREVENT DROWNING
- OR WINTER KILLING OF THE PLANTS. B. STONES LARGER THAN 4 INCHES AND TRASH SHOULD BE REMOVED BECAUSE THEY INTERFERE WITH SEEDING AND FUTURE MAINTENANCE OF THE AREA. WHERE FEASIBLE, THE SOIL SHOULD BE TILLED TO A DEPTH OF ABOUT 4 INCHES TO PREPARE A SEEDBED AND FERTILIZER AND LIME MIXED INTO THE SOIL. THE SEEDBED SHOULD BE LEFT IN A REASONABLY FIRM AND SMOOTH CONDITION. THE LAST TILLAGE OPERATION SHOULD BE PERFORMED ACROSS THE SLOPE WHEREVER PRACTICAL.

3. ESTABLISHING A STAND

- A. LIME AND FERTILIZER SHOULD BE APPLIED PRIOR TO OR AT THE TIME OF SEEDING AND INCORPORATED INTO THE SOIL. TYPES AND AMOUNTS OF LIME AND FERTILIZER SHOULD BE BASED ON AN EVALUATION OF SOIL TESTS. WHEN A SOIL TEST IS NOT AVAILABLE, THE FOLLOWING MINIMUM AMOUNTS SHOULD BE
- AGRICULTURAL LIMESTONE, 2 TONS PER ACRE OR 100 LBS. PER 1,000 SQ.FT. NITROGEN(N), 50 LBS. PER ACRE OR 1.1 LBS. PER 1,000 SQ.FT.
- PHOSPHATE(P205), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT. POTASH(K20), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT.
- (NOTE: THIS IS THE EQUIVALENT OF 500 LBS. PER ACRE OF 10-20-20 FERTILIZER OR 1,000 LBS. PER
- ACRE OF 5-10-10.) B. SEED SHOULD BE SPREAD UNIFORMLY BY THE METHOD MOST APPROPRIATE FOR THE SITE. METHODS INCLUDE BROADCASTING, DRILLING AND HYDROSEEDING. WHERE BROADCASTING IS USED, COVER SEED WITH
- .25 INCH OF SOIL OR LESS, BY CULTIPACKING OR RAKING. C. REFER TO THE 'SEEDING GUIDE' AND 'SEEDING RATES' TABLES ON THIS SHEET FOR APPROPRIATE SEED MIXTURES AND RATES OF SEEDING. ALL LEGUMES (CROWNVETCH, BIRDSFOOT, TREFOIL AND FLATPEA)
- MUST BE INOCULATED WITH THEIR SPECIFIC INOCULANT PRIOR TO THEIR INTRODUCTION TO THE SITE. D. WHEN SEEDED AREAS ARE MULCHED, PLANTINGS MAY BE MADE FROM EARLY SPRING TO EARLY OCTOBER WHEN SEEDED AREAS ARE NOT MULCHED, PLANTINGS SHOULD BE MADE FROM EARLY SPRING TO MAY 20th OR FROM AUGUST 10th TO SEPTEMBER 1st.

A. HAY, STRAW, OR OTHER MULCH, WHEN NEEDED, SHOULD BE APPLIED IMMEDIATELY AFTER SEEDING. B. MULCH WILL BE HELD IN PLACE USING APPROPRIATE TECHNIQUES FROM THE BEST MANAGEMENT PRACTICE FOR MULCHING. HAY OR STRAW MULCH SHALL BE PLACED AT A RATE OF 90 LBS PER 1000 S.F.

5. MAINTENANCE TO ESTABLISH A STAND

- A. PLANTED AREAS SHOULD BE PROTECTED FROM DAMAGE BY FIRE, GRAZING, TRAFFIC, AND DENSE WEED
- B. FERTILIZATION NEEDS SHOULD BE DETERMINED BY ONSITE INSPECTIONS. SUPPLEMENTAL FERTILIZER IS USUALLY THE KEY TO FULLY COMPLETE THE ESTABLISHMENT OF THE STAND BECAUSE MOST PERENNIALS TAKE 2 TO 3 YEARS TO BECOME FULLY ESTABLISHED.
- C. IN WATERWAYS, CHANNELS, OR SWALES WHERE UNIFORM FLOW CONDITIONS ARE ANTICIPATED, ANNUAL MOWING MAY BE NECESSARY TO CONTROL GROWTH OF WOODY VEGETATION.

USE	SEEDING MIXTURE 1/	DROUGHTY	WELL DRAINED	MODERATELY WELL DRAINED	POORLY DRAINED
STEEP CUTS AND FILLS, BORROW AND DISPOSAL AREAS	A B C	FAIR POOR POOR FAIR	GOOD GOOD GOOD EXCELLENT	GOOD FAIR EXCELLENT EXCELLENT	FAIR FAIR GOOD POOR
WATERWAYS, EMERGENC SPILLWAYS, AND OTHER CHANNELS WITH FLOWING WATER.		GOOD GOOD	GOOD EXCELLENT	GOOD EXCELLENT	FAIR FAIR
LIGHTLY USED PARKING LOTS, ODD AREAS, UNUSED LANDS, AND LOW INTENSITY USE RECREATION SITES.	A B C	GOOD GOOD GOOD	GOOD GOOD EXCELLENT	GOOD FAIR EXCELLENT	FAIR POOR FAIR
PLAY AREAS AND ATHLETIC FIELDS. (TOPSOIL IS ESSENTIAL FOR GOOD TURF.)	E F	FAIR FAIR	EXCELLENT EXCELLENT	EXCELLENT EXCELLENT	<u>2/</u> 2/

GRAVEL PIT, SEE NH-PM-24 IN APPENDIX FOR RECOMMENDATION REGARDING RECLAMATION OF SAND AND GRAVEL PITS.

/ REFER TO SEEDING MIXTURES AND RATES IN TABLE BELOW. 27 POORLY DRAINED SOILS ARE NOT DESIRABLE FOR USE AS PLAYING AREA AND ATHLETIC FIELDS.

NOTE: TEMPORARY SEED MIX FOR STABILIZATION OF TURF SHALL BE WINTER RYE OR OATS AT A RATE OF 2.5 LBS. PER 1000 S.F. AND SHALL BE PLACED PRIOR TO OCTOBER 15th, IF PERMANENT SEEDING NOT

SEEDING GUIDE

MIXTURE	POUNDS PER ACRE	POUNDS PER 1.000 Sq. Ft.			
A. TALL FESCUE CREEPING RED FESCUE RED TOP TOTAL	20 20 <u>2</u> 42	0.45 0.45 <u>0.05</u> 0.95			
B. TALL FESCUE CREEPING RED FESCUE CROWN VETCH OR	15 10 15	0.35 0.25 0.35			
FLAT PEA TOTAL	30 40 OR 55	0.75 0.95 OR 1.35			
C. TALL FESCUE CREEPING RED FESCUE BIRDS FOOT TREFOIL TOTAL	20 20 <u>8</u> 48	0.45 0.45 <u>0.20</u> 1.10			
D. TALL FESCUE FLAT PEA TOTAL	20 30 50	0.45 <u>0.75</u> 1.20			
E. CREEPING RED FESCUE 1/ KENTUCKY BLUEGRASS 1/ TOTAL	50 <u>50</u> 100	1.15 <u>1.15</u> 2.30			
F. TALL FESCUE 1	150	3.60			
1/FOR HEAVY USE ATHLETIC FIELDS CONSULT THE UNIVERSITY OF NEW HAMPSHIRE COOPERATIVE EXTENSION TURF SPECIALIST FOR CURRENT VARIETIES AND SEEDING RATES.					

SEEDING RATES

WIRE SCREEN SHALL BE PLACED BETWEEN STONE AND BLOCKS TO PREVENT THE AGGREGATE FROM BEING WASHED INTO THE STRUCTURE —CONCRETE BLOCKS STONE FILTER RUNOFF WATER WITH SEDIMENT - WIRE SCREEN

MAINTENANCE NOTE:

1. ALL STRUCTURES SHOULD BE INSPECTED AFTER EVERY RAINFALL AND REPAIRS MADE AS NECESSARY. SEDIMENT SHOULD BE REMOVED FROM TRAPPING DEVICES AFTER THE SEDIMENT HAS REACHED A MAXIMUM OF ONE HALF THE DEPTH OF THE TRAP. THE SEDIMENT SHOULD BE DISPOSED IN A SUITABLE UPLAND AREA AND PROTECTED FROM EROSION BY EITHER STRUCTURE OR VEGETATIVE MEANS. THE TEMPORARY TRAPS SHOULD BE REMOVED AND THE AREA REPAIRED AS SOON AS THE CONTRIBUTING DRAINAGE AREA TO THE INLET HAS BEEN COMPLETELY STABILIZED.

-FILTERED WATER

- DROP INLET WITH GRATE

TEMPORARY CATCH BASIN INLET PROTECTION (Block and Gravel Drop Inlet Sediment Filter)

-SUBGRADE

NOT TO SCALE

CONSTRUCTION SEQUENCE

- PRIOR TO THE START OF ANY ACTIVITY, IT IS THE RESPONSIBILITY OF THE SITE'S SITE DEVELOPER (OR OWNER) TO FILE A NOTICE OF INTENT (NOI) FORM WITH THE ENVIRONMENTAL PROTECTION AGENCY (EPA) IN ORDER TO GAIN COVERAGE UNDER THE NPDES GENERAL PERMIT FOR STORM WATER DISCHARGES FROM CONSTRUCTION ACTIVITIES. A PRE CONSTRUCTION MEETING IS TO BE HELD WITH ALL DEPARTMENT HEADS PRIOR TO THE START OF CONSTRUCTION.
- 2. CUT AND REMOVE TREES IN CONSTRUCTION AREA AS REQUIRED OR DIRECTED.
- 3. INSTALL FIBER BERM, HAY BALES AND CONSTRUCTION ENTRANCES PRIOR TO THE START OF CONSTRUCTION. THESE ARE TO BE MAINTAINED UNTIL THE FINAL PAVEMENT SURFACING AND LANDSCAPING AREAS ARE ESTABLISHED.
- CLEAR, CUT, GRUB AND DISPOSE OF DEBRIS IN APPROVED FACILITIES. THIS INCLUDES ANY REQUIRED DEMOLITION OF EXISTING STRUCTURES, UTILITIES, ETC.
- 5. CONSTRUCT AND/OR INSTALL TEMPORARY OR PERMANENT SEDIMENT AND/OR DETENTION BASIN(S) AS REQUIRED. THESE FACILITIES SHALL BE INSTALLED AND STABILIZED PRIOR TO DIRECTING RUN-OFF TO THEM.
- 6. STRIP LOAM AND PAVEMENT PER THE RECOMMENDATIONS OF THE PROJECT ENGINEER AND STOCKPILE EXCESS MATERIAL. STABILIZE STOCKPILE AS NECESSARY.
- 7. PERFORM PRELIMINARY SITE GRADING IN ACCORDANCE WITH THE PLANS.
- 8. INSTALL THE SEWER AND DRAINAGE SYSTEMS FIRST, THEN ANY OTHER UTILITIES IN ACCORDANCE WITH THE PLAN AND DETAILS, ANY CONFLICTS BETWEEN UTILITIES ARE TO BE RESOLVED WITH THE INVOLVEMENT AND APPROVAL OF THE ENGINEER. 9. INSTALL INLET PROTECTION AT ALL CATCH BASINS AS THEY ARE CONSTRUCTED IN ACCORDANCE WITH DETAILS.
- 10. ALL SWALES AND DRAINAGE STRUCTURES ARE TO BE CONSTRUCTED AND STABILIZED PRIOR TO HAVING RUN-OFF DIRECTED TO THEM.
- 11. DAILY, OR AS REQUIRED, CONSTRUCT TEMPORARY BERMS, DRAINAGE DITCHES, CHECK DAMS, SEDIMENT TRAPS, ETC., TO PREVENT EROSION ON THE SITE AND PREVENT ANY SILTATION OF ABUTTING WATERS AND/OR PROPERTY.
- 12. PERFORM FINAL FINE GRADING, INCLUDING PLACEMENT OF 'SELECT' SUBGRADE MATERIALS.
- 13. PAVE ROADWAY AND DRIVEWAYS WITH INITIAL 'BASE COURSE'.
- 14. PERFORM ALL REMAINING SITE CONSTRUCTION (i.e. BUILDING, CURBING, UTILITY CONNECTIONS, ETC.).
- 15. LOAM AND SEED ALL DISTURBED AREAS AND INSTALL ANY REQUIRED SEDIMENT AND EROSION CONTROL FACILITIES (i.e. RIP RAP, EROSION CONTROL BLANKETS, ETC.).
- 16. FINISH PAVING ROADWAY AND DRIVEWAYS WITH 'FINISH' COURSE.
- 17. ROADWAY AND DRIVEWAYS SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- 18. ALL CUT AND FILL SLOPES SHALL BE SEEDED/LOAMED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- 19. COMPLETE PERMANENT SEEDING AND LANDSCAPING.
- 20. REMOVE TEMPORARY EROSION CONTROL MEASURES AFTER SEEDING AREAS HAVE BEEN 75%-85% ESTABLISHED AND SITE IMPROVEMENTS ARE COMPLETE. SMOOTH AND RE-VEGETATE ALL DISTURBED AREAS.
- 21. CLEAN SITE AND ALL DRAINAGE STRUCTURES, PIPES AND SUMPS OF ALL SILT AND DEBRIS.
- 22. INSTALL ALL PAINTED PAVEMENT MARKINGS AND SIGNAGE PER THE PLANS AND DETAILS.
- 23. ALL EROSION CONTROLS SHALL BE INSPECTED WEEKLY AND AFTER EVERY QUARTER-INCH OF RAINFALL
- 24. UPON COMPLETION OF CONSTRUCTION, IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO NOTIFY ANY RELEVANT PERMITTING AGENCIES THAT THE CONSTRUCTION HAS BEEN FINISHED IN A SATISFACTORY MANNER.

LUSTER CLUSTER

635 SAGAMORE AVE., PORTSMOUTH, NH

Designed and Produced in NH

Stratham, NH 03885

E-MAIL: JBE@JONESANDBEACH.COM

Project:

EROSION AND SEDIMENT CONTROL DETAILS

SHEET 21 OF 21

DRAWING No.

JBE PROJECT NO. 18134.1

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	4	10/22/24	REVISED PER ALTUS AND TAC COMMENTS	DJM
	3	9/16/24	REVISED PER ALTUS AND TAC COMMENTS	DJM
	2	8/14/24	REVISED PER CITY REVIEW ENGINEER COMMENTS	
	1	4/19/24	REVISED PER TAC COMMENTS	DJM
	0	3/18/24	ISSUED FOR REVIEW	KDR
	REV.	DATE	REVISION	BY
		<u>. </u>		

603-772-4746 85 Portsmouth Ave. Civil Engineering Services PO Box 219

635 SAGAMORE DEVELOPMENT LLC Owner of Record 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

