



February 14, 2022

Portsmouth Planning Board 1 Junkins Ave Portsmouth, NH 03801

SUBJECT: Drive-Thru Conditional Use Request Granite State Convenience Proposed Retail Motor Fuel Outlet 2255 Lafayette Road Map 272 Lot 3

Dear Members of the Portsmouth Planning Board:

On behalf of Granite State Convenience **Greenman-Pedersen**, **Inc. (GPI)** is hereby requesting a Conditional Use Permit from the Portsmouth Planning Board for the following:

• Section 10.440 to allow a drive-thru in the Gateway Corridor (G1) Zone

The project site consists of one parcel identified as Map 272 Lot 3 which totals approximately 2.571 acres. The site is bordered by Lafayette Road (Route 1) to the northwest, commercial properties to the northeast and southwest and wooded areas containing wetlands to the south and southeast. The site is previously developed and contains a Burger King restaurant with drive-thru, which is currently not in use, and associated paved parking lot and driveways to Lafayette Road. The majority of the lot is paved and on-site drainage structures are limited to a single catch basin in the landscaped area northwest of the existing building which had no visible pipe outlet at the time of survey. Granite State Convenience is proposing to raze the existing restaurant and construct a retail motor fuel outlet consisting of a 5,555 sf convenience store/sandwich shop with drive-through service and a fueling canopy with 5 retail fuel dispenser islands (10 fueling locations), and associated paved driveways and parking.

This request is made in accordance with the provisions contained in Article 10.243.20 of the City of Portsmouth Zoning Ordinance. GPI is providing the following information in support of the criteria listed in that Section:

Conditional uses designated in Section 10.440 – Table of Uses, as well as other conditional uses for which no specific criteria are set forth in the Ordinance, shall comply with all of the following criteria:

(1) The design of proposed structures, their height and scale in relation to the site's surroundings, the nature and intensity of the proposed use or activity, and the layout and design of the site will be compatible with adjacent and nearby properties, buildings and uses, will complement or enhance the character of surrounding development, and will encourage the appropriate and orderly development and use of land and buildings in the surrounding area.

The site was previously permitted and used as a restaurant with drive-thru. The proposed development is appropriate in character to the site. The neighboring businesses along Lafayette Road are similar commercial uses and the proposed development will match the spirit of the neighborhood. Increased landscaping will enhance the character of the development, as well as an enhanced building façade.

(2) All necessary public and private utility infrastructure and services will be available and adequate to serve the proposed use.

Eversource, electric service, has confirmed they have enough capacity to serve the proposed development. Municipal water and sewer are available to the site. Until/Northern Utilities Natural Gas Division has confirmed natural gas is available to supply the proposed development at 2255 Lafayette Road.

(3) The site and surrounding streets will have adequate vehicular and pedestrian infrastructure to serve the proposed use consistent with the City's Master Plan.

Due to the site's location along Lafayette Road, Route One, there is no pedestrian access to the site or any of the adjacent properties at this time. A 12 ft NHDOT reserve strip and a 8 ft wide Portsmouth Multiuse Path are proposed along the frontage for future DOT and Municipal use.

The site has adequate maneuvering space for the drive thru with sufficient room for 13 stacked vehicles within the drive thru lanes, and adequate space for delivery trucks and emergency vehicles around the site.

(4) The proposed structures, uses, or activities will not have significant adverse impacts on abutting and surrounding properties on account of traffic, noise, odors, vibrations, dust, fumes, hours of operation, and exterior lighting and glare.

There will be no significant adverse impacts to the surrounding properties as the site is surrounded by similar commercial uses and is consistent with the existing use.

(5) The proposed structures and uses will not have significant adverse impacts on natural or scenic resources surrounding the site, including wetlands, floodplains, and significant wildlife habitat.

The proposed development is consistent with the existing use and adjacent properties, and will not have a negative scenic impact on the neighborhood. The proposed site work has been designed to have the least adverse impact to the wetland buffer. The development will result in a decrease of over 9,000 sf of impervious cover within the wetland buffer zone and will increase wetland buffer widths.

(6) The proposed use will not cause or contribute to a significant decline in property values of adjacent properties.

The proposed use will not cause any decrease to property values as the proposed use is consistent with the existing use and the uses of abutting commercial properties.

If you have any questions or need additional information, please feel free to contact me directly at 603-374-7906 or by email at nduquette@gpinet.com

Sincerely,

Nicole Duquette

Nicole Duquette, LEED AP Project Manager

enclosure(s)

cc: Brad Pernaw, Granite State Convenience





February 14, 2022

Portsmouth Conservation Commission 1 Junkins Ave Portsmouth, NH 03801

SUBJECT: Wetland Buffer Conditional Use Request Granite State Convenience Proposed Retail Motor Fuel Outlet 2255 Lafayette Road Map 272 Lot 3

Dear Members of the Portsmouth Conservation Commission:

On behalf of Granite State Convenience **Greenman-Pedersen**, **Inc. (GPI)** is hereby requesting a Wetland Buffer Conditional Use Permit from the Portsmouth Conservation Commission for the following:

• Article 10.1016 to allow development within the wetland buffer zone

The project site consists of one parcel identified as Map 272 Lot 3 which totals approximately 2.571 acres. The site is bordered by Lafayette Road (Route 1) to the northwest, commercial properties to the northeast and southwest and wooded areas containing wetlands to the south and southeast. The site is previously developed and contains a Burger King restaurant with drive-thru, which is currently not in use, and associated paved parking lot and driveways to Lafayette Road. The majority of the lot is paved and on-site drainage structures are limited to a single catch basin in the landscaped area northwest of the existing building which had no visible pipe outlet at the time of survey. Granite State Convenience is proposing to raze the existing restaurant and construct a retail motor fuel outlet consisting of a 5,555 sf convenience store/sandwich shop with drive-through service and a fueling canopy with 5 retail fuel dispenser islands (10 fueling locations), and associated paved driveways and parking.

This request is made in accordance with the provisions contained in Article 10.1017.50 of the City of Portsmouth Zoning Ordinance. GPI is providing the following information in support of the criteria listed in that Section:

Any proposed development, other than installation of utilities within a right-of-way, shall comply with all of the following criteria:

(1) The land is reasonably suited to the use, activity or alteration.

The land has previously been disturbed for a similar use.

The proposed development will consist of razing the existing fast food restaurant and removing 59,940 sf of impervious pavement and concrete, and constructing a development with a smaller development footprint. In addition, approximately 9,000 sf of current impervious area will be restored to its natural state with the proposed development.

The majority of the wetland buffer disturbance area is within the buffer to a swale between the site and the neighboring property to the east. This swale conveys water from the NH DOT drainage system.

(2) There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use, activity or alteration.

The site has been designed in a way that minimizes activity in the wetland buffer area. The total impervious area within the wetland buffer will be decreased by over 9,000 sf between the existing and proposed use. The distance between the developed area will increase from 10 ft to the dumpster and 14 ft to paved surfaces in the existing condition to 25 ft in the proposed condition.

(3) There will be no adverse impact on the wetland functional values of the site or surrounding properties;

As stated in criterion 3, the proposed development will decrease impervious cover within the wetland buffer area and increase wetland buffer widths. The proposed development also includes a comprehensive stormwater management system which will decrease the pollutant load to the wetland by installing deep sump catch basins with "Eliminator" oil hoods, first defense hydrodynamic separator unit, and an oil/water separator tank.

(4) Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals; and

There will be no alteration to natural vegetative state in the wetland buffer as all work will occur in previously disturbed areas.

(5) The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this Section.

The proposed site work has been designed to have the least adverse impact to the wetland buffer. Per Conservation Commission comments on the Preliminary Site Plan, the underground storage tanks have been shifted to the west side of the lot furthest away from the wetland and outside the wetland buffer, the loading zone has been relocated to the westerly side of the property so the southern edge of the development can shift further out of the wetland buffer, and parking spaces have been eliminated on the eastern side of the development. In addition, as recommended by the Conservation Commission, a depressed area has been created along the northeast of the site to collect and filter snowmelt from snow storage to snowmelt from directly entering the wetland.

(6) Any area within the vegetated buffer strip will be returned to a natural state to extent feasible.

A portion of the previously disturbed area within the wetland buffer will be restored to a natural state as a part of this project.

If you have any questions or need additional information, please feel free to contact me directly at 603-374-7906 or by email at nduquette@gpinet.com

Sincerely,

Nicole Duquette

Nicole Duquette, LEED AP Project Manager

enclosure(s)

cc: Brad Pernaw, Granite State Convenience

ABUTTERS & NOTIFICATION LIST For GRANITE STATE CONVENIENCE 2255 LAYFAYETTE ROAD PARCEL ID: 0272-0003 PORTSMOUTH, NH GPI # NEX-2021163 AS OF 5/25/22

PARCEL ID #	NAME & ADDRESS
0272-0003 (SUBJECT PARCEL)	MASTORAN RESTAURANTS, INC. 822 LEXINGTON STREET 2 ND FLOOR WALTHAM, MA 02154
0272-0002	2225 LAFAYETTE LLC 125 AVIATION AVENUE # 202 PORTSMOUTH, NH 03801
0272-0001	2219 LAFAYETTE ROAD, LLC 549 US HIGHWAY 1 BYPASS PORTSMOUTH, NH 03801
0272-0004	RYE PORT PROPERTIES, LLC P.O. BOX 345 STRATHAM, NH 03885
0272-0006	SPRINGBROOK CIRCLE CONDOMINIUMS
OFFICERS:	DAVID WAJDA, PRESIDENT SPRINGBROOK CIRCLE CONDO ASSOCIATION 2000 SPRINGBROOK CIRCLE PORTSMOUTH, NH 03801
	DEAN SAVRAMIS, VICE PRESIDENT SPRINGBROOK CIRCLE CONDO ASSOCIATION 2000 SPRINGBROOK CIRCLE PORTSMOUTH, NH 03801
	JAMES MATTHEWS, TREASURER SPRINGBROOK CIRCLE CONDO ASSOCIATION 2000 SPRINGBROOK CIRCLE PORTSMOUTH, NH 03801
	TOM PUIIA, TRUSTEE SPRINGBROOK CIRCLE CONDO ASSOCIATION 2000 SPRINGBROOK CIRCLE PORTSMOUTH, NH 03801

ABUTTERS & NOTIFICATION LIST For GRANITE STATE CONVENIENCE 2255 LAYFAYETTE ROAD PARCEL ID: 0272-0003 PORTSMOUTH, NH GPI # NEX-2021163 AS OF 5/25/22

SABINE DESHAZO, TRUSTEE SPRINGBROOK CIRCLE CONDO ASSOCIATION 2000 SPRINGBROOK CIRCLE PORTSMOUTH, NH 03801

0273-0007-0001 FESTIVAL FUN PARKS, LLC C/O PROPERTY TAX SERVICE CO. P.O. BOX 543185 DALLAS, TX 75354

ENGINEER/SURVEYOR GREENMAN-PEDERSEN, INC. 44 STILES ROAD, SUITE ONE SALEM, NH 03079

WETLAND/SOIL SCIENTIST MARK WEST WEST ENVIRONMENTAL, INC. 48 STEVENS HILL ROAD NOTTINGHAM, NH 03290

APPLICANT GRANITE STATE CONVENIENCE 25 SPRINGER ROAD HOOKSETT, NH 03106

ATTORNEY	JOHN K. BOSEN, ESQ
	BOSEN & ASSOCIATES, P.L.L.C
	266 MIDDLE STREET
	PORTSMOUTH, NH 03801

Green Building Initiatives

REF:	NEX-2021163
DATE:	February 14, 2022
то:	City of Portsmouth Planning Board
FROM:	Nicole Duquette, Greenman-Pedersen, Inc.
RE:	2255 Lafayette Road – Land Use Application Green Building Initiatives

The applicant is proposing to demolish the existing Burger King restaurant and construct a retail motor fuel outlet consisting of a 5,555 square foot convenience store/sandwich shop and drive-thru and a fueling area with 5 retail fueling islands (10 fueling locations). The proposed site work includes many "green" building components and systems, making the project toxic free, allergy & asthma friendly, and will lower the environmental impact during construction and operation. "Green" components are listed and described below.

<u>Structure</u>

- Wood studs are 100% recyclable
- Plywood sheathing is 100% recyclable

Doors and Windows

- Aluminum entrance doors with recycled materials
- Wood windows with Low-E insulating glass, Energy Star

Flooring

• Vinyl Composition tile with recycled content

Walls and Ceilings

- Salvaged barnboard walls and ceilings
- Salvaged timber beams and rafters
- Salvaged corrugated roof panels used as ceilings
- Suspended acoustic ceiling tiles with 100% recyclable materials
- Aluminum ceiling grids with recycled content

Paints, Coatings & Sealants, non-toxic

• Zero VOC paints & sealants

Stone

• Stone veneer on exterior walls

Wood Products

- Cabinets recycled wood, formaldehyde-free
- Adhesives with low or zero VOC

Building Insulation

• Cellulose insulation with recycled content

Plumbing

- Low flow toilets
- Automatic shutoff faucets

Electrical

- L.E.D. light fixtures
- Electrical switches with automatic shut on-off (motion sensors)
- Future EV charging stations

<u>HVAC</u>

- Duct wrap with recycled materials
- Ground based heat pump system
- Exhaust fans with automatic shut off

Roofing

• Asphalt shingles are 100% recyclable

Site Work and Landscaping

• Indigenous/native planting for less lawn coverage & irrigation

PROPOSED RETAIL MOTOR FUEL OUTLET SITE REDEVELOPMENT PLANS for

ASSESSORS MAP 272 LOT 3 2255 LAFAYETTE ROAD PORTSMOUTH, NEW HAMPSHIRE Prepared for:

GRANITE STATE CONVENIENCE, LLC 25 SPRINGER ROAD HOOKSETT, NH 03106



LOCATION MAP (NOT TO SCALE)

INDEX TO DRAWINGS

- TITLE SHEET
- **EXISTING CONDITIONS PLAN** 2.
- DEMOLITION PLAN 3.
- SITE PLAN 4.
- **GRADING & DRAINAGE PLAN** 5.
- UTILITY PLAN 6.
- 7. **EROSION & SEDIMENT CONTROL PLAN**
- LANDSCAPE PLAN 8.
- **DETAIL SHEET** 9.
- 10. **DETAIL SHEET**
- DETAIL SHEET 11. 12. DETAIL SHEET
- 13. DETAIL SHEET
- **DETAIL SHEET** 14.
- 15. SIGN & GRAPHICS PLAN
- 1 OF 1. TRUCK TURN PLAN
- 1 OF 2. LIGHTING PLAN (RL-7838-S1)
- 2 OF 2. LIGHTING DETAILS (RL-7838-S1)
- **1 OF 2. EXTERIOR ELEVATIONS (P201)**
- 2 OF 2. EXTERIOR ELEVATIONS (P202)
- 1 OF 1. PROPOSED CANOPY ELEVATIONS

enman-Pedersen. In 44 Stiles Road, Suite One PREPARED FOR **GRANITE STATE** CONVENIENCE 110 MOTOR 380 **A** R REVISIONS **REV. SHEETS 4-8. TT** /10/22 REV. SHEETS 4-8, 12, 14, TT, ADD SHEET 13 REV. SHEETS 2-9, 11, 3/22/22 TT **REV. SHEET 4** 2/9/22 NO. DATE REVISION **JANUARY 26, 2022** DRAWN/DESIGN BY CHECKED BY CCC/NID DRJ TITLE SHEET

SCALE: NOT TO SCALE PROJECT NO. NEX-2021163 1 OF 15







LOCATION MAP (NOT TO SCALE)

1) A DEMOLITION PERMIT MUST BE OBTAINED FROM THE CITY OF PORTSMOUTH PRIOR TO COMMENCEMENT OF WORK. ALL EXISTING UTILITY DISCONNECTIONS MUST BE COORDINATED WITH **RESPECTIVE UTILITY COMPANIES.**

2) ALL DEMOLITION ACTIVITIES ARE TO BE PERFORMED IN STRICT ADHERENCE TO ALL FEDERAL, STATE AND LOCAL REGULATIONS. CONTRACTOR TO INSTALL EROSION CONTROL DEVICES IN ACCORDANCE WITH EROSION AND SEDIMENT CONTROL PLAN PRIOR TO BEGINNING DEMOLITION

3) PROCEED WITH DEMOLITION IN A SYSTEMATIC MANNER, FROM THE TOP OF THE STRUCTURE(S)

4) DEMOLISH CONCRETE IN ALL SECTIONS

5) BREAK UP CONCRETE SLABS-ON-GRADE, UNLESS OTHERWISE DIRECTED BY THE CONSTRUCTION

6) CONDUCT ALL DEMOLITION OPERATIONS IN A MANNER THAT WILL PREVENT INJURY, DAMAGE TO STRUCTURES, ADJACENT BUILDINGS AND ALL PERSONS.

7) REFRAIN FROM USING EXPLOSIVES WITHOUT PRIOR WRITTEN CONSENT OF THE DEVELOPER AND APPLICABLE GOVERNMENTAL AUTHORITIES.

8) CONDUCT DEMOLITION SERVICES IN SUCH A MANNER TO INSURE MINIMUM INTERFERENCE WITH ROADS, STREETS, WALKS AND OTHER ADJACENT FACILITIES. DO NOT CLOSE OR OBSTRUCT STREETS, WALKS OR OTHER OCCUPIED FACILITIES WITHOUT PRIOR WRITTEN PERMISSION OF THE DEVELOPER AND APPLICABLE GOVERNMENTAL AUTHORITIES. PROVIDE ALTERNATIVE ROUTES AROUND CLOSED OR OBSTRUCTED TRAFFIC WAYS IF REQUIRED BY APPLICABLE GOVERNMENTAL

9) USE WATERING, TEMPORARY ENCLOSURES AND OTHER SUITABLE METHODS, AS NECESSARY TO LIMIT THE AMOUNT OF DUST AND DIRT RISING AND SCATTERING IN THE AIR. CLEAN ADJACENT STRUCTURE AND IMPROVEMENTS OF ALL DUST AND DEBRIS CAUSED BY THE DEMOLITION OPERATIONS. RETURN ALL ADJACENT AREAS TO THE CONDITIONS EXISTING PRIOR TO THE START

10) ACCOMPLISH AND PERFORM THE DEMOLITION IN SUCH A MANNER AS TO PREVENT THE UNAUTHORIZED ENTRY OF PERSONS AT ANY TIME.

11) COMPLETELY FILL BELOW GRADE AREAS AND VOIDS RESULTING FROM THE DEMOLITION OF STRUCTURES AND FOUNDATIONS WITH SOIL MATERIALS CONSISTING OF STONE, GRAVEL AND SAND, FREE FROM DEBRIS, TRASH, FROZEN MATERIALS, ROOTS AND OTHER ORGANIC MATTER. STONES USED WILL NOT BE LARGER THAT 6 INCHES IN DIMENSION. MATERIAL FROM DEMOLITION MAY NOT BE USED AS FILL. PRIOR TO PLACEMENT OF FILL MATERIALS, UNDERTAKE ALL NECESSARY ACTION IN ORDER TO INSURE THAT AREAS TO BE FILLED ARE FREE OF STANDING WATER, FROZEN MATERIAL, TRASH, DEBRIS. PLACE FILL MATERIALS LAYERS NOT EXCEEDING 6 INCHES IN LOOSE DEPTH AND COMPACT EACH LAYER AT PLACEMENT TO 95% OPTIMUM DENSITY, GRADE SURFACE TO MEET ADJACENT CONTOURS AND TO PROVIDE SURFACE DRAINAGE.

12) REMOVE FROM THE DESIGNATED SITE, AT THE EARLIEST POSSIBLE TIME, ALL DEBRIS RUBBISH, SALVAGEABLE ITEMS, HAZARDOUS AND COMBUSTIBLE SERVICES. REMOVED MATERIALS MAY NOT BE STORED, SOLD OR BURNED ON SITE. REMOVAL OF HAZARDOUS AND COMBUSTIBLE MATERIALS SHALL BE ACCOMPLISHED IN ACCORDANCE WITH THE PROCEDURES AS AUTHORIZED BY THE FIRE DEPARTMENT OR OTHER APPROPRIATE REGULATORY AGENCIES AND DEPARTMENTS.

13) DISCONNECT, SHUT OFF AND SEAL ALL UTILITIES SERVING THE STRUCTURE(S) TO BE DEMOLISHED BEFORE THE COMMENCEMENT OF THE DESIGNATED DEMOLITION. MARK FOR POSITION ALL UTILITY DRAINAGE AND SANITARY LINES AND PROTECT ALL ACTIVE LINES. CLEARLY IDENTIFY BEFORE THE COMMENCEMENT OF DEMOLITION SERVICES THE REQUIRED INTERRUPTION OF ACTIVE SYSTEMS THAT MAY AFFECT OTHER PARTIES, AND NOTIFY ALL APPLICABLE UTILITY COMPANIES TO INSURE THE CONTINUATION OF SERVICE.

14) PROTECT EXISTING DRAINAGE SYSTEM(S) AS NECESSARY TO PREVENT SEDIMENT FROM ENTERING DURING CONSTRUCTION. SEE DETAIL SHEETS FOR EROSION CONTROL DEVICES.

15) ALL WORK WITHIN ROADWAY RIGHT-OF-WAYS TO CONFORM TO CITY STANDARDS.

16) THE LIMITS OF WORK SHALL BE CLEARLY MARKED IN THE FIELD PRIOR TO THE START OF CONSTRUCTION OR SITE CLEARING.

17) IT SHALL BE THE CONTRACTORS RESPONSIBILITY TO NOTIFY DIG SAFE (DIAL 811) 72 HOURS PRIOR TO ANY EXCAVATION ON THIS SITE. CONTRACTOR SHALL ALSO NOTIFY LOCAL WATER DEPARTMENT TO MARK OUT THEIR UTILITIES.

18) NOTES ON THIS PLAN THAT READ "TBR" REPRESENT FEATURES TO BE REMOVED. ANY FEATURES NOT LABELED "TBR" OR "TO BE REMOVED" SHALL BE CONSIDERED EXISTING TO REMAIN. 19) EXISTING WATER SERVICE LOCATION IS UNKNOWN. CONTRACTOR TO LOCATE AND DISCONTINUE

SEE EROSION & SEDIMENT CONTROL PLAN FOR CONSTRUCTION SEQUENCE, TEMPORARY EROSION CONTROL MEASURES, AND LOCATION OF EROSION CONTROL DEVICES. SEE LANDSCAPE PLAN FOR LIMITS OF CLEARING.

603.893.0720 Greenman-Pedersen, 44 Stiles Road, Suite Salem, NH 03079	Engineering Design Planning Construction GPINE Inc. One	Management T.COM
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SIGN I.D. NUMBER	TEXT/COLOR	SIZE/REMARKS
R1-1	STOP R/W	30" x 30" NEW SIGN WITH POST
R5–1	DO NOT ENTER R/W	30" x 30" NEW SIGN WITH POST
R7–8	RESERVED PARKING L G/B/W	12" x 18" NEW SIGN WITH POST
R7-8A	ACCESSIBLE G/W	6" X 12"



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VERTICAL GRANITE CURB SINGLE SOLID LINE WHITE GAS LINE UNDERGROUND COMM WATER LINE UNDERGROUND ELECTRIC CHAIN LINK FENCE CONTOUR ELEVATION TREE UTILITY POLE GUY WIRE OVERHEAD WIRE TREELINE SIGN SPOT ELEVATION CATCH BASIN CLEANOUT SEWER MANHOLE TELEPHONE MANHOLE WATER SHUT OFF BOLLARD GAS METER LIGHT POLE • • • • • • • • • WETLAND LINE EASEMENT LINE PROPERTY LINE ABUTTER PROPERTY LINE ZONE LINE NUMBER OF PARKING SPACES



CHAIN LINK FENCE PROP. 12" PAINTED -STOP BAR PROPOSED PROPANE CAGE AND ICE CHEST

<u>M</u>

PROP. 270 LF, 4' HIGH-

PROP. PAVEMENT MARKING (TYP.) -PROP. 12" PAINTED STOP BAR -PROP. VERTICAL GRANITE CURB (VGC) TYP. -PROP. MULTI-PRODUCT BLENDING -DISPENSER (3 TOTAL)

CUSTOM POOLS LOU'S CUSTOM EXHAUST

> PROP. MULTI-PRODUCT -BLENDING DISPENSER WITH DIESEL (2 TOTAL)

> > CHAINLINK FENCE (TYF ' PROP. R1-1-& R5-1 SIGNS

> > > FOUND HS 704 FLUSH

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GAS LINE

WATER LINE

UTILITY POLE

OVERHEAD WIRE

SPOT ELEVATION

SEWER MANHOLE

WATER SHUT OFF

TELEPHONE MANHOLE

CATCH BASIN

CLEANOUT

BOLLARD

GAS METER

LIGHT POLE

EASEMENT LINE

PROPERTY LINE

PROP. CLEANOUT

PROP. CATCH BASIN

PROP. DRAIN MANHOLE

PROP. SPOT ELEVATION

MEET EXISTING GRADE

TOP OF WALL ELEV.

BOTTOM OF WALL ELEV.

ZONE LINE

PROP. CONTOUR ELEVATION

GRADE BREAK

TEST PIT

ABUTTER PROPERTY LINE

GUY WIRE

TREELINE

SIGN

TREE

VERTICAL GRANITE CURB

UNDERGROUND COMM

CHAIN LINK FENCE

CONTOUR ELEVATION

UNDERGROUND ELECTRIC

SINGLE SOLID LINE WHITE

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<u>EROM:</u> STRUCTURE NUMBER	PIPE SIZE (INCHES)	type of Pipe	APPROX. PIPE LENGTH (FEET)	SLOPE OF PIPE (FT./FT.)	TO: STRUCTURE NUMBER
CB-1	12	HDPE	51	0.011	DMH-1
CB-2	12	HDPE	139	0.005	CB-6
CB-3(FD)	12	HDPE	29	0.063	DET IN-1
CB-4(FD)	18	HDPE	81	0.005	DMH-2
CB-5	18	HDPE	70	0.005	CB-4(FD)
CB-6	15	HDPE	93	0.005	CB-5
DET OUT	24	HDPE	7	0.000	OCS-1
DMH-1	12	HDPE	66	0.014	CB-6
DMH-2	. 6	HDPE	10	0.010	OWS-IN
DMH-2	18	HDPE	29	0.032	DET IN-2
DMH-3	12	HDPE	30	0.010	CB-3(FD)
JELLYFISH OUT	18	HDPE	12	0.012	FES-1
OCS-1	18	HDPE	- 3	0.029	JELLYFISH IN
OWS-OUT	6	HDPE	7	0.013	DET IN-3

DRAINAGE STRUCTURES

CB-1 RIM=64.55 INV.OUT=61.05

CB-2 RIM=63.70

INV.OUT=60.10

CB-3(FD) RIM=62.80

INV.IN=58.90(DMH-3) INV.OUT=58.80 CB-4(FD)(DG) RIM=61.70

INV.IN=58.05(CB-5) INV.OUT=57.95

RIM=63.05 INV.IN=58.65(CB-6) INV.OUT=58.40

CB-6 RIM=63.90 INV.IN=59.40(CB-2) INV.IN=59.50(DMH-1) INV.OUT=59.15

DMH-1 RIM=65.30 INV.IN=60.50(CB-1) INV.OUT=60.40

RIM=63.30 INV.IN=57.55(CB-4(FD)) INV.OUT=57.95(18" BYPASS) INV.OUT=57.45 (6" LOW FLOW)

DMH-3 RIM=64.00 INV.IN=59.25(RD) INV.OUT=59.20

FES-1 INV.=56.25 (OWS-1) RIM=63.75± INV.IN=57.35 INV.OUT=57.10 UNDERGROUND DETENTION SYSTEM (UG DET)

4,000 GAL OIL/WATER SEPARATOR-1

36"ø SOLID (WT) PIPES 4 ROWS + 2 HEADERS 67.00'L x 19.25'W S=0.000 FT/FT INV.PIPE=57.00 INV'S.IN=57.00 INV.OUT=57.00 (SEE DETAIL)

OUTLET CONTROL STRUCTURE (OCS-1) RIM=63.70 INV.IN=57.00 INV.OUT=57.00 (SEE DETAIL)

JELLYFISH FILTER (CONTECH JFPD0806 OR APPROVED EQUAL) RIM=62.00

INV.IN=56.90 INV.OUT=56.40 (SEE DETAIL)

(FD) DENOTES FIRST DEFENSE FD-4HC HYRODYNAMIC PARTICLE SEPARATOR OR APPROVED EQUAL.

(WT) DENOTES WATERTIGHT PIPE JOINTS (DG) DENOTES DOUBLE CATCH BASIN

18"PVC -INV.=56.94 PROP. SNOW -COLLECTION AREA MAG NAIL SET IN UP#146 10T 93.5 BA24 ELEV.=66.84 CHAINLINK FENCE (TYP. RIM=65.64 <u>v=59.05(18</u>

WITH CAP-

<u>sili</u>

CLEANOUT & RISER -

COVERS SHALL BE HEAVY DUTY CAST

IRON COVERS SET IN

MIN. 8" THICK, 4.25'

WIDE CONCRETE

PADS (TYP)

4 UP 0.2'













LOCATION MAP (NOT TO SCALE)

1) ALL SITE DRAINAGE PIPE SHALL BE CORRUGATED HIGH-DENSITY POLYETHYLENE PIPE WITH STANDARD JOINTS, DUAL-WALL, SMOOTH INTERIOR, AS MANUFACTURED BY ADS, INC., OR APPROVED EQUAL, UNLESS OTHERWISE NOTED ON PLAN. THE UNDERGROUND DETENTION SYSTEM SHALL HAVE WATER TIGHT JOINTS MEETING ASTM D3212 SPECIFICATIONS.

2) ALL ROOF AND CANOPY DRAIN PIPE SHALL BE 6" PVC (SDR-35).

3) ELEVATIONS ARE BASED ON NAVD88 DATUM.

4) ALL PROPOSED ELEVATIONS AS SHOWN ARE BOTTOM OF CURB ELEVATIONS, UNLESS OTHERWISE NOTED.

5) ANY UTILITY FIELD ADJUSTMENTS SHALL BE APPROVED BY THE ENGINEER OF RECORD AND COORDINATED WITH THE APPROPRIATE LOCAL UTILITY COMPANY.

6) THE LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE ONLY. THE CONTRACTOR IS TO VERIFY EXACT LOCATION PRIOR TO CONSTRUCTION. THE CONTRACTOR IS TO NOTIFY THE DESIGN ENGINEER OF ANY DISCREPANCIES. CONSTRUCTION SHALL COMMENCE BEGINNING AT THE LOWEST INVERT (POINT OF CONNECTION) AND PROGRESS UP GRADIENT. PROPOSED INTERFACE POINTS (CROSSINGS) WITH EXISTING UNDERGROUND INSTALLATIONS SHALL BE FIELD VERIFIED BY TEST PIT PRIOR TO COMMENCEMENT OF CONSTRUCTION.

7) ALL CONSTRUCTION SHALL CONFORM TO MUNICIPAL DPW AND ALL APPLICABLE STATE AND FEDERAL STANDARDS.

8) THE CONTRACTOR SHALL CALL AND COORDINATE WITH DIG-SAFE (DIAL 811) PRIOR TO COMMENCING ANY EXCAVATION.

9) THIS SITE WILL REQUIRE A USEPA NPDES PERMIT FOR STORMWATER DISCHARGE FOR THE SITE CONSTRUCTION SINCE THE DISTURBANCE EXCEEDS ONE ACRE (ACTUAL DISTURBANCE = 75,000 SF±). THE CONSTRUCTION SITE OPERATOR SHALL DEVELOP AND IMPLEMENT A CONSTRUCTION STORM WATER POLLUTION PREVENTION PLAN (SWPPP) WHICH SHALL REMAIN ON SITE AND MADE ACCESSIBLE TO THE PUBLIC. A COMPLETED NOTICE OF TERMINATION (NOT) SHALL BE SUBMITTED TO NPDES PERMITTING AUTHORITY WITHIN 30 DAYS AFTER EITHER OF THE FOLLOWING CONDITIONS HAVE BEEN MET: FINAL STABILIZATION HAS BEEN ACHIEVED ON ALL PORTIONS OF THE SITE FOR WHICH THE PERMITTEE IS RESPONSIBLE; OR ANOTHER OPERATOR/PERMITTEE HAS ASSUMED CONTROL OVER ALL AREAS OF THE SITE THAT HAVE NOT BEEN FINALLY STABILIZED.

10) ANY UTILITIES TO BE TAKEN OUT OF SERVICE SHALL BE DISCONNECTED AS DIRECTED UTILITY COMPANY AND LOCAL DPW.

11) ALL TRAFFIC CONTROL AND TEMPORARY CONSTRUCTION SIGNAGE ARRANGEMENTS, ACCEPTABLE TO NHDOT AND THE CITY DEPARTMENT OF PUBLIC WORKS, SHALL BE EMPLOYED DURING OPERATIONS WITHIN THE PUBLIC RIGHT-OF-WAY.

12) ALL ADA ACCESSIBLE WALKWAYS CANNOT EXCEED 5% RUNNING SLOPE AND 2% CROSS SLOPE, RAMPS CANNOT EXCEED 8.33% RUNNING SLOPE AND 2% CROSS SLOPE, AND ACCESSIBLE PARKING STALLS AND ACCESS AISLES CANNOT EXCEED 2% SLOPE IN ANY DIRECTION. PRIOR TO CONSTRUCTION, CONTRACTOR SHALL NOTIFY ENGINEER OF ANY DISCREPANCIES.

13) SEE UTILITY PLAN FOR DETAILED UTILITY LAYOUT.

14) ALL PROPOSED CATCH BASINS SHALL HAVE 4' SUMPS AND OUTLETS EQUIPPED WITH "ELIMINATOR" OIL HOODS OR APPROVED EQUAL.

15) ALL PIPE DATA IS CALCULATED TO CENTER OF STRUCTURE, TYP.

16) CONTRACTOR TO REFER TO THE INSPECTION & MAINTENANCE (I&M) MANUAL FOR STORMWATER MANAGEMENT SYSTEMS & SITE MAINTENANCE DURING AND AFTER CONSTRUCTION.

17) CONTRACTOR TO INSTALL RISER STRUCTURES AT EACH CORNER OF UNDERGROUND DETENTION SYSTEMS AND CLEANOUTS AT EACH END OF EACH ROW TO PROVIDE ACCESS POINTS FOR CLEANING AND MAINTENANCE. - TOTAL RISERS PROPOSED = 4

- TOTAL CLEANOUTS PROPOSED = 4



PROJECT NO.

NEX-2021163



VGC	VERTICAL GRANITE CURB
SSLW	SINGLE SOLID LINE WHIT
G	GAS LINE
	UNDERGROUND COMM
W	WATER LINE
E	UNDERGROUND ELECTRIC
	CHAIN LINK FENCE
	CONTOUR ELEVATION
۹ Ø	TREE
С)	UTILITY POLE
	GUY WIRE
	OVERHEAD WIRE
	TREELINE
	SIGN
×96.65	SPOT ELEVATION
	CATCH BASIN
0	CLEANOUT
S	SEWER MANHOLE
(\mathbf{T})	TELEPHONE MANHOLE
# <u>\$</u> 0	WATER SHUT OFF
ο	BOLLARD
GM	GAS METER
\$	LIGHT POLE
<u></u>	WETLAND LINE
	EASEMENT LINE
	PROPERTY LINE
6447.5444.75 (1999)	ABUTTER PROPERTY LINE
	ZONE LINE
C.O.	PROP. CLEANOUT
CB-1 🏾	PROP. CATCH BASIN
DMH-1 🔘	PROP. DRAIN MANHOLE
SMH-1 🔘	PROP. SEWER MANHOLE
	PROP. GATE VALVE







LOCATION MAP (NOT TO SCALE)

NOTES:

- 1) ALL SANITARY SEWER PIPE SHALL BE PVC (SDR-35), UNLESS OTHERWISE NOTED.
- 2) ALL WATER PIPE SHALL BE POLYETHYLENE, UNLESS OTHERWISE NOTED.
- 3) ANY UTILITY FIELD ADJUSTMENTS SHALL BE APPROVED BY THE ENGINEER OF RECORD AND COORDINATED WITH THE APPROPRIATE LOCAL UTILITY COMPANY.
- 4) THE LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE ONLY. THE CONTRACTOR IS TO VERIFY EXACT LOCATION PRIOR TO CONSTRUCTION. THE CONTRACTOR IS TO NOTIFY THE DESIGN ENGINEER OF ANY DISCREPANCIES.
- 5) ALL CONSTRUCTION SHALL CONFORM TO MUNICIPAL DPW AND ALL APPLICABLE STATE AND FEDERAL STANDARDS.
- 6) THE CONTRACTOR SHALL CALL AND COORDINATE WITH DIG-SAFE (1-888-344-7233) PRIOR TO COMMENCING ANY EXCAVATION.
- 7) ALL WATER AND SEWER CONSTRUCTION SHALL CONFORM TO DEPARTMENT OF PUBLIC WORKS SPECIFICATIONS.
- 8) THIS SITE IS SERVED BY MUNICIPAL SEWER AND WATER.
- 9) ALL ELECTRIC, TELEPHONE AND CABLE TV LINES ARE TO BE UNDERGROUND AND INSTALLED IN CONFORMANCE WITH APPLICABLE UTILITY CO. SPECIFICATIONS.
- 10) ANY UTILITIES TO BE TAKEN OUT OF SERVICE SHALL BE DISCONNECTED AS DIRECTED BY UTILITY COMPANY AND LOCAL DPW.
- 11) ALL TRAFFIC CONTROL AND TEMPORARY CONSTRUCTION SIGNAGE ARRANGEMENTS, ACCEPTABLE TO NHDOT AND CITY DEPARTMENT OF PUBLIC WORKS, SHALL BE EMPLOYED DURING OPERATIONS WITHIN THE PUBLIC RIGHT-OF-WAY.
- 12) SEE GRADING & DRAINAGE PLAN FOR DETAILED DRAINAGE INFORMATION.
- 13) ELECTRICAL CONDUIT WITHIN 20' OF TANKS OR DISPENSERS MAY NEED TO BE RIGID METAL CONDUIT WITH CONCRETE ENCASEMENT. CONTRACTOR TO COORDINATE WITH UTILITY COMPANY AND/OR TOWN ELECTRICAL INSPECTOR AS REQUIRED.
- 14) REFER TO DETAIL SHEETS FOR ALL UTILITY AND DRAINAGE STRUCTURE DETAILS AND ADDITIONAL INFORMATION.
- 15) ELECTRIC CONDUIT TO BE PROVIDED FOR FUTURE EV CHARGING STATIONS. 16) EXISTING WATER SERVICE LOCATION IS UNKNOWN. CONTRACTOR TO LOCATE AND DISCONTINUE SERVICE AT THE MAIN.
- 17) CONTRACTOR TO CONTACT EASTERN PIPE SERVICES TO PLUG THE SERVICE FROM THE MAIN WITHOUT DISTURBING THE WETLAND. AFTER PLUGGED, CONTRACTOR SHALL FILL THE EXISTING SERVICE WITH FLOWABLE FILL.
- 18) CONTRACTOR SHALL CONTACT PORTSMOUTH DPW AT LEAST 48 HOURS PRIOR TO SEWER CONSTRUCTION TO WITNESS SEWER SERVICE INSTALLATION.

	AVAILABLE
OF PORTSMOUTH PUBLIC WORKS DEPT., PETER RICE 603-427-1530	YES
OF PORTSMOUTH PUBLIC WORKS DEPT., PETER RICE 603-427-1530	YES
1L, DAVE MACLEAN 603-294-5261	YES
RSOURCE, CASEY MCDONALD 603-519-0924	YES
SOLIDATED COMMUNICATIONS	YES

	-				
	SE	WER PIP	E SCHED	ULE	
<u>FROM:</u> TRUCTURE NUMBER	PIPE SIZE (inches)	type of Pipe	APPROX. PIPE LENGTH (feet)	SLOPE OF PIPE (ft./ft.)	<u>to:</u> Structure Number
BLDG.	6	CI	20	0.056	GR. TRAP
GR. TRAP	6	PVC	35	0.081	SMH-1
BLDG.	6	PVC	41	0.062	WYE
SMH-1	6	PVC	178	0.052	SEWER MAIN

SEWER STRUCTURES 1,500 GAL. GREASE TRAP

RIM=64.10 INV.IN=60.10 INV.OUT=59.85 SMH-1 (DROP) RIM=63.00 INV.IN=57.00

INV.OUT=55.70 PROP. WYE INV.=58.95±

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SCALE:

PROJECT NO.

NEX-2021163

1"=30'



CONSTRUCTION SEQUENCE:

- 1) SEDIMENT AND EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO ANY ON-SITE CONSTRUCTION AS SHOWN. ADDITIONAL TEMPORARY SEDIMENT AND EROSION CONTROL MEASURES SHALL BE INSTALLED AS SOON AS PRACTICAL.
- 2) REMOVE AND STOCKPILE SOIL AS REQUIRED. STOCKPILE SHALL BE SURROUNDED WITH HAYBALES TO PREVENT EROSION.
- 3) CONSTRUCT DRIVEWAYS AND PERFORM SITE GRADING.
- 4) INSTALL UNDERGROUND UTILITIES & DRAINAGE.
- 5) BEGIN TEMPORARY AND PERMANENT SEEDING AND MULCHING. ALL CUT AND FILL SLOPES SHALL BE SEEDED OR MULCHED IMMEDIATELY AFTER THEIR CONSTRUCTION.
- 6) DAILY, OR AS REQUIRED, CONSTRUCT, INSPECT, AND IF NECESSARY, RECONSTRUCT TEMPORARY BERMS, DRAINS, DITCHES, SILT FENCES, HAYBALES AND SEDIMENT TRAPS INCLUDING MULCHING AND SEEDING.
- 7) BEGIN EXCAVATION FOR AND CONSTRUCTION OF BUILDINGS.
- 8) FINISH PAVING ALL DRIVES AND PARKING AREAS. CLEAN ALL DRAINAGE STRUCTURES.
- 9) COMPLETE PERMANENT SEEDING AND LANDSCAPING.
- 10) AFTER GRASS HAS BEEN FULLY GERMINATED IN ALL SEEDED AREAS, REMOVE ALL TEMPORARY EROSION CONTROL MEASURES.

WINTER STABILIZATION NOTES:

MAINTENANCE REQUIREMENTS: MAINTENANCE MEASURES SHOULD CONTINUE AS NEEDED THROUGHOUT CONSTRUCTION, INCLUDING THE OVER-WINTER PERIOD. AFTER EACH RAINFALL, SNOWSTORM, OR PERIOD OF THAWING AND RUNOFF, THE SITE CONTRACTOR SHOULD CONDUCT AN INSPECTION OF ALL INSTALLED EROSION CONTROL MEASURES AND PERFORM REPAIRS AS NEEDED TO INSURE THEIR CONTINUING FUNCTION. FOR ANY AREA STABILIZED BY TEMPORARY OR PERMANENT SEEDING PRIOR TO THE ONSET OF THE WINTER SEASON, THE CONTRACTOR SHOULD CONDUCT AN INSPECTION IN THE SPRING TO ASCERTAIN THE CONDITION OF VEGETATION COVER, AND REPAIR ANY DAMAGE AREAS OR BARE SPOTS AND RESEED AS REQUIRED TO ACHIEVE AN ESTABLISHED VEGETATIVE COVER (AT LEAST 85% OF AREA VEGETATED WITH HEALTHY, VIGOROUS GROWTH). SPECIFICATIONS:

TO ADEQUATELY PROTECT WATER QUALITY DURING COLD WEATHER AND DURING SPRING RUNOFF, THE FOLLOWING STABILIZATION TECHNIQUES SHOULD BE EMPLOYED DURING THE PERIOD FROM OCTOBER 15TH THROUGH MAY 15TH.

- 1) THE AREA OF EXPOSED, UNSTABILIZED SOIL SHOULD BE LIMITED TO ONE ACRE AND SHOULD BE PROTECTED AGAINST EROSION BY THE METHODS DESCRIBED IN THIS SECTION PRIOR TO ANY THAW OR SPRING MELT EVENT. SUBJECT TO APPLICABLE REGULATIONS, THE ALLOWABLE AREA OF EXPOSED SOIL MAY BE INCREASED IF ACTIVITIES ARE CONDUCTED ACCORDING TO A WINTER CONSTRUCTION PLAN, DEVELOPED BY A PROFESSIONAL ENGINEER LICENSED TO PRACTICE IN THE STATE OF NEW HAMPSHIRE OR A CERTIFIED PROFESSIONAL IN EROSION AND SEDIMENT CONTROL AS CERTIFIED BY THE CSPESC COUNCIL OF ENVIROCERT INTERNATIONAL, INC.
- 2) STABILIZATION AS FOLLOWS SHOULD BE COMPLETED WITHIN A DAY OF ESTABLISHING THE GRADE THAT IS FINAL OR THAT OTHERWISE WILL EXIST FOR MORE THAN 5 DAYS:
- A. ALL PROPOSED VEGETATED AREAS HAVING A SLOPE OF LESS THAN 15% WHICH DO NOT EXHIBIT A MINIMUM OF 85% VEGETATIVE GROWTH BY OCTOBER 15TH, OR WHICH ARE DISTURBED AFTER OCTOBER 15TH, SHOULD BE SEEDED AND COVERED WITH 3 TO 4 TONS OF HAY OR STRAW MULCH PER ACRE SECURED WITH ANCHORED NETTING, OR 2 INCHES OF EROSION CONTROL MIX (SEE
- DESCRIPTION OF EROSION CONTROL MIX BERMS FOR MATERIAL SPECIFICATION). B. ALL PROPOSED VEGETATED AREAS HAVING A SLOPE OF GREATER OOTHAN 15% WHICH DO NOT EXHIBIT A MINIMUM OF 85% VEGETATIVE GROWTH BY OCTOBER 15TH, OR WHICH ARE DISTURBED AFTER OCTOBER 15TH, SHOULD BE SEEDED AND COVERED WITH A PROPERLY INSTALLED AND ANCHORED EROSION CONTROL BLANKET OR WITH A MINIMUM 4 INCH THICKNESS OF EROSION CONTROL MIX, UNLESS OTHERWISE SPECIFIED BY THE MANUFACTURER. NOTE THAT COMPOST BLANKETS SHOULD NOT EXCEED 2 INCHES IN THICKNESS OR THEY MAY OVERHEAT.
- ALL STONE-COVERED SLOPES MUST BE CONSTRUCTED AND STABILIZED BY OCTOBER 15.
- 4) INSTALLATION OF ANCHORED HAY MULCH OR EROSION CONTROL MIX SHOULD NOT OCCUR OVER SNOW OF GREATER THAN ONE INCH IN DEPTH.
- 5) ALL MULCH APPLIED DURING WINTER SHOULD BE ANCHORED (E.G., BY NETTING, TRACKING, WOOD CELLULOSE FIBER).
- 6) STOCKPILES OF SOIL MATERIALS SHOULD BE MULCHED FOR OVER WINTER PROTECTION WITH HAY OR STRAW AT TWICE THE NORMAL RATE OR WITH A FOUR-INCH LAYER OF EROSION CONTROL MIX. MULCHING SHOULD BE DONE WITHIN 24 HOURS OF STOCKING, AND RE-ESTABLISHED PRIOR TO ANY RAINFALL OR SNOWFALL. NO SOIL STOCKPILE SHOULD BE PLACED (EVEN COVERED WITH MULCH) WITHIN 100 FEET FROM ANY WETLAND OR OTHER WATER RESOURCE AREA.
- 7) FROZEN MATERIALS, (E.G., FROST LAYER THAT IS REMOVED DURING WINTER CONSTRUCTION), SHOULD BE STOCKPILED SEPARATELY AND IN A LOCATION THAT IS AWAY FROM ANY AREA NEEDING TO BE PROTECTED. STOCKPILES OF FROZEN MATERIAL CAN MELT IN THE SPRING AND BECOME UNWORKABLE AND DIFFICULT TO TRANSPORT DUE TO THE HIGH MOISTURE CONTENT IN THE SOIL.
- 8) INSTALLATION OF EROSION CONTROL BLANKETS SHOULD NOT OCCUR OVER SNOW OF GREATER THAN ONE INCH IN DEPTH OR ON FROZEN GROUND.
- 9) ALL GRASS-LINED DITCHES AND CHANNELS SHOULD BE CONSTRUCTED AND STABILIZED BY SEPTEMBER 1. ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85% VEGETATIVE GROWTH BY OCTOBER 15TH, OR WHICH ARE DISTURBED AFTER OCTOBER 15TH, SHOULD BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS, AS DETERMINED BY A QUALIFIED PROFESSIONAL ENGINEER OR A CERTIFIED PROFESSIONAL IN EROSION AND SEDIMENT CONTROL AS CERTIFIED BY THE CSPESC COUNCIL OF ENVIROCERT INTERNATIONAL, INC. IF A STONE LINING IS NECESSARY, THE CONTRACTOR MAY NEED TO RE-GRADE THE DITCH AS REQUIRED TO PROVIDE ADEQUATE CROSS-SECTION AFTER ALLOWING FOR PLACEMENT OF THE STONE.
- 10) ALL STONE-LINED DITCHES AND CHANNELS MUST BE CONSTRUCTED AND STABILIZED BY OCTOBER 15.
 11) AFTER OCTOBER 15, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK
- HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3 INCHES OF CRUSHED GRAVEL PER NHDOT ITEM 304.3.
 12) SEDIMENT BARRIERS THAT ARE INSTALLED DURING FROZEN CONDITIONS
- SHOULD CONSIST OF EROSION CONTROL MIX BERMS, OR CONTINUOUS CONTAINED BERMS. SILT FENCES AND HAY BALES SHOULD NOT BE INSTALLED WHEN FROZEN CONDITIONS PREVENT PROPER EMBEDMENT OF THESE BARRIERS.



(NOT TO SCALE)

EROSION CONTROL NOTES:

- 1) THE EROSION CONTROL PROCEDURES SHALL CONFORM TO THE NH STORMWATER MANUAL, VOLUME 3, EROSION & SEDIMENT CONTROLS DURING CONSTRUCTION, DECEMBER 2008, OR LATEST EDITION.
- 2) DURING CONSTRUCTION AND THEREAFTER, EROSION CONTROL MEASURES ARE TO BE IMPLEMENTED AS NOTED: THE SMALLEST PRACTICAL AREA OF LAND SHOULD BE EXPOSED AT ANY ONE TIME DURING DEVELOPMENT. WHEN LAND IS EXPOSED DURING DEVELOPMENT, THE EXPOSURE SHOULD BE KEPT TO THE SHORTEST PRACTICAL PERIOD OF TIME AS APPROVED BY THE ENGINEER. LAND SHOULD NOT BE LEFT EXPOSED DURING THE WINTER MONTHS.
- 3) LIMIT OF MAXIMUM AREA OF EXPOSED SOIL AT ANY ONE TIME TO LESS THAN 5 ACRES. THE EXPOSED AREA THAT IS BEING ACTIVELY WORKED DURING WINTER IS TO BE LESS THAN 3 ACRES DURING THE WINTER SEASON.
- 4) ALL PERMANENT STORM WATER STRUCTURES SHALL BE STABILIZED PRIOR TO DIRECTING FLOW INTO THEM. AN AREA SHALL BE CONSIDERED STABLE IF ONE OF THE FOLLOWING HAS OCCURED:
 A) BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED.
 B) A MINIMUM OF 85 PERCENT VEGETATED GROWTH HAS BEEN ESTABLISHED.
 C) A MINIMUM OF 3 INCHES OF NON-EROSIVE MATERIAL SUCH AS STONE OR RIP-RAP HAS BEEN INSTALLED.
- D) OR, EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.
 5) SILT FENCE SHALL BE INSTALLED AND MAINTAINED DURING AND AFTER DEVELOPMENT TO REMOVE SEDIMENT FROM RUNOFF WATER AND FROM LAND UNDERGOING DEVELOPMENT. WHERE POSSIBLE, NATURAL DRAINAGE WAYS SHOULD BE UTILIZED AND LEFT OPEN TO REMOVE EXCESS SURFACE WATER. SILT FENCE TO BE MAINTAINED AND CLEANED UNTIL ALL SLOPES HAVE A HEALTHY STAND OF GRASS.
- 6) ALL DISTURBED AREAS AND SIDE SLOPES WHICH ARE FINISHED GRADED, WITH NO FURTHER CONSTRUCTION TO TAKE PLACE, SHALL BE LOAMED AND SEEDED WITHIN 72 HOURS AFTER FINAL GRADING. A MINIMUM OF 4" OF LOAM SHALL BE INSTALLED WITH NOT LESS THAN ONE POUND OF SEED PER 50 SQUARE YARDS OF AREA. THE SEED MIX SHALL BE AS DESIGNATED BELOW.
- 7) ANY DISTURBED AREAS WHICH ARE TO BE LEFT TEMPORARILY, AND WHICH WILL BE REGRADED LATER DURING CONSTRUCTION SHALL BE MACHINE HAY MULCHED AND SEEDED WITH RYE GRASS TO PREVENT EROSION. THE MAXIMUM LENGTH OF TIME FOR THE EXPOSURE OF DISTURBED SOILS SHALL BE 45 DAYS. HAY OR STRAW MULCH SHALL BE APPLIED TO ALL FRESHLY SEEDED AREAS AT THE RATE OF 2 TONS PER ACRE. BALES SHALL BE UNSPOILED, AIR DRIED, AND FREE FROM WEED, SEEDS AND ANY COARSE MATERIAL.
- 8) DURING GRADING OPERATIONS INSTALL HAY BALE BARRIERS ALONG TOE OF SLOPE OF FILL AREAS WHERE SHOWN. BARRIERS ARE TO BE MAINTAINED UNTIL DISTURBED AREAS ARE PAVED OR GRASSED.
- 9) THE FILL MATERIAL SHALL BE OF APPROVED SOIL TYPE FREE FROM STUMPS, ROOTS, WOOD, ETC. TO BE PLACED IN 12" LIFTS OR AS SPECIFIED. BULLDOZERS, TRUCKS, TRACTORS, OR ROLLERS MAY BE USED FOR COMPACTION BY ROUTING THE EQUIPMENT TO ALL AREAS OR EACH LAYER.
- 10) AVOID THE USE OF FUTURE OPEN SPACES (LOAM & SEED) WHEREVER POSSIBLE DURING CONSTRUCTION. CONSTRUCTION TRAFFIC SHALL USE THE ROADBEDS OF FUTURE ROADS.

TEMPORARY EROSION CONTROL MEASURES:

- 1) THE SMALLEST PRACTICAL AREA OF LAND SHALL BE EXPOSED AT ANY ONE TIME.
- 2) HAY BALE BARRIERS AND SEDIMENT CONTROL FENCE SHALL BE INSTALLED AS REQUIRED. BARRIERS AND FENCE ARE TO BE MAINTAINED AND CLEANED UNTIL ALL SLOPES HAVE A HEALTHY STAND OF GRASS.
- 3) BALED HAY AND MULCH SHALL BE MOWINGS OF ACCEPTABLE HERBACEOUS GROWTH, FREE FROM NOXIOUS WEEDS OR WOODY STEMS, AND SHALL BE DRY. NO SALT HAY SHALL BE USED.
- 4) FILL MATERIAL SHALL BE FREE FROM STUMPS, WOOD, ROOTS, ETC.
- 5) STOCKPILED MATERIALS SHALL BE PLACED ONLY IN AREAS SHOWN ON THE PLANS. STOCKPILES SHALL BE PROTECTED BY HAY BALE BARRIERS AND SEEDED TO PREVENT EROSION. THESE MEASURES SHALL REMAIN UNTIL ALL MATERIAL HAS BEEN PLACED OR DISPOSED OFF SITE.
- 6) ALL DISTURBED AREAS SHALL BE LOAMED AND SEEDED. A MINIMUM OF 4 INCHES OF LOAM SHALL BE INSTALLED WITH NOT LESS THAN ONE POUND OF SEED PER 50 SQUARE YARDS OF AREA.
- 7) SEED MIX SHALL BE EQUAL PARTS OF RED FESCUE (CREEPING), KENTUCKY BLUE GRASS, REDTOP, PERENNIAL RYEGRASS.
- 8) AFTER ALL DISTURBED AREAS HAVE BEEN STABILIZED, THE TEMPORARY EROSION CONTROL MEASURES ARE TO BE REMOVED.
- 9) PAVED ROADWAYS MUST BE KEPT CLEAN AT ALL TIMES.
- 10) ALL CATCH BASIN INLETS WILL BE PROTECTED WITH INLET PROTECTION.
- 11) ALL STORM DRAINAGE OUTLETS WILL BE STABILIZED AND CLEANED AS REQUIRED, BEFORE THE DISCHARGE POINTS BECOME OPERATIONAL.
- 12) ALL DEWATERING OPERATIONS MUST DISCHARGE DIRECTLY INTO A SEDIMENT FILTER AREA.

13) TO PREVENT TRACKING OF SEDIMENT ONTO THE EXISTING ROADS, ALL CONSTRUCTION TRAFFIC CAN ONLY EXIT THE SITE OVER THE CONSTRUCTION ENTRANCES SHOWN ON THIS PLAN.

PROPOSED RETAIL MOTOR FUEL OUTLET 2255 LAFAYETTE ROAD PORTSMOUTH, NH 03801	FUEL OUTLET	2255 LAFAYETTE ROAD	PORTSMOUTH, NH 03801
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VGC

<u>vgc</u>	VERTICAL GRANI
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G	GAS LINE
U/C&T	UNDERGROUND
w	WATER LINE
E	UNDERGROUND
	CHAIN LINK FE
	CONTOUR ELEV
•	TREE
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0	CLEANOUT
S	SEWER MANHOL
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*80	WATER SHUT OF
0	BOLLARD
GM	GAS METER
\$	LIGHT POLE
QQQQQQQQ	WETLAND LINE
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	ZONE LINE

NITE CURB LINE WHITE COMM ELECTRIC INCE ATION ANHOLE FF PERTY LINE





((SLOPES LESS THAN 4:1)		LBS
EPING RED FESCUE		
ENNIAL RYEGRASS		
TOP		-

G P Engineering Design Planning Construction Management 603.893.0720 GPINET.COM Greenman-Pedersen, Inc. 44 Stiles Road, Suite One Salem, NH 03079										
PREPARED FOR GRANITE STATE CONVENIENCE, LLC 25 SPRINGER ROAD HOOKSETT, NH										
PROPOSED RETAIL MOTOR FUEL OUTLET 2255 LAFAYETTE ROAD PORTSMOUTH, NH 03801										
PROPERTY OF NEW HAMOS N. DORY N. MASON No. 17099 CENSED N. MASON No. 17099 CENSED N. MASON N. CENSED N. MASON N. CENSED N. MASON N. CORY N. CORY										
	REVIS	SIONS								
3	REV. PER	TAC	5/10/22							
2	MISC. REVI	SIONS	4/19/22							
NO.	COMME	NTS ON	DATE							
	JANUARY	26, 202	22							
	VN/DESIGN BY	CHEC	KED BY							
LANDSCAPE PLAN										
SCALE: 1"=30'										
PROJECT NO. NEX-2021163										
NEX-2021163 8 OF 15										













NOT TO SCALE









VGC	VERTIC
SSLW	SINGLE
G	GAS L
	UNDEF
w	WATER
E	UNDEF
0	CHAIN
	CONTO
« Ø	TREE
5 C	UTILITY
<	GUY W
······	OVERH
	TREEL
	SIGN
×30.0°	SPOT
	CATCH
0	CLEAN
S	SEWER
Ū	TELEPI
# <u>S</u> o	WATER
0	BOLLA
GM	GAS M
¢	LIGHT
o	WETLA
· · · · · · · · · · · · · · · · · · ·	EASEM
·	PROPE
	ABUTT
	ZONE

CAL GRANITE CURB E SOLID LINE WHITE LINE RGROUND COMM LINE RGROUND ELECTRIC LINK FENCE OUR ELEVATION Y POLE WIRE HEAD WIRE INE ELEVATION BASIN TUON MANHOLE HONE MANHOLE SHUT OFF RD **IETER** POLE AND LINE MENT LINE ERTY LINE TER PROPERTY LINE LINE







							~																								Ž						
а ал		۵0°	É			S	556°2	29'08"	W																				2	80.00	8 8 3 3						
		400																			ō.o	Ō.0									N33						
						4					ð.o	ō.0	Ō.0	Ō.0	ō.0	Ö.0	ō.o	ō.o	ō.o	ō.0	ō.o	Ō.0	Ō.0	ō.0													
									Ō.0	Ō.0	0.0	Ō.O	ō.o	Ō.0	ō.0	ō.0	ò.o	0.0	ō.o	0.0	ð.o	Ō.0	Ō.0	0.0	ō.0	ō.0					Ŷ						
							0.0	ò.o	ō.o	Ö.0	ō.o	ō.o	0.0	0.0	0.0	ō.0	مة. NÅI	P [°] 2	72	LÕ	Т ^{6.0}	0.0	0.0	ō.o	ō.o	ò.o	ō.o	ō.0	Ō.0	0.0							
					0.0	ō.o	0.0	0.0	0.0	0.0	Ō.O	ō.o	0.0	0.0	ð.0	^{0.0} 1	11,99 2.571)8 \$9. Ac.±	Ft ^{ð.1}	0.1	0 .1	0.1	Ö.1	ò.o	ò.o	0.0	ò.o	0.0	ð.o	0.0	ō.o	ò.o	Ö.0				
			÷.	0.0 +	0.0 +	ŏ.o	0.0	0.0 +	0.0	0.0 +	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1	ò.1	0.1	0.1	0.1	0.1	0.1	ò,1	ò.o	0.0	0.0 -	0.0	0.0	ō.0	ō.0	0.0 +	0.0	0.0		
			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,1	0.1	0.1	0.1	0.0	0.1	0,1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.1	ò.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
		† .0	0.0	0.0 ħ.n	0.0	0.0 5.0	0,0	0.0	0.1	0.1 "h.2	0.1 ñ.2	0.1	0.1	0.0	0,1	0.1	0.1 č.a	0.2	0.3 Ö.7	0.5 * 7	0.8	0.9	0.7 be	0.4	0.2 õe	0.1	0.1 "o 4	0.0	0.0	0.0	0.0	0,0	0,0	0.0	0.0	0.0	
		0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.2	0.2	0.2 0.4	0.2	0.1 Ř.1	0.2	0.2	0.2	0.3	0.7	3.2	3.1 4.0	3.0 4.9	2.0 3.8	1.4 2.9	1.0	0.2	0.1	0.0	0.0	0.0	0.0 0.0	0.0 0.0	0.0	0.0 ň n	0.0 ħ.0	0.0	
		ō.0	0.0	0.0	ō.o	0.1	0.1	0.1	0.4	0.5	0.6	1.1	2.2	0.1	[*] 2.6	1.4	0.8	1.2	3.0	5.7	6.14	• 7.1	÷.3	5.4	2.1	0.7	0.2	0.1	±0.0	0.1	ō.1	0.0	0.0	0.0	[†] 0.0	ō.0	0.0
		ō.0	ō.0	ō.o	ō.o	Ö.1	0 .3	0.5	0.7	0.9	1.3	2.5	3.3	⁺ 4.6	3.7	2.0	1.7	1.7	3.3	5.7	B 7.9	8.0	6.1	5.5	24	1.1				0.2	0.1	[†] 0.0	[†] 0.0	0.0	0.0	[†] 0.0	0.0
		ō.0	. 0.0	[†] 0.0	ō.o	0.2	Ò.5	1.0	1.4	1.6	2.2	5 .0	4.9	7.1	3 5.7	5.7	3.0	1.9	[∓] 3.0	6.6	⁻ 6.5	5.5	[†] 7.4	5.5	- 23	1.3	0.9	0.8	 0.9	0 .6	0 .2	0.1	ō.o	ō.o	Ō.0	ō.0	ō.o
		ō.0	ō.o	0.0	0.1	0 .3	1.2	[‡] .2	JES -	2.3	2.8	5.7	6.1	[*] 8.2	В 7.5	5.8] 3.4	⁺ 2.1	[*] 3.4	4.2	, 3.3	3.6	⁻ 3.3	[*] 4.2	3.0	[*] 2.1	2.4	[‡] 1.8	⁻ 2.0	1.9	0 .4	0 .1	ò.1	ō.0	0.0	ð.o	ò.o
		0.0	Ö.0	0 .1	Ö.1	Ö.4	1.8	3.4	4.6	3 .1	[‡] 2.7	[‡] 5.2	7.4	6.1	7.0	6.6	⁻ 3.1	∋ ^{^{2.0}}	⁺ 2.3	2.2	2.3	2.2	⁺ 2.2	[*] 2.3	[*] 2.4	2.5	- 4.0	5.0	5.0		Ö.6	[†] 0.1	ō.1	0.0	ō.o	0.0	ō.0
		ō.o	· 0.0 ·	ŏ.1	0.2	Ö. 7	ž.9	7.3	6.2	^{3.8}	<u></u> 3.1	4.8	42	⁺ 4.2	<u>3.9</u>	4.7	<u></u> 3.6	上 山1.8 一	1.2	1.2	1.5	1.7	1.5	1.5	1.8	2.6	⁻ 3.2	6 .7	5.4	4.3	Ö.8	ò.2	ō.1	0.1	ō.o	0.0	ō.0
	ō.o	ō.o	ō.0	0.1	ð.2	1.0	5.0	12.3 27	6.6	4.1	2.9	2.9	2.5	2.7	2.6	2.6	2.6	1.6	1 .0	[†] 0.8	0.9	[†] 1.0	[†] 1.0	1.2	1.8	2.7	3.4	4.6	7.0		1.3	0.3	[†] 0.1	ō.o	ō.0	ō.o	ō.o
	0.0	ō.0	0.0	0.1	0.3	1.0	5.8	D 11.2	[*] 7.0	4.0	2.1	b. 6									-0.6 	ō.7	0.7	1.0	1.6	2.6	3.2	5.4	≤ ^{7.4} Å	⁺ 4.9	[†] .0	0 .3	Ō.1	0.1	ō.o	0.0	ö.o
	0.0	0.0	ō.0	0.1	0.2	0.9	÷.5	8.4	6.4	3.8	.7										0 .5	0.6	0.5	ō.8	1.3	2.2	[‡] 3.9	6 .5	₹ <u>5.2</u>	5.1	0 .7	[†] 0.2	Ö.1	ō.1	[†] 0.0	b.o	0.0
	0.0	Ô.0	0.0	[‡] 0.1	ō.2	0.6	2.2	[‡] 4.5	5.2	3.1	.5										ò.7—	1.0 	1.1	1.1	1.2/°	2.2	3.6	3.3	()3.3 Z	3.1	0.6	ð.1	ò.1	ò.o	0.0	0 .0	0.0
	0.0	ō.0	0.0	0.1	Ö.1	ð.5	1.8	3.1	3.7	[*] 2.2	.4										2:0	3.2 	3.7	2.7	8	1.7	2.1	2.0		1.4	0.5	0.1	ð.1	ō.o	ō.o	ō.0	ō.o
	Ō.O	[†] 0.0	ō.0	0.1	Ö.1	0.6	1.7	[‡] .3	⁻ 2.5	2.4	2.0										3.7	4.2	4.9	97	³ .1	1.9	2.1	2.6	2.1	1.3	0.4	0.1	0.1	ō.o	0.0	0.0	ō.o
	0.0	ō.o	0.1	0,1	Ö.1	0.9	3.3	3.4	3.6	3.7	 		JJ	h	L		_p		- ega	ц ц	6.5	⊂ 6 63	₹.2 В	5.2	5.4	2.7	2.9	4.3	[*] 3.2	1.8	0.5	0.1	0.1	0.0	[†] .0	0.0	0.0
	0.0 *	0.0	0.1	0.1	0.2	1.1	5,4	5.3	6.5	3.7	2.2	1.1	0.7	0.5	0.5	0.5	0.5	0.8 • • • • • •	1.5 	3.5	5.8 ¹	8.2	8.4	6.0	5.7	3.2	4.0 + ▲	6 .0	6.2	2.4	0.6	0.2	0.1 +	ō.o	ò.o	ō.0	ō.0
	0.0	0.0	0.1	0.2	0.3	1.8 1 5.0 A	5.2	7.6	5.2	3.0 	2.5	1.5	0.9	0.7	0.6	0.6	0.6	0.8	15	3.2	6.9	6.7	5.9 ⁺	7.7	* 5 .4	3.4	4.4	6.5	11.5	4.3	0.8	0.2	0.1	0.0	0.0	0.0	0.0
	υ.υ 	0.0	0.0 Å 1	0.2 10.2	0.4 ñ.3	2.3	o.o + 4.7	7.1 5.8	4.1	3.9 3.4	2.0 3.0	1.9 23	12	1.0	1.7	16	<u>17</u>	10	1 8 *2.5	3.8 - 3.4	4./	4.0	4.2	4.0	4.8 *2 0	3.5	4.3	0.0 4 A	9.7 29	5.5	0.1	0.0	0.0	0.0	0.0	0.0	0.0 *.0
	0.0 0.0	0.0 0.0	0.1	÷.1	ō.2	1.1	-5,2	5.2	5.6	5.1	[*] 4.1	⁻ 3.8	[*] 3.7	· 3.7	3.7	3.8	3.7	[‡] 4.0	4.3	4.3	4.4	4.4	3.1 [‡] 4.1	2.0 3.0	2.3 2.1	ž.4	4.1	5.7	5.2	2.1	0.7 0.5	0.1	0.1	ō.o	ō.o	0.0 Ō.0	0.0
	Ö.0	0.0	[†] 0.1	⁺ 0.1	[†] 0.1	0.7	+2.3	[‡] 2.6	3.9	8.8 1	6 ¹ 3.7	16.9 ₁	7 16.8,	a ¹ 17.5	17,7	17.0	17.1	17.4	17.9	17.5	17.0	, ¹ 7.4	13.7	* 8.3	3.5	±.0	 3.0	[‡] 4.1	- 3.0	1.5	Ď.3	0.1	0.1	ö.o	0.0	[†] 0.0	ů.0
	0.0	0.0	⁺ 0.1	⁺ 0.1	0.1	[†] 0.5	+ + ,	1.7	4.6	25	2 33 42	44 38	2 <u> </u>	2 	19 	20 	3 48 4	21 C2 5 40 45	22 CZ 40 45	2 	3 2 9 <u>2 (</u> : 44 40	24 52 42 44	25 	20	5.2	[*] 2.0	2.2	2.2	[†] 1.7	ō.8	0.2	[†] 0.1	[†] 0.1	ō.o	[‡] .0	.0	[*] 0.0
	⁺ 0.0	[†] 0.0	0.0	0.1	0.1	0.4	[.] 0.8	1.5	⁺ 4.6	27 27	43 -46	56 44 56 54	47 47 45 52	49 58 B	49 4 57 4	7 47 54 9 47 57	4 7 8 9 5	0 48 48 8 54 46	48 56 54 68	45 ⁵⁶	46 46 46 48	48 56	42 32 50 38	21 19	[‡] 5.3	[‡] 2.0	[†] 1.8	1.4	[†] 1.0	0.5	Ō.2	0.1	0.0	⁺ 0.0	ō.0	[†] 0.0	.0 0.0
	0.0	ig p	0.0	0,1	¹ 0.1	0.3	0.9	[†] 1.7	⁺ 3.7	24 15	39 31 4+	44 53	39 50	48	49 4 5 44 2	4 42 44 9 28 44 11	8 1 5 2 46 4	3 52 38 5 38 26	53 36 45 13	42 49 45 41	141 44 27 29	1 47 4 7 244 4 7 19	39 37 39 37	16 12	[‡] 3.8	⁺ 2.0	[†] 1.9	1.4	[‡] 0.8	[†] 0.4	0.2	[†] 0,1	[†] 0.0	⁺ 0.0	[†] 0.0	0.0	[†] 0.0
	0.0	08'37	[†] 0.0	0.1	0.1	0.4	1.4	[‡] 2.7	3.7	5.3	C1 31.2	35.1	C1 (15.5	35.8	C 33.5	1 C1 20.9	[‡] 36.4	C1 26.9	C1 31.5	³ 6.1	C1 16.1	C1 34.2	C 32.2	5.1	[‡] 2.0	2.4	3. 0	¹ .9	1.0	[†] 0.4	.1	0.1	[*] 0.0	Ō.0	0.0	[†] 0.0	0.0
	0,0	\$ 833 833	[†] 0.0	0.1	0.1	0.5	÷.8	[⁺] 3.5	[⁺] 5.0	4.5	9.0	10.9	6.7	[‡] 11.0	[*] 9.7	7.4	11.8	7.8	8.9	11.5	[*] 6.7	10.3	9.3	[*] 3.0	2.2	[‡] 3.6	[*] 4.4	⁺ 3.0	¹ .5	Ö.4	0.1	0.1	0.0	ō.0	0.0	0.0	0.0
	0,0	0,0	0.0	0.1	0.2	[†] 0.7	* 2.9	[*] 7.3	[†] 6.2	⁺ 4.0	[*] 2.5	⁷ 2.1	[*] 2.0	[‡] 2.0	[‡] 2.1	2.1	2.0	2.1	[*] 2.1	2.0	[*] 2.0	2.0	[†] 1.9	[*] 1.7	[*] 2.6	[†] 6.2	[*] 6.6	⁺ 4.0	¹ .5	^{0.2}	Ö.1	0.1	0.0	Ō.0	[†] 0.0	0.0	0.0
	[*] 0.0	0.0	0.0	⁺ 0.1	0.2	0.9 2	5.0 26	[†] 12.4	[*] 6.5	[*] 3.8	1.6		0.8				 0.8	[†] 0;8			⁰ .8		1.0	1.4	3.3	[‡] 7.4	[‡] 10.8	4.9		^{0.2}) 0.1	0.1	[†] 0.0	0.0	0.0	[†] 0.0	[‡] 0.0
	Ö.0	Ō.0	ō.0	Ö.1	0.2	i.o	5.7	11.4	[‡] 6.7	3.5	İ.4	0.7	Ö.4	0.4	ō.4	Ö.4	ö.4 ∏	0.4	Ö.4	0 .4	Ö.4	0.5	Ö. 7	1.7	⁺ 4.4	[*] 6.7	9.9	₩5.7 3	1.0	Ö.2	Ö.1	Ö.0	Ö.0	Ö.O	ō.0	Ö. 0	ō.o
	0.0	Ŏ.0	ō.o	Ö.1	ð.2	0. 8	3.4	[*] 8.2	6.1	⁻ 3.4	1.2	0.5	⁰ .3	0.2	0.2	ō.2	. <u>0</u> .2	0.2	ò.2	0.2	0.2	Ö.3	0.7	+1	5.5	7.2	8.2	3.8	Ö.6	Ö.0	ò.1	ō.o	0.0	Ō.0	ō.0	0.0	ō.0
	Ö.0	0.0	ō.o	0.1	ð.1	0.5	2	4.1	⁺ 4.9	2.7	ð.9	ð.3	0.2	0 .1	Ö.1	ð.1	Ö.1	Ö.1	Ö .1	Ö.1	[†] .2	0 .3	ō.7	1.9	⁺ 4.4	4.7	2.8	1.5	0.3	ð.1	Ō.1	0.0	ð.0	Ō.0	ō.0	0.0	0.0
	Ö.0	0.0 €			- <u>ð.1</u>	280,Ø	0' 1.4	2.6		1.7	$\mathbf{\mathbf{x}}$	- .3-											- 0.7	1.6	2.6	2.7		++	8.1 N5	6°29'0	0.0)8"E ,	0.0		- Ö.0	-0.0	ð.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.2 	0.6	1.1	1.4	1.1	 * .	0.2~ t.a	<u>-0.1</u>	<u>0.1</u>	<u>0.1</u>	<u>0.1</u>	<u>0.1</u>	<u>0,1</u>	0.1	0.1	0.2	-9.5	0.6	1.0	1.1 	1.1	0.6	0.2		0.0	0.0 	0.0	0.0	0.0	0.0	Ö.0	0.0
	0.0	0.0 t.o	0.0	0.0	0.0	0.1	0.3	0.5 t.c	0.7		0.4	0.2	0.1	0.1	0.0	0.0	0.0	0.1 5.c	0.1	0.1	0.2	0.3	0.4	0.5	0.5	0.4 t. c.	0.2	0.1 t.a	0.0	0.0-	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		0.0	0.0	0.0	0.0	0.1 5.0	0.1 5.4	0.2	0.3	0.4	0.3	0.1 5 4 1	0.1 I 224 P	0.1 	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3 5.4	0.2	0.2	- 0.1 too	0.0 ħ.o	0.0 5.0	0.0	0.0 5.0	0.0 5.0	0.0 5.0	0.0 ឯក	0.0 ħ.o	0.0 bo	
		0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.1	0,2 0,1	0.1	0.1	*.1 (LAN (PUBI	- /X) _IÇ	(💾 66¦± \	I I'E NIDE	: K (R _b Q.'	U'AI ₩ _₽ ⟩₀	プ:【t ホ₀	اש> 1	ا ('U)0.1	0.1 0.1	0.1	ō.1	0.0	0.0 0.0	0.0	ō.o	0.0 5 A	0.0 0.0	0.0 to 0	0.0	0.0 ħ.o	0.0	
		÷.,0	÷.0	0.0	[†] 0.0	. 0.0	0.0	0.0	0.1	 Ö.1	0.1	[*] 0.1	0,1	, [†] 0,0	÷	0,0	÷0	0.0	÷0	0.0	[*] 0.0	0.0	0.0	0.0	0.0	ô.0	0.0	÷0	ō.o	[†] 0.0	[*] 0.0	ð.o	[†] 0.0	0.0	÷		
				[†] 0,0	0.0	0,0	⁺ 0.0	0.0	0.0	[†] 0.0	[*] 0.0	[†] 0.0	[†] 0.0	.0 [*]	÷ 0.0	[†] 0.0	⁺ 0.0	[†] 0.0	[‡] 0.0	[†] 0.0	[‡] 0.0	[†] 0,0	[†] 0.0	0.0	.0 [*]	⁺ 0.0	0.0	[†] 0.0	[*] 0.0						знте	ON	
HARP	FACE	LIGH	ITINC	3 —			0.0	0.0	0.0	0 .0	0.0	0.0	0.0	[*] 0.0	Ō.0	Ō.0	[†] 0.0	.0	0.0	[†] 0.0	[†] 0.0	0.0	0.0	[†] 0.0	[†] 0.0	0 .0	0.0	[†] 0.0	0.0								ч I V \
	(SE		AIL)									°0.0	[†] 0.0	[†] 0.0	[†] 0.0	0.0	⁺ 0.0	[†] 0.0	[†] 0.0	[†] 0.0	0.0	. 0	[†] 0.0	[†] 0.0	[†] 0.0	0.0	0.0	0.0					e SC	FIEDI		



				31	⁺ 31	30	⁺ 28
f	-32 -	32 -	33	34	-+ 	⁺ 32	⁺ 30
	34	-34	35	35	-34-	⁺ 34	⁺ 32
	-+- 40	39	38	⁺ 37	⁺ 35	34	⁺ 33
	+ 41	4 0	39	⁺ 37	⁺ 36	35	34
	+ 41	4 0	⁺ 39	⁺ 37	⁺ 35	34	33
	39	⁺ 38	37	36	⁺ 35	34	⁻ 33
	37	⁺ 36	36	35	⁺ 34	34	33
	35	⁺ 35	⁺ 34	⁺ 33	⁺ 33	33	32
	34	⁺ 33	⁺ 33	⁺ 32	⁺ 31	31	31
	33	⁺ 33	32	31	30	30	30
	<u> </u> + 34	- 32	-32	- 31	- 3 0	30	/

HARP FACE VERTICAL LIGHTING DETAIL SCALE: $\frac{1}{2}$ " = 1 '

LIGHTING IS REGULATED BY LOCAL ORDINANCES

FOOTCANDLE LEVELS CALCULATED AT GRADE USING INITIAL LUMEN VALUES											
LABEL	AVG	MAX	MIN	AVG/MIN	MAX/MIN						
IRVING HARP FACE (VERTICAL)	33.88	41	28	1.21	1.46						
PAVED AREA	4.78	36.4	0.5	9.56	72.80						
UNDEFINED	0.35	7.1	0.0	N.A.	N.A.						
UNDER CANOPY	42.73	58	12	3.56	4.83						

NOTE: - ALL AREA LIGHTS ON NEW 17 FT. POLE MOUNTED ON 2-1/2 FT. CONCRETE BASE

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LUMINAIRE SCHEDU	MINAIRE SCHEDULE												
SYMBOL	QTY	LABEL	ARRANGEMENT	LUMENS	LLF	BUG RATING	WATTS/LUMINAIRE	TOTAL WATTS	MANUFACTURER	CATALOG LOGIC			
	2	А	SINGLE	16998	1.030	B2-U0-G3	132	264	Cree Inc	OSQ-ML-B-DA-XX + OSQL-B-22L-57K7-4M-UL-NMXX + OSQ-BLSLF			
	3	В	SINGLE	22098	1.030	B3-U0-G3	132	396	Cree Inc	OSQ-ML-B-DA-XX + OSQL-B-22L-57K7-4M-UL-NM-XX			
	10	C1	SINGLE	12862	1.030	B2-U1-G1	141	1410	RUUD LIGHTING, INC., A CREE COMPANY	CAN-304-AF-RS-06-E-UL-WH-700-57K			
	10	C2	SINGLE	13251	1.030	B3-U0-G1	134	1340	CREE, INC.	CAN-304-SL-RS-06-E-UL-XX-700-57K			
	4	D	Single	17499	1.030	B2-U0-G3	132	528	Cree Inc	OSQ-ML-B-DA-XX + OSQL-B-22L-57K7-3M-UL-NM-XX + OSQ-BLSLF			

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LUMINAIRE LOCA	ATION SUMMARY	
LUM NO.	LABEL	MTG. HT.
1	Α	19.5
2	Α	19.5
3	В	19.5
4	В	19.5
5	В	19.5
6	C1	14.5
7	C1	14.5
8	C1	14.5
9	C1	14.5
10	C1	14.5
11	C1	14.5
12	C1	14.5
13	C1	14.5
14	C1	14.5
15	C1	14.5
16	C2	14.5
17	C2	14.5
18	C2	14.5
19	C2	14.5
20	C2	14.5
21	C2	14.5
22	C2	14.5
23	C2	14.5
24	C2	14.5
25	C2	14.5
26	D	19.5
27	D	19.5
28	D	19.5
29	D	19.5

THIS SITE IS LOCATED IN A REGION WHERE

SCALE: LAYOUT BY: 1" = 30' JSG DWG SIZE: DATE: 1/10/22 D

IRVING OIL GRANITE STATE C-STORE DRAWING NUMBER: RL-7838-S1











USE OF, INSTALLATION OF AND/OR INTEGRITY OF EXISTING BUILDING(S), SURROUNDING AREA FOR PRODUCT(S) SUCH AS EXISTING POLE(S), ANCHOR BOLT(S), BASE(S), ARCHITECTURAL AND SIGNAGE STRUCTURE(S), LANDSCAPING PLAN(S), LIGHTING PLAN(S), FIXTURE SELECTION(S) AND PLACEMENT, MATERIAL(S), COLOR ACCURACY, TEXTURE(S), AND ANYTHING ATTRIBUTED TO PHOTO REALISM THAT IS CREATED. FURTHERMORE, RED LEONARD ASSOCIATES INC., DOES NOT ASSUME LIABILITY WHATSOEVER FOR ANY PURCHASES MADE BY CLIENT BEFORE, DURING, OR AT THE CONCLUSION OF THE PUBLISHED WORK. THE CUSTOMER, ITS RELATIVE AFFILIATES, AS WELL AS ANY OTHER PERSON(S) IN VIEWING OF THIS PRODUCT IS RESPONSIBLE FOR VERIFYING COMPLIANCE WITH ANY BUT NOT LIMITED TO ALL CODES, PERMITS, RESTRICTIONS, INSTRUCTIONS, PURCHASES, AND INSTALLATIONS OF OBJECTS VIEWED WITHIN THIS DOCUMENT(S) OR PROJECT(S). SYMBOLS ARE NOT DRAWN TO SCALE. SIZE IS FOR CLARITY PURPOSES ONLY. SIZES AND DIMENSIONS ARE APPROXIMATE, ACTUAL MEASUREMENTS MAY VARY. DRAWINGS ARE NOT INTENDED FOR ENGINEERING OR CONSTRUCTION USE. THIS DOCUMENT, ANY RED LEONARD DRAWING(S), OR PROJECT(S) IS NOT TO BE USED AND/OR INTENDED FOR ENGINEERING OR CONSTRUCTION PURPOSES, BUT FOR ILLUSTRATIVE PURPOSES ONLY. ANY USE OF THIS DOCUMENTATION AND/OR OTHER ARTICLES PRODUCED BY RED LEONARD WITHOUT WRITTEN AUTHORIZATION FROM JAYME J. LEONARD IS STRICTLY PROHIBITED.

IRVING OIL GRANITE STATE C-STORE DRAWING NUMBER: RL-7838-S1

PROJECT NAME:





STORMWATER MANAGEMENT REPORT

PROPOSED RETAIL MOTOR FUEL OUTLET TAX MAP 272 LOT 3 2255 LAFAYETTE ROAD PORTSMOUTH, NEW HAMPSHIRE





44 Stiles Road, Suite One Salem, NH 03079 (603) 893-0720

Prepared For:

Granite State Convenience, LLC



Revised: April 19, 2022 February 3, 2022

(GPI Project No.: NEX-2021163)

Granite State Convenience, LLC Proposed Retail Motor Fuel Outlet Stormwater Management Report

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Drainage Area Plans	Inside Back Cover
Inspection and Maintenance Manual (I&M)	Inside Back Cover

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

SECTION 1

EXECUTIVE SUMMARY

This report contains a stormwater management analysis for the proposed retail fuel development located at 2255 Lafayette Road (Route 1) in Portsmouth, New Hampshire. The analysis includes both pre- and post-development calculations of stormwater runoff rates at specific locations on the project site.

This analysis has been prepared in accordance with both City of Portsmouth requirements and the guidelines contained in the New Hampshire Department of Environmental Services (NHDES) New Hampshire Stormwater Manual.

The project site consists of one parcel identified as Map 272 Lot 3 which totals approximately 2.571 acres. The site is bordered by Lafayette Road (Route 1) to the northwest, commercial properties to the northeast and southwest and wooded areas containing wetlands to the south and southeast.

The applicant is proposing to construct a 4,970 square foot convenience store with food service and drive-thru, a fueling canopy with 5 retail fuel islands and 10 fueling locations, and associated paved driveways and parking. Access to the proposed developed site will be provided by two separate one-way ingress and one-way egress from Lafayette Road. Two underground storage tanks (USTs) will be located along the western site driveway to Lafayette Road. Water and sewer for the proposed building will be provided by municipal services. Electric service will be provided via an existing utility pole on Lafayette Road and a new on-site transformer.

In order to mitigate increases in peak discharge rates of stormwater runoff as a result of the new impervious surfaces, a comprehensive stormwater management system has been designed that includes deep-sump, hooded catch basins, First Defense Hydrodynamic Separators, an oil/water separator, a Jellyfish Filter treatment unit, and an underground detention system with outlet control structure.

Based on site topography and discharge points, one analysis point is identified for the purposes of this analysis. Design Point #1 represents overland flow which flows southeast eventually to an on-site wetland which is part of a larger off-site wetland system.

The table below summarizes the comparative pre- and post-development peak rates of stormwater runoff at the design point.

Design Storm	Pre-Development	Post-Development	Change								
	(cfs)	(cfs)	(cfs)								
DESIGN POINT #1 – Wetland											
2-year	3.5	3.4	-0.1								
10-year	8.1	6.8	-1.3								
25-year	12.0	9.7	-2.3								
50-year	15.8	12.1	-3.7								

TABLE 1: PEAK RATE ANALYSIS SUMMARY

(All values shown are peak rates in CFS)

In conclusion, by incorporating a new on-site drainage system that includes provisions for stormwater treatment and detention, there will be a decrease in the peak rates of stormwater runoff leaving the property at the design point as a result of this project.

Implementing the maintenance procedures outlined in the Inspection and Maintenance Manual (I&M) will ensure the long-term performance of the system.

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

SECTION 2

EXISTING CONDITIONS

The project site consists of one parcel identified as Map 272 Lot 3 which totals approximately 2.571 acres. The site is bordered by Lafayette Road (Route 1) to the northwest, commercial properties to the northeast and southwest and wooded areas containing wetlands to the south and southeast.

The site is previously developed and contains a Burger King restaurant with drive-thru, which is currently vacant, and associated paved parking lot and driveways to Lafayette Road. The majority of the lot is paved and on-site drainage structures are limited to a single catch basin in the landscaped area northwest of the existing building which had no visible pipe outlet at the time of survey. The majority of stormwater runoff currently sheet flows uncontrolled and untreated over the pavement to the southeast eventually off the edge of pavement to the wetland.

Site topography is variable, with slopes ranging from mild (2% on the maintained front lawn) to severe (25% or greater) near the wetland areas. Elevations range from 53 at the southern edge of the property to 67 at the northwest property corner along Lafayette Road.

The NRCS Web Soil Survey identifies on-site soils as Urban Land with no Hydrologic Soil Group (HSG) classification. Areas directly south of the site are identified as Pipestone sand with an HSG-A classification which is used in the analysis.

Test pits were performed by Greenman-Pedersen, Inc. (GPI) on September 30, 2021. Test Pits encountered Loamy Sand with estimated seasonal high groundwater table (ESHWT) encountered at 36 inches below ground in Test Pit 9-1 and not encountered in Test Pit 9-2. Refusal was encountered at 38 inches and 48 inches below ground respectively. Test pit logs are included in Appendix C.

On-site wetlands were delineated by West Environmental, Inc. on July 30, 2021 along the northeast and southeast property lines and are shown on the Existing Conditions Plan with the associated 100-foot wetland buffer.

The site is not located in a special flood hazard area (100-year flood) per Flood Insurance Rate Map Number 33015C0270F, with an effective date of January 29, 2021.

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

SECTION 3

PROPOSED CONDITIONS

The applicant is proposing to construct a 4,970 square foot convenience store with food service and drive-thru, a fueling canopy with 5 retail fuel islands and 10 fueling locations, and associated paved driveways and parking. Access to the proposed developed site will be provided by two separate one-way ingress and one-way egress from Lafayette Road. Two underground storage tanks (USTs) will be located along the western site driveway to Lafayette Road. Water and sewer for the proposed building will be provided by municipal services. Electric service will be provided via an existing utility pole on Lafayette Road and a new on-site transformer.

In order to mitigate increases in peak discharge rates of stormwater runoff as a result of the new impervious surfaces, a comprehensive stormwater management system has been designed that includes deep-sump, hooded catch basins, First Defense Hydrodynamic Separators, an oil/water separator, a Jellyfish Filter treatment unit, and an underground detention system with outlet control structure.

To safeguard against oil or gas introduction into the drainage system, stormwater runoff from areas in which fuel is dispensed will be collected in hooded catch basins with deep sumps and routed through an oil/water separator unit. Such pretreatment of stormwater reduces both suspended solids and oils in the drainage system and is recommended by NHDES. Runoff will then enter an underground detention system consisting of four (4) rows of 36-inch HDPE pipe with watertight joints. This system, together with the outlet control structure, will attenuate peak rates of runoff discharging to the design point during all design storms. Finally, runoff discharging from the detention system will flow through a Jellyfish Filter which uses membrane filters to remove fine particles and particulate-bound pollutants such as nitrogen, phosphorous, metals, and hydrocarbons.

The Jellyfish Filter is performance tested to achieve 89% TSS and 51% total Nitrogen (TN) removal efficiencies, which satisfy the Enhanced Stormwater Treatment Standards described in Section 7.6.2 of the *Site Plan Review Regulations*.

Recharge of runoff from non-high load areas (where petroleum products are not dispensed) was explored but was not possible due to the presence of high groundwater and the nature of the existing topography.

The total area of disturbance related to the proposed redevelopment and stormwater management system construction is approximately 75,000 square feet therefore the project will require an EPA Construction General Permit under the NPDES program. The area of disturbance is less than 100,000 square feet, therefore, the project is not subject to an NHDES Alteration of Terrain (AoT) permit.

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

SECTION 4 STORMWATER MODELING METHODOLOGY

The drainage system for this project was modeled using HydroCAD, a stormwater modeling computer program that analyzes the hydrology, and hydraulics of stormwater runoff. HydroCAD is based largely on the hydrology techniques developed by the Soil Conservation Service (SCS/NRCS), combined with other hydrology and hydraulics calculations. For a given rainfall event, these techniques are used to generate hydrographs throughout a watershed. This provides verification that a given drainage system is adequate for the area under consideration, or to predict where flooding or erosion is likely to occur.

In HydroCAD, each watershed is modeled as a subcatchment, streams and culverts as a Reach (or Pond, depending on available storage capacity), and large wetlands and other natural or artificial storage areas as a Pond. SCS hydrograph generation and routing procedures were used to model both Pre-development and Post-development runoff conditions.

The Pre-development and Post-development watershed limits and the subcatchment characteristics were determined using both USGS and on-the-ground topographic survey information and through visual, on-site inspection. Conservative estimates were used at all times in estimating the hydrologic characteristics of each watershed or subcatchment.

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

APPENDIX A

Figures



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National Flood Hazard Layer FIRMette



Legend



Stormwater Management Report

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

APPENDIX B

Soils Information



United States Department of Agriculture

Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants Custom Soil Resource Report for Rockingham County, New Hampshire



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



	MAP L	EGEND		MAP INFORMATION
Area of In	terest (AOI) Area of Interest (AOI)	8	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:24,000.
Soils	Soil Map Unit Polygons	0	Very Stony Spot	Warning: Soil Map may not be valid at this scale.
~	Soil Map Unit Lines	\$7	Wet Spot Other	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil
Special	Point Features	**	Special Line Features	line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed
	Blowout	Water Fea	Itures Streams and Canals	scale.
×	Clay Spot	Transport ++++	ation Rails	Please rely on the bar scale on each map sheet for map measurements.
◇ ★	Closed Depression Gravel Pit	~	Interstate Highways	Source of Map: Natural Resources Conservation Service
0 0 0	Gravelly Spot	~	Major Roads	Coordinate System: Web Mercator (EPSG:3857)
@ 	Landfill Lava Flow	Backgrou	Local Roads	Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts
<u>له</u>	Marsh or swamp		Aerial Photography	distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.
~ 0	Miscellaneous Water			This product is generated from the USDA-NRCS certified data as
0	Perennial Water			of the version date(s) listed below.
+	Saline Spot			Soil Survey Area: Rockingham County, New Hampshire Survey Area Data: Version 22, May 29, 2020
0 0 0 0	Sandy Spot			Soil map units are labeled (as space allows) for map scales
-	Severely Eroded Spot Sinkhole			1.50,000 of larger.
à	Slide or Slip			14, 2017
ø	Sodic Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Symbol Map Unit Name		Acres in AOI	Percent of AOI					
140B	Chatfield-Hollis-Canton complex, 0 to 8 percent slopes, rocky	5.4	17.5%					
299	Udorthents, smoothed	4.6	14.8%					
314A Pipestone sand, 0 to 5 percent slopes		13.9	44.6%					
699	Urban land	7.2	23.1%					
Totals for Area of Interest		31.1	100.0%					

Map Unit Legend

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate

pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Rockingham County, New Hampshire

140B—Chatfield-Hollis-Canton complex, 0 to 8 percent slopes, rocky

Map Unit Setting

National map unit symbol: 2w82m Elevation: 380 to 1,070 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 145 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Chatfield, very stony, and similar soils: 35 percent Hollis, very stony, and similar soils: 25 percent Canton, very stony, and similar soils: 25 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Chatfield, Very Stony

Setting

Landform: Ridges, hills Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope Down-slope shape: Convex Across-slope shape: Linear, convex Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

Typical profile

Oi - 0 to 1 inches: slightly decomposed plant material

A - 1 to 2 inches: fine sandy loam

Bw - 2 to 30 inches: gravelly fine sandy loam

2R - 30 to 40 inches: bedrock

Properties and qualities

Slope: 0 to 8 percent
Surface area covered with cobbles, stones or boulders: 1.6 percent
Depth to restrictive feature: 20 to 41 inches to lithic bedrock
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 4.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: B Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

Description of Canton, Very Stony

Setting

Landform: Ridges, hills, moraines Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest, nose slope Down-slope shape: Convex, linear Across-slope shape: Convex Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material *A - 2 to 5 inches:* fine sandy loam *Bw1 - 5 to 16 inches:* fine sandy loam *Bw2 - 16 to 22 inches:* gravelly fine sandy loam *2C - 22 to 67 inches:* gravelly loamy sand

Properties and qualities

Slope: 0 to 8 percent
Surface area covered with cobbles, stones or boulders: 1.6 percent
Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural stratification
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: B Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

Description of Hollis, Very Stony

Setting

Landform: Ridges, hills Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope Down-slope shape: Convex Across-slope shape: Linear, convex Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material *A - 2 to 7 inches:* gravelly fine sandy loam

Bw - 7 to 16 inches: gravelly fine sandy loam

2R - 16 to 26 inches: bedrock

Properties and qualities

Slope: 0 to 8 percent
Surface area covered with cobbles, stones or boulders: 1.6 percent
Depth to restrictive feature: 8 to 23 inches to lithic bedrock
Drainage class: Somewhat excessively drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: D Ecological site: F144AY033MA - Shallow Dry Till Uplands Hydric soil rating: No

Minor Components

Freetown

Percent of map unit: 5 percent Landform: Bogs, marshes, depressions, kettles, swamps Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Newfields, very stony

Percent of map unit: 5 percent Landform: Hills, ground moraines, moraines Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Concave Hydric soil rating: No

Walpole, very stony

Percent of map unit: 3 percent Landform: Outwash plains, depressions, depressions, deltas, outwash terraces Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Rock outcrop

Percent of map unit: 2 percent Landform: Ridges, hills Hydric soil rating: Unranked

299—Udorthents, smoothed

Map Unit Setting

National map unit symbol: 9cmt Elevation: 0 to 840 feet Mean annual precipitation: 44 to 49 inches Mean annual air temperature: 48 degrees F Frost-free period: 155 to 165 days Farmland classification: Not prime farmland

Map Unit Composition

Udorthents and similar soils: 100 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents

Properties and qualities

Depth to restrictive feature: More than 80 inches Drainage class: Excessively drained Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None

314A—Pipestone sand, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 9cn2 Elevation: 0 to 2,100 feet Mean annual precipitation: 28 to 55 inches Mean annual air temperature: 45 to 52 degrees F Frost-free period: 100 to 200 days Farmland classification: Not prime farmland

Map Unit Composition

Pipestone and similar soils: 75 percent *Minor components:* 25 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Pipestone

Setting

Landform: Outwash terraces

Typical profile

H1 - 0 to 6 inches: sand *H2 - 6 to 33 inches:* sand

H3 - 33 to 60 inches: sand

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00 to 20.00 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 4.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: A/D Ecological site: F144AY027MA - Moist Sandy Outwash Hydric soil rating: Yes

Minor Components

Not named wet

Percent of map unit: 5 percent Landform: Outwash terraces Hydric soil rating: Yes

Scarboro

Percent of map unit: 5 percent Landform: Depressions Hydric soil rating: Yes

Chocorua

Percent of map unit: 5 percent Landform: Bogs Hydric soil rating: Yes

Deerfield

Percent of map unit: 5 percent Hydric soil rating: No

Squamscott

Percent of map unit: 5 percent Landform: Marine terraces Hydric soil rating: Yes

699—Urban land

Map Unit Composition

Urban land: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Minor Components

Not named

Percent of map unit: 15 percent *Hydric soil rating:* No

Soil Information for All Uses

Soil Properties and Qualities

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

Hydrologic Soil Group

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.





Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
140B	Chatfield-Hollis-Canton complex, 0 to 8 percent slopes, rocky	В	5.4	17.5%
299	Udorthents, smoothed		4.6	14.8%
314A	Pipestone sand, 0 to 5 percent slopes	A/D	13.9	44.6%
699	Urban land		7.2	23.1%
Totals for Area of Interes	st	31.1	100.0%	

Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

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Stormwater Management Report

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

APPENDIX C

Test Pit Logs

TEST PIT DATA

Client: Project Addres Town, State: Job Number: Date: Performed by:	Grani SS: 2255 Portsr NEX- Septe Diane	te State Convenience Lafayette Road nouth, NH -2021163 mber 30, 2021 Pantermoller			
Test Pit No. ESHWT: Refusal:		9-1 >48" 48"	SCS Star Roc	S Soil: ading Water: ats:	Pipestone None None
Depth 0-30" 30-48" 48"	Horizon A B R	Soil Texture Loamy Sand Loamy Sand	Color 10yr 2/2 10yr 4/4	Consistence FR FR	Mottles; Quantity/Contrast
Test Pit No. ESHWT: Refusal:		9-2 36" 38"	SCS Star Roc	5 Soil: nding Water: nts:	Pipestone None None
Depth 0-24" 24-33" 33-38" 38"	Horizon A B C R	Soil Texture Loamy Sand Loamy Sand Loamy Sand	Color 10yr 3/2 10yr 5/8 2.5y 7/4	Consistence FR FR FR	Mottles; Quantity/Contrast @ 36" Distinct

NOTES



Stormwater Management Report

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

Revised: April 19, 2022

APPENDIX D

Pre-Development HydroCAD Computations



2255 Lafayette Road - Portsmouth, NH

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Area Listing (all nodes)

	Area	CN	Description
(a	cres)		(subcatchment-numbers)
(0.683	39	>75% Grass cover, Good, HSG A (100S)
	1.376	98	Paved parking, HSG A (100S)
(0.123	98	Roofs, HSG A (100S)
(0.461	30	Woods, Good, HSG A (100S)
:	2.643	71	TOTAL AREA

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
2.643	HSG A	100S
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
0.000	Other	
2.643		TOTAL AREA

2255 Lafayette Road - Portsmouth, NH

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.683	0.000	0.000	0.000	0.000	0.683	>75% Grass cover, Good	100S
1.376	0.000	0.000	0.000	0.000	1.376	Paved parking	100S
0.123	0.000	0.000	0.000	0.000	0.123	Roofs	100S
0.461	0.000	0.000	0.000	0.000	0.461	Woods, Good	100S
2.643	0.000	0.000	0.000	0.000	2.643	TOTAL AREA	

	2255 Lafayette Road - Portsr	mouth, NH
21163 Pre-Development	Type III 24-hr 2-Year Rain	fall=3.71"
Prepared by Greenman-Pedersen, Inc.	Printed	1/19/2022
HydroCAD® 10.10-5a s/n 01710 © 2020 HydroCAD Software Solutions	S LLC	Page 1

Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 100S: Overland Flow toRunoff Area=2.643 ac56.72% ImperviousRunoff Depth=1.20"Flow Length=179'Tc=6.0 minCN=71Runoff=3.52 cfs0.264 af

Link DP#1: Design Point #1 - Wetland

Inflow=3.52 cfs 0.264 af Primary=3.52 cfs 0.264 af

Total Runoff Area = 2.643 ac Runoff Volume = 0.264 af Average Runoff Depth = 1.20" 43.28% Pervious = 1.144 ac 56.72% Impervious = 1.499 ac

	2255 Lafayette	e Road - Ports	mouth, NH
21163 Pre-Development	Type III 24-hr	10-Year Rair	nfall=5.65"
Prepared by Greenman-Pedersen, Inc.		Printed	1/19/2022
HydroCAD® 10.10-5a s/n 01710 © 2020 HydroCAD Software Solution	ns LLC		Page 5

Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 100S: Overland Flow toRunoff Area=2.643 ac56.72% ImperviousRunoff Depth=2.62"Flow Length=179'Tc=6.0 minCN=71Runoff=8.07 cfs0.577 af

Link DP#1: Design Point #1 - Wetland

Inflow=8.07 cfs 0.577 af Primary=8.07 cfs 0.577 af

Total Runoff Area = 2.643 ac Runoff Volume = 0.577 af Average Runoff Depth = 2.62" 43.28% Pervious = 1.144 ac 56.72% Impervious = 1.499 ac
Summary for Subcatchment 100S: Overland Flow to Wetland

Runoff = 8.07 cfs @ 12.09 hrs, Volume= 0.577 af, Depth= 2.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.65"

Area	(ac) C	N Des	scription		
0.	683 3	39 >75	5% Grass c	over, Good,	, HSG A
1.	376 9	98 Pav	ed parking	, HSG A	
0.	123 9	98 Ro	ofs, HSG A		
0.4	461 3	30 Wo	ods, Good,	HSG A	
2.	643 7	71 We	ighted Aver	rage	
1.	144	43.	28% Pervio	us Area	
1.4	499	56.	72% Imperv	/ious Area	
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.0	12	0.0900	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.71"
1.2	13	0.0540	0.18		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.71"
0.5	51	0.0590	1.70		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
1.5	103	0.0510	1.13		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
5.2	179	Total,	Increased t	o minimum	Tc = 6.0 min

Summary for Link DP#1: Design Point #1 - Wetland

Inflow A	rea =	2.643 ac, 56.7	72% Impervious	, Inflow Depth =	2.62" for	10-Year event
Inflow	=	8.07 cfs @ 12	2.09 hrs, Volum	e= 0.577	af	
Primary	=	8.07 cfs @ 12	2.09 hrs, Volum	e= 0.577	af, Atten=	0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs

	2255 Lafayette	e Road - Ports	mouth, NH
21163 Pre-Development	Type III 24-hr	25-Year Rair	nfall=7.16"
Prepared by Greenman-Pedersen, Inc.		Printed	1/19/2022
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Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 100S: Overland Flow toRunoff Area=2.643 ac56.72% ImperviousRunoff Depth=3.86"Flow Length=179'Tc=6.0 minCN=71Runoff=11.96 cfs0.850 af

Link DP#1: Design Point #1 - Wetland

Inflow=11.96 cfs 0.850 af Primary=11.96 cfs 0.850 af

Total Runoff Area = 2.643 ac Runoff Volume = 0.850 af Average Runoff Depth = 3.86" 43.28% Pervious = 1.144 ac 56.72% Impervious = 1.499 ac

	2255 Lafayette	e Road - Ports	mouth, NH
21163 Pre-Development	Type III 24-hr	50-Year Rair	nfall=8.58"
Prepared by Greenman-Pedersen, Inc.		Printed	1/19/2022
HydroCAD® 10.10-5a s/n 01710 © 2020 HydroCAD Software Solution	is LLC		Page 3

Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 100S: Overland Flow toRunoff Area=2.643 ac56.72% ImperviousRunoff Depth=5.09"Flow Length=179'Tc=6.0 minCN=71Runoff=15.75 cfs1.120 af

Link DP#1: Design Point #1 - Wetland

Inflow=15.75 cfs 1.120 af Primary=15.75 cfs 1.120 af

Total Runoff Area = 2.643 ac Runoff Volume = 1.120 af Average Runoff Depth = 5.09" 43.28% Pervious = 1.144 ac 56.72% Impervious = 1.499 ac

Stormwater Management Report

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

Revised: April 19, 2022

APPENDIX E

Post-Development HydroCAD Computations



2255 Lafayette Road - Portsmouth, NH

21163 Post-Development REV1 Prepared by Greenman-Pedersen, Inc. HydroCAD® 10.10-7a s/n 01710 © 2021 HydroCAD Software Solutions LLC Printed 4/19/2022 Page 2

Area Listing (all nodes)

Area	CN	Description
 (acres)		(subcatchment-numbers)
 0.731	39	>75% Grass cover, Good, HSG A (1S, 2S, 3S, 4S, 6S, 100S)
1.349	98	Paved parking, HSG A (1S, 2S, 3S, 4S, 5S, 6S, 7S, 100S)
0.114	98	Roofs, HSG A (8S)
0.449	30	Woods, Good, HSG A (100S)
2.643	70	TOTAL AREA

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
2.643	HSG A	1S, 2S, 3S, 4S, 5S, 6S, 7S, 8S, 100S
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
0.000	Other	
2.643		TOTAL AREA

2255 Lafayette Road - Portsmouth, NH

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Gibunu Covers (dil Houes)											
HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment				
 (acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers				
 0.731	0.000	0.000	0.000	0.000	0.731	>75% Grass cover, Good	1S, 2S,				
							3S, 4S,				
							6S,				
							100S				
1.349	0.000	0.000	0.000	0.000	1.349	Paved parking	1S, 2S,				
							3S, 4S,				
							5S, 6S,				
							7S,				
							100S				
0.114	0.000	0.000	0.000	0.000	0.114	Roofs	8S				
0.449	0.000	0.000	0.000	0.000	0.449	Woods, Good	100S				
2.643	0.000	0.000	0.000	0.000	2.643	TOTAL AREA					

Ground Covers (all nodes)

21163 Post-Development REV1

2255 Lafayette Road - Portsmouth, NH

Prepared by Greenman-Pedersen, Inc.Printed 4/19/2022HydroCAD® 10.10-7a s/n 01710 © 2021 HydroCAD Software Solutions LLCPage 5

Pipe Listing (all nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)
1	CB1	61.05	60.50	50.9	0.0108	0.012	0.0	12.0	0.0
2	CB2	60.20	59.50	138.6	0.0051	0.012	0.0	12.0	0.0
3	CB3	58.80	57.00	28.8	0.0625	0.012	0.0	12.0	0.0
4	CB4	57.95	57.55	80.7	0.0050	0.012	0.0	18.0	0.0
5	CB5	58.40	58.05	70.4	0.0050	0.012	0.0	18.0	0.0
6	CB6	59.25	58.65	93.9	0.0064	0.012	0.0	15.0	0.0
7	DET	57.00	56.90	3.0	0.0333	0.012	0.0	18.0	0.0
8	DMH1	60.40	59.50	65.9	0.0137	0.012	0.0	12.0	0.0
9	DMH2	57.45	57.35	10.4	0.0096	0.012	0.0	6.0	0.0
10	DMH2	57.95	57.00	29.4	0.0323	0.012	0.0	18.0	0.0
11	DMH3	59.20	58.90	30.5	0.0098	0.012	0.0	12.0	0.0
12	JF	56.40	56.25	12.4	0.0121	0.012	0.0	18.0	0.0
13	OWS	57.10	57.00	7.5	0.0133	0.012	0.0	6.0	0.0

21163 Post-Development REV12255 Lafayette Road - Portsmouth, NH
Type III 24-hr 2-Year Rainfall=3.71"Prepared by Greenman-Pedersen, Inc.Printed 4/19/2022HydroCAD® 10.10-7a s/n 01710 © 2021 HydroCAD Software Solutions LLCPage 1Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: To CB-1	Runoff Area=0.390 ac 61.82% Impervious Runoff Depth=1.45" Tc=6.0 min CN=75 Runoff=0.65 cfs 0.047 af
Subcatchment 2S: To CB-2	Runoff Area=0.206 ac 97.16% Impervious Runoff Depth=3.25" Tc=6.0 min CN=96 Runoff=0.73 cfs 0.056 af
Subcatchment 3S: To CB-3	Runoff Area=0.123 ac 79.43% Impervious Runoff Depth=2.29" Tc=6.0 min CN=86 Runoff=0.33 cfs 0.023 af
Subcatchment 4S: To CB-4	Runoff Area=0.331 ac 90.25% Impervious Runoff Depth=2.84" Tc=6.0 min CN=92 Runoff=1.07 cfs 0.078 af
Subcatchment 5S: To CB-5	Runoff Area=0.172 ac 100.00% Impervious Runoff Depth=3.48" Tc=6.0 min CN=98 Runoff=0.62 cfs 0.050 af
Subcatchment 6S: To CB-6	Runoff Area=0.135 ac 97.82% Impervious Runoff Depth=3.36" Tc=6.0 min CN=97 Runoff=0.48 cfs 0.038 af
Subcatchment 7S: Canopy	Runoff Area=0.081 ac 100.00% Impervious Runoff Depth=3.48" Tc=0.0 min CN=98 Runoff=0.36 cfs 0.023 af
Subcatchment 8S: Roof	Runoff Area=0.114 ac 100.00% Impervious Runoff Depth=3.48" Tc=0.0 min CN=98 Runoff=0.50 cfs 0.033 af
Subcatchment 100S: Overland	d Flow to Runoff Area=1.091 ac 11.63% Impervious Runoff Depth=0.06" Flow Length=416' Tc=8.1 min CN=42 Runoff=0.01 cfs 0.006 af
Pond CB1: CB-1	Peak Elev=61.46' Inflow=0.65 cfs 0.047 af 12.0" Round Culvert n=0.012 L=50.9' S=0.0108 '/' Outflow=0.65 cfs 0.047 af
Pond CB2: CB-2	Peak Elev=60.71' Inflow=0.73 cfs 0.056 af 12.0" Round Culvert n=0.012 L=138.6' S=0.0051 '/' Outflow=0.73 cfs 0.056 af
Pond CB3: CB-3(FD)	Peak Elev=59.33' Inflow=1.05 cfs 0.080 af 12.0" Round Culvert n=0.012 L=28.8' S=0.0625 '/' Outflow=1.05 cfs 0.080 af
Pond CB4: CB-4(FD)	Peak Elev=59.21' Inflow=3.54 cfs 0.269 af 18.0" Round Culvert n=0.012 L=80.7' S=0.0050 '/' Outflow=3.54 cfs 0.269 af
Pond CB5: CB-5	Peak Elev=59.46' Inflow=2.48 cfs 0.191 af 18.0" Round Culvert n=0.012 L=70.4' S=0.0050 '/' Outflow=2.48 cfs 0.191 af
Pond CB6: CB-6	Peak Elev=60.03' Inflow=1.86 cfs 0.141 af 15.0" Round Culvert n=0.012 L=93.9' S=0.0064 '/' Outflow=1.86 cfs 0.141 af
Pond DET: Underground Dete	ention System Peak Elev=58.57' Storage=837 cf Inflow=4.31 cfs 0.349 af Outflow=3.36 cfs 0.349 af

		2255 Lafa	yette Road - Portsmouth, NH
21163 Post-Developm	nent REV1	Type III 2	2-Year Rainfall=3.71?
Prepared by Greenman	-Pedersen, Inc.		Printed 4/19/2022
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Pond DMH1: DMH-1		Peak Elev=6	0.81' Inflow=0.65 cfs 0.047 af
	12.0" Round Culvert n=	=0.012 L=65.9' S=0.013	7 '/' Outflow=0.65 cfs 0.047 af
Dand DMU2, DMU 2		Dook Flov-5	9 99' Inflow-2 54 of 0 260 of
	Primary=0.56 cfs 0.189 af S	econdary=3 05 cfs 0 080	0.00 IIII0w= 3.54 cts 0.209 at
		ccondary=0.00 cr3 0.000	
Pond DMH3: DMH-3		Peak Elev=5	9.71' Inflow=0.86 cfs 0.056 af
	12.0" Round Culvert n=	=0.012 L=30.5' S=0.0098	3 '/' Outflow=0.86 cfs 0.056 af
Pond JF: Jellyfish Filter		Peak Elev=5	7.38' Inflow=3.36 cfs_0.349 af
	18.0" Round Culvert n=	=0.012 L=12.4' S=0.012	1 '/' Outflow=3.36 cfs 0.349 af
Dand OMC: Oil/Matar Ca		Dook Flow	9.711 Inflow-0.56 of 0.190 of
Pond Ows: Oil/water Se	parator	Peak Elev-0	5.71 IIII0W-0.56 cfs 0.189 af
		I-0.012 L-7.5 3-0.013	57 Outilow=0.50 cis 0.169 al
Link DP#1: Design Point	#1 - Wetland		Inflow=3.36 cfs 0.354 af
U			Primary=3.36 cfs 0.354 af
Total Pu	noff Aron = 2642 an Bunof	f Volumo = 0.354 of A	vorago Bunoff Donth - 1 61"
i oldi Ku	44.63% P	ervious = 1.179 ac 5	5.37% Impervious = 1.463 ac

	2255 Lafayette Ro	ad - Portsmouth, NH
21163 Post-Development REV1	Type III 24-hr 10-	Year Rainfall=5.65"
Prepared by Greenman-Pedersen, Inc.		Printed 4/19/2022
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Time span=0.00-30.00 brs. dt=0.02	1 brs 3001 points	

Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: To CB-1		Runo	ff Area=0.	390 ac Tc=6	61.82 .0 min	% Imper CN=75	vious Runc	Runoff off=1.37	Dep cfs	th=2.99" 0.097 af
Subcatchment 2S: To CB-2		Runo	ff Area=0.	206 ac Tc=6	97.16 .0 min	% Imper CN=96	vious Runc	Runoff off=1.13	Dep cfs	th=5.18" 0.089 af
Subcatchment 3S: To CB-3		Runo	ff Area=0.	123 ac Tc=6	79.43 .0 min	% Imper CN=86	vious Runc	Runoff off=0.57	Dep cfs	th=4.08" 0.042 af
Subcatchment 4S: To CB-4		Runo	ff Area=0.	331 ac Tc=6	90.25 .0 min	% Imper CN=92	vious Runc	Runoff off=1.73	Dep cfs	th=4.73" 0.130 af
Subcatchment 5S: To CB-5		Runoff	Area=0.1	72 ac Tc=6	100.00 .0 min	% Imper CN=98	vious Runc	Runoff off=0.95	Dep cfs	th=5.41" 0.077 af
Subcatchment 6S: To CB-6		Runo	ff Area=0.	135 ac Tc=6	97.82 .0 min	% Imper CN=97	vious Runc	Runoff off=0.74	Dep cfs	th=5.30" 0.060 af
Subcatchment 7S: Canopy		Runoff	Area=0.0	81 ac Tc=0	100.00 .0 min	% Imper CN=98	vious Runc	Runoff off=0.54	Dep cfs	th=5.41" 0.036 af
Subcatchment 8S: Roof		Runoff	Area=0.1	14 ac Tc=0	100.00 .0 min	% Imper CN=98	vious Runc	Runoff off=0.77	Dep cfs	th=5.41" 0.051 af
Subcatchment 100S: Overland	d Flow to	Runo Flow Le	ff Area=1. ngth=416	091 ac ′ Tc=8	11.63 .1 min	% Imper CN=42	vious Runc	Runoff off=0.24	Dep cfs	th=0.50" 0.045 af
Pond CB1: CB-1	12.0" Ro	und Culvert	t n=0.012	P L=50.§	eak Ele 9' S=0.	ev=61.69 .0108 '/'	' Inflo Outflo	w=1.37 w=1.37	cfs cfs	0.097 af 0.097 af
Pond CB2: CB-2	12.0" Rou	nd Culvert	n=0.012	P L=138.6	eak Ele 6' S=0.	ev=61.00 .0051 '/'	' Inflo Outflo	w=1.13 w=1.13	cfs cfs	0.089 af 0.089 af
Pond CB3: CB-3(FD)	12.0" Ro	und Culvert	: n=0.012	P L=28.8	eak Ele 3' S=0.	ev=59.53 0625 '/'	' Inflo Outflo	w=1.67 w=1.67	cfs cfs	0.129 af 0.129 af
Pond CB4: CB-4(FD)	18.0" Ro	und Culvert	: n=0.012	P L=80.7	eak Ele 7' S=0.	ev=60.15 .0050 '/'	' Inflo Outflo	w=5.91 w=5.91	cfs cfs	0.454 af 0.454 af
Pond CB5: CB-5	18.0" Ro	und Culvert	: n=0.012	P L=70.4	eak Ele 4' S=0.	ev=60.37 .0050 '/'	' Inflo Outflo	w=4.19 w=4.19	cfs cfs	0.323 af 0.323 af
Pond CB6: CB-6	15.0" Ro	und Culvert	t n=0.012	P L=93.9	eak Ele 9' S=0.	ev=60.69 .0064 '/'	' Inflo Outflo	w=3.24 w=3.24	cfs cfs	0.246 af 0.246 af
Pond DET: Underground Dete	ention Sys	stem Pe	ak Elev=5	9.33' S	torage	=1,459 ci	f Inflo Outflo	w=7.16 w=6.74	cfs cfs	0.583 af 0.583 af

		2	2255 Lafayett	e Road - Portsm	outh, NH
21163 Post-Developm	nent REV1	T_{j}	ype III 24-hr	10-Year Rainfa	all=5.65"
Prepared by Greenman	I-Pedersen, Inc.			Printed 4	/19/2022
HydroCAD® 10.10-7a s/n	<u>01710 © 2021 HydroCAD Sc</u>	oftware Solutions I	LLC		Page 7
Pond DMH1: DMH-1		Pea	ak Elev=61.12	Inflow=1.37 cfs	0.097 af
	12.0" Round Culvert	n=0.012 L=65.9'	S=0.0137 '/'	Outflow=1.37 cfs	0.097 af
Pond DMH2: DMH-2		Pea	ak Elev=59.71	' Inflow=5.91 cfs	0.454 af
	Primary=0.57 cfs 0.282 af	Secondary=5.46	cfs 0.172 af	Outflow=5.91 cfs	0.454 af
Pond DMH3: DMH-3		Pea	ak Elev=59.87	' Inflow=1.31 cfs	0.088 af
	12.0" Round Culvert	n=0.012 L=30.5'	S=0.0098 '/'	Outflow=1.31 cfs	0.088 af
Pond JF: Jellyfish Filter		Pea	ak Elev=57.95	' Inflow=6.74 cfs	0.583 af
	18.0" Round Culvert	n=0.012 L=12.4'	S=0.0121 '/'	Outflow=6.74 cfs	0.583 af
Pond OWS: Oil/Water Se	parator	Pea	ak Elev=59.52	Inflow=0.57 cfs	0.282 af
	6.0" Round Culver	t n=0.012 L=7.5'	S=0.0133 '/'	Outflow=0.57 cfs	0.282 af
Link DP#1: Design Point	: #1 - Wetland			Inflow=6.83 cfs	0.628 af
				Primary=6.83 cfs	0.628 af
Total Ru	noff Area = 2.643 ac Run 44 63%	off Volume = 0.6 Pervious = 1 17	628 af Avera	age Runoff Dept % Impervious =	h = 2.85" 1 463 ac
			0.00	/0 1110000	

Summary for Subcatchment 1S: To CB-1

Runoff = 1.37 cfs @ 12.09 hrs, Volume= 0.097 af, Depth= 2.99" Routed to Pond CB1 : CB-1

Area	(ac)	CN	Desc	ription		
0.	149	39	>75%	6 Grass co	over, Good,	, HSG A
0.	241	98	Pave	d parking,	HSG A	
0.	390	75	Weig	hted Aver	age	
0.	149		38.18	3% Pervio	us Area	
0.	241		61.82	2% Imperv	vious Area	
_						
Tc	Leng	th S	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
6.0						Direct Entry,

Summary for Subcatchment 2S: To CB-2

Runoff = 1.13 cfs @ 12.08 hrs, Volume= 0.089 af, Depth= 5.18" Routed to Pond CB2 : CB-2

Area	(ac)	CN	Desc	ription		
0.	006	39	>75%	6 Grass co	over, Good,	I, HSG A
0.	200	98	Pave	ed parking,	HSG A	
0.	206	96	Weig	ghted Aver	age	
0.	006		2.84	% Perviou	s Ārea	
0.	200		97.16	6% Imperv	vious Area	
-			~		a	
IC	Leng	th :	Slope	Velocity	Capacity	Description
<u>(min)</u>	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
6.0						Direct Entry,

Summary for Subcatchment 3S: To CB-3

Runoff = 0.57 cfs @ 12.09 hrs, Volume= 0.042 af, Depth= 4.08" Routed to Pond CB3 : CB-3(FD)

Area (ac)) CN	l Desc	cription		
0.025	5 39) >75%	% Grass co	over, Good,	I, HSG A
0.097	7 98	8 Pave	ed parking,	HSG A	
0.123	8 86	6 Weig	ghted Aver	age	
0.025	5	20.5	7% Pervio	us Area	
0.097	7	79.4	3% Imperv	vious Area	
Tc Le (min) (ength feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Subcatchment 4S: To CB-4

Runoff = 1.73 cfs @ 12.08 hrs, Volume= 0.130 af, Depth= 4.73" Routed to Pond CB4 : CB-4(FD)

Area	(ac)	CN	Desc	ription		
0.	032	39	>75%	6 Grass co	over, Good,	I, HSG A
0.	299	98	Pave	d parking,	HSG A	
0.	331	92	Weig	hted Aver	age	
0.	032		9.75	% Perviou	s Ārea	
0.	299		90.2	5% Imperv	vious Area	
_						
Tc	Lengt	th :	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
6.0						Direct Entry,

	2255 Lafayette Road - Portsmouth, NH
21163 Post-Development REV1	Type III 24-hr 10-Year Rainfall=5.65"
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Summary for Subcatchment 5S: To CB-5

Runoff = 0.95 cfs @ 12.08 hrs, Volume= 0.077 af, Depth= 5.41" Routed to Pond CB5 : CB-5

Area (ac)	CN	Desc	ription		
0.1	172	98	Pave	d parking,	HSG A	
0.1	172		100.0	00% Impe	rvious Area	a
Tc _(min)	Lengt (fee	h ያ t)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0						Direct Entry,

Summary for Subcatchment 6S: To CB-6

Runoff	=	0.74 cfs @	12.08 hrs,	Volume=	0.060 af,	Depth=	5.30"
Routed	to Pond	CB6 : CB-6					

Area (ac)	CN	Description		
0.003	39	>75% Grass c	over, Good,	, HSG A
0.132	98	Paved parking	, HSG A	
0.135	97	Weighted Aver	rage	
0.003		2.18% Perviou	s Area	
0.132		97.82% Imperv	/ious Area	
Tc Leng (min) (fee	jth S et)	Slope Velocity (ft/ft) (ft/sec)	Capacity (cfs)	Description
6.0				Direct Entry,

Summary for Subcatchment 7S: Canopy

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 0.54 cfs @ 12.00 hrs, Volume= Routed to Pond DMH3 : DMH-3 0.036 af, Depth= 5.41"

Area (ac)	CN	Desc	ription		
0.081	98	Pave	d parking,	HSG A	
0.081		100.0	00% Impe	rvious Area	3
Tc Le (min) (ngth feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry,

Summary for Subcatchment 8S: Roof

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 0.77 cfs @ 12.00 hrs, Volume= Routed to Pond DMH3 : DMH-3 0.051 af, Depth= 5.41"

Area (ac)	CN	Desc	cription		
0.114	98	Roof	s, HSG A		
0.114		100.	00% Impe	rvious Area	3
Tc Len (min) (fe	gth et)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0					Direct Entry,

Summary for Subcatchment 100S: Overland Flow to Wetland

Runoff	=	0.24 cfs @	12.34 hrs,	Volume=	0.045 af,	Depth=	0.50"
Routed	d to Lin	k DP#1 : Desig	n Point #1 -	Wetland		•	

	Area ((ac) C	N Des	cription			
	0.5	516 3	39 >75°	% Grass co	over, Good,	, HSG A	
	0.1	127 9	98 Pave	ed parking	, HSG A		
_	0.4	449 3	30 Woo	ods, Good,	HSG A		
	1.(091 4	12 Wei	ghted Aver	age		
	0.9	964	88.3	7% Pervio	us Area		
	0.1	127	11.6	3% Imper	vious Area		
	Тс	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	2.5	25	0.0320	0.17		Sheet Flow,	
						Grass: Short n= 0.150 P2= 3.71"	
	4.1	286	0.0280	1.17		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
	1.5	105	0.0510	1.13		Shallow Concentrated Flow,	
_						Woodland Kv= 5.0 fps	
	8.1	416	Total				

Summary for Pond CB1:	CB-1	
HydroCAD® 10.10-7a s/n 01710 © 2021 HydroCAD Software Solutio	ns LLC	Page 17
Prepared by Greenman-Pedersen, Inc.		Printed 4/19/2022
21163 Post-Development REV1	Type III 24-hr	10-Year Rainfall=5.65'
	2255 Lafayette	ક Road - Portsmouth, NH

0.390 ac, 61.82% Impervious, Inflow Depth = 2.99" for 10-Year event Inflow Area = 1.37 cfs @ 12.09 hrs, Volume= Inflow = 0.097 af 1.37 cfs @ 12.09 hrs, Volume= Outflow = 0.097 af, Atten= 0%, Lag= 0.0 min Primary 1.37 cfs @ 12.09 hrs, Volume= 0.097 af = Routed to Pond DMH1 : DMH-1 Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 61.69' @ 12.10 hrs Flood Elev= 64.55' Device Routing Invert Outlet Devices #1 12.0" Round Culvert Primary 61.05' L= 50.9' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 61.05' / 60.50' S= 0.0108 '/' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.35 cfs @ 12.09 hrs HW=61.68' TW=61.08' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 1.35 cfs @ 3.65 fps)

21163 Post-Development REV1 Prepared by Greenman-Pedersen, Inc. <u>HydroCAD® 10.10-7a s/n 01710 © 2021 HydroCAD Software Solu</u>	2255 Lafayette Road - Portsmouth, NH <i>Type III 24-hr 10-Year Rainfall=5.65"</i> Printed 4/19/2022 utions LLC Page 18				
Summary for Pond CB	2: CB-2				
Inflow Area = 0.206 ac, 97.16% Impervious, Inflow Dep Inflow = 1.13 cfs @ 12.08 hrs, Volume= 0 Outflow = 1.13 cfs @ 12.08 hrs, Volume= 0 Primary = 1.13 cfs @ 12.08 hrs, Volume= 0 Routed to Pond CB6 : CB-6 0 0 0	th = 5.18" for 10-Year event 0.089 af 0.089 af, Atten= 0%, Lag= 0.0 min 0.089 af				
Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 61.00' @ 12.12 hrs Flood Elev= 63.70'					

Device	Routing	Invert	Outlet Devices
#1	Primary	60.20'	12.0" Round Culvert L= 138.6' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 60.20' / 59.50' S= 0.0051 '/' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.05 cfs @ 12.08 hrs HW=60.94' TW=60.53' (Dynamic Tailwater) ☐ 1=Culvert (Outlet Controls 1.05 cfs @ 2.34 fps)

	2255 Lafayette	e Road - Ports	mouth, NH
21163 Post-Development REV1	Type III 24-hr	10-Year Rair	nfall=5.65"
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Summary for Pond CB3: CB-3(FD)

0.317 ac, 92.05% Impervious, Inflow Depth = 4.90" for 10-Year event Inflow Area = Inflow 1.67 cfs @ 12.00 hrs, Volume= = 0.129 af 1.67 cfs @ 12.00 hrs, Volume= 0.129 af, Atten= 0%, Lag= 0.0 min Outflow = 1.67 cfs @ 12.00 hrs, Volume= 0.129 af Primary = Routed to Pond DET : Underground Detention System Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 59.53' @ 12.11 hrs Flood Elev= 62.80' Device Routing Invert Outlet Devices 12.0" Round Culvert #1 Primary 58.80' L= 28.8' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 58.80' / 57.00' S= 0.0625 '/' Cc= 0.900

n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.65 cfs @ 12.00 hrs HW=59.50' TW=58.52' (Dynamic Tailwater) -1=Culvert (Inlet Controls 1.65 cfs @ 2.84 fps)

21163 Post-Dev	velopment REV1	2255 Lafayette Road - Portsmouth, NH Type III 24-hr 10-Year Rainfall=5.65"			
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	Summary for Pond CB4: CB-4(FD)				
Inflow Area =	1.234 ac, 84.61% Impervious, Inflow De	pth = 4.41" for 10-Year event			
Inflow =	5.91 cfs @ 12.09 hrs, Volume=	0.454 af			
Outflow =	5.91 cfs @ 12.09 hrs, Volume=	0.454 af, Atten= 0%, Lag= 0.0 min			
Primary =	5.91 cfs @ 12.09 hrs, Volume=	0.454 af			

Routed to Pond DMH2 : DMH-2

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 60.15' @ 12.10 hrs Flood Elev= 61.70'

Device	Routing	Invert	Outlet Devices
#1	Primary	57.95'	18.0" Round Culvert L= 80.7' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 57.95' / 57.55' S= 0.0050 '/' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.77 sf

Primary OutFlow Max=5.41 cfs @ 12.09 hrs HW=60.06' TW=59.65' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 5.41 cfs @ 3.06 fps)

	2255 Lafayette	e Road - Portsmouth, NH
21163 Post-Development REV1	Type III 24-hr	10-Year Rainfall=5.65"
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Summary for Pond CB5: CB-5

0.903 ac, 82.54% Impervious, Inflow Depth = 4.29" for 10-Year event Inflow Area = 4.19 cfs @ 12.09 hrs, Volume= Inflow = 0.323 af 4.19 cfs @ 12.09 hrs, Volume= 0.323 af, Atten= 0%, Lag= 0.0 min Outflow = Primary 4.19 cfs @ 12.09 hrs, Volume= 0.323 af = Routed to Pond CB4 : CB-4(FD) Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 60.37' @ 12.11 hrs Flood Elev= 63.05' Device Routing Invert Outlet Devices 18.0" Round Culvert #1 Primary 58.40' L= 70.4' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 58.40' / 58.05' S= 0.0050 '/' Cc= 0.900

n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.77 sf

Primary OutFlow Max=3.10 cfs @ 12.09 hrs HW=60.19' TW=60.06' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 3.10 cfs @ 1.76 fps)

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Summary for Pond CB6: CB-6

0.732 ac, 78.44% Impervious, Inflow Depth = 4.03" for 10-Year event Inflow Area = Inflow 3.24 cfs @ 12.09 hrs, Volume= = 0.246 af 3.24 cfs @ 12.09 hrs, Volume= 0.246 af, Atten= 0%, Lag= 0.0 min Outflow = Primary 3.24 cfs @ 12.09 hrs, Volume= 0.246 af = Routed to Pond CB5 : CB-5 Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 60.69' @ 12.12 hrs Flood Elev= 63.90' Device Routing Invert Outlet Devices #1 59.25' 15.0" Round Culvert Primary L= 93.9' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 59.25' / 58.65' S= 0.0064 '/' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=2.79 cfs @ 12.09 hrs HW=60.54' TW=60.20' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 2.79 cfs @ 2.73 fps)

Summary for Pond DET: Underground Detention System

Inflow Area =		1.552 ac, 86.13%	Impervious, Inflow Depth = 4.51" for 10-Year event
Inflow	=	7.16 cfs @ 12.08 h	hrs, Volume= 0.583 af
Outflow	=	6.74 cfs @ 12.11 l	hrs, Volume= 0.583 af, Atten= 6%, Lag= 1.8 min
Primary	=	6.74 cfs @ 12.11 l	hrs, Volume= 0.583 af
Routed	to Pond	JF : Jellyfish Filter	
Routing by	y Dyn-Sto	r-Ind method, Time	Span= 0.00-30.00 hrs, dt= 0.01 hrs
Peak Elev	′= 59.33' (@ 12.11 hrs Surf.A	rea= 1,290 sf Storage= 1,459 cf
Flood Elev	v= 60.50'	Surf.Area= 1,290 s	sf Storage= 1,977 cf
Plug-Flow	detentior	n time= (not calculat	ed: outflow precedes inflow)
Center-of-Mass det. time= 1.7 min (774.8 - 773.1)			4.8 - 773.1)
Volume	Inver	t Avail.Storage	Storage Description
#1A	57.00	" 0 cf	19.25'W x 67.00'L x 3.50'H Field A
			4,514 cf Overall - 2,468 cf Embedded = 2,046 cf x 0.0% Voids
#2A	57.00	l' 1,977 cf	ADS N-12 36" x 4 Inside #1
			Inside= 36.1"W x 36.1"H => 7.10 sf x 20.00'L = 142.0 cf
			Outside= 42.0"W x 42.0"H => 8.86 sf x 20.00'L = 177.1 cf
			Row Length Adjustment= +40.00' x 7.10 sf x 4 rows
			19.25' Header x 7.10 sf x 2 = 273.3 cf Inside

1,977 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	57.00'	18.0" Round Culvert
			L= 3.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 57.00' / 56.90' S= 0.0333 '/' Cc= 0.900
			n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.77 sf
#2	Device 1	57.00'	5.0" Vert. Orifice/Grate X 3.00 C= 0.600
			Limited to weir flow at low heads
#3	Device 1	57.50'	5.0" Vert. Orifice/Grate X 2.00 C= 0.600
			Limited to weir flow at low heads
#4	Device 1	59.00'	18.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Primary OutFlow Max=6.71 cfs @ 12.11 hrs HW=59.33' TW=57.95' (Dynamic Tailwater) -**1=Culvert** (Passes 6.71 cfs of 9.98 cfs potential flow) 2=Orifice/Grate (Orifice Controls 2.31 cfs @ 5.65 fps) -3=Orifice/Grate (Orifice Controls 1.54 cfs @ 5.65 fps) -4=Orifice/Grate (Weir Controls 2.86 cfs @ 1.87 fps)

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Chamber Model = ADS N-12 36" (ADS N-12® Pipe)

Inside= 36.1"W x 36.1"H => 7.10 sf x 20.00'L = 142.0 cf Outside= 42.0"W x 42.0"H => 8.86 sf x 20.00'L = 177.1 cf Row Length Adjustment= +40.00' x 7.10 sf x 4 rows

42.0" Wide + 21.0" Spacing = 63.0" C-C Row Spacing

1 Chambers/Row x 20.00' Long +40.00' Row Adjustment +3.50' Header x 2 = 67.00' Row Length 4 Rows x 42.0" Wide + 21.0" Spacing x 3 = 19.25' Base Width 42.0" Chamber Height = 3.50' Field Height

4 Chambers x 142.0 cf +40.00' Row Adjustment x 7.10 sf x 4 Rows + 19.25' Header x 7.10 sf x 2 = 1,977.3 cf Chamber Storage 4 Chambers x 177.1 cf +40.00' Row Adjustment x 8.86 sf x 4 Rows + 19.25' Header x 8.86 sf x 2 = 2,466.7 cf Displacement

4,514.1 cf Field - 2,466.7 cf Chambers = 2,047.4 cf Stone x 0.0% Voids = 0.0 cf Stone Storage

Chamber Storage = 1,977.3 cf = 0.045 af Overall Storage Efficiency = 43.8% Overall System Size = 67.00' x 19.25' x 3.50'

4 Chambers 167.2 cy Field 75.8 cy Stone





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	Summary for Pond DMH1: DMH-1				
Inflow Area =	0.390 ac, 61.82% Impervious, Inflow D	Depth = 2.99" for 10-Year event			
Inflow =	1.37 cfs @ 12.09 hrs, Volume=	0.097 af			
Outflow =	1.37 cfs @ 12.09 hrs, Volume=	0.097 af, Atten= 0%, Lag= 0.0 min			
Primary =	1.37 cfs @ 12.09 hrs, Volume=	0.097 af			

Routed to Pond CB6 : CB-6

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 61.12' @ 12.12 hrs Flood Elev= 65.30'

Device	Routing	Invert	Outlet Devices				
#1	Primary	60.40'	12.0" Round Culvert L= 65.9' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 60.40' / 59.50' S= 0.0137 '/' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.79 sf				
Primary OutFlow Max=1.29 cfs @ 12.09 hrs HW=61.08' TW=60.56' (Dynamic Tailwater) ←1=Culvert (Outlet Controls 1.29 cfs @ 3.20 fps)							

21163 Post-Development REV12255 Lafayette Road - Portsmouth, NH
Type III 24-hr 10-Year Rainfall=5.65"Prepared by Greenman-Pedersen, Inc.Printed 4/19/2022HydroCAD® 10.10-7a s/n 01710 © 2021 HydroCAD Software Solutions LLCPage 26

Summary for Pond DMH2: DMH-2

Inflow Area	a =	1.234 ac, 8	34.61% Impe	ervious,	Inflow D)epth =	4.4	1" for	10-`	Year ev	/ent
Inflow	=	5.91 cfs @	12.09 hrs,	Volume	=	0.454	af				
Outflow	=	5.91 cfs @	12.09 hrs,	Volume	=	0.454	af, A	Atten= 0)%,	Lag= 0	.0 min
Primary	=	0.57 cfs @	11.67 hrs,	Volume	=	0.282	af			•	
Routed	to Pond	OWS : Oil/V	Vater Separ	ator							
Secondary	=	5.46 cfs @	12.09 hrs,	Volume	=	0.172	af				
Routed	to Pond	DET : Unde	rground Det	ention S	ystem						

Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 59.71' @ 12.10 hrs Flood Elev= 63.30'

Device	Routing	Invert	Outlet Devices
#1	Primary	57.45'	6.0" Round Culvert L= 10.4' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 57.45' / 57.35' S= 0.0096 '/' Cc= 0.900
#2	Secondary	57.95'	n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.20 sf 18.0" Round Culvert L= 29.4' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 57.95' / 57.00' S= 0.0323 '/' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.77 sf

Primary OutFlow Max=0.56 cfs @ 11.67 hrs HW=58.25' TW=57.90' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 0.56 cfs @ 2.83 fps)

Secondary OutFlow Max=5.17 cfs @ 12.09 hrs HW=59.66' TW=59.30' (Dynamic Tailwater) -2=Culvert (Inlet Controls 5.17 cfs @ 2.93 fps)

Summary for Pond DMH3: DMH-3							
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21163 Post-Development REV1	Type III 24-hr	10-Year Rainfall=5.65"					
	2255 Lafayett	e Road - Portsmouth, NH					

0.195 ac,100.00% Impervious, Inflow Depth = 5.41" for 10-Year event Inflow Area = 1.31 cfs @ 12.00 hrs, Volume= Inflow = 0.088 af 1.31 cfs @ 12.00 hrs, Volume= Outflow = 0.088 af, Atten= 0%, Lag= 0.0 min 1.31 cfs @ 12.00 hrs, Volume= Primary 0.088 af = Routed to Pond CB3 : CB-3(FD) Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 59.87' @ 12.00 hrs Flood Elev= 64.00' Device Routing Invert Outlet Devices #1 59.20' 12.0" Round Culvert Primary L= 30.5' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 59.20' / 58.90' S= 0.0098 '/' Cc= 0.900

n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.27 cfs @ 12.00 hrs HW=59.87' TW=59.50' (Dynamic Tailwater) -1=Culvert (Outlet Controls 1.27 cfs @ 3.22 fps)

223	5 Lalayelle Road - Portsmouth, NH
21163 Post-Development REV1 Type	e III 24-hr 10-Year Rainfall=5.65"
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Summary for Pond JF: Jellyfish Filter

1.552 ac, 86.13% Impervious, Inflow Depth = 4.51" for 10-Year event Inflow Area = 6.74 cfs @ 12.11 hrs, Volume= Inflow = 0.583 af 6.74 cfs @ 12.11 hrs, Volume= 0.583 af, Atten= 0%, Lag= 0.0 min Outflow = Primary 6.74 cfs @ 12.11 hrs, Volume= 0.583 af = Routed to Link DP#1 : Design Point #1 - Wetland Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 57.95' @ 12.11 hrs Flood Elev= 62.00' Device Routing Invert Outlet Devices 18.0" Round Culvert #1 Primary 56.40' L= 12.4' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 56.40' / 56.25' S= 0.0121 '/' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 1.77 sf

Primary OutFlow Max=6.73 cfs @ 12.11 hrs HW=57.95' TW=0.00' (Dynamic Tailwater) -1=Culvert (Barrel Controls 6.73 cfs @ 4.58 fps) 21163 Post-Development REV12255 Lafayette Road - Portsmouth, NH
Type III 24-hrPrepared by Greenman-Pedersen, Inc.Printed 4/19/2022HydroCAD® 10.10-7a s/n 01710 © 2021 HydroCAD Software Solutions LLCPage 29

Summary for Pond OWS: Oil/Water Separator

Inflow Area = 1.234 ac, 84.61% Impervious, Inflow Depth = 2.74" for 10-Year event 0.57 cfs @ 11.67 hrs, Volume= Inflow = 0.282 af Outflow = 0.57 cfs @ 11.67 hrs, Volume= 0.282 af, Atten= 0%, Lag= 0.0 min 0.57 cfs @ 11.67 hrs, Volume= 0.282 af Primary = Routed to Pond DET : Underground Detention System Routing by Dyn-Stor-Ind method, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs Peak Elev= 59.52' @ 12.10 hrs Flood Elev= 63.75' Device Routing Invert Outlet Devices 6.0" Round Culvert L= 7.5' CPP, square edge headwall, Ke= 0.500 #1 Primary 57.10' Inlet / Outlet Invert= 57.10' / 57.00' S= 0.0133 '/' Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 0.20 sf

Summary for Link DP#1: Design Point #1 - Wetland

Inflow A	Area	=	2.643 ac, 5	55.37% Impe	ervious,	Inflow Depth =	2.8	5" for 10-`	Year event
Inflow	=	=	6.83 cfs @	12.11 hrs,	Volume	= 0.628	af		
Primary	/ =	=	6.83 cfs @	12.11 hrs,	Volume	= 0.628	af,	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-30.00 hrs, dt= 0.01 hrs
21163 Post-Development REV1	2255 Lafayette Road - Portsmouth, NH Type III 24-hr 25-Year Rainfall=7.16"
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Time span=0.00-30.00 brs. c	It=0.01 brs. 3001 points

Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: To CB-1	Runoff Area=0	.390 ac 61.82% Impe Tc=6.0 min CN=75	rvious Runoff Depth=4.29" 5 Runoff=1.96 cfs 0.139 af
Subcatchment 2S: To CB-2	Runoff Area=0	.206 ac 97.16% Impe Tc=6.0 min CN=96	rvious Runoff Depth=6.68" 8 Runoff=1.44 cfs 0.115 af
Subcatchment 3S: To CB-3	Runoff Area=0	.123 ac 79.43% Impe Tc=6.0 min CN=86	rvious Runoff Depth=5.52" 8 Runoff=0.77 cfs 0.056 af
Subcatchment 4S: To CB-4	Runoff Area=0	.331 ac 90.25% Impe Tc=6.0 min CN=92	rvious Runoff Depth=6.21" 2 Runoff=2.23 cfs 0.171 af
Subcatchment 5S: To CB-5	Runoff Area=0.	172 ac 100.00% Impe Tc=6.0 min CN=98	rvious Runoff Depth=6.92" 8 Runoff=1.21 cfs 0.099 af
Subcatchment 6S: To CB-6	Runoff Area=0	.135 ac 97.82% Impe Tc=6.0 min CN=97	rvious Runoff Depth=6.80" ′ Runoff=0.95 cfs 0.077 af
Subcatchment 7S: Canopy	Runoff Area=0.0	081 ac 100.00% Impe Tc=0.0 min CN=98	rvious Runoff Depth=6.92" 8 Runoff=0.69 cfs 0.046 af
Subcatchment 8S: Roof	Runoff Area=0.	114 ac 100.00% Impe Tc=0.0 min CN=98	rvious Runoff Depth=6.92" 3 Runoff=0.98 cfs 0.066 af
Subcatchment 100S: Overland	Flow to Runoff Area=1 Flow Length=416	.091 ac 11.63% Impe 5' Tc=8.1 min CN=42	rvious Runoff Depth=1.06" ? Runoff=0.83 cfs 0.097 af
Pond CB1: CB-1	2.0" Round Culvert n=0.012	Peak Elev=62.58 2 L=50.9' S=0.0108 '/'	8' Inflow=1.96 cfs 0.139 af Outflow=1.96 cfs 0.139 af
Pond CB2: CB-2	2.0" Round Culvert n=0.012	Peak Elev=62.29 L=138.6' S=0.0051 '/'	9' Inflow=1.44 cfs 0.115 af Outflow=1.44 cfs 0.115 af
Pond CB3: CB-3(FD)	2.0" Round Culvert n=0.012	Peak Elev=59.74 2 L=28.8' S=0.0625 '/'	4' Inflow=2.14 cfs 0.169 af Outflow=2.14 cfs 0.169 af
Pond CB4: CB-4(FD)	8.0" Round Culvert n=0.012	Peak Elev=61.09 2 L=80.7' S=0.0050 '/'	5' Inflow=7.78 cfs 0.601 af Outflow=7.78 cfs 0.601 af
Pond CB5: CB-5	8.0" Round Culvert n=0.012	Peak Elev=61.4 2 L=70.4' S=0.0050 '/'	5' Inflow=5.55 cfs 0.430 af Outflow=5.55 cfs 0.430 af
Pond CB6: CB-6	5.0" Round Culvert n=0.012	Peak Elev=62.00 2 L=93.9' S=0.0064 '/'	5' Inflow=4.34 cfs 0.331 af Outflow=4.34 cfs 0.331 af
Pond DET: Underground Deten	tion System Peak Elev=	59.55' Storage=1,623 o	cf Inflow=9.41 cfs 0.770 af Outflow=8.99 cfs 0.770 af

		23	255 Lafayette	e Road - Portsmo	outh, NH
21163 Post-Developr	nent REV1	Ту	vpe III 24-hr	25-Year Rainfa	all=7.16"
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Pond DMH1: DMH-1		Pea	ık Elev=62.34	' Inflow=1.96 cfs	0.139 af
	12.0" Round Culvert n	=0.012 L=65.9'	S=0.0137 '/'	Outflow=1.96 cfs	0.139 af
Pond DMH2: DMH-2		Pea	k Elev=60.23	Inflow=7.78 cfs	0.601 af
	Primary=0.58 cfs 0.351 af S	econdary=7.21	cfs 0.251 af	Outflow=7.78 cfs	0.601 af
Pond DMH3: DMH-3		Pea	k Elev=60.00	Inflow=1.67 cfs	0.112 af
	12.0" Round Culvert n	=0.012 L=30.5'	S=0.0098 '/'	Outflow=1.67 cfs	0.112 af
Pond JF: Jellyfish Filter		Pea	k Elev=58.43	Inflow=8.99 cfs	0.770 af
	18.0" Round Culvert n	=0.012 L=12.4'	S=0.0121 '/'	Outflow=8.99 cfs	0.770 af
Pond OWS: Oil/Water Se	eparator	Pea	ık Elev=59.89	Inflow=0.58 cfs	0.351 af
	6.0" Round Culvert	n=0.012 L=7.5'	S=0.0133 '/'	Outflow=0.58 cfs	0.351 af
Link DP#1: Design Point	t #1 - Wetland			Inflow=9.72 cfs	0.867 af
				Primary=9.72 cfs	0.867 af
Total Ru	noff Area = 2.643 ac Runof 44.63% P	f Volume = 0.8 ervious = 1.17	67 af Avera 9 ac 55.37	ge Runoff Deptl % Impervious =	n = 3.94" 1.463 ac

21163 Post-Development REV12255 Lafayette Road - Portsmouth, NH
Type III 24-hrPrepared by Greenman-Pedersen, Inc.Printed 4/19/2022HydroCAD® 10.10-7a s/n 01710 © 2021 HydroCAD Software Solutions LLCPage 5Time span=0.00-30.00 hrs, dt=0.01 hrs, 3001 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: To CB-1	Runoff Area=0.390 ac 61.82% Impervious Runoff Depth=5.57" Tc=6.0 min CN=75 Runoff=2.53 cfs 0.181 af
Subcatchment 2S: To CB-2	Runoff Area=0.206 ac 97.16% Impervious Runoff Depth=8.10" Tc=6.0 min CN=96 Runoff=1.73 cfs 0.139 af
Subcatchment 3S: To CB-3	Runoff Area=0.123 ac 79.43% Impervious Runoff Depth=6.89" Tc=6.0 min CN=86 Runoff=0.95 cfs 0.070 af
Subcatchment 4S: To CB-4	Runoff Area=0.331 ac 90.25% Impervious Runoff Depth=7.62" Tc=6.0 min CN=92 Runoff=2.71 cfs 0.210 af
Subcatchment 5S: To CB-5	Runoff Area=0.172 ac 100.00% Impervious Runoff Depth=8.34" Tc=6.0 min CN=98 Runoff=1.45 cfs 0.119 af
Subcatchment 6S: To CB-6	Runoff Area=0.135 ac 97.82% Impervious Runoff Depth=8.22" Tc=6.0 min CN=97 Runoff=1.14 cfs 0.093 af
Subcatchment 7S: Canopy	Runoff Area=0.081 ac 100.00% Impervious Runoff Depth=8.34" Tc=0.0 min CN=98 Runoff=0.83 cfs 0.056 af
Subcatchment 8S: Roof	Runoff Area=0.114 ac 100.00% Impervious Runoff Depth=8.34" Tc=0.0 min CN=98 Runoff=1.17 cfs 0.079 af
Subcatchment 100S: Overland	Flow to Runoff Area=1.091 ac 11.63% Impervious Runoff Depth=1.72" Flow Length=416' Tc=8.1 min CN=42 Runoff=1.65 cfs 0.157 af
Pond CB1: CB-1	Peak Elev=64.55' Inflow=2.53 cfs 0.181 af 12.0" Round Culvert n=0.012 L=50.9' S=0.0108 '/' Outflow=2.53 cfs 0.181 af
Pond CB2: CB-2	Peak Elev=64.04' Inflow=1.73 cfs 0.139 af 2.0" Round Culvert n=0.012 L=138.6' S=0.0051 '/' Outflow=1.73 cfs 0.139 af
Pond CB3: CB-3(FD)	Peak Elev=60.39' Inflow=2.59 cfs 0.206 af 12.0" Round Culvert n=0.012 L=28.8' S=0.0625 '/' Outflow=2.59 cfs 0.206 af
Pond CB4: CB-4(FD)	Peak Elev=62.24' Inflow=9.55 cfs 0.742 af 18.0" Round Culvert n=0.012 L=80.7' S=0.0050 '/' Outflow=9.55 cfs 0.742 af
Pond CB5: CB-5	Peak Elev=62.82' Inflow=6.84 cfs 0.532 af 18.0" Round Culvert n=0.012 L=70.4' S=0.0050 '/' Outflow=6.84 cfs 0.532 af
Pond CB6: CB-6	Peak Elev=63.72' Inflow=5.39 cfs 0.413 af 15.0" Round Culvert n=0.012 L=93.9' S=0.0064 '/' Outflow=5.39 cfs 0.413 af
Pond DET: Underground Dete	ntion System Peak Elev=60.21' Storage=1,972 cf Inflow=11.53 cfs 0.948 af Outflow=10.55 cfs 0.948 af

			2255 Lafayett	e Road - Portsmo	outh, NH
21163 Post-Developm	nent REV1	T	ype III 24-hr	50-Year Rainfa	all=8.58"
Prepared by Greenman	-Pedersen, Inc.			Printed 4	/19/2022
HydroCAD® 10.10-7a s/n 0	1710 © 2021 HydroCA	D Software Solutions I	LLC		Page 6
Pond DMH1: DMH-1		Pe	ak Elev=64.17	" Inflow=2.53 cfs	0.181 af
	12.0" Round Cul	vert n=0.012 L=65.9'	S=0.0137 '/'	Outflow=2.53 cfs	0.181 af
Pond DMH2: DMH-2		Pe	ak Elev=61.12	' Inflow=9.55 cfs	0.742 af
	Primary=0.73 cfs 0.40	9 af Secondary=8.82	cfs 0.333 af	Outflow=9.55 cfs	0.742 af
Pond DMH3: DMH-3		Pe	ak Elev=60.43	' Inflow=2.00 cfs	0.135 af
	12.0" Round Cul	vert n=0.012 L=30.5'	S=0.0098 '/'	Outflow=2.00 cfs	0.135 af
Pond JF: Jellyfish Filter		Pea	k Elev=58.69'	Inflow=10.55 cfs	0.948 af
-	18.0" Round Culve	ert n=0.012 L=12.4' 3	S=0.0121 '/' (Outflow=10.55 cfs	0.948 af
Pond OWS: Oil/Water Se	parator	Pe	ak Elev=60.66	' Inflow=0.73 cfs	0.409 af
	6.0" Round Cu	ılvert n=0.012 L=7.5'	S=0.0133 '/'	Outflow=0.73 cfs	0.409 af
Link DP#1: Design Point	#1 - Wetland			Inflow=12.14 cfs	1.105 af
•			F	Primary=12.14 cfs	1.105 af
Total Rui	ا off Area = 2.643 ac مەر	Runoff Volume = 1.1 63% Pervious = 1 17	105 af Avera 79 ac 55 37	age Runoff Dept	h = 5.02" 1 463 ac

Stormwater Management Report

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

Revised: April 19, 2022

APPENDIX F

Supplemental Calculations and Backup Data

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing	Yes	Per Env-Wq	2yr 3.71
State	New Hampshire	1503.08(I) these	10yr 5.65
Location		values are increased	25vr 7.16
Longitude	70.780 degrees West	by 15% for the	50vr 8 58
Latitude	43.034 degrees North	analysis	00y1 0.00
Elevation	0 feet	analysis	
Date/Time	Wed, 22 Sep 2021 13:51:31 -0400		

Extreme Precipitation Estimates

	•																				
	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.50	0.65	0.82	1.04	1yr	0.71	0.98	1.22	1.57	2.04	2.68	195	1yr	2.37	2.83	3.25	3.97	4.59	1yr
2yr	0.32	0.50	0.62	0.82	1.03	1.30	2yr	0.89	1.18	1.52	1.95	2.50	<mark>3.23</mark>	3.60	2yr	2.86	3.46	3.97	4.72	5.37	2yr
5yr	0.37	0.58	0.73	0.98	1.25	1.61	5yr	1.08	1.47	1.89	2.44	3.16	4.10	4.62	5yr	3.63	4.44	5.09	5.99	6.76	5yr
10yr	0.41	0.65	0.82	1.12	1.46	1.90	10yr	1.26	1.73	2.24	2.91	3.78	<mark>4.91</mark>	5.58	10yr	4.34	5.37	6.15	7.17	8.05	10yr
25yr	0.48	0.76	0.97	1.34	1.78	2.35	25yr	1.54	2.15	2.79	3.65	4.78	<mark>6.23</mark>	7.16	25yr	5.51	6.89	7.89	9.12	10.14	25yr
50yr	0.54	0.86	1.11	1.55	2.08	2.77	50yr	1.80	2.54	3.31	4.36	5.71	<mark>7.46</mark>	8.66	50yr	6.60	8.33	9.54	10.93	12.09	50yr
100yr	0.60	0.97	1.25	1.78	2.43	3.28	100yr	2.10	2.99	3.93	5.20	6.83	8.94	10.48	100yr	7.91	10.08	11.53	13.11	14.41	100yr
200yr	0.68	1.11	1.44	2.06	2.85	3.86	200yr	2.46	3.54	4.65	6.18	8.16	10.71	12.67	200yr	9.48	12.19	13.95	15.74	17.19	200yr
500yr	0.81	1.33	1.73	2.51	3.51	4.81	500yr	3.03	4.41	5.82	7.78	10.32	13.62	16.31	500yr	12.06	15.68	17.95	20.04	21.72	500yr

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.23	0.36	0.44	0.59	0.72	0.88	1yr	0.62	0.87	0.92	1.33	1.68	2.26	2.56	1yr	2.00	2.46	2.89	3.18	3.94	1yr
2yr	0.32	0.49	0.60	0.81	1.00	1.19	2yr	0.87	1.16	1.37	1.82	2.33	3.08	3.49	2yr	2.73	3.36	3.86	4.59	5.12	2yr
5yr	0.35	0.54	0.67	0.92	1.18	1.41	5yr	1.01	1.38	1.61	2.12	2.73	3.83	4.25	5yr	3.39	4.09	4.77	5.60	6.32	5yr
10yr	0.39	0.60	0.74	1.03	1.33	1.61	10yr	1.15	1.57	1.81	2.38	3.05	4.42	4.94	10yr	3.91	4.75	5.54	6.51	7.29	10yr
25yr	0.44	0.67	0.84	1.20	1.58	1.91	25yr	1.36	1.87	2.10	2.75	3.53	4.78	6.01	25yr	4.23	5.78	6.80	7.95	8.82	25yr
50yr	0.49	0.74	0.92	1.33	1.78	2.18	50yr	1.54	2.13	2.35	3.06	3.93	5.41	6.96	50yr	4.79	6.69	7.94	9.25	10.20	50yr
100yr	0.54	0.82	1.03	1.48	2.04	2.48	100yr	1.76	2.43	2.63	3.40	4.34	6.09	8.06	100yr	5.39	7.75	9.28	10.78	11.79	100yr
200yr	0.60	0.90	1.15	1.66	2.31	2.83	200yr	2.00	2.77	2.94	3.77	4.79	6.84	9.33	200yr	6.06	8.97	10.84	12.57	13.65	200yr
500yr	0.70	1.04	1.34	1.94	2.76	3.39	500yr	2.39	3.31	3.42	4.29	5.45	7.99	11.32	500yr	7.07	10.89	13.33	15.44	16.55	500yr

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.29	0.44	0.54	0.72	0.89	1.09	1yr	0.77	1.06	1.26	1.74	2.20	3.01	3.17	1yr	2.66	3.05	3.61	4.40	5.09	1yr
2yr	0.34	0.52	0.64	0.87	1.07	1.27	2yr	0.92	1.24	1.48	1.96	2.51	3.45	3.72	2yr	3.05	3.58	4.11	4.87	5.67	2yr
5yr	0.40	0.62	0.77	1.05	1.34	1.63	5yr	1.16	1.59	1.88	2.53	3.25	4.37	4.98	5yr	3.87	4.79	5.42	6.40	7.18	5yr
10yr	0.47	0.72	0.89	1.25	1.61	1.98	10yr	1.39	1.94	2.28	3.10	3.95	5.38	6.21	10yr	4.76	5.97	6.82	7.87	8.78	10yr
25yr	0.58	0.88	1.09	1.56	2.06	2.58	25yr	1.77	2.52	2.96	4.07	5.14	7.82	8.33	25yr	6.92	8.01	9.12	10.36	11.43	25yr
50yr	0.67	1.03	1.28	1.84	2.47	3.14	50yr	2.13	3.07	3.60	5.00	6.31	9.79	10.42	50yr	8.66	10.02	11.38	12.74	13.98	50yr
100yr	0.79	1.20	1.50	2.17	2.98	3.83	100yr	2.57	3.74	4.37	6.15	7.74	12.24	13.04	100yr	10.83	12.53	14.18	15.70	17.09	100yr
200yr	0.93	1.40	1.77	2.56	3.57	4.67	200yr	3.08	4.57	5.34	7.58	9.51	15.35	16.32	200yr	13.58	15.70	17.71	19.33	20.91	200yr
500yr	1.15	1.71	2.21	3.20	4.56	6.07	500yr	3.93	5.94	6.93	10.02	12.51	20.72	21.97	500yr	18.34	21.13	23.74	25.46	27.30	500yr



OUTLET APRON DESIGN

Project:Lafayette Rd, Portsmouth, NHJob #2021163Date:26-Jan-22

603.893.0720 Engineering Design Planning Construction Manager GPINET.COM Greenman-Pedersen, Inc. 44 Stiles Road Suite One Salem, NH 03079

FES-1 (from HydroCAD POND DET) Q25 = 9 cfs

 $D_o = 18$ inches Tw = 0.8 feet

Design Criteria

Apron Dimensions

The dimensions of the apron at the outlet of the pipe shall be determined as follows:

1.) The width of the apron at the outlet of the pipe or channel shall be 3 times the diameter of the pipe, or the width of the channel.

2.) The length of the apron shall be determined from the following formula when the tailwater depth at the outlet of the pipe or channel is less than one-half the diameter of the pipe or one-half the width of the channel:

Where:

La is the length of the apron Q is the discharge from the pipe or channel D_0 is the diameter of pipe of width of channel

3.) When the depth of the tailwater at the outlet of the pipe or channel is equal to or greater than one-half the diameter of the pipe or the width of the channel. Then the following formula applies:

- 4.) Where there is no well defined channel downstream of the outlet, the width of the downstream end of the apron shall be determined as follows:
 - a. For minimum tailwater conditions where the tailwater depth is less than the elevation of the center of the pipe:

W=3*Do+La W= **23.82** feet

b. For maximum tailwater conditions where the tailwater depth is greater than the elevation of the center of the pipe:

USE THIS W=3*Do+0.4*La W= 14.58 feet

- 5.) Where there is a stable well-defined channel downstream of the apron, the bottom of the apron shall be equal to the width of the channel.
- 6.) The side of the apron in a well-defined channel shall be 2:1 (horizontal to vertical) or flatter. The height of the structural lining along the channel sides shall begin at the elevation equal to the top of conduit and taper down to the channel bottom through the length of the apron.
- 7.) The bottom grade of the apron shall be level (0% grade). No overfall is allowable at the end of the apron.
- 8.) The apron shall be located so that there are no bends in the horizontal alignment of the apron.

Rock Riprap

The following criteria shall be used to determine the dimensions of the rock riprap used for the apron:

1.) The median stone diameter shall be determined using the formula:

d ₅₀ =0.02*Q^4/3/(Tw*D _o)			
d_{50} = 3.72 inches	USE	4 inches	
	d ₅₀ r	ninimum 3 inches	5

Where:

 d_{50} is the median stone diameter in feet

Tw is the tailwater depth above the invert of the pipe channel in feet Q is the discharge from the pipe or channel in cubic feet per second D_o is the diameter of the pipe or width of the channel in feet

- 2.) Fifty percent by weight of the riprap mixture shall be smaller the than median size stone designated as d_{50} . The largest stone size in the mixture shall be 1.5 times the d_{50} size.
- 3.) The quality and gradation of the rock, the thickness of the riprap lining, filter material and the quality of the stone shall meet the requirements in the Rock Riprap BMP. The minimum depth shall be 6 inches or 1.5 times the largest stone size in the mixture whichever is larger (d).

Thickness of the riprap

 $d = 1.5*(d100 \text{ avg.}(largest stone size}))$

d= 10 inches*

* must use a minimum of 6"

Rock Rip Rap Gradation

% of weight smaller			
than the given size	size of sto	ne in i	nches
100	5.6	to	7.4
85	4.8	to	6.7
50	3.7	to	5.6
15	1.1	to	1.9



First Defense® High Capacity

Advanced Hydrodynamic Separator

Product Summary

A Simple Solution for your Trickiest Sites

First Defense® High Capacity is a versatile stormwater separator with some of the highest approved flow rates in the United States, enabling engineers and contractors to save site space and projects costs by using the smallest possible footprint. It also works with single and multiple inlet pipes and inlet grates has an internal bypass to convey infrequent peak flows directly to the outlet.

Fig.1 The First Defense® High Capacity has internal components designed to efficiently capture pollutants and prevent washout at



Product Profile

- 1. Inlet Grate (optional)
- 2. Precast chamber
- 3. Inlet Pipe (optional)
- 4. Floatables Draw Off Slot 9. Outlet chute (not pictured)
- 5. Inlet Chute
- 6. Internal Bypass
- 7. Outlet pipe
- 8. Oil and Floatables Storage
- 10. Sediment Storage Sump

Applications

- » Areas requiring a minimum of 50% TSS removal
- » Stormwater treatment at the point of entry into the drainage line
- Sites constrained by space, topography or drainage profiles with limited » slope and depth of cover
- » Highways, car parks, industrial areas and urban developments
- » Pre-treatment to ponds, storage systems, green infrastructure

How it Works

Highest Flow through the Smallest Footprint



Contaminated stormwater runoff enters the inlet chute from a surface grate and/or inlet pipe. The inlet chute introduces flow into the chamber tangentially to create a low energy vortex flow regime (magenta arrow) that directs sediment into the sump while oils, floating trash and debris rise to the surface.

Treated stormwater exits through a submerged outlet chute located opposite to the direction of the rotating flow (blue arrow). Enhanced vortex separation is provided by forcing the rotating flow within the vessel to follow the longest path possible rather than directly from inlet to outlet.

Higher flows bypass the treatment chamber to prevent turbulence and washout of captured pollutants. An internal bypass conveys infrequent peak flows directly to the outlet eliminating the need for, and expense of, external bypass control structures. A floatables draw off slot functions to convey floatables into the treatment chamber prior to bypass.

Benefits

Small & Simple

- >> Cut footprint size, cut costs: First Defense® provides space-saving, easy-to-install surface water treatment in standard sized chambers/ manholes
- » Adapt to site limitations: Variable configuratoins will help you effectively slip First Defense[®] into a tight spot. It also works well with large pipes, multiple inlet pipes and inlet grates.
- >>> Save installation time: Every First Defense® unit is delivered to site pre-assembled and ready for installation – so installation is as easy as fitting any chamber/manhole.

Stormwater Solutions → hydro-int.com/firstdefense

Sizing & Design

This adaptable online treatment system works easily with large pipes, multiple inlet pipes, inlet grates and now, contains a high capacity bypass for the conveyance of large peak flows. Designed with site flexibility in mind, the First Defense[®] High Capacity allows engineers to maximize available site space without compromising treatment level.



Free Sizing Tool



This simple online tool will recommend the best separator, model size and online/offline arrangement based on site-specific data entered by the user.

Go to hydro-int.com/sizing to access the tool.

First Defense [®] High Capacity Model Number	Diameter	Typical TSS Treatment Flow Rates		Peak Online	Maximum Pipe	Oil Storage	Typical Sediment	Minimum Distance from	Standard Distance from Outlet
	Diamotor	NJDEP Certified	110µm	Flow Rate	Diameter ¹	Capacity	Capacity ²	Outlet Invert to Top of Rim ³	Invert to Sump Floor
	(ft / m)	(cfs / L/s)	(cfs / L/s)	(cfs / L/s)	(in / mm)	(gal / L)	(yd³ / m³)	(ft / m)	(ft / m)
FD-3HC	3 / 0.9	0.84 / 23.7	1.06 / 30.0	15 / 424	18 / 450	125 / 473	0.4 / 0.3	2.0 - 3.5 / 0.6 - 1.0	3.71 / 1.13
FD-4HC	4 / 1.2	1.50 / 42.4	1.88 / 53.2	18 / 510	24 / 600	191 / 723	0.7 / 0.5	2.3 - 3.9 / 0.7 - 1.2	4.97 / 1.5
FD-5HC	5 / 1.5	2.35 / 66.2	2.94 / 83.2	20 / 566	24 / 600	300 / 1135	1.1 / .84	2.5 - 4.5 / 0.7 - 1.3	5.19 / 1.5
FD-6HC	6 / 1.8	3.38 / 95.7	4.23 / 119.8	32 / 906	30 / 750	496 / 1,878	1.6 / 1.2	3.0 - 5.1 / 0.9 - 1.6	5.97 / 1.8
FD-8HC	8 / 2.4	6.00 / 169.9	7.52 / 212.9	50 / 1415	48 / 1200	1120 / 4239	2.8 / 2.1	3.0 - 6.0 / 0.9 -1.8	7.40 / 2.2
FD-10HC	10 / 3.0	9.38 / 265.6 11.75 / 332.7		50 / 1415	48 / 1200	1742 / 6594	4.4 / 3.3	6.5 -8.0 / 2.0 - 2.4	10.25 / 3.12

¹Contact Hydro International when larger pipe sizes are required.

²Contact Hydro International when custom sediment storage capacity is required.

³Minimum distance for models depends on pipe diameter.



Maintenance

Easy vactor hose access through the center shaft of the system makes for quick, simple sump cleanout while trash and floatables can be fished out from the surface with a net.

Nobody maintains our systems better than we do. To ensure optimal, ongoing device performance, be sure to recommend Hydro International as a preferred service and maintenance provider to your clients.

Hydro S.

- ♥ Hydro International, 94 Hutchins Drive, Portland, ME 04102
- **5 Tel**: (207) 756-6200
- Email: stormwaterinquiry@hydro-int.com
- R Web: www.hydro-int.com/firstdefense

Download Drawings!

 \rightarrow hydro-int.com/fddrawings

Access the Operation & Maintenance Manual

→ hydro-int.com/fd-om



Jellyfish[®] Filter Stormwater Treatment



The experts you need to solve your stormwater challenges

Contech is the leader in stormwater solutions, helping engineers, contractors and owners with infrastructure and land development projects throughout North America.

With our responsive team of stormwater experts, local regulatory expertise and flexible solutions, Contech is the trusted partner you can count on for stormwater management solutions.

Your Contech Team









STORMWATER CONSULTANT

It's my job to recommend the best solution to meet permitting requirements.

STORMWATER DESIGN ENGINEER

I work with consultants to design the best approved solution to meet your project's needs.

REGULATORY MANAGER

I understand the local stormwater regulations and what solutions will be approved.

SALES ENGINEER

I make sure our solutions meet the needs of the contractor during construction.

Contech is your partner in stormwater management solutions



Setting new standards in Stormwater Treatment – Jellyfish® Filter

The Jellyfish Filter is a stormwater quality treatment technology featuring high flow pretreatment and membrane filtration in a compact stand-alone system. Jellyfish removes floatables, trash, oil, debris, TSS, fine silt-sized particles, and a high percentage of particulate-bound pollutants; including phosphorus, nitrogen, metals and hydrocarbons. The high surface area membrane cartridges, combined with up-flow hydraulics, frequent, passive backwashing, and rinseable/ reusable cartridges ensure long-lasting performance. The Jellyfish Filter has been tested in the field and laboratory, and has received approval from numerous stormwater regulatory agencies.

Jellyfish[®] Filter



How the Jellyfish[®] Filter Treats Stormwater

Tested in the field and laboratory ...

- Stormwater enters the Jellyfish through the inlet pipe and traps floating pollutants behind the maintenance access wall and below the cartridge deck.
- Water is conveyed below the cartridge deck where a separation skirt around the cartridges isolates oil, trash and debris outside the filtration zone.
- Water is directed to the filtration zone and up through the top of the cartridge where it exits via the outlet pipe.
- The membrane filters provide a very large surface area to effectively remove fine sand and silt-sized particles, and a high percentage of particulate-bound pollutants such as nitrogen, phosphorus, metals, and hydrocarbons while ensuring long-lasting treatment.
- As influent flow subsides, the water in the backwash pool flows back into the lower chamber. This passive backwash extends cartridge life.
- The draindown cartridge(s) located outside the backwash pool enables water levels to balance.



Learn More: www.ContechES.com/jellyfish



Pretreat bioretention or infiltration with Jellyfish to extend service life.

Setting new standards in Stormwater Treatment

Jellyfish[®] Filter Performance Testing Results



APPLICATION TIPS

- The Peak Diversion Jellyfish provides treatment and highflow bypass in one structure, eliminating the need for a separate bypass structure.
- LID and GI are complemented by filtration solutions, as they help keep sites free from fine sediments that can impede performance, remove unsightly trash, and provide a single point of maintenance.
- Selecting a filter with a long maintenance cycle and low maintenance cost will result in healthy waterways and happy property owners.



The pleated tentacles of the Jellyfish® Filter provide a large surface area for pollutant removal.

POLLUTANT OF CONCERN	% REMOVAL
Total Trash	99%
Total Suspended Solids (TSS)	89%
Total Phosphorus (TP)	59 %
Total Nitrogen (TN)	51%
Total Copper (TCu)	> 50%
Total Zinc (TZn)	> 50%



Sources: TARP II Field Study – 2012 JF 4-2-1 Configuration MRDC Floatables Testing – 2008 JF6-6-1 Configuration



FLOW

Jellyfish® Filter Features and Benefits

FEATURE	BENEFITS
High surface area membrane filtration	Low flux rate promotes cake filtration and slows membrane occlusion
High design treatment flow rate per cartridge (up to 80 gpm (5 L/s))	Compact system with a small footprint, lower construction cost
Low driving head (typically 18 inches or less (457 mm))	Design flexibility, lower construction cost
Lightweight cartridges with passive backwash	Easy maintenance and low life-cycle cost



The Jellyfish Filter can be configured in a manhole, catch basin, or vault.

Select Jellyfish[®] Filter Certifications and Verifications

The Jellyfish Filter has been reviewed by numerous state and federal programs, including:

- Washington State Department of Ecology (TAPE) GULD BASIC, Phosphorus
- Virginia Department of Environmental Quality (VA DEQ)
- Texas Commission of Environmental Quality (TCEQ)
- Canada ISO 14034 Environmental Management Environmental Technology Verification (ETV)
- Philadelphia Water District (PWD)
- Maryland Department of the Environment (MD DOE)



Field tested and performance verified

Jellyfish[®] Filter Configurations

Multiple system configurations to optimize your site

The Jellyfish Filter can be manufactured in a variety of configurations: manhole, catch basin, vault, fiberglass tank, or custom configurations. Typically, 18 inches (457 mm) of driving head is designed into the system. For low drop sites, the designed driving head can be less.



Jellyfish® Filter Maintenance

- Jellyfish Filter cartridges are light weight and reusable
- Maintenance of the filter cartridges is performed by removing, rinsing and reusing the cartridge tentacles.
- Vacuum extraction of captured pollutants in the sump is recommended at the same time.
- Full cartridge replacement intervals differ by site due to varying pollutant loading and type, and maintenance frequency.
 Replacement is anticipated every 2-5 years.
- Contech[®] has created a network of Certified Maintenance Providers to provide maintenance on stormwater BMP's.



The Jellyfish® Filter tentacle is light and easy to clean.



A partner





STORMWATER SOLUTIONS





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11. Data Quality Assessment

Data was analyzed using statistical methods in accordance with guidelines in the **TARP Protocol for Stormwater Best Management Practice Demonstrations**, and the **VTAP Guidance for Evaluating Stormwater Manufactured Treatment Devices**. Data was examined by statistical and regression analysis, ANOVA statistics, non-parametric analysis, correlations, probability distributions of data, normality testing, standards, and physical data replication.

Data integrity in the laboratory was addressed in a multi-level review process for all analyses conducted. The initial step in this review process was conducted by each lab analyst as tests were conducted. Calibration values and procedures were checked against previous tests to alert the analyst to in case of malfunction in equipment or test errors.

The second level of review was conducted by the lab director who collected results and entered these values into the tabular spreadsheets for each test. Each of the results was checked for accuracy of input as well as to appropriateness for the samples which were analyzed. All results were overseen or conducted personally by the lab manager. All preliminary calculations were reviewed.

The final level of review was conducted by the project manager who reviewed all results generated within the laboratory.

12. Conclusions

Field testing of an Imbrium Systems' Jellyfish[®] Filter model JF4-2-1 with second-generation filtration cartridges was conducted in accordance with the TARP and VTAP field test protocols. The physical modeling campaign was carried out on the University of Florida campus with the full-scale unit loaded by rainfall-runoff from a surface parking watershed. A total of 25 monitored storm events, with 15 inches of cumulative rainfall depth, were treated by the JF4 during this study. Of the 25 storms treated, two storms generated flows exceeding the maximum design flow of 200 gpm. No maintenance was required or conducted during the 13-month monitoring period from May 28, 2010 to June 27, 2011.

Treatment results generated median SSC and TSS removal efficiency results of 99% and 89%, respectively. Median removal efficiency was 59% for Total Phosphorus and 51% for Total Nitrogen. For Total Copper, Zinc, Lead and Chromium median removal efficiencies were 90, 70, 81, and 36%, respectively. The d_{50} for influent and effluent particle sizes were 82 and 3 µm, respectively. Median head loss never exceeded 8.4 inches (21.4 cm) for any event and across the entire monitoring campaign the median head loss was 3.3 inches (8.3 cm). Dry basis particulate matter (PM) recovered from the treatment unit totaled 166 pounds, and the JF4-2-1 had a volumetric capacity to retain a significantly larger mass of PM. Median and peak head losses were driven predominately by flow rate and to a much lesser degree by filter cartridge ripening which was muted. At the completion of the monitoring campaign, a 95% mass balance was obtained on particulate matter (PM) which validates the testing methods used throughout this study. This mass balance on PM is an independent requirement to validate the influent and effluent monitoring and validates the most rigorous unit operation and process physical modeling available. The results obtained in this field study demonstrate that the Jellyfish Filter's particulate removal performance is reasonably insensitive to incoming particle size distribution (PSD) and runoff event duration.









INSPECTION & MAINTENANCE MANUAL FOR STORMWATER MANAGEMENT SYSTEMS

PROPOSED RETAIL MOTOR FUEL OUTLET TAX MAP 272 LOT 3 2255 LAFAYETTE ROAD PORTSMOUTH, NEW HAMPSHIRE





44 Stiles Road, Suite One Salem, NH 03079 (603) 893-0720

Prepared For:

Granite State Convenience, LLC 25 Springer Road Hooksett, NH 03106

> Revised: April 19, 2022 February 3, 2022

(GPI Project No.: NEX-2021163)

Granite State Convenience, LLC Proposed Retail Motor Fuel Outle Inspection & Maintenance Manual

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Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

SECTION 1 I & M DOCUMENTATION REQUIREMENTS

The Owner of Record shall be responsible for the continued operation, and maintenance of all stormwater management systems in accordance with this manual and Section 7.6.5 of the City of Portsmouth Site Plan Review Regulations. Logs of inspections and maintenance shall be maintained and filed with the City of Portsmouth as needed. Copies will need to be kept for the most recent three years and made available to the Planning Board and City Engineer upon request.

Logs shall include the date on which each inspection or maintenance task was performed, a description of the inspection findings or maintenance completed, and the name of the inspector or maintenance personnel performing the task. If a maintenance task requires the cleanout of any sediments or debris, the location where the sediment and debris was disposed after removal will be indicated. Disposal of the accumulated sediment and hydrocarbons must be in accordance with applicable local, state, and federal guidelines and regulations.

All stormwater facilities associated with this development are identified on Figure 1 contained within Section 3 of this manual and listed individually on the log form included herein, and shall be inspected and maintained in accordance with the procedures outlined in Section 4.

Granite State Convenience, Portsmouth, New Hampshire

February 3, 2022

SECTION 2 BMP SPECIFIC I & M PROCEDURES

Driveway/Parking Lot Sweeping

Sweeping shall be done once in the early fall and then immediately following spring snowmelt to remove sand and other debris and when visual buildup of debris is apparent. Pavement surfaces shall be swept at other times such as in the fall after leaves have dropped to remove accumulated debris. Since contaminants typically accumulate within 12 inches of the curbline, street cleaning operations should concentrate in cleaning curb and gutter lines for maximum pollutant removal efficiency. Other areas shall also be swept periodically when visual buildup of debris is apparent. Once removed from paved surfaces, the sweeping must be handled and disposed of properly. Disposal of the accumulated sediment and hydrocarbons must be in accordance with applicable local, state, and federal guidelines and regulations.

Deep Sump Hooded Catch Basins

Inspect and clean as required all catch basins at least two times per year including at the end of the foliage and snow removal seasons. Sediment must be removed whenever the depth of deposits is greater than or equal to one half the depth from the bottom of sump to the invert of the lowest pipe in the basin. If the basin outlet is designed with a hood to trap floatable materials check to ensure watertight seal is working. Damaged hoods should be replaced when noted by inspection. At a minimum, remove floating debris and hydrocarbons at the time of the inspection. Sediment and debris can be removed by a clamshell bucket; however, a vacuum truck is preferred. Disposal of the accumulated sediment and hydrocarbons must be in accordance with applicable local, state, and federal guidelines and regulations.

Outlet Aprons/Weirs

Inspect at least once annually for damage and deterioration. Repair damages immediately.

Oil/Water Separator

The system should initially be inspected within the first three months after completion of the site's construction and after any rainfall greater than 1-inch. The units should be inspected after every major storm but at least on a monthly basis. Cleaning of the units should be done at least twice a year and should include the following:

- 1. Removal of accumulated oil and grease and sediment by using a vacuum truck or similar catch basin cleaning device.
- 2. Visually inspect, and clean as needed, inlet and outlets including tees during each inspection.
- 3. At a minimum, remove any floating debris at the time of the inspection.

Disposal of the accumulated sediment and hydrocarbons must be in accordance with applicable local, state, and federal guidelines and regulations.

Hydrodynamic Separators (First Defense Units)

Initial maintenance to be performed twice a year for the first year after the unit is online and operational. A vacuum truck must be used at a minimum of once per year for sediment removal. Refer to the attached First Defense Owner's manual for operation and maintenance procedures and schedules thereafter.

Granite State Convenience, Portsmouth, New Hampshire

February 3, 2022

Jellyfish Filter Treatment Unit

See attached product maintenance materials by Contech ES.

Underground Detention System

All subsurface systems should initially be inspected within the first three months after completion of the site's construction.

Preventive maintenance should be performed at least every six months and sediment shall be removed from pretreatment BMP's after every major storm event. The Detention System shall be inspected on regular bi-annual scheduled dates. Sediment and debris removal should be through the use of truck mounted vacuum equipment. Outlet pipes should be flushed to point of discharge on the same frequency as mentioned above. Disposal of the accumulated sediment and hydrocarbons must be in accordance with applicable local, state, and federal guidelines and regulations.

The following is the recommended procedure to inspect the underground system in service:

- 1. Locate the riser or cleanout section of the system. The riser/cleanout will typically be 6 or 12" in diameter or larger.
- 2. Remove the lid from the riser/cleanout.
- 3. Measure the sediment buildup at each riser and cleanout location. Only certified confined space entry personnel having appropriate equipment should be permitted to enter the system.
- 4. Inspect each manifold, all laterals, and outlet pipes for sediment build up, obstructions, or other problems. Obstructions should be removed at this time.
- 5. If measured sediment build up is between 2" to 8", cleaning should be considered; if sediment build up exceeds 8", cleaning should be performed at the earliest opportunity. A thorough cleaning of the system (manifolds and laterals) shall be performed by water jets and/or truck mounted vacuum equipment.

Pretreatment BMP's shall be inspected and cleaned during the regular bi-annual inspections.

The inlet and outlet of the subsurface systems should be checked periodically to ensure that flow structures are not blocked by debris. All pipes connecting the structures to the system should be checked for debris that may obstruct flow. Inspections should be conducted monthly during wet weather conditions from March to November.

Vegetated Areas

Inspect slopes and embankments early in the growing season to identify active or potential erosion problems. Replant bare areas or areas with sparse growth. Where rill erosion is evident, armor the area with an appropriate lining or divert the erosive flows to on-site areas able to withstand the concentrated flows. During the summer months, all landscape features are to be maintained with the minimum possible amount of fertilizers, pesticides or herbicides.

Winter Maintenance

Proposed snow storage is located along the edge of the roadways. Any excess snow is to be trucked offsite. During the winter months all snow is to be stored such that snowmelt is

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controlled. Avoid disposing of snow on top of storm drain catch basins or in stormwater drainage swales or ditches. The minimum amount of deicing chemicals needed is to be used. It is recommended that winter maintenance contractors be current UNHT2 Green SnowPro Certified applicators or equivalent. In addition, a NHDES Salt Applicator Certification is recommended, but not required. Information on these certifications can be found in the links provided below:

- http://t2.unh.edu/green-snopro-training-and-nhdes-certification
- http://des.nh.gov/organization/divisions/water/wmb/was/salt-reduction-initiative/saltapplicator-certification.htm

Control of Invasive Species

During maintenance activities, check for the presence of invasive species. Invasive species must be managed/removed in accordance with RSA 430:530 and AGR 3800. See Section 4 of this manual for information from the University of New Hampshire Cooperative Extension and the New Hampshire Guide to Upland Invasive Species from the New Hampshire Department of Agriculture Markets and Food, Plant Industry Division or the information provided on their website (http://www.agriculture.nh.gov/divisions/plant-industry/invasive-plants.htm).

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

Revised: April 19, 2022

SECTION 3 LONG TERM MAINTENANCE PLAN EXHIBIT





Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

Revised: April 19, 2022

SECTION 4

CONTROL OF INVASIVE SPECIES

CONTACT INFORMATION

TERRESTRIAL PLANTS

Douglas Cygan, Invasive Species Coordinator, NH Department of Agriculture, Markets & Food, Division of Plant Industry, 29 Hazen Drive, Concord, NH 03301 (603) 271-3488, douglas.cygan@agr.nh.gov Website: www.agriculture.nh.gov

AQUATIC PLANTS

Amy Smagula, Clean Lakes and Exotic Species Coordinator, NH Department of Environmental Services, 29 Hazen Drive, PO Box 95, Concord, NH 03302 (603) 271-2248, asmagula@des.state.nh.us.

RESOURCES

NH Coastal Watershed Invasive Plant Partnership (CWIPP) www.des.nh.gov/organization/divisions/water/wmb/coastal/cwipp/index.htm **Invasive Plant Atlas of New England (IPANE)** http://invasives.eeb.uconn.edu/ipane Natural Resource Conservation Service (NRCS) http://plants.usda.gov New England Wildflower Society (NEWS) www.newfs.org New Hampshire Department of Agriculture, Markets & Food (DAMF) www.agriculture.nh.gov New Hampshire Department of Resources & Economic Development. Natural Heritage Bureau (DRED) http://www.naturalheritage.org New Hampshire Department of Resources & Economic Development. **Division of Forests and Lands (DRED)** http://www.nhdfl.org/organization/div nhnhi.htm New Hampshire Department of Environmental Services (DES) www.des.state.nh.us/wmb/exoticspecies New Hampshire Fish & Game Department www.wildlife.state.nh.us The Nature Conservancy (TNC) www.nature.org U.S. Department of Agriculture's Animal Plant Health Inspection Service (USDA

> APHIS) www.aphis.usda.gov University of New Hampshire Cooperative Extension (UNHCE) www.ceinfo.unh.edu

Funding for the printing of this booklet provided by: U.S. Department of Agriculture's Animal Plant Health Inspection Service

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New Hampshire Department of Agriculture Markets and Food, Plant Industry Division



5th Edition 2018

Douglas Cygan

New Hampshire Department of Agriculture, Markets & Food Terrestrial Invasive Plant Species

Introduction

Throughout the world, non-native invasive species have become an overwhelming problem resulting in impacts to the natural environment and managed landscapes. Invasive species typically possess certain traits that give them an advantage over most native species. The most common traits include the production of many offspring, early and rapid development, and adaptability and high tolerance to many environmental conditions. These traits allow invasive species to be highly competitive and, in many cases, suppress native species. Studies show that invasives can reduce natural diversity, impact endangered or threatened species, reduce wildlife habitat, create water quality impacts, stress and reduce forest and agricultural crop production, damage personal property, and cause health problems.

Invasive species began arriving in North America in the mid-to-late 1700s by various means. Many were brought here for ornamental uses, erosion control, or to provide for wildlife habitat. Others arrived inadvertently through international travel and commerce.

Impacts and Actions

Biologists have found that invasive species cover more than 100 million acres of land in the U.S. and their population numbers continue to spread. The repeated process of spread has become so extreme that invasive species cost the United States billions of dollars per year. This is a result of lost agricultural and forest crops, impacts to natural resources and the environment, and the control efforts required to eradicate them.

On February 3, 1999, President Clinton signed Executive Order 13112, which established the National Invasive Species Council. The Council is responsible for assessing the impacts of invasive species, providing the nation with guidance and leadership on invasive species issues, and seeing that federal programs are coordinated and compatible with state and local initiatives.

Each state is also required to participate by evaluating and responding to their invasive species concerns. In the summer of 2000, the State of New Hampshire passed House Bill 1258-FN, which created the Invasive Species Act (ISA) and the New Hampshire Invasive Species Committee.

GLOSSARY OF PLANT TERMS

Alternate: Arranged singly at each node, as leaves or buds on different sides of a stem.

Annual: Living or growing for only one year or season.

Aril: A fleshy, usually brightly colored cover of a seed that develops from the ovule stalk and partially or entirely envelops the seed.

Axis: The point at which the leaf is attached to the main stem or branch. Berry: A small, juicy, fleshy fruit.

Biennial: Having a life cycle that normally takes two growing seasons to complete.

Capsule: A dry dehiscent fruit that develops from two or more united capsules. **Compound:** Composed of more than one part.

Deciduous: Shedding or losing foliage at the end of the growing season.

Dehiscent: The spontaneous opening of a fruit at maturity.

Drupe: A fleshy fruit usually having a single hard stone enclosing a seed.

Entire: Referring to a leaf not having an indented margin.

Filiform: Having the form resembling a thread or filament.

Furrowed: A rut groove or narrow depression.

Glabrous: Having no hairs or projections; smooth.

Imbricate: To be arranged with regular overlapping edges.

Inflorescence: A cluster of small flowers arranged on a flower stalk.

Lanceolate: A leaf tapering from a rounded base toward an apex, lance-shaped

Lenticels: The small, corky pores or narrow lines on the surface of the stems of woody plants that allow the interchange of gases between the interior tissue and the surrounding air.

Lustrous: Having a sheen or glow.

Native: A species that originated in a certain place or region; indigenous.

Naturalized: Adapted or acclimated to a new environment without cultivation.

Opposite: Growing in pairs on either side of a stem.

Ovate: Broad or rounded at the base and tapering toward the end.

Panicle: A branched cluster of flowers in which the branches are racemes

Peduncle: The stalk of a solitary flower of an inflorescence.

Peltate: Leaf being round with the stem attached near its center.

Perennial: Living three or more years.

Perfect: Having both stamens and pistals in the same flower.

Pod: A dry, several-sealed, dehiscent fruit.

Pubescent: Covered in fine short hairs.

Raceme: Elongated cluster of flowers along the main stem in which the flowers at the base open first.

Rhizome: A horizontal, usually underground stem that often sends out roots and shoots from its nodes.

Samara: A winged, often one-seed indehiscent fruit as of the ash, elm or maple. Simple: Having no divisions or branches; not compound.

Umbel: A flat-topped or rounded inflorescence.

Lythrum salicaria - Purple Loosestrife

Family: Lythraceae Native to: Eurasia

Description: Perennial growing 30-80" tall by $\frac{2}{3}$'s as wide. Stems: 4-6 sided, turning woody in summer. Leaves: Opposite to whorled, lanceolate, 2-4" long. Flowers: Spiked raceme, purple to magenta, June to October. Fruit: Capsule. Habitat: Mostly found in wetlands and aquatic systems, full to partial sun. Spread: Each plant can produce approximately 2.5-4.5 million seeds. Seeds dispersed by water, wildlife and humans. Comments: Invades wetlands suppressing native species and destroying wildlife habitat. Controls: Hand pull, use a spade to dig larger plants or use biocontrols (Galerucella Spp., top left is a larvae & top right is an adult).





Photos by Douglas Cygan

Family: Poaceae

Native to: Eurasia

Phragmites australis - Common Reed

Description: Perennial rhizomatous grass growing 14' tall. Stems: Called 'culms' are large, hollow and grow up to 1" dia. Leaves: Lanceolate, up to 24" long, bluish-green in color. Flowers: Panicles with many spikelets having seven small reddish flowers. Habitat: Mostly found in marshlands, but also grows in freshwater wetlands and aquatic systems, full to partial sun. Spread: Spreads primarily by rhizomes. Comments: Forms dense colonies that suppress native species and alter wildlife habitat. Controls: Hand pull small plants. Use a spade to dig larger plants or apply herbicides.



New Hampshire Invasive Species Committee

The New Hampshire Invasive Species Committee (ISC) is an advisory group for the Commissioner of the NH Department of Agriculture, Markets & Food (DAMF) on matters concerning invasive species in the state. The ISC consists of 11 appointed members representing the following: the NH Department of Agriculture, the NH Department of Environmental Services, the NH Department of Resources & Economic Development, the NH Department of Transportation, the NH Department of Fish & Game, The College of Life Science & Agriculture of the University of NH, the UNH Cooperative Extension, environmental interests, horticultural interests, general public interests, and livestock owners & feed growers interests. The ISC meets regularly to conduct the following efforts:

- Review information;
- Evaluate and discuss potentially invasive plant, insect and fungi species of concern;
- Host guest presentations on related topics;
- Develop outreach and educational materials;
- Formulate management practices as guidance for the control of invasive species; and
- Prepare lists of proposed prohibited and restricted species.

(Note: This committee is not charged with the evaluation or listing of aquatic plant species, which is conducted by the Department of Environmental Services under RSA-487:16-a. However, a brief description of the program and four of the aquatic species are described on pages 29 & 30 of this book).

New Hampshire Rules

In accordance with the Invasive Species Act (ISA), HB 1258-FN, the DAMF is the lead state agency for terrestrial invasive plants, insects and fungi species. The DAMF has the responsibility for the evaluation, publication and development of rules on invasive plant species. This is for the purpose of protecting the health of native species, the environment, commercial agriculture, forest crop production, and human health. Therefore, the rule, Agr 3800, states "No person shall collect, transport, import, export, move, buy, sell, distribute, propagate or transplant any living or viable portion of any listed prohibited invasive plant species, which includes all of their cultivars and varieties, listed" (see the New Hampshire Department of Agriculture's website at www.agriculture.nh.gov to review the complete set of rules).





Invasive Upland Plant Species (Agr 3800)

Common Name	<u>Scientific Name</u>	Page	
Jorway Maple	Acer platanoides	6	
Tree of Heaven	Ailanthus altissima	7	
Barlic Mustard	Alliaria petiolata	8	
apanese Barberry	Berberis thunbergii	9	
European Barberry	Berberis vulgaris	10	
Driental Bittersweet	Celastrus orbiculatus	11	
potted Knapweed	Centaurea biebersteinii	12	
Black Swallow-Wort	Cynanchum nigrum	13	
ale Swallow-Wort	Cynanchum rosicum	13	
Autumn Olive	Elaeagnus umbellata	14	
Burning Bush	Euonymus alatus	15	
Biant Hogweed	Heracleum mantegazzianum	16	
Dame's Rocket	Hesperis matronalis	17	
erennial Pepperweed	Lepidium latifolium	18	
Blunt-Leaved Privet	Ligustrum obtusifolium	19	
howy Bush Honeysuckle	Lonicera x bella	20	
apanese Honeysuckle	Lonicera japonica	20	
Iorrow's Honeysuckle	Lonicera morrowii	21	
atarian Honeysuckle	Lonicera tatarica	21	
apanese Stilt-grass	Microstegium vimineum	22	
apanese Knotweed	Polygonum cuspidatum	23	
/lile-a-Minute Vine	Polygonum perfoliatum	23	
Bohemian Knotweed	Reynoutria japonica	23	
Common Buckthorn	Rhamnus cathartica	24	
Blossy Buckthorn	Rhamnus frangula	24	
/ultiflora Rose	Rosa multiflora	25	

Invasive Insect Species (To see the complete list of all 16 invasive insects refer to rules Agr 3800)			
Hemlock Wooly Adelgid	Adelges tsugae	26	
Emerald Ash Borer	Agrilus planipennis	27	
Asian Longhorned Beetle	Anoplothora glabripennis	28	

Invasive Aquatic Plant Species To see the complete list of invasive aquatic plants refer to DES's Env-Wq 1300 rules			
Variable Milfoil	Myriophyllum heterophyllum	29	
Purple Loosestrife	Lythrum salicaria	30	
Common Reed	Phragmites australis	30	

New Hampshire Department of Environmental Services Aquatic Invasive Plant Species

"Exotic aquatic species" are plants or animals that are not part of New Hampshire's native aquatic flora and fauna. Since the first exotic aquatic plant infestation in New Hampshire was discovered in 1965 in Lake Winnipesaukee, exotic aquatic plant infestations have increased to a total of 83 infestations in 72 waterbodies in 2008. Species present include variable milfoil (63 waterbodies), Eurasian milfoil (3 waterbodies), fanwort (9 waterbodies), water chestnut (1 waterbody) and Brazilian elodea (1 waterbody), Curly Leaf Pondweed (3 waterbodies), and European Naiad (3 waterbodies), and Didymo (1 waterbody). Most of these exotic plants can propagate by fragmentation as well as by seed.

Exotic aquatic plant fragments can easily become attached to aquatic recreational equipment, such as boats, motors, and trailers, and can spread from waterbody to waterbody through transient boating activities. Infestations can have detrimental effects on the ecological, recreational, aesthetic, and economic values of the state's precious surface waters, limiting use of the waterbodies and decreasing shorefront property values by as much as 1020 percent according to a UNH study (Halstead, et al., 2001).

Myriophyllum heterophyllum - Variable Milfoil Family: Haloragaceae Native to: Eurasia

Description: Submerged aquatic perennial growing 20' tall. Stems: Round, thick and reddish. Leaves: Feathery leaflets surrounding the stem. Flowers: Stalks that emerge above the water with green leaves, June to August. Habitat: Lakes, ponds, calm streams, and other similar aquatic systems with full to partial sun. Spread: It reproduces primarily by vegetative propagules when individual plant segments break off, and dispersed by water movement, humans, and boats. Comments: Invades water bodies, suppresses native species and destroys fish habitat. Controls: Prevention, hand pulling, bottom screening, and aquatic herbicide use.







Photos by Amy Smagula

N

Family: Cerambycidae Native to: Europe Anoplophora glabripennis - Asian Longhorned Beetle



Asian Longhorned Beetle-Anoplophora glabripennis (Photo by Chris Rallis)

The Asian longhorned beetle (ALB) is a serious threat to a large variety of deciduous hardwoods in North America. ALB is a large glossy black insect with white spots dotting its elytra. Adults grow to 1-1.5" long and have whitish bandings on their antennae. Females are typically bigger than males. Tree injury occurs when larvae tunnel through the xylem (heartwood) of the host, thus weakening the tree. Hosts trees include, but aren't limited to: Maple, Chestnut, Poplar, Willow, Birch, Elm, and Mountain ash. Adult females chew a crater in the bark and lay 1-egg per site. Upon hatching the larvae feed on the wood and emerge as adults in 1-2 years through perfect $\frac{3}{8}$ diameter exit holes. Other signs include coarse wood shavings called frass, oozing sap, oviposition sites, leaf-feeding damage, and mature beetles. If found, please call the NH Dept. of Agriculture at (603) 271-2561.



Egg (Rutgers University)



Larval damage (Rutgers Uni



Adult feeding damage on leaf 3/8" diameter exit hole Photos by Douglas Cygan, Chris Rallis & Rutgers University



There are many things that you, as an individual, can do to help control the spread of invasive species and preserve native flora and fauna:

- Minimize impacts to natural vegetation, soils, and drainage.
- Learn how to identify invasive plants and know how to tell them apart from native species.
- Control invasives on your property by following recommended practices.
- When landscaping, ask your local garden center or contact your County • Extension Service about alternative plantings.
- Become active in local or regional initiatives to control invasives.
- After working in an area with invasive species remove any soil, or propagules that may have adhered to clothing, shoes, vehicle tires, etc.

CONTROL METHODS

Mechanical: Mechanical control involves hand pulling, digging, cultivation, mowing, cutting or utilizing some type of physical barrier such as a tarpaulin, mulch, wood chips, etc. This method is most effective when populations of unwanted species are low.

Cultural: Cultural control is the manipulation of a plant community to prevent the introduction or spread of an unwanted species. This can be accomplished by modifying the growing environment such as the soil, available light or moisture, or planting trees or shrubs that can outcompete the invasive species.

Chemical: Chemical control involves the use of an approved herbicide to manage a targeted species. The application method must be chosen to avoid damage to beneficial or native species. The applicator must adhere to all State and Federal pesticide regulations and in many cases be licensed by the state. For more information, contact the NH Department of Agricul-Division 603-271-3550 Pesticide Control at ture's or www.agriculture.nh.gov.

Biological: Biological control is the use of native or introduced beneficial organisms to naturally reduce populations of unwanted species. Most biological controls are found to be self-sustaining and host specific.



Cutting-Hand tools Herbiciding Mowing Digging Cutting-Saws

Biocontrol

Acer platanoides - Norway Maple

Family: Aceraceae Native to: Europe



Norway Maple-Acer platanoides

Description: Large deciduous tree 60' high by 40' wide. Bark: Gravish and somewhat furrowed. Twigs: Smooth, olive-brown. Buds: Terminal, imbricate, rounded, smooth, greenish-red. Leaves: Opposite, 4-7" wide, 5-lobed, dark green to dark red above, lustrous below. Flowers: Greenishvellow, April. Fruit: Horizontal samara. Milky white sap-leaf petiole

Zone: 3-7. Habitat: Moist, well drained soils, full sun to partial shade. Spread: Seeds spread by wind and water. Comments: Leaf stalks exude milky white sap. Fast growing, buds break earlier than most native species. Naturalizes in woodlands where it can outcompete native species. Controls: Pull or dig seedlings/saplings.

Cut large trees and prune suckers when they sprout. Herbicide: foliar spray, cutstem, bark banding, or slash bark with ax and apply to wounds.



Norway Maple (in yellow) Invasion in Franklin, NH



Leaf with winged seed



Flowers greenish-yellow



Bark is gravish & furrowed Leaves turn vellow in Fall Photos by Douglas Cygan

Terminal buds rounded

Agrilus planipennis - Emerald Ash Borer

Family: Buprestidae Native to: Asia



Emerald Ash Borer-Agrilus planipennis

Dead standing Ash trees (Canadian Forest Service)

Emerald Ash Borers (EAB) are small invasive wood boring beetles that attack all species of ash trees (Fraxinus spp.). Native to East Asia, it is suspected that they were accidentally introduced to North America in infested wood packing material. The adults are 3/8" to $\frac{1}{2}$ " in length by 1/16" in width. Their bodies have a dark metallic green appearance. Adults emerge from a D-shaped exit hole from late May to mid-July and live for 3-6 weeks, during which time they feed on ash foliage, and fly 1-mile or so in search of a mate and to lay eggs. Females will lay 60-90 eggs in the crevices of ash tree bark. Larvae emerging from the eggs create distinctive S -shaped feeding galleries within the cambi-

um which is directly beneath the bark. These feeding galleries can girdle the tree and result in tree death. Movement of EAB into new uninfested areas is principally through transportation of firewood. If found, please contact the NH Dept. of Agriculture at (603) 271-2561.



Larvae in feeding galleries





Adult with wings spread





D-shaped exit hole EAB Purple prism trap Photos by Douglas Cygan & Chris Rallis
Adelges tsugae - Hemlock Wooly Adelgid

Family: Adelgidae Native to: Asia



Hemlock Wooly Adelgid-Adelges tsugae Nests

Hemlock Wooly Adelgid (Adelges tsugae) (HWA) is a serious pest to all North American hemlock trees (Tsuga spp.). It is native to Japan & China and was first found in the Pacific Northwest in the 1920's. By the 1950's it had reached the east coast and now infects hemlock trees from Georgia to Maine. It spreads by

movement of nursery stock, wind and animals. These insects are extremely small averaging about $\frac{1}{8}$ " in length with piercing-sucking mouth parts similar in appearance to aphids. All adults are females with each producing 50-300 eggs. To protect themselves & their eggs they produce a white-waxy covering. Adults Eggs & crawlers (Chris Rallis) insert their piercing mouth parts into the stem at the base of the needles. Trees die from needle loss & lack of nutrition. If found, please call the NH Dept. of Agriculture at (603) 271-2561.







Heavily infested branch



Crawlers (Chris Rallis) Crawler leaving nest (Chris Rallis) Photos by Douglas Cygan & Chris Rallis

Ailanthus altissima - Tree of Heaven

Family: Simaroubaceae Native to: China



Tree of Heaven-Ailanthus altissima

Tree of Heaven invasion

Description: Deciduous tree up to 60' tall by 40' wide. Bark: Gravish, slightly Twigs:Reddish-brown. furrowed. Leaves: Compound, 18-24" long with 13 -25 leaflets arranged alternately on stem, lanceolate, 3-5" long with 2-4 teeth near base. Flowers: Panicles, 8-16" long, yellowish-green, mid-June. Fruit: Samara. Zone: 4-8. Habitat: Highly adaptable and pollution tolerant, full sun to partial shade. Spread: Seeds are wind dispersed. Comments: Very fast growing, dense canopy shades out native species. Controls: Remove seedlings and saplings by hand. Larger trees can be mechanically removed or cut. To prevent suckering, if trees are cut, apply herbicide to cut portion of stump.









Bark gravish & furrowed Winged seed cluster Photos by Douglas Cygan

DO NOT MOVE FIREWOOD

Alliaria petiolata - Garlic Mustard

Family: Cruciferae Native to: Europe



Garlic Mustard-Alliaria petiolata

Description: Cool season biennial, 2nd year plants flower and reach $2-3^{1}/2$ tall. Leaves: Triangular, coarsely toothed, heart-shaped. Flowers: Umbel, small, 4petals, white, April-May. Fruit: Pods, seeds turn black when mature. Zone: 4-8. Habitat: Prefers moist shaded floodplains, forests and roadsides, adaptable to most soil and light conditions. Spread: Seeds spread by water and wildlife. Comments: Plants spread quickly into natural areas leading to competition and displacement of native species. Controls: Small populations can be hand pulled while large populations can be continuously cut back to prevent flower-

ing and seed production. Herbicide treatments are also effective.



Woodland invasion (photo by Cornell University)





Flowers 4-petaled, white



Flower buds

Photos by Douglas Cygan

Rosa multiflora - Multiflora Rose

Family: Rosaceae Native to: Japan & Korea



Multiflora Rose-Rosa multiflora

Multiflora Rose invasion, Canterbury, NH

Description: Hardy shrub / climber reaching up to 15' or more in height and 10' in width. Stems: Long and arching, forming dense clumps, thorns may or may not be present. Leaves: Alternately arranged, compound with 7-9 leaflets and having feather margins at base. Flowers: Clusters of white or pink, June to July. Fruit: Rose hips turn red in fall. Zone: 3-8. Habitat: Prefers moist, well drained soils, full sun. Spread: Fruits with seeds are dispersed by birds. Comments: Very aggressive, leading to competition and displacement of native species. Controls: Hand or mechanical removal. cutting, or herbicide application.





Twig/stem bark







Fruit is called a hip Photos by Douglas Cygan

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Rhamnus cathartica - Common Buckthorn

Family: Rhamnaceae Native to: Eurasia

Description: Deciduous shrub or small tree measuring 20' by 15'. Bark: Gravish to brown with raised lenticels. Stems: Cinnamon colored with terminal spine. Leaves: Alternate, simple and broadly ovate with toothed margins. Flowers: Inconspicuous, 4-petaled, greenishyellow, mid-June. Fruit: Fleshy, 1/4" diameter turning black in the fall. Zone: 3-7. Habitat: Adapts to most conditions including pH, heavy shade to full sun. Spread: Seeds are bird dispersed. Comments: Highly: Aggressive, fast growing, outcompetes native species. Controls: Remove seedlings and saplings by hand. Larger trees can be cut or plants can be treated with an herbicide.







Family: Rhamnaceae

Native to: Japan

Rhamnus frangula - Glossy Buckthorn

Description: Tall deciduous shrub up to 20' in height by 15' wide, **Bark:** Gravish with whitish lenticels. Twigs: Reddishbrown. Leaves: Ovate, 4-5" long by 3-4" wide, arranged alternate or whorled on stem. Flowers: Small, greenishwhite, mid-June. Fruit: Fleshy, turning black in the fall. Zone: 2-7. Habitat: Highly adaptable and pollution tolerant, full sun to partial shade. Spread: Seeds are bird dispersed. Comments: Very fast growing, dense canopy shades out native species. Controls: Remove seedlings and saplings by hand. Larger trees can be cut or herbicide may be used.





Berberis thunbergii - Japanese Barberry

Family: Berberidaceae Native to: Japan



Japanese Barberry-Berberis thunbergii

Japanese Barberry invasion, Antrim, NH



'Crimson Pygmy' variety







Flowers vellowish



Fruit is a fleshy drupe Photos by Douglas Cygan





Thorn

Frost covered Barberry

Berberis vulgaris - European Barberry

Family: Berberidaceae Native to: China



European Barberry-Berberis vulgaris

Description: Shrub 3-8' in height by 3-6' in width. Stems: Tan bark with 3 long spines at each leaf axis. Leaves: Alternate, simple, $\frac{1}{2}$ "-1 $\frac{1}{2}$ " long, bright green above, dull below. Flowers: Perfect, yellow, $\frac{1}{2}$ " long, mid-April to May. Fruit: Oblong drupe turning pale red in fall. Zone: 4-8. Habitat: Prefers full sun to partial shade and open spaces to wooded areas. Spread: Seeds are dispersed by birds and wildlife. Comments: Highly adaptable to most environments and is pollution tolerant. Controls: Hand pull young plants. Cut or mechanically remove older larger plants or apply approved herbicides for large

populations.



Woodland invasion, Claremont, NH





Flowers

Stems

Flowers whitish-vellow



Photos by Douglas Cygan

Polygonum cuspidatum - Japanese Knotweed Family: Polygonaceae Native to: Japan

Description: Perennial reaching 10' in height and width. Bohemian Knotweed (Revnoutria x bohemica) is similar. Stems: Greenish, hollow and jointed, similar to bamboo. Leaves: Alternate, broadly ovate, 3-7" long. Flowers: Small, whitish, forming panicles, August-September. Seeds: Calyx, brown, triangular. Habitat: Found in woodland sites, open spaces, ditches, roadsides, riverbanks. Prefers moist, well-drained soils. Spread: Stem & root fragments, and by seed. Comments: Aggressive, spreads quickly along surface waters and in right-of-ways. Controls: Do **not mow**, cut stems at base then smother by covering area with heavy-duty fabric/plastic, herbicides also recommended.







Polygonum perfoliatum - Mile-a-Minute Vine Family: Polygonaceae Native to: Asia

Description: Very fast growing herbaceous perennial vine growing to 25' in height. Stems: Greenish with stiff barbs used for support. Leaves: Alternate, triangular in shape with clasping bract at the base, 1-3" long. Flowers: Racemes, inconspicuous and white forming at the bract, August - October. Seeds: An achene within a greenish, berry-like fruit. Habitat: Grows in partial shade to full sun, fields, roadsides & forests. Prefers moist, well-drained soils. Spread: Seed spread by birds & wildlife. Comments: Fast growing, aggressive. Controls: Mowing, hand cutting or herbicide use is recommended.







Photos by Leslie J. Mehrhoff

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Microstegium vimineum - Japanese Stilt Grass





Japanese Stilt Grass-Microstegium vimineum

Description: Weak-stemmed annual grass, reaching 2-4' tall. Leaves: Lanceolate, tapered at both ends, 2-3" long with silvery stripe of reflective hairs down the midrib. Flowers: Racemes occur at the ends of the stalk itself, late August. Fruit: Achenes develop in late fall. Zone: 5-11. Habitat: Occurs along riverbanks, floodplains, forests and roadsides, adaptable to most soil and light conditions. Spread: Seeds spread by water, wildlife & humans. Comments: Plants spread quickly into natural areas leading to competition and displacement of native species. Controls: Small populations can be hand pulled while large populations can be continuously cut back to prevent flowering and seed production. Herbicide treatments are also effective.



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Japanese Stilt Grass woodland invasion



Root (UMASS Extension)



Leaf with silvery reflective hairs along midrib



Seed-Achene Fall-leaves turn purplish Photos courtesy of Leslie J. Mehrhoff/UCONN-IPANE and UMASS Extension

Celastrus orbiculatus - Oriental Bittersweet





Oriental Bittersweet-Celastrus orbiculatus

Oriental Bittersweet invasion, Concord, NH

Description: Deciduous vine reaching heights of 40-60'. Bark: Tannish, furrowed. Leaves: Alternate, ovate, bluntly toothed, 3-4" long by 2/3's as wide, tapered at the base. Flowers: Small, greenish, blooming in spring. Fruit: Yellow dehiscent capsule surrounding an orangered aril. Fruits occur in the axils of the whereas native bittersweet stems (Celastrus scandens) fruits at the ends. Zone: 4-8. Habitat: Disturbed edges, roadsides, fields, forests and along rivers and streams. Spread: Birds and humans. Comments: Very aggressive, climbs up and over trees and smothers them. Do not buy wreaths made of these vines. Con-

trols: Difficult to manage. Cutting, pulling, or recommended herbicide use applied to foliage, bark, or cut-stump.











Mature Orange-yellow fruit Photos by Douglas Cygan

Fruit is a fleshy capsule

Centaurea maculosa - Spotted Knapweed

Family: Compositae Native to: Eurasia



Spotted Knapweed—Centaurea maculosa

Description: Tall erect herbaceous perennial living 3-5 years. **Leaves:** Alternate, divided, Pale green, 1-3" long. **Flowers:** Aster-like, terminal, purple, July-August. **Fruit:** Each plant produces thousands of brownish seeds per year. **Zone:** 3-10. **Habitat:** Invades dry sunny roadsides, fields and waste places. Its

large taproot allows it to survive harsh winters and draught **Spread:** Seeds spread by wind and wildlife. **Comments:** Plants spread quickly into natural meadows and fields leading to competition and displacement of native species. Roots excrete a toxin killing off other plants. **Controls:** Small populations can

be hand pulled while large populations can be continuously cut back to prevent flowering and seed production. Herbicide treatments are also effective.



Invasion (photo by Leslie Mehrhoff)





Seed head

Flowers-Aster like



Stems Seeds Photos by Leslie Mehrhoff & Douglas Cygan

Lonicera morrowii - Morrow's Honeysuckle Family: Caprifoliaceae Native to: Japan

Description: Shrub reaching 6-8' tall. Stems: Smooth, glabrous, Tannish, hollow. Leaves: Ovate, simple, entire, opposite, pubescent beneath, $1-2^{1}/_{2}$ " long. Flowers: Tubular, white, turning yellow with age, May to June. Fruits: Berry turning red. Zone: 3 . Habitat: Moist to wet shaded floodplains, forests, roadsides, fields, waste places. Spread: Seeds are dispersed by wildlife and humans. Comments: Rapidly invades sites, forming a dense vegetative layer that outcompetes native flora and fauna species. Controls: Hand control is effective for small plants, while mechanical removal and repetitive cutting also work well. Herbicide treatment is better for areas with greater infestations.







Lonicera tatarica - Tatarian Honeysuckle

Family: Caprifoliaceae Native to: Eurasia

Description: Upright deciduous shrub reaching 6-15' tall. Stems: Smooth, glabrous, tan, hollow. Leaves: Ovate, smooth, bluish-green, opposite, $1-2^{1}/2^{"}$ long. Flowers: Tubular, pink or white, April to May. Fruit: Berry with two seeds, turning red in fall. Zone: 3. Habitat: Under story species in woodland sites, also invades open spaces. Thrives in moist soils. Spread: Seeds dispersed by wildlife and humans. Comments: Rapidly invades forests, fields, roadsides and floodplains. Outcompetes native species. Controls: Hand control is effective for small plants while mechanical removal, cutting and chemical applications are better for larger stands.







Photos by Leslie J. Mehrhoff & Berry Photo by Douglas Cygan

Lonicera x bella - Showy Bush Honeysuckle

Family: Caprifoliaceae Native to: Eurasia

Description: Shrub reaching 20' in height and width. Stems: Greenish to tan with corky wings. Leaves: Oppositely arranged, simple and elliptic, 1-3" long by half as wide, light green. Flowers: Yellow, white or pink, May to early June. Fruit: Fleshy red, forming in pairs in leaf axis. Zone: 4. Habitat: Prefers dry upland soils, full sun to heavy shade, pH adaptable. Spread: Seeds are dispersed by birds. Comments: L. x bella is a cross between L. tatarica & L. morrowii. Spreads into natural areas forming dense stands, which displace native species. Controls: Hand or mechanical removal, continuous cutting, girdling, and herbicide treatment.







Photos courtesy of Leslie J. Mehrhoff/UCONN-IPANE

Lonicera japonica - Japanese Honeysuckle

Family: Caprifoliaceae Native to: Eurasia

Description: Climbing vine. Stems: Reddish-brown, pubescent. Leaves: Opposite and not clasping the stem as opposed to the three native honeysuckle vines that do clasp the stem, oblong, $1^{1/2}$ -2" long, rounded at base. Flowers: Tubular, white or yellow, fragrant, May to mid-July. Fruit: Berry, smooth, blackish to slightly purplish. **Zone:** 4-8. Habitat: Prefers moist soils and full sun to partial shade. Spread: Seeds spread by wildlife. Comments: Vines grow quickly, covering native vegetation, resulting in loss of habitat. Controls: hand or mechanical removal, cutting, girdling, chemical.







otos courtesy of John M. Randall/The Nature Conservancy & Leaf Photo by Leslie J. Mehrhoff

Cynanchum nigrum - Black Swallow-Wort

Family: Asclepiadaceae Native to: Eurasia

Description: Perennial herbaceous vine that grows to 6'. Leaves: Opposite, lanceolate, dark glossy green, simple with a smooth edge, 2-4" long. Flowers: Small $^{1}/_{4}$ ", 5-petaled, purplish, from June to September. Seed: Seeds are similar to those of milkweed. Zone: 4 to 8. Habitat: It prefers full to partial sun. Spread: Seeds dispersed by wind. Comments: Invades roadsides, fields, disturbed sites, meadows, and woodlands, outcompeting native species. Controls: Hand pull young plants. Remove and destroy seed pods before they open. Apply herbicides as a foliar spray during the growing season. If plants are to be dug, use a spade and make sure that all root fragments are removed.







Photos by Douglas Cygan

Cynanchum rossicum - Pale Swallow-Wort

Family: Asclepiadaceae Native to: China

Description: Perennial vine growing to 3-6'. Very similar to black swallowwort with the exception of the flowers. **Leaves:** Opposite, lanceolate, 2-4" long. **Flowers:** Magenta, ³/₈", flowering from June to September. **Seed:** Seeds are similar to milkweed. **Zone:** 4 to 8. **Habitat:** It prefers full to partial sun. **Spread:** Seeds dispersed by wind. **Comments:** Invades roadsides, fields, disturbed sites, meadows and woodlands. **Controls:** Hand pull young plants. Remove and destroy seed pods before they open. Apply herbicides as

a foliar spray. Dig using a spade to ensure all root fragments are removed.







Photos courtesy of John M. Randall/The Nature Conservancy

Elaeagnus umbellata - Autumn Olive

Family: Elaeagnaceae Native to: Asia



Autumn Olive-Elaeagnus umbellata

Description: Weedy deciduous shrub measuring 20' by 20'. Bark: Silverygray and smooth with whitish lenticels. Stems: Cinnamon-brown. Leaves: Elliptical, 2-3" long, glossy, green above and silverish below. Flowers: Solitary, whitish, 4-petaled, mid-June. Fruit: Drupe. Zone: 3-8. Habitat: Naturalizes in open spaces exposed to full sun. Spread: Seeds dispersed by birds and wildlife. Comments: Very aggressive. Outcompetes and displaces native species. Controls: Remove seedlings and saplings by hand. Larger shrubs can be mechanically removed, or cut and apply herbicide to stump.







Flowers whitish



Fruit is a fleshy drupe Photos by Douglas Cygan

Ligustrum obtusifolium - Blunt-leaved Privet

Family: Oleaceae Native to: Europe



Blunt-leaved Privet-Ligustrum obtusifolium

Description: Shrub reaching 12' tall by 10-12' wide. Stems: Greenish, smooth. Leaves: Opposite, simple and elliptic, 1-3" long by half as wide, blunt tipped, light green. Flowers: Small white panicles, May to early June. Fruit: Small blackish drupe. Zone: 4-7. Habitat: Prefers dry upland soils, full sun to heavy shade, pH adaptable. Spread: Seeds dispersed by birds. Comments: Becomes established in natural areas leading to competition and displacement of native species. Controls: Hand or mechanical removal, cutting, herbicide applications such as foliar or cut-stem.



Blunt-leaved Privet (Photo: Leslie J. Mehrhoff)



Twig/stem bark





Leave

Terminal bud







Fall color Fruit is a dark drupe Photos by Douglas Cygan & Leslie Mehrhoff





Lepidium latifolium - Perennial Pepperweed Family: Native t





Perennial Pepperweed-Lepidium latifolium

Description: Long lived perennial growing 2-4' tall. **Leaves:** Alternate, lanceolate with serrated edge. **Flowers:** Terminal, tightly clustered, white, July. **Fruit:** Silicle, rounded, flattish, hairy $1/_{16}$ " long. **Zone:** 4-8. **Habitat:** Prefers wet, brack-ish soils such as coastal tidal marshes and ditches, wetlands, and floodplains.

Spread: Seeds and creeping rhizome fragments spread by water, wildlife and humans. **Comments:** Plants spread quickly into natural areas leading to competition and displacement of native coastal wetland species. **Controls:** Small populations can be hand pulled while large populations can be continuously cut

back to prevent flowering and seed production. Herbicide treatments are also effective.









Persistent stems Seeds (photo—USDA) Photos by Kevin Lucey & Jennifer Forman

Rhizome root with shoot

Euonymus alatus - Burning Bush

Family: Celastraceae Native to: Asia



Burning Bush-Euonymus alatus

Burning Bush invasion, Boscawen, NH

Description: Deciduous shrub reaching 20' in height and width. Stems: Greenish with corky wings. Leaves: Oppositely arranged, simple and elliptic, 1-3" long by half as wide, light green. Flowers: Inconspicuous greenish-yellow, May to June. Fruit: Fleshy green capsule turning red in fall. Zone: 3 to 8. Habitat: Prefers dry upland soils, full sun to heavy shade, pH adaptable. Spread: Seeds are dispersed by birds and wildlife. Comments: Outcompetes and displaces native species. Controls: Hand remove seedlings and saplings. Use a spade or shovel to dig out larger plants. Large populations may be controlled with herbicide use.







Terminal buds







Fall color Fruit is a fleshy capsule Photos by Douglas Cygan

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Heracleum mantegazzianum - Giant Hogweed

Family: Apiaceae Native to: China



Giant Hogweed-Heracleum mantegazzianum

Description: Biennial growing to 15' tall. Stems: Greenish with purple splotches, 2-4" diameter with coarse hairs, hollow. Leaves: Large, compound, deeply incised, 3-5' wide, hairy on underside. Flowers: White inflorescence, 1-2' in diameter, May-June. Seeds: Flattened, $\frac{3}{8}$ " long, ovate with 4 brown resin canals. Zone: 3-8. Habitat: Found in wet areas, roadsides, gardens, open spaces, full sun to partial shade. Spread: Seeds dispersed by water, wildlife and humans. Comments: The clear, watery sap is phototoxic to human skin, causing severe blistering and burns. Spreads readily and displaces native species. Controls: Remove plants by digging up tap root. Herbicide can also be used as a foliar treatment.



Open field invasion (Photo-Bugwood.org)



UGA5186075





130-150 Floral ravs



Flowers whitish umbel

Photos by Douglas Cygan

Hesperis matronalis - Dame's Rocket

Family: Brassicaceae Native to: Eurasia



Dame's Rocket—Hesperis matronalis

Dame's Rocket invasion

Description: Cool season biennial, 2nd year plants flower and reach 30" tall. Leaves: Alternately arranged and lanceolate in shape with toothed margins. Flowers: Terminal racemes, 4-petals. purplish, early to mid spring. Fruit: Pods, seeds turn brown when mature. Zone: 4-8. Habitat: Prefers partial sun, moist to mesic conditions such as floodplains, forests and roadsides, adaptable to full sun with adequate moisture. Spread: Seeds spread by water and wildlife. Comments: Plants spread quickly into natural areas leading to competition and displacement of native species. Controls: Small populations can be hand pulled while large populations can be continuously cut back to prevent flowering and seed production. Herbicide treat-



ments are also effective.







Flower buds





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Stormwater Inspection & Maintenance Manual

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

Revised: April 19, 2022

SECTION 5 STORMWATER INSPECTION & MAINTENANCE LOG

STORMWATER INSPECTION MAINTENANCE LOG

2255 Lafayette Road- Portsmouth, NH

General Information					
Project Name	Retail Motor Fuel Outlet	Location	Portsmouth, NH		
Date of Inspection		Start/ End Time			
Inspector's Name(s)					
Inspector's Title(s)					
Inspector's Contact					
Information					

	Site Specific BMP's	Maintenance Interval
1	Street Sweeping	1 year
2	Deep Sump Catch Basins	6 months
3	Outlet Apron/Weirs	1 Year
4	Oil/Water Separator	6 months
5	Hydrodynamic Separators (First Defense Unit)	1 Year (See separate maintenance log for First Defense Unit)
6	Jellyfish Filter	1 Year (See separate maintenance log for Jellyfish Filter)
7	Underground Detention System	6 months

STORMWATER INSPECTION MAINTENANCE LOG

2255 Lafayette Road - Portsmouth, NH

	Corrective					
BMB Description	Action	Notes				
	Required?	Notes				
	nequieu.					
	Street Swee	ping				
Evidence of debris accumulation	Yes No					
Evidence of oil grease	Yes No					
Other (specify)	Yes No					
	Deep Sump Catc	h Basins				
Grates clear of debris	Yes No					
Inlet and outlet clear of debris	Yes No					
Evidence of oil grease	🗌 Yes 🗌 No					
Observance of accumulated sediment	🗌 Yes 🗌 No	Sediment Depth =				
Evidence of structural deterioration	🗌 Yes 🗌 No					
Evidence of flow bypassing facility	🗌 Yes 🗌 No					
Other (specify)	🗌 Yes 🗌 No					
	Outlet Aprons	/Weirs				
Inlet/ inflow pipe clear of debris	Yes No					
Overflow spillway clear of debris	Yes No					
Evidence of rilling or gullying	Yes No					
Tree growth	🗌 Yes 🗌 No					
Other (specify)	Yes No					
Oil / Water Seperator						
Grates clear of debris	Yes No					
Inlet and outlet clear of debris	Yes No					
Observance of accumulated sediment	Yes No	Sediment Depth =				
Evidense of oil grease	🗌 Yes 🗌 No					
Evidence of flow bypassing facility	Yes No					
Hydrody	namic Separator (First Defense Unit)				
See separate maintenance log for First De	fense Unit					
	Jellyfish Fil	ter				
See separate maintenance log for Jellyfish	Filter					
Ur	nderground Deten	tion System				
Inlet and outlet clear of debris	Yes No					
Pipe bottom clear of debris	Yes No					
Observance of accumulated sediment	Yes No	Sediment Depth =				
Bottom dewaters within 72 hrs. of a	Yes No					
storm event						
Outlet control structure clear of debris	Yes No					
Other (specify)						

NOTE: Photos shall be provided with each inspection log and shall be sufficiently labeled to identify photo location.

Stormwater Inspection & Maintenance Manual

Granite State Convenience, Portsmouth, New Hampshire February 3, 2022

SECTION 6

Revised: April 19, 2022

DE-ICING LOG

Deicing Log

Date Applied	Type of Deicing Material	Amount Applied





Operation and Maintenance Manual

First Defense® and First Defense® High Capacity

Vortex Separator for Stormwater Treatment

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Hydro Maintenance Services

Hydro International has been engineering stormwater treatment systems for over 30 years. We understand the mechanics of removing pollutants from stormwater and how to keep systems running at an optimal level.

NOBODY KNOWS OUR SYSTEMS BETTER THAN WE DO



AVOID SERVICE NEGLIGENCE

Sanitation services providers not intimately familiar with stormwater treatment systems are at risk of the following:

- Inadvertently breaking parts or failing to clean/replace system components appropriately.
- Charging you for more frequent maintenance because they lacked the tools to service your system properly in the first place.
- Billing you for replacement parts that might have been covered under your Hydro warranty plan
- Charging for maintenance that may not yet have been required.

LEAVE THE DIRTY WORK TO US

Trash, sediment and polluted water is stored inside treatment systems until they are removed by our team with a vactor truck. Sometimes teams must physically enter the system chambers in order to prepare the system for maintenance and install any replacement parts. Services include but are not limited to:

- · Solids removal
- · Removal of liquid pollutants
- Replacement media installation (when applicable)



BETTER TOOLS, BETTER RESULTS

Not all vactor trucks are created equal. Appropriate tools and suction power are needed to service stormwater systems appropriately. Companies who don't specialize in stormwater treatment won't have the tools to properly clean systems or install new parts.



SERVICE WARRANTY

Make sure you're not paying for service that is covered under your warranty plan. Only Hydro International's service teams can identify tune-ups that should be on us, not you.

TREATMENT SYSTEMS SERVICED BY HYDRO:

- Stormwwater filters
- Stormwater separators
- Baffle boxes
- Biofilters/biorention systems
- Storage structures
- Catch basins
- Stormwater ponds
- Permeable pavement





1 (888) 382-7808

LEARN MORE AT HYDRO-INT.COM/SERVICE



I. First Defense® by Hydro International

Introduction

The First Defense[®] is an enhanced vortex separator that combines an effective and economical stormwater treatment chamber with an integral peak flow bypass. It efficiently removes total suspended solids (TSS), trash and hydrocarbons from stormwater runoff without washing out previously captured pollutants. The First Defense[®] is available in several model configurations (refer to *Section II. Model Sizes & Configurations*, page 4) to accommodate a wide range of pipe sizes, peak flows and depth constraints.

Operation

The First Defense® operates on simple fluid hydraulics. It is selfactivating, has no moving parts, no external power requirement and is fabricated with durable non-corrosive components. No manual procedures are required to operate the unit and maintenance is limited to monitoring accumulations of stored pollutants and periodic clean-outs. The First Defense® has been designed to allow for easy and safe access for inspection, monitoring and clean-out procedures. Neither entry into the unit nor removal of the internal components is necessary for maintenance, thus safety concerns related to confined-spaceentry are avoided.

Pollutant Capture and Retention

The internal components of the First Defense[®] have been designed to optimize pollutant capture. Sediment is captured and retained in the base of the unit, while oil and floatables are stored on the water surface in the inner volume (Fig.1).

The pollutant storage volumes are isolated from the built-in bypass chamber to prevent washout during high-flow storm events. The sump of the First Defense[®] retains a standing water level between storm events. This ensures a quiescent flow regime at the onset of a storm, preventing resuspension and washout of pollutants captured during previous events.

Accessories such as oil absorbent pads are available for enhanced oil removal and storage. Due to the separation of the oil and floatable storage volume from the outlet, the potential for washout of stored pollutants between clean-outs is minimized.

Applications

- Stormwater treatment at the point of entry into the drainage line
- Sites constrained by space, topography or drainage profiles with limited slope and depth of cover
- Retrofit installations where stormwater treatment is placed on or tied into an existing storm drain line
- · Pretreatment for filters, infiltration and storage

Advantages

- Inlet options include surface grate or multiple inlet pipes
- Integral high capacity bypass conveys large peak flows without the need for "offline" arrangements using separate junction manholes
- Proven to prevent pollutant washout at up to 500% of its treatment flow
- Long flow path through the device ensures a long residence time within the treatment chamber, enhancing pollutant settling
- Delivered to site pre-assembled and ready for installation



Fig.1 Pollutant storage volumes in the First Defense®.

II. Model Sizes & Configurations

The First Defense[®] inlet and internal bypass arrangements are available in several model sizes and configurations. The components of the First Defense[®]-4HC and First Defense[®]-6HC have modified geometries as to allow greater design flexibility needed to accommodate various site constraints.

All First Defense[®] models include the internal components that are designed to remove and retain total suspended solids (TSS), gross solids, floatable trash and hydrocarbons (Fig.2a - 2b). First Defense[®] model parameters and design criteria are shown in Table 1.

First Defense® Components

- 1. Built-In Bypass
- 4. Floatables Draw-off Port
- 2. Inlet Pipe
- 5. Outlet Pipe
- 3. Inlet Chute

a.

- 6. Floatables Storage
- 7. Sediment Storage
- 8. Inlet Grate or Cover





Fig.2a) First Defense[®]-4 and First Defense[®]-6; b) First Defense[®]-4HC and First Defense[®]-6HC, with higher capacity dual internal bypass and larger maximum pipe diameter.

First Defense [®] High Capacity	Diameter	Typical TSS Treatment Flow Rates		Peak I	Maximum Pine	¹ Oil Storage 1 Capacity	Typical Sediment Storage Capacity ²	Minimum Distance from Outlet Invert to Top of Rim ³	Standard Distance from Outlet Invert to Sump Floor
Model Number	Diamotor	NJDEP Certified	106µm	Flow Rate Diameter ¹					
	(ft / m)	(cfs / L/s)	(cfs / L/s)	(cfs / L/s)	(in / mm)	(gal / L)	(yd³/ m³)	(ft / m)	(ft / m)
FD-3HC	3 / 0.9	0.84 / 23.7	1.60 / 45.3	15 / 424	18 / 457	125 / 473	0.4 / 0.3	2.0 - 3.5 / 0.6 - 1.0	3.71 / 1.13
FD-4HC	4 / 1.2	1.50 / 42.4	1.88 / 50.9	18 / 510	24 / 600	191 / 723	0.7 / 0.5	2.3 - 3.9 / 0.7 - 1.2	4.97 / 1.5
FD-5HC	5 / 1.5	2.34 / 66.2	2.94 / 82.1	20 / 566	24 / 609	300 / 1135	1.1 / .84	2.5 - 4.5 / 0.7 - 1.3	5.19 / 1.5
FD-6HC	6 / 1.8	3.38 / 95.7	4.73 / 133.9	32 / 906	30 / 750	496 / 1,878	1.6 / 1.2	3.0 - 5.1 / 0.9 - 1.6	5.97 / 1.8
FD-8HC	8 / 2.4	6.00 / 169.9	7.52 / 212.9	50 / 1,415	48 / 1219	1120 / 4239	2.8 / 2.1	3.0 - 6.0 / 0.9 -1.8	7.40 / 2.2

¹Contact Hydro International when larger pipe sizes are required.

²Contact Hydro International when custom sediment storage capacity is required.

³Minimum distance for models depends on pipe diameter.

Hydro International (Stormwater), 94 Hutchins Drive, Portland ME 04102 Tel: (207) 756-6200 Fax: (207) 756-6212 Web: www.hydro-int.com

III. Maintenance

Overview

The First Defense[®] protects the environment by removing a wide range of pollutants from stormwater runoff. Periodic removal of these captured pollutants is essential to the continuous, long-term functioning of the First Defense[®]. The First Defense[®] will capture and retain sediment and oil until the sediment and oil storage volumes are full to capacity. When sediment and oil storage capacities are reached, the First Defense[®] will no longer be able to store removed sediment and oil. Maximum pollutant storage capacities are provided in Table 1.

The First Defense[®] allows for easy and safe inspection, monitoring and clean-out procedures. A commercially or municipally owned sump-vac is used to remove captured sediment and floatables. Access ports are located in the top of the manhole.

Maintenance events may include Inspection, Oil & Floatables Removal, and Sediment Removal. Maintenance events do not require entry into the First Defense[®], nor do they require the internal components of the First Defense[®] to be removed. In the case of inspection and floatables removal, a vactor truck is not required. However, a vactor truck is required if the maintenance event is to include oil removal and/or sediment removal.

Maintenance Equipment Considerations

The internal components of the First Defense[®]-HC have a centrally located circular shaft through which the sediment storage sump can be accessed with a sump vac hose. The open diameter of this access shaft is 15 inches in diameter (Fig.3). Therefore, the nozzle fitting of any vactor hose used for maintenance should be less than 15 inches in diameter.



Fig.3 The central opening to the sump of the First Defense®-HC is 15 inches in diameter.

Determining Your Maintenance Schedule

The frequency of clean out is determined in the field after installation. During the first year of operation, the unit should be inspected every six months to determine the rate of sediment and floatables accumulation. A simple probe such as a Sludge-Judge[®] can be used to determine the level of accumulated solids stored in the sump. This information can be recorded in the maintenance log (see page 9) to establish a routine maintenance schedule.

The vactor procedure, including both sediment and oil / flotables removal, for a 6-ft First Defense® typically takes less than 30 minutes and removes a combined water/oil volume of about 765 gallons.

First Defense® Operation and Maintenance Manual

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Inspection Procedures

- Set up any necessary safety equipment around the access port or grate of the First Defense[®] as stipulated by local ordinances. Safety equipment should notify passing pedestrian and road traffic that work is being done.
- 2. Remove the grate or lid to the manhole.
- Without entering the vessel, look down into the chamber to inspect the inside. Make note of any irregularities. Fig.4 shows the standing water level that should be observed.
- Without entering the vessel, use the pole with the skimmer net to remove floatables and loose debris from the components and water surface.
- Using a sediment probe such as a Sludge Judge[®], measure the depth of sediment that has collected in the sump of the vessel.
- On the Maintenance Log (see page 9), record the date, unit location, estimated volume of floatables and gross debris removed, and the depth of sediment measured. Also note any apparent irregularities such as damaged components or blockages.
- 7. Securely replace the grate or lid.
- 8. Take down safety equipment.
- Notify Hydro International of any irregularities noted during inspection.

Floatables and Sediment Clean Out

Floatables clean out is typically done in conjunction with sediment removal. A commercially or municipally owned sumpvac is used to remove captured sediment and floatables (Fig.5).

Floatables and loose debris can also be netted with a skimmer and pole. The access port located at the top of the manhole provides unobstructed access for a vactor hose and skimmer pole to be lowered to the base of the sump.

Scheduling

- Floatables and sump clean out are typically conducted once a year during any season.
- Floatables and sump clean out should occur as soon as possible following a spill in the contributing drainage area.



Fig.4 Floatables are removed with a vactor hose (First Defense model FD-4, shown).

Recommended Equipment

- Safety Equipment (traffic cones, etc)
- · Crow bar or other tool to remove grate or lid
- Pole with skimmer or net (if only floatables are being removed)
- Sediment probe (such as a Sludge Judge[®])
- Vactor truck (flexible hose recommended)
- First Defense[®] Maintenance Log

Hydro International (Stormwater), 94 Hutchins Drive, Portland ME 04102 Tel: (207) 756-6200 Fax: (207) 756-6212 Web: www.hydro-int.com

First Defense® Operation and Maintenance Manual

Floatables and sediment Clean Out Procedures

- Set up any necessary safety equipment around the access port or grate of the First Defense[®] as stipulated by local ordinances. Safety equipment should notify passing pedestrian and road traffic that work is being done.
- 2. Remove the grate or lid to the manhole.
- **3.** Without entering the vessel, look down into the chamber to inspect the inside. Make note of any irregularities.
- Remove oil and floatables stored on the surface of the water with the vactor hose (Fig.5) or with the skimmer or net (not pictured).
- Using a sediment probe such as a Sludge Judge[®], measure the depth of sediment that has collected in the sump of the vessel and record it in the Maintenance Log (page 9).
- Once all floatables have been removed, drop the vactor hose to the base of the sump. Vactor out the sediment and gross debris off the sump floor (Fig.5).
- 7. Retract the vactor hose from the vessel.
- 8. On the Maintenance Log provided by Hydro International, record the date, unit location, estimated volume of floatables and gross debris removed, and the depth of sediment measured. Also note any apparent irregularities such as damaged components, blockages, or irregularly high or low water levels.



Fig.5 Sediment is removed with a vactor hose (First Defense model FD-4, shown).

9. Securely replace the grate or lid.

Maintenance at a Glance

Inspection	- Regularly during first year of installation - Every ଓ months after the first year of installation			
Oil and Floatables Removal	- Once per year, with sediment removal - Following a spill in the drainage area			
Sediment Removal	- Once per year or as needed - Following a spill in the drainage area			
NOTE: For most clean outs the entire volume of liquid does not need to be removed from the manhole. Only remove the first few inches of oils and floatables from the water surface to reduce the total volume of liquid removed during a clean out				



First Defense® Installation Log

HYDRO INTERNATIONAL REFERENCE NUMBER:	
SITE NAME:	
SITE LOCATION:	
OWNER:	CONTRACTOR:
CONTACT NAME:	CONTACT NAME:
COMPANY NAME:	COMPANY NAME:
ADDRESS:	ADDRESS:
TELEPHONE:	TELEPHONE:
FAX:	FAX:

INSTALLATION DATE: / /

MODEL SIZE (CIRCLE ONE):	FD-4	FD-4HC	FD-6	FD-6HC
INLET (CIRCLE ALL THAT APPLY):	GRATED INL	ET (CATCH BASIN)	INLET PIPE (F	LOW THROUGH)



First Defense[®] Inspection and Maintenance Log

Date	Initials	Depth of Floatables and Oils	Sediment Depth Measured	Volume of Sediment Removed	Site Activity and Comments



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CALL 1 (888) 382-7808 TO SCHEDULE AN INSPECTION

Stormwater Solutions

94 Hutchins Drive Portland, ME 04102

Tel: (207) 756-6200 Fax: (207) 756-6212 stormwaterinquiry@hydro-int.com

www.hydro-int.com



Jellyfish® Filter Owner's Manual





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Jellyfish Filter	er Inspection and Maintenance Log	
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THANK YOU FOR PURCHASING THE JELLYFISH® FILTER!

Contech Engineered Solutions would like to thank you for selecting the Jellyfish Filter to meet your project's stormwater treatment needs. With proper inspection and maintenance, the Jellyfish Filter is designed to deliver ongoing, high levels of stormwater pollutant removal.

If you have any questions, please feel free to call us or e-mail us:

Contech Engineered Solutions 9025 Centre Pointe Drive, Suite 400 | West Chester, OH 45069 513-645-7000 | 800-338-1122 www.ContechES.com info@conteches.com



WARNINGS / CAUTION

- 1. FALL PROTECTION may be required.
- 2. <u>WATCH YOUR STEP</u> if standing on the Jellyfish Filter Deck at any time; Great care and safety must be taken while walking or maneuvering on the Jellyfish Filter Deck. Attentive care must be taken while standing on the Jellyfish Filter Deck at all times to prevent stepping onto a lid, into or through a cartridge hole or slipping on the deck.
- 3. The Jellyfish Filter Deck can be SLIPPERY WHEN WET.
- 4. If the Top Slab, Covers or Hatches have not yet been installed, or are removed for any reason, great care must be taken to <u>NOT DROP ANYTHING ONTO THE JELLYFISH FILTER DECK</u>. The Jellyfish Filter Deck and Cartridge Receptacle Rings can be damaged under high impact loads. This type of activity voids all warranties. All damaged items to be replaced at owner's expense.
- 5. Maximum deck load 2 persons, total weight 450 lbs.

Safety Notice

Jobsite safety is a topic and practice addressed comprehensively by others. The inclusions here are intended to be reminders to whole areas of Safety Practice that are the responsibility of the Owner(s), Manager(s) and Contractor(s). OSHA and Canadian OSH, and Federal, State/Provincial, and Local Jurisdiction Safety Standards apply on any given site or project. The knowledge and applicability of those responsibilities is the Contractor's responsibility and outside the scope of Contech Engineered Solutions.

Confined Space Entry

Secure all equipment and perform all training to meet applicable local and OSHA regulations regarding confined space entry. It is the Contractor's or entry personnel's responsibility to proceed safely at all times.

Personal Safety Equipment

Contractor is responsible to provide and wear appropriate personal protection equipment as needed including, but not limited to safety boots, hard hat, reflective vest, protective eyewear, gloves and fall protection equipment as necessary. Make sure all equipment is staffed with trained and/or certified personnel, and all equipment is checked for proper operation and safety features prior to use.

- Fall protection equipment
- Eye protection
- Safety boots
- Ear protection
- Gloves
 - Ventilation and respiratory protection
 - Hard hat
 - Maintenance and protection of traffic plan

Chapter 1

1.0 – Owner Specific Jellyfish Filter Product Information

Below you will find a reference page that can be filled out according to your Jellyfish Filter specification to help you easily inspect, maintain and order parts for your system.

Owner Name:	
Phone Number:	
Site Address:	
Site GPS Coordinates/unit location:	
Unit Location Description:	
Jellyfish Filter Model No.:	
Contech Project & Sequence Number	
No. of Hi-Flo Cartridges	
No. of Cartridges:	
Length of Draindown Cartridges:	
No. of Blank Cartridge Lids:	
Bypass Configuration (Online/Offline):	

Notes:

Chapter 2

2.0 – Jellyfish Filter System Operations and Functions

The Jellyfish Filter is an engineered stormwater quality treatment technology that removes a high level and wide variety of stormwater pollutants. Each Jellyfish Filter cartridge consists of eleven membrane - encased filter elements ("filtration tentacles") attached to a cartridge head plate. The filtration tentacles provide a large filtration surface area, resulting in high flow and high pollutant removal capacity.

The Jellyfish Filter functions are depicted in Figure 1 below.



Jellyfish Filter cartridges are backwashed after each peak storm event, which removes accumulated sediment from the membranes. This backwash process extends the service life of the cartridges and increases the time between maintenance events.

For additional details on the operation and pollutant capabilities of the Jellyfish Filter please refer to additional details on our website at <u>www.ContechES.com</u>.

2.1 – Components and Cartridges

The Jellyfish Filter and components are depicted in Figure 2 below.



Tentacles are available in various lengths as depicted in Table 1 below.

Cartridge Lengths	Dry Weight	Hi-Flo Orifice Diameter	Draindown Orifice Diameter
15 inches (381 mm)	10 lbs (4.5 kg)	35 mm	20 mm
27 inches (686 mm)	14.5 lbs (6.6 kg)	45 mm	25 mm
40 inches (1,016 mm)	19.5 lbs (8.9 kg)	55 mm	30 mm
54 inches (1,372 mm)	25 lbs (11.4 kg)	70 mm	35 mm

Table 1 – Cartridge Lengths / Weights and Cartridge Lid Orifice Diameters

2.2 – Jellyfish Membrane Filtration Cartridge Assembly

The Jellyfish Filter utilizes multiple membrane filtration cartridges. Each cartridge consists of removable cylindrical filtration "tentacles" attached to a cartridge head plate. Each filtration tentacle has a threaded pipe nipple and o-ring. To attach, insert the top pipe nipples with the o-ring through the head plate holes and secure with locking nuts. Hex nuts to be hand tightened and checked with a wrench as shown below.

2.3 – Jellyfish Membrane Filtration Cartridge Installation

- Cartridge installation will be performed by trained individuals and coordinated with the installing site Contractor. Flow diversion devices are required to be in place until the site is stabilized (final paving and landscaping in place). Failure to address this step completely will reduce the time between required maintenance.
- Descend to the cartridge deck (see Safety Notice and page 3).
- Refer to Contech's submittal drawings to determine proper quantity and placement of Hi-Flo, Draindown and Blank cartridges with appropriate lids. Lower the Jellyfish membrane filtration cartridges into the cartridge receptacles within the cartridge deck. It is possible that not all cartridge receptacles will be filled with a filter cartridge. In that case, a blank headplate and blank cartridge lid (no orifice) would be installed.



Cartridge Assembly

Do not force the tentacles down into the cartridge receptacle, as this may damage the membranes. Apply downward pressure on the cartridge head plate to seat the lubricated rim gasket (thick circular gasket surrounding the circumference of the head plate) into the cartridge receptacle. (See Figure 3 for details on approved lubricants for use with rim gasket.)

- Examine the cartridge lids to differentiate lids with a small orifice, a large orifice, and no orifice.
 - Lids with a <u>small orifice</u> are to be inserted into the <u>Draindown cartridge receptacles</u>, outside of the backwash pool weir.
 - Lids with a large orifice are to be inserted into the <u>Hi-Flo cartridge receptacles</u> within the backwash pool weir.
 - Lids with <u>no orifice</u> (blank cartridge lids) and a <u>blank headplate</u> are to be inserted into unoccupied cartridge receptacles.
- To install a cartridge lid, align both cartridge lid male threads with the cartridge receptacle female threads before rotating approximately 1/3 of a full rotation until firmly seated. Use of an approved rim gasket lubricant may facilitate installation.

3.0 Inspection and Maintenance Overview

The primary purpose of the Jellyfish® Filter is to capture and remove pollutants from stormwater runoff. As with any filtration system, these pollutants must be removed to maintain the filter's maximum treatment performance. Regular inspection and maintenance are required to insure proper functioning of the system. Maintenance frequencies and requirements are site specific and vary depending on pollutant loading. Additional maintenance activities may be required in the event of non-storm event runoff, such as base-flow or seasonal flow, an upstream chemical spill or due to excessive sediment loading from site erosion or extreme runoff events. It is a good practice to inspect the system after major storm events.

Inspection activities are typically conducted from surface observations and include:

- Observe if standing water is present
- Observe if there is any physical damage to the deck or cartridge lids
- Observe the amount of debris in the Maintenance Access Wall (MAW) or inlet bay for vault systems

Maintenance activities include:

- Removal of oil, floatable trash and debris
- Removal of collected sediments
- Rinsing and re-installing the filter cartridges
- Replace filter cartridge tentacles, as needed

4.0 Inspection Timing

Inspection of the Jellyfish Filter is key in determining the maintenance requirements for, and to develop a history of, the site's pollutant loading characteristics. In general, inspections should be performed at the times indicated below; or per the approved project stormwater quality documents (if applicable), whichever is more frequent.



Note: Separator Skirt not shown

- 1. A minimum of quarterly inspections during the first year of operation to assess the sediment and floatable pollutant accumulation, and to ensure proper functioning of the system.
- 2. Inspection frequency in subsequent years is based on the inspection and maintenance plan developed in the first year of operation. Minimum frequency should be once per year.
- 3. Inspection is recommended after each major storm event.
- 4. Inspection is required immediately after an upstream oil, fuel or other chemical spill.

5.0 Inspection Procedure

The following procedure is recommended when performing inspections:

- 1. Provide traffic control measures as necessary.
- 2. Inspect the MAW or inlet bay for floatable pollutants such as trash, debris, and oil sheen.
- 3. Measure oil and sediment depth in several locations, by lowering a sediment probe until contact is made with the floor of the structure. Record sediment depth, and presences of any oil layers.
- 4. Inspect cartridge lids. Missing or damaged cartridge lids to be replaced.
- 5. Inspect the MAW (where appropriate), cartridge deck and receptacles, and backwash pool weir, for damaged or broken components.

5.1 Dry weather inspections

- Inspect the cartridge deck for standing water, and/or sediment on the deck.
- No standing water under normal operating conditions.
- Standing water inside the backwash pool, but not outside the backwash pool indicates, that the filter cartridges need to be rinsed.



Inspection Utilizing Sediment Probe

- Standing water outside the backwash pool is not anticipated and may indicate a backwater condition caused by high water elevation in the receiving water body, or possibly a blockage in downstream infrastructure.
- Any appreciable sediment (≥1/16") accumulated on the deck surface should be removed.

5.2 Wet weather inspections

- Observe the rate and movement of water in the unit. Note the depth of water above deck elevation within the MAW or inlet bay.
- Less than 6 inches, flow should be exiting the cartridge lids of each of the draindown cartridges (i.e. cartridges located outside the backwash pool).
- Greater than 6 inches, flow should be exiting the cartridge lids of each of the draindown cartridges and each of the hi-flo cartridges (i.e. cartridges located inside the backwash pool), and water should be overflowing the backwash pool weir.
- 18 inches or greater and relatively little flow is exiting the cartridge lids and outlet pipe, this condition indicates that the filter cartridges need to be rinsed.

6.0 Maintenance Requirements

Required maintenance for the Jellyfish Filter is based upon results of the most recent inspection, historical maintenance records, or the site specific water quality management plan; whichever is more frequent. In general, maintenance requires some combination of the following:

- 1. Sediment removal for depths reaching 12 inches or greater, or within 3 years of the most recent sediment cleaning, whichever occurs sooner.
- 2. Floatable trash, debris, and oil removal.
- 3. Deck cleaned and free from sediment.
- 4. Filter cartridges rinsed and re-installed as required by the most recent inspection results, or within 12 months of the most recent filter rinsing, whichever occurs sooner.
- 5. Replace tentacles if rinsing does not restore adequate hydraulic capacity, remove accumulated sediment, or if damaged or missing. It is recommended that tentacles should remain in service no longer than 5 years before replacement.
- 6. Damaged or missing cartridge deck components must be repaired or replaced as indicated by results of the most recent inspection.
- 7. The unit must be cleaned out and filter cartridges inspected immediately after an upstream oil, fuel, or chemical spill. Filter cartridge tentacles should be replaced if damaged or compromised by the spill.

7.0 Maintenance Procedure

The following procedures are recommended when maintaining the Jellyfish Filter:

- 1. Provide traffic control measures as necessary.
- 2. Open all covers and hatches. Use ventilation equipment as required, according to confined space entry procedures. *Caution: Dropping objects onto the cartridge deck may cause damage*.
- 3. Perform Inspection Procedure prior to maintenance activity.

- 4. To access the cartridge deck for filter cartridge service, descend into the structure and step directly onto the deck. Caution: Do not step onto the maintenance access wall (MAW) or backwash pool weir, as damage may result. Note that the cartridge deck may be slippery.
- 5. Maximum weight of maintenance crew and equipment on the cartridge deck not to exceed 450 lbs.

7.1 Filter Cartridge Removal

- 1. Remove a cartridge lid.
- 2. Remove cartridges from the deck using the lifting loops in the cartridge head plate. Rope or a lifting device (available from Contech) should be used. *Caution: Should a snag occur, do not force the cartridge upward as damage to the tentacles may result. Wet cartridges typically weigh between 100 and 125 lbs.*
- 3. Replace and secure the cartridge lid on the exposed empty receptacle as a safety precaution. Contech does not recommend exposing more than one empty cartridge receptacle at a time.

7.2 Filter Cartridge Rinsing

- 1. Remove all 11 tentacles from the cartridge head plate. Take care not to lose or damage the O-ring seal as well as the plastic threaded nut and connector.
- 2. Position tentacles in a container (or over the MAW), with the



threaded connector (open end) facing down, so rinse water is flushed through the membrane and captured in the container.

3. Using the Jellyfish rinse tool (available from Contech) or a low-pressure garden hose sprayer, direct water spray onto the tentacle membrane, sweeping from top to bottom along the length of the tentacle. Rinse until all sediment is removed from the membrane. *Caution: Do not use a high pressure sprayer or focused stream of water on the membrane. Excessive water pressure may damage the membrane*.
5. Reassemble cartridges as detailed later in this document. Reuse O-rings and nuts, ensuring proper placement on each tentacle.

7.3 Sediment and Flotables Extraction

- 1. Perform vacuum cleaning of the Jellyfish Filter only after filter cartridges have been removed from the system. Access the lower chamber for vacuum cleaning only through the maintenance access wall (MAW) opening. Be careful not to damage the flexible plastic separator skirt that is attached to the underside of the deck on manhole systems. Do not lower the vacuum wand through a cartridge receptacle, as damage to the receptacle will result.
- 2. Vacuum floatable trash, debris, and oil, from the MAW opening or inlet bay. Alternatively, floatable solids may be removed by a net or skimmer.
- 3. Pressure wash cartridge deck and receptacles to remove all



Rinsing Cartridge with Contech Rinse Tool

sediment and debris. Sediment should be rinsed into the sump area. Take care not to flush rinse water into the outlet pipe.

- 4. Remove water from the sump area. Vacuum or pump equipment should only be introduced through the MAW or inlet bay.
- 5. Remove the sediment from the bottom of the unit through the MAW or inlet bay opening.
- 6. For larger diameter Jellyfish Filter manholes (\geq 8-ft) and some



Vacuuming Sump Through MAW

vaults complete sediment removal may be facilitated by removing a cartridge lid from an empty receptacle and inserting a jetting wand (not a vacuum wand) through the receptacle. Use the sprayer to rinse loosened sediment toward the vacuum hose in the MAW opening, being careful not to damage the receptacle.

7.4 Filter Cartridge Reinstallation and Replacement

- 1. Cartridges should be installed after the deck has been cleaned. It is important that the receptacle surfaces be free from grit and debris.
- 2. Remove cartridge lid from deck and carefully lower the filter cartridge into the receptacle until head plate gasket is seated squarely in receptacle. *Caution: Do not force the cartridge downward; damage may occur.*
- 3. Replace the cartridge lid and check to see that both male threads are properly seated before rotating approximately 1/3 of a full rotation until firmly seated. Use of an approved rim gasket lubricant may facilitate installation. See next page for additional details.
- 4. If rinsing is ineffective in removing sediment from the tentacles, or if tentacles are damaged, provisions must be made to replace the spent or damaged tentacles with new tentacles. Contact Contech to order replacement tentacles.

7.5 Chemical Spills

Caution: If a chemical spill has been captured, do not attempt maintenance. Immediately contact the local hazard response agency and contact Contech.

7.6 Material Disposal

The accumulated sediment found in stormwater treatment and conveyance systems must be handled and disposed of in accordance with regulatory protocols. It is possible for sediments to contain measurable concentrations of heavy metals and organic chemicals (such as pesticides and petroleum products). Areas with the greatest potential for high pollutant loading include industrial areas and heavily traveled roads. Sediments and water must be disposed of in accordance with all applicable waste disposal regulations. When scheduling maintenance, consideration must be made for the disposal of solid and liquid wastes. This typically requires coordination with a local landfill for solid waste disposal. For liquid waste disposal a number of options are available including a municipal vacuum truck decant facility, local waste water treatment plant or on-site treatment and discharge.

Jellyfish Filter Components & Filter Cartridge Assembly and Installation





TABLE	1: BOM

ITEM NO.	DESCRIPTION
1	JF HEAD PLATE
2	JF TENTACLE
3	JF O-RING
	JF HEAD PLATE
4	GASKET
5	JF CARTRIDGE EYELET
6	JF 14IN COVER
7	JF RECEPTACLE
	BUTTON HEAD CAP
8	SCREW M6X14MM SS
9	JF CARTRIDGE NUT

TABLE 2: APPROVED GASKET LUBRICANTS

PART NO.	MFR	DESCRIPTION
78713	LA-CO	LUBRI-JOINT
40501	HERCULES	DUCK BUTTER
30600	OATEY	PIPE LUBRICANT
PSLUBXL1Q	PROSELECT	PIPE JOINT LUBRICANT

NOTES:

Head Plate Gasket Installation:

Install Head Plate Gasket (Item 4) onto the Head Plate (Item 1) and liberally apply a lubricant from Table 2: Approved Gasket Lubricants onto the gasket where it contacts the Receptacle (Item 7) and Cartridge Lid (Item 6). Follow Lubricant manufacturer's instructions.

Lid Assembly:

Rotate Cartridge Lid counter-clockwise until both male threads drop down and properly seat. Then rotate Cartridge Lid clock-wise approximately one-third of a full rotation until Cartridge Lid is firmly secured, creating a watertight seal.

Jellyfish Filter Inspection and Maintenance Log

Owner:			Jellyfish Mode	l No.:		_
Location:			GPS Coordina	tes:		-
Land Use:	Commercial:	Industrial:	Servi	ce Station:		
	Road/Highway:	Airport:	Resid	lential:	Parking Lo	ot:
[
Date/Time:						
Inspector:						
Maintenance	e Contractor:					
Visible Oil Pre	esent: (Y/N)					
Oil Quantity F	Removed					
Floatable Deb	oris Present: (Y/N)					
Floatable Deb	oris removed: (Y/N)					
Water Depth	in Backwash Pool					
Cartridges ex	ternally rinsed/re-commissic	oned: (Y/N)				
New tentacle	es put on Cartridges: (Y/N)					
Sediment Dep	pth Measured: (Y/N)					
Sediment Dep	pth (inches or mm):					
Sediment Rer	moved: (Y/N)					
Cartridge Lids	s intact: (Y/N)					
Observed Dar	mage:					
Comments:						

TRAFFIC IMPACT AND SITE ACCESS STUDY

PROPOSED RETAIL FUEL OUTLET

Portsmouth, New Hampshire

February 2022

Prepared for

Granite State Convenience, LLC







Transportation: Engineering • Planning • Design

TRAFFIC IMPACT & SITE ACCESS STUDY PROPOSED RETAIL FUEL OUTLET PORTSMOUTH, NEW HAMPSHIRE **FEBRUARY 24, 2022**

& Company, Inc.

INTRODUCTION

This study has been prepared for Granite State Convenience, LLC to assess the traffic impacts associated with the proposed gasoline station/convenience store (with drive-through window) that will replace the existing Burger King fast-food restaurant located at 2255 Lafayette Road in Portsmouth, New Hampshire. A traffic study scope meeting was conducted with the NHDOT and city officials on July 28, 2021. At that meeting the study area was identified as including the US1 / South Site Driveway and the US1 / North Site Driveway / Water Country Driveway on Lafayette Road. The analysis periods included the weekday morning (AM) and evening (PM) peak hour periods. Subsequent to the scope meeting, Pernaw & Company, Inc. elected to add the Saturday midday (SAT) peak hour case given the heavy use of the Water Country driveway on weekends. Both Opening Year (2023) and Horizon Year (2033) analyses are included herein.

This report is intended to summarize the traffic count data collected, the future traffic projections, the technical analyses, and our findings relative to traffic operations, capacity, and safety.

PROPOSAL

Granite State Convenience, LLC proposes to raze the existing fast-food restaurant building and replace it with a new 5,555 sf convenience store (with drive-through window) and 10 vehicle fueling positions. Access to the site will continue to be provided via the South Site Driveway (entrance only) and egress from the site will continue to be provided via the North Site Driveway (exit only) that is located across from the Water Country driveway. Figure 1 shows the location of the subject site with respect to the area highway system. Appendix A contains a preliminary site plan prepared by Greenman-Pedersen, Inc. (GPI) and the Scope Meeting notes.

EXISTING CONDITIONS

ROADWAYS

Lafayette Road (US1) functions as a multi-lane principal arterial highway that carries through traffic in a general north-south direction between points south in Hampton and beyond, through Portsmouth, to points north in Maine. The roadway segment north of the site provides one travel lane in each direction and a continuous two-way left-turn lane. The roadway segment south of the site provides an additional southbound travel lane. There are paved shoulders of variable width on both sides of the roadway. The horizontal alignment of the highway follows a straight tangent section south of the site, and it transitions to a large-radius northbound curve to the left to the north of the subject site. The vertical alignment of the roadway is generally flat in this area. The speed limit is posted at 35 mph in both directions.



Pernaw & Company, Inc.

NORTH



= AUTOMATIC TRAFFIC RECORDER LOCATION (NHDOT)

= INTERSECTION TURNING MOVEMENT COUNT LOCATION

2122A

Figure 1

Site Location

Traffic Impact and Site Access Study, Proposed Retail Fuel Outlet, Portsmouth, New Hampshire



TRAFFIC VOLUMES

The New Hampshire Department of Transportation conducted a short-term automatic traffic recorder count on US1 (north of Ocean Road) approximately one mile south of the subject site in June 2019. Based on this count data, the NHDOT estimates that this section of US1 carried an Annual Average Daily Traffic (AADT) volume of 18,484 vehicles per day (vpd) in 2019. The 2020 AADT estimate is lower at 15,600 vpd due to the ongoing pandemic.

The raw traffic count data collected at this count station is summarized graphically on Page 4 in terms of daily and hourly variations. This data demonstrates that weekday traffic demand in the study area generally reaches peak levels during the typical AM and PM commuter periods. Appendix B contains the detail sheets pertaining to this count.

To establish the current traffic demand at the subject site, Pernaw & Company, Inc. conducted turning movement and vehicle classification counts at the two existing site driveways on US1 on Thursday, July 29, 2021 from 7:00 to 9:00 AM and from 3:00 to 6:00 PM, and on Saturday, July 31, 2021 from 9:00 AM to 2:00 PM. Several facts and conclusions are evident from this count data:

- Peak traffic periods were found to occur from 7:45 to 8:45 AM in the morning, from 3:30 to 4:30 PM in the evening, and from 11:15 AM to 12:15 PM on Saturday.
- During the morning peak hour, the two-way traffic flow on US1 (south of the site) totaled 1,487 vehicles and the predominant travel direction was northbound (55%). The existing Burger King business generated 25 vehicle-trips during the AM peak hour period, with one errant vehicle entering the site via the exit-only driveway.
- During the evening peak hour, the two-way traffic flow on US1 (south of the site) totaled 2,045 vehicles and the predominant travel direction was southbound (51%). The existing Burger King business generated 64 vehicle-trips during the PM peak hour period, and four errant vehicles were observed entering the site via the exit-only driveway.
- During the Saturday midday peak hour, the two-way traffic flow on US1 (south of the site) totaled 2,065 vehicles and the predominant travel direction was northbound (56%). The existing Burger King business generated 82 vehicle-trips during the SAT peak hour period, and six vehicles were observed entering the site via the exit-only driveway.
- The Water Country driveway was essentially inactive during the weekday peak hour periods, and quite busy during the Saturday midday peak hour. During the Saturday midday peak hour, the Water Country driveway accommodated 239 arrivals; with equal percentages from the north and south.
- Truck traffic in the study area ranged from 4-5% (AM), 2-4% (PM) and 1% (SAT) during the peak hour periods.

The peak hour traffic count data for the study area intersections are summarized on Figure 2. Appendix C contains the detail sheets from the manual turning movement counts.









Traffic Impact and Site Access Study, Proposed Retail Fuel Outlet, Portsmouth, New Hampshire

Figure 2



NO-BUILD TRAFFIC VOLUMES

In order to identify the net impact that site traffic will have in the study area, future traffic projections with and without the proposed redevelopment project are necessary. The future traffic projections <u>without</u> the proposed development are referred to as the "No-Build" traffic projections and these are summarized on Figure 3 (2023) and Figure 4 (2033).

These projections are based on the existing traffic volumes (July 2021 data), a 1.0 percent annual background traffic growth rate (compounded annually) to account for normal growth in the area, a peak-month seasonal adjustment factor of 1.02, and Covid-19 adjustment factors of 1.16 (AM), 1.09 (PM), and 1.04 (Saturday) to reflect non-pandemic conditions. At the scope meeting no other recently approved development projects that could affect traffic volumes in the study area were identified.

The No-Build traffic projections therefore reflect worst-case, peak-month, peak-hour conditions without a pandemic. Calculations pertaining to the derivation of the background traffic growth rate, seasonal adjustment factor, and Covid-19 factors are contained in Appendix D.



Traffic Impact and Site Access Study, Proposed Retail Fuel Outlet, Portsmouth, New Hampshire

Figure 3

2122A



Traffic Impact and Site Access Study, Proposed Retail Fuel Outlet, Portsmouth, New Hampshire

Figure 4

2122A



SITE GENERATED TRAFFIC

To estimate the quantity of vehicle-trips that will be produced by the replacement gasoline station/convenience store Pernaw & Company, Inc. considered both the standardized trip-generation rates published by the Institute of Transportation Engineers (ITE)¹, and similar site data. More specifically, ITE Land Use Code (LUC) 945 - Convenience Store/Gas Station, was selected and the gross floor area of the store was utilized as the independent variable. As requested at the scope meeting, supplemental driveway counts were conducted at the Common Man Roadside site on South Willow Street in Manchester, New Hampshire. Table 1A summarizes the results of the trip generation analyses and compares this with the former use of the site.

Table 1A		Trip Generatio	n Summary / Cor	mparison
			Proposed Re	tail Fuel Outlet
		Existing Burger King Site ¹	ITE Trip Generation Estimate ²	Similar Site Trip Generation ³
Weekday Total				
	Entering		1,729 veh	
	Exiting	NA	<u>1,729</u> veh	NA
	Total		3,458 trips	
Weekday AM Peal	Hour			
	Entering	16 veh	158 veh	72 veh
	Exiting	<u>9 veh</u>	<u>158 veh</u>	66 veh
	Total	25 trips	316 trips	138 trips
Weekday PM Peak	Hour			
	Entering	34 veh	134 veh	79 veh
	Exiting	<u>30</u> veh	<u>135 veh</u>	74 veh
	Total	64 trips	269 trips	153 trips
Ostandara Tatal				
Salurday Tolar	Entering		1.450 yeb	
	Eviting	ΝΔ	1,459 Ven	ΝΔ
	Total		2 918 trins	1 10-7
	15101		2,010 (1)03	
Saturday Peak Ho	ur			
	Entering	40 veh	146 veh	73 veh
	Exiting	<u>42</u> <u>veh</u>	<u>152 veh</u>	<u>70 veh</u>
	Total	82 trips	298 trips	143 trips

¹ Driveway counts conducted at 2255 Lafayette Road in Portsmouth, NH on July 7/29/21& 7/31/21

²ITE Land Use Code 945 - Convenience Store / Gas Station (5,555 sf / trip rate method)

³ Driveway counts conducted at 1805 South Willow Street in Manchester, NH on July 7/29/21& 7/31/21 at the Common Man Roadside site.

¹ Institute of Transportation Engineers, *Trip Generation*, eleventh edition (Washington, D.C., 2021)



This table shows that the proposed gasoline station/convenience store will generate approximately 316 (AM), 269 (PM), and 298 (SAT) vehicle-trips during the peak hour periods. This type of development generates a combination of "primary" type trips (new trips to the area) and "pass-by" trips (drawn from existing traffic stream) as shown in Table 1B.

Table 1B		Trip Gen	eration Composit	ion
		Primary Trips	Pass-By Trips ¹	Total Trips
Weekday AM Peak	Hour			
	Entering	38 veh	120 veh	158 veh
	Exiting	<u>38 veh</u>	<u>120</u> veh	<u>158 veh</u>
	Total	76 trips	240 trips	316 trips
Weekday PM Peak	Hour			
	Entering	33 veh	101 veh	134 veh
	Exiting	34 veh	<u>101 veh</u>	<u>135 veh</u>
	Total	67 trips	202 trips	269 trips
Saturday Peak Ho	ır			
	Entering	34 veh	112 veh	146 veh
	Exiting	40 veh	<u>112 veh</u>	<u>152 veh</u>
	Total	74 trips	224 trips	298 trips

¹ *ITE Trip Manual*, 11th Edition, 3rd Edition, LUC 945, AM = 76%, PM = 75% and assume Saturday = 75%

This table shows that the clear majority of trips will be drawn from the existing traffic stream on US1; whereas the minority represents new trips to the area. Appendix E contains the trip generation computations for this project, as well as diagrams summarizing the travel patterns associated with the primary and pass-by trips.



BUILD TRAFFIC VOLUMES

The future traffic projections with the proposed redevelopment project in full operation are referred to as the "Build" traffic projections and these are summarized schematically on Figure 5 (2023) and Figure 6 (2033). These projections are based on the No-Build projections (Figures 3 & 4), the site generated traffic levels depicted in Table 1A, and the expectation that the majority of the primary vehicle-trips (70%) will travel to/from points north on US1, and the remaining 30% to/from points south.

These travel patterns were based on analysis of the "journey to work" data from the latest census and our familiarity with the study area. The distribution of the pass-by trips was based on the proportion of northbound versus southbound vehicles on US1. Consequently, these trip distribution patterns varied depending upon the peak hour period.



Traffic Impact and Site Access Study, Proposed Retail Fuel Outlet, Portsmouth, New Hampshire

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Traffic Impact and Site Access Study, Proposed Retail Fuel Outlet, Portsmouth, New Hampshire



IMPACT SUMMARY

The net impact that the proposed redevelopment project will have on traffic levels on US1 can be estimated by comparing the No-Build traffic projections with the Build traffic projections. This comparison is summarized on Figure 7 and it demonstrates that the greatest impact to <u>roadway</u> <u>volumes</u> will occur north of the subject site. The greatest hourly increase is expected to occur during the weekday AM peak hour with +50 additional vehicles (total both directions) or by +3%. The net impact south of the site is estimated at 1% or less during the peak hour periods.

To put these percentages into perspective, the NHDOT count data in Appendix B shows that random traffic flow from one day to the next accounts for peak hour changes of 2-3 percent.

Pernaw & Company, Inc.

	e % Change	eh 6% eh 5%	eh 3%	eh 1%		e % Change
L	Chang	+113 ve +92 ve	+50 ve	+13 ve		Chang
AM Peak Hou	2023 Build	1906 1889	1840	1807	M Peak Hour	2023 Build
1	2023 No-Build	1793 1797	1790	1794	-	2023 No-Build
	Location	Intersection A Intersection B	Checkpoint 1	Checkpoint 2		Location



		% Change	3%	ה 3%	1%	1%
łour		Change	+72 veh	+74 veh	+25 veh	+17 veh
turday Peak H	2023	Build	2466	2329	2277	2251
Sa	2023	No-Build	2394	2255	2252	2234
		Location	Intersection A	Intersection B	Checkpoint 1	Checkpoint 2

neg

+5 veh

2353 2324

2319

Checkpoint 2 Checkpoint 1

2323

+30 veh

3% 3% 1%

+80 veh

2416 2402

2336 2331

Intersection A Intersection B

+71 veh

Traffic Impact and Site Access Study, Proposed Retail Fuel Outlet, Portsmouth, New Hampshire 2023 Impact Summary

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Figure 7



TRAFFIC OPERATIONS AND SAFETY

INTERSECTION CAPACITY - UNSIGNALIZED INTERSECTIONS

The short-range (2023) and long-range (2033) traffic projections form the basis for assessing traffic operations at the site driveway intersections on US1. These intersections were analyzed according to the methodologies of the *Highway Capacity Manual* as replicated by the latest edition of the *Synchro Traffic Signal Coordination Software (Version 10)*, which also performs unsignalized intersection capacity analyses.

Capacity and Level of Service (LOS) calculations pertaining to unsignalized intersections address the quality of service for those vehicles turning into and out of intersecting side streets or driveways. The availability of adequate gaps in the traffic stream on the major street (US1) actually controls the potential capacity for vehicle movements from the driveway approaches. Levels of Service are simply letter grades (A-F) that categorize the vehicle delays associated with specific turning maneuvers. Table 2 describes the criteria used in this analysis.

Table 2	Level-of-Serv Unsignalized	ice Criteria for Intersections
Control Delay	Level of Service by Vo	olume-to-Capacity Ratio
(seconds/vehicle)	<u>v/c≤1.0</u>	<u>v/c>1.0</u>
0 - 10	А	F
> 10 - 15	В	F
> 15 - 25	С	F
> 25 - 35	D	F
> 35 - 50	E	F
> 50	F	F

Source: Transportation Research Board, Highway Capacity Manual 2010.

The results of this analysis for the US1 / North Site Driveway / Water Country Driveway intersection are summarized on Table 3. The analysis confirms that left-turn departures from the northerly site driveway will encounter long delays (LOS F) during all three peak hour periods, similar to all other streets and driveways that intersect this corridor. As a result, on-site vehicle queues of up to ten vehicles could occur during the Saturday midday peak hour during the summer months. Analysis of the right-turn departure movement revealed that this movement will operate at LOS C (AM & PM) and LOS D (SAT) in the opening year, and at LOS D in 2033 (summer months). Vehicle queues are expected to remain short in the right-turn departure lane. These results demonstrate the importance of providing two departure lanes on the north site driveway approach to US1.

The results of this analysis for the US1 / South Site Driveway intersection are summarized on Table 4, and applies to the southbound left-turn arrival movement only. Left-turn arrivals will operate well <u>below</u> capacity and at LOS B or higher during all hours of the day through 2033 and beyond. The 95th percentile queue in the center turn lane on US1 will remain short (1 vehicle) during all three peak hour periods.

Appendix F contains the calculations pertaining to these analyses.



	ur	Queue ⁴
	Peak Hou	LOS ³
	Saturday	V/C ²
s iveway		Delay ¹
y Analysi h Site Dri	ur	Queue ⁴
apacity / Nortl	1 Peak Ho	LOS ³
ction C riveway	eekday PN	V/C ²
d Interse ountry Di	M	Delay ¹
Controlle / Water C	ur	Queue ⁴
STOP oute 1	l Peak Ho	LOS ³
US R(eekday AN	V/C ²
	Ň	Delay ¹
8		
Table :		

		A	acruay Aiv			AA	ceruay I N			-	Jakuray I	Can Livu	
		Delay	V/C ²	LOS ³	Queue ⁴	Delay ¹	V/C ²	LOS ³	Queue ⁴	Delay ¹	V/C^2	LOS ³	Queue ⁴
US Route 1 - NB LT													
	2021 Existing	9.0	0.00	۷	ž	10.7	00.0	В	7	11.8	0.19	В	~
	2023 No Build	9.5	00.0	٩	¥	11.5	00.0	В	¥	12.5	0.21	В	-
	2023 Build	9.6	00.0	A	Ŷ	11.7	00.0	В	ř	12.6	0.22	ш	-
	2033 No Build	9.8	00.0	A	Ŷ	12.3	00.0	Ш	ř	13.4	0.23	В	-
	2033 Build	10.0	00.0	٩	¥	12.5	00.0	В	¥	13.6	0.24	В	-
North Site Driveway -	WB LT & TH												
	2021 Existing	35.6	0.02	ш	۲ ۲	86.3	0.20	ш	-	195.6	0.51	ш	7
	2023 No Build	54.5	0.03	ш	¥	149.7	0.34	ш	~	>300	0.69	ш	2
	2023 Build	165.1	06.0	ш	5	>300*	1.81	ш	7	>300*	2.78	ш	6
	2033 No Build	73.2	0.04	ш	Ÿ	245.9	0.49	ш	2	>300	0.98	ш	ю
	2033 Build	296.8	1.20	ш	9	>300*	2.65	ш	8	>300*	4.01	ш	10
North Site Driveway -	WB RT												
	2021 Existing	15.7	0.02	O	۲ ۲	18.1	0.08	U	ž	19.8	0.11	U	¥
	2023 No Build	18.8	0.03	υ	ž	21.1	0.10	υ	ž	22.1	0.12	υ	ř
	2023 Build	23.6	0.35	o	2	24.9	0.31	υ	-	27.1	0.38	۵	2
	2033 No Build	21.6	0.04	υ	ž	24.3	0.12	υ	ž	26.2	0.15	۵	ب
	2033 Build	28.6	0.41	Δ	7	30.1	0.36	۵	7	34.7	0.45	۵	2
US Route 1 - SB LT													
	2021 Existing	9.7	0.00	۷	ž	10.2	0.01	В	7	10.5	0.01	В	¥
	2023 No Build	10.5	00.0	В	Ŷ	10.8	0.01	В	۲ ۲	10.9	0.01	ш	Ŷ
	2023 Build (prohibited)												
	2033 No Build	11.2	00.0	В	¥	11.5	0.01	В	¥	11.7	0.01	В	¥
	2033 Build (prohibited)	ı	·	ı	,	,	,	,	ı		,	ı	
	c			c									

¹ HCM Control Delay (seconds per vehicle), ² HCM Volume to Capacity Ratio, ³ HCM Level of Service, ⁴ HCM 95th Percentile Queue (vehicles) *HCM 2010 Pg 19-28: "If demand exceeds capacity during a 15-minute period, the delay results computed by the procedures may not be accurate"



			1						
			Queue ⁴		ř	ř	-	v	-
		^b eak Hour	LOS ³		Ш	В	В	Ш	В
		Saturday F	V/C ²		0.03	0.04	0.14	0.04	0.16
	0		Delay ¹		11.4	12.0	12.9	12.9	14.1
	/ Analysi ay	ır	Queue ⁴		Ŷ	Ŷ	-	Ŷ	-
	apacity Drivew	l Peak Hou	LOS ³		ш	В	В	Ш	Ю
	ction C th Site	eekday PN	V/C ²		0.02	0.02	0.13	0.02	0.15
	d Interse e 1 / Sou	M	Delay ¹		10.3	11.0	11.8	11.1	12.7
	STOP-Controlle US Rout	ur	Queue ⁴		ž	¥	v	¥	-
		1 Peak Ho	LOS ³		٨	В	В	В	В
		eekday AN	V/C ²		00.0	0.01	0.13	0.01	0.14
		M	Delay ¹		9.8	10.6	11.4	11.2	12.2
					2021 Existing	2023 No Build	2023 Build	2033 No Build	2033 Build
	Table 4			US Route 1 - SB LT					

¹ HCM Control Delay (seconds per vehicle), ² HCM Volume to Capacity Ratio, ³ HCM Level of Service, ⁴ HCM 95th Percentile Queue (vehicles)



AUXILIARY TURN LANE ANALYSES

Left-Turn Treatment - The type of treatment needed to accommodate left-turning vehicles from any street or highway to an intersecting side street (or driveway) can range from no treatment, where turning volumes are low; to the provision of a bypass lane for through traffic to travel around left-turning vehicles; to the addition of a formal center turn lane used exclusively by left-turning vehicles for deceleration and storage while waiting to complete their maneuvers. Favorably, this section of US1 currently provides a center turn lane that will be used by vehicles entering the subject site at the southerly site driveway.

Right-Turn Treatment - The type of treatment needed to accommodate right-turning vehicles from any street or highway to any intersecting side street (or driveway) can range from a radius only, where turning volumes are low; to the provision of a short 10:1 right-turn taper; to the addition of an exclusive right-turn lane, where turning volumes and through traffic volumes are significant.

Analysis of the 2023 Build traffic volume projections using NCHRP 457 guidelines confirmed that right-turn treatment is desirable at the southerly site driveway on US1. Although this could be accomplished by widening the existing shoulder to 10-feet (minimum), it would involve work along the southerly abutter's frontage and the relocation of at least one significant utility pole. Recognizing that this type of treatment is not provided at other commercial driveways on the corridor, it may be more appropriate for corridor-wide shoulder widening to be considered as part of NHDOT Project 29640. In the interim, the northbound travel lane on US1 will continue to function as a shared through-right lane.

The results of these analyses are summarized on Table 5.

Minor-Road Approach Analysis – The type of treatment needed to accommodate exiting vehicles from the minor-road approach at a stop-controlled intersection can range from a single lane (shared left-right lane) in low-volume conditions, to two exit lanes (exclusive left-turn lane and exclusive right-turn lane) where turning volumes and through traffic volumes are significant, to multiple exit lanes in extreme cases.

Analysis of the 2023 Build traffic volumes using NCHRP 457 guidelines is also summarized on Table 5 and it indicates that providing two exit lanes on the northerly site driveway approach to US1 is advisable given the anticipated traffic volumes, and the capacity analysis results. Consequently, it is recommended that the northerly site driveway should be delineated with a shared left-through lane and an exclusive right-turn lane.

The auxiliary turn lane warrants analyses are included in Appendix G.

DRIVE-THROUGH QUEUING

The extent of vehicle queuing at the drive-through window was analyzed to ensure that spillback onto US1 will not occur. The 95th percentile vehicle queue is expected to range from 4 to 6 vehicles depending upon the arrival rate and service times (see Appendix H). Spillback is not expected to occur as there is sufficient storage space for up to 14 vehicles without impacting the flow of through traffic on the US1 corridor.



Stephen G. Pernaw & Company, Inc.

Table 5	Auxiliary Turn Lane Warrants Analysis US Route 1 / Existing Site Driveways										
		2023 AM Build Volumes	2023 PM Build Volumes	2023 Saturday Build Volumes							
I. RIGHT-TURN LANE	WARRANTS ANALYSIS										
South Site Drivew ay Peak Hour Inputs	::										
Right-Tu	urn Volume (NB)	77	59	72							
Approa	ich Volume (NB)	983	1137	1259							
	Speed (mph)	35	35	35							
Limiting Right-Tu	rn Volume (veh/h)	18	10	7							
Add Right-Turi	n Bay?	YES	YES	YES							
II. MINOR-ROAD APP North Site Drivew ay Peak Hour Inputs	ROACH GEOMETRY ANAL	YSIS									
Major-Road	Volume (NB-SB)	1748	2280	2315							
% Right-Turr	ns on Minor (EB)	59	54	57							
Minor-Road A	pproach Volume	158	135	152							
Limiting Minor-Ro	oad Volume (veh/h)	92	43	43							
Consider TWO	Approach Lanes?	YES	YES	YES							



STUDY FINDINGS AND RECOMMENDATIONS

Based upon the existing conditions data collected on US1, the anticipated traffic volume increases associated with the proposed redevelopment of the subject site with a new gasoline station/convenience store, and the analysis of future traffic conditions at the two site driveway intersections on US1, Pernaw & Company, Inc. finds that:

- The traffic counts conducted by Pernaw & Company, Inc. at the site driveways on US1 in July 2021 revealed that the peak traffic hours typically occurred from 7:45 to 8:45 AM and from 3:30 to 4:30 PM on a typical weekday. On Saturday the peak traffic hour occurred from 11:15 AM to 12:15 PM. Overall, the busiest traffic hour on US1 occurred during the Saturday midday peak hour south of the subject site with a two-way traffic volume that totaled 2,065 vehicles.
- 2. Driveway counts conducted at the existing fast-food restaurant revealed that it generated 25 (AM), 64 (PM), and 82 (Saturday) vehicle-trips during those peak hour periods.
- 3. The trip generation analysis revealed that, on an average weekday basis, the proposed gasoline station/convenience store will generate approximately 316 (AM), 269 (PM) and +298 (SAT) vehicle-trips during the peak hour periods. The majority of these trips (75%) are expected to be "pass-by" type trips; i.e., not new trips to the area.
- 4. Analysis of the horizon year (2033) traffic projections confirmed that left-turn departures from the northerly site driveway will encounter long delays (LOS F) during all three peak hour periods, similar to all other streets and driveways that intersect this corridor. As a result, on-site vehicle queues of up to ten vehicles could occur during the Saturday midday peak hour during the summer months. Analysis of the right-turn departure movement revealed that this movement will operate at LOS C and LOS D (SAT) in the opening year, and at LOS D in 2033 (summer months). Vehicle queues are expected to remain short in the right-turn departure lane. Left-turn arrivals at the southerly site driveway are expected to operate at LOS B or higher during all hours of the day through 2033 and beyond. The 95th percentile queue in the center turn lane on US1 will remain short (1 vehicle) during all three peak hour periods.
- 5. The auxiliary turn lane warrants analyses contained herein indicates that right-turn treatment is desirable at the southerly site driveway on US1. Recognizing that this type of treatment is <u>not</u> provided at other commercial driveways on the corridor, it may be more appropriate for corridor-wide shoulder widening to be considered as part of NHDOT Project 29640. In the interim, the northbound travel lane on US1 will continue to function as a shared through-right lane, similar to other streets and driveways on this corridor. Providing two exit lanes on the northerly site driveway approach to US1 is advisable given the anticipated traffic volumes, and the capacity analysis results.
- 6. The northerly site driveway should operate under STOP sign control (MUTCD R1-1). It should be supplemented by a 24-inch white stop line and a short section of 4-inch single white lane line to separate left-turn and right-turn exiting. To correct the situation where vehicles are currently entering the site via the exit-only driveway, it is recommended that



"Do Not Enter" signs (MUTCD R5-1) be installed on both sides of the northerly site driveway, facing US1.

With implementation of the recommendations contained herein, vehicular access and egress at the subject site will be reasonably safe and efficient from a transportation engineering standpoint, for the size and type of development that is proposed.



APPENDIX

Appendix A	Site Plan
Appendix B	Automatic Traffic Recorder Counts
Appendix C	Intersection Turning Movement Counts
Appendix D	Seasonal Adjustment Factor / Historical Growth Rate / COVID Factor
Appendix E	Site Generated Traffic Volumes / Trip Distribution
Appendix F	Capacity and Level of Service Calculations – Unsignalized
Appendix G	Auxiliary Turn Lane Warrants Analysis
Appendix H	Miscellaneous

Appendix A

Site Plan



SCOPING MEETING FOR TRAFFIC IMPACTS OF DEVELOPMENT

Date: July 28, 2021

Town/City: Portsmouth

Location / District: US 1 / District 6

Consultants: Stephen G. Pernaw & Company, Inc., Greenman-Pederson, Inc.

<u>Size & Type of Development</u>: The existing site at 2255 Lafayette Rd contains a Burger King that will be replaced by a 5,555 SF gas station/convenience store with 10 vehicle fueling positions. The convenience store will include a sandwich shop (Common Man Roadside) with a drive-through.

<u>Site Access</u>: Access provided via two existing driveways from the site onto US 1. NHDOT District 6 requested both site driveways be kept as entrance and exit only instead of being converted into full access driveways. The consultants indicated the change would be incorporated.

Phasing: One phase.

Study Area: The study area will include both driveways at US 1.

Analysis Periods: Weekday AM & PM peak hours.

Opening Year / Future Year: 2022/2032? Consultant to revise as appropriate for what is reasonable for the development project.

Additional data: AM and PM peak hour TMCs should be estimated to evaluate right-turn lane warrants.

Background growth / other development: A background growth rate of 1% compounded annually should be used.

NHDOT Highway Design noted the 29640 Portsmouth project is in the vicinity of the proposed development. The project is still in the early stages and may not change the basic lane use of US 1, but is anticipated to make more accommodations for bikes and pedestrians, such as changes in shoulder width and sidewalks.

<u>Site Trip Generation / Distribution / Pass-by</u>: The consultant should evaluate trip generation at the site driveways based on the existing similar facility in Manchester and provide appropriate supporting data for their trip estimation. Trip composition should also be shown.

Based on an email from District 6, the Burger King ITE trip generation estimate provided by the consultant seemed reasonable to use, as opposed to collecting new TMCs.

Design Considerations: NHDOT Highway Design requested right-turn lane warrant evaluations (NCHRP 457) be conducted.

The consultant needs to demonstrate that drive-through queues will not back up onto US 1.

<u>Other Issues</u>: NHDOT District 6 stated that a 12' reserve easement on the frontage of the property needs to be shown on the site plans in case of future expansion, based on policy from 1984.

Submitted by: Stuart Thompson NHDOT BOT

Date: September 7, 2021

cc: All Attendees (Attached)

Appendix B Automatic Traffic Recorder Counts





Transportation Data Management System

List View All DIRs Record He ы 1 of 1 Goto Record go Location ID 82379150 MPO ID SPOT Туре HPMS ID **On NHS** Yes On HPMS Yes LRS ID U0000001 LRS Loc Pt. SF Group 04 . **Route Type** AF Group 04 ۶ Route US 1 GF Group E Þ Active Yes Class Dist Grp Default • Category 3 Seas Clss Grp Default Þ WIM Group Default Þ QC Group Default Fnct'l Class Other Principal Arterial Milepost Located On Lafayette Rd Loc On Alias US 1 (LAFAYETTE RD) NORTH OF OCEAN RD (SB-NB) (81379211-81379212) More Detail 🕨 STATION DATA Directions: 2-WAY NB SB AADT 🧐 Year AADT **DHV-30** Κ% D % PA BC Src Grown 2020 $15,600^3$ 9 50 14,196 (91%) 1,404 (9%) from 2019 2019 18,484 1,674 9 50 16,931 (92%) 1,553 (8%) Grown 2018 19,865³ 8 53 18,315 (92%) 1,550 (8%) from 2017 Grown 2017 19,475³ 8 53 18,075 (93%) 1,400 (7%) from 2016 2016 19.093 1,621 8 53 17,413 (91%) 1,680 (9%) > >>| 1-5 of 17 **Travel Demand Model** Model Model AM PPV MD PHV AM PHV MD PPV PM PHV PM PPV NT PHV NT PPV AADT Year **VOLUME COUNT** VOLUME TREND Date Int Total Year **Annual Growth** -Thu 6/6/2019 60 21,455 2020 -16% -Wed 6/5/2019 60 21,364 2019 -7% -Tue 6/4/2019 60 21,469 2018 2% -Tue 7/19/2016 60 19,597 2017 2% 1 Sun 7/17/2016 60 16,959 2016 7% -Fri 9/27/2013 60 20,159 2015 3% -Thu 9/26/2013 60 19,003 2014 2% -Wed 9/25/2013 60 18,690 2013 -7% 1 Tue 9/24/2013 60 18.712





Transportation Data Management System



Excel Version

Weekly Volume Re	port		
Location ID:	82379150	Type:	SPOT
Located On:	Lafayette Rd	:	
Direction:	2-WAY		
Community:	PORTSMOUTH	Period:	Mon 6/3/2019 - Sun 6/9/2019
AADT:	18484		

Start Time	Mon	Tue	Wed	Thu	Fri	Sat	Sun	Avg	Graph
12:00 AM		88	68	70				75	0.4%
1:00 AM		45	34	35				38	0.2%
2:00 AM		46	28	40				38	0.2%
3:00 AM		84	70	73				76	0.4%
4:00 AM		112	107	87				102	0.5%
5:00 AM		352	338	318				336	1.6%
6:00 AM		631	643	618				631	2.9%
7:00 AM		1197	1218	1093				1,169	5.5%
8:00 AM		1451	1421	1456	D			1,443	6.7%
9:00 AM		1273	1232	1176				1,227	5.7%
10:00 AM		1373	1333	1331				1,346	6.3%
11:00 AM		1542	1513	1451				1,502	7.0%
12:00 PM		1632	1647	1617				1,632	7.6%
1:00 PM		1500	1569	1583				1,551	7.2%
2:00 PM		1508	1505	1529				1,514	7.1%
3:00 PM		1640	1618	1643				1,634	7.6%
4:00 PM		1617	1576	1562				1,585	7.4%
5:00 PM	(1674	1635	1639				1,649	7.7%
6:00 PM		1263	1300	1345				1,303	6.1%
7:00 PM		884	914	991				930	4.3%
8:00 PM		734	754	829				772	3.6%
9:00 PM		474	501	526				500	2.3%
10:00 PM		234	216	270				240	1.1%
11:00 PM		115	124	173				137	0.6%
Total	0	21,469	21,364	21,455	0	0	0		
24hr Total		21469	21364	21455				21,429	
AM Pk Hr		11:00	11:00	8:00					
AM Peak	-	1542	1513	1456				1,504	
PM Pk Hr		5:00	12:00	3:00					
PM Peak		1674	1647	1643				1,655	
% Pk Hr		7.80%	7.71%	7.66%				7.72%	

 $\Delta = 3\%$

Q= 2%

Appendix C

Intersection Turning Movement Counts

Stephen G. Pernaw & Company, Inc. P.O. Box 1721 Concord, New Hampshire 03302

Weather: Clear Collected By: MV Job Number: 2122A Town/State: Portsmouth, NH File Name : 2122A_B_King_AM_&_PM Site Code : 2122A Start Date : 7/29/2021 Page No : 2

		US F From	Route 1 North		B	urger Kir Fron	ng Drivew n East	/ay	US Route 1 From South				
Start Time	Thru	Left	U-Turn	App. Total	Right	Left	U-Turn	App. Total	Right	Thru	U-Turn	App. Total	Int Total
Peak Hour Analysis I	rom 07:00	AM to	08:45 AM	- Peak 1 of 1					5			, pp. reter	inte rotai
Peak Hour for Entire	Intersectio	n Begin	s at 07:45	AM									
07:45 AM	170	2	0	172	0	0	0	0	2	224	0	226	398
08:00 AM	173	1	0	174	0	0	0	0	3	197	Õ	200	374
08:15 AM	167	0	0	167	0	0	0	0	6	197	Ō	203	370
08:30 AM	164	0	0	164	0	0	0	0	1	183	Ō	184	348
Total Volume	674	3	0	677	0	0	0	0	12	801	0	813	1490
% App. Total	99.6	0.4	0		0	0	0	4,94503	1.5	98.5	Õ		
PHF	.974	.375	.000	.973	.000	.000	.000	.000	.500	.894	.000	.899	.936



Stephen G. Pernaw & Company, Inc. P.O. Box 1721 Concord, New Hampshire 03302

Weather: Clear Collected By: MV Job Number: 2122A Town/State: Portsmouth, NH File Name : 2122A_B_King_AM_&_PM Site Code : 2122A Start Date : 7/29/2021 Page No : 2

		US R From	toute 1 North		В	urger Kii Fror	ng Drivew n East	/ay	US Route 1 From South				
Start Time	Thru	Left	U-Turn	App. Total	Right	Left	U-Turn	App. Total	Right	Thru	U-Turn	App Total	Int Total
Peak Hour Analysis I	From 07:45	5 AM to 0	8:30 AM	- Peak 1 of 1				PP: The second	, and		o rum	ripp. rotar	int. Total
Peak Hour for Entire	Intersectio	n Begins	at 07:45	AM									
07:45 AM	13	ŏ	0	13	0	0	0	0	0	11	Ō	11	24
08:00 AM	8	0	0	8	0	Ō	Ō	õ	õ	5	ň	5	13
08:15 AM	7	0	0	7	Ō	Ō	Õ	õ	õ	7	n n	7	14
08:30 AM	7	0	0	7	0	Ō	0	õ	õ	5	Ő	5	17
Total Volume	35	0	0	35	0	0	0	0	0	28	0	28	63
% App. Total	100	0	0		0	0	0	-	ñ	100	ñ	20	05
PHF	.673	.000	.000	.673	.000	.000	.000	.000	.000	.636	.000	.636	656


Weather: Clear Collected By: MV Job Number: 2122A Town/State: Portsmouth, NH

	Groups Printed- CARS - TRUCKS													
		US F	Route 1		E	Burger Ki	ng Drivew	ay		USF	Route 1			
		From	North			Fror	n East			From	South			
Start Time	Thru	Left	U-Turn	App. Total	Right	Left	U-Turn	App. Total	Right	Thru	U-Turn	App. Total	Int. Total	
07:00 AM	91	0	0	91	0	0	0	0	0	115	0	115	206	
07:15 AM	105	1	0	106	0	0	0	0	0	142	0	142	248	
07:30 AM	146	1	0	147	0	0	0	0	1	195	0	196	343	
07:45 AM	170	2	0	172	0	0	0	0	2	224	0	226	398	
Total	512	4	0	516	0	0	0	0	3	676	0	679	1195	
												07010701	1.1.5.5.5.	
08:00 AM	173	1	0	174	0	0	0	0	3	197	0	200	374	
08:15 AM	167	0	0	167	0	0	0	0	6	197	0	203	370	
08:30 AM	164	0	0	164	0	0	0	0	1	183	0	184	348	
08:45 AM	165	1	0	166	0	0	0	0	1	207	0	208	374	
Total	669	2	0	671	0	0	0	0	11	784	0	795	1466	
Grand Total	1181	6	0	1187	0	0	0	0	14	1460	0	1474	2661	
Apprch %	99.5	0.5	0		0	0	0		0.9	99.1	Ō			
Total %	44.4	0.2	0	44.6	0	0	0	0	0.5	54.9	Ō	55.4		
CARS	1115	6	Ō	1121	0	0	0	0	14	1393	0	1407	2528	
% CARS	94.4	100	0	94.4	0	0	0	0	100	95.4	0	95.5	95	
TRUCKS	66	0	0	66	0	0	0	0	0	67	Ō	67	133	
% TRUCKS	5.6	0	0	5.6	0	0	0	0	Ó	4.6	Ō	4.5	5	



Weather: Clear Collected By: MV Job Number: 2122A Town/State: Portsmouth, NH

n App. Total Int. Total
) 14 16
) 9 14
) 9 28
) 11 24
) 43 82
) 5 13
) 7 14
) 5 12
) 7 12
) 24 51
) 67 133
)
50.4



Weather: Clear Collected By: MV Job Number: 2122A Town/State: Portsmouth, NH

		US R From	oute 1 North		В	urger Kir Fron	ng Drivew n East	ay		US F From	Route 1 n South		
Start Time	Thru	hru Left U-Turn App. Total				Left	U-Turn	App. Total	Right	Thru	U-Turn	App. Total	Int. Total
Peak Hour Analysis F	From 03:00	PM to 0	5:45 PM	- Peak 1 of 1					•				
Peak Hour for Entire	Intersectio	n Begins	at 03:30	PM									
03:30 PM	249	2	0	251	0	0	0	0	5	249	0	254	505
03:45 PM	256	3	0	259	0	0	0	0	3	244	0	247	506
04:00 PM	278	4	0	282	0	0	0	0	5	240	0	245	527
04:15 PM	259	2	0	261	0	0	0	0	6	251	0	257	518
Total Volume	1042	11	0	1053	0	0	0	0	19	984	0	1003	2056
% App. Total	99	1	0		0	0	0		1.9	98.1	0		
PHF	.937	.688	.000	.934	.000	.000	.000	.000	.792	.980	.000	.976	.975



Weather: Clear Collected By: MV Job Number: 2122A Town/State: Portsmouth, NH

		US R From	oute 1 North		В	Burger Kin Fror	ng Drivew n East	ay		US f Fron	Route 1 n South		
Start Time	Thru	Left	U-Turn	App. Total	Right	Left	U-Turn	App. Total	Right	Thru	U-Turn	App. Total	Int. Total
Peak Hour Analysis I	From 03:30	PM to 0	4 15 PM	- Peak 1 of 1									
Peak Hour for Entire	Intersectio	n Begins	at 03:30	PM									
03:30 PM	6	Õ	0	6	0	0	0	0	0	16	0	16	22
03:45 PM	5	0	0	5	0	0	0	0	0	10	Ō	10	15
04:00 PM	1	0	0	1	0	0	0	0	0	5	Ō	5	6
04:15 PM	4	0	0	4	0	0	0	0	1	3	0	4	8
Total Volume	16	0	0	16	0	0	0	0	1	34	0	35	51
% App. Total	100	0	0		0	0	0	20530	2.9	97.1	0		• • •
PHF	.667	.000	.000	.667	.000	.000	.000	.000	.250	.531	.000	.547	.580



Weather: Clear Collected By: MV Job Number: 2122A Town/State: Portsmouth, NH

 Groups Printed- CARS - TRUCKS													
		US R	oute 1		E	Burger Ki	ng Drivew	ay		US F	Route 1		
		From	North			Fror	n East			Fron	n South		
Start Time	Thru	Left	U-Turn	App. Total	Right	Left	U-Turn	App. Total	Right	Thru	U-Turn	App. Total	Int. Total
03:00 PM	273	3	0	276	0	0	0	0	4	233	0	237	513
03:15 PM	242	3	0	245	0	0	0	0	1	225	0	226	471
03:30 PM	249	2	0	251	0	0	0	0	5	249	0	254	505
 03:45 PM	256	3	0	259	0	0	0	0	3	244	0	247	506
Total	1020	11	0	1031	0	0	0	0	13	951	0	964	1995
04:00 PM	278	4	0	282	0	0	0	0	5	240	0	245	527
04:15 PM	259	2	0	261	0	0	0	0	6	251	0	257	518
04:30 PM	259	4	0	263	0	1	0	1	4	223	0	227	491
 04:45 PM	261	2	0	263	0	1	0	1	7	222	Ō	229	493
Total	1057	12	0	1069	0	2	0	2	22	936	Ō	958	2029
05:00 PM	245	2	0	247	0	0	0	0	5	261	0	266	513
05:15 PM	248	3	0	251	0	0	0	0	9	215	0	224	475
05:30 PM	212	4	0	216	1	0	0	1	2	218	0	220	437
 05:45 PM	214	1	0	215	0	0	0	0	6	214	0	220	435
Total	919	10	0	929	1	0	0	1	22	908	0	930	1860
												1	
Grand Total	2996	33	0	3029	1	2	0	3	57	2795	0	2852	5884
Apprch %	98.9	1.1	0		33.3	66.7	0		2	98	Ō		
Total %	50.9	0.6	0	51.5	0	0	0	0.1	1	47.5	Ō	48.5	
CARS	2948	33	0	2981	1	2	0	3	56	2736	0	2792	5776
% CARS	98.4	100	0	98.4	100	100	0	100	98.2	97.9	0	97.9	98.2
TRUCKS	48	0	0	48	0	0	0	0	1	59	0	60	108
% TRUCKS	1.6	0	0	1.6	0	Ō	0	0	1.8	2.1	Õ	2.1	1.8
2/2											-		

Weather: Clear Collected By: MV Job Number: 2122A Town/State: Portsmouth, NH



Weather: Clear Collected By: MV Job Number: 2122A Town/State: Portsmouth, NH

					Group	s Printed	- TRUCK	S					
		US F From	Route 1 North		В	urger Kii Fror	ng Drivew n East	ay		US F From	Route 1 n South		
Start Time	Thru	Left	U-Turn	App. Total	Right	Left	U-Turn	App. Total	Right	Thru	U-Turn	App. Total	Int. Total
03:00 PM	14	0	0	14	0	0	0	0	0	11	0	11	25
03:15 PM	6	0	0	6	0	0	0	0	0	3	0	3	9
03:30 PM	6	0	0	6	0	0	0	0	0	16	Ō	16	22
03:45 PM	5	0	0	5	0	0	0	Ō	Ō	10	Õ	10	15
Total	31	0	0	31	0	0	0	0	0	40	0	40	71
04:00 PM	1	0	0	1	0	0	0	0	0	5	0	5	6
04:15 PM	4	0	0	4	0	0	0	0	1	3	Ō	4	Ř
04:30 PM	2	0	0	2	0	0	0	0	Ó	3	Õ	3	5
04:45 PM	4	0	0	4	0	Ó	Ō	Ō	Ō	õ	õ	õ	4
Total	11	0	0	11	0	0	0	0	1	11	0	12	23
05:00 PM	1	0	0	1	0	0	0	0	0	3	0	3	4
05:15 PM	2	0	0	2	0	0	0	0	0	0	0	0	2
05:30 PM	0	0	0	0	0	0	0	0	0	4	0	4	4
05:45 PM	3	0	0	3	0	0	0	0	0	1	0	1	4
Total	6	0	0	6	0	0	0	0	0	8	0	8	14
Grand Total	48	0	0	48	0	0	0	0	1	59	0	60	108
Apprch %	100	0	0		0	Ó	Ō	-	1.7	98.3	õ	50	,50
Total %	44.4	0	0	44.4	Ō	Ō	Ō	0	0.9	54.6	õ	55.6	



Weather: Clear Collected By: MV Job Number: 2122A Town/State: Manchester: NH

		US R From	oute 1 North		В	Burger Kii Fror	ng Drivew n East	/ay		US F Fron	Route 1 n South		
Start Time	Thru	Left	U-Turn	App. Total	Right	Left	U-Turn	App. Total	Right	Thru	U-Turn	App. Total	Int. Total
Peak Hour Analysis F	From 09:00	AM to C	1:45 PM	- Peak 1 of 1									
Peak Hour for Entire	Intersectio	n Begins	at 11:15	AM									
11:15 AM	213	4	0	217	1	0	0	1	2	289	0	291	509
11:30 AM	232	6	0	238	0	0	0	0	6	271	Ō	277	515
11:45 AM	223	6	0	229	0	0	0	0	4	286	0	290	519
12:00 PM	238	3	0	241	0	0	0	0	3	298	0	301	542
Total Volume	906	19	0	925	1	0	0	1	15	1144	0	1159	2085
% App. Total	97.9	2.1	0		100	0	0		1.3	98.7	0		
PHF	.952	.792	.000	.960	.250	.000	.000	.250	.625	.960	.000	.963	.962



Weather: Clear Collected By: MV Job Number: 2122A Town/State: Manchester: NH

		US R From	oute 1 North		В	urger Kir Fron	ng Drivew n East	/ay		US F From	Route 1 South		
Start Time	Thru	Thru Left U-Turn App. Total				Left	U-Turn	App. Total	Right	Thru	U-Turn	App. Total	Int. Total
Peak Hour Analysis F	From 11:15	AM to 1	2:00 PM	- Peak 1 of 1					0				-
Peak Hour for Entire	Intersectio	n Begins	at 11:15	AM									
11:15 AM	4	Ō	0	4	0	0	0	0	0	1	0	1	5
11:30 AM	2	0	0	2	0	0	0	0	0	5	0	5	7
11:45 AM	2	0	0	2	0	0	0	0	0	4	0	4	6
12:00 PM	4	0	0	4	0	0	0	0	0	2	0	2	6
Total Volume	12	0	0	12	0	0	0	0	0	12	0	12	24
% App. Total	100	0	0		0	0	0		0	100	0		
PHF	.750	.000	.000	.750	.000	.000	.000	.000	.000	.600	.000	.600	.857



Stephen G. Pernaw & Company, Inc. P.O. Box 1721

Weather: Clear Collected By: MV Job Number: 2122A Town/State: Manchester: NH File Name : 2122A_B King Sat Site Code : 2122A Start Date : 7/31/2021 Page No : 1

					Groups Pr	inted- CA	RS - TRI	JCKS					
1		US R From	toute 1 North		E	Burger Kir Fron	ng Drivew n East	/ay		US F From	Route 1 n South		
Start Time	Thru	Left	U-Turn	App. Total	Right	Left	U-Turn	App. Total	Right	Thru	U-Turn	App. Total	Int. Total
09:00 AM	170	1	0	171	0	0	0	0	0	166	0	166	337
09:15 AM	165	4	0	169	0	0	0	0	4	177	0	181	350
09:30 AM	185	4	0	189	1	0	0	1	5	211	0	216	406
09:45 AM	197	3	0	200	0	0	0	0	3	207	0	210	410
Total	717	12	0	729	1	0	0	1	12	761	0	773	1503
10:00 AM	183	2	0	185	0	0	0	0	1	248	0	249	434
10:15 AM	195	2	1	198	õ	õ	õ	õ	4	257	õ	261	459
10:30 AM	205	3	Ó	208	õ	Õ	Ō	Ő	1	231	õ	232	440
10:45 AM	234	5	Ō	239	1	Õ	õ	1	3	266	õ	269	509
Total	817	12	1	830	1	0	0	1	9	1002	0	1011	1842
11.00 AM	217	5	0	222	0	0	0	0	5	240	٥	245	467
11:15 AM	213	4	Ő	217	1	õ	õ	1	2	289	ň	291	509
11:30 AM	232	6	Õ	238	ò	õ	õ		Ĩ	271	ň	277	515
11:45 AM	223	6	Ō	229	ŏ	õ	õ	õ	4	286	õ	290	519
Total	885	21	0	906	1	0	0	1	17	1086	0	1103	2010
12:00 PM	238	3	0	241	0	0	0	0	3	298	0	301	542
12:15 PM	187	4	0	191	0	0	0	0	7	246	0	253	444
12:30 PM	214	2	0	216	0	0	0	0	5	256	0	261	477
12:45 PM	231	3	0	234	0	0	0	0	9	264	0	273	507
Total	870	12	0	882	0	0	0	0	24	1064	0	1088	1970
01:00 PM	222	2	0	224	0	0	0	0	6	290	0	296	520
01:15 PM	234	8	0	242	0	1	0	1	11	256	Ō	267	510
01:30 PM	219	5	0	224	1	0	0	1	8	267	0	275	500
01:45 PM	199	0	0	199	0	0	0	0	1	255	Ō	256	455
Total	874	15	0	889	1	1	0	2	26	1068	0	1094	1985
Grand Total	4163	72	1	4236	4	1	0	5	88	4981	0	5069	9310
Apprch %	98.3	1.7	0		80	20	0		1.7	98.3	0		
Total %	44.7	0.8	0	45.5	0	0	0	0.1	0.9	53.5	0	54.4	
CARS	4115	72	1	4188	4	1	0	5	88	4930	0	5018	9211
% CARS	98.8	100	100	98.9	100	100	0	100	100	99	0	99	98.9
TRUCKS	48	0	0	48	0	0	0	0	0	51	0	51	99
% TRUCKS	1.2	0	0	1.1	0	0	0	0	0	1	0	1	1.1

Concord, New Hampshire 03302

Weather: Clear Collected By: MV Job Number: 2122A Town/State: Manchester: NH



Weather: Clear Collected By: MV Job Number: 2122A Town/State: Manchester: NH

					Group	s Printed	- TRUCK	S					
		US R	oute 1		E	Burger Ki	ng Drivew	ay		US F	Route 1		
		From	North			Fror	n East	-		From	South		
Start Time	Thru	Left	U-Turn	App. Total	Right	Left	U-Turn	App. Total	Right	Thru	U-Turn	App. Total	Int. Total
 09:00 AM	2	0	0	2	0	0	0	0	0	4	0	4	6
09:15 AM	3	0	0	3	0	0	0	0	0	0	0	0	3
09:30 AM	1	0	0	1	0	0	0	0	0	1	0	1	2
09:45 AM	2	0	0	2	0	0	0	0	0	3	0	3	5
 Total	8	0	0	8	0	0	0	0	0	8	0	8	16
10:00 AM	1	0	0	1	0	0	0	0	0	2	0	2	3
10:15 AM	3	0	0	3	0	0	0	0	0	1	0	1	4
10:30 AM	1	0	0	1	0	0	0	0	0	4	0	4	5
 10:45 AM	3	0	0	3	0	0	0	0	0	1	0	1	4
Total	8	0	0	8	0	0	0	0	0	8	0	8	16
11:00 AM	4	0	0	4	0	0	0	0	0	1	0	1	5
11:15 AM	4	0	0	4	0	0	0	0	0	1	0	1	5
11:30 AM	2	0	0	2	0	0	0	0	0	5	0	5	7
 11:45 AM	2	0	0	2	0	0	0	0	0	4	0	4	6
Total	12	0	0	12	0	0	0	0	0	11	0	11	23
12:00 PM	4	0	0	4	0	0	0	0	0	2	0	2	6
12:15 PM	3	0	0	3	0	0	0	0	0	6	0	6	9
12:30 PM	2	0	0	2	0	0	0	0	0	2	0	2	4
 12:45 PM	1	0	0	1	0	0	0	0	0	1	0	1	2
Total	10	0	0	10	0	0	0	0	0	11	0	11	21
01:00 PM	2	0	0	2	0	0	0	0	0	3	0	3	5
01:15 PM	5	0	0	5	0	0	0	0	0	4	0	4	9
01:30 PM	2	0	0	2	0	0	0	0	0	1	0	1	3
 01:45 PM	1	0	0	1	0	0	0	0	0	5	0	5	6
Total	10	0	0	10	0	0	0	0	0	13	0	13	23
Grand Total	48	0	0	48	0	0	0	0	0	51	0	51	99
Apprch %	100	0	0		0	0	0		0	100	0		
Total %	48.5	0	0	48.5	0	0	0	0	0	51.5	0	51.5	

Weather: Clear Collected By: MV Job Number: 2122A Town/State: Manchester: NH





					1			1	
	Bu	Irger King - N	North Drivew	/ay	v	Vater Count	ry	Sum	
	RO	LO	LI	RI	RI	LI	LO		-
7:00 AM	0	0	0	0	0	0	0	0	
7:15 AM	0	2	1	0	0	0	0	3	
7:30 AM	2	0	0	0	0	0	0	2	_
7:45 AM	1	1	0	0	0	0	0	2	7
8:00 AM	3	0	0	0	0	1	0	4	11
8:15 AM	2	0	1	0	0	0	0	3	11
8:30 AM	1	1	0	0	1	0	0	3	12
8:45 AM	1	2	0	0	0	0	0	3	13
								20	
Total Count									
7 AM - 9 AM	10	6	2	0	1	1	0	20	
Peak Hour									
7:45 - 8:45 AM	7	2	1	0	1	1	0	12	

Burger King Driveway Volumes (Thursday, 7/29/21) Lafayette Road, Portsmouth, New Hampshire



			-		1	•		1	
	Βι	urger King - I	North Drivew	/ay	v v	Vater Count	ry	Sum	
	RO	LO	LI	RI	RI	LI	LO		
3:00 PM	5	2	0	0	2	0	0	9	
3:15 PM	4	5	1	0	0	2	0	12	
3:30 PM	5	0	1	0	0	0	0	6	
3:45 PM	3	4	2	0	0	0	1	10	37
4:00 PM	9	3	0	1	0	0	0	13	41
4:15 PM	3	3	0	0	0	1	0	7	36
4:30 PM	4	5	1	0	o	0	0	10	40
4:45 PM	4	2	0	0	0	1	0	7	37
5:00 PM	3	2	0	0	1	0	0	6	30
5:15 PM	8	3	0	0	0	0	0	11	34
5:30 PM	2	3	0	0	0	0	0	5	29
5:45 PM	3	6	0	0	0	2	0	11	33
								107	
Total Count									
3 PM - 6 PM	53	38	5	1	3	6	1	107	
Peak Hour									
3:30 - 4:30 PM	20	10	3	1	0	1	1	36	

Burger King Driveway Volumes (Thursday, 7/29/21) Lafayette Road, Portsmouth, New Hampshire



I

		Burger h	King - North	Driveway			Water Countr	у	Sum	
					Straight					-
	RO	LO	LI	RI	Across	RI	LI	LO		
9:00 AM	1	4	1	0	1	10	6	0	23	
9:15 AM	3	1	0	0	0	23	7	0	34	
9:30 AM	3	1	1	0	5	37	5	0	52	
9:45 AM	5	3	3	0	4	45	19	0	79	188
10:00 AM	3	1	0	0	3	59	36	0	102	267
10:15 AM	4	0	2	0	1	60	21	0	88	321
10:30 AM	0	3	1	0	3	48	22	0	77	346
10: 45 AM	4	1	0	0	1	34	2	0	42	309
11:00 AM	3	1	0	0	3	54	19	0	80	287
11: 15 AM	3	3	1	0	4	38	30	0	79	278
11:30 AM	6	2	1	1	0	36	27	0	73	274
11:45 AM	10	2	1	0	1	24	34	0	72	304
12:00 PM	7	2	1	1	1	15	29	0	56	280
12:15 PM	5	3	0	0	4	18	28	0	58	259
12:30 PM	4	0	1	0	3	15	27	0	50	236
12:45 PM	3	7	0	1	0	19	22	0	52	216
1:00 PM	6	1	1	0	2	16	44	0	70	230
1:15 PM	3	4	0	0	2	14	18	0	41	213
1:30 PM	5	5	0	0	3	10	20	0	43	206
1:45 PM	7	7	1	0	0	7	22	о	44	198
									1215	
Total Count										
9 AM - 2 PM	85	51	15	3	41	582	438	0	1215	
Peak Hour										
11:15 AM - 12:15 PM	26	9	4	2	6	113	120	0	280	

Burger King Driveway Volumes (Saturday, 7/31/21) Lafayette Road, Portsmouth, New Hampshire

1



	Common Man Roadside Market - S. Willow Street, Manchester, New Hampshire									
				Goffs Falls				s Falls		
_	SW	Villow	Main Driveway			W Drwy		Sum		
	RI	RO	RI	RO	LO	LI	LO	RO		
7:00 AM	5	4	2	8	0	6	1	1	27	
7:15 AM	9	3	2	8	2	5	2	0	31	
7:30 AM	16	1	2	3	4	3	2	1	32	
7:45 AM	6	9	0	5	4	7	5	0	36	126
8:00 AM	13	3	3	2	4	4	4	0	33	132
8:15 AM	13	2	3	7	4	2	5	1	37	138
8:30 AM	9	3	2	4	1	1	6	1	27	133
8:45 AM	8	3	4	6	3	4	2	1	31	128
									254	
Total Count										
7 AM - 9 AM	79	28	18	43	22	32	27	5	254	
									-	
Peak Hour										
7:30 - 8:30 AM	48	15	8	17	16	16	16	2	138	
Total Count	Ins =	129		Peak Hour	Ins =	72				
	• • • • • • •									

Similar Site Driveway Volumes (Thursday, 7/29/21)

Total Count	Ins = 129	Peak Hour	Ins = 72
	Outs = 125		Outs = 66
	254		138



	Common Man Roadside Market - S. Willow Street, Manchester, New Hampshire									
				Goffs F	alls		Goffs	s Falls		
_	SN	/illow		Main Driveway			W Drwy		Sum	_
	RI	RO	RI	RO	LO	LI	LO	RO		-
3:00 PM	9	4	5	6	5	2	1	1	33	
3:15 PM	3	3	3	5	3	2	2	0	21	_
3:30 PM	16	4	6	5	2	3	2	3	41	
3:45 PM	12	3	5	8	4	5	2	3	42	137
4:00 PM	14	6	2	5	1	5	5	1	39	143
4:15 PM	7	3	2	6	1	2	7	3	31	153
4:30 PM	12	2	3	2	2	5	3	2	31	143
4:45 PM	13	4	3	5	2	3	7	0	37	138
5:00 PM	11	4	1	5	3	2	5	1	32	32
5:15 PM	6	1	5	5	2	4	1	2	26	58
5:30 PM	11	6	4	5	1	3	3	3	36	94
5:45 PM	9	2	2	7	5	4	3	1	33	127
									402	
Total Count										
3 PM - 6 PM	123	42	41	64	31	40	41	20	402	
Peak Hour										
3:30 - 4:30 PM	49	16	15	24	8	15	16	10	153	
Total Count	Ins =	204		Peak Hour	Ins =	79				
	Outs =	198			Outs =	74				
		402				153				

Similar Site Driveway Volumes (Thursday, 7/29/21)



	С	ommon Mar	Roadside	Market - S. Wil	low Street	, Manchester	r, New Hamp	shire		
				Goffs F	alls		Goffs	Falls		
	SW	lllow		Main Driv	veway		w c	Drwy	Sum	-10
	RI	RO	RI	RO	LO	LI	LO	RO		
9:00 AM	6	3	7	4	1	2	2	0	25	
9:15 AM	5	5	3	4	3	3	3	2	28	
9:30 AM	3	2	7	4	2	3	1	1	23	
9:45 AM	10	2	7	9	6	4	3	1	42	118
10:00 AM	7	2	9	5	3	1	3	1	31	124
10:15 AM	7	3	4	8	3	5	1	0	31	127
10:30 AM	7	6	1	1	1	1	2	1	20	124
10:45 AM	11	6	7	5	3	3	3	0	38	120
11:00 AM	5	5	5	5	1	5	1	0	27	116
11:15 AM	9	1	5	4	5	2	3	2	31	116
11:30 AM	11	2	3	6	3	0	1	1	27	123
11: 45 AM	13	3	3	11	7	4	1	0	42	127
12:00 PM	4	2	5	5	5	7	4	0	32	132
12:15 PM	6	1	6	7	4	1	2	1	28	129
12:30 PM	10	1	5	9	3	4	3	4	39	141
12:45 PM	10	2	1	4	3	5	4	2	31	130
1:00 PM	12	7	6	8	2	5	2	1	43	141
1:15 PM	9	5	2	3	4	4	3	0	30	143
1:30 PM	10	5	2	11	3	5	2	0	38	142
1:45 PM	8	4	5	4	4	2	2	0	29	140
									635	
Total Count										
9 AM - 2 PM	163	67	93	117	66	66	46	17	635	
Peak Hour										
12:30 - 1:30 PM	41	15	14	24	12	18	12	7	143	
Total Count	Ins =	322		Peak Hour	Ins =	73				
	Outs =	313			Outs =	70				
		635				143				

<u>Similar Site Driveway Volumes (Saturday, 7/31/21)</u>

Appendix D Seasonal Adjustment Factor / Historical Growth Rate / COVID Factor

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Seasonal Adjustment Factors NHDOT Group 4 (Urban Highways)



Stephen G. Pernaw & Company, Inc.

Year 2019 Monthly Data - Urban

		Adjustr	nent to
Month	ADT	Average	Peak
Jan	11,431	1.12	1.23
Feb	11,848	1.08	1.18
Mar	12,141	1.06	1.15
Apr	12,860	1.00	1.09
May	13,551	0.95	1.03
Jun	13,785	0.93	1.02
Jul	13,942	0.92	1.01
Aug	14,016	0.92	1.00
Sep	13,379	0.96	1.05
Oct	13,339	0.96	1.05
Nov	12,265	1.05	1.14
Dec	11,496	1.12	1.22

Year 2018 Monthly Data - Urban

		Adjustment to		
<u>Month</u>	ADT	Average	Peak	
Jan	11,282	1.13	1.24	
Feb	11,848	1.08	1.18	
Mar	11,828	1.08	1.18	
Apr	12,491	1.02	1.12	
May	13,587	0.94	1.03	
Jun	13,911	0.92	1.00	
Jul	13,765	0.93	1.01	
Aug	13,945	0.92	1.00	
Sep	13,168	0.97	1.06	
Oct	13,367	0.96	1.04	
Nov	12,215	1.05	1.14	
Dec	11,963	1.07	1.17	

Year 2017 Monthly Data - Urban

		Adjustment to				
<u>Month</u>	ADT	Average	Peak			
Jan	12254	1.21	1.33			
Feb	13494	1.10	1.21			
Mar	14,335	1.03	1.14			
Apr	15004	0.99	1.09			
May	15547	0.95	1.05			
Jun	16310	0.91	1.00			
Jul	15523	0.95	1.05			
Aug	15974	0.93	1.02			
Sep	15546	0.95	1.05			
Oct	15104	0.98	1.08			
Nov	14,544	1.02	1.12			
Dec	14151	1.05	1.15			

Average Peak-Month Factor 1.02	2
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Stephen G. Pernaw & Company, Inc.

STEPHEN G. PERNAW & COMPANY, INC.PROJECT:Proposed Gas Station/Convenience Store, Manchester, New HampshireNUMBER:2122ACOUNT STATION:82379150

HISTORICAL GROWTH CALCULATIONS

LOCATION :	US1 - North of Ocean Rd, Portsmouth, NH
CASE :	AADT

ARITHMETIC PROJECTIONS

YEAR	AADT			PROJEC	CTIONS	
		Regression O	utput:			
2016	19093	Constant	309144	2019	19014	
2017	19475	Std Err of Y Est	683.84366	2020	18870	
2018	19865	R Squared	0.0994176	2021	18726	
2019	18484	No. of Observations	4	2022	18583	
		Degrees of Freedom	2	2023	18439	
				2024	18295	
		X Coefficient	-143.7	2025	18152	
		Std Err of Coef.	305.82418	2026	18008	
				2027	17864	
				2028	17720	
				2029	17577	

RATE = -144 VPD/YEAR

GEOMETRIC PROJECTIONS

YEAR	AADT	Ln AADT			PROJEC	CTIONS	
			Regression O	utput:			
2016	19093	9.85708	Constant	25.48353	2019	19001	
2017	19475	9.87689	Std Err of Y Est	0.035581	2020	18854	
2018	19865	9.89671	R Squared	0.1058373	2021	18709	
2019	18484	9.82466	No. of Observations	4	2022	18564	
			Degrees of Freedom	2	2023	18421	
					2024	18279	
			X Coefficient	-0.0077421	2025	18138	
			Std Err of Coef.	0.0159123	2026	17998	
					2027	17859	
					2028	17722	
					2029	17585	
				$\neg \land \land$			

CONCLUSION: USE 1%/YEAR

RATE = -0.8 % / YEAR





Transportation Data Management System

List View			
Record H	4936 🕨 🖬 of 5746 Goto Record	go	
Location ID	82379150	MPO ID	
Туре	SPOT	HPMS ID	
On NHS	Yes	On HPMS	Yes
LRS ID	U0000001	LRS Loc Pt.	
SF Group	04	Route Type	
AF Group	04	Route	US 1
GF Group	E	Active	Yes
Class Dist Grp	Default	Category	3
Seas Clss Grp	Default		
WIM Group	Default 🕨		
QC Group	Default		
Fnct'l Class	Other Principal Arterial	Milepost	
Located On	Lafayette Rd		
Loc On Alias	US 1 (LAFAYETTE RD) NORTH OF OCEAN RD (SB-NB)	(81379211-81379	9212)
More Detail 🕨			
STATION DAT	A		

Directions: 2-WAY NB SB

				del.
A	А	D	T.	

	Year	AADT	DHV-30	К%	D %	PA	BC	Src
	2020	15,600 ³		9	50	14,196 (91%)	1,404 (9%)	Grown from 2019
	2019	18,484	1,674	9	50	16,931 (92%)	1,553 (8%)	
	2018	19,865 ³		8	53	18,315 (92%)	1,550 (8%)	Grown from 2017
	2017	19,475 ³		8	53	18,075 (93%)	1,400 (7%)	Grown from 2016
	2016	19,093	1,621	8	53	17,413 (91%)	1,680 (9%)	
<<	<	> >>	1-5 of 17					

	Model Year	Model AADT	AM PHV	AM PPV	MD PHV	MD PPV	PM PHV	PM PPV	NT PHV	NT PP	
VOLU	JME COUN	1T				VOLUME TREND					
		Date		Int	Total	Year An			nual Growth		
-	Th	u 6/6/2019		60 2	21,455	2020			16%		
1	We	ed 6/5/2019		60 2	21,364	2019		-7%			
5	Tu	e 6/4/2019		60 2	21,469	2018		2%			
1	Tue	e 7/19/2016		60 [·]	19,597	2017		-			
1	Su	n 7/17/2016		60 [~]	16,959	2016		70/			
1	Fri	9/27/2013		60 2	20,159	2010		7 70			
	Thu	u 9/26/2013		60 ·	19,003	2015 3%			576 50/		
1	We	d 9/25/2013		60 ·	18,690	2014		2%			
-	Tue	9/24/2013		60 .	18,712	2013	-7%				
1	Mon 9/23/2013			60 -	18,246	2010		-	2%		
12	T			_		2007		(0%		





Transportation Data Management System

	List View All DIRs											
Red	cord 🖊	1		of 1	Goto Re	ecord	go					
L	ocation ID	02345001	<u></u>					MPO ID				
	Туре	SPOT					н	IPMS ID				
	On NHS	Yes					0	n HPMS	Yes			
	LRS ID	U0000001					LRS	Loc Pt.				
	SF Group	04	****	- <u> </u>			Rol	ite Type				
	AF Group	04						Route	US 1			
	GF Group	E						Active	Yes			
Class	s Dist Grp	Default) c	ategory	1			
Seas	S Clss Grp	Default										
N	/IM Group	Default		· · · · · · ·								
	QC Group	Perm										
Fr	nct'l Class	Other Principa	al Arterial				N	lilepost				
	ocated On	Lafayette Rd						05 040 15	000			
LOC	c On Allas	US 1 (LAFAY)	ETTERD)	NORTH	JF NORTH	RD (SB-NE	3) (013450	05-01345	006)			
More	Detail 🕨	l										
STA	TION DAT	Ά							S	how Data		
Direc	tions: 2	-WAY NB	SB 🚱	1								
	Larrage	1	1									
	6											
AAI	DT 🔛			16.04	D 4/		-		_	_		
	2020	13 085	1 464	К %	D %)	ΡΔ		-	••••		
	2020	10,000	1.404	54 10 54 12,7			06 (01%)	1 250	تر (۵%)	Src		
	2010	16 139	1 576	10 10	54 50	12,72 14 78	26 (91%) 33 (92%)	а 1,259 1 356	(9%) (8%)	Src		
	2018	16,139 16 254	1,576	10 10 10	54 50 54	12,72 14,78 14 98	26 (91%) 33 (92%) 35 (92%)	1,259 1,356 1 269	; (9%) (8%) (8%)	Src		
	2018 2017	16,139 16,254 16,356	1,576 1,620	10 10 10	54 50 54	12,72 14,78 14,98	26 (91%) 33 (92%) 35 (92%)	1,259 1,356 1,269	(9%) (8%) (8%)	Src		
	2018 2017 2016	16,139 16,254 16,356 16,353	1,576 1,620	10 10 10	54 50 54	12,72 14,78 14,98	26 (91%) 33 (92%) 35 (92%)	1,259 1,356 1,269	(9%) (8%) (8%)	Src		
1<<	2018 2017 2016	16,139 16,254 16,356 16,353	1,576 1,620	10 10 10	54 50 54	12,72 14,78 14,98	26 (91%) 33 (92%) 35 (92%)	1,259 1,356 1,269	(9%) (8%) (8%)	Src		
<< Trav	2018 2017 2016	16,139 16,254 16,356 16,353 > >>	1,576 1,620 1-5 of 6	10 10 10	54 50 54	12,72 14,78 14,98	26 (91%) 33 (92%) 95 (92%)	1,259 1,356 1,269	(9%) (8%) (8%)	Src		
<< Trav	2018 2017 2016 < [el Deman Model	16,139 16,254 16,356 16,353 > >> d Model Model	1,576 1,620 1-5 of (10 10 10 36	54 50 54	12,72 14,78 14,98	26 (91%) 33 (92%) 35 (92%)	1,259 1,356 1,269	(9%) (8%) (8%)			
I<< Trav	2018 2017 2016 Contemport el Deman Model Year	16,139 16,254 16,356 16,353 > >> d Model AADT	1,576 1,620 1-5 of 0	10 10 10 56 AM PPV	54 50 54	12,72 14,78 14,98 MD PPV	26 (91%) 33 (92%) 35 (92%) PM PHV	В 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) NT PHV	Src NT PPV		
I<< Trav	2018 2017 2016 Contemport 2016 Contemport 2018 2018 2018 2018 2018 2018 2017 2017 2017 2017 2017 2017 2017 2017	16,139 16,254 16,356 16,353 > >> d Model AADT	1,576 1,620 1-5 of 0	10 10 10 66 AM PPV	54 50 54	12,72 14,78 14,98 MD PPV	26 (91%) 33 (92%) 35 (92%) 95 (92%) PM PHV E TRENI	на 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) NT PHV	Src NT PPV		
Trav VOL	2018 2017 2016 I Deman Model Year UME COU	16,139 16,254 16,356 16,353 > >> d Model AADT JNT Date	1,576 1,620 1-5 of (10 10 10 66 AM PPV	54 50 54 / MD PHV Total	12,72 14,78 14,98 MD PPV VOLUM Year	26 (91%) 33 (92%) 35 (92%) 95 (92%) PM PHV E TRENI	на 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) NT PHV	Src NT PPV		
Image: Volume	2018 2017 2016 el Deman Year UME COL	16,139 16,254 16,356 16,353 > >> d Model Model AADT JNT Date on 1/17/2022	1,576 1,620 1-5 of 0 AM PHV	10 10 10 66 AM PPV	54 50 54 / MD PHV Total 10,741	12,72 14,78 14,98 MD PPV VOLUMI Year 2020	26 (91%) 33 (92%) 35 (92%) 95 (92%) PM PHV E TRENI	на 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) NT PHV al Growth 13%	Src NT PPV		
VOL	2018 2017 2016 el Deman Model Year UME COU MM S	16,139 16,254 16,356 16,353 > >> d Model Model AADT JNT Date on 1/17/2022 un 1/16/2022	1,576 1,620 1-5 of (10 10 10 56 AM PPV Int 60 60	54 50 54 MD PHV Total 10,741 9,370	12,72 14,78 14,98 MD PPV VOLUM Year 2020 2019	26 (91%) 33 (92%) 35 (92%) 95 (92%) PM PHV E TRENI	на 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) (8%) NT PHV al Growth 13% 1%	Src NT PPV		
VOL	2018 2017 2016 el Deman Model Year UME COL MM S S	16,139 16,254 16,356 16,353 > >> d Model Model AADT JNT Date on 1/17/2022 un 1/16/2022 at 1/15/2022 bi 1/14/2022	1,576 1,620 1-5 of (AM PHV	10 10 10 66 AM PPV 60 60 60 60	54 50 54 (MD PHV Total 10,741 9,370 10,960 15,276	12,72 14,78 14,98 MD PPV VOLUM Year 2020 2019 2018	26 (91%) 33 (92%) 35 (92%) PM PHV E TRENI	на 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) (8%) NT PHV al Growth 13% -1%	Src NT PPV		
VOL	2018 2017 2016 el Deman Model Year UME COL M S S S F F	16,139 16,254 16,356 16,353 > >> d Model Model Model AADT JNT Date on 1/17/2022 un 1/16/2022 at 1/15/2022 tri 1/14/2022 bu 1/13/2022	1,576 1,620 1-5 of (10 10 10 66 60 60 60 60 60	54 50 54 MD PHV 10,741 9,370 10,960 15,376 14 777	12,72 14,78 14,98 MD PPV VOLUMI Year 2020 2019 2018 2017	26 (91%) 33 (92%) 35 (92%) PM PHV E TRENI	на 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) (8%) NT PHV al Growth 13% .1% .1% .1% 0%	Src NT PPV		
VOL	2018 2017 2016 el Deman Model Year UME COU MM S S S F T	16,139 16,254 16,356 16,353 > >> d Model Model AADT JNT Date on 1/17/2022 un 1/16/2022 ri 1/14/2022 ri 1/14/2022 hu 1/13/2022 ed 1/12/2022	1,576 1,620 1-5 of (10 10 10 56 AM PPV Int 60 60 60 60 60 60 60	54 50 54 MD PHV Total 10,741 9,370 10,960 15,376 14,777 14 301	12,72 14,78 14,98 MD PPV VOLUM Year 2020 2019 2018 2017 2016	26 (91%) 33 (92%) 95 (92%) PM PHV E TRENI	на 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) (8%) NT PHV al Growth 13% -1% -1% 0% 0%	Src NT PPV		
VOL	2018 2017 2016 el Deman Model Year UME COL M S S S F T T W	16,139 16,254 16,356 16,353 > >> d Model Model Model AADT JNT Date on 1/17/2022 at 1/15/2022 at 1/15/2022 at 1/15/2022 at 1/12/2022 bu 1/12/2022 ue 1/11/2022	1,576 1,620 1-5 of (10 10 10 66 60 60 60 60 60 60 60 60	54 50 54 (MD PHV Total 10,741 9,370 10,960 15,376 14,777 14,301 13,232	12,72 14,78 14,98 MD PPV VOLUM Year 2020 2019 2018 2017 2016 2015	26 (91%) 33 (92%) 35 (92%) PM PHV E TRENI	на 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) (8%) NT PHV al Growth 13% -1% -1% 0% 0% 0% 1%	Src NT PPV		
VOL	2018 2017 2016 el Deman Model Year UME COL M S S S S F T T W W	16,139 16,254 16,356 16,353 > >> d Model Model Model Model INT Date on 1/17/2022 un 1/16/2022 at 1/15/2022 at 1/15/2022 at 1/12/2022 d 1/12/2022 ue 1/11/2022 on 1/10/2022	1,576 1,620 1-5 of (10 10 10 66 60 60 60 60 60 60 60 60 60 60 60 60	54 50 54 MD PHV 10,741 9,370 10,960 15,376 14,777 14,301 13,232 14,050	12,72 14,78 14,98 MD PPV VOLUMI Year 2020 2019 2018 2017 2016 2015 2014	26 (91%) 33 (92%) 35 (92%) PM PHV E TRENI	на 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) (8%) NT PHV al Growth 13% .1% .1% 0% 0% 1% .1%	Src NT PPV		
VOL Trav	2018 2017 2016 el Deman Model Year UME COU MM S S S F T T WW S	16,139 16,254 16,353 > >> d Model Model AADT JNT Date on 1/17/2022 un 1/16/2022 at 1/15/2022 at 1/15/2022 at 1/12/2022 d 1/12/2022 d 1/12/2022 d 1/12/2022 d 1/12/2022 d 1/12/2022 d 1/10/2022 d 1/10/2022 d 1/10/2022	1,576 1,620 1-5 of (10 10 10 56 60 60 60 60 60 60 60 60 60 60 60 60 60	54 50 54 MD PHV Total 10,741 9,370 10,960 15,376 14,777 14,301 13,232 14,050 7,851	12,72 14,78 14,98 MD PPV VOLUM Year 2020 2019 2018 2017 2016 2015 2014 2013	26 (91%) 33 (92%) 95 (92%) PM PHV E TRENI	на 1,259 1,356 1,269 РМ РРV	(9%) (8%) (8%) (8%) NT PHV al Growth 13% -1% -1% 0% 0% 0% 1% -1% -1%	Src NT PPV		

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CALCULATION SHEET



Stephen G. Pernaw & Company, Inc.

Project:	Retail Fuel Outlet	Job Number:	2122A
Calculated By:	SP	Date:	1/25/2022
Checked By:	CA	Date:	1/25/2022
Sheet No:	1	Of:	1
Subject	Covid-19 Adjustment Fa	ctors	

NHDOT Cou	int Sta	ation 023	45001 (US1	North Hampt	on) J	uly 2021 \	/olumes (v	with Covid):				
July 2	021 A	AM Volum	nes	July 2	021	PM Volum	ies_	July 20	021 S	SAT Volur	nes	
7/26/2021	М	1,096	veh	7/26/2021	М	1, 423	veh	7/31/2021	S	1,486	veh	
7/27/2021	Т	1,157	veh	7/27/2021	Т	1,490	veh					
7/28/2021	W	1,191	veh	7/28/2021	w	1,517	veh					
7/29/2021	ΤH	1,174	veh	7/29/2021	тн	1,486	veh					
7/30/2021	F	1,138	veh	7/30/2021	F	1,577	veh					
Averag	e =	1,151	veh	Average	e =	1,499	veh	Average	e =	1,486	veh	
B. NHDOT Cou	int Sta	ation 0234	45001 (US1	North Hampt	on) J	uly 2019 \	/olumes (v	without Covid):				
July 2	019 A	AM Volum	nes	July 2	019	PM Volum	ies	July 20	019 5	AT Volur	nes	
7/22/2019	М	1,219	veh	7/22/2019	М	1,494	veh	7/27/2019	s	1,485	veh	
7/23/2019	Т	1,258	veh	7/23/2019	Т	1,539	veh					
7/24/2019	W	1,363	veh	7/24/2019	w	1,582	veh					
7/25/2019	TH	1,310	veh	7/25/2019	тн	1,545	veh					
7/26/2019	F	1,274	veh	7/26/2019	F	1,663	veh					
Average	e =	1,285	veh	Average	e =	1,565	veh	Average	e =	1,485	veh	
ctor 2019 volu	mest	to 2021 u	sing a two p	percent annua	grow	th rate:						
ctor 2019 volu Averag	mes f	to 2021 u 1,336	sing a two p veh	percent annual Average	l grov e =	<u>/th rate:</u> 1,627	veh	Average	9 =	1,544	veh	
ctor 2019 volu Averag	<u>mes 1</u> e =	<u>to 2021 u</u> 1,336	sing a two p	percent annual Averag	l grov	<u>/th rate:</u> 1,627	veh	Average) =	1,544	veh	
Averag	e =	to 2021 u 1,336	sing a two p	bercent annual Averagi	grow	<u>/th rate:</u> 1,627	veh	Average) =	1,544	veh	
ctor 2019 volu Averag	mes f	to 2021 u 1,336 stment Fa	veh	Averag	e =	<u>vth rate:</u> 1,627	veh	Average	9 =	1,544	veh	
Average	e =	to 2021 u 1,336 stment Fa	veh	Averag	e =	<u>th rate:</u> 1,627	veh	Average) =	1,544	veh	
Average	<u>mes 1</u> e = Adjus = 1,33	to 2021 u 1,336 stment Fa 36 / 1,115	veh	Averag	e =	<u>th rate:</u> 1,627	veh	Average	9 =	1,544	veh	
Average Alculate Covid AM Factor = PM Factor =	<u>mes 1</u> e = Adjus = 1,33 = 1,62	to 2021 u 1,336 stment Fa 36 / 1,115 27 / 1,499	veh ictors = 1.16 = 1.09 6 = 1.04	Average	e =	<u>th rate:</u> 1,627	veh	Average	e =	1,544	veh	
Average Alculate Covid AM Factor = PM Factor = SAT Factor	<u>mes 1</u> e = Adjus = 1,33 = 1,62	to 2021 u 1,336 stment Fa 36 / 1,115 27 / 1,499 544 / 1,48	veh veh = 1.16 = 1.09 6 = 1.04	Averag	1 grow	<u>th rate:</u> 1,627	veh	Average	3=	1,544	veh	
Average Average Alculate Covid AM Factor = PM Factor = SAT Factor	<u>mes 1</u> e = Adjus = 1,33 = 1,62	to 2021 u 1,336 stment Fa 36 / 1,115 27 / 1,499 544 / 1,48	veh ictors = 1.16 = 1.09 6 = 1.04	Average	9 =	<u>th rate:</u> 1,627	veh	Average) =	1,544	veh	
Average Alculate Covid AM Factor = PM Factor = SAT Factor	<u>mes 1</u> e = = 1,33 = 1,62	to 2021 u 1,336 stment Fa 36 / 1,115 27 / 1,499 544 / 1,48	veh veh = 1.16 = 1.09 6 = 1.04	Average	9 =	<u>th rate:</u> 1,627	veh	Average)=	1,544	veh	
Average Average Alculate Covid AM Factor = PM Factor = SAT Factor	<u>mes 1</u> e = = 1,33 = 1,62 = 1,62	to 2021 u 1,336 stment Fa 36 / 1,115 27 / 1,499 544 / 1,48	veh ictors = 1.16 = 1.09 6 = 1.04	Average	9 =	<u>th rate:</u> 1,627	veh	Average) =	1,544	veh	
Average Alculate Covid AM Factor = PM Factor = SAT Factor	<u>mes 1</u> e = Adjus = 1,33 = 1,62 = 1,52	to 2021 u 1,336 stment Fa 36 / 1,115 27 / 1,499 544 / 1,48	veh veh = 1.16 = 1.09 6 = 1.04	ercent annual Average	e =	<u>th rate:</u> 1,627	veh	Average	3=	1,544	veh	
Average Average Alculate Covid AM Factor = PM Factor = SAT Factor	<u>mes 1</u> e = = 1,33 = 1,62 = 1,62	to 2021 u 1,336 stment Fa 36 / 1,115 27 / 1,499 544 / 1,48	xeh xeh actors = 1.16 = 1.09 6 = 1.04	Percent annual Average	9 =	<u>th rate:</u> 1,627	veh	Average) =	1,544	veh	
Average Average Alculate Covid AM Factor = PM Factor = SAT Factor	<u>mes 1</u> e = Adjus = 1,33 = 1,62 = 1,5	to 2021 u 1,336 stment Fa 36 / 1,115 27 / 1,499 544 / 1,48	sing a two p veh ictors i = 1.16 i = 1.09 6 = 1.04	percent annual Average	9 =	<u>th rate:</u> 1,627	veh	Average) =	1,544	veh	
Average Average alculate Covid AM Factor = PM Factor = SAT Factor	<u>mes 1</u> e = = 1,33 = 1,62 : = 1,62	to 2021 u 1,336 stment Fa 36 / 1,115 27 / 1,499 544 / 1,48	veh inctors = 1.16 = 1.09 6 = 1.04	percent annual Average	9 =	<u>th rate:</u> 1,627	veh	Average) =	1,544	veh	





Transportation Data Management System



Excel Version

Weekly Volume R	Neekly Volume Report										
Location ID:	02345001	Туре:	SPOT								
Located On:	Lafayette Rd	:									
Direction:	2-WAY										
Community:	NORTH HAMPTON	Period:	Mon 7/22/2019 - Sun 7/28/2019								
AADT:	16139										

	Start Time	Mon	Tue	Wed	Thu	Fri	Sat	Sun	Avg	Graph
	12:00 AM	63	58	56	72	83	114	104	79	0.4%
	1:00 AM	37	30	57	34	62	53	59	47	0.3%
	2:00 AM	41	21	34	36	42	38	31	35	0.2%
	3:00 AM	31	22	52	49	50	27	29	37	0.2%
	4:00 AM	105	98	85	89	76	59	26	77	0.4%
1	5:00 AM	265	265	287	288	289	139	98	233	1.2%
	6:00 AM	628	597	681	664	615	325	228	534	2.9%
	7:00 AM	1097	1095	1165	1114	1104	611	403	941	5.0%
1	8:00 AM	1219	1258	1363	1310	1274	883	696	1,143	6.1%
1	9:00 AM	1130	1155	1232	1299	1340	1163	882	1,172	6.3%
	10:00 AM	1209	1192	1189	1345	1404	1408	1152	1,271	6.8%
	11:00 AM	1242	1342	1257	1305	1410	1485	1179	1,317	7.0%
	12:00 PM	1431	1374	1337	1418	1539	1498	1323	1,417	7.6%
1	1:00 PM	1366	1366	1226	1353	1481	1551	1313	1,379	7.4%
	2:00 PM	1263	1468	1390	1440	1592	1499	1352	1,429	7.6%
1	3:00 PM	1360	1433	1381	1531	1603	1449	1362	1,446	7.7%
1	4:00 PM	1494	1539	1582	1545	1663	1266	1366	1,494	8.0%
_	5:00 PM	1484	1498	1513	1540	1606	1128	1347	1,445	7.7%
Ì	6:00 PM	1011	1046	1105	1122	1214	1021	1322	1,120	6.0%
Ì	7:00 PM	541	728	774	815	857	795	948	780	4.2%
Ì	8:00 PM	429	514	576	608	703	681	653	595	3.2%
Ì	9:00 PM	310	348	394	408	476	465	359	394	2.1%
1	10:00 PM	146	211	210	238	241	323	209	225	1.2%
I	11:00 PM	94	112	127	123	171	152	80	123	0.7%
Ī	Total	17,996	18,770	19,073	19,746	20,895	18,133	16,521		
[24hr Total	17996	18770	19073	19746	20895	18133	16521	18,733	
	AM Pk Hr	11:00	11:00	8:00	10:00	11:00	11:00	11:00		
	AM Peak	1242	1342	1363	1345	1410	1485	1179	1,338	
	PM Pk Hr	4:00	4:00	4:00	4:00	4:00	1:00	4:00		
	PM Peak	1494	1539	1582	1545	1663	1551	1366	1,534	
	% Pk Hr	8.30%	8.20%	8.29%	7.82%	7.96%	8.55%	8.27%	8.20%	





Transportation Data Management System



Excel Version

Weekly Volume R	eport		
Location ID:	02345001	Type:	SPOT
Located On:	Lafayette Rd	:	
Direction:	2-WAY		
Community:	NORTH HAMPTON	Period:	Mon 7/26/2021 - Sun 8/1/2021
AADT:			

[Start Time	Mon	Tue	Wed	Thu	Fri	Sat	Sun	Avg	Graph
I	12:00 AM	36	61	50	62	57	85	89	63	0.4%
İ	1:00 AM	19	32	30	28	27	51	53	34	0.2%
	2:00 AM	21	21	26	18	21	32	31	24	0.1%
	3:00 AM	32	37	36	41	42	34	24	35	0.2%
	4:00 AM	83	89	87	97	84	57	36	76	0.4%
I	5:00 AM	259	271	238	221	247	123	94	208	1.2%
	6:00 AM	597	610	595	594	531	251	166	478	2.7%
1	7:00 AM	999	1004	1071	1033	964	509	354	848	4.8%
1	8:00 AM	1096	(1157)	(1191)	1174	1138	820	551	1,018	5.8%
1	9:00 AM	1064	1136	1111	1093	1140	1073	785	1,057	6.0%
	10:00 AM	1164	1215	1183	1233	1294	1324	1030	1,206	6.9%
	11:00 AM	1258	1290	1302	1335	1338 (1486	1188	1,314	7.5%
	12:00 PM	1341	1331	1317	1424	1499	1585	1291	1,398	8.0%
	1:00 PM	1249	1316	1328	1341	1424	1600	1228	1,355	7.7%
	2:00 PM	1352	1355	1386	1404	1473	1544	1343	1,408	8.0%
1	3:00 PM	1406	1458	1478	1486	(1577)	1461	1322	1,455	8.3%
	4:00 PM	1423	(1490)	1508	1452	1462	1349	1348	1,433	8.2%
	5:00 PM	1350	1476	1517	1414	1343	1058	1250	1,344	7.7%
1	6:00 PM	939	960	996	922	979	884	1006	955	5.4%
	7:00 PM	643	555	754	562	792	755	695	679	3.9%
	8:00 PM	548	418	592	417	574	565	485	514	2.9%
	9:00 PM	326	287	365	287	401	404	256	332	1.9%
	10:00 PM	187	159	204	180	244	250	169	199	1.1%
	11:00 PM	94	81	97	105	142	141	74	105	0.6%
	Total	17,486	17,809	18,462	17,923	18,793	17,441	14,868		
	24hr Total	17486	17809	18462	17923	18793	17441	14868	17,540	
	AM Pk Hr	11:00	11:00	11:00	11:00	11:00	11:00	11:00		
	AM Peak	1258	1290	1302	1335	1338	1486	1188	1,314	
	PM Pk Hr	4:00	4:00	5:00	3:00	3:00	1:00	4:00		
	PM Peak	1423	1490	1517	1486	1577	1600	1348	1,492	
	% Pk Hr	8.14%	8.37%	8.22%	8.29%	8.39%	9.17%	9.07%	8.52%	

Appendix E

Site Generated Traffic Volumes / Trip Distribution











Pernaw & Company, Inc.

2122A

Appendix

Traffic Impact and Site Access Study, Proposed Common Man Roadside, Portsmouth, New Hampshire

Site Generated Traffic Volumes - Burger King-Primary Trips





C Help C Stepher Pernaw B Sign out

🔏 Graph Look Up





ITETripGen Web-based App

C Help O Stephen Pernaw G Sign out






C Hep O Stephen Pernaw G Sign out C**(**)

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C Help O Stephen Pernaw

the free	Data Plot and Equation	- Small Sample Size	DATA STATISTICS
SOURCE:			Land Use: Convenience Store/Gas Station - GFA (5 5-10k) (945) Click for Description and Data Prote
Generation Manual, 11th Ed 🔶	5,000		Independent Variable: Vehicle Fueling Positions
CH BY LAND USE CODE:			Time Period: Weekday
USE GROUP:	4,000 X		Setting:Location: General Urban/Suburban
0-999) Services			Тпр Туре: Vehicle
USE : - Convenience Store/Gas Station	3,000		Number of Studies:
USE SUBCATEGORY:	φήT =		Avg. Num. of Vehicle Fueling Positions
A (5 5-10k)	F 2,000		Average Rate
NG/LOCATION:			345 75
teral Urban/Suburban	000		Range of Rates 345 75 - 345 75
ENDENT VARIABLE (IV):			Standard Deviation
icle Fueling Positions			VERY AVAILABLE VERY
JERIOD:	00 5 10 15 20	25 30	Fifted Curve Equation: Not Given
skday	X = Number of Vehicle Fueling Positions		R2.
YPE; (cle	Resat Zoom Restore		Directional Distribution:
A IV VALUE TO CALCULATE TRIPS:	× Study Site	Average Rate	Calculated Trin Ends:

ITETripGen Web-based App		•	🖉 Help 🔂 Stephen Pernaw 😨 Sign out
👬 Graph Look Up			()
Query Filter	Data Plot and Equation	Caution – Small Sample Size	DATA STATISTICS
DATA SOURCE:			Land Use: Convenience Store/Gas Station - GFA (4-5 5k) (945) Click for Discrimition and Data Plots
Trip Generation Manual, 11th Ed			Independent Variable: Vehicle Fuelting Positions
SEARCH BY LAND USE CODE:	4,000		Time Period: Saturday
LAND USE GROUP:	×		Setting/Location: General Urban/Suburban
(900-999) Services	3,000		Trip Type: Vehicle
LAND USE : 945 - Convenience Store/Gas Station	spua		Number of Studies:
LAND USE SUBCATEGORY:	The Trip 2,000		Avg. Num. of Vehicle Fueling Positions: 12
GFA (4-5 5K)			Average Rate [.] 291.67
General Urban/Suburban	1,000		Range of Rates: 291 67 - 291.67
INDEPENDENT VARIABLE (IV): Vehicle Fueling Positions			Standard Deviation
TIME PERIOD:	00 5 10 15 20	25 30	Fitted Curve Equation: Not Given
Saturday 🗸	X = Number of Vehicle Fueling Positi	Su	R ² .
TRIP TYPE: Vehicle	Reset Zoom Restore		Directional Distribution: 50% entering, 50% exiting
ENTER IV VALUE TO CALCULATE TRIPS:	X Study Site	Average Rate	Calculated Trip Ends: Average Rate: 2917 (Total), 1458 (Entry), 1459 (Exit)



TRIP DISTRIBUTION ANALYSIS

Home Destination Report - Where Workers Live Who are Employed in the Selection Area - by County Subdivisions

		Gatev	way %	Gateway	Allocation	
		US1 N	US1 S	US1 N	US1 S	
	Count					
Portsmouth city (Rockingham, NH)	4,271	0.85	0.15	3630	641	4271
Dover city (Strafford, NH)	3,058	1.00		3058	0	3058
Rochester city (Strafford, NH)	1,981	1.00		1981	0	1981
Hampton town (Rockingham, NH)	1,111		1.00	0	1111	1111
Somersworth city (Strafford, NH)	1,105	1.00		1105	0	1105
Exeter town (Rockingham, NH)	867		1.00	0	867	867
Newmarket town (Rockingham, NH)	820		1.00	0	820	820
Stratham town (Rockingham, NH)	744		1.00	0	744	744
Kittery town (York, ME)	696	1.00		696	0	696
Manchester city (Hillsborough, NH)	667		1.00	0	667	667
	15320			10470	4850	15320
				68.3%	31.7%	100%
				70	30	100

Appendix F

Capacity and Level of Service Calculations – Unsignalized

Intersection													
Int Delay, s/veh	0.1												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations		/			A	Ţ	1	f,	-	۲	_ 1	Ţ	-
Traffic Vol, veh/h	0	- 0	- 0	2	0	7	1	800	-0.	1	675	1	
Future Vol, veh/h	0	0	0	2	0	7	1	800	0	1	675	1	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	-	-	-	0	50	-	-	625	-	100	
Veh in Median Storage,	# -	0	-	-	0	_	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	97	97	97	
Heavy Vehicles, %	0	0	0	0	0	0	0	4	- 0	0	5	- 0	
Mvmt Flow	0	0	0	2	0	8	1	889	0	1	696	1	

Major/Minor			Minor1			Major1		N	Major2			
Conflicting Flow All			1590	1590	889	697	0	0	889	0	0	
Stage 1			891	891	-	-	-	-	-	-	-	
Stage 2			699	699	-	-	-	-	-	-	-	
Critical Hdwy			6.4	6.5	6.2	4.1	-	-	4.1	-	-	
Critical Hdwy Stg 1			5.4	5.5	-	-	-	-	_	-	-	
Critical Hdwy Stg 2			5.4	5.5	-	-	-	-	-	-	-	
Follow-up Hdwy			3.5	4	3.3	2.2	-	-	2.2	-	-	
Pot Cap-1 Maneuver			120	109	345	909	-	-	771	-	-	
Stage 1			404	363	-	-	-	. .	-	-	-	
Stage 2			497	445	-	-	-		-	-	-	
Platoon blocked, %							-	-		-	-	
Mov Cap-1 Maneuver			120	0	345	909	-	-	771	-	-	
Mov Cap-2 Maneuver			120	0	-	-	-	-	-	-	-	
Stage 1			404	0	-	-	-	-	-	-	-	
Stage 2			497	0	-	-	-	-	-	-	-	
Approach			WB			NB			SB			
HCM Control Delay, s			20.1			0			0			
HCM LOS			С									
Minor Lane/Major Mvmt	NBL	NBT	NBRV	VBLn1V	VBLn2	SBL	SBT	SBR				
Capacity (veh/h)	909	-	-	120	345	771	-	-				
HCM Lane V/C Ratio	0.001	-	-	0.019	0.023	0.001	-	-				
HCM Control Delay (s)	9	-	-	35.6	15.7	9.7	-	-				
HCM Lane LOS	А	-	-	Е	С	А	-	-				
HCM 95th %tile Q(veh)	0	-	-	0.1	0.1	0	-	-				

Intersection													
Int Delay, s/veh	0.1												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations		/	/		्स	1	্ শ	ţ,	/	٦.	> †	1	1
Traffic Vol, veh/h	0	0	0	2	0	- 8/	1	966	/ O-	1	814	1	
Future Vol, veh/h	0	0	0	2	0	8	1	966	0	1	814	1	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	-	-	-	0	50	-	-	625	-	100	
Veh in Median Storage,	, # -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	97	97	97	
Heavy Vehicles, %	0	0	0	0	0	0	0	4	0	0	5	0	
Mvmt Flow	0	0	0	2	0	9	1	1073	0	1	839	1	

Major/Minor		ſ	Minor1			Major1		ľ	Major2				
Conflicting Flow All			1917	1917	1073	840	0	0	1073	0	0	 	
Stage 1			1075	1075	-	-	-	-	-	-	-		
Stage 2			842	842	-	-	-	-	-	-, :	- 1		
Critical Hdwy			6.4	6.5	6.2	4.1	-	-	4.1	-	-		
Critical Hdwy Stg 1			5.4	5.5	-	-	-	-	-	-	-		
Critical Hdwy Stg 2			5.4	5.5	-	-	-	-	-	-	-		
Follow-up Hdwy			3.5	4	3.3	2.2	-	-	2.2	-	-		
Pot Cap-1 Maneuver			75	68	270	804	-	-	657	-	-		
Stage 1			331	298	-	-	-	-	-	-	-		
Stage 2			426	383	-	2	-	-	-	-	-		
Platoon blocked, %							-	-		-	-		
Mov Cap-1 Maneuver			75	0	270	804	-	-	657	-	-		
Mov Cap-2 Maneuver			75	0	-	-	-	-	-	-	-		
Stage 1			331	0	-	-	-	-	-	-	-		
Stage 2			425	0	-	-	-	-	-	-	-		
Approach			WB			NB			SB				
HCM Control Delay, s			25.9			0			0				
HCM LOS			D										
Minor Lane/Major Mvmt	NBL	NBT	NBRW	/BLn1V	VBLn2	SBL	SBT	SBR					
Capacity (veh/h)	804	-	-	75	270	657	-	-					2
HCM Lane V/C Ratio	0.001	-	-	0.03	0.033	0.002	-	-					
HCM Control Delay (s)	9.5	-	-	54.5	18.8	10.5	-	-					
HCM Lane LOS	А	-	-	F	С	В	-	-					
HCM 95th %tile Q(veh)	0	-	-	0.1	0.1	0	-	-					

Stephen G. Pernaw & Company, Inc.

HCM 6th TWSC <u>1: US1 & Water Country/North Site Driveway</u>

Intersection														
Int Delay, s/veh	7													
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR		
Lane Configurations Traffic Vol, veh/h	0	∕ ₀	 0 	65	्र ी 0	93	<u>ار م</u>	₽ 905	0	۲ ٥	↑ 841		/	
Future Vol, veh/h	0	0	0	65	0	93	1	905	0	0	841	1		
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0		
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free		
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None		
Storage Length	-	-	-	-	-	0	50	-	-	625	-	100		
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-		
Grade, %	-	0	-	-	0	-	0-	0	-	-	0	-		
Peak Hour Factor	90	90	90	90	90	90	90	90	90	97	97	97		
Heavy Vehicles, %	0	0	0	0	0	0	0	4	0	0	5	0		
Mvmt Flow	0	0	0	72	0	103	1	1006	0	0	867	1		

Major/Minor		ſ	Minor1		Ν	/lajor1			Major2			
Conflicting Flow All			1876	1876	1006	868	0	0	1006	0	0	
Stage 1			1008	1008	-	-	-	-	-	-	-	
Stage 2			868	868	-	-	-	-	-	-	-	
Critical Hdwy			6.4	6.5	6.2	4.1	-	-	4.1	-	-	
Critical Hdwy Stg 1			5.4	5.5		-	-	-	-	-	-	
Critical Hdwy Stg 2			5.4	5.5	С -	-	-	-	-	-	-	
Follow-up Hdwy			3.5	4	3.3	2.2	-	-	2.2	-	-	
Pot Cap-1 Maneuver			80	72	295	785		-	697	-	-	
Stage 1			356	321	-	-	-	-	-	-	-	
Stage 2			414	372	-	-	-	-	-	-	-	
Platoon blocked, %							-	-		-	-	
Mov Cap-1 Maneuver			80	0	295	785	-	-	697	-	-	
Mov Cap-2 Maneuver			80	0	-	-	-	-	-	-	-	
Stage 1			356	0	-	_	-	-	-	-	-	
Stage 2			414	0	-	-	-	-	-	-	-	
Approach			WB			NB			SB			
HCM Control Delay, s			81.8			0		·····	0			
HCM LOS			F						•			
Minor Lane/Major Mvmt	NBL	NBT	NBRV	VBLn1V	VBLn2	SBL	SBT	SBR				
Capacity (veh/h)	785	-	-	80	295	697	-	-				
HCM Lane V/C Ratio	0.001	-	-	0.903	0.35	-	-	-				
HCM Control Delay (s)	9.0			165 1	23.6	0						

HCM Lane V/C Ratio	0.001	-	-	0.903	0.35	-	-	-
HCM Control Delay (s)	9.6	-	-	165.1	23.6	0	-	-
HCM Lane LOS	А	-	-	F	С	А	-	-
HCM 95th %tile Q(veh)	0	-	-	4.7	1.5	0	-	-

Intersection													
Int Delay, s/veh	0.2				·								
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations				_	्रम	Ţ	1	f)		্ৰী	1	1	/
Traffic Vol, veh/h	0	<u> </u>	0	2	0	8	-1-	1086	0.	1	899	1*	
Future Vol, veh/h	0	0	0	2	0	8	1	1086	0	1	899	1	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	-	-	-	0	50	-	-	625	-	100	
Veh in Median Storage	, # -	0	-	-	0	2	_	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	97	97	97	
Heavy Vehicles, %	0	0	0	0	0	0	0	4	0	0	5	0	
Mvmt Flow	0	0	0	2	0	9	1	1207	0	1	927	1	

Major/Minor			Vinor1			Major1		1	Major2				
Conflicting Flow All			2139	2139	1207	928	0	0	1207	0	0		
Stage 1			1209	1209	-	-	-	-	-	-	-		
Stage 2			930	930	-	-	-	-	-	-	-		
Critical Hdwy			6.4	6.5	6.2	4.1	-	-	4.1	-	-		
Critical Hdwy Stg 1			5.4	5.5	-	-	-	-	-	-	-		
Critical Hdwy Stg 2			5.4	5.5	-	-	-	-	-	-	-		
Follow-up Hdwy			3.5	4	3.3	2.2	-	-	2.2	-	-		
Pot Cap-1 Maneuver			55	50	226	745	-	-	585	-	-		
Stage 1			285	258	-	-	-	-	-	-	-		
Stage 2			387	349	-	-	-	-	-	-	-		
Platoon blocked, %							-	-		-	-		
Mov Cap-1 Maneuver			55	0	226	745	-	-	585	-	-		
Mov Cap-2 Maneuver			55	0	-	-	-	-	-	-	-		
Stage 1			285	0	-	-	-	-	-	-	-		
Stage 2			386	0	-	-	-	-	-	-	-		
Approach			WB			NB			SB				
HCM Control Delay, s			31.9			0			0			<u></u>	
HCM LOS			D			-			·				
		NDT											
Minor Lane/Major Mvmt	NBL	NBI	NBRV	VBLn1V	VBLn2	SBL	SBI	SBR					 <u></u>
Capacity (veh/h)	745	-	-	55	226	585	-	-					
HCM Lane V/C Ratio	0.001	-	-	0.04	0.039	0.002	-	-					
HCM Control Delay (s)	9.8	-	-	73.2	21.6	11.2	-	-					
HCM Lane LOS	A	-	-	F	C	В	-	-					
HCM 95th %tile Q(veh)	0	-	-	0.1	0.1	0	-	-					

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Intersection													
Int Delay, s/veh	10.8												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations		1	1	1	्री	7	٦	4	1	্র	1	7	1
Traffic Vol, veh/h	0	0	0	65	0	9 3	1	1007	0	0	926		
Future Vol, veh/h	0	0	0	65	0	93	1	1007	0	0	926	1	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	-	-		0	50	-	-	625	-	100	
Veh in Median Storage	,# -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	97	97	97	
Heavy Vehicles, %	0	0	0	0	0	0	0	4	0	0	5	0	
Mvmt Flow	0	0	0	72	0	103	1	1119	0	0	955	1	
Major/Minor			I	Minor1		ſ	Major1		P	Major2			
Conflicting Flow All				2077	2077	1119	956	0	0	1119	0	0	
Stage 1				1121	1121	-	-	-	-	-	-	-	
Stage 2				956	956	-	-	-	-	-	-	-	
Critical Hdwy				6.4	6.5	6.2	4.1	-	-	4.1	-	-	
Critical Hdwy Stg 1				5.4	5.5	-	-	-	-	-	-	-	
Critical Hdwy Stg 2				5.4	5.5	-	-	-	-	-	-	-	
Follow-up Hdwy				3.5	4	3.3	2.2	-	-	2.2	-	-	
Pot Cap-1 Maneuver				~ 60	54	254	727		-	632	-	-	
Stage 1				314	284	-	-	-	-	-	-	-	
Stage 2				376	339	-	-	-	-	-	-	-	
Platoon blocked, %								-	-		-	-	
Mov Cap-1 Maneuver				~ 60	0	254	727	-	-	632	-	-	
Mov Cap-2 Maneuver				~ 60	0	-	-	5 4 0	-	-	-	-	
Stage 1				314	0	-	-	-	-	-	-	-	
Stage 2				376	0	-	-	-	-	-	-	-	

Approach	WB	NB	SB	
HCM Control Delay, s	138.9	0	0	
HCM LOS	F			

Minor Lane/Major Mvmt	NBL	NBT	NBRV	VBLn1\	WBLn2	SBL	SBT	SBR
Capacity (veh/h)	727	-	-	60	254	632	-	-
HCM Lane V/C Ratio	0.002	-	-	1.204	0.407	-	-	-
HCM Control Delay (s)	10	-	-	296.8	28.6	0	-	-
HCM Lane LOS	А	-	-	F	D	А	-	-
HCM 95th %tile Q(veh)	0	-	-	6	1.9	0	-	-
Notes								

~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined

*: All major volume in platoon

HCM 6th TWSC 1: US1 & Water Country/North Site Driveway

Int Delay, s/veh 0.6 Movement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR Lane Configurations Traffic Vol. veh/h 0 0 0 10 0 20 1 982 1 3 1043 0
Movement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR Lane Configurations 0 0 0 0 0 20 1 982 1 3 1043 0
Lane Configurations Traffic Vol. veh/h 0 0 0 10 0 20 1 982 1 3 1043 0
Traffic Vol. veh/h $0 - 0 - 10 - 0 - 20 - 1 - 3 - 1043 - 0$
Future Vol, veh/h 0 0 0 10 0 20 1 982 1 3 1043 0
Conflicting Peds, #/hr 0 0 0 0 0 0 0 0 0 0 0 0 0
Sign Control Stop Stop Stop Stop Stop Stop Free Free Free Free Free Free
RT Channelized None None None None
Storage Length 0 50 625 - 100
Veh in Median Storage, # - 0 0 0 0 -
Grade, % - 0 0 0 0 -
Peak Hour Factor 90 90 90 90 90 90 98 98 98 93 93 93
Heavy Vehicles, % 0 0 0 0 0 0 0 0 4 0 0 2 0
Mvmt Flow 0 0 0 11 0 22 1 1002 1 3 1122 0

Major/Minor			Minor1			Major1			Major2				
Conflicting Flow All			2133	2133	1003	1122	0	0	1003	0	0		
Stage 1			1005	1005	-	-	-	-	-	-	-		
Stage 2			1128	1128	-	-	-	-	-	-	-		
Critical Hdwy			6.4	6.5	6.2	4.1	-	-	4.1	-	-		
Critical Hdwy Stg 1			5.4	5.5	-	-	-	-	-	-	-		
Critical Hdwy Stg 2			5.4	5.5	-	-	-	-	-	-	-		
Follow-up Hdwy			3.5	4	3.3	2.2	-	-	2.2	-	-		
Pot Cap-1 Maneuver			55	50	297	630	-	-	698	-	-		
Stage 1			357	322	-	-	-	-	-	-	-		
Stage 2			312	282	-		-	-	-	-	-		
Platoon blocked, %							-	-		-	-		
Mov Cap-1 Maneuver			55	0	297	630	-	-	698	-	-		
Mov Cap-2 Maneuver			55	0	-	-	-	-	-	-	-		
Stage 1			356	0	-	-	-	-	-	-	-		
Stage 2			311	0	-	-		-	-	-	-		
Approach	· · · ·		WB			NB			SB				
HCM Control Delay, s			40.8			0			0				
HCM LOS			Е										
Minor Lane/Major Mvmt	NBL	NBT	NBRV	VBLn1V	VBLn2	SBL	SBT	SBR					
Capacity (veh/h)	630	-	-	55	297	698	-	-					
HCM Lane V/C Ratio	0.002		-	0.202	0.075	0.005	-	-					
HCM Control Delay (s)	10.7	-	-	86.3	18.1	10.2	-	-					
HCM Lane LOS	В	-	-	F	С	В	-	-					
HCM 95th %tile Q(veh)	0	¥	-	0.7	0.2	0	-	-					

Intersection													
Int Delay, s/veh	1												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations			/	-	्रस	1	۲	ţ,	_	ň	1	ť.	/
Traffic Vol, veh/h	0	0	0	11	V Ö	22	1	1114	1	3	1183	0	harden and a second sec
Future Vol, veh/h	0	0	0	11	0	22	1	1114	1	3	1183	0	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	-	-	-	0	50	-	-	625	-	100	
Veh in Median Storage,	# -	0	: .	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	98	98	98	93	93	93	
Heavy Vehicles, %	0	0	0	0	0	0	0	4	0	0	2	0	
Mvmt Flow	0	0	0	12	0	24	1	1137	1	3	1272	0	
Major/Minor			,	linort			Voier1			MalarQ			

iviajor/iviinor			Minor1			Major1			Major2				
Conflicting Flow All		-	2418	2418	1138	1272	0	0	1138	0	0	 	
Stage 1			1140	1140	-	-	-	-	-	-	-		
Stage 2			1278	1278	-	-	-	-	-	-	-		
Critical Hdwy			6.4	6.5	6.2	4.1	-	-	4.1	-	-		
Critical Hdwy Stg 1			5.4	5.5	-	-	-	-	-	-	-		
Critical Hdwy Stg 2			5.4	5.5	-	-	-	-	5	-	-		
Follow-up Hdwy			3.5	4	3.3	2.2	-	-	2.2	-	-		
Pot Cap-1 Maneuver			36	33	248	553	-	-	621	-	-		
Stage 1			308	278	-	-	-	-	-	-	-		
Stage 2			264	239	-	-	-		-	-	-		
Platoon blocked, %							-	-		-	-		
Mov Cap-1 Maneuver			36	0	248	553	-	-	621	-	-		
Mov Cap-2 Maneuver			36	0	-	-	-	-	-	-	-		
Stage 1			307	0	-	-	-	_	-	-	-		
Stage 2			263	0	-	-	-	-	-	2	-		
Approach			WB			NB			SB				
HCM Control Delay, s			64			0			0				
			Г										
Minor Lane/Major Mvmt	NBL	NBT	NBRV	VBLn1V	VBLn2	SBL	SBT	SBR					
Capacity (veh/h)	553	-	-	36	248	621	-	-					
HCM Lane V/C Ratio	0.002	-	-	0.34	0.099	0.005	-	-					
HCM Control Delay (s)	11.5	-	-	149.7	21.1	10.8	-	-					
HCM Lane LOS	В	-	-	F	С	В	-	-					
HCM 95th %tile Q(veh)	0	-	-	1.1	0.3	0	-	-					

Intersection														
Int Delay, s/veh	17.5													
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR		
Lane Configurations		/	A Martin		्र स	1	শ	્ર 🖡		1	1	1		
Traffic Vol, veh/h	0	× 0	0	62	Ö	73	1	1076	0	0	1203	0		
Future Vol, veh/h	0	0	0	62	0	73	1	1076	0	0	1203	0		
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0		
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free		
RT Channelized	-		None		-	None	-	-	None	-	-	None		
Storage Length	-	-	-		-	0	50	-	-	625	-	100		
Veh in Median Storage.	# -	0	-	-	0	-	-	0	-	-	0	-		
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-		
Peak Hour Factor	90	90	90	90	90	90	98	98	98	93	93	93		
Heavy Vehicles, %	0	0	0	0	0	0	0	4	0	0	2	0		
Mvmt Flow	0	0	Ő	69	0	81	1	1098	Ō	Ō	1294	0		
Major/Minor			r	Minor1			Major1		ſ	/lajor2				
Conflicting Flow All				2394	2394	1098	1294	0	0	1098	0	0		
Stage 1				1100	1100	-	-		-	-	-	-		
Stage 2				1294	1294	-	-	-	-	-	-	-		
Critical Hdwv				6.4	6.5	6.2	4.1	-	_	4.1	_	-		
Critical Hdwy Stg 1				5.4	5.5	_	-	-	-	-	-	-		
Critical Hdwy Stg 2				5.4	5.5	-	-	-	-	-	-	-		
Follow-up Hdwy				3.5	4	3.3	2.2	-	-	2.2	-	-		
Pot Cap-1 Maneuver				~ 38	34	261	542	-	-	643	_	-		
Stage 1				322	290	-	-	-	_	-	-	-		
Stage 2				260	235	-	-	-	-	-	-	-		
Platoon blocked, %								-	-		-	-		
Mov Cap-1 Maneuver				~ 38	0	261	542	-	-	643	-	-		
Mov Cap-2 Maneuver				~ 38	0			-	_	-	-	-		
Stage 1				321	0	-	-	-	_	-	-	_		
Stage 2				260	0	-	-	-	-	-	. . -	-		
Approach				WB			NB			SB				
HCM Control Delay, s				296.1			0			0				
HCM LOS				F										
Minor Long/Maior Marint			NDT					ODT	000					
		INDL EAO	IND I	NDRV			SBL	201	SBK				 	
Capacity (ven/n)		0.000	-	-	38	261	643	-	-					
HOM Control Delaw (=)		0.002	-	-	1.813	0.311	-		-					
HCM Long L CC		11.7	-	-\$	015.4	24.9	0	-	-					
		В	-	-		U C	A	-	-					
HCIM 95th %tile Q(veh)		0	-	-	7.4	1.3	0	-	-					

Notes

~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

HCM 6th TWSC 1: US1 & Water Country/North Site Driveway

Intersection														
Int Delay, s/veh	1.3											·		
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR		
Lane Configurations		/			/ स	1		1		21	>↑	1	/	
Traffic Vol, veh/h	0	/ 0	- 0	11	0	22	11	1231	1	3	1307	0	P	
Future Vol, veh/h	0	0	0	11	0	22	1	1231	1	3	1307	0		
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0		
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free		
RT Channelized	-		None		-	None	-	-	None	_	-	None		
Storage Length	_	-	-	-	-	0	50	-	-	625	-	100		
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-		
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-		
Peak Hour Factor	90	90	90	90	90	90	98	98	98	93	93	93		
Heavy Vehicles, %	0	0	0	0	0	0	0	4	0	0	2	0		
Mvmt Flow	0	0	0	12	0	24	1	1256	1	3	1405	0		
Major/Minor			٨	/inor1		ſ	Major1		1	Major2				
Conflicting Flow All				2670	2670	1257	1405	0	0	1257	0	0		
Stage 1				1259	1259	-	-	-	-	-	-	_		
Stage 2				1411	1411	-	-	-	-	-	-	-		
Critical Hdwy				6.4	6.5	6.2	4.1	-	-	4.1	-	_		
Critical Hdwy Stg 1				5.4	5.5	-	-	-	-		-	-		
Critical Hdwy Stg 2				5.4	5.5	-	-	-	-	-	-	-		
Follow-up Hdwv				3.5	4	3.3	22	-	21	22	-	-		

Critical Hdwy	6.4	6.5	6.2	4.1	-	-	4.1	-	-	
Critical Hdwy Stg 1	5.4	5.5	-	-	-	-	-	-	29 -1 9	
Critical Hdwy Stg 2	5.4	5.5	-	-	-	-10	-	-	-	
Follow-up Hdwy	3.5	4	3.3	2.2	-		2.2	-	-	
Pot Cap-1 Maneuver	25	23	211	492	-	-	560	-	-	
Stage 1	270	244	-	-	-	-	-	-	-	
Stage 2	228	206	-	-	-	-	-	-	-	
Platoon blocked, %					-	-		-	~	
Mov Cap-1 Maneuver	25	0	211	492	-	-	560	-	-	
Mov Cap-2 Maneuver	25	0	-	-	-	-	-	-	-	
Stage 1	269	0	-	-	-	-	-	-	-	
Stage 2	227	0	-	-	-	7	-	-	-	
Approach	WB			NB			SB			
HCM Control Delay, s	98.2			0			0			
HCMLOS	F						-			

Minor Lane/Major Mvmt	NBL	NBT	NBRV	VBLn1\	NBLn2	SBL	SBT	SBR
Capacity (veh/h)	492	-	-	25	211	560		-
HCM Lane V/C Ratio	0.002	-	-	0.489	0.116	0.006	-	-
HCM Control Delay (s)	12.3	-	-	245.9	24.3	11.5	-	-
HCM Lane LOS	В	-	-	F	С	В	-	2
HCM 95th %tile Q(veh)	0	-	-	1.5	[′] 0.4	0	-	-

Intersection														
Int Delay, s/veh	27.1													
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR		
Lane Configurations		-	-	1	_ ধ	1	1	4	1	্ৰ	21	1		
Traffic Vol, veh/h	0 י	0	0	62	0	- 73	1	1193	0	0	1327	0		
Future Vol, veh/h	0	0	0	62	0	73	1	1193	0	0	1327	0		
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0		
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free		
RT Channelized	-	-	None	-	-	None	_	-	None	_	-	None		
Storage Length	-	-	-	-	-	0	50		-	625	-	100		
Veh in Median Storage.	# -	0	-	_	0	-	-	0	-		0	-		
Grade. %	-	0	-	-	0	-	-	ñ	-	-	ñ	_		
Peak Hour Factor	90	90	90	90	90	90	98	98	98	93	93	03		
Heavy Vehicles %	0	0	0	0	0	0	0	4	0	0	2	0		
Mumt Flow	n N	0	ň	60	0	81 81	1	1017	0	0	1407	0		
	U	U	U	00	0	01	I	1217	U	U	1427	0		
Maior/Minor			I	Minor1		I	Maior1		Ν	Aaior2				
Conflicting Flow All				2646	2646	1217	1427	0	0	1217	Ω	0	 	
Stage 1				1219	1219			-	-			-		
Stage 2				1427	1427	_	_	_	_	_	_	-		
Critical Hdwy				61	65	62	11	_	-		-	-		
Critical Hdwy Sta 1				5.4	5.5	0.2	4.1	-	-	4.1	-	-		
Critical Hdwy Stg 1				5.4	5.5	-	-	-	-	-	-	-		
				2.4	0.0	-	-	-	-		-	-		
Pot Con 1 Manauvor				3.0	4	0.0	402	-	-	Z.Z		-		
Fut Cap-1 Walleuver				~ 20	24	223	403		-	000	-	-		
				202	200	-	-	-	-	-	-	-		
Stage 2				224	203	-	-	-	-	-	-	-		
Platoon blocked, %				~ ~ ~				-	-		-	-		
Mov Cap-1 Maneuver				~ 26	0	223	483	-	-	580	-	-		
Mov Cap-2 Maneuver				~ 26	0	-	-	-	-	-	-	-		
Stage 1				281	0	-	-1	-	-	-	-	-		
Stage 2				224	0	-	-	-	-	-	-	-		
Approach										60				
HCM Control Dolour			•	ENE D			IND 0			<u></u>				
HCM LOS			¢	505.3 F			U			0				
				•										
Minor Lane/Major Mvmt		NBL	NBT	NBRW	/BLn1V	VBLn2	SBL	SBT	SBR					
Capacity (veh/h)		483	-	-	26	223	580	-	-					
HCM Lane V/C Ratio		0.002	-	-	2.65	0.364	-	-	-					
HCM Control Delay (s)		12.5	-	\$1	064.9	30.1	0	-	-					
HCM Lane LOS		В	-	-	F	D	А	-	-					
HCM 95th %tile Q(veh)		0	-	-	8.4	1.6	0	-	-					

Notes

\$: Delay exceeds 300s +: Computation Not Defined ~: Volume exceeds capacity *: All major volume in platoon

Intersection												
Int Delay, s/veh	2.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		_	~		्स	1	_1	- î÷	1	্র	1	1
Traffic Vol, veh/h	0	0	0	9	6	26	120	1023	2	4	916	113
Future Vol, veh/h	0	0	0	9	6	26	120	1023	2	4	916	113
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	2	None
Storage Length	-	-	-	-	-	0	50	-	-	625	-	100
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	90	90	90	90	90	90	96	96	96	96	96	96
Heavy Vehicles, %	0	0	0	0	0	0	Õ	1	0	0	1	Ō
Mvmt Flow	0	0	0	10	7	29	125	1066	2	4	954	118

Major/Minor			Minor1			Major1			Major2				
Conflicting Flow All			2338	2397	1067	1072	0	0	1068	0	0		
Stage 1			1317	1317	-		-	-	-	-	-		
Stage 2			1021	1080	-	-	-	-	-	-	-		
Critical Hdwy			6.4	6.5	6.2	4.1	-	-	4.1	-	-		
Critical Hdwy Stg 1			5.4	5.5	-	-	-	-	-	-	-		
Critical Hdwy Stg 2			5.4	5.5	-	-	-	-	-	1-	-		
Follow-up Hdwy			3.5	4	3.3	2.2	-	-	2.2	-	-		
Pot Cap-1 Maneuver			41	34	272	658	-	-	660	-	-		
Stage 1			253	229	-	-	-	-	-	-	-		
Stage 2			351	297	-	_	-	-	-	-	-		
Platoon blocked, %							-	-		-	-		
Mov Cap-1 Maneuver			33	0	272	658	-	-	660	-	-		
Mov Cap-2 Maneuver			33	0	-	-	-	-	-	-	-		
Stage 1			205	0	-	-	-	-	-	-	-		
Stage 2			349	0	-	-	-	-	-	-	-		
Approach			WB			NB			SB				
HCM Control Delay, s			84.1			1.2			0				
HCM LOS			F										
Minor Lane/Major Mvmt	NBL	NBT	NBRV	/BLn1V	VBLn2	SBL	SBT	SBR					
Capacity (veh/h)	658	-	-	33	272	660	-	-					
HCM Lane V/C Ratio	0.19	-	-	0.505	0.106	0.006	-	-					
HCM Control Delay (s)	11.8	-	-	195.6	19.8	10.5	-	-					
HCM Lane LOS	В	-	-	F	С	В	-	-					
HCM 95th %tile Q(veh)	0.7	-	-	1.7	0.4	0	-	-					

Int Delay, s/veh 3 Movement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR Lane Configurations	Intersection													
Movement EBL EBL EBR WBL WBR NBL NBT NBR SBL SBT SBR Lane Configurations Traffic Vol, veh/h 0 0 0 9 6 27 125 1112 2 4 991 118 Future Vol, veh/h 0 0 0 9 6 27 125 1112 2 4 991 118 Conflicting Peds, #/hr 0	Int Delay, s/veh	3								1 11000				
Lane Configurations Image: Configuration of the second	Movement E	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Traffic Vol, veh/h 0 0 0 9 6 27 125 1112 2 4 991 118 Future Vol, veh/h 0 0 0 9 6 27 125 1112 2 4 991 118 Conflicting Peds, #/hr 0 <td< td=""><td>Lane Configurations</td><td></td><td>9</td><td></td><td></td><td>र्न</td><td>1</td><td>্রী</td><td>ĥ</td><td>-</td><td>ľ</td><td>†</td><td>Ţ</td><td>1</td></td<>	Lane Configurations		9			र्न	1	্রী	ĥ	-	ľ	†	Ţ	1
Future Vol, veh/h 0 0 0 9 6 27 125 1112 2 4 991 118 Conflicting Peds, #/hr 0	Traffic Vol, veh/h	0	1	0	- 91	6	27	125	1112-	2	4	991	118	1
Conflicting Peds, #/hr 0 <td>Future Vol, veh/h</td> <td>0</td> <td>0</td> <td>0</td> <td>9</td> <td>6</td> <td>27</td> <td>125</td> <td>1112</td> <td>2</td> <td>4</td> <td>991</td> <td>118</td> <td></td>	Future Vol, veh/h	0	0	0	9	6	27	125	1112	2	4	991	118	
Sign Control Stop Stop Stop Stop Stop Stop Stop Free	Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
RT Channelized - - None - - None - - None Storage Length - - - - 0 50 - - 625 - 100 Veh in Median Storage, # 0 - - 0 - - 0 - - 0 - Grade, % - 0 - - 0 - - 0 - - 0 - Peak Hour Factor 90 90 90 90 90 96 96 96 96 96 96 96 Heavy Vehicles, % 0 0 0 0 0 1 0 0 1 0	Sign Control S	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
Storage Length - - - 0 50 - - 625 - 100 Veh in Median Storage, # 0 - - 0 - - 0 - 0 - Grade, % - 0 - - 0 - - 0 - Peak Hour Factor 90 90 90 90 90 96 96 96 96 96 Heavy Vehicles, % 0 0 0 0 0 1 0 0 1 0	RT Channelized	-	_	None	-	-	None	-	-	None	-	-	None	
Veh in Median Storage, # - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - -	Storage Length	-	-	-	-	-	0	50	-	-	625	-	100	
Grade, % - 0 - - 0 - - 0 - Peak Hour Factor 90 90 90 90 90 90 96 <td>Veh in Median Storage, #</td> <td>-</td> <td>0</td> <td>-</td> <td>-</td> <td>0</td> <td>-</td> <td>-</td> <td>0</td> <td>-</td> <td>-</td> <td>0</td> <td>-</td> <td></td>	Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor 90 90 90 90 90 90 96	Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Heavy Vehicles, % 0 0 0 0 0 0 0 0 1 0 0 1 0	Peak Hour Factor	90	90	90	90	90	90	96	96	96	96	96	96	
	Heavy Vehicles, %	0	0	0	0	0	0	0	1	0	0	1	0	
Mvmt Flow 0 0 0 10 7 30 130 1158 2 4 1032 123	Mvmt Flow	0	0	0	10	7	30	130	1158	2	4	1032	123	

Major/Minor			Minor1			Major1			Major2				
Conflicting Flow All			2521	2582	1159	1155	0	0	1160	0	0		
Stage 1			1419	1419	-	-	-	-	-	-	-		
Stage 2			1102	1163	-	-	-	-	-	-	-		
Critical Hdwy			6.4	6.5	6.2	4.1	-	-	4.1	-	-		
Critical Hdwy Stg 1			5.4	5.5	-	-	-	-	-	-	-		
Critical Hdwy Stg 2			5.4	5.5	-	-	-	-	-	-	-		
Follow-up Hdwy			3.5	4	3.3	2.2	-	-	2.2	-	-		
Pot Cap-1 Maneuver			31	26	241	612	-	-	610	-	-		
Stage 1			226	205	-	-	-	-	-	-	-		
Stage 2			321	271	-	-	-	-	-	-	-		
Platoon blocked, %							-	-		-	-		
Mov Cap-1 Maneuver			24	0	241	612	-	-	610	-	-		
Mov Cap-2 Maneuver			24	0	-	-	-	-	-	-	-		
Stage 1			178	0	-	-	-	-	-	-	-		
Stage 2			319	0	-	-	-	-	-	-	-		
Approach			WB			NB			SB				
HCM Control Delay, s			126.1			1.3			0				
HCM LOS			F										
Minor Lane/Major Mvmt	NBL	NBT	NBRV	/BLn1V	VBLn2	SBL	SBT	SBR					
Capacity (veh/h)	612	-	-	24	241	610	-	-					
HCM Lane V/C Ratio	0.213	-	-	0.694	0.124	0.007	-	-					
HCM Control Delay (s)	12.5	-	-\$	313.4	22.1	10.9	-	-					
HCM Lane LOS	В	-	-	F	С	В	-1	-					
HCM 95th %tile Q(veh)	0.8	-	-	2.1	0.4	0	-	-					

HCM 6th TWSC <u>1: US1 & Water Country/North Site Driveway</u>

Intersection														
Int Delay, s/veh	33													
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR		
Lane Configurations					्र्स	1	্ৰ শ	4	1	٦	1	1	1	
Traffic Vol, veh/h	0	0	0	59	6	87	125	1063	0	Ö	1009	118		
Future Vol, veh/h	0	0	0	59	6	87	125	1063	0	0	1009	118		
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0		
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free		
RT Channelized		-	None	-	-	None	-	-	None	-	-	None		
Storage Length	-	-	-	-	-	0	50	-	-	625	-	100		
Veh in Median Storage	,# -	0	-	-	0	-	-	0	-	-	0	-		
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-		
Peak Hour Factor	90	90	90	90	90	90	96	96	96	96	96	96		
Heavy Vehicles, %	0	0	0	0	0	0	0	1	0	0	1	0		
Mvmt Flow	0	0	0	66	7	97	130	1107	0	0	1051	123		
Major/Minor			١	Minor1		1	Major1		N	Major2				
Conflicting Flow All				2480	2541	1107	1174	0	0	1107	0	0		
Stage 1				1367	1367	-	-	-	-	-	-	-		
Stage 2				1113	1174	-	-	-	-	-	-	5 -		
Critical Hdwy				6.4	6.5	6.2	4.1	-	-	4.1	-	-		
Critical Hdwy Stg 1				5.4	5.5	-	-	-	-	-	-	-		
Critical Hdwy Stg 2				5.4	5.5	-	-	_	-	-	-	-		
Follow-up Hdwy				3.5	4	3.3	2.2	-	-	2.2	-	-		
Pot Cap-1 Maneuver				~ 33	27	258	602	-	-	638	-	-		
Stage 1				239	217	-	-	-	-	-	-	-		
Stage 2				317	268		-	-	-	-	-	-		
Platoon blocked, %								-	-		-	-		
Mov Cap-1 Maneuver				~ 26	0	258	602	-	-1	638	11-	-		
Mov Cap-2 Maneuver				~ 26	0	-	-	-		-		-		
Stage 1				187	0	-	-	-	-	-	-			
Stage 2				317	0	-	220	-	-	-	-	-		
-														

Approach	WB	NB	SB	
HCM Control Delay, s	\$ 494.7	1.3	0	
HCM LOS	F			

Minor Lane/Major Mvmt	NBL	NBT	NBR	NBLn1	WBLn2	SBL	SBT	SBR	
Capacity (veh/h)	602		-	26	258	638	-	-	
HCM Lane V/C Ratio	0.216	-	-	2.778	0.375	-	-	-	
HCM Control Delay (s)	12.6	-	\$	1120.6	27.1	0	-11	-	
HCM Lane LOS	В	-	-	F	D	А	-	-	
HCM 95th %tile Q(veh)	0.8	-		8.8	1.7	0	-	-	
Notes									

~: Volume exceeds capacity \$: Delay exceeds 300s

+: Computation Not Defined

*: All major volume in platoon

HCM 6th TWSC <u>1: US1 & Water Country/North Site Driveway</u>

Intersection													
Int Delay, s/veh	4.1												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations			-		_ स	1	1	÷,	-	_ শ	1	ť	~
Traffic Vol, veh/h	0	0	0	9	6	27	125	1242	21	4	1094	118	and the second s
Future Vol, veh/h	0	0	0	9	6	27	125	1242	2	4	1094	118	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	-	-	-	0	50	-	-	625	-	100	
Veh in Median Storage	, # -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	96	96	96	96	96	96	
Heavy Vehicles, %	0	0	0	0	0	0	0	1	0	0	1	0	
Mvmt Flow	0	0	0	10	7	30	130	1294	2	4	1140	123	

Major/Minor			Minor1			Major1		ľ	Major2			
Conflicting Flow All			2765	2826	1295	1263	0	0	1296	0	0	
Stage 1			1555	1555	-	-	-	-	-	-	-	
Stage 2			1210	1271	-	÷	-	-	-	-	-	
Critical Hdwy			6.4	6.5	6.2	4.1	-	-	4.1	-	-	
Critical Hdwy Stg 1			5.4	5.5	-	-	-	-	-	-	-	
Critical Hdwy Stg 2			5.4	5.5	-	-	-	-	-	-	-	
Follow-up Hdwy			3.5	4	3.3	2.2	-	-	2.2	-	-	
Pot Cap-1 Maneuver			22	18	200	557	-	-	541	_	-	
Stage 1			194	176	1	-	-	-	-	-	-	
Stage 2			285	241	-	-	-		-	-	-	
Platoon blocked, %							-	-		-	-	
Mov Cap-1 Maneuver			17	0	200	557	-	-	541	-	-	
Mov Cap-2 Maneuver			17	0	-	-	-	-	-	-		
Stage 1			149	0	-	-	-	-	-		-	
Stage 2			283	0	-	-	-	-	2	-	-	
Approach			WB			NB			SB			
HCM Control Delay, s	•••••••••••••••••••••••••••••••••••••••		201.8			1.2			0			 ·
HCM LOS			F									
Minor Lane/Major Mvmt	NBL	NBT	NBRW	/BLn1W	VBLn2	SBL	SBT	SBR				
Capacity (veh/h)	557	-	-	17	200	541	-	-				
HCM Lane V/C Ratio	0.234	-	-	0.98	0.15	800.0	-	-				
LICM Control Delay (a)	40.4			A 540	00.0	44.77						

HCM Control Delay (s) 13.4 -- \$518 26.2 11.7 --- F D - 2.5 0.5 HCM Lane LOS В -D В --HCM 95th %tile Q(veh) 0.9 -0 --

Intersection														
Int Delay, s/veh	47.6													
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR		
Lane Configurations			1	1	र्म 🖣	1	<u>_ 1</u>	- Þ	1	1	≥ †	11		
Traffic Vol, veh/h	0	0	0	59	6	87	125	1192	0	0	1112	118		
Future Vol, veh/h	0	0	0	59	6	87	125	1192	0	0	1112	118		
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0		
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free		
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None		
Storage Length	-	-	-	-	-	0	50	-	-	625	-	100		
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-		
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-		
Peak Hour Factor	90	90	90	90	90	90	96	96	96	96	96	96		
Heavy Vehicles, %	0	0	0	0	0	0	0	1	0	0	1	0		
Mymt Flow	0	0	0	66	7	97	130	1242	0	0	1158	123		
Major/Minor			١	Minor1		Ν	/lajor1		Ν	/lajor2				
Conflicting Flow All				2722	2783	1242	1281	0	0	1242	0	0		
Stage 1				1502	1502	-	-	-	-	-	-	-		
Stage 2				1220	1281	-	-	-	-	-	-	-		
Critical Hdwy				6.4	6.5	6.2	4.1	-	-	4.1	-	-		
Critical Hdwy Stg 1				5.4	5.5	-	-	-	-	- 1	-	-		
Critical Hdwy Stg 2				5.4	5.5	-	-	-	-	-	-	-		
Follow-up Hdwy				3.5	4	3.3	2.2	-	-	2.2	-	-		
Pot Cap-1 Maneuver				~ 23	19	215	549	-	-	568	-	-		
Stage 1				206	187	-	2	-	3 - 0	-	-	-		
Stage 2				282	238	-	-	-	-		-	-		
Platoon blocked. %								-	-		-	-		
Mov Cap-1 Maneuver				~ 18	0	215	549	-	-	568	9	-		
Mov Cap-2 Maneuver				~ 18	0		-	-	-	-	-	-		
Stage 1				157	Ő	-	-	-	-	-	-	-		
Stage 2				282	Õ	-	-	-	-	-	-	-		
okago z				202	Ũ									
Approach				WB			NB			SB				
HCM Control Delay, s			\$	784.7			1.3			0				
HCM LOS				F										
Minor Lane/Major Mvmt		NBL	NBT	NBRW	/BLn1V	VBLn2	SBL	SBT	SBR					
Capacity (veh/h)		549	-	-	18	215	568	-	-				 	
HCM Lane V/C Ratio		0.237	-	-	4.012	0.45		-						
HCM Control Delay (s)		13.6	-	\$ 1	788.6	34.7	0	-	-					
HCM Lane LOS		В	-	-	F	D	А	-	-					

Notes

HCM 95th %tile Q(veh)

~: Volume exceeds capacity

0.9

9.6

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2.1

А

0

\$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

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HCM 6th TWSC 2: US1 & South Site Driveway

Intersection						
Int Delay, s/veh	0					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	×4	/	4		۲.	≜ ≜
Traffic Vol. veh/h	0	<pre>/ 0</pre>	801	12	✓ 3	674
Future Vol, veh/h	0	0	801	12	3	674
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized		None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storag	e,# 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	90	90	. 90	90	. 97	97
Heavy Vehicles, %	0	0	4	0	0	5
Mymt Flow	0	0	890	13	3	695
	-	-			2	
Major/Minor	Minor1	٨	Acier1		Major2	
	1051	007		0		
Connicting Flow All	1201	897	U	U	903	U
Stage 1	897	-	-	-	-	-
Stage 2	354	-	-	-	-	-
	6.6	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.8	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	179	341	-	-	761	·
Stage 1	401	-	-	÷	-	-
Stage 2	687	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	178	341	-	-	761	-
Mov Cap-2 Maneuver	178	-	-	-	-	-
Stage 1	401	-	-	-	-	-
Stage 2	684	-	-	-	-	-
2						
Approach	WB		NB		SB	
HCM Control Delay, s	0		0		0	
HCM LOS	A		-		-	
	-					
Minor Lane/Maior Mvn	nt	NBT	NBRW	VBLn1	SBL	SBT
Capacity (veh/h)				-	761	
HCM Lane V/C Ratio		-	_		0 004	_
HCM Control Delay (s))	-	_	0	9.004	
HCM Lane LOS	,	-	_	Δ	Δ	_
HCM 95th %tile Q/veh)	-	-	-	0	-
HUM 95th %tile Q(veh)	-	-	-	0	-

t Delay, s/veh 0	
ovement WBL WBR NB1 NBR SBL SBT	
ane Configurations Y b	
raffic Vol, veh/h 0 0 967 14 3 813	
uture Vol, veh/h 0 0 967 14 3 813	
onflicting Peds, #/hr 0 0 0 0 0 0	
gn Control Stop Stop Free Free Free	
T Channelized - None - None	
lorage Length 50 -	
eh in Median Storage, # 0 - 0 0	
rade, % 0 - 0 0	
eak Hour Factor 90 90 90 97 97	
eavy Vehicles, % 0 0 4 0 0 5	
vmt Flow 0 0 1074 16 3 838	
ajor/Minor Minor1 Major1 Major2	
onflicting Flow All 1507 1082 0 0 1090 0	
Stage 1 1082	
Stage 2 425	
ritical Hdwy 6.6 6.2 4.1 -	
ritical Hdwy Stg 1 5.4	
ritical Hdwy Stg 2 5.8	
ollow-up Hdwy 3.5 3.3 2.2 -	
ot Cap-1 Maneuver 124 267 648 -	
Stage 1 328	
Stage 2 633	
atoon blocked, %	
ov Cap-1 Maneuver 123 267 648 -	
ov Cap-2 Maneuver 123	
Stage 1 328	
Stage 2 630	
pproach WB NB SB	
CM Control Delay, s 0 0 0	
CM LOS A	
nor Lane/Major Mvmt NBT NBRWBLn1 SBL SBT	
apacity (veh/h) 648 -	
CM Lane V/C Ratio 0.005 -	
CM Control Delay (s) 0 10.6 -	
CM Lane LOS A B -	

HCM 6th TWSC 2: US1 & South Site Driveway

Intersection							
Int Delay, s/veh	0.5						
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	Y	1	ĵ.	1	্ৰশ	<u>_</u>	
Traffic Vol, veh/h	0	0	906	77	81	824	
Future Vol, veh/h	0	0	906	77	81	824	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Stop	Stop	Free	Free	Free	Free	
RT Channelized	-	None	-	None	-	None	
Storage Length	-	-	-	-	50	-	
Veh in Median Storag	e,# 0	-	0	-	-	0	
Grade, %	0	-	0	-	~	0	
Peak Hour Factor	90	90	90	90	97	97	,
Heavy Vehicles, %	0	0	4	0	0	5	
Mvmt Flow	0	0	1007	86	84	849	
	-				- •		
Major/Minor	Minor1	1	Maior1		Major?		
Conflicting Flow All	1642	1050		Δ	1002	0	
	1043	1050	U	U	1093	U	
Stage 1	1000	-	-	-	-	-	
Stage 2	593	-	-	-	-	-	
Critical Howy	0.0	6. Z	-	-	4.1	-	
Critical Howy Stg 1	5.4	-	-	-	-	-	
Critical Howy Stg 2	5.8		-	-	-	-	
Follow-up Hawy	3.5	3.3	-	-	2.2		
Pot Cap-1 Maneuver	101	278	-	-	646	-	
Stage 1	340	-	-	-	-	-	
Stage 2	521	-	-	-	-	-	
Platoon blocked, %			-	-		-	
Mov Cap-1 Maneuver	88	278	-	-	646	-	
Mov Cap-2 Maneuver	88	-	-	-	-	-	
Stage 1	340	-	-	-	-	-	
Stage 2	453	-	-	-	-	-	
Approach	WB		NB		SB		
HCM Control Delay, s	0		0		1		
HCM LOS	А						
Minor Lane/Major Myr	nt	NBT	NRRV	VBI n1	SBI	SBT	
Canacity (veh/h)					6/6		
HCM Lane V/C Patio		-	-	-	040	-	
HCM Control Delay (s)	-	-	-	11 /	-	
HCM Lane LOS	7	-	-	۰ ۸	11.4 D	-	
HOM OF the Olice		-	-	А	D A	-	
LICINI ADIU XIIIE M(Aeu	IJ	-	-	-	0.4	-	

Stephen G. Pernaw & Company, Inc.

Intersection						
Int Delay, s/veh	0					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	¥	-	đ,		1	_ ^ †
Traffic Vol, veh/h	0	0	1069	14	3	898
Future Vol, veh/h	0	0	1069	14	3	898
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage	e,#0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	90	90	90	90	97	97
Heavy Vehicles, %	0	0	4	0	0	5
Mvmt Flow	0	0	1188	16	3	926
Maior/Minor	Minor1	1	Maior1	i	Maior2	
Conflicting Flow All	1665	1196	0	0	1204	0
Stage 1	1196	-	-	-		-
Stage 2	469	2	_	-	-	-
Critical Hdwv	6.6	6.2	-	-	4.1	-
Critical Hdwy Sto 1	5.4	-	-	-	-	-
Critical Hdwy Sto 2	5.8	-	-	-	-	-
Follow-up Hdwv	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	98	229	-	-	587	-
Stage 1	289		-	-	-	-
Stage 2	602	-	-	-	_	_
Platoon blocked. %			-	-		-
Mov Cap-1 Maneuver	98	229	-	-	587	-
Mov Cap-2 Maneuver	98		-	-	-	-
Stage 1	289	-	-	-	-	-
Stage 2	599	-	-	-	_	-
Approach	WB		NB		SB	
HCM Control Delay s	0		0		0	
HCM LOS	Ă		v		v	
Minor Lane/Major Mvm	ıt	NBT	NBRV	/BLn1	SBL	SBT
Capacity (veh/h)		-		-	587	
HCM Lane V/C Ratio		-	_	-	0.005	-
HCM Control Delay (s)		_	-	0	11.2	-
HCM Lane LOS		-	-	Ă	B	-
HCM 95th %tile Q(veh)	I	-	-	-	0	-
HCM 95th %tile Q(veh)	I	-	-	-	0	-

Intersection						
Int Delay, s/veh	0.5					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Ý		1		শ	桥
Traffic Vol, veh/h	0	V 0*	1008	77	81	909
Future Vol, veh/h	0	0	1008	77	81	909
Conflicting Peds, #/hr	. 0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storag	je,#0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	90	90	90	90	97	97
Heavy Vehicles, %	0	0	4	0	0	5
Mvmt Flow	0	0	1120	86	84	937
Major/Minor	Minor1	1	Vajor1	1	Major2	
Conflicting Flow All	1800	1163	0	0	1206	0
Stage 1	1163	-	-	-	-	-
Stage 2	637	-	-	-	-	-
Critical Hdwy	6.6	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.8	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	80	239	-	-	586	-
Stage 1	300	-	-	-	-	-
Stage 2	494	-	-	-		-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	69	239	-	-	586	-
Mov Cap-2 Maneuver	· 69	-	-	-	-	-
Stage 1	300	-	-	-	-	-
Stage 2	423	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	0		0		1	
HCM LOS	А					
Minor Lane/Major Mvi	mt	NBT	NBRV	/BLn1	SBL	SBT
Capacity (veh/h)		-	-	-	586	-
HCM Lane V/C Ratio		-	-	-	0.143	-
HCM Control Delay (s	5)	-	-	0	12.2	-
HCM Lane LOS		-	-	Α	В	-
HCM 95th %tile Q(veh	ר)	-	57	-	0.5	-

Intersection						
Int Delay, s/veh	0.1					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	¥		ĥ		٣	**
Traffic Vol, veh/h	0	0	984	/ 19	11	/1042
Future Vol, veh/h	0	0	984	19	11	1042
Conflicting Peds, #/hr	• 0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storag	je,#0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	90	90	98	98	93	93
Heavy Vehicles, %	0	0	4	ď	0	2
Mvmt Flow	0	0	1004	19	12	1120
Major/Minor	Minor1	ſ	Major1		Major2	
Conflicting Flow All	1598	1014	0	0	1023	0
Stage 1	1014	-	-	-	-	-
Stage 2	584	-	-	-	-	-
Critical Hdwy	6.6	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.8	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	108	292	-	-	686	-
Stage 1	353	-	-	-	-	-
Stage 2	526	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	106	292	-	-	686	-
Mov Cap-2 Maneuver	106	-	-	-	-	-
Stage 1	353	-	-	-	-	-
Stage 2	517	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	0	-	0		0.1	
HCM LOS	А					
Minor Lane/Major Myr	nt	NRT		/RI n1	SBI	SBT
Canacity (veh/h)					696	001
HCM Lane V/C Ratio		-	-	-	000	-
HCM Control Delay (s)	-	-	0	10.3	
HCM Lane LOS	,	_	-	Δ	10.0 R	-
HCM 95th %tile O/veh	a)	-	-	-	Λ1	-
	')		-	-	0.1	-

Intersection						
Int Delay, s/veh	0.1					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W		1		3	**
Traffic Vol. veh/h	0	0.	1116	21	12	1182
Future Vol. veh/h	õ	0	1116	21	12	1182
Conflicting Peds. #/hr	Õ	Õ	0	0	.2	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	P	None	-	None	_	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage	e.#0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	90	90	98	98	93	93
Heavy Vehicles. %	0	0	4	0	0	2
Mvmt Flow	0	Ó	1139	21	13	1271
Major/Minor	Minor1	N	Major1	,	Vaioro	
	1010	1150			1160	0
Stogo 1	1150	1100	U	U	0011	U
Stage 2	1100	-	-	-	-	-
Sidge 2	200	-	-	-	-	-
Critical House Sta 4	0.0 E A	0.2	-	-	4.1	-
Critical Howy Stg 1	5.4	-	-	-	-	-
Critical Howy Stg 2	5.8	-	-	-	-	-
Follow-up Hawy	3.5	3.3	-	-	2.2	5
Pot Cap-1 Maneuver	79	244	-	-	610	-
Stage 1	304	-	-	-	-	-
Stage 2	480	-	-	-	-	-
Platoon blocked, %			-	-	0.10	-
Mov Cap-1 Maneuver	77	244	-	-	610	-
Mov Cap-2 Maneuver	77	-	-	-	-	-
Stage 1	304	-	-	-	-	-
Stage 2	470	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	0		0		0.1	
HCM LOS	А					
Minor Lane/Major Myn	nt	NBT	NRRM	/BLn1	SBI	SBT
Canacity (yoh/h)		וטח	NDIN		610	100
HCM Lane V/C Patio		-	-	-	010	-
HCM Control Delay (e)				-	0.021 11	-
HCM ane OS	,	_	-	Δ	R	-
HCM 95th %tile O(veh)	-	14	-	01	-
TOW OUT MUS QUE	/	-	-	-	0.1	

Intersection						
Int Delay, s/veh	0.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		1	-		<u></u>
Traffic Vol, veh/h	0	0	1078	59	75	1187
Future Vol, veh/h	0	0	1078	59	75	1187
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storage	e,#0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	90	90	98	98	93	93
Heavy Vehicles, %	0	0	4	0	0	2
Mymt Flow	0	0	1100	60	81	1276
	5	•			• ·	
		-		-		
	Minor1	1	viajor1		vlajor2	
Conflicting Flow All	1930	1130	0	0	1160	0
Stage 1	1130	-	-	-	-	-
Stage 2	800	-	-	-	-	-
Critical Hdwy	6.6	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.8	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	66	250	-	-	610	-
Stage 1	311	-	-	-	-	-
Stage 2	408	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	57	250	-	-	610	-
Mov Cap-2 Maneuver	57	-	-	-	_	-
Stage 1	311	-	-	_	-	-
Stage 2	354		-	-	-	_
01490 2	007					2
Approach	WB		NB		SB	
HCM Control Delay s	0	· · · · ·	0		0.7	· · · · ·
HCM LOS	Δ		v		0.1	
	~					
200 - L. 200						
Minor Lane/Major Mvm	nt	NBT	NBRV	VBLn1	SBL	SBT
Capacity (veh/h)		-	-	-	610	-
HCM Lane V/C Ratio		-	-	-	0.132	-
HCM Control Delay (s)		-	-	0	11.8	-
HCM Lane LOS		-	-	А	В	-
HCM 95th %tile Q(veh))	-	-	-	0.5	-

Intersection						
Int Delay, s/veh	0.1			••••••		
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	¥	7	4		া	
Traffic Vol, veh/h	0	V 0.	1233	21	12	1306
Future Vol, veh/h	0	0	1233	21	12	1306
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	<u> </u>	_	-	-	50	-
Veh in Median Storage	e,# 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	90	90	98	98	93	93
Heavy Vehicles, %	0	0	4	0	0	2
Mvmt Flow	0	0	1258	21	13	1404
Major/Minor	Minor1	ſ	Major1	I	Major2	
Conflicting Flow All	1997	1269	0	0	1279	0
Stage 1	1269	-	-	-	-	-
Stage 2	728	-	-	-	-	-
Critical Hdwy	6.6	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.8	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	60	208	-	-	550	-
Stage 1	267	-	-	-	-	-
Stage 2	444	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	59	208	-	-	550	-
Mov Cap-2 Maneuver	59	-	-	-	-	-
Stage 1	267	-	-	-	-	-
Stage 2	433	-	-	.	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	0		0		0.1	
HCM LOS	А					
Minor Lane/Major Mvn	nt	NBT	NBRV	VBLn1	SBL	SBT
Capacity (veh/h)		-	-	-	550	-
HCM Lane V/C Ratio		-	-	-	0.023	-
HCM Control Delay (s))	-	-	0	11.7	-
HCM Lane LOS		-	-	А	В	-
HCM 95th %tile Q(veh	i) -	-	-	-	0.1	-

Intersection						
Int Delay, s/veh	0.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	¥		1.		٦	**
Traffic Vol. veh/h	0	0	1194	59	75	1311
Future Vol. veh/h	Ő	0	1194	59	75	1311
Conflicting Peds. #/hr	Ő	Õ	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	_	-	50	-
Veh in Median Storage	e# 0	_	0	-	-	0
Grade %	0, " 0	-	Ő	-	_	õ
Peak Hour Factor	90	90	98	98	93	93
Heavy Vehicles %	0	0	4	0	0	2
Mumt Flow	0	0	1218	0	81	1/10
WWWITTIOW	0	0	1210	00	01	1410
Major/Minor	Minor1	N	Major1		Major2	
Conflicting Flow All	2115	1248	0	0	1278	0
Stage 1	1248	-	-	-	-	-
Stage 2	867	-	-	-	-	-
Critical Hdwy	6.6	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.8	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	50	213	-	-	550	
Stage 1	273	-	_	-		-
Stage 2	377	-		-	-	-
Platoon blocked %	0		_			_
Mov Can-1 Maneuver	13	213	_		550	_
Mov Cap-1 Maneuver	-+	213	~	-	000	-
Stoco 1	43	-	-	-	-	-
Stage 1	2/3	-	-	-	-	-
Stage 2	322	70	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	0		0		0.7	
HCM LOS	А					
Minor Lane/Major Mun	nt	NPT	NDDW		CDI	орт
	щ	INDI	NBRV	VOLNI	SBL	201
Capacity (ven/n)		-	-	-	550	-
HUM Lane V/C Ratio	N N	-	-	-	0.14/	-
HCM Control Delay (s))	-	-	0	12.7	-
HCM Lane LOS		-	-	A	B	-
HCM 95th %tile Q(veh	I)	-	-	-	0.5	-

Intersection							
Int Delay, s/veh	0.1						
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	Ý		- Ja	-	1	↑ ↑	1
Traffic Vol, veh/h	0	1	1144	15	19	906 🗸	
Future Vol, veh/h	0	1	1144	15	19	906	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Stop	Stop	Free	Free	Free	Free	
RT Channelized	-	None	-	None	-	None	
Storage Length	-	-	-	-	50	-	
Veh in Median Storage	e,#0	-	0	-	-	0	
Grade, %	0	-	0	-	-	0	
Peak Hour Factor	90	90	96,	96	96	96	
Heavy Vehicles, %	0	0	1	0	0	1,	
Mvmt Flow	0	1	1192	16	20	944	
Maior/Minor	Minor1	r	Major1		Maior2		
Conflicting Flow All	1712	1200		0	1208	Λ	
Stage 1	1200	.200	-	-		-	
Stage 2	512	-	-	_	_	_	
Critical Hdwy	66	62			41		
Critical Hdwy Sto 1	54	0.2	-	-	т. ı -	_	
Critical Hdwy Stg 2	5.8	-	-	-	-	_	
Follow-up Hdwy	3.5	3.3	-	-	22	-	
Pot Cap-1 Maneuver	92	228	-	-	585	-	
Stage 1	288		-	-	-	-	
Stage 2	572	-	_	-	-	_	
Platoon blocked %	012		-	-		_	
Mov Cap-1 Maneuver	89	228	-	-	585	-	
Mov Cap-2 Maneuver	89		-	-	-	-	
Stage 1	288	-	-	_	-	-	
Stage 2	553	-	_	-	-	-	
Approach	WB		NB		SB		
HCM Control Delay s	20.9		0		0.2		
HCM LOS	C		J		0.2		
	Ŭ						
Minor Lane/Major Mvm	nt	NBT	NBRW	/BLn1	SBL	SBT	
Capacity (veh/h)		-	-	228	585	-	
HCM Lane V/C Ratio		-	-	0.005	0.034	-	
HCM Control Delay (s)		-	-	20.9	11.4	_	
HCM Lane LOS		-	-	C	В	-	
HCM 95th %tile Q(veh))	-	-	0	0.1	-	
				-			

Intersection						
Int Delay, s/veh	0.1					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	¥		4î		ሻ	<u>_</u>
Traffic Vol, veh/h	.0	1	1238	16	20	980
Future Vol, veh/h	0	1	1238	16	20	980
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storag	e, # 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	90	90	96	96	96	96
Heavy Vehicles, %	0	0	1	0	0	1
Mvmt Flow	0	1	1290	17	21	1021
Major/Minor	Minor1	ſ	Major1		Major2	
Conflicting Flow All	1852	1299	0	0	1307	0
Stage 1	1299	-	-	-	-	-
Stage 2	553	-	-	-	-	-
Critical Hdwy	6.6	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	~
Critical Hdwy Stg 2	5.8	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	_	-	2.2	-
Pot Cap-1 Maneuver	74	199	-	-	536	-
Stage 1	258	-	-	-	-	-
Stage 2	546	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	71	199	-	-	536	-
Mov Cap-2 Maneuver	71	-	-	-	-	-
Stage 1	258	- ³	-	-	-	-
Stage 2	525	-	-	-	-	-
Approach	WB		NB	100.007	SB	
HCM Control Delay, s	23.2		0		0.2	
HCM LOS	С					
Minor Lane/Major Mvn	nt	NBT	NBRV	VBLn1	SBL	SBT
Capacity (veh/h)		-	-	199	536	-
HCM Lane V/C Ratio		-	-	0.006	0.039	-
HCM Control Delay (s))	-	-	23.2	12	-
HCM Lane LOS		-	-	С	В	-
HCM 95th %tile Q(veh)	-	-	0	0.1	-

Intersection						
Int Delay, s/veh	0.4					
Movement	WBL	WBR	NBT	NBR	SBI	SBT
Lane Configurations	M		_ <u>1</u> _		3	<u></u>
Traffic Vol. veh/h	0	1 0.	1187	72	74	aan
Future Vol. veh/h	Ő	, 0	1187	72	74	990
Conflicting Peds #/hr	r Ö	ñ	0	0	0	0.00
Sign Control	Ston	Ston	Free	Free	Free	Free
RT Channelized	0.0p	None	1100	None	1100	None
Storage Length	_	-	_	None	50	NONÇ
Veh in Median Storac	۔ 0 # ۵	_	-	_	50	0
Grade %	<i>j</i> e, <i>π</i> 0	_	0	-	-	0
Deak Hour Eactor	0	- 00	0	-	-	06
Hear Nobiolog %	90	90	90	90	90	90
Mumt Flow	0	0	1000	75	0	1
www.fiow	U	0	1230	75		1031
Major/Minor	Minor1	M	Major1		Major2	
Conflicting Flow All	1944	1274	0	0	1311	0
Stage 1	1274	-		-	-	-
Stage 2	670		-	-	-	-
Critical Hdwv	6.6	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Sto 2	5.8	-	-	-	-	-
Follow-up Hdwy	3.5	33	-	-	22	-
Pot Cap-1 Maneuver	65	206	-	-	534	
Stage 1	265	200	-	-		_
Stage 2	476	_	_		_	-
Platoon blocked %	470	-	-	-	-	-
May Cap 1 Manager	. EC	206	-	-	504	-
Mov Cap-1 Maneuver	00	200	-	-	034	-
wov Cap-2 Maneuver	56	-	-	-	-	-
Stage 1	265	-	-	-	-	-
Stage 2	407	-	-	-	•	-
Approach	WB		NB		SB	
HCM Control Delay, s	0		0		0.9	
HCM LOS	Ă		5		0.0	
Minor Lane/Major Mvr	mt	NBT	NBRV	VBLn1	SBL	SBT
Capacity (veh/h)		-	-	-	534	-
HCM Lane V/C Ratio		-	-	-	0.144	-
HCM Control Delay (s	5)	-	14	0	12.9	-
HCM Lane LOS		-	-	А	В	-
HCM 95th %tile Q(ver	ר)	-	-	-	0.5	-

Intersection						
Int Delay, s/veh	0.1					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W		ţ,		٦	**
Traffic Vol. veh/h	0	$\sqrt{1}$	1368	16	20	1083
Future Vol. veh/h	0	1	1368	16	20	1083
Conflicting Peds. #/hr	Ō	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized		None	-	None	-	None
Storage Length	-	-	-	-	50	-
Veh in Median Storag	e.# 0	-	0	-	-	0
Grade. %	0,	-	Õ	-	-	Õ
Peak Hour Factor	90	90	96	96	96	96
Heavy Vehicles %	0	0	1	0	0	1
Mymt Flow	0	1	1425	17	21	1128
	Ŭ	•	1420		21	1120
Major/Minor Minor1 Major1 Major2						
Conflicting Flow All	2040	1/2/		0	1440	
Store 1	1/2/	1434	0	0	1442	U
Stage 2	606	-	-	-	-	-
Critical Udway	600	-	-	-	-	-
Critical Houry Sta 1	0.0 E 4	0.Z	-	-	4.1	-
Critical Howy Stg 1	0.4 5 0	-	-	-	-	-
Enlicar Huwy Sig Z	0.0 0.5	-	-	-	-	-
Police-up nawy	3.5	3.3	-	-	Z.Z	-
Pot Cap-1 Maneuver	56	166	-	-	4/6	-
Stage 1	222	-	-	-	-	-
Stage 2	513	-	-	-		-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	54	166	-	-	476	-
Mov Cap-2 Maneuver	54	-	-	-	-	-
Stage 1	222	-	-	-	-	-
Stage 2	490	-	-	-	-	-
Approach	WB		NB		SB	
HCM Control Delay, s	26.8		0		0.2	
HCM LOS	D					
Minor Lane/Major Mvn	nt	NBT	NBRW	/BLn1	SBL	SBT
Capacity (veh/h)		-	-	166	476	-
HCM Lane V/C Ratio		-	-	0.007	0.044	-
HCM Control Delay (s)		-	-	26.8	12.9	-
HCM Lane LOS		-	-	D	B	-
HCM 95th %tile Q(veh)	-	-	0	0.1	-
	'			v	0.1	

Intersection					
Int Delay, s/veh 0.	1				
Movement WB	_ WBR	NBT	NBR	SBL	SBT
Lane Configurations	f	1		ĥ	44
Traffic Vol, veh/h	o ∕ o	1317	72	74	1093
Future Vol, veh/h	0 0	1317	72	74	1093
Conflicting Peds, #/hr	0 0	0	0	0	0
Sign Control Sto	o Stop	Free	Free	Free	Free
RT Channelized	- None	-	None	-	None
Storage Length		-	-	50	-
Veh in Median Storage, #) -	0	-	-	0
Grade, %) -	0	-	-	0
Peak Hour Factor 9) 90	96	96	96	96
Heavy Vehicles, %	0 (1	0	0	1
Mvmt Flow	0 (1372	75	77	1139
Maior/Minor Minor	1	Maior1	ſ	Maior2	
Conflicting Flow All 213	4 1410	0	0	1447	0
Stage 1 141) -	-	-	-	-
Stage 2 72	1 -	-	-	-	-
Critical Hdwy 6.	6.2	-	-	4.1	-
Critical Hdwy Stg 1 5.	4 -	-	-	-	-
Critical Hdwy Stg 2 5.	3 -	-	-	-	-
Follow-up Hdwy 3.	5 3.3	-	-	2.2	-
Pot Cap-1 Maneuver 4	9 171	-	-	474	-
Stage 1 22	3 -	-	-	-	-
Stage 2 44	3 -	-	-	-	-
Platoon blocked, %		-	-		-
Mov Cap-1 Maneuver 4	l 171	-	-	474	-
Mov Cap-2 Maneuver 4	-	-	-	-	-
Stage 1 22	3 -	-	-	-	-
Stage 2 37	4 -	-	-	-	-
Approach WI	3	NB		SB	
HCM Control Delay, s)	0	· · ·	0.9	
HCM LOS	۱	2			
Minor Lane/Major Mvmt	NBT	NBRV	VBLn1	SBL	SBT
Capacity (veh/h)	-	Ξ.	-	474	-
HCM Lane V/C Ratio	-	-	-	0.163	-
HCM Control Delay (s)	-	-	0	14.1	-
HCM Lane LOS	-	-	А	В	-
HCM 95th %tile Q(veh)	-	-	-	0.6	-

Appendix G

Auxiliary Turn Lane Warrants Analysis
2023 AM Build US Route 1 / South Site Driveway



Figure 2 - 6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

INPUT



2023 PM Build US Route 1 / South Site Driveway

Stephen G. Pernaw & Company, Inc.

Figure 2 - 6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

INPUT



2023 Saturday Build US Route 1 / South Site Driveway



Figure 2 - 6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

INPUT



2023 AM Build US Route 1 / Existing North Site Driveway



Figure 2 - 4. Guideline for determining minor-road approach geometry at two-way stop-controlled intersections.

INPUT

		Consider two approach lanes				/	/		/	One approach lane is o.k.		200 400 600 800 1000 1200 1400 1600 1800 2000	Major-Road Volume (total of both directions), veh/h		
	200 '(I	ıoi	t 29	ib ənc	ດດ ບາງ ບາງ ບາງ ບາງ	ləv n	101	(p)	503	or-F	c ui	N			
Value	1748	59%	158			Value	92							Follow-up gap, s:	3.3
								geometry:	nes					l gap, s:	6.2
	veh/h:						veh/h:	proach	proach la					Critica	

Left-turn and through capacity, veh/h: * according to Table 17 - 5 of the HCM

4.0

6.5

2023 PM Build US Route 1 / Existing North Site Driveway



Figure 2 - 4. Guideline for determining minor-road approach geometry at two-way stop-controlled intersections.

INPUT

	200 200		
alue	280	4%	35
N8	3	ۍ ا	1
	veh/h:		
	f both directions),	is on minor road, %:	ne direction), veh/h:

Left-turn and through capacity, veh/h: * according to Table 17 - 5 of the HCM

2023 Saturday Build US Route 1 / Existing North Site Driveway



Figure 2 - 4. Guideline for determining minor-road approach geometry at two-way stop-controlled intersections.

INPUT

		Consider two approach lanes				/		/		lane is o.k.		600 800 1000 1200 1400 1600 1800 2000	 d Volume (total of both directions), veh/h			
	(), 1), 500	ior	toe	300) อเ	ləv Un	70	, p	100	One approach	c -	200 400	Major-Roac			
value	2315	57%	152			Value	43							Follow-up gap, s:	3.3	4.0
	, veh/h:						veh/h:	proach geometry:	proach lanes					Critical gap, s:	6.2	6.5
Variable	Major-road volume (total of both directions)	Percentage of right-turns on minor road, %:	Minor-road volume (one direction), veh/h:		OUTPUT	Variable	Limiting minor-road volume (one direction),	Guidance for determining minor-road ap	Consider TWO ap				CALIBRATION CONSTANTS	Minor Road	Right-turn capacity, veh/h:	Left-turn and through capacity, veh/h:

Left-turn and through capacity, veh/h: * according to Table 17 - 5 of the HCM Appendix H

Miscellaneous



DRIVE-THROUGH QUEUEING ANALYSIS

INTERSEC MOVEMEN	TION: T:	Common Man Roadside Drive Through Lane			
	SERVIC	E TIME (Minutes)			
S	TOTAL E	ELAPSED TIME (SEC):	3600		
F	SIDE ST	REET ARRIVALS	47		30% drive-throughs
C	SIDE ST		80		service ratte = 45 sec/veh
I	ARRIVA	LRATE	0.0131		
u	SERVIC	E RATE	0.0222		
Р	TRAFFIC	CINTENSITY FACTOR	0.5875		
1 AVERA		JE LENGTH	0.83674		
2 AVERA	GE NUM	BER IN SYSTEM	1.42424		
3 VARIAI	NCE OF #	IN SYSTEM	3.45271		
4 AVERA	GE WAIT	ING TIME	64.0909		
5 AVERA	GE TIME	IN SYSTEM	109.091		
6 PROBA	ABILTY OI	F 0 VEHICLES IN QUEUE	41.3%	41.3%	
7 PROBA	ABILTY O	F 1 VEHICLES IN QUEUE	24.2%	65.5%	
8 PROBA	ABILTY OI	F 2 VEHICLES IN QUEUE	14.2%	79.7%	
9 PROBA	ABILTY O	F 3 VEHICLES IN QUEUE	8.4%	88.1%	
10 PROBA	ABILTY OI	F 4 VEHICLES IN QUEUE	4.9%	93.0%	
11 PROBA	ABILTY OI	5 VEHICLES IN QUEUE	2.9%	95.9%	95th percentile queue = 5 veh.
12 PROBA	ABILTY OI	F 6 VEHICLES IN QUEUE	1.7%	97.6%	
13 PROBA	BILTY O	F 7 VEHICLES IN QUEUE	1.0%	98.6%	
14 PROBA	ABILTY OF	F 8 VEHICLES IN QUEUE	0.6%	99.2%	
15 PROBA	ABILTY OF	F 9 VEHICLES IN QUEUE	0.3%	99.5%	
16 PROBA	BILTY OI	F 10 VEHICLES IN QUEUE	0.2%	99.7%	
17 PROBA	ABILTY OF	T 11 VEHICLES IN QUEUE	0.1%	99.8%	
18 PROBA	ABILTY OF	F 12 VEHICLES IN QUEUE	0.1%	99.9%	
19 PROBA	BILTY OF	F 13 VEHICLES IN QUEUE	0.0%	99.9%	
20 PROBA	BILTY OF	F 14 VEHICLES IN QUEUE	0.0%	100.0%	
21 PROBA	BILTY OF	F 15 VEHICLES IN QUEUE	0.0%	100.0%	