SITE PLAN REVIEW TECHNICAL ADVISORY COMMITTEE PORTSMOUTH, NEW HAMPSHIRE

CONFERENCE ROOM A CITY HALL, MUNICIPAL COMPLEX, 1 JUNKINS AVENUE

Members of the public also have the option to join the meeting over Zoom (See below for more details)*

2:00 PM September 3, 2024

AGENDA

I. APPROVAL OF MINUTES

A. Approval of minutes from the August 6, 2024 Site Plan Review Technical Advisory Committee Meeting.

II. OLD BUSINESS

- A. The request of 635 Sagamore Development LLC (Owner), For property located at 635 Sagamore Avenue requesting Site Plan approval for the removal of the existing structures and construction of 4 single-family dwellings on one lot with associated site improvements. Said property is located on Assessor Map 222 Lot 19 and lies within the Single Residence A (SRA) District. LU-22-209)
- **B.** The request of **Oak Street Real Estate Capital (Owner), 100 Durgin Lane Owner, LLC (Applicant),** for property located at **100 Durgin Lane** requesting Subdivision approval of a lot line adjustment and Site Plan Review approval for the demolition of the existing buildings and the construction of 360 rental housing units in a mix of 3-story and 4-story buildings with associated site improvements including parking, pedestrian access, community spaces, utilities, stormwater management, lighting, and landscaping. Said property is located on Assessor Map 239 Lot 18 and lies within the Gateway Corridor (G1) District. (LU-24-62)

III. NEW BUISINESS

A. The request of Northeast Credit Union (Owner), and Liberty Mutual Insurance (Owner), for properties located at 100 Borthwick Avenue and 0 Borthwick Avenue requesting lot line adjustment to add approximately 4.80 Acres to Map 240 Lot 3. Said properties are located on Assessor Map 259 Lot 15 and Map 240 Lot 3 and lie within the Office Research (OR) District. (LU-24-151)

IV. ADJOURNMENT

*Members of the public also have the option to join this meeting over Zoom, a unique meeting ID and password will be provided once you register. To register, click on the link below or copy and paste this into your web browser:

https://us06web.zoom.us/webinar/register/WN 12YCI10ITkaiVe3Lrb0ttA

SITE PLAN REVIEW TECHNICAL ADVISORY COMMITTEE PORTSMOUTH, NEW HAMPSHIRE

CONFERENCE ROOM A CITY HALL, MUNICIPAL COMPLEX, 1 JUNKINS AVENUE

2:00 PM August 6, 2024

MEMBERS PRESENT:

Peter Stith, Chairperson, Planning Manager; David Desfosses, Construction Technician Supervisor; Chad Putney, Fire Prevention Officer; Shanti Wolph, Chief

Building Inspector; Zachary Cronin, Assistant City Engineer,

Eric Eby, Parking and Transportation Engineer; Mike Maloney; Deputy Police Chief, Vincent Hayes; Planner I

MEMBERS ABSENT: Peter Britz, Director of Planning & Sustainability

ADDITIONAL

STAFF PRESENT: Stefanie Casella, Planner II

MINUTES

I. APPROVAL OF MINUTES

- **A.** Approval of minutes from the June 4, 2024 Site Plan Review Technical Advisory Committee Meeting.
- **B.** Approval of minutes from the July 2, 2024 Site Plan Review Technical Advisory Committee Meeting.

[3:02] E. Eby made a motion to accept both sets of minutes. P. Britz seconded the motion. The motion passed unanimously.

II. OLD BUSINESS

A. REQUEST TO POSTPONE The request of 635 Sagamore Development LLC (Owner), For property located at 635 Sagamore Avenue requesting Site Plan approval for the removal of the existing structures and construction of 4 single-family dwellings on one lot with associated site improvements. Said property is located on Assessor Map 222 Lot 19 and lies within the Single Residence A (SRA) District. REQUEST TO POSTPONE (LU-22-209)

[3:12] Chairman Stith announced that this application was still postponed as they are awaiting a third-party review.

B. The request of **Oak Street Real Estate Capital (Owner), 100 Durgin Lane Owner, LLC (Applicant),** for property located at **100 Durgin Lane** requesting Subdivision approval of a lot line adjustment and Site Plan Review approval for the demolition of the existing buildings and the construction of 360 rental housing units in a mix of 3-story and 4-story buildings with associated site improvements including parking, pedestrian access, community spaces, utilities, stormwater management, lighting, and landscaping. Said property is located on Assessor Map 239 Lot 18 and lies within the Gateway Corridor (G1) District. (LU-24-62)

SPEAKING TO THE APPLICATION

[4:45] Brett Benson, Andrew Hayes, Nick Aceto and Neil Hansen came to present this application. Mr. Benson ran through a slideshow with project updates that have occurred since the last TAC meeting. These included: the community building for residents would now be included in a residential building and not a stand alone building, buildings have been moved further from the wetland buffer since the April submission, and stormwater system changes. Mr. Benson and Mr. Aceto went over site constraints, wetland buffer impacts, the proposed open spaces, community spaces and landscaping. Mr. Hansen and Mr. Aceto then addressed staff comments:

1. Please demonstrate how you are complying with the City's landscaped island standards in Site Plan Regs Section 6.6.

They believe they are in compliance with larger than needed landscaped island widths and deliberate placements.

2. Please update plant quantities on landscape plan (Sheet L-300)

They full intend to do this and need to work with the client to work through the quantities.

3. If hardscaping is planned for areas of the wetland buffer (bituminous paving and granite steps on the north side), please provide impact numbers (Sheet L-200).

They believe have accounted for all of the hardscaping areas within the impervious calculations.

4. Please share more details on shared multi modal way and how it will promote slow traffic.

The intent of the multi-modal way is to provide traffic calming with street trees, on-street parking and landscaped islands. The intent is to provide visual friction as you move along the corridor in a vehicle.

5. Does the sheltered parking have solar?

They are continuing to study this, the orientation is optimal for solar and they believe it will be easy to accommodate solar panels.

- 6. Please explain why lots 2 and 3 can not be combined into one lot.
- 7. Please demonstrate vehicular and utility access for all lots to/from a public way.

To answer comments 6 and 7 - the intent is to preserve the three lots that exist today at the property and they have proposed to redraw the lot lines to not impose on the proposed structures. Their intent is to have a master easement agreement across the three properties to link them all together.

8. Weston & Sampson and the City's legal department have agreed on the three-party agreement contract language. It will be issued shortly. Staff will provide more comments after report has been issued.

The third-party review for stormwater is coming from the AOT review from NHDES. This will be submitted in the next submission.

[19:29] C. Putney asked the applicants to show the fire hydrant locations in their final submission and to include arrows in their wayfinding pointing towards the buildings they indicate.

[20:05] P. Britz noted that it looks like there had been an improvement with the previous path going through the rain garden and the current proposal looks easier for maintenance of the rain garden. He asked if the proposed seating would be an issue for mowing, the applicants responded no. P. Britz also noted that the newly proposed guardrail to discourage foot traffic was a good addition. Mr. Hayes noted the improvement in the wetland buffer and the overall reduction of impervious throughout the whole site.

[22:41] S. Wolph asked if the parcel lines would be reconfigured so that there would be nothing going through buildings. Mr. Hansen responded that no lot lines would be going through the buildings and all of the existing access and utility easements would be cleaned up and reconfigured for the newly proposed roadway layout. Mr. Benson noted that there would be imaginary lot lines drawn between the buildings to help distinguish fire separation distances. Mr. Hayes noted that for the easement agreements, their intent is to record the easement agreements as a condition precedent to the building permit. P. Britz responded that they will need an easement plan to show all the proposed easements, especially the cross easements between lots. Mr. Hansen responded that there were separate easement plan sheets in the back of the current application.

[25:05] D. Desfosses mentioned a few things for the applicants to consider before the next submission. He apologized for the delay of the third-party review from Weston and Sampson and noted that DPW has not reviewed those plans because they are awaiting Weston and Sampson. The engineering comments from DPW are forthcoming. Additionally, he is not satisfied with the access to the hotel by building #1. He believes that the hotel should have its own driveway off of the access road. He noted that would be okay with submitting to NHDES and DPW just reviewing

their comments when it comes to stormwater. Mr. Hayes noted that they had studied multiple configurations for the hotel access and could schedule a follow-up meeting to discuss those in more detail.

[27:00] P. Britz asked what had happened to the rain garden that had previously been proposed for the entry area. Mr. Hansen noted that as part of this TAC application, it had not changed but as part of the submission for the Conservation Commission in August, updated plans show the rain garden removed from that area. The stormwater and drainage system had been reconfigured to deal with this. The greenspace in the roundabout will be a planted space. D. Desfosses asked about the City stormwater system within that area and Mr. Hansen responded and they discussed an easement proposal for the City stormwater system. Once the third-party stormwater is received, D. Desfosses noted that they would have to have discussions about off-site improvements.

PUBLIC HEARING

[29:17] Chairman Stith opened the public hearing.

Elizabeth Bratter of 159 McDonough Street came to speak. She mentioned that she had sent a letter as well. She is hoping that the northern park will be passive, as was encouraged by the Conservation Commission. She did list some concerns about the traffic study and its study area, comments made during the July Conservation Commission meeting that she would like to see addressed, had questions about the rain gardens and where they drained to and wondered what had happened to previous plan iterations showing a retaining wall.

[33:52] Chairman Stith closed the public hearing.

DISCUSSION AND DECISION OF THE BOARD

[34:18] Chairman Stith considered a motion to postpone. D. Desfosses made the motion to postpone this application. Z. Cronin seconded the motion. The motion passed unanimously.

III. NEW BUISINESS

A. The request of Ricci Lumber (Applicant) Portsmouth Hardware & Lumber LLC (Owner), for property located at 105 Bartlett Street requesting Site Plan Review Approval for the demolition of existing sheds and construction of three new storage sheds with associated site improvements. Said property is located on Assessor Map 157 Lot 2 and lies within the Character District 4-W (CD4-W) District. (LU-24-132)

SPEAKING TO THE APPLICATION

[35:15] Pat Moretti (Ricci Lumber), Ed Hayes (property owner), Neil Hansen (Tighe & Bond) and Bret Kelly (Kodiak Building Partners) came to present this application. Mr. Moretti mentioned that this had been an ongoing project and they were currently addressing phase two which is the removal of some older wooden structures and replacement with modern structures. In a previous submission, they were considering a barn structure that would overhang part of an existing sewer

easement and have since removed that impediment from the project. The new proposed shed barn will be off the easement by 10-11 feet. Existing lighting would remain the same for this project and stormwater separation would be addressed during the construction of these buildings. The existing exit routes remain the same. Proposed fire requirements have been submitted and they are awaiting review. Any new fencing will conform to City requirements or seek a variance for approvals.

Mr. Moretti then addressed one of the comments sent by staff:

1. Please submit a green building statement or submit a waiver from this requirement.

This has been drafted and will be submitted.

[40:55] Mr. Hayes mentioned that the upcoming construction project adjacent to the lumber yard would be addressing the separation of sewer and stormwater shortly. He also noted that any need for an easement between this property and the railroad will be done and the property owners have a good relationship with the railroad and will work with them on whatever they need.

2. Lot merger must be part of proposed project.

This is acceptable to the property owner.

[42:55] E. Eby asked Mr. Hayes which railroad company he has had discussion with. Mr. Hayes responded that it is the same group who used to be Boston and Maine and Pan Am.

[43:37] S. Wolph asked if they would need an easement for maintenance from the railroad. Mr. Hayes said that once the buildings are built, there should be a few feet to work within for maintenance needs. They will be steel-sided buildings and should not require much maintenance. The space between the property line does get very tight in some areas. S. Wolph also mentioned that they agree about not needing to sprinkler the building and that they could put the buildings closer with more fire prevention techniques in the wall. C. Putney noted that any padlocking that is proposed would have to go through the Fire Department's Knox system. Any electronic gates would need an override Know key provided to the Fire Department.

[47:25] Chairman Stith asked if the applicants would be constructing Building #3 at all. Mr. Moretti stated that the ground down at Building #3 is not as good as where they are currently working so it will take significant work to get the foundation in. This also means that it will be over budget so they will be looking to install that later down the road. C. Putney asked about emergency egress lighting and Mr. Moretti stated that the business closes at 4:30 every day so there should be enough natural lighting for all the proposed new buildings.

3. Please inform Robert Previti of lot merger proposal.

[49:41] Mr. Moretti addressed this staff comment and said that he had contacted Mr. Previti and left him a voicemail.

4. Provide distance between proposed buildings and the sewer main as well as distance to sewer easement.

[49:09] Mr. Hansen responded to this comment and noted that he had pulled those dimensions and would put the on the plans going forward. For Building #1, it is 11.4' from the building footing to the edge of the easement and 21.4' from the centerline of the sewer. Building #2 is 25.5' from the footing to the edge of the easement and 35.5' to the centerline of the sewer.

5. Include maintenance easement to benefit City outside of current easement that allows the City to place shoring or other necessary measures to protect your foundations in the event that replacement or maintenance is necessary on the sewer main.

[50:02] Mr. Moretti asked what the City would be looking for in a maintenance easement. Z. Cronin responded that if there is an issue with the sewer main, they will need to dig down pretty deep and DPW would need to establish shoring enough to protect the foundations of the proposed new buildings. DPW is looking for the right to put shoring further outside of the existing easement potentially in order to protect the buildings in case of a sewer impact. D. Desfosses noted that this could be done with a note on the plan that should cover how if sewer maintenance is needed, the property owners would allow the City to maintain it.

6. All comments are in regards to proposed buildings 1 and 2. No comments are being provided for proposed future building 3. Proposed future building 3 may be too close to the sewer main to be constructable and will need to return to TAC.

A statement has been supplied stating that they are not pursuing the construction of Building #3 at this time. It will also be removed from the site plans prior to going to the Planning Board.

[52:36] D. Desfosses noted that last time the applicants were before them, the truck turning templates did not look possible. Mr. Hansen noted that they had submitted new truck turning templates and went through the turning radii and the delivery traffic patterns. Discussion continued about the possible turning methods. Mr. Hansen will adjust the curb in one spot and the template will be readjusted to respond to DPW feedback.

PUBLIC HEARING

[58:01] Chairman Stith opened the public hearing. No one spoke. The public hearing was closed.

DISCUSSION AND DECISION OF THE BOARD

[58:22] S. Wolph made a motion to recommend approval to the Planning Board with the following condition:

1. Applicant will submit new turning movements to DPW prior to Planning Board submission demonstrating that trucks can exit through the rear gate.

C. Putney seconded the motion. The motion passed unanimously. A discussion continued about the timeline for submitting materials to DPW prior to the next Planning Board submission.

IV. ADJOURNMENT

The meeting adjourned at 2:57 p.m.



C. The request of Christ Church Parish, (Owner), Portsmouth Housing Authority (Applicant), for property located at 1035 Lafayette Road seeking Conditional Use Permits from Section 10.5B41.10 for a Development Site, from Section 10.5B72 for density bonus incentive for increased dwelling units per building and a Conditional Use Permit from Section 10.1112.14 to provide less than the required parking and Site Plan Review Approval for construction of a 4-story, 44-unit multi-family residential building to the south of the existing church building, conversion of the first-floor of the existing church into office space and construction of a 7-unit transitional housing addition. The lower level of the existing church will be renovated for the daycare and the church will be relocated to the existing rectory building on the site. The project will include associated site improvements such as parking, pedestrian connections, access to public transportation, utilities, stormwater management, lighting, and landscaping. Said property is located on Assessor Map 246 Lot 1 and lies within the Gateway Center (G2) District. (LU-24-92)

SPEAKING TO THE APPLICATION

PUBLIC HEARING

DISCUSSION AND DECISION OF THE BOARD

V. NEW BUISINESS

A. The request of Lonza Biologics (Owner), for property located at 101 International Drive requesting Site Plan Approval for the addition of two (2) industrial equalization (EQ) tanks and one (1) pump house located between the EQ Tanks that will include portions of the existing detention basin to be regraded. Installation of a new outlet structure to support the resized detention basin and a stormwater filtration system are proposed with this project. Said property is located on Assessor Map 305 Lot 6 and lies within the Airport Business Commercial (ABC) District. (LU-24-112)

SPEAKING TO THE APPLICATION

PUBLIC HEARING

DISCUSSION AND DECISION OF THE BOARD

B. The request of **231** Corporate Drive LLC (Owner), for property located at 231 Corporate Drive requesting Site Plan Review Approval for the construction of a 2,340 SF addition for a linear accelerator vault to support the veterinary hospital. The project includes removal of a row of parking which will reduce overall impervious surface impacts within the wetland buffer by approximately 8,801 SF. The project consists of associated site improvements such as lighting, landscaping, and stormwater management. Said property is located on Assessor Map 314 Lot 2 and lies within the Airport Business Commercial (ABC) District. (LU-24-114)

SPEAKING TO THE APPLICATION

PUBLIC HEARING

DISCUSSION AND DECISION OF THE BOARD

VI. **ADJOURNMENT**



85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

August 21, 2024

Portsmouth Technical Advisory Committee Attn: Peter Stith, Principal Planner 1 Junkins Avenue, Suite 3rd Floor Portsmouth, NH 03801

RE: Response Letter – Peer Review 635 Sagamore Ave, Portsmouth, NH Tax Map 222, Lot 19 JBE Project No. 18134.1

Dear Mr. Stith,

We are in receipt of comments from Eric Weinrieb, P.E., Altus Engineering dated June 4, 2024. Review comments are listed below with our responses in bold. In addition to the below comments, the City DPW requested two changes to the plans and drainage model at an on-site meeting with Mike Garrepy of 635 Sagamore Development, LLC on July 24th, 2024 while the new test pits were being dug.

It was recommended that the site and offsite contributing watershed area be modelled as Hydrologic Soil Group C rather than B. According to the site-specific soil survey performed on the subject parcel by Gove Environmental Services, Inc., the pervious areas of the subject parcel consist of two soil types: Chatfield-Hollis-Rock Outcrop complex and Chatfield Variant, both of which are classified as Hydrologic Soil Group B. However, it is our understanding that the Society of Soil Scientists of Northern New England is currently in the process of revising "Ksat Values for New Hampshire Soils," SSSNNE Special Publication No. 5, and that among the revisions, Chatfield will be classified as a HSG C soil moving forward. These changes are anticipated to take effect in the next year. For this reason, we agree with this approach of modelling the site watershed as HSG C. We consulted the project soil scientist, Jim Gove of Gove Environmental Services, Inc., and he agrees with this approach as well. Therefore, we have modelled the site watershed entirely as HSG C in both the pre- and post-construction conditions drainage analysis.

A new catch basin has been installed just to the south of the intersection between Sagamore Avenue and the Tidewatch Condominium roadway curb cut as part of the ongoing Sagamore Avenue roadway improvements. For this reason, DPW recommended that we mimic existing flow patterns to the extent possible. We have moved catch basins 101 and 102 to be just behind the driveway for Unit 1 to maintain existing drainage flow patterns.. The peak flow rate and volume toward both the Sagamore Avenue right of way and the back of the site is still reduced from the pre-construction condition with this change. Because of the addition of the proposed catch basin along the Sagamore Avenue gutter line, the water that reaches the Sagamore Avenue right of way from the subject parcel will be captured into a closed drainage system rather than be allowed to flow down the Tidewatch Condominium roadway and contribute to the existing drainage situation like it does currently.

Because the peak flow and runoff volumes toward the newly installed catch basin from the subject parcel are being decreased, and less impervious surface is proposed to drain toward it from the subject parcel in the post-construction condition, we anticipate that the City's drainage system is equipped to handle this. For this reason, the pollutant removal calculations that were provided within the drainage report in order to demonstrate compliance with Section 7.6.2.1(a) of the Site Plan Review Regulations have been revised to omit the on-site impervious surface that drains toward the Sagamore Avenue right of way and to only account for the runoff toward Analysis Points 3 and 4, which are different points along the Tidewatch Condominium roadway.

ALTUS COMMENTS:

- 1. Based on the observations, the test pits may not be correctly depicted on the plans. RESPONSE: The test pits have been survey located and are now shown in their correct locations.
- 2. The design is deficient test pits in the infiltration areas including both the stone drip edges and the infiltration pond. Additional pits will be required to demonstrate that infiltration is viable on this site. It is suggested that Altus witness the test pits to confirm the site conditions.

RESPONSE: Additional test pits were performed on July 24th, 2024 and witnessed by Dave Desfosses of the City DPW rather than Altus as recommended given time constraints and vacation schedules.

3. The NRCS soils report for Chatfield-Hollis-Rock Outcrop indicates that the KSAT value is very low, 0.00 in/hr. It is Altus' opinion that unless supported otherwise with test pits and infiltration tests, infiltration is not viable on this parcel.

RESPONSE: Infiltration tests have been performed and the existing soil on the site has a much higher saturated hydraulic conductivity than initially anticipated. Infiltration test results are included within the appendix of the revised drainage report. The proposed bioretention system is now modelled with an infiltration rate of 7.4 inches per hour because the material between the bottom of the coarse gravel layer and the seasonal high water table will be native. An infiltration rate of 0.3 inches per hour is still being used for the stone infiltration areas as the subgrade will be fill material.

4. Additional proposed spot grades are suggested to ensure that the transition from a super elevated roadway to a crowned roadway will properly drain.

RESPONSE: Additional spot grades have been added to the grading and drainage plan to ensure that this section of the roadway will properly drain.

5. The Developer is proposing buffer plantings in various locations on the site. The site has significant ledge outcrops that are not delineated on the plans. It is suggested that the ledge outcrops are shown on the plan to ensure that the natural features are being maintained and that the planting can be installed as depicted on the plans.

RESPONSE: Ledge outcrops are now shown on the plans. The proposed plantings in the vicinity of the ledge outcrops have been adjusted to go around the ledge outcrops rather than over them.



6. Proposed plantings are shown behind building units 1 and 2. There is mature vegetation in this area. The Designer and landscape architect should look at the existing vegetation to see if the existing buffer can be maintained and enhanced.

RESPONSE: Buffer plantings are proposed in order to enhance the existing vegetated buffer. Per Note #17 on the landscape plan, the contractor <u>shall</u> place plantings where necessary in order to enhance the existing wooded buffer and block visibility from Tidewatch Condominium property.

- 7. Based on the Cuomo report and Altus' observations, note 6 on Sheet C2 needs to be corrected. The 100-foot wetland buffer extends onto the property. The buffer should be depicted on the plans. RESPONSE: Brenden Walden, CWS, and Mike Cuomo, CWS, determined in the field that the wetlands on the Tidewatch Condominium property are well offsite. See attached letter from RCCD. It is apparent that the proposed disturbance is outside of the wetland buffer, because the proposed disturbance is approximately 100 feet from the far edge of pavement of the Tidewatch Condominium roadway at its closest point. Note #6 on Sheet C2 has been revised.
- 8. Units 3 and 4 are described as being walk out basements. It is presumed that units 3 and 4 will not have perimeter drains as the Designer is proposing to utilize stone drip edges for infiltration. The foundation/stone drip edge detail indicates that there are no perimeter drains for those units. It is unclear if units 1 and 2 will have basements and perimeter drains. Outlets for perimeter drains should be depicted on the plans.

RESPONSE: The stone drip edges are now proposed to be lined and underdrained to prevent infiltration to the perimeter drain. We are instead placing 3' of stone underneath the decks for Units 3 and 4 and routing the drip edge underdrains into the stone underneath the decks in order to infiltrate the roof water. This is not required for flow or volume reduction, but the stone is proposed for infiltration in order to meet the City of Portsmouth's stormwater pollutant removal requirement (Site Plan Review Regulations 7.6.2.1(a)).

All four units will need to have perimeter drains. However, foundation drain locations are typically determined by the building contractor and not shown on proposed development plans. It should be noted that the basements for the back two units are going to be almost entirely above the seasonal high water table.

9. It is unclear as to why a portion of the roadway turnaround area is within the limited common area for unit 3.

RESPONSE: The limited common area for Unit 3 has been revised to exclude the turnaround.

10. A portion of the retaining wall is within the common area of unit 4. The condominium documents should clearly indicate who is responsible for the maintenance of the retaining wall. RESPONSE: The limited common area lines for Unit 4 have been adjusted so that the retaining wall is in common area.

11. The Designer should check the north arrow on the Highway Access Plan.

RESPONSE: The north arrow on Sheet H1 has been revised for accuracy.



12. The plans indicate that the patios will be constructed using permeable pavers. The detail seems to indicate that the pavers will not be permeable. Additionally, the Designer needs to demonstrate that there is an adequate receiving area beneath the pavers to provide infiltration. RESPONSE: The note stating that the patios will be constructed using permeable pavers has been removed.

13. It appears that the north bound 244-foot stopping distance sight line intercepts the road surface. The Designer should check their design assumptions.

RESPONSE: The plans depict two different stopping sight distance lines in the northbound direction. One of these represents a 244-foot stopping sight line as recommended per AASHTO for a road with the slope of Sagamore Avenue in this location and an 85th percentile speed of 33 mph as was determined by Stephen Pernaw. We acknowledge that this cuts through the existing grade line. The other represents the 228 feet of stopping sight distance that is actually provided.

We have attached correspondence with Eric Eby, dated from December 2023 to February 2024, concerning the stopping sight lines at the intersection of Sagamore Avenue and the proposed driveway particularly in the northbound direction. Mr. Eby ultimately signed off on our proposal for a driveway with a stopping sight distance of 228 feet, given that the driveway is proposed in its optimal location and that this will be an improvement over the existing paved apron for the Luster King. We also considered placing the curb cut on the southern end of the subject parcel. From the southern end of the subject parcel, only 139 feet stopping sight distance would be available in the southbound direction. Mr. Eby stated in the enclosed email, dated February 23, 2024, that the driveway may meet the AASHTO recommended 244 feet of stopping sight distance after the Sagamore Avenue roadwork is completed, but that if it still comes short, then mitigation measures such as a blind driveway sign or an advisory speed plaque of 25 MPH could be added just to the south of the crest of the hill along the northbound travel lane.

14. It appears that the rim of the pond overflow structure is only 4.2-inches below the berm elevation. It does not appear that there is adequate freeboard. Additionally, the drainage computations indicate that the peak elevation in the 50-year storm event will be 62.85, less than 2-inches below the top of the berm.

RESPONSE: The rim of the overflow structure has been lowered in order to provide a foot of freeboard on the bioretention pond in the 50-year storm. The overflow rim will be one foot below the pond berm and the 50-year storm peak elevation will be equal to the elevation of the overflow rim. Additionally, the design infiltration rate has been increased to 7.4 inches per hour per the results of the infiltration tests in order to model the pond more accurately. This also helps us to achieve a foot of freeboard.

15. The notes on the anti-seep collar detail conflicts with locations shown on the plans. Clarification is needed.

RESPONSE: The Anti-Seep Collar detail states that anti-seep collars shall be placed 15' and 25' downstream of a culvert inlet unless otherwise specified, AND that they shall be placed on both sides of a clay core. The outlet culvert from the proposed bioretention pond, which passes through a clay core berm, is only 20' long. Therefore, anti-seep collars are proposed on both sides of the clay core berm. In our judgement there is no reason to place another one 5 feet from the outlet headwall.



16. It is presumed that the clay core berm will interface with exposed ledge. The detail should clearly note how the interface will be constructed to ensure that there is no seepage.

RESPONSE: Note #5 has been added to the clay core berm detail on Sheet D4, stating that ledge shall be removed to at least 2' outside of and below the clay core.

17. The Designer needs to confirm that their design intent is to have the top portion of the pond underdrain in the pea stone layer.

RESPONSE: The underdrain invert has been lowered so that the underdrain will be entirely within the coarse stone layer.

18. Catch basins should be installed off-line to be considered adequate for pre-treatment. RESPONSE: A sediment forebay has been added to the proposed bioretention pond for pre-treatment. Deep sumps for pre-treatment are no longer proposed.

PRE-DEVELOPMENT DRAINAGE ANALYSIS:

19. Pre-development subcatchment 1S needs to be amended to include all of the area upgradient to the south that discharges onto the site and into Sagamore Avenue.

RESPONSE: Pre-development subcatchment 1S has been amended to extend to the crest of the hill along Sagamore Avenue.

20. Based on the site conditions at the time of the visit, it appears that most of the area shown in subcatchment 2S is actually part of subcatchment 1S.

RESPONSE: The boundary between subcatchments 1S and 2S has been moved to the north in order to follow the high point.

21. The Designer should confirm the offsite contribution to subcatchment 4S.

RESPONSE: This has been reviewed in the field. We have made minor adjustments to subcatchment boundary as it is apparent that more of the ledge outcrop drains toward the subject parcel than we initially realized.

22. Due to the severity of the site grades, the Designer should consider limiting the Tc to 50-feet. Altus finds it curious that both pre-development subcatchment 2S and 3S have the same lengths for sheet flow.

RESPONSE: The sheet flow segments in each Tc path, both pre- and post-development, have been limited to 50 feet.

23. It is Altus' opinion that the longest flow path shown on the plans for both subcatchments 3S and 4S are underestimated. The Designer should confirm their assumptions.

RESPONSE: We ran other flow paths in HydroCAD and it turns out that our originally selected Tc paths for both of these subcatchments actually are the longest flow paths. The existing watershed plan shows the other candidate Tc paths within subcatchments 3S and 4S along with the resulting times of concentration. We have also reviewed and confirmed the modelled lengths and slopes for the Tc paths for both of these subcatchments.

24. Reach 1R is unnecessary and should be included as part of the longest flow path in subcatchment 3S.

RESPONSE: Reach 1R has been removed from the pre-construction drainage analysis and instead included as a Tc segment for Subcatchment 3S. It is included as a reach in the post-construction conditions analysis as Reach 8R, which is downstream of reaches 6R and 7R,



only because any overflow from the bioretention pond and from the stone under the decks for Units 3 and 4 is directed toward the swale. Subcatchment 3S is not directed toward Reach 8R in the post-construction drainage analysis and instead it is modelled as a Tc segment for the subcatchment.

25. The watershed plan indicates that the off-site topography is from NH Granit lidar. The plans should include the off-site topography for the portion of the Tidewatch condominium roadway and the northerly abutter's property.

RESPONSE: NH Granit lidar topography has been added for the portion of the Tidewatch Condominium roadway nearest the subject parcel and for the northerly abutter's property.

26. One of the project points of analysis should be the off-site catch basin on Tidewatch. RESPONSE: Analysis Point 4 is the off-site catch basin adjacent to the Tidewatch Condominium mailhouse.

27. Altus notes that the Tidewatch closed drainage system does not operate properly. Stormwater bypasses the culverts as the roadway and drainage system is not properly maintained.

RESPONSE: This is evident as confirmed in the field during a rainstorm on May 30, 2024. As such, runoff that reaches Analysis Point 1 (the location of the newly installed catch basin) in the existing condition analysis then follows a series of reaches representing the curb lines of Sagamore Avenue and of the Tidewatch Condominium roadway, bypassing the existing catch basins, and ending at Analysis Point 3 (the same water collection point along the Tidewatch Condominium Roadway toward which the proposed bioretention pond outlets). Effectively, all runoff that ends up in the Sagamore Avenue right of way from the subject parcel in the existing condition reaches the low point along the Tidewatch Condominium roadway because of the fact that the existing catch basins along the Tidewatch Condominium roadway were observed to not operate properly.

However, where a new catch basin is being installed in the gutter line of Sagamore Avenue just to the south of the intersection of Sagamore Avenue and the Tidewatch Condominium roadway, the runoff toward the Sagamore Avenue right of way (Analysis Point 1) is NOT routed to the Tidewatch water collection point (Analysis Point 3) in the post-construction conditions analysis. Instead, Analysis Point 1 represents the new catch basin in the post-construction conditions analysis.

28. Post Development drainage analysis will be reviewed after the predevelopment issues have been addressed.

RESPONSE: No response necessary.

29. Compliance with Section 7.2 of the Site Plan Review Regulations will be completed upon receipt of revised plans and documents.

RESPONSE: No response necessary.



Included with this response letter are the following:

- 1. One (1) Full Size Revised Plan Set.
- 2. One (1) Drainage Analysis (Infiltration Test Results Enclosed).
- 3. Updated Test Pit Log.
- 4. Email Chain between JBE and Eric Eby regarding stopping sight distance, last message dated February 23, 2024.
- 5. RCCD Offsite Wetland Letter.
- 6. Dave Desfosses Email dated July 25, 2024.

Thank you very much for your time.

Very truly yours,

JONES & BEACH ENGINEERS, INC.

Daniel Meditz, P.E.

Project Engineer

Eric Weinrieb, P.E., Altus Engineering (via email and hand delivered) cc:

Michael Garrepy (via email)





City of Portsmouth, New Hampshire Site Plan Application Checklist

This site plan application checklist is a tool designed to assist the applicant in the planning process and for preparing the application for Planning Board review. The checklist is required to be completed and uploaded to the Site Plan application in the City's online permitting system. A preapplication conference with a member of the planning department is strongly encouraged as additional project information may be required depending on the size and scope. The applicant is cautioned that this checklist is only a guide and is not intended to be a complete list of all site plan review requirements. Please refer to the Site Plan review regulations for full details.

Applicant Responsibilities (Section 2.5.2): Applicable fees are due upon application submittal along with required attachments. The application shall be complete as submitted and provide adequate information for evaluation of the proposed site development. Waiver requests must be submitted in writing with appropriate justification.

Name of Applicant: 635 Sagamore Development, LLC	_ Date Submitted:3/18/	24	
Application # (in City's online permitting):LU-24-34			
Site Address: 635 Sagamore Avenue		Map: 222 Lot: 19	

	Application Requirements			
$\overline{\mathbf{A}}$	Required Items for Submittal	Item Location (e.g. Page or Plan Sheet/Note #)	Waiver Requested	
X	Complete <u>application</u> form submitted via the City's web-based permitting program (2.5.2.1(2.5.2.3A)		N/A	
X	All application documents, plans, supporting documentation and other materials uploaded to the application form in viewpoint in digital Portable Document Format (PDF). One hard copy of all plans and materials shall be submitted to the Planning Department by the published deadline. (2.5.2.8)		N/A	

	Site Plan Review Application Required Information			
$\overline{\mathbf{A}}$	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested	
	Statement that lists and describes "green" building components and systems. (2.5.3.1B)	Pending		
X	Existing and proposed gross floor area and dimensions of all buildings and statement of uses and floor area for each floor. (2.5.3.1C)	Architectural Plans	N/A	
X	Tax map and lot number, and current zoning of all parcels under Site Plan Review. (2.5.3.1D)	Cover Sheet & Sheet C2	N/A	

	Site Plan Review Application Required Information			
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested	
X	Owner's name, address, telephone number, and signature. Name, address, and telephone number of applicant if different from owner. (2.5.3.1E)	Cover Sheet	N/A	
X	Names and addresses (including Tax Map and Lot number and zoning districts) of all direct abutting property owners (including properties located across abutting streets) and holders of existing conservation, preservation or agricultural preservation restrictions affecting the subject property. (2.5.3.1F)	Cover Sheet	N/A	
X	Names, addresses and telephone numbers of all professionals involved in the site plan design. (2.5.3.1G)	Cover Sheet	N/A	
X	List of reference plans. (2.5.3.1H)	C1	N/A	
X	List of names and contact information of all public or private utilities servicing the site. (2.5.3.1)	Cover Sheet	N/A	

	Site Plan Specifications		
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
X	Full size plans shall not be larger than 22 inches by 34 inches with match lines as required, unless approved by the Planning Director (2.5.4.1A)	Required on all plan sheets	N/A
X	Scale: Not less than 1 inch = 60 feet and a graphic bar scale shall be included on all plans. (2.5.4.1B)	Required on all plan sheets	N/A
X	GIS data should be referenced to the coordinate system New Hampshire State Plane, NAD83 (1996), with units in feet. (2.5.4.1C)	C1, Note #3	N/A
X	Plans shall be drawn to scale and stamped by a NH licensed civil engineer. (2.5.4.1D)	Required on all plan sheets	N/A
Х	Wetlands shall be delineated by a NH certified wetlands scientist and so stamped. (2.5.4.1E)	None Observed, Wetland Delineation Report Include	N/A
X	Title (name of development project), north point, scale, legend. (2.5.4.2A)	Cl	N/A
X	Date plans first submitted, date and explanation of revisions. (2.5.4.2B)	All Sheets	N/A
X	Individual plan sheet title that clearly describes the information that is displayed. (2.5.4.2C)	Required on all plan sheets	N/A
×.	Source and date of data displayed on the plan. (2.5.4.2D)	Cl	N/A

	Site Plan Specifications – Required Exhibits and Data			
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested	
	 Existing Conditions: (2.5.4.3A) Surveyed plan of site showing existing natural and built features; Existing building footprints and gross floor area; Existing parking areas and number of parking spaces provided; Zoning district boundaries; Existing, required, and proposed dimensional zoning requirements including building and open space coverage, yards and/or setbacks, and dwelling units per acre; Existing impervious and disturbed areas; Limits and type of existing vegetation; Wetland delineation, wetland function and value assessment (including vernal pools); SFHA, 100-year flood elevation line and BFE data, as required. 	C1		
K	 2. Buildings and Structures: (2.5.4.3B) Plan view: Use, size, dimensions, footings, overhangs, 1st fl. elevation; Elevations: Height, massing, placement, materials, lighting, façade treatments; Total Floor Area; Number of Usable Floors; Gross floor area by floor and use. 	Architectural Plans		
X	 3. Access and Circulation: (2.5.4.3C) Location/width of access ways within site; Location of curbing, right of ways, edge of pavement and sidewalks; Location, type, size and design of traffic signing (pavement markings); Names/layout of existing abutting streets; Driveway curb cuts for abutting prop. and public roads; If subdivision; Names of all roads, right of way lines and easements noted; AASHTO truck turning templates, description of minimum vehicle allowed being a WB-50 (unless otherwise approved by TAC). 	C2 T1-T2		
x	 4. Parking and Loading: (2.5.4.3D) Location of off street parking/loading areas, landscaped areas/buffers; Parking Calculations (# required and the # provided). 	C2, Note #3		
X	 Water Infrastructure: (2.5.4.3E) Size, type and location of water mains, shut-offs, hydrants & Engineering data; Location of wells and monitoring wells (include protective radii). 	C4		
	Sewer Infrastructure: (2.5.4.3F) Size, type and location of sanitary sewage facilities & Engineering data, including any onsite temporary facilities during construction period.	C4 & P2		

X	7. Utilities: (2.5.4.3G)	
	• The size, type and location of all above & below ground utilities;	
	Size type and location of generator pads, transformers and other	C4
	fixtures.	
X	8. Solid Waste Facilities: (2.5.4.3H)	C2, Note #22
		C2, NOCE #22
	The size, type and location of solid waste facilities.	
Х	9. Storm water Management: (2.5.4.3I)	
	 The location, elevation and layout of all storm-water drainage. 	Snow Storage - C2
	 The location of onsite snow storage areas and/or proposed off- 	
	site snow removal provisions.	Everything Else - C3
	 Location and containment measures for any salt storage facilities 	
	Location of proposed temporary and permanent material storage	
	locations and distance from wetlands, water bodies, and	
-	stormwater structures.	
X	10. Outdoor Lighting: (2.5.4.3J)	
	Type and placement of all lighting (exterior of building, parking lot	L2
_	and any other areas of the site) and photometric plan.	
X	11. Indicate where dark sky friendly lighting measures have	Everywhere
-	been implemented. (10.1)	-
x	12. Landscaping: (2.5.4.3K)	
	Identify all undisturbed area, existing vegetation and that	L1
	which is to be retained;	
	 Location of any irrigation system and water source. 	
X	13. Contours and Elevation: (2.5.4.3L)	
	 Existing/Proposed contours (2 foot minimum) and finished 	C3
	grade elevations.	
X	14. Open Space: (2.5.4.3M)	
	 Type, extent and location of all existing/proposed open space. 	C2, Note #2
	AT AN	
	15. All easements, deed restrictions and non-public rights of	N/A
	ways. (2.5.4.3N)	
	16. Character/Civic District (All following information shall be	
	included): (2.5.4.3P)	N/A
	 Applicable Building Height (10.5A21.20 & 10.5A43.30); 	N/A
	Applicable Special Requirements (10.5A21.30); Applicable Special Requirements (10.5A21.30);	
	Proposed building form/type (10.5A43); (10.5A43);	
1	 Proposed community space (10.5A46). 	
	17 Special Flood Harrard Areas (2 F 4 20)	
	 17. Special Flood Hazard Areas (2.5.4.3Q) The proposed development is consistent with the need to 	
	minimize flood damage;	
	All public utilities and facilities are located and construction to	N/A
	minimize or eliminate flood damage;	
	Adequate drainage is provided so as to reduce exposure to	
	flood hazards.	
\Box	The seal of section 2	

	Other Required Information			
\square	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested	
Х	Traffic Impact Study or Trip Generation Report, as required. (3.2.1-2)	Included with Submissio	n	
X	Indicate where Low Impact Development Design practices have been incorporated. (7.1)	СЗ		
X	Indicate whether the proposed development is located in a wellhead protection or aquifer protection area. Such determination shall be approved by the Director of the Dept. of Public Works. (7.3.1)	C2, Note #23		
Х	Stormwater Management and Erosion Control Plan. (7.4)	Included with Submissio	n	
X	Inspection and Maintenance Plan (7.6.5)	Included with Submission	1	

	Final Site Plan Approval Required Information			
V	Required Items for Submittal	Item Location V (e.g. Page/line or Rec Plan Sheet/Note #)		
X	All local approvals, permits, easements and licenses required, including but not limited to: • Waivers; • Driveway permits; • Special exceptions; • Variances granted; • Easements; • Licenses. (2.5.3.2A)	C2, Note # 4 & 5		
X	Exhibits, data, reports or studies that may have been required as part of the approval process, including but not limited to: Calculations relating to stormwater runoff; Information on composition and quantity of water demand and wastewater generated; Information on air, water or land pollutants to be discharged, including standards, quantity, treatment and/or controls; Estimates of traffic generation and counts pre- and post-construction; Estimates of noise generation; A Stormwater Management and Erosion Control Plan; Endangered species and archaeological / historical studies; Wetland and water body (coastal and inland) delineations; Environmental impact studies. (2.5.3.2B)	Included with Submissi	on	
X	A document from each of the required private utility service providers indicating approval of the proposed site plan and indicating an ability to provide all required private utilities to the site. (2.5.3.2D)	Pending		

	Final Site Plan Approval Required Information				
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested		
X	A list of any required state and federal permit applications required for the project and the status of same. (2.5.3.2E)	C2, Note #5			
X	A note shall be provided on the Site Plan stating: "All conditions on this Plan shall remain in effect in perpetuity pursuant to the requirements of the Site Plan Review Regulations." (2.5.4.2E)	C2, Note #21	N/A		
X	For site plans that involve land designated as "Special Flood Hazard Areas" (SFHA) by the National Flood Insurance Program (NFIP) confirmation that all necessary permits have been received from those governmental agencies from which approval is required by Federal or State law, including Section 404 of the Federal Water Pollution Control Act Amendments of 1972, 33 U.S.C. 1334. (2.5.4.2F)	N/A			
X	Plan sheets submitted for recording shall include the following notes: a. "This Site Plan shall be recorded in the Rockingham County Registry of Deeds." b. "All improvements shown on this Site Plan shall be constructed and maintained in accordance with the Plan by the property owner and all future property owners. No changes shall be made to this Site Plan without the express approval of the Portsmouth Planning Director." (2.13.3)	C2, Note #19 & 20	N/A		

Book: 6332 Page: 1158

Return to:

E # 21060614 09/24/2021 09:32:59 AM Book 6332 Page 1158 Page 1 of 2

Register of Deeds, Rockingham County

LCHIP ROA585829 TRANSFER TAX R0109828

25.00 5.807.00 14.00

RECORDING SURCHARGE

WARRANTY DEED

KNOW ALL BY THESE PRESENTS, that I, WILLIAM A. HINES, married person, TRUSTEE OF THE WILLIAM A. HINES FAMILY REVOCABLE TRUST a/k/a The Hines Family Revocable Trust of 2006, of 635 Sagamore Avenue, Portsmouth, New Hampshire 03801, for consideration paid. hereby grant to 635 SAGAMORE DEVELOPMENT, LLC, a New Hampshire limited liability company with a mailing address of 3612 Lafayette Road, Dept. 4, Portsmouth, New Hampshire 03801 with WARRANTY COVENANTS, the following described premises:

A certain tract of land with the buildings thereon, situate on Sagamore Avenue in said Portsmouth, more particularly described as follows:

Beginning at a point on Sagamore Avenue at land now or formerly of Arnold, thence running Westerly by said Arnold land three hundred (300) feet, more or less, to land now or formerly of W.W. and D.M. Johnston; thence turning and running Northwesterly by said Johnston land one hundred and twentyfour (124) feet; thence turning and running Northerly also by said Johnston land one hundred sixtytwo (162) feet to land now or formerly of C.W. Walker; thence turning and running Easterly by said Walker land four hundred nineteen (419) feet to Sagamore Avenue; thence turning and running Easterly one hundred forty (140) feet; thence turning and running along said Sagamore Avenue thirty (30) feet to land of one Smith; thence turning and running Westerly one hundred forty (140) feet; thence turning and running Southerly ninety (90) feet; thence turning and running Easterly one hundred forty (140) feet to Sagamore Avenue; the last three bounds being land of Smith; thence turning running Southerly by said Sagamore Avenue one hundred sixty (160) feet to the point of beginning.

EXCEPTING AND RESERVING to the said William A. Hines and his wife Bonnie Hines a life estate in the above-described property permitting them to reside in the existing residential apartment on the property for the remainder of William A. Hines natural life, plus one year unless Bonne Hines shall have predeceased.

Meaning and intending to convey the same premises conveyed to the Grantor by deed of William A. Hines dated February 11, 2008 and recorded in the Rockingham County Registry of Deeds at Book 4885, Page 1538.

BY SIGNING BELOW, William A. Hines and Bonnie Hines release all homestead rights to the Premises.

Book: 6332 Page: 1159

TRUSTEE CERTIFICATE

I, William A. Hines, Trustee of the William A. Hines Family Revocable Trust A/K/A The Hines Family Revocable Trust of 2006, hereby covenant that said Trust is duly organized under the laws of the State of New Hampshire; that I am the sole trustee pursuant to said Declaration of Trust; that said Trust is still in full force and effect; that I have the power thereunder to convey as aforesaid; and that, in making this conveyance, I have, in all respects, acted pursuant to the authority vested in and granted to me therein and no purchaser or third party shall be bound to inquire whether the Trustee has said power or are properly exercising said power or to see to the application of any trust assets paid to the Trustee for a conveyance thereof.

Signed this 3rd day of September, 2021.

William A. Hines, Trustee of the William A. Hines Family Revocable Trust A/K/A The Hines Family Revocable Trust of 2006

Bonnie Hines

STATE OF NEW HAMPSHIRE COUNTY OF ROCKINGHAM

On this, the 3rd day of September, 2021, before me, the undersigned Officer, personally appeared William A. Hines, Trustee of the William A. Hines Family Revocable Trust A/K/A The Hines Family Revocable Trust of 2006, known to me, or satisfactorily proven, to be the person whose name is subscribed to the foregoing instrument, and acknowledged that he executed the same for the purposes set forth therein.

Justice of the Peace/Notary Public My commission expires:

AMMINITAL.

COMMISSION EXPIRES

COMMISSION

STATE OF NEW HAMPSHIRE COUNTY OF ROCKINGHAM

On this, the 3rd day of September, 2021, before me, the undersigned Officer, personally appeared Bonnie Hines, known to me, or satisfactorily proven, to be the person whose name is subscribed to the foregoing instrument, and acknowledged that she executed the same for the purposes set forth the resignation.

ustice of the Peace/Notary Public

My commission expires:

< Sagamore A... Save □ :

Letter of Authorization

635 Sagamore Development, LLC, owner of property located at 635 Sagamore Avenue in Portsmouth, NH, known as Tax Map 222, Lot 19, do hereby authorize Jones & Beach Engineers, Inc. ("JBE"), Garrepy Planning Consultants, LLC ("GPC"), and Hoefle, Phoenix, Gormley & Roberts, PLLC ("HPGR") to act on its behalf concerning the previously mentioned property.

I hereby appoint JBE, GPC and HPGR as agents to act on behalf of 635 Sagamore Development, LLC in the Planning Board and Zoning Board application process, to include any required signatures.

635 Sagamore Development, LLC

Timothy L. Black, Duly Authorized

January 5, 2022 Date









GOVE ENVIRONMENTAL SERVICES, INC. TEST PIT DATA

Project 635 Sagamore Ave

Client 635 Sagamore Development LLC

GES Project No. GES 2021307

MM/DD/YY Staff 3-18-2022 JPG

Test Pit No. 1

ESHWT: n/a

Termination @ 15"

Refusal: 15" SCS Soil: Hollis

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0-5" **NONE FSL** GR 10YR 3/2 FR **NONE** 5-15" 10YR 5/6 **FSL** GR FR

Test Pit No. 2

ESHWT: n/a

Termination @ 25"

Refusal: 25" SCS Soil: Chatfield

Obs. Water: none

Redox; Quantity/Contrast Depth Color Texture Structure Consistence 0-5" 10YR 3/2 **FSL** GR FR **NONE** 5-25" **FSL** GR FR **NONE** 10YR 5/6

Test Pit No. 3

ESHWT: n/a

Termination @ 25"

Refusal: 25" SCS Soil: Chatfield

Obs. Water: none

Depth Color **Texture** Structure Consistence Redox; Quantity/Contrast 0-6" 10YR 3/2 **FSL** GR FR **NONE** NONE 6-25" **FSL** GR FR 10YR 5/6

Hollis

Test Pit No. 4

ESHWT: n/a

Termination @ 15"

Refusal: 15" SCS Soil:

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0–15" 10YR 3/2 FSL GR FR NONE

Test Pit No. 5

ESHWT: 30"

Termination @ 36"

Refusal: 36" SCS Soil: Chatfield variant

Obs. Water: none

Depth Texture Structure Consistence Redox; Quantity/Contrast Color 0-8" **NONE** 10YR 3/2 **FSL** GR FR 8-30" 10YR 4/6 **FSL** GR FR **NONE** 30-36" 2.5Y 5/3 **FSL** GR FR 10% Distinct

Test Pit No. 6

ESHWT: n/a

Termination @ 12"

Refusal: 12" SCS Soil: Hollis

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0–12" 10YR 3/2 FSL GR FR NONE

Test Pit No. 7

ESHWT: n/a

Termination @ 27"

Refusal: 27" SCS Soil: Chatfield

Obs. Water: none

Depth Texture Structure Redox; Quantity/Contrast Color Consistence 0-4" 10YR 3/2 **FSL** GR FR **NONE** 4-27" 10YR 5/6 **FSL** GR FR **NONE**

Test Pit No. 8

ESHWT: 35"

Termination @ 40"

Refusal: 40" Obs. Water: none SCS Soil:

Chatfield variant

Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-6"	10YR 3/2	FSL	GR	FR	NONE
6-35"	10YR 5/6	FSL	GR	FR	NONE
35–40"	2.5Y 5/3	FSL	OM	FI	10% Distinct

Test Pit No. 9

ESHWT: n/a

Termination @ 27"

Refusal: 27" Obs. Water: none SCS Soil:

Chatfield

Scituate

Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-4"	10YR 3/2	FSL	GR	FR	NONE
4–27"	10YR 5/6	FSL	GR	FR	NONE

Test Pit No. 10

ESHWT: 35

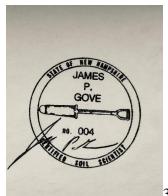
Termination @ 62"

Refusal: 62"

Obs. Water: none

Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-10"	10YR 3/2	FSL	GR	FR	NONE
10-35"	10YR 5/6	FSL	GR	FR	NONE
35–62"	2.5Y 5/3	FSL	PL	FI	10%. Distinct

SCS Soil:



Legend:

FSL = fine sandy loam GR = granular PL = platy FI = firm



GOVE ENVIRONMENTAL SERVICES, INC.

TEST PIT DATA

Project 635 Sagamore Ave., Portsmouth NH Client 635 Sagamore Development LLC

GES Project No. 2021308

MM/DD/YY Staff 07-24-2024 James Gove, CSS#004

Witnessed by: David Desfosses, City of Portsmouth

Test Pit No. Soils Series: Udorthents 11 ESHWT:: none Landscape: Paved Termination @ 32" Slope:

32" Parent Material: Refusal: Fill over till Obs. Water: None Hydrologic Soil Group: Impervious

Horizon Color (Munsell) Texture Structure-Consistence-Redox

Fill 1, 0-8" 10YR4/4 fine sandy loam massive-friable-none Fill 2, 8-19" 10YR2/1 ground pavement massive-firm-none Bw 18-32" 10YR5/6 fine sandy loam granular-friable-none

Test Pit No. **12** Soils Series: Chatfield ESHWT:: Hillside none Landscape: Termination @ 28" Slope: \mathbf{C}

Parent Material: Refusal: 28" Bedrock Till

Obs. Water: None Hydrologic Soil Group: В

Color (Munsell) Texture Structure-Consistence-Redox Horizon

A 0-6" 10YR3/2 fine sandy loam granular-friable-none granular-friable-none Bw 6-28" 10YR5/6 fine sandy loam

Bedrock ranges from 20" to 28" in test pit.

Test Pit No.13Soils Series:ChatfieldESHWT::noneLandscape:HillsideTermination @36"Slope:C

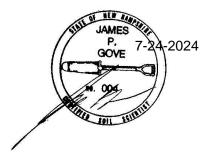
Refusal: 36" Parent Material: Bedrock Till

Obs. Water: None Hydrologic Soil Group: B

Horizon Color (Munsell) Texture Structure-Consistence-Redox fine sandy loam granular-friable-none A 0-6" 10YR3/2 Bw 6-24" 10YR4/6 fine sandy loam granular-friable-none C 24-36" fine sandy loam granular-friable-none 2.5Y5/3

Bedrock ranges from 24" to 36" in test pit.

Note: Site should be calculated as HSG C, due to the limited infiltration in thin soil layers above the bedrock.



Test Pit Data: 635 Sagamore Ave. 7-24-2024 —Page 4 of 4

Daniel Meditz

From: Eric B. Eby <ebeby@cityofportsmouth.com>

Sent: Friday, February 23, 2024 9:06 AM

To: Daniel Meditz; Joseph Coronati; Zachary M. Cronin; Dave J. Desfosses

Cc: Mike Garrepy (mgarrepy@gmail.com); Steve Pernaw

Subject: RE: 18134.1 - Luster Cluster, Sight Distance

You don't often get email from ebeby@cityofportsmouth.com. Learn why this is important

Daniel

I've had a chance to review the Green Book section on sight distance and I am fine with your calcs and explanation. As described in the Green Book, stopping sight distance is broken into two portions. One is the distance traveled during the brake reaction time and the second is the distance to brake the vehicle to a stop. At 33 mph, the brake reaction distance is 121 feet, meaning that with a sight distance of 228 feet, 107 feet remains to bring the vehicle to a stop. This is approximately the 100 feet that is being assumed in this case, so I am fine with your calculations. As the sight distance is very close to the minimum requirement, there is a chance it may meet the minimum requirements after the City finishes the roadwork planned for this year. I would recommend checking it again after the roadwork is complete and if still short on the sight line, then I would recommend the installation of an advance warning sign for BLIND DRIVEWAY with a supplementary advisory speed plaque of 25 MPH.

Best,

Eric

Eric B. Eby, P.E.

City Engineer – Parking, Transportation, and Planning Department of Public Works
City of Portsmouth
680 Peverly Hill Road
Portsmouth, NH 03801
(603) 766-1415
Cell (603)-815-1761

From: Daniel Meditz < DMeditz@jonesandbeach.com>

Sent: Wednesday, February 21, 2024 8:51 AM

To: Eric B. Eby <ebeby@cityofportsmouth.com>; Joseph Coronati <jcoronati@Jonesandbeach.com>; Zachary M. Cronin

<zmcronin@cityofportsmouth.com>; Dave J. Desfosses <djdesfosses@cityofportsmouth.com>

Cc: Mike Garrepy (mgarrepy@gmail.com) <mgarrepy@gmail.com>; Steve Pernaw <sgp@pernaw.com>

Subject: RE: 18134.1 - Luster Cluster, Sight Distance

Eric,

The 100 feet braking distance was an approximation after consulting with Steve Pernaw, who is copied on this email. The only thing it really effects in terms of our analysis is that the slope we used to determine the required stopping sight distance is based on the average slope for the first 100' along the approach.

Thanks,

Daniel Meditz, P.E.

Lead Design Engineer

JONES&BEACH ENGINEERS, INC.

85 Portsmouth Avenue PO Box 219 Stratham, NH 03885 (603) 772-4746 (ext. #128) http://www.jonesandbeach.com

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From: Eric B. Eby < <u>ebeby@cityofportsmouth.com</u>>

Sent: Friday, February 16, 2024 3:43 PM

To: Daniel Meditz <DMeditz@jonesandbeach.com>; Joseph Coronati <jcoronati@Jonesandbeach.com>; Zachary M.

Cronin < cronin@cityofportsmouth.com">com; Dave J. Desfosses < djdesfosses@cityofportsmouth.com> cc: Mike Garrepy@gmail.com">cc: Mike Garrepy@gmail.com; Steve Pernaw < sgp@pernaw.com>

Subject: RE: 18134.1 - Luster Cluster, Sight Distance

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Daniel

Thank you for the explanation and revised plans. I think we are very close. I want to check on the 100-foot assumption of when vehicles apply their brakes. Is that guidance from the Green Book or just an assumption on your part? That distance would seem to depend on their speed. I think they may be applying the brakes sooner, and on the northbound approach they may still be going uphill, which could reduce the required sight distance needed and allow the minimum sight line to be provided.

For a vehicle waiting to turn out of the driveway onto Sagamore, they need to be able to see the minimum stopping sight distance to the south, which, if the driver's eye is at 69 feet, would appear to be sufficient, even for the sight line as currently calculated. This is based on my rough drawing of lines on my computer screen. That can be checked once we agree on what the sight distance should be for the northbound approach.

I agree it will be an improvement over existing conditions, but I would prefer that we do all we can to meet or exceed the required minimums.

I am out of the office this afternoon, so I don't have access to the Green Book or my other materials on sight distance. I will check them when I return on Tuesday.

Eric B. Eby, P.E.

City Engineer – Parking, Transportation, and Planning Department of Public Works
City of Portsmouth
680 Peverly Hill Road
Portsmouth, NH 03801
(603) 766-1415
Cell (603)-815-1761

From: Daniel Meditz < <u>DMeditz@jonesandbeach.com</u>>

Sent: Thursday, February 15, 2024 3:44 PM

To: Eric B. Eby <<u>ebeby@cityofportsmouth.com</u>>; Joseph Coronati <<u>jcoronati@Jonesandbeach.com</u>>; Zachary M. Cronin <<u>zmcronin@cityofportsmouth.com</u>>; Dave J. Desfosses <<u>djdesfosses@cityofportsmouth.com</u>>

Cc: Mike Garrepy (mgarrepy@gmail.com) < mgarrepy@gmail.com>; Steve Pernaw < sgp@pernaw.com>

Subject: RE: 18134.1 - Luster Cluster, Sight Distance

Eric,

Thank you for reviewing. The profile I was showing actually reflected the grade of the centerline of Sagamore Avenue where I had the stationing, though I can see the confusion as I had the sight line itself thick, dashed and in red. I inverted the color scheme for those but I am still showing the line of sight from the driveway as a solid line. Second, I switched the profile from being along the centerline of the road to the centerline of each lane. Third, I am no longer accounting for the driveway grade in the stopping sight distance profile – As you said, that will impact intersection sight distance but not stopping sight distance.

I have updated the plans and report accordingly. Let me know if you have any more questions or comments.

Thanks,

Daniel Meditz, P.E.

Lead Design Engineer

JONES&BEACH ENGINEERS, INC.

85 Portsmouth Avenue PO Box 219 Stratham, NH 03885 (603) 772-4746 (ext. #128) http://www.jonesandbeach.com

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From: Eric B. Eby < ebeby@cityofportsmouth.com>

Sent: Thursday, February 15, 2024 2:07 PM

To: Daniel Meditz <DMeditz@jonesandbeach.com>; Joseph Coronati <jcoronati@Jonesandbeach.com>; Zachary M.

Cronin < cronin@cityofportsmouth.com">com; Dave J. Desfosses < djdesfosses@cityofportsmouth.com cc: Mike Garrepy@gmail.com">cc: Mike Garrepy@gmail.com sgp@pernaw.com com com step

Subject: RE: 18134.1 - Luster Cluster, Sight Distance

Daniel

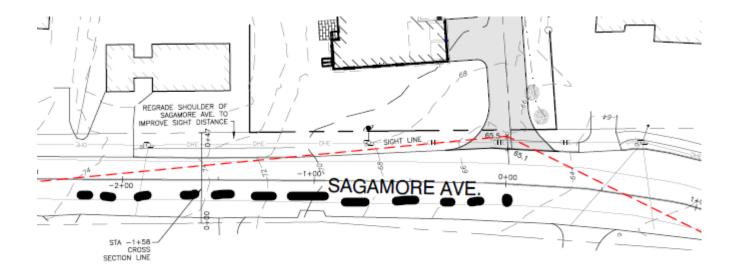
Looking at the plans, it appears that the sight line was plotted along the red dashed line. However, this line would represent the intersection sight line and not the stopping sight line. The 2-foot object height for stopping sight distance needs to be at a point in the travel lane, not at a point 14.5 feet from the edge of the travel lane. Stopping sight distance is for approaching vehicles to be able to see and react to a vehicle stopped in Sagamore Ave waiting to turn left into the site driveway. I don't know how much of a difference, if any, the location of the 2-foot object will have on the sight lines, but it needs to be shown and the report updated to reflect the proper location.

The black dotted line in the figure below illustrates where the 2-foot object should be located.

Let me know if you have any questions.

Best,

Eric



Eric B. Eby, P.E.

City Engineer – Parking, Transportation, and Planning Department of Public Works City of Portsmouth 680 Peverly Hill Road Portsmouth, NH 03801 (603) 766-1415 Cell (603)-815-1761

From: Daniel Meditz < <u>DMeditz@jonesandbeach.com</u>>

Sent: Wednesday, February 14, 2024 8:58 AM

To: Eric B. Eby < ebeby@cityofportsmouth.com; Joseph Coronati < jcoronati@Jonesandbeach.com; Zachary M. Cronin

<zmcronin@cityofportsmouth.com>; Dave J. Desfosses <djdesfosses@cityofportsmouth.com>

Cc: Mike Garrepy (mgarrepy@gmail.com) < mgarrepy@gmail.com>; Steve Pernaw < sgp@pernaw.com>

Subject: RE: 18134.1 - Luster Cluster, Sight Distance

Eric,

Please see attached technical report and revised sight distance plans. The northern curb cut would provide us with the best sight distance. Please review and let us know if you have any questions.

Thanks,

Daniel Meditz, P.E.

Lead Design Engineer

JONES&BEACH ENGINEERS, INC.

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From: Eric B. Eby < ebeby@cityofportsmouth.com>

Sent: Wednesday, January 3, 2024 12:03 PM

 $\textbf{To:} \ Joseph\ Coronati \\ @ Jones and beach.com \\ >; \ Zachary\ M.\ Cronin \\ < \underline{zmcronin@cityofportsmouth.com} \\ >; \ Dave\ J.$

Desfosses <djdesfosses@cityofportsmouth.com>

Cc: Mike Garrepy (mgarrepy@gmail.com) <mgarrepy@gmail.com>; Steve Pernaw <sgp@pernaw.com>; Daniel Meditz

<DMeditz@jonesandbeach.com>

Subject: RE: 18134.1 - Luster Cluster, Sight Distance

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Joe,

Thank you for the updated plans.

Looking at the sight lines, <u>neither driveway location has adequate Stopping Sight distance under current conditions</u>. Due to the existing grade of the driveway at 695 Sagamore, we wouldn't be able to lower the top of the hill on Sagamore more than a few inches. While you might want to look and determine if it is possible to raise your driveway a bit to improve Intersection Sight lines, a profile adjustment of Sagamore is most likely the key to providing adequate Stopping Sight distance. Raising Sagamore a bit near the driveway should also be looked at to see if it is feasible without acquiring easements.

Stopping Sight distance is the critical requirement, whereas Intersection Sight distance is desirable but at a minimum must at least equal the Stopping Sight distance. With that in mind, the Option 2 location would appear to have more of a chance of meeting Stopping Sight line requirements if the profile of the roadway could be modified sufficiently. I would suggest that you develop a profile of Sagamore Ave that will provide the minimum Stopping Sight distance at the Option 2 location and then we can review that with our design consultant to determine if it is feasible.

Eric B. Eby, P.E.

City Engineer – Parking, Transportation, and Planning Department of Public Works
City of Portsmouth
680 Peverly Hill Road
Portsmouth, NH 03801
(603) 766-1415
Cell (603)-815-1761

From: Joseph Coronati < jcoronati@Jonesandbeach.com>

Sent: Wednesday, January 3, 2024 10:06 AM

To: Eric B. Eby <<u>ebeby@cityofportsmouth.com</u>>; Zachary M. Cronin <<u>zmcronin@cityofportsmouth.com</u>>; Dave J.

Desfosses <didesfosses@cityofportsmouth.com>

Cc: Mike Garrepy (mgarrepy@gmail.com>; Steve Pernaw <sgp@pernaw.com>; Daniel Meditz DMeditz@jonesandbeach.com>

Subject: Re: 18134.1 - Luster Cluster, Sight Distance

Eric,

Hope you had a good holiday. Was wondering if you have had a chance to review this.

thanks

Joseph Coronati
Vice President
Jones & Beach Engineers, Inc.
85 Portsmouth Avenue
PO Box 219
Stratham, NH 03885
(603) 772-4746 (ext. #114)
jcoronati@jonesandbeach.com
http://www.jonesandbeach.com

From: Joseph Coronati

Sent: Thursday, December 21, 2023 1:28:06 PM

To: Eric B. Eby <ebeby@cityofportsmouth.com>; Zachary M. Cronin <zmcronin@cityofportsmouth.com>; Dave J.

Desfosses <djdesfosses@cityofportsmouth.com>

Cc: Mike Garrepy (mgarrepy@gmail.com) <mgarrepy@gmail.com>; Steve Pernaw <sgp@pernaw.com>; Daniel Meditz

<DMeditz@jonesandbeach.com>

Subject: RE: 18134.1 - Luster Cluster, Sight Distance

Eric,

Here's the modified plans and the speed study that Steve Pernaw did for the site. Let us know if you want to have a quick Teams meeting to determine the best driveway location.

Thanks

Joseph Coronati

Vice President

JONES&BEACH ENGINEERS, INC.

85 Portsmouth Avenue PO Box 219 Stratham, NH 03885 (603) 772-4746 (ext. #114) jcoronati@jonesandbeach.com http://www.jonesandbeach.com

From: Eric B. Eby < ebeby@cityofportsmouth.com>

Sent: Thursday, December 7, 2023 12:47 PM

To: Joseph Coronati < <u>icoronati@Jonesandbeach.com</u>>; Zachary M. Cronin < <u>zmcronin@cityofportsmouth.com</u>>; Dave J.

Desfosses < djdesfosses@cityofportsmouth.com >

Cc: Mike Garrepy (mgarrepy@gmail.com) <mgarrepy@gmail.com>

Subject: RE: 18134.1 - Luster Cluster, Sight Distance

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Joe

Thank you for the plans and the update. Looking quickly at the profile plans, you have provided plans for both Intersection Sight Distance (ISD) on Sheet H1 and Stopping Sight Distance (SSD) on Sheet H2. ISD is for vehicles turning out of the driveway. SSD is for vehicles approaching the driveway on Sagamore Ave. The ISD appears to be plotted correctly. However, in the case of SSD, the 3.5-foot driver height should be a 2-foot object height. Revising the plans

with the 2-foot object height is needed to provide a more complete picture of the constraints and limitations at the driveway location.

It also appears that you used a 33 MPH design speed in your calculations. Did we give you that information or did you do your own speed data collection? Need to be sure that it is based on 85th %ile speeds, and not just an estimation. I am available anytime on Tuesday and Wednesday next week, as well as parts of other days.

Eric B. Eby, P.E.

City Engineer – Parking, Transportation, and Planning Department of Public Works
City of Portsmouth
680 Peverly Hill Road
Portsmouth, NH 03801
(603) 766-1415
Cell (603)-815-1761

From: Joseph Coronati < jcoronati@Jonesandbeach.com >

Sent: Wednesday, December 6, 2023 5:16 PM

To: Eric B. Eby <ebeby@cityofportsmouth.com>; Zachary M. Cronin <zmcronin@cityofportsmouth.com>; Dave J.

Desfosses < djdesfosses@cityofportsmouth.com >

Cc: Mike Garrepy (mgarrepy@gmail.com) <mgarrepy@gmail.com>

Subject: 18134.1 - Luster Cluster, Sight Distance

Eric, Zach & Dave,

We have been coordinating with Steve Pernaw, who is retired so this took a little longer than expected. Please review the plans and let us know if you have any questions. I think in the end, it would be better to look at each of these locations in person as it is tight. The sight lines go over sidewalk, which is changing and uneven and over lawn areas with vegetation at the uphill section. I'm not sure how much you are lowering the hill in your next contract with Severino.

Let me know if you can meet next week to look at this so we can determine the best driveway location.

Thanks

Joseph Coronati

Vice President

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ROCKINGHAM COUNTY CONSERVATION DISTRICT

110 North Road, Brentwood, NH 03833-6614 Tel: 603-679-2790 • Fax: 603-679-2860 www.rockinghamccd.org

23 May 2024

Peter Britz, Director of Planning City of Portsmouth Planning Dept. 1 Junkins Avenue Portsmouth, NH 03801

RE: 635 Sagamore Avenue

Tax map/lot: 222, lot 19 RCCD #PR222-19 N24

Dear Mr. Britz;

At your instruction, Rockingham County Conservation District (RCCD) performed a wetland review of this site. The scope of work included a wetland review on the project site and a determination of reference lines for buffer measurements from off-site wetlands. A site visit was conducted on 22 May 2024 by Michael Cuomo of the Rockingham County Conservation District and Brenden Walden of Gove Environmental Services.

- 1) Confirming the findings of Mr. Walden's letter dated 8 November 2021, there are no wetlands on the project site.
- 2) There are two wetlands across the street from the project site on the Tidewatch Condominium property. The attached Sketch One shows the general locations, overlaid on part of the Jones and Beach existing conditions plan. The wetlands were not flagged because they are off the project site. Measurements were taken from the wetland boundary to the centerline of the road for location reference. The Easterly wetland requires a 100 foot buffer and the Westerly wetland does not, according to the City's GIS.
- 3) Sketch Two is taken from the City's GIS. It generally shows the two wetlands discussed above and a third 'wetland' south and east of the project site, partially on the Tidewatch Condominium property. This 'wetland' does not exist; its is a map error.

Sincerely,

Michael Cuomo

Whatams

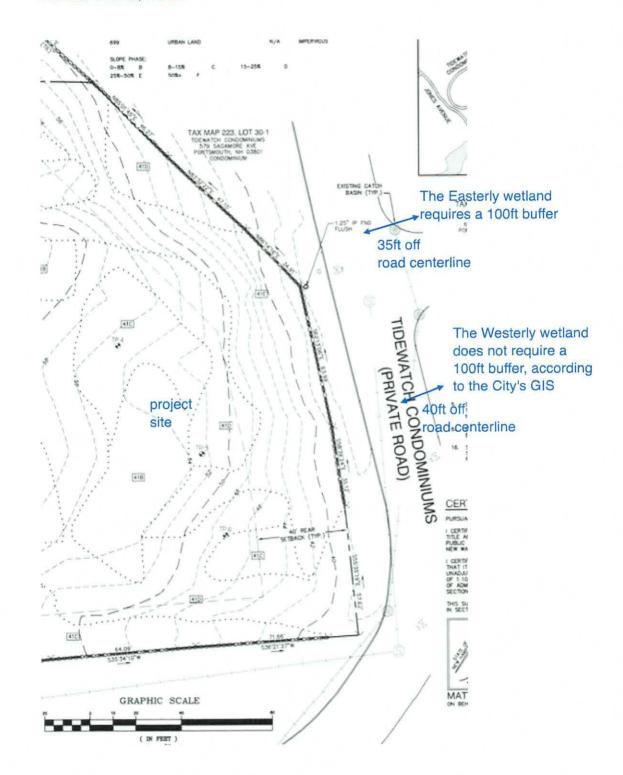
NH Certified Soil Scientist #6

NH Certified Wetland Scientist #4

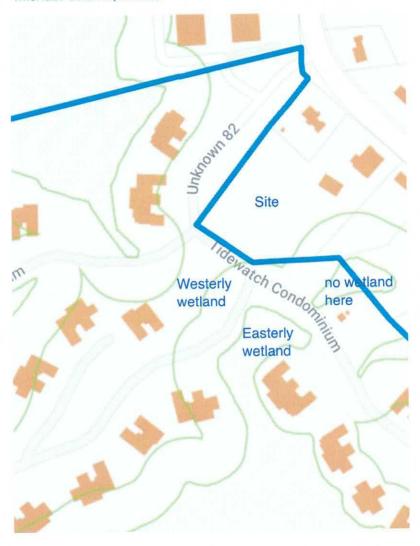
Copy to:

plbritz@cityofportsmouth.com

bwalden@gesinc.biz mgarrepy@gmail.com Sketch One Part of 635 Sagamore Ave, Portsmouth Buffer from off-site wetlands 23 May 2024 Michael Cuomo, RCCD



Sketch Two 635 Sagamore Avenue, Portsmouth Wetlands around site 23 May 2024 Michael Cuomo, RCCD



Daniel Meditz

From: Paige Libbey

Sent: Tuesday, August 20, 2024 10:28 AM

To: Daniel Meditz

Subject: FW: 18134.1 - Luster Cluster, 635 Sagamore Ave.

Paige Libbey, P.E.

Associate Principal

JONES&BEACH ENGINEERS, INC.

85 Portsmouth Avenue PO Box 219 Stratham, NH 03885 (603) 772-4747 (ext. #126) http://www.jonesandbeach.com

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From: Dave J. Desfosses <djdesfosses@cityofportsmouth.com>

Sent: Friday, July 26, 2024 6:47 AM

To: Joseph Coronati < jcoronati@Jonesandbeach.com>

Cc: Mark Rainey <mrainey@severinotrucking.com>; Mike Garrepy (mgarrepy@gmail.com) <mgarrepy@gmail.com>; Paige Libbey <pli>plibbey@jonesandbeach.com>; Zachary M. Cronin <zmcronin@cityofportsmouth.com>; eric weinrieb

<eweinrieb@altus-eng.com>; Douglas N. Sparks <dnsparks@cityofportsmouth.com>

Subject: RE: 18134.1 - Luster Cluster, 635 Sagamore Ave.

From: Joseph Coronati < jcoronati@Jonesandbeach.com>

Sent: Thursday, July 25, 2024 3:47 PM

To: Dave J. Desfosses < <u>djdesfosses@cityofportsmouth.com</u>>; James V. Tow < <u>jvtow@cityofportsmouth.com</u>>; eric

weinrieb <eweinrieb@altus-eng.com>

Cc: Mark Rainey <mrainey@severinotrucking.com>; Mike Garrepy (mgarrepy@gmail.com) <mgarrepy@gmail.com>;

Paige Libbey < plibbey@jonesandbeach.com >

Subject: 18134.1 - Luster Cluster, 635 Sagamore Ave.

Dave.

Thanks for witnessing the test pits with us this week. I talked with Mike Garrepy about the drainage and the new catch basin that was installed recently on Sagamore ave by Severino. It sounded like you were ok if we allowed some of our stormwater from the front of the site to drain out into Sagamore ave and go down the gutter line to the new catch basin. This would allow us to move the first row of catch basins in our driveway back onto our site and avoid the congestion of the utilities that have been stubbed onto the property, which would be great. Can you let us know if we have understood correctly so we don't redesign to something that you aren't comfortable with?

Yes, mimic existing conditions regarding flow patterns and show existing conditions correctly.

On the water service to the building, we have an existing water service located near the front door of the Luster King building. There is a tenant in the property so we can't stop the water supply unless we re-connect the building. We would prefer not to run a temporary service from our new water stub that was placed on the lot as it will be a lot of ledge removal needed to do that and that area is currently being used as a staging area for Severino. Can we keep the water service in place and cap it at the back of the sidewalk once construction begins on the 4 unit housing project so we don't have to go out to the watermain (which is on our side of the road, but the sidewalk will be newly installed)?

The service MUST be terminated at the main. If you don't remove the water service before the final paving of Sagamore Ave, the City will be forced to make the applicant mill and pave Sagamore Ave so that there is no patch unless you wait the 4 years for the moratorium to end.

Let me know if you want to have a call to all get on the same page or a meeting, virtual or in person.

Thanks

JOSEPH CORONATI Vice President JONES&BEACH ENGINEERS, INC.

85 Portsmouth Avenue PO Box 219 Stratham, NH 03885 (603) 772-4746 (ext. #114) jcoronati@jonesandbeach.com http://www.jonesandbeach.com

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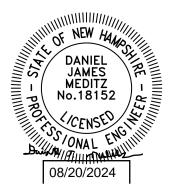
DRAINAGE ANALYSIS

SEDIMENT AND EROSION CONTROL PLAN

"Luster Cluster" 635 Sagamore Ave. Portsmouth, NH 03801 Tax Map 222, Lot 19

Prepared for:

635 Sagamore Development LLC 3612 Lafayette Rd., Dept 4 Portsmouth, NH 03801



Prepared by:
Jones & Beach Engineers, Inc.
85 Portsmouth Avenue
P.O. Box 219
Stratham, NH 03885
(603) 772-4746
March 14, 2024
Revised April 18, 2024
Revised August 16, 2024
JBE Project No. 18134.1

EXECUTIVE SUMMARY

635 Sagamore Development LLC proposes to demolish an existing commercial development and construct a 4-unit multi-family residential site on the subject parcel located at 635 Sagamore Ave. in Portsmouth, NH. In the existing condition, the subject parcel is home to two buildings and a paved parking area that used to comprise the "Luster King," a former auto detailing business that has since closed.

A drainage analysis of the entire site as well as offsite contributing watershed area was conducted for the purpose of estimating the peak rate of stormwater runoff and to subsequently design adequate drainage structures. Two models were compiled, one for the area in its existing (pre-construction) condition, and a second for its proposed (post-construction) condition. The analysis was conducted using data for the 2 Year – 24 Hour (3.70"), 10 Year – 24 Hour (5.61"), 25 Year – 24 Hour (7.12"), and 50 Year – 24 Hour (8.53") storm events using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment. This data was taken from the Extreme Precipitation Tables developed by the Northeast Regional Climate Center (NRCC), and the values have been increased by 15% due to the project being within the Coastal/Great Bay Region. A summary of the existing and proposed conditions peak rates of runoff toward the three analysis points and toward the existing drainage ditch on the Tidewatch Condominium property (Reach 1R) in units of cubic feet per second (cfs) is as follows:

Analysis Point	2 Y	2 Year		10 Year		25 Year		50 Year	
	Pre	Post	Pre	Post	Pre	Post	Pre	Post	
Analysis Point #1	1.35	1.02	2.37	1.82	3.18	2.45	3.93	3.03	
Analysis Point #2	0.09	0.06	0.20	0.13	0.29	0.19	0.37	0.24	
Analysis Point #3	2.88	2.24	5.74	4.16	8.14	5.50	10.41	7.16	
Analysis Point #4	1.08	0.82	2.18	1.68	3.10	2.40	3.97	3.08	

A similar summary of the existing and proposed peak volumes in units of acre-feet is as follows:

Analysis Point	2 Year		10 Year		25 Year		50 Year	
	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Analysis Point #1	0.100	0.076	0.177	0.135	0.241	0.185	0.301	0.231
Analysis Point #2	0.007	0.005	0.014	0.009	0.021	0.014	0.027	0.018
Analysis Point #3	0.247	0.157	0.487	0.331	0.693	0.488	0.892	0.641
Analysis Point #4	0.084	0.061	0.167	0.122	0.238	0.175	0.307	0.266

Peak flows and volumes are being reduced in the post-construction condition toward all analysis points during all analyzed storm events. The subject parcel is located in the Single Residence A (SRA) Zoning District. The subject parcel currently consists of the aforementioned former commercial site which is proposed to be demolished. Despite impervious surface existing on the subject parcel now, the proposed development results in an increase in impervious surface on the subject parcel. The addition of the proposed impervious surfaces causes an increase in the curve number (C_n) and a decrease in the time of concentration (T_c) , and if a stormwater management system were not implemented, the net result of this would be a potential increase in peak rates of runoff from the site. In order to avoid this potential, a stormwater management system has been designed, consisting of a bioretention system with a sediment forebay for pre-treatment of runoff, stone drip edges, and stone underneath decks. Due to the use of these stormwater management features, the peak flow and volume

of runoff will be reduced toward all analysis points during all analyzed storm events in the proposed condition as compared to the existing condition, and the treatment requirements of the City of Portsmouth are met. Additionally, the NHDES Alteration of Terrain Bureau's groundwater recharge volume and channel protection requirements are met with the proposed development. Although some runoff from the front of the site proposed to drain into the Sagamore Avenue right of way and into a new catch basin without on-site treatment, the catch basin was presumably designed for the impervious surface being directed toward it from the Luster King development that currently exists. We are decreasing the amount of impervious surface as well as the peak flow rate and volume of runoff being directed toward this catch basin compared to what it was designed for. Therefore, if there is a treatment system at the outfall of the closed drainage network, then it will continue to function as designed for the runoff being directed to it from the proposed development. The stormwater management system as designed meets all requirements of the City of Portsmouth stormwater regulations per Section 7.1 and 7.4-7.6 of the Site Plan Review Regulations.

The use of Best Management Practices per the NHDES <u>Stormwater Manual</u> have been applied to the design of this stormwater management system and will be observed during all stages of construction. All land disturbed during construction will be stabilized within thirty days of groundbreaking and abutting property owners will suffer minimal adversity resultant to this development.

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1.0 RAINFALL CHARACTERISTICS

This drainage report includes an existing conditions analysis of the area involved in the proposed development, as well as a proposed condition, or post-construction analysis, of the same area. These analyses were accomplished using the USDA SCS TR-20 Method within the HydroCAD 10.20-3c Stormwater Modeling System. The curve numbers were developed using the SCS TR-55 Runoff Curve numbers for Urban Areas. A Type III SCS 24-hour rainfall distribution was utilized in analyzing the data for the 2 Year – 24 Hour (3.70"), 10 Year – 24 Hour (5.61"), 25 Year – 24 Hour (7.12"), and 50 Year – 24 Hour (8.53") storm events. This data was taken from the Extreme Precipitation Tables developed by the Northeast Regional Climate Center (NRCC), and the values have been increased by 15% due to the project being within the Coastal/Great Bay Region.

The peak rates and volume of runoff will be reduced from the existing condition, thereby minimizing any potential for a negative impact on abutting properties. This is accomplished through treatment of stormwater runoff and attenuation of peak flows and volumes resulting from storm events.

2.0 EXISTING CONDITIONS ANALYSIS

In the existing condition, the site consists of two commercial buildings as well as a shed and a paved parking area that comprise the former Luster King auto detailing business, which has since closed. Most of the area behind the existing commercial development is wooded with light underbrush and large ledge outcrops. Due to these features of the woodlands, the woods area has been modelled as "fair" rather than "good" for the purposes of stormwater runoff calculations. There is some lawn space around the existing developed area as well.

The existing topography and roof ridges divide the subject parcel and offsite contributing watershed areas into four subcatchments, draining toward three analysis points. Subcatchment 1 represents the front of the subject parcel as well as a stretch of the northbound lane of Sagamore Avenue and some offsite contributing watershed. This subcatchment is entirely developed in the existing condition, and it drains directly into the Sagamore Ave. right of way, down a flow path modelled as Reach 3R. Reach 3R ends at Analysis Point 1, a specific point along the Sagamore Avenue right of way. The reason why Analysis Point 1 was located at the specific place where it was is explained later in this report.

Runoff that reaches Analysis Point 1 from the subject parcel then follows the curb lines of Sagamore Avenue and of the Tidewatch Condominium Roadway, modelled as Reaches 4R and 5R, toward an existing water collection point on the side of the Tidewatch Condominium Roadway where it appears that a significant amount of runoff puddles in the existing condition, modelled as Analysis Point 3.

A new catch basin has been installed just to the south of the intersection of Sagamore Avenue and the Tidewatch Condominium roadway as part of the ongoing Sagamore Avenue roadway improvements. This catch basin captures all runoff directed toward Analysis Point 1 immediately downstream of Reach 3R. Therefore, Analysis Point 1 was placed at the location of the newly installed catch basin The addition of this catch basin prevents water from the Sagamore Avenue right of way up to the top of the hill to the south of the subject parcel from draining down the Tidewatch Condominium roadway, and therefore it will somewhat mitigate the existing drainage issue. However, because this catch basin was not yet installed at the time that the design of the proposed project began, we are modelling the hydrology of the site as it was before the catch basin was installed for the purposes of the existing conditions analysis. This is consistent with Env-Wq 1503.12(d), which requires that the existing conditions for a project site be modelled as the site was 10 years ago. In the proposed conditions

analysis, we are modelling the site hydrology as it will be with the catch basin installed, as we assume that it will be installed by the time that the proposed development is constructed.

Subcatchment 2S represents a small section of the developed portion of the property to the north of an existing high point which drains on to abutting Tax Map 222, Lot 20, modelled as Analysis Point 2. It is very important that peak flows and volumes draining toward Analysis Points 1 and 2 are reduced in the post-construction condition, as these two analysis points represent a highway and a house lot, respectively. Runoff directed toward Analysis Point 2 is directed through Reach 2R, a flow path through Tax Map 222 Lot 20, toward aforementioned Reach 3R, from where the runoff then collects at AP1 before following Reaches 4R and 5R toward Analysis Point 3. In effect, the runoff directed toward AP1 includes the runoff directed toward AP2, and the runoff directed toward AP3 includes the runoff directed toward both AP1 and AP2 in the existing condition.

The largest subcatchment is Subcatchment 3S. Subcatchment 3S is roughly the western quarter of the property and it consists primarily of woodland with large ledge outcrops. Subcatchment 3S drains toward an existing drainage ditch alongside and below the grade of the Tidewatch Condominium private roadway, which is curbed so that no runoff from the roadway itself enters the ditch. This drainage ditch is modelled as a Tc segment for the subcatchment and it drains toward Analysis Point 3. Analysis Point 3 is an existing water collection point along the Tidewatch Condominium Road. In theory, water that collects here eventually infiltrates or overflows, but from on-site observations, there is erosion and puddling which is evidence that runoff mostly stops in this spot. Therefore, it is modelled as an analysis point with no overflow. This point receives the runoff from 3S as well as the runoff from AP1 and AP2 upstream.

Finally, a section of both developed and undeveloped land in the western end of the property, modelled as Subcatchment 4S, drains into abutting woodland on the Tidewatch Condominium property and ultimately toward a catch basin adjacent to the Tidewatch Condominium mailhouse that is modelled as Analysis Point 4.

Existing soil types were determined through a Site Specific Soil Survey conducted by a Certified Soil Scientist. The pervious soils are categorized into Hydrologic Soil Group (HSG) B while the impervious areas of the subject parcel are categorized as Urban Land (SSS Symbol 699). The pervious sections of the property are represented as Chatfield-Hollis-Rock Outcrop complex and Chatfield Variant (moderately well drained). Although these soils are categorized as HSG B currently, it is our understanding that the "Ksat Values for New Hampshire Soils," Special Publication No. 5 sponsored by the Society of Soil Scientists of Northern New England (SSSNNE) is in the process of being updated and there are plans to reclassify Chatfield as a HSG C soil. For this reason, Dave Desfosses of the Portsmouth Department of Public Works has requested that we model the entire site and all offsite contributing watershed areas as HSG C. We asked the project soil scientist, who confirmed that this is an acceptable approach in his professional opinion as well. Therefore, we have modelled the entire site and all offsite areas as HSG C.

According to "Ksat Values for New Hampshire Soils," Special Publication No. 5 sponsored by the Society of Soil Scientists of Northern New England (SSSNNE), Chatfield, Chatfield Variant, and Hollis soils all have identical saturated hydraulic conductivities, ranging from 0.6 to 6.0 inches/hour within both the B and C horizons.

To further determine the appropriate Ksat to use for design, infiltration testing was performed on site using a Compact Constant Head Permeameter (CCHP, also known as an amoozemeter) on July 2,

2024. Three (3) pits were dug using a shovel in the soil and three (3) infiltration tests were performed in each pit. The first pit was dug in the front of the site in order to evaluate the feasibility of adding a new infiltration practice here. The second pit was dug in the footprint of the proposed bioretention system. The third and final pit was dug in the vicinity of Unit #4.

Standard size auger holes, 4 cm in diameter were dug within each pit to the depth of the bottom of each respective practice to obtain an accurate permeability reading below the bottom of the proposed systems. Water was then discharged through the soil and the drop in water level on the tube in which the water was stored before being discharged was recorded at several time intervals. The comparison between the drop in water level and the elapsed time from the start of the test was used to calculate the Ksat value. For example, if the water level dropped 3 cm after 5 minutes and 5 cm after 10 minutes, this was recorded and used as data to calculate the Ksat using the formulas listed in the data spreadsheets in the appendix of this report. The Ksat values from each time increment were then averaged to determine the mean Ksat, and lowest mean Ksat from each area was divided by a factor of safety of two in order to determine the saturated hydraulic conductivity to use for design purposes.

It should be noted that the CCHP was observed to drain very rapidly on these holes and it was difficult to achieve a steady state. The device was consistently draining while still attempting to fill the auger holes with water. When the test could finally be started, the first one or two increments on each test needed to be discarded from the results because they were much larger than the following increments after the soils were saturated and the infiltration rate stabilized. The saturated hydraulic conductivity that was determined at each test site was ultimately much higher than anticipated, but logically it makes sense as the substrate was observed to consist of coarse sand with many stones.

The results of the permeability testing are as summarized below:

Test	Ksat (in/hr)
Front of site – Test #1	27.33
Front of site – Test #2	30.85
Front of site – Test #3	22.26
Front of site – Low Ksat	22.26
Bioretention – Test #1	14.84
Bioretention – Test #2	33.41
Bioretention – Test #3	65.74
Bioretention – Low Ksat	14.84
Unit 4 – Test #1	30.64
Unit 4 – Test #2	25.41
Unit 4 – Test #3	37.31
Unit 4 – Low Ksat	25.41

A further breakdown of the data used to arrive at the final Ksat values is included in the appendix of this report. Applying a factor of safety of two, this comes out to a saturated hydraulic conductivity of 11.1 in/hr to use for the front of the site, 7.4 in/hr to use for the bioretention system, and 12.71 in/hr to use for the infiltration practices around the back two units. Because the bioretention system is in a cut, the field-observed Ksat of 7.4 in/hr was utilized. Because the infiltration practices are in a fill, a design infiltration rate of 0.3 in/hr was utilized as a worst-case scenario for the fill material.

3.0 PROPOSED CONDITIONS ANALYSIS

The addition of the proposed impervious surfaces causes an increase in the curve number (C_n) and a decrease in the time of concentration (T_c), and if a stormwater management system were not implemented, the net result of this would be a potential increase in peak rates of runoff from the site. A stormwater management system was designed in order to avoid this potential. The proposed development, consisting of the aforementioned four (4) residential units with associated paved roadway and driveways as well as stormwater management features divide the subject parcel into fifteen (15) subcatchments. Subcatchments 1S-4S drain directly toward Analysis Points 1-4, respectively, as previously outlined. However, because a new catch basin will now intercept the flow that reaches the Sagamore Avenue right of way (Analysis Point 1) from the subject parcel, analysis point 3 is no longer modelled downstream of analysis point 1.

Subcatchment 5S has been removed from the drainage analysis as it was the subcatchment associated with a stormwater pond that has since been removed from the drainage design. Subcatchments 6S-9S drain through catch basins into a closed drainage system which outlets toward a bioretention pond modelled as Pond 1P. The bioretention pond is designed to treat and infiltrate runoff directed toward it during smaller storms, or in larger storms, infiltrate as much as possible and attenuate and slowly discharge outflow. The bioretention pond will have a sediment forebay for pre-treatment. Any discharge from Pond 1P follows a path through Subcatchment 3S represented as Reach 7R, toward Reach 8R, an existing roadside ditch on the Tidewatch condominium property leading to Analysis Point 3.

Subcatchments 11S and 12S consist of lawn and roof areas that drain toward yard drains 1 and 2, respectively. The runoff that is caught by these yard drains additionally enters the previously described closed drainage system that outlets toward Pond 1P.

Subcatchments 13S and 14S represent roof and deck areas on Units 3-4 which are routed toward infiltration stone underneath these units back decks. These devices are modelled as Ponds 3P and 4P.

Subcatchments 15S and 16S represent roof areas on Units 3 and 4 which drain into stone drip edges. The stone drip edges, modelled as Ponds 5P and 6P, will be lined and underdrained for the sole purpose of directing this roof water into the aforementioned stone areas underneath the back decks of these units (3P and 4P) in order to meet the City's pollutant removal requirements.

Finally, Subcatchment 18S represents the grassed and roof area that drains directly toward Pond 1P without passing through the closed drainage system in the proposed condition.

As a result of the implementation of this stormwater management system, peak flows and runoff volumes are reduced toward all four analysis points during all analyzed storm events in the proposed condition as compared with the existing condition. The NHDES Alteration of Terrain Bureau allows an increase in runoff volume of up to 0.1 acre-feet during the 2-year 24-hour storm event. We are decreasing runoff volumes and therefore this would be approvable by the AOT Bureau if the project needed an AOT permit (which it does not as the area of disturbance is below 100,000 SF).

Furthermore, the project as designed exceeds the AOT Bureau's groundwater recharge volume requirement. A GRV worksheet is contained within the appendix of this report in order to illustrate this. Therefore, we have designed the drainage system to avoid adverse impacts to abutting infrastructure and the requirement per Section 7.1 of the Site Plan Review Regulations to "design

practices to the maximum extent practical (MEP) to reduce stormwater runoff volumes, maintain predevelopment site hydrology, and protect water quality in receiving waters" is met. Furthermore, rain gardens (also known as bioretention systems) are recommended as a Low Impact Development practice in this same section of the regulations. We are using bioretention systems to treat and attenuate runoff from paved areas of the subject parcel in the proposed condition.

According to the NH Stormwater Manual, bioretention systems provide a pollutant removal efficiency of 90% for TSS and 65% for nitrogen, and drip edges provide a removal efficiency of 90% for TSS and 55% for nitrogen. While drip edges cannot be used for infiltration in this case as the units will have foundation drains, stone underneath a deck is assumed to provide similar stormwater treatment to a stone drip edge. The City of Portsmouth Site Plan Review Regulations stipulate that stormwater BMPs shall be designed for 80% TSS removal and 50% nitrogen removal of stormwater runoff from post-construction impervious surfaces. This plan meets the pollutant removal requirement for runoff directed toward Analysis Points 3 and 4 in the post-construction condition. A breakdown of pollutant removal efficiencies for the runoff that passes through the bioretention ponds, stone infiltration areas, or no treatment BMP and reaches Analysis Points 3 and 4 from the subject parcel is contained within the appendix of this report in order to demonstrate this.

No impervious surface is directed toward Analysis Point 2 post-construction. Presumably, the flow directed toward the new catch basin along the gutter line of Sagamore Avenue from the existing Luster King development was accounted for in the design of the City's closed drainage network. Because the amount of impervious surface being directed toward Analysis Point 1 is being decreased post-construction, we presume that whatever stormwater management the City had proposed for the runoff downstream of the new catch basin will continue to function as intended post-construction. Therefore, no on-site treatment BMP's are proposed for the impervious surface directed toward Analysis Point 1 post-construction, and the impervious surface directed toward analysis point 1 post-construction is excluded from the pollutant removal calculations. Even if we did propose a treatment BMP for the runoff directed toward the Sagamore Avenue right of way, what would result is a point discharge of stormwater from an outlet pipe or weir directly toward pavement, which is not advisable. Therefore, this water *cannot* be treated on site, which will not be a problem assuming that the City designed an appropriate BMP for the runoff directed toward its catch basin from the Luster King site.

5.0 CONCLUSION

This proposed site development will have minimal adverse effect on abutting infrastructures, properties, and downstream wetlands by way of stormwater runoff or siltation. Appropriate steps will be taken to eliminate erosion and sedimentation; this will be accomplished through the construction of a drainage system consisting of site grading, catch basins, yard drains, a bioretention system, lined stone drip edges, infiltration stone underneath decks, and temporary erosion control measures including but not limited to silt fence and the use of a stabilized construction entrance. Best Management Practices developed by the State of New Hampshire have been utilized in the design of this system and their application will be enforced throughout the construction process. Peak rates and volumes of runoff from the site will be reduced toward all analysis points during all analyzed storm events.

This project disturbs less than 100,000 S.F. and does <u>not</u> require a NHDES Alteration of Terrain Permit.

1 Medits

Respectfully Submitted,

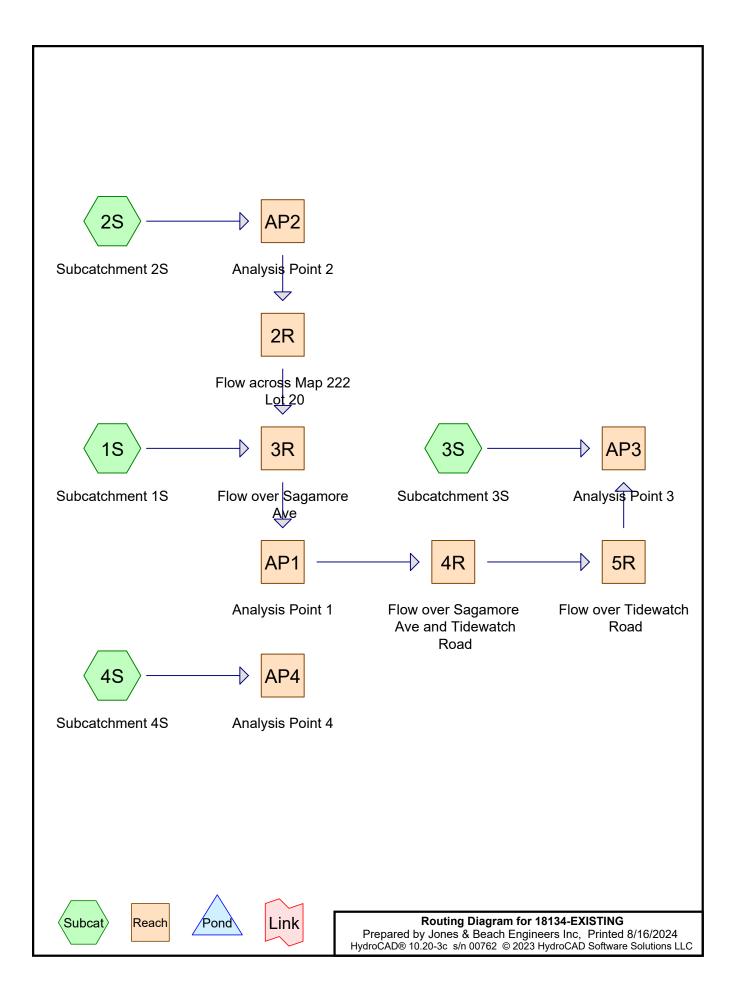
JONES & BEACH ENGINEERS, INC.

Daniel Meditz, P.E Lead Design Engineer

APPENDIX I

EXISTING CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Complete 10 YEAR Summary 25 YEAR Complete 50 YEAR



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Area Listing (all nodes)

Area	CN	Description	
(acres)		(subcatchment-numbers)	
0.621	74	>75% Grass cover, Good, HSG C (1S, 2S, 3S, 4S)	
0.230	98	Paved parking, HSG C (1S, 4S)	
0.129	98	Roofs, HSG C (1S, 3S, 4S)	
1.535	73	Woods, Fair, HSG C (3S, 4S)	
0.003	70	Woods, Good, HSG C (1S, 2S)	
2.518	77	TOTAL AREA	

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
2.518	HSG C	1S, 2S, 3S, 4S
0.000	HSG D	
0.000	Other	
2.518		TOTAL AREA

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S Runoff Area=20,592 sf 54.90% Impervious Runoff Depth>2.36"

Flow Length=187' Tc=6.0 min CN=87 Runoff=1.28 cfs 0.093 af

Subcatchment2S: Subcatchment2S Runoff Area=2,614 sf 0.00% Impervious Runoff Depth>1.38"

Flow Length=20' Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.09 cfs 0.007 af

Subcatchment3S: Subcatchment3SRunoff Area=58,629 sf 0.32% Impervious Runoff Depth>1.31"

Flow Length=447' Tc=11.9 min CN=73 Runoff=1.62 cfs 0.147 af

Subcatchment4S: Subcatchment4S Runoff Area=27,837 sf 14.82% Impervious Runoff Depth>1.58"

Flow Length=216' Tc=7.8 min CN=77 Runoff=1.08 cfs 0.084 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.07' Max Vel=0.25 fps Inflow=0.09 cfs 0.007 af

n=0.150 L=52.0' S=0.0385 '/' Capacity=6.22 cfs Outflow=0.08 cfs 0.007 af

Reach 3R: Flow over Sagamore Ave Avg. Flow Depth=0.14' Max Vel=2.71 fps Inflow=1.35 cfs 0.100 af

n=0.016 L=101.0' S=0.0297 '/' Capacity=39.77 cfs Outflow=1.35 cfs 0.100 af

Reach 4R: Flow over Sagamore Ave and Avg. Flow Depth=0.14' Max Vel=2.85 fps Inflow=1.35 cfs 0.100 af

 $n = 0.016 \quad L = 145.0' \quad S = 0.0345 \; \text{'/'} \quad Capacity = 42.85 \; \text{cfs} \quad Outflow = 1.34 \; \text{cfs} \quad 0.100 \; \text{af}$

Reach 5R: Flow over Tidewatch Road Avg. Flow Depth=0.12' Max Vel=3.37 fps Inflow=1.34 cfs 0.100 af

n=0.016 L=253.0' S=0.0553 '/' Capacity=54.28 cfs Outflow=1.30 cfs 0.100 af

Reach AP1: Analysis Point 1 Inflow=1.35 cfs 0.100 af

Outflow=1.35 cfs 0.100 af

Reach AP2: Analysis Point 2 Inflow=0.09 cfs 0.007 af

Outflow=0.09 cfs 0.007 af

Reach AP3: Analysis Point 3 Inflow=2.88 cfs 0.247 af

Outflow=2.88 cfs 0.247 af

Reach AP4: Analysis Point 4 Inflow=1.08 cfs 0.084 af

Outflow=1.08 cfs 0.084 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.331 af Average Runoff Depth = 1.58" 85.76% Pervious = 2.159 ac 14.24% Impervious = 0.359 ac Prepared by Jones & Beach Engineers Inc

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1SRunoff Area=20,592 sf 54.90% Impervious Runoff Depth>4.14"
Flow Length=187' Tc=6.0 min CN=87 Runoff=2.19 cfs 0.163 af

Subcatchment2S: Subcatchment2S Runoff Area=2,614 sf 0.00% Impervious Runoff Depth>2.86" Flow Length=20' Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.20 cfs 0.014 af

Subcatchment3S: Subcatchment3S Runoff Area=58,629 sf 0.32% Impervious Runoff Depth>2.76"

Flow Length=447' Tc=11.9 min CN=73 Runoff=3.56 cfs 0.310 af

Subcatchment4S: Subcatchment4SRunoff Area=27,837 sf 14.82% Impervious Runoff Depth>3.14"
Flow Length=216' Tc=7.8 min CN=77 Runoff=2.18 cfs 0.167 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.10' Max Vel=0.31 fps Inflow=0.20 cfs 0.014 af n=0.150 L=52.0' S=0.0385 '/' Capacity=6.22 cfs Outflow=0.18 cfs 0.014 af

Reach 3R: Flow over Sagamore AveAvg. Flow Depth=0.17' Max Vel=3.11 fps Inflow=2.36 cfs 0.177 af n=0.016 L=101.0' S=0.0297'/' Capacity=39.77 cfs Outflow=2.37 cfs 0.177 af

Reach 4R: Flow over Sagamore Ave and Avg. Flow Depth=0.17' Max Vel=3.28 fps Inflow=2.37 cfs 0.177 af n=0.016 L=145.0' S=0.0345 '/' Capacity=42.85 cfs Outflow=2.35 cfs 0.177 af

Reach 5R: Flow over Tidewatch Road Avg. Flow Depth=0.15' Max Vel=3.87 fps Inflow=2.35 cfs 0.177 af n=0.016 L=253.0' S=0.0553 '/' Capacity=54.28 cfs Outflow=2.30 cfs 0.177 af

Reach AP1: Analysis Point 1 Inflow=2.37 cfs 0.177 af

Outflow=2.37 cfs 0.177 af

Reach AP2: Analysis Point 2 Inflow=0.20 cfs 0.014 af
Outflow=0.20 cfs 0.014 af

Reach AP3: Analysis Point 3 Inflow=5.74 cfs 0.487 af

Outflow=5.74 cfs 0.487 af

Reach AP4: Analysis Point 4 Inflow=2.18 cfs 0.167 af

Outflow=2.18 cfs 0.167 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.654 af Average Runoff Depth = 3.12" 85.76% Pervious = 2.159 ac 14.24% Impervious = 0.359 ac Prepared by Jones & Beach Engineers Inc

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 2.19 cfs @ 12.09 hrs, Volume=

0.163 af, Depth> 4.14"

Routed to Reach 3R: Flow over Sagamore Ave

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Α	rea (sf)	CN E	Description		
		2,869	98 F	Roofs, HSC	G C	
		8,436	98 F	Paved park	ing, HSG C	
		9,256	74 >	∙75% Ġras	s cover, Go	ood, HSG C
		31	70 V	Voods, Go	od, HSG C	
		20,592	87 V	Veighted A	verage	
		9,287			vious Area	
		11,305	5	54.90% Imp	ervious Ar	ea
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.5	46	0.1090	0.31		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.1	4	0.0670	1.26		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.70"
	0.1	41	0.0670	5.25		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
	0.4	96	0.0360	3.85		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
	2 1	107	Total I	norgand t	a minimum	To = 6.0 min

3.1 187 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.20 cfs @ 12.09 hrs, Volume=

0.014 af, Depth> 2.86"

Routed to Reach AP2: Analysis Point 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Aı	rea (sf)	CN	Description								
		2,495	74	>75% Grass cover, Good, HSG C								
_		119	70	Woods, Good, HSG C								
		2,614	74	Weighted A	verage							
		2,614		100.00% P	ervious Are	a						
	Tc	Length	Slope	,	Capacity	Description						
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	1.3	20	0.1000	0.25		Sheet Flow,						
_						Grass: Short	n= 0.150	P2= 3.70"				

1.3 20 Total, Increased to minimum Tc = 6.0 min

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Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 3.56 cfs @ 12.17 hrs, Volume=

0.310 af, Depth> 2.76"

Routed to Reach AP3: Analysis Point 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN E	Description								
	187	98 F	Roofs, HSG	G C							
	9,391	74 >	, ,								
	49,051	73 V	73 Woods, Fair, HSG C								
	58,629		Veighted A								
	58,442	_		vious Area							
	187	C).32% Impe	ervious Are	a						
_		01		0 "	D 18						
Tc	Length	Slope	•	Capacity	Description						
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
8.6	50	0.0415	0.10		Sheet Flow,						
					Woods: Light underbrush n= 0.400 P2= 3.70"						
0.7	62	0.0968	1.56		Shallow Concentrated Flow,						
					Woodland Kv= 5.0 fps						
0.7	54	0.0741	1.36		Shallow Concentrated Flow,						
4.0	400	0.4000	4.50		Woodland Kv= 5.0 fps						
1.3	122	0.1000	1.58		Shallow Concentrated Flow,						
0.0	450	0.0400	4.55	40.00	Woodland Kv= 5.0 fps						
0.6	159	0.0189	4.55	18.20	Trap/Vee/Rect Channel Flow,						
					Bot.W=1.00' D=1.00' Z= 3.0 '/' Top.W=7.00'						
					n= 0.030 Short grass						
11.9	447	Total									

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 2.18 cfs @ 12.11 hrs, Volume= 0.167 af, Depth> 3.14"

Routed to Reach AP4 : Analysis Point 4

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

Area (sf)	CN	Description				
2,555	98	Roofs, HSG C				
1,571	98	Paved parking, HSG C				
5,912	74	>75% Grass cover, Good, HSG C				
 17,799	73	Woods, Fair, HSG C				
27,837	77	Weighted Average				
23,711		85.18% Pervious Area				
4,126		14.82% Impervious Area				

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.9	14	0.0210	0.13		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	4.2	36	0.1280	0.14		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	0.5	50	0.1280	1.79		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	1.0	87	0.0800	1.41		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.2	29	0.2860	2.67		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	7.8	216	Total			

Summary for Reach 2R: Flow across Map 222 Lot 20

Inflow Area = 0.060 ac, 0.00% Impervious, Inflow Depth > 2.86" for 10 Yr 24 Hr +15% event

Inflow = 0.20 cfs @ 12.09 hrs, Volume= 0.014 af

Outflow = 0.18 cfs @ 12.13 hrs, Volume= 0.014 af, Atten= 7%, Lag= 1.9 min

Routed to Reach 3R: Flow over Sagamore Ave

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.31 fps, Min. Travel Time= 2.8 min Avg. Velocity = 0.11 fps, Avg. Travel Time= 7.6 min

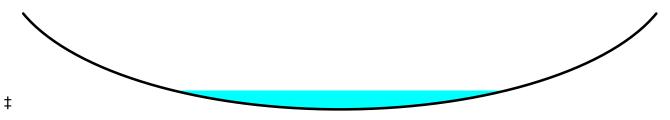
Peak Storage= 30 cf @ 12.13 hrs

Average Depth at Peak Storage= 0.10', Surface Width= 8.86' Bank-Full Depth= 0.50' Flow Area= 6.7 sf, Capacity= 6.22 cfs

20.00' x 0.50' deep Parabolic Channel, n= 0.150 Sheet flow over Short Grass

Length= 52.0' Slope= 0.0385 '/'

Inlet Invert= 66.00', Outlet Invert= 64.00'



Summary for Reach 3R: Flow over Sagamore Ave

[90] Warning: Qout>Qin may require smaller dt or Finer Routing [62] Hint: Exceeded Reach 2R OUTLET depth by 0.08' @ 12.05 hrs

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 4.00" for 10 Yr 24 Hr +15% event

Inflow = 2.36 cfs @ 12.09 hrs, Volume= 0.177 af

Outflow = 2.37 cfs @ 12.10 hrs, Volume= 0.177 af, Atten= 0%, Lag= 0.4 min

Routed to Reach AP1 : Analysis Point 1

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.11 fps, Min. Travel Time= 0.5 min

Avg. Velocity = 1.23 fps, Avg. Travel Time= 1.4 min

Peak Storage= 77 cf @ 12.10 hrs

Average Depth at Peak Storage= 0.17', Surface Width= 8.77' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 39.77 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 101.0' Slope= 0.0297 '/'

Inlet Invert= 64.00', Outlet Invert= 61.00'

‡

Summary for Reach 4R: Flow over Sagamore Ave and Tidewatch Road

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 4.00" for 10 Yr 24 Hr +15% event

Inflow = 2.37 cfs @ 12.10 hrs, Volume= 0.177 af

Outflow = 2.35 cfs @ 12.11 hrs, Volume= 0.177 af, Atten= 1%, Lag= 0.6 min

Routed to Reach 5R: Flow over Tidewatch Road

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.28 fps, Min. Travel Time= 0.7 min

Avg. Velocity = 1.30 fps, Avg. Travel Time= 1.9 min

Peak Storage= 104 cf @ 12.11 hrs

Average Depth at Peak Storage= 0.17', Surface Width= 8.50' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 42.85 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough

Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 145.0' Slope= 0.0345 '/'

Inlet Invert= 61.00', Outlet Invert= 56.00'

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Summary for Reach 5R: Flow over Tidewatch Road

[61] Hint: Exceeded Reach 4R outlet invert by 0.15' @ 12.10 hrs

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 3.99" for 10 Yr 24 Hr +15% event

Inflow = 2.35 cfs @ 12.11 hrs, Volume= 0.177 af

Outflow = 2.30 cfs @ 12.12 hrs, Volume= 0.177 af, Atten= 2%, Lag= 1.0 min

Routed to Reach AP3: Analysis Point 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.87 fps, Min. Travel Time= 1.1 min Avg. Velocity = 1.56 fps, Avg. Travel Time= 2.7 min

Peak Storage= 149 cf @ 12.12 hrs

Average Depth at Peak Storage= 0.15', Surface Width= 7.73' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 54.28 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 253.0' Slope= 0.0553 '/'

‡

Inlet Invert= 56.00', Outlet Invert= 42.00'

Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 4.00" for 10 Yr 24 Hr +15% event

Inflow = 2.37 cfs @ 12.10 hrs, Volume= 0.177 af

Outflow = 2.37 cfs @ 12.10 hrs, Volume= 0.177 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 4R: Flow over Sagamore Ave and Tidewatch Road

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.060 ac, 0.00% Impervious, Inflow Depth > 2.86" for 10 Yr 24 Hr +15% event

Inflow = 0.20 cfs @ 12.09 hrs, Volume= 0.014 af

Outflow = 0.20 cfs @ 12.09 hrs, Volume= 0.014 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 2R: Flow across Map 222 Lot 20

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.879 ac, 14.04% Impervious, Inflow Depth > 3.11" for 10 Yr 24 Hr +15% event

Inflow = 5.74 cfs @ 12.15 hrs, Volume= 0.487 af

Outflow = 5.74 cfs @ 12.15 hrs, Volume= 0.487 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.639 ac, 14.82% Impervious, Inflow Depth > 3.14" for 10 Yr 24 Hr +15% event

Inflow = 2.18 cfs @ 12.11 hrs, Volume= 0.167 af

Outflow = 2.18 cfs @ 12.11 hrs, Volume= 0.167 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S Runoff Area=20,592 sf 54.90% Impervious Runoff Depth>5.59"

Flow Length=187' Tc=6.0 min CN=87 Runoff=2.91 cfs 0.220 af

Subcatchment2S: Subcatchment2S Runoff Area=2,614 sf 0.00% Impervious Runoff Depth>4.14"

Flow Length=20' Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.29 cfs 0.021 af

Subcatchment3S: Subcatchment3S Runoff Area=58,629 sf 0.32% Impervious Runoff Depth>4.03"

Flow Length=447' Tc=11.9 min CN=73 Runoff=5.22 cfs 0.452 af

Subcatchment4S: Subcatchment4S Runoff Area=27,837 sf 14.82% Impervious Runoff Depth>4.47"

Flow Length=216' Tc=7.8 min CN=77 Runoff=3.10 cfs 0.238 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.12' Max Vel=0.35 fps Inflow=0.29 cfs 0.021 af

n=0.150 L=52.0' S=0.0385 '/' Capacity=6.22 cfs Outflow=0.27 cfs 0.021 af

Reach 3R: Flow over Sagamore Ave Avg. Flow Depth=0.19' Max Vel=3.35 fps Inflow=3.17 cfs 0.241 af

n=0.016 L=101.0' S=0.0297'/' Capacity=39.77 cfs Outflow=3.18 cfs 0.241 af

Reach 4R: Flow over Sagamore Ave and Avg. Flow Depth=0.19' Max Vel=3.54 fps Inflow=3.18 cfs 0.241 af

n=0.016 L=145.0' S=0.0345 '/' Capacity=42.85 cfs Outflow=3.16 cfs 0.241 af

Reach 5R: Flow over Tidewatch Road Avg. Flow Depth=0.17' Max Vel=4.18 fps Inflow=3.16 cfs 0.241 af

n=0.016 L=253.0' S=0.0553'/' Capacity=54.28 cfs Outflow=3.10 cfs 0.241 af

Reach AP1: Analysis Point 1 Inflow=3.18 cfs 0.241 af

Outflow=3.18 cfs 0.241 af

Reach AP2: Analysis Point 2 Inflow=0.29 cfs 0.021 af

Outflow=0.29 cfs 0.021 af

Reach AP3: Analysis Point 3 Inflow=8.14 cfs 0.693 af

Outflow=8.14 cfs 0.693 af

Reach AP4: Analysis Point 4 Inflow=3.10 cfs 0.238 af

Outflow=3.10 cfs 0.238 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.931 af Average Runoff Depth = 4.44" 85.76% Pervious = 2.159 ac 14.24% Impervious = 0.359 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S Runoff Area=20,592 sf 54.90% Impervious Runoff Depth>6.96"

Flow Length=187' Tc=6.0 min CN=87 Runoff=3.58 cfs 0.274 af

Subcatchment2S: Subcatchment2S Runoff Area=2,614 sf 0.00% Impervious Runoff Depth>5.40"

Flow Length=20' Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.37 cfs 0.027 af

Subcatchment3S: Subcatchment3S Runoff Area=58,629 sf 0.32% Impervious Runoff Depth>5.27"

Flow Length=447' Tc=11.9 min CN=73 Runoff=6.81 cfs 0.591 af

Subcatchment4S: Subcatchment4S Runoff Area=27,837 sf 14.82% Impervious Runoff Depth>5.76"

Flow Length=216' Tc=7.8 min CN=77 Runoff=3.97 cfs 0.307 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.13' Max Vel=0.38 fps Inflow=0.37 cfs 0.027 af

n=0.150 L=52.0' S=0.0385 '/' Capacity=6.22 cfs Outflow=0.35 cfs 0.027 af

Reach 3R: Flow over Sagamore Ave Avg. Flow Depth=0.21' Max Vel=3.53 fps Inflow=3.92 cfs 0.301 af

n=0.016 L=101.0' S=0.0297'/' Capacity=39.77 cfs Outflow=3.93 cfs 0.301 af

Reach 4R: Flow over Sagamore Ave and Avg. Flow Depth=0.20' Max Vel=3.73 fps Inflow=3.93 cfs 0.301 af

 $n = 0.016 \quad L = 145.0' \quad S = 0.0345 \; \text{'/'} \quad Capacity = 42.85 \; \text{cfs} \quad Outflow = 3.92 \; \text{cfs} \quad 0.301 \; \text{af}$

Reach 5R: Flow over Tidewatch Road Avg. Flow Depth=0.19' Max Vel=4.42 fps Inflow=3.92 cfs 0.301 af

n=0.016 L=253.0' S=0.0553'/' Capacity=54.28 cfs Outflow=3.85 cfs 0.301 af

Reach AP1: Analysis Point 1 Inflow=3.93 cfs 0.301 af

Outflow=3.93 cfs 0.301 af

Reach AP2: Analysis Point 2 Inflow=0.37 cfs 0.027 af

Outflow=0.37 cfs 0.027 af

Reach AP3: Analysis Point 3 Inflow=10.41 cfs 0.892 af

Outflow=10.41 cfs 0.892 af

Reach AP4: Analysis Point 4 Inflow=3.97 cfs 0.307 af

Outflow=3.97 cfs 0.307 af

Total Runoff Area = 2.518 ac Runoff Volume = 1.199 af Average Runoff Depth = 5.72" 85.76% Pervious = 2.159 ac 14.24% Impervious = 0.359 ac Prepared by Jones & Beach Engineers Inc

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 3.58 cfs @ 12.09 hrs, Volume=

0.274 af, Depth> 6.96"

Routed to Reach 3R: Flow over Sagamore Ave

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Α	rea (sf)	CN I	Description							
		2,869	98 I	Roofs, HSG C							
		8,436	98 I	Paved park	Paved parking, HSG C						
		9,256	74	>75% Ġras	s cover, Go	ood, HSG C					
_		31	70 \	Noods, Go	od, HSG C						
		20,592	87 \	Weighted A	verage						
		9,287	4	15.10% Pei	rvious Area	ľ					
		11,305	į	54.90% lmp	pervious Ar	ea					
	Тс	Length	Slope		Capacity	Description					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	2.5	46	0.1090	0.31		Sheet Flow,					
						Grass: Short n= 0.150 P2= 3.70"					
	0.1	4	0.0670	1.26		Sheet Flow,					
						Smooth surfaces n= 0.011 P2= 3.70"					
	0.1	41	0.0670	5.25		Shallow Concentrated Flow,					
						Paved Kv= 20.3 fps					
	0.4	96	0.0360	3.85		Shallow Concentrated Flow,					
_						Paved Kv= 20.3 fps					
	2.4	107	Total	laaraaaad t	a mainimatum	To = 6.0 min					

3.1 187 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.37 cfs @ 12.09 hrs, Volume=

0.027 af, Depth> 5.40"

Routed to Reach AP2: Analysis Point 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Aı	rea (sf)	CN	Description							
		2,495	74	>75% Grass cover, Good, HSG C							
_		119	70	Woods, Good, HSG C							
		2,614	74	Weighted Average							
		2,614		100.00% P	ervious Are	a					
	Tc	Length	Slope	,	Capacity	Description					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	1.3	20	0.1000	0.25		Sheet Flow,					
_						Grass: Short	n= 0.150	P2= 3.70"			

1.3 20 Total, Increased to minimum Tc = 6.0 min

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Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 6.81 cfs @ 12.16 hrs, Volume= 0.591 af, Depth> 5.27"

Routed to Reach AP3 : Analysis Point 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN D	escription						
	187		,						
	9,391	74 >	74 >75% Grass cover, Good, HSG C						
	49,051	73 Woods, Fair, HSG C							
	58,629 73 Weighted Average								
	58,442	9	9.68% Per	vious Area					
	187	0	.32% Impe	ervious Are	a				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
8.6	50	0.0415	0.10		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 3.70"				
0.7	62	0.0968	1.56		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
0.7	54	0.0741	1.36		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
1.3	122	0.1000	1.58		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
0.6	159	0.0189	4.55	18.20	Trap/Vee/Rect Channel Flow,				
					Bot.W=1.00' D=1.00' Z= 3.0 '/' Top.W=7.00'				
					n= 0.030 Short grass				
11.9	447	Total							

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 3.97 cfs @ 12.11 hrs, Volume= 0.307 af, Depth> 5.76"

Routed to Reach AP4: Analysis Point 4

A	rea (sf)	CN	Description				
	2,555	98	Roofs, HSG C				
	1,571	98	aved parking, HSG C				
	5,912	74	>75% Grass cover, Good, HSG C				
	17,799	73	Woods, Fair, HSG C				
	27,837	77	Weighted Average				
	23,711		85.18% Pervious Area				
	4,126		14.82% Impervious Area				

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1.9	14	0.0210	0.13		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	4.2	36	0.1280	0.14		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	0.5	50	0.1280	1.79		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	1.0	87	0.0800	1.41		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.2	29	0.2860	2.67		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	7.8	216	Total	·		

Summary for Reach 2R: Flow across Map 222 Lot 20

Inflow Area = 0.060 ac, 0.00% Impervious, Inflow Depth > 5.40" for 50 Yr 24 Hr +15% event

Inflow = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af

Outflow = 0.35 cfs @ 12.12 hrs, Volume= 0.027 af, Atten= 4%, Lag= 1.5 min

Routed to Reach 3R: Flow over Sagamore Ave

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.38 fps, Min. Travel Time= 2.3 min Avg. Velocity = 0.13 fps, Avg. Travel Time= 6.6 min

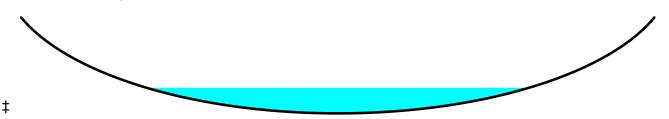
Peak Storage= 48 cf @ 12.12 hrs

Average Depth at Peak Storage= 0.13', Surface Width= 10.32' Bank-Full Depth= 0.50' Flow Area= 6.7 sf, Capacity= 6.22 cfs

20.00' x 0.50' deep Parabolic Channel, n= 0.150 Sheet flow over Short Grass

Length= 52.0' Slope= 0.0385 '/'

Inlet Invert= 66.00', Outlet Invert= 64.00'



Summary for Reach 3R: Flow over Sagamore Ave

[90] Warning: Qout>Qin may require smaller dt or Finer Routing [62] Hint: Exceeded Reach 2R OUTLET depth by 0.08' @ 12.05 hrs

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 6.78" for 50 Yr 24 Hr +15% event

Inflow = 3.92 cfs @ 12.09 hrs, Volume= 0.301 af

Outflow = 3.93 cfs @ 12.10 hrs, Volume= 0.301 af, Atten= 0%, Lag= 0.4 min

Routed to Reach AP1 : Analysis Point 1

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.53 fps, Min. Travel Time= 0.5 min

Avg. Velocity = 1.38 fps, Avg. Travel Time= 1.2 min

Peak Storage= 112 cf @ 12.10 hrs

Average Depth at Peak Storage= 0.21', Surface Width= 10.60' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 39.77 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25' Length= 101.0' Slope= 0.0297 '/'

Inlet Invert= 64.00', Outlet Invert= 61.00'

‡

Summary for Reach 4R: Flow over Sagamore Ave and Tidewatch Road

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 6.78" for 50 Yr 24 Hr +15% event

Inflow = 3.93 cfs @ 12.10 hrs, Volume= 0.301 af

Outflow = 3.92 cfs @ 12.11 hrs, Volume= 0.301 af, Atten= 0%, Lag= 0.5 min

Routed to Reach 5R: Flow over Tidewatch Road

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.73 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.46 fps, Avg. Travel Time= 1.7 min

Peak Storage= 152 cf @ 12.11 hrs

Average Depth at Peak Storage= 0.20', Surface Width= 10.29' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 42.85 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 145.0' Slope= 0.0345 '/'

Inlet Invert= 61.00', Outlet Invert= 56.00'

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Summary for Reach 5R: Flow over Tidewatch Road

[61] Hint: Exceeded Reach 4R outlet invert by 0.18' @ 12.10 hrs

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 6.78" for 50 Yr 24 Hr +15% event

Inflow = 3.92 cfs @ 12.11 hrs, Volume= 0.301 af

Outflow = 3.85 cfs @ 12.12 hrs, Volume= 0.301 af, Atten= 2%, Lag= 0.8 min

Routed to Reach AP3: Analysis Point 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 4.42 fps, Min. Travel Time= 1.0 min Avg. Velocity = 1.74 fps, Avg. Travel Time= 2.4 min

Peak Storage= 220 cf @ 12.12 hrs

Average Depth at Peak Storage= 0.19', Surface Width= 9.37' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 54.28 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25'

Length= 253.0' Slope= 0.0553 '/'

Inlet Invert= 56.00', Outlet Invert= 42.00'

‡

Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.533 ac, 48.72% Impervious, Inflow Depth > 6.78" for 50 Yr 24 Hr +15% event

Inflow = 3.93 cfs @ 12.10 hrs, Volume= 0.301 af

Outflow = 3.93 cfs @ 12.10 hrs, Volume= 0.301 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 4R: Flow over Sagamore Ave and Tidewatch Road

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.060 ac, 0.00% Impervious, Inflow Depth > 5.40" for 50 Yr 24 Hr +15% event

Inflow = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af

Outflow = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 2R: Flow across Map 222 Lot 20

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.879 ac, 14.04% Impervious, Inflow Depth > 5.70" for 50 Yr 24 Hr +15% event

Inflow = 10.41 cfs @ 12.15 hrs, Volume= 0.892 af

Outflow = 10.41 cfs @ 12.15 hrs, Volume= 0.892 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.639 ac, 14.82% Impervious, Inflow Depth > 5.76" for 50 Yr 24 Hr +15% event

Inflow = 3.97 cfs @ 12.11 hrs, Volume= 0.307 af

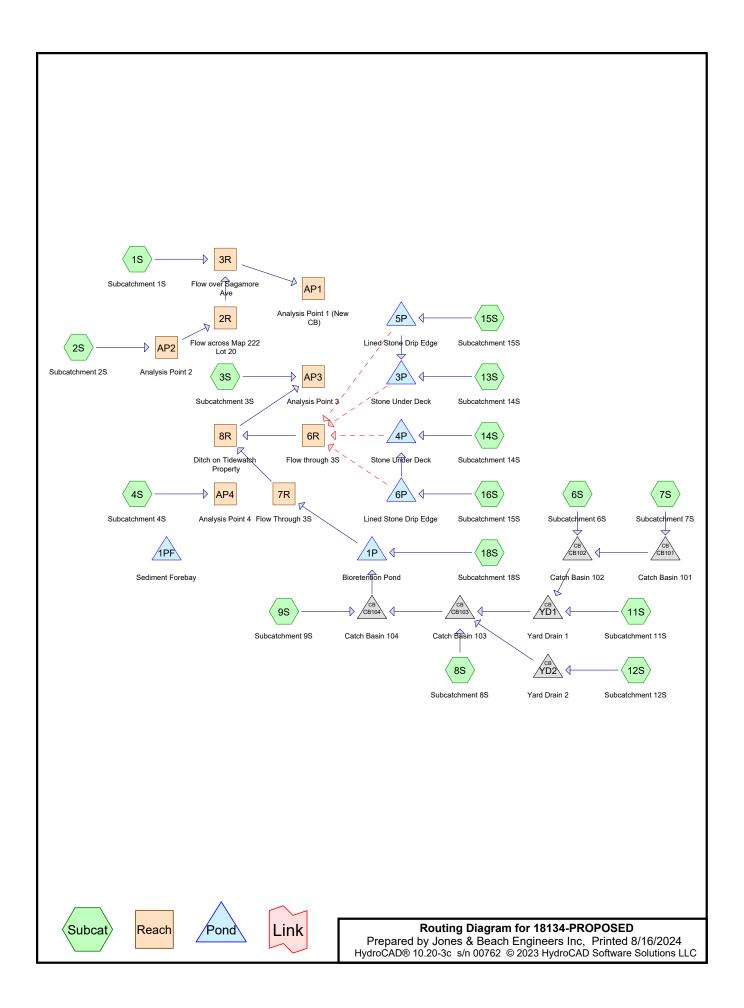
Outflow = 3.97 cfs @ 12.11 hrs, Volume= 0.307 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

APPENDIX II

PROPOSED CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Complete 10 YEAR Summary 25 YEAR Complete 50 YEAR



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Area Listing (all nodes)

Are	a CN	Description
(acres	s)	(subcatchment-numbers)
1.15	5 74	>75% Grass cover, Good, HSG C (1S, 2S, 3S, 4S, 11S, 12S, 18S)
0.28	7 98	Paved parking, HSG C (1S, 6S, 7S, 8S, 9S, 11S, 18S)
0.24	1 98	Roofs, HSG C (1S, 4S, 8S, 11S, 12S, 13S, 14S, 15S, 16S, 18S)
0.00	9 98	Water Surface, 0% imp, HSG C (15S, 16S)
0.82	6 73	Woods, Fair, HSG C (3S, 4S)
2.51	8 79	TOTAL AREA

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Soil Listing (all nodes)

Are	ea Soil	Subcatchment
(acres	s) Group	Numbers
0.00	0 HSG A	
0.00	0 HSG B	
2.51	8 HSG C	1S, 2S, 3S, 4S, 6S, 7S, 8S, 9S, 11S, 12S, 13S, 14S, 15S, 16S, 18S
0.00	0 HSG D	
0.00	0 Other	
2.51	18	TOTAL AREA

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-inc	Thethod - Folid fodding by Dyff-Stof-ilid method
Subcatchment1S: Subcatchment1S	Runoff Area=16,321 sf 51.36% Impervious Runoff Depth>2.27" Flow Length=186' Tc=6.0 min CN=86 Runoff=0.98 cfs 0.071 af
Subcatchment2S: Subcatchment2S Flow Length=20'	Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>1.38" Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.06 cfs 0.005 af
Subcatchment3S: Subcatchment3S	Runoff Area=44,464 sf 0.00% Impervious Runoff Depth>1.31" low Length=447' Tc=11.9 min CN=73 Runoff=1.23 cfs 0.112 af
Subcatchment4S: Subcatchment4S	Runoff Area=20,991 sf 8.04% Impervious Runoff Depth>1.51" Flow Length=210' Tc=6.2 min CN=76 Runoff=0.82 cfs 0.061 af
Subcatchment6S: Subcatchment6S	Runoff Area=1,084 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af
Subcatchment7S: Subcatchment7S	Runoff Area=954 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.08 cfs 0.006 af
Subcatchment8S: Subcatchment8S	Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.24 cfs 0.020 af
Subcatchment9S: Subcatchment9S	Runoff Area=325 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.03 cfs 0.002 af
Subcatchment11S: Subcatchment11S Flow Length=77'	Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>2.27" Slope=0.0396 '/' Tc=6.0 min CN=86 Runoff=0.27 cfs 0.020 af
Subcatchment12S: Subcatchment12S Flow Length=50'	Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>1.95" Slope=0.0320 '/' Tc=6.0 min CN=82 Runoff=0.19 cfs 0.014 af
Subcatchment13S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment14S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment15S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment16S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment18S: Subcatchment18S	Runoff Area=9,821 sf 17.16% Impervious Runoff Depth>1.65" Flow Length=58' Tc=6.0 min CN=78 Runoff=0.42 cfs 0.031 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.06' Max Vel=0.22 fps Inflow=0.06 cfs 0.005 af

n=0.150 L=52.0' S=0.0385 '/' Capacity=6.22 cfs Outflow=0.05 cfs 0.005 af

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

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Reach 3R: Flow over Sagamore AveAvg. Flow Depth=0.13' Max Vel=2.52 fps Inflow=1.03 cfs 0.076 af n=0.016 L=101.0' S=0.0297'/' Capacity=39.77 cfs Outflow=1.02 cfs 0.076 af

Reach 6R: Flow through 3SAvg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af n=0.030 L=81.0' S=0.3457'/ Capacity=740.30 cfs Outflow=0.00 cfs 0.000 af

Reach 7R: Flow Through 3SAvg. Flow Depth=0.10' Max Vel=3.09 fps Inflow=1.08 cfs 0.045 af n=0.030 L=220.0' S=0.0909 '/' Capacity=66.79 cfs Outflow=1.08 cfs 0.045 af

Reach 8R: Ditch on Tidewatch Property Avg. Flow Depth=0.27' Max Vel=2.16 fps Inflow=1.08 cfs 0.045 af n=0.030 L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=1.05 cfs 0.045 af

Reach AP1: Analysis Point 1 (New CB)

Inflow=1.02 cfs 0.076 af
Outflow=1.02 cfs 0.076 af

Reach AP2: Analysis Point 2 Inflow=0.06 cfs 0.005 af Outflow=0.06 cfs 0.005 af

Reach AP3: Analysis Point 3 Inflow=2.24 cfs 0.157 af
Outflow=2.24 cfs 0.157 af

Reach AP4: Analysis Point 4 Inflow=0.82 cfs 0.061 af

Outflow=0.82 cfs 0.061 af

Pond 1P: Bioretention Pond

Peak Elev=59.91' Storage=61 cf Inflow=1.32 cfs 0.100 af

Discarded=0.23 cfs 0.055 af Primary=1.08 cfs 0.045 af Outflow=1.32 cfs 0.100 af

Pond 1PF: Sediment Forebay Peak Elev=0.00' Storage=0 cf

Pond 3P: Stone Under Deck
Peak Elev=64.99' Storage=0.005 af Inflow=0.11 cfs 0.009 af
Discarded=0.00 cfs 0.005 af Secondary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.005 af

Pond 4P: Stone Under Deck
Peak Elev=65.95' Storage=0.005 af Inflow=0.11 cfs 0.009 af
Discarded=0.00 cfs 0.005 af Secondary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.005 af

Pond 5P: Lined Stone Drip Edge Peak Elev=66.05' Storage=0.000 af Inflow=0.06 cfs 0.005 af Primary=0.06 cfs 0.005 af Secondary=0.00 cfs 0.000 af Outflow=0.06 cfs 0.005 af

Pond 6P: Lined Stone Drip Edge Peak Elev=66.05' Storage=0.000 af Inflow=0.06 cfs 0.005 af Primary=0.06 cfs 0.005 af Secondary=0.00 cfs 0.000 af Outflow=0.06 cfs 0.005 af

Pond CB101: Catch Basin 101 Peak Elev=66.78' Inflow=0.08 cfs 0.006 af

12.0" Round Culvert n=0.012 L=14.0' S=0.0071 '/' Outflow=0.08 cfs 0.006 af

Pond CB102: Catch Basin 102 Peak Elev=66.69' Inflow=0.16 cfs 0.014 af 12.0" Round Culvert n=0.012 L=15.0' S=0.0067 '/' Outflow=0.16 cfs 0.014 af

Pond CB103: Catch Basin 103 Peak Elev=66.36' Inflow=0.87 cfs 0.067 af 12.0" Round Culvert n=0.012 L=43.0' S=0.0070 '/' Outflow=0.87 cfs 0.067 af

Type III 24-hr 2 Yr 24 Hr +15% Rainfall=3.70"

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Pond CB104: Catch Basin 104 Peak Elev=65.97' Inflow=0.90 cfs 0.069 af

12.0" Round Culvert n=0.012 L=31.0' S=0.0065 '/' Outflow=0.90 cfs 0.069 af

Pond YD1: Yard Drain 1 Peak Elev=66.62' Inflow=0.44 cfs 0.033 af

12.0" Round Culvert n=0.012 L=52.0' S=0.0058 '/' Outflow=0.44 cfs 0.033 af

Pond YD2: Yard Drain 2 Peak Elev=67.28' Inflow=0.19 cfs 0.014 af

8.0" Round Culvert n=0.012 L=13.0' S=0.0669 '/' Outflow=0.19 cfs 0.014 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.366 af Average Runoff Depth = 1.74" 79.02% Pervious = 1.990 ac 20.98% Impervious = 0.528 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

3 , ,	0 , ,
Subcatchment1S: Subcatchment1S	Runoff Area=16,321 sf 51.36% Impervious Runoff Depth>4.04" Flow Length=186' Tc=6.0 min CN=86 Runoff=1.70 cfs 0.126 af
Subcatchment2S: Subcatchment2S Flow Length=20'	Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>2.86" Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.13 cfs 0.009 af
Subcatchment3S: Subcatchment3S	Runoff Area=44,464 sf 0.00% Impervious Runoff Depth>2.76" low Length=447' Tc=11.9 min CN=73 Runoff=2.70 cfs 0.235 af
Subcatchment4S: Subcatchment4S	Runoff Area=20,991 sf 8.04% Impervious Runoff Depth>3.04" Flow Length=210' Tc=6.2 min CN=76 Runoff=1.68 cfs 0.122 af
Subcatchment6S: Subcatchment6S	Runoff Area=1,084 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.13 cfs 0.011 af
Subcatchment7S: Subcatchment7S	Runoff Area=954 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.12 cfs 0.010 af
Subcatchment8S: Subcatchment8S	Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.37 cfs 0.031 af
Subcatchment9S: Subcatchment9S	Runoff Area=325 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.04 cfs 0.003 af
Subcatchment11S: Subcatchment11S Flow Length=77'	Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>4.04" Slope=0.0396 '/' Tc=6.0 min CN=86 Runoff=0.48 cfs 0.035 af
Subcatchment12S: Subcatchment12S Flow Length=50'	Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>3.63" Slope=0.0320 '/' Tc=6.0 min CN=82 Runoff=0.35 cfs 0.026 af
Subcatchment13S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment14S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment15S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af
Subcatchment16S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af
Subcatchment18S: Subcatchment18S	Runoff Area=9,821 sf 17.16% Impervious Runoff Depth>3.23" Flow Length=58' Tc=6.0 min CN=78 Runoff=0.84 cfs 0.061 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.08' Max Vel=0.28 fps Inflow=0.13 cfs 0.009 af

n=0.150 L=52.0' S=0.0385 '/' Capacity=6.22 cfs Outflow=0.12 cfs 0.009 af

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Reach 3R: Flow over Sagamore AveAvg. Flow Depth=0.16' Max Vel=2.91 fps Inflow=1.81 cfs 0.135 af n=0.016 L=101.0' S=0.0297 '/' Capacity=39.77 cfs Outflow=1.82 cfs 0.135 af

Reach 6R: Flow through 3S Avg. Flow Depth=0.00' Max Vel=1.03 fps Inflow=0.02 cfs 0.001 af

n=0.030 L=81.0' S=0.3457 '/' Capacity=740.30 cfs Outflow=0.02 cfs 0.001 af

Reach 7R: Flow Through 3SAvg. Flow Depth=0.12' Max Vel=3.45 fps Inflow=1.46 cfs 0.095 af n=0.030 L=220.0' S=0.0909 '/' Capacity=66.79 cfs Outflow=1.45 cfs 0.095 af

11-0.000 L-220.0 0-0.0000 / Oupdoity-00.70 013 Outilow-1.40 013 0.000 df

Reach 8R: Ditch on Tidewatch Property Avg. Flow Depth=0.32' Max Vel=2.37 fps Inflow=1.45 cfs 0.096 af n=0.030 L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=1.46 cfs 0.096 af

Reach AP1: Analysis Point 1 (New CB)

Inflow=1.82 cfs 0.135 af
Outflow=1.82 cfs 0.135 af

Reach AP2: Analysis Point 2 Inflow=0.13 cfs 0.009 af
Outflow=0.13 cfs 0.009 af

Reach AP3: Analysis Point 3 Inflow=4.16 cfs 0.331 af

Outflow=4.16 cfs 0.331 af

Reach AP4: Analysis Point 4 Inflow=1.68 cfs 0.122 af

Outflow=1.68 cfs 0.122 af

Pond 1P: Bioretention Pond

Peak Elev=60.98' Storage=212 cf Inflow=2.33 cfs 0.177 af

Discarded=0.46 cfs 0.082 af Primary=1.46 cfs 0.095 af Outflow=1.92 cfs 0.177 af

Pond 1PF: Sediment Forebay Peak Elev=0.00' Storage=0 cf

Pond 3P: Stone Under Deck Peak Elev=66.20' Storage=0.008 af Inflow=0.17 cfs 0.014 af Discarded=0.01 cfs 0.007 af Secondary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.007 af

Pond 4P: Stone Under Deck
Peak Elev=67.08' Storage=0.008 af Inflow=0.17 cfs 0.014 af
Discarded=0.01 cfs 0.007 af Secondary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.007 af

Pond 5P: Lined Stone Drip Edge Peak Elev=66.20' Storage=0.000 af Inflow=0.10 cfs 0.008 af Primary=0.10 cfs 0.008 af Secondary=0.00 cfs 0.000 af Outflow=0.10 cfs 0.008 af

Pond 6P: Lined Stone Drip Edge Peak Elev=67.00' Storage=0.001 af Inflow=0.10 cfs 0.008 af Primary=0.10 cfs 0.008 af Secondary=0.02 cfs 0.001 af Outflow=0.10 cfs 0.007 af

Pond CB101: Catch Basin 101 Peak Elev=66.88' Inflow=0.12 cfs 0.010 af

12.0" Round Culvert n=0.012 L=14.0' S=0.0071 '/' Outflow=0.12 cfs 0.010 af

Pond CB102: Catch Basin 102 Peak Elev=66.85' Inflow=0.25 cfs 0.021 af

12.0" Round Culvert n=0.012 L=15.0' S=0.0067 '/' Outflow=0.25 cfs 0.021 af

Pond CB103: Catch Basin 103 Peak Elev=66.59' Inflow=1.45 cfs 0.113 af

12.0" Round Culvert n=0.012 L=43.0' S=0.0070 '/' Outflow=1.45 cfs 0.113 af

Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

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Pond CB104: Catch Basin 104 Peak Elev=66.18' Inflow=1.49 cfs 0.116 af

12.0" Round Culvert n=0.012 L=31.0' S=0.0065 '/' Outflow=1.49 cfs 0.116 af

Pond YD1: Yard Drain 1 Peak Elev=66.81' Inflow=0.73 cfs 0.056 af

12.0" Round Culvert n=0.012 L=52.0' S=0.0058 '/' Outflow=0.73 cfs 0.056 af

Pond YD2: Yard Drain 2 Peak Elev=67.39' Inflow=0.35 cfs 0.026 af

8.0" Round Culvert n=0.012 L=13.0' S=0.0669 '/' Outflow=0.35 cfs 0.026 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.697 af Average Runoff Depth = 3.32" 79.02% Pervious = 1.990 ac 20.98% Impervious = 0.528 ac

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 1.70 cfs @ 12.09 hrs, Volume=

0.126 af, Depth> 4.04"

Routed to Reach 3R: Flow over Sagamore Ave

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Α	rea (sf)	CN [Description						
		6,930	98 F	98 Paved parking, HSG C						
		7,938	74 >	· · · · · · · · · · · · · · · · · · ·						
		1,453	98 F	Roofs, HSC	G C					
		16,321	86 \	Neighted A	verage					
		7,938	4	18.64% Pe	rvious Area					
		8,383	5	51.36% Imp	pervious Ar	ea				
	Тс	Length	Slope	•	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	2.5	50	0.1250	0.33		Sheet Flow,				
						Grass: Short n= 0.150 P2= 3.70"				
	0.0	6	0.1250	2.47		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.3	30	0.0670	1.81		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.4	100	0.0360	3.85		Shallow Concentrated Flow,				
						Paved Kv= 20.3 fps				
	3.2	186	Total,	Increased t	to minimum	Tc = 6.0 min				

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.13 cfs @ 12.09 hrs, Volume=

0.009 af, Depth> 2.86"

Routed to Reach AP2 : Analysis Point 2

	Aı	rea (sf)	CN	Description								
		1,728	74	74 >75% Grass cover, Good, HSG C								
		1,728		100.00% Pervious Area								
	Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	Description						
_	1.3	20	0.1000	0.25		Sheet Flow,						
						Grass: Short	n= 0.150	P2= 3.70"				
	1.3	20	Total,	Increased t	o minimum	Tc = 6.0 min						

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Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 2.70 cfs @ 12.17 hrs, Volume= 0.235 af, Depth> 2.76"

Routed to Reach AP3: Analysis Point 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Α	rea (sf)	CN D	escription		
		16,641			•	ood, HSG C
		27,823	<u>73 V</u>	<u>Voods, Fai</u>	r, HSG C	
		44,464	73 V	Veighted A	verage	
		44,464	1	00.00% Pe	ervious Are	a
	Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	8.6	50	0.0415	0.10		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	0.7	62	0.0968	1.56		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.7	54	0.0741	1.36		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	1.3	122	0.1000	1.58		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.6	159	0.0189	4.55	18.20	Trap/Vee/Rect Channel Flow,
	0.0	.00	0.0.00		.0.20	Bot.W=1.00' D=1.00' Z= 3.0 '/' Top.W=7.00'
						n= 0.030 Short grass
	11.9	447	Total			0.000 0 9.2.00
		771	rotai			

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 1.68 cfs @ 12.10 hrs, Volume= 0.122 af, Depth> 3.04"

Routed to Reach AP4: Analysis Point 4

 Area (sf)	CN	Description					
11,135	74	75% Grass cover, Good, HSG C					
8,169	73	Woods, Fair, HSG C					
 1,687	98	Roofs, HSG C					
20,991	76	Weighted Average					
19,304		91.96% Pervious Area					
1,687		8.04% Impervious Area					

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_					(013)	
	1.5	14	0.0357	0.16		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	1.9	14	0.1429	0.12		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	1.3	22	0.1333	0.29		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.3	50	0.1333	2.56		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	1.0	80	0.0750	1.37		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.2	30	0.2667	2.58		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	6.2	210	Total			

Summary for Subcatchment 6S: Subcatchment 6S

Runoff = 0.13 cfs @ 12.09 hrs, Volume=

0.011 af, Depth> 5.37"

Routed to Pond CB102 : Catch Basin 102

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN I	Description							
	1,084	98 I	98 Paved parking, HSG C							
	1,084		100.00% Impervious Area							
Тс	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
6.0					Direct Entry,					

Summary for Subcatchment 7S: Subcatchment 7S

Runoff = 0.12 cfs @ 12.09 hrs, Volume=

0.010 af, Depth> 5.37"

Routed to Pond CB101: Catch Basin 101

A	rea (sf)	CN E	CN Description							
	954	98 F	98 Paved parking, HSG C							
	954	1	100.00% Impervious Area							
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
6.0					Direct Entry,					

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Summary for Subcatchment 8S: Subcatchment 8S

Runoff 0.37 cfs @ 12.09 hrs, Volume= 0.031 af, Depth> 5.37"

Routed to Pond CB103: Catch Basin 103

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN	Description						
	2,554	98	Paved parking, HSG C						
	457	98	Roofs, HSG	S C					
	3,011	98	Weighted A	Weighted Average					
	3,011		100.00% Impervious Area						
Tc	Length	Slope	e Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)					
6.0					Direct Entry,				

Direct Entry,

Summary for Subcatchment 9S: Subcatchment 9S

Runoff 0.04 cfs @ 12.09 hrs, Volume= 0.003 af, Depth> 5.37"

Routed to Pond CB104: Catch Basin 104

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Α	rea (sf)	CN [Description	Description							
		325	98 F	Paved park	eved parking, HSG C							
		325	•	100.00% Impervious Area								
	Tc	Length	Slope	Velocity	Capacity	Description						
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
-	6.0					Direct Entry.						

Summary for Subcatchment 11S: Subcatchment 11S

0.035 af, Depth> 4.04" 0.48 cfs @ 12.09 hrs, Volume=

Routed to Pond YD1: Yard Drain 1

Area (sf)	CN	Description				
1,998	98	Roofs, HSG C				
2,312	74	>75% Grass cover, Good, HSG C				
261	98	Paved parking, HSG C				
4,571	86	Weighted Average				
2,312		50.58% Pervious Area				
2,259		49.42% Impervious Area				

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	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	4.0	50	0.0396	0.21		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.3	27	0.0396	1.39		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	4.0					T 00 :

4.3 77 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 12S: Subcatchment 12S

Runoff = 0.35 cfs @ 12.09 hrs, Volume=

0.026 af, Depth> 3.63"

Routed to Pond YD2: Yard Drain 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

_	Α	rea (sf)	CN	Description						
		1,318	98	Roofs, HSG	G C					
_		2,416	74	>75% Gras	s cover, Go	ood, HSG C				
		3,734	82	Weighted A	verage					
		2,416		64.70% Per	rvious Area	1				
		1,318		35.30% Imp	pervious Ar	ea				
	_				_					
	Tc	Length	Slope	,	Capacity	Description				
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)					
	4.3	50	0.0320	0.19		Sheet Flow,				
						Grass: Short	n= 0.150	P2= 3.70"		
	12	50	Total	Ingrasad t	o minimum	To = 6.0 min				

4.3 50 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 13S: Subcatchment 14S

Runoff = 0.07 cfs @ 12.09 hrs, Volume=

0.006 af, Depth> 5.37"

Routed to Pond 3P: Stone Under Deck

A	rea (sf)	CN [Description							
	560	98 F	98 Roofs, HSG C							
	560	1	100.00% Impervious Area							
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
6.0					Direct Entry,					

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Summary for Subcatchment 14S: Subcatchment 14S

Runoff = 0.07 cfs @ 12.09 hrs, Volume=

0.006 af, Depth> 5.37"

Routed to Pond 4P: Stone Under Deck

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Area (s	f)	CN	Description						
	56	60	98	8 Roofs, HSG C						
	56	0		100.00% Impervious Area						
T (mir	c Lenç	_	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
6.	0					Direct Entry,				

Summary for Subcatchment 15S: Subcatchment 15S

Runoff = 0.10 cfs @ 12.09 hrs, Volume=

0.008 af, Depth> 5.37"

Routed to Pond 5P: Lined Stone Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN	Description				
	590	98	Roofs, HSC	G C			
	189	98	Water Surfa	ace, 0% imp	np, HSG C		
	779	98	Weighted Average				
	189		24.26% Pe	vious Area	a		
	590		75.74% lm	pervious Ar	rea		
т.	ما العرب ما	Clana	\/alaaitu	Consoitu	Description		
Tc	Length	Slope	•	Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)			
6.0					Direct Entry,		

Summary for Subcatchment 16S: Subcatchment 15S

Runoff = 0.10 cfs @ 12.09 hrs, Volume=

0.008 af, Depth> 5.37"

Routed to Pond 6P: Lined Stone Drip Edge

	Area (sf)	CN	Description
•	590	98	Roofs, HSG C
	189	98	Water Surface, 0% imp, HSG C
•	779	98	Weighted Average
	189		24.26% Pervious Area
	590		75.74% Impervious Area

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Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
6.0					Direct Entry,	

Summary for Subcatchment 18S: Subcatchment 18S

Runoff = 0.84 cfs @ 12.09 hrs, Volume=

0.061 af, Depth> 3.23"

Routed to Pond 1P: Bioretention Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

_	Α	rea (sf)	CN I	Description				
		8,136	74 >	74 >75% Grass cover, Good, HSG C				
		1,285	98 I	98 Roofs, HSG C				
		400	98 I	98 Paved parking, HSG C				
		9,821	78 \	78 Weighted Average				
		8,136	8	32.84% Pe	rvious Area	l .		
		1,685	•	17.16% lm <mark>։</mark>	pervious Ar	ea		
	Tc	Length	Slope	•	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	2.5	43	0.0930	0.29		Sheet Flow,		
						Grass: Short n= 0.150 P2= 3.70"		
	0.4	7	0.3333	0.33		Sheet Flow,		
						Grass: Short n= 0.150 P2= 3.70"		
	0.0	8	0.3333	4.04		Shallow Concentrated Flow,		
_						Short Grass Pasture Kv= 7.0 fps		
	2.0	E0.	Tatal	1		To - C 0 main		

2.9 58 Total, Increased to minimum Tc = 6.0 min

Summary for Reach 2R: Flow across Map 222 Lot 20

Inflow Area = 0.040 ac. 0.00% Impervious, Inflow Depth > 2.86" for 10 Yr 24 Hr +15% event

Inflow = 0.13 cfs @ 12.09 hrs, Volume= 0.009 af

Outflow = 0.12 cfs @ 12.13 hrs, Volume= 0.009 af, Atten= 8%, Lag= 2.2 min

Routed to Reach 3R: Flow over Sagamore Ave

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.28 fps, Min. Travel Time= 3.1 min

Avg. Velocity = 0.10 fps, Avg. Travel Time= 8.6 min

Peak Storage= 22 cf @ 12.13 hrs

Average Depth at Peak Storage= 0.08', Surface Width= 8.03' Bank-Full Depth= 0.50' Flow Area= 6.7 sf, Capacity= 6.22 cfs

20.00' x 0.50' deep Parabolic Channel, n= 0.150 Sheet flow over Short Grass

Length= 52.0' Slope= 0.0385 '/'

Inlet Invert= 66.00', Outlet Invert= 64.00'

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Summary for Reach 3R: Flow over Sagamore Ave

[90] Warning: Qout>Qin may require smaller dt or Finer Routing [62] Hint: Exceeded Reach 2R OUTLET depth by 0.08' @ 12.05 hrs

Inflow Area = 0.414 ac, 46.45% Impervious, Inflow Depth > 3.92" for 10 Yr 24 Hr +15% event

Inflow = 1.81 cfs @ 12.09 hrs, Volume= 0.135 af

Outflow = 1.82 cfs @ 12.10 hrs, Volume= 0.135 af, Atten= 0%, Lag= 0.5 min

Routed to Reach AP1: Analysis Point 1 (New CB)

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 2.91 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.16 fps, Avg. Travel Time= 1.5 min

Peak Storage= 63 cf @ 12.10 hrs

Inlet Invert= 64.00', Outlet Invert= 61.00'

Average Depth at Peak Storage= 0.16', Surface Width= 7.93' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 39.77 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25' Length= 101.0' Slope= 0.0297 '/'

‡

Summary for Reach 6R: Flow through 3S

Inflow = 0.02 cfs @ 12.59 hrs, Volume= 0.001 af

Outflow = 0.02 cfs @ 12.61 hrs, Volume= 0.001 af, Atten= 10%, Lag= 1.2 min

Routed to Reach 8R: Ditch on Tidewatch Property

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 1.03 fps, Min. Travel Time= 1.3 min

Avg. Velocity = 1.03 fps, Avg. Travel Time= 1.3 min

Peak Storage= 1 cf @ 12.61 hrs

Average Depth at Peak Storage= 0.00', Surface Width= 3.35'

Bank-Full Depth= 1.00' Flow Area= 33.3 sf, Capacity= 740.30 cfs

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50.00' x 1.00' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 81.0' Slope= 0.3457 '/' Inlet Invert= 66.00', Outlet Invert= 38.00'



Summary for Reach 7R: Flow Through 3S

Inflow Area = 0.539 ac, 45.26% Impervious, Inflow Depth = 2.11" for 10 Yr 24 Hr +15% event

Inflow = 1.46 cfs @ 12.14 hrs, Volume= 0.095 af

Outflow = 1.45 cfs @ 12.14 hrs, Volume= 0.095 af, Atten= 1%, Lag= 0.0 min

Routed to Reach 8R: Ditch on Tidewatch Property

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.45 fps, Min. Travel Time= 1.1 min Avg. Velocity = 1.15 fps, Avg. Travel Time= 3.2 min

Peak Storage= 92 cf @ 12.14 hrs

Average Depth at Peak Storage= 0.12', Surface Width= 3.75' Bank-Full Depth= 1.00' Flow Area= 6.0 sf, Capacity= 66.79 cfs

3.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 3.0 '/' Top Width= 9.00'

Length= 220.0' Slope= 0.0909 '/'

Inlet Invert= 58.00', Outlet Invert= 38.00'



Summary for Reach 8R: Ditch on Tidewatch Property

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[62] Hint: Exceeded Reach 6R OUTLET depth by 0.32' @ 12.15 hrs

[62] Hint: Exceeded Reach 7R OUTLET depth by 0.19' @ 12.15 hrs

Inflow Area = 0.539 ac, 45.26% Impervious, Inflow Depth = 2.14" for 10 Yr 24 Hr +15% event

Inflow = 1.45 cfs @ 12.14 hrs, Volume= 0.096 af

Outflow = 1.46 cfs @ 12.16 hrs, Volume= 0.096 af, Atten= 0%, Lag= 1.2 min

Routed to Reach AP3: Analysis Point 3

Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 2.37 fps, Min. Travel Time= 1.1 min

Avg. Velocity = 0.87 fps, Avg. Travel Time= 3.1 min

Peak Storage= 98 cf @ 12.16 hrs

Average Depth at Peak Storage= 0.32', Surface Width= 2.90' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.18 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 3.0 '/' Top Width= 7.00'

Length= 159.0' Slope= 0.0189 '/'

Inlet Invert= 38.00', Outlet Invert= 35.00'



Summary for Reach AP1: Analysis Point 1 (New CB)

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.414 ac, 46.45% Impervious, Inflow Depth > 3.92" for 10 Yr 24 Hr +15% event

Inflow = 1.82 cfs @ 12.10 hrs, Volume= 0.135 af

Outflow = 1.82 cfs @ 12.10 hrs, Volume= 0.135 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.040 ac, 0.00% Impervious, Inflow Depth > 2.86" for 10 Yr 24 Hr +15% event

Inflow = 0.13 cfs @ 12.09 hrs, Volume= 0.009 af

Outflow = 0.13 cfs @ 12.09 hrs, Volume= 0.009 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 2R: Flow across Map 222 Lot 20

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.560 ac, 15.65% Impervious, Inflow Depth > 2.55" for 10 Yr 24 Hr +15% event

Inflow = 4.16 cfs @ 12.17 hrs, Volume= 0.331 af

Outflow = 4.16 cfs @ 12.17 hrs, Volume= 0.331 af, Atten= 0%, Lag= 0.0 min

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.482 ac, 8.04% Impervious, Inflow Depth > 3.04" for 10 Yr 24 Hr +15% event

1.68 cfs @ 12.10 hrs, Volume= Inflow 0.122 af

Outflow 1.68 cfs @ 12.10 hrs, Volume= 0.122 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Bioretention Pond

Existing high contour within footprint of filter course = 61.0, SHWT depth = 35" per TP 10, so SHWT EI. = 58.08, which is 0.01' below the bottom of stone. However, in our experience, modelling the SHWTwith such a small separation to the bottom of stone causes an unrealistically high amount of infiltration to appear in the calculations. Therefore, the SHWT has been modelled 2" lower as a factor of safety.

0.539 ac, 45.26% Impervious, Inflow Depth > 3.94" for 10 Yr 24 Hr +15% event Inflow Area =

Inflow 2.33 cfs @ 12.09 hrs, Volume= 0.177 af

1.92 cfs @ 12.15 hrs, Volume= 0.177 af, Atten= 18%, Lag= 3.3 min Outflow

Discarded = 0.46 cfs @ 12.15 hrs, Volume= 0.082 af 1.46 cfs @ 12.14 hrs, Volume= 0.095 af Primary

Routed to Reach 7R: Flow Through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 60.98' @ 12.14 hrs Surf.Area= 683 sf Storage= 212 cf

Plug-Flow detention time= 2.0 min calculated for 0.177 af (100% of inflow)

Center-of-Mass det. time= 1.7 min (793.7 - 792.0)

Volume	Invert Ava	il.Storage	Storage	Description		
#1	58.09'	2,677 cf	Custon	n Stage Data (Irreg	gular)Listed below	(Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
58.09	117	48.0	0.0	0	0	117
58.10	117	48.0	40.0	0	0	117
59.09	117	48.0	40.0	46	47	165
59.10	117	48.0	15.0	0	47	165
60.59	117	48.0	15.0	26	73	237
60.60	117	48.0	100.0	1	74	237
60.99	702	116.0	100.0	144	218	1,126
61.00	1,026	144.0	100.0	9	227	1,705
62.00	1,487	163.0	100.0	1,249	1,476	2,194
62.70	1,898	178.0	100.0	1,182	2,658	2,618
62.71	1,898	178.0	100.0	19	2,677	2,620

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Device	Routing	Invert	Outlet Devices
#1	Primary	58.35'	12.0" Round Culvert
	·		L= 20.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 58.35' / 58.00' S= 0.0175 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf
#2	Device 1	58.35'	6.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	61.70'	18.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Discarded	58.09'	7.400 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 57.92' Phase-In= 0.10'

Discarded OutFlow Max=0.46 cfs @ 12.15 hrs HW=60.97' (Free Discharge) **4=Exfiltration** (Controls 0.46 cfs)

Primary OutFlow Max=1.46 cfs @ 12.14 hrs HW=60.97' TW=58.12' (Dynamic Tailwater)

1=Culvert (Passes 1.46 cfs of 4.35 cfs potential flow)

2=Orifice/Grate (Orifice Controls 1.46 cfs @ 7.42 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 1PF: Sediment Forebay

[43] Hint: Has no inflow (Outflow=Zero)

Volume	Invert	Avail.Storag	e Storage	Description		
#1	59.00'	231 c	f Custom	n Stage Data (Pris	matic)Listed below (Recalc)	_
Elevation (feet)	Surf (s		nc.Store ıbic-feet)	Cum.Store (cubic-feet)		
59.00 60.00 61.00		15 101 245	0 58 173	0 58 231		

Summary for Pond 3P: Stone Under Deck

Ledge surface modelled 24" below original grade based on TP 13 (Bedrock found from 24" to 36". Proposed grade is approximately 3.2' above existing grade and therefore 5.2' above ledge.

Inflow Area = 0.031 ac, 85.88% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event Inflow = 0.17 cfs @ 12.09 hrs, Volume= 0.014 af

Outflow = 0.01 cfs @ 14.27 hrs, Volume= 0.007 af, Atten= 95%, Lag= 130.9 min

Discarded = 0.00 cfs @ 14.20 hrs, Volume= 0.007 af

Secondary = 0.00 cfs @ 14.27 hrs, Volume= 0.000 af

Routed to Reach 6R : Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.20' @ 14.20 hrs Surf.Area= 0.006 ac Storage= 0.008 af

Plug-Flow detention time= 327.0 min calculated for 0.007 af (49% of inflow) Center-of-Mass det. time= 190.7 min (942.0 - 751.3)

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Volume	Invert	Avail.Storage	Storage Description
#1	62.90'	0.008 af	14.00'W x 20.00'L x 3.30'H Prismatoid 0.021 af Overall x 40.0% Voids
Device	Routing	Invert Ou	utlet Devices
#0	Secondary	66.20' A u	stomatic Storage Overflow (Discharged without head)
#1	Discarded	62.90' 0.3	300 in/hr Exfiltration over Surface area
		Co	onductivity to Groundwater Elevation = 61.00' Phase-In= 0.10'

Discarded OutFlow Max=0.01 cfs @ 14.20 hrs HW=66.20' (Free Discharge) 1=Exfiltration (Controls 0.01 cfs)

Secondary OutFlow Max=0.00 cfs @ 14.27 hrs HW=66.20' TW=66.00' (Dynamic Tailwater)

Summary for Pond 4P: Stone Under Deck

Ledge surface modelled 20" below original grade based on TP 12 (Bedrock ranging from 20" to 28". Proposed grade is approximately 3.2' above existing grade and therefore 4.87' above ledge.

[80] Warning: Exceeded Pond 6P by 0.08' @ 13.05 hrs (0.27 cfs 0.041 af)

Inflow Area = 0.031 ac, 85.88% Impervious, Inflow Depth > 5.33" for 10 Yr 24 Hr +15% event Inflow = 0.17 cfs @ 12.09 hrs, Volume= 0.014 af

Outflow = 0.01 cfs @ 13.01 hrs, Volume= 0.007 af, Atten= 96%, Lag= 55.1 min

Discarded = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach 6R : Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 67.08' @ 13.01 hrs Surf.Area= 0.006 ac Storage= 0.008 af

Plug-Flow detention time= 329.3 min calculated for 0.007 af (52% of inflow) Center-of-Mass det. time= 185.7 min (947.7 - 762.0)

Volume	Invert	Avail.Storage	Storage Description	
#1	63.90'	0.008 af	14.00'W x 20.00'L x 3.30'H Prismatoid 0.021 af Overall x 40.0% Voids	_
Device	Routing	Invert Ou	tlet Devices	_
#0	Secondary	67.20' A u	tomatic Storage Overflow (Discharged without head)	
#1	Discarded		00 in/hr Exfiltration over Surface area nductivity to Groundwater Elevation = 62.33' Phase-In= 0.10'	

Discarded OutFlow Max=0.01 cfs @ 13.01 hrs HW=67.08' (Free Discharge) 1=Exfiltration (Controls 0.01 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=63.90' TW=66.00' (Dynamic Tailwater)

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Summary for Pond 5P: Lined Stone Drip Edge

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=51)

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event

Inflow = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af

Outflow = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af, Atten= 0%, Lag= 0.5 min

Primary = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af

Routed to Pond 3P : Stone Under Deck

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach 6R: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.20' @ 14.25 hrs Surf.Area= 0.003 ac Storage= 0.000 af

Plug-Flow detention time= 9.8 min calculated for 0.008 af (100% of inflow) Center-of-Mass det. time= 9.5 min (755.3 - 745.7)

Volume	Invert	Avail.Storage	Storage Description
#1	66.00'	0.001 af	2.00'W x 63.00'L x 1.01'H Prismatoid
			0.003 af Overall x 40.0% Voids

Device	Routing	Invert	Outlet Devices
#0	Secondary	67.01'	Automatic Storage Overflow (Discharged without head)
#1	Primary	66.00'	6.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#2	Secondary	67.00'	63.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Primary OutFlow Max=0.09 cfs @ 12.09 hrs HW=66.07' TW=64.86' (Dynamic Tailwater) 1=Orifice/Grate (Weir Controls 0.09 cfs @ 0.86 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=66.00' TW=66.00' (Dynamic Tailwater)

2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 6P: Lined Stone Drip Edge

[44] Hint: Outlet device #1 is below defined storage

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=55)

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event

Inflow = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af

Outflow = 0.10 cfs @ 12.09 hrs, Volume= 0.007 af, Atten= 0%, Lag= 0.1 min

Primary = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af

Routed to Pond 4P : Stone Under Deck

Secondary = 0.02 cfs @ 12.59 hrs, Volume= 0.001 af

Routed to Reach 6R: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

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Peak Elev= 67.00' @ 12.60 hrs Surf.Area= 0.003 ac Storage= 0.001 af

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 41.0 min (786.8 - 745.7)

Volume	Invert	Avail.Storage	Storage Description
#1	66.01'	0.001 af	2.00'W x 63.00'L x 1.01'H Prismatoid 0.003 af Overall x 40.0% Voids
Device	Routing	Invert Οι	utlet Devices
#1	Primary		O" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#2	Secondary		.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			ead (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
		2.5	50 3.00
		Co	pef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
		3.3	30 3.31 3.32

Primary OutFlow Max=0.09 cfs @ 12.09 hrs HW=66.07' TW=65.81' (Dynamic Tailwater) 1=Orifice/Grate (Weir Controls 0.09 cfs @ 0.86 fps)

Secondary OutFlow Max=0.02 cfs @ 12.59 hrs HW=67.00' TW=66.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Weir Controls 0.02 cfs @ 0.12 fps)

Summary for Pond CB101: Catch Basin 101

Inflow Area = 0.022 ac,100.00% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event

Inflow = 0.12 cfs @ 12.09 hrs, Volume= 0.010 af

Outflow = 0.12 cfs @ 12.09 hrs, Volume= 0.010 af, Atten= 0%, Lag= 0.0 min

Primary = 0.12 cfs @ 12.09 hrs, Volume= 0.010 af

Routed to Pond CB102: Catch Basin 102

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 66.88' @ 12.10 hrs

Flood Elev= 70.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	66.60'	12.0" Round Culvert
			L= 14.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 66.60' / 66.50' S= 0.0071 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.10 cfs @ 12.09 hrs HW=66.87' TW=66.84' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.10 cfs @ 0.84 fps)

Summary for Pond CB102: Catch Basin 102

Inflow Area = 0.047 ac,100.00% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr +15% event

Inflow = 0.25 cfs @ 12.09 hrs, Volume= 0.021 af

Outflow = 0.25 cfs @ 12.09 hrs, Volume= 0.021 af, Atten= 0%, Lag= 0.0 min

Primary = 0.25 cfs @ 12.09 hrs, Volume= 0.021 af

Routed to Pond yd1: Yard Drain 1

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.85' @ 12.09 hrs

Flood Elev= 70.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	66.40'	12.0" Round Culvert
			L= 15.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 66.40' / 66.30' S= 0.0067 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.22 cfs @ 12.09 hrs HW=66.84' TW=66.80' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.22 cfs @ 0.97 fps)

Summary for Pond CB103: Catch Basin 103

Inflow Area = 0.307 ac, 64.59% Impervious, Inflow Depth > 4.43" for 10 Yr 24 Hr +15% event

Inflow = 1.45 cfs @ 12.09 hrs, Volume= 0.113 af

Outflow = 1.45 cfs @ 12.09 hrs, Volume= 0.113 af, Atten= 0%, Lag= 0.0 min

Primary = 1.45 cfs @ 12.09 hrs, Volume= 0.113 af

Routed to Pond CB104: Catch Basin 104

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 66.59' @ 12.09 hrs

Flood Elev= 72.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	65.80'	12.0" Round Culvert
			L= 43.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 65.80' / 65.50' S= 0.0070 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=1.42 cfs @ 12.09 hrs HW=66.58' TW=66.17' (Dynamic Tailwater) 1=Culvert (Outlet Controls 1.42 cfs @ 2.99 fps)

Summary for Pond CB104: Catch Basin 104

Inflow Area = 0.314 ac, 65.44% Impervious, Inflow Depth > 4.45" for 10 Yr 24 Hr +15% event

Inflow = 1.49 cfs @ 12.09 hrs, Volume= 0.116 af

Outflow = 1.49 cfs @ 12.09 hrs, Volume= 0.116 af, Atten= 0%, Lag= 0.0 min

Primary = 1.49 cfs @ 12.09 hrs, Volume= 0.116 af

Routed to Pond 1P: Bioretention Pond

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 66.18' @ 12.09 hrs

Flood Elev= 71.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	65.40'	12.0" Round Culvert L= 31.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 65.40' / 65.20' S= 0.0065 '/' Cc= 0.900

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n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=1.46 cfs @ 12.09 hrs HW=66.17' TW=60.89' (Dynamic Tailwater) 1=Culvert (Barrel Controls 1.46 cfs @ 3.10 fps)

Summary for Pond YD1: Yard Drain 1

Inflow Area = 0.152 ac, 65.02% Impervious, Inflow Depth > 4.45" for 10 Yr 24 Hr +15% event

Inflow = 0.73 cfs @ 12.09 hrs, Volume= 0.056 af

Outflow = 0.73 cfs @ 12.09 hrs, Volume= 0.056 af, Atten= 0%, Lag= 0.0 min

Primary = 0.73 cfs @ 12.09 hrs, Volume= 0.056 af

Routed to Pond CB103: Catch Basin 103

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 66.81' @ 12.09 hrs

Flood Elev= 69.30'

Device	Routing	Invert	Outlet Devices
#1	Primary	66.20'	12.0" Round Culvert
			L= 52.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 66.20' / 65.90' S= 0.0058 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.71 cfs @ 12.09 hrs HW=66.80' TW=66.58' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.71 cfs @ 2.06 fps)

Summary for Pond YD2: Yard Drain 2

Inflow Area = 0.086 ac, 35.30% Impervious, Inflow Depth > 3.63" for 10 Yr 24 Hr +15% event

Inflow = 0.35 cfs @ 12.09 hrs, Volume= 0.026 af

Outflow = 0.35 cfs @ 12.09 hrs, Volume= 0.026 af, Atten= 0%, Lag= 0.0 min

Primary = 0.35 cfs @ 12.09 hrs, Volume= 0.026 af

Routed to Pond CB103: Catch Basin 103

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 67.39' @ 12.09 hrs

Flood Elev= 70.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	67.00'	8.0" Round Culvert
			L= 13.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 67.00' / 66.13' S= 0.0669 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.35 cfs @ 12.09 hrs HW=67.38' TW=66.58' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.35 cfs @ 1.67 fps)

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S Runoff Area=16,321 sf 51.36% Impervious Runoff Depth>5.48" Flow Length=186' Tc=6.0 min CN=86 Runoff=2.27 cfs 0.171 af Subcatchment2S: Subcatchment2S Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>4.14" Flow Length=20' Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.19 cfs 0.014 af Runoff Area=44,464 sf 0.00% Impervious Runoff Depth>4.03" Subcatchment3S: Subcatchment3S Flow Length=447' Tc=11.9 min CN=73 Runoff=3.96 cfs 0.343 af Subcatchment4S: Subcatchment4S Runoff Area=20,991 sf 8.04% Impervious Runoff Depth>4.36" Flow Length=210' Tc=6.2 min CN=76 Runoff=2.40 cfs 0.175 af Subcatchment6S: Subcatchment6S Runoff Area=1,084 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.17 cfs 0.014 af Subcatchment7S: Subcatchment7S Runoff Area=954 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.013 af Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>6.88" Subcatchment8S: Subcatchment8S Tc=6.0 min CN=98 Runoff=0.47 cfs 0.040 af Subcatchment9S: Subcatchment9S Runoff Area=325 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af Subcatchment11S: Subcatchment11S Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>5.48" Slope=0.0396 '/' Tc=6.0 min CN=86 Runoff=0.64 cfs 0.048 af Flow Length=77' Subcatchment12S: Subcatchment12S Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>5.02" Flow Length=50' Slope=0.0320 '/' Tc=6.0 min CN=82 Runoff=0.49 cfs 0.036 af Runoff Area=560 sf 100.00% Impervious Runoff Depth>6.88" Subcatchment13S: Subcatchment14S Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af Subcatchment14S: Subcatchment14S Runoff Area=560 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af Subcatchment15S: Subcatchment15S Runoff Area=779 sf 75.74% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.12 cfs 0.010 af Subcatchment16S: Subcatchment15S Runoff Area=779 sf 75.74% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.12 cfs 0.010 af Runoff Area=9,821 sf 17.16% Impervious Runoff Depth>4.58" Subcatchment18S: Subcatchment18S Flow Length=58' Tc=6.0 min CN=78 Runoff=1.18 cfs 0.086 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.10' Max Vel=0.31 fps Inflow=0.19 cfs 0.014 af n=0.150 L=52.0' S=0.0385 '/' Capacity=6.22 cfs Outflow=0.18 cfs 0.014 af

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Reach 3R: Flow over Sagamore AveAvg. Flow Depth=0.18' Max Vel=3.14 fps Inflow=2.44 cfs 0.185 af n=0.016 L=101.0' S=0.0297 '/' Capacity=39.77 cfs Outflow=2.45 cfs 0.185 af

Reach 6R: Flow through 3SAvg. Flow Depth=0.02' Max Vel=1.81 fps Inflow=0.20 cfs 0.008 af n=0.030 L=81.0' S=0.3457 '/' Capacity=740.30 cfs Outflow=0.20 cfs 0.008 af

Reach 7R: Flow Through 3SAvg. Flow Depth=0.13' Max Vel=3.53 fps Inflow=1.55 cfs 0.137 af n=0.030 L=220.0' S=0.0909 '/' Capacity=66.79 cfs Outflow=1.55 cfs 0.137 af

Reach 8R: Ditch on Tidewatch Property Avg. Flow Depth=0.34' Max Vel=2.47 fps Inflow=1.71 cfs 0.145 af n=0.030 L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=1.71 cfs 0.145 af

Reach AP1: Analysis Point 1 (New CB)

Inflow=2.45 cfs 0.185 af
Outflow=2.45 cfs 0.185 af

Reach AP2: Analysis Point 2 Inflow=0.19 cfs 0.014 af
Outflow=0.19 cfs 0.014 af

Reach AP3: Analysis Point 3 Inflow=5.50 cfs 0.488 af
Outflow=5.50 cfs 0.488 af

Reach AP4: Analysis Point 4 Inflow=2.40 cfs 0.175 af
Outflow=2.40 cfs 0.175 af

Pond 1P: Bioretention Pond

Peak Elev=61.27' Storage=524 cf Inflow=3.14 cfs 0.241 af

Discarded=0.59 cfs 0.104 af Primary=1.55 cfs 0.137 af Outflow=2.14 cfs 0.240 af

Pond 1PF: Sediment Forebay Peak Elev=0.00' Storage=0 cf

Pond 3P: Stone Under Deck
Peak Elev=66.20' Storage=0.008 af Inflow=0.21 cfs 0.018 af
Discarded=0.01 cfs 0.007 af Secondary=0.11 cfs 0.004 af Outflow=0.12 cfs 0.010 af

Pond 4P: Stone Under Deck
Peak Elev=67.20' Storage=0.008 af Inflow=0.26 cfs 0.015 af
Discarded=0.01 cfs 0.007 af Secondary=0.11 cfs 0.001 af Outflow=0.12 cfs 0.009 af

Pond 5P: Lined Stone Drip Edge Peak Elev=66.21' Storage=0.000 af Inflow=0.12 cfs 0.010 af Primary=0.12 cfs 0.010 af Secondary=0.00 cfs 0.000 af Outflow=0.12 cfs 0.010 af

Pond 6P: Lined Stone Drip Edge Peak Elev=67.01' Storage=0.001 af Inflow=0.12 cfs 0.010 af Primary=0.19 cfs 0.008 af Secondary=0.08 cfs 0.003 af Outflow=0.08 cfs 0.010 af

Pond CB101: Catch Basin 101 Peak Elev=67.00' Inflow=0.15 cfs 0.013 af 12.0" Round Culvert n=0.012 L=14.0' S=0.0071 '/' Outflow=0.15 cfs 0.013 af

Pond CB102: Catch Basin 102 Peak Elev=66.99' Inflow=0.32 cfs 0.027 af 12.0" Round Culvert n=0.012 L=15.0' S=0.0067 '/' Outflow=0.32 cfs 0.027 af

Pond CB103: Catch Basin 103 Peak Elev=66.77' Inflow=1.91 cfs 0.150 af

12.0" Round Culvert n=0.012 L=43.0' S=0.0070 '/' Outflow=1.91 cfs 0.150 af

Type III 24-hr 25 Yr 24 Hr +15% Rainfall=7.12"

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Pond CB104: Catch Basin 104 Peak Elev=66.34' Inflow=1.96 cfs 0.154 af

12.0" Round Culvert n=0.012 L=31.0' S=0.0065 '/' Outflow=1.96 cfs 0.154 af

Pond YD1: Yard Drain 1 Peak Elev=66.97' Inflow=0.96 cfs 0.075 af

12.0" Round Culvert n=0.012 L=52.0' S=0.0058 '/' Outflow=0.96 cfs 0.075 af

Pond YD2: Yard Drain 2 Peak Elev=67.47' Inflow=0.49 cfs 0.036 af

8.0" Round Culvert n=0.012 L=13.0' S=0.0669 '/' Outflow=0.49 cfs 0.036 af

Total Runoff Area = 2.518 ac Runoff Volume = 0.978 af Average Runoff Depth = 4.66" 79.02% Pervious = 1.990 ac 20.98% Impervious = 0.528 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=16,321 sf 51.36% Impervious Runoff Depth>6.84" Flow Length=186' Tc=6.0 min CN=86 Runoff=2.81 cfs 0.214 af
Subcatchment2S: Subcatchment2S Flow Length=20'	Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>5.40" Slope=0.1000 '/' Tc=6.0 min CN=74 Runoff=0.24 cfs 0.018 af
Subcatchment3S: Subcatchment3S	Runoff Area=44,464 sf 0.00% Impervious Runoff Depth>5.27" low Length=447' Tc=11.9 min CN=73 Runoff=5.17 cfs 0.448 af
Subcatchment4S: Subcatchment4S	Runoff Area=20,991 sf 8.04% Impervious Runoff Depth>5.64" Flow Length=210' Tc=6.2 min CN=76 Runoff=3.08 cfs 0.226 af
Subcatchment6S: Subcatchment6S	Runoff Area=1,084 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.20 cfs 0.017 af
Subcatchment7S: Subcatchment7S	Runoff Area=954 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.18 cfs 0.015 af
Subcatchment8S: Subcatchment8S	Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.57 cfs 0.048 af
Subcatchment9S: Subcatchment9S	Runoff Area=325 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment11S: Subcatchment11S Flow Length=77'	Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>6.84" Slope=0.0396 '/' Tc=6.0 min CN=86 Runoff=0.79 cfs 0.060 af
Subcatchment12S: Subcatchment12S Flow Length=50'	Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>6.36" Slope=0.0320 '/' Tc=6.0 min CN=82 Runoff=0.61 cfs 0.045 af
Subcatchment13S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.11 cfs 0.009 af
Subcatchment14S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.11 cfs 0.009 af
Subcatchment15S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af
Subcatchment16S: Subcatchment15S	Runoff Area=779 sf 75.74% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af
Subcatchment18S: Subcatchment18S	Runoff Area=9,821 sf 17.16% Impervious Runoff Depth>5.88" Flow Length=58' Tc=6.0 min CN=78 Runoff=1.50 cfs 0.110 af

Reach 2R: Flow across Map 222 Lot 20 Avg. Flow Depth=0.11' Max Vel=0.34 fps Inflow=0.24 cfs 0.018 af

n=0.150 L=52.0' S=0.0385 '/' Capacity=6.22 cfs Outflow=0.23 cfs 0.018 af

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Reach 3R: Flow over Sagamore AveAvg. Flow Depth=0.19' Max Vel=3.31 fps Inflow=3.03 cfs 0.231 af n=0.016 L=101.0' S=0.0297'/' Capacity=39.77 cfs Outflow=3.03 cfs 0.231 af

Reach 6R: Flow through 3SAvg. Flow Depth=0.03' Max Vel=2.25 fps Inflow=0.51 cfs 0.014 af n=0.030 L=81.0' S=0.3457 '/' Capacity=740.30 cfs Outflow=0.46 cfs 0.014 af

Reach 7R: Flow Through 3SAvg. Flow Depth=0.13' Max Vel=3.60 fps Inflow=1.64 cfs 0.178 af n=0.030 L=220.0' S=0.0909 '/' Capacity=66.79 cfs Outflow=1.64 cfs 0.178 af

Reach 8R: Ditch on Tidewatch Property Avg. Flow Depth=0.37' Max Vel=2.60 fps Inflow=2.08 cfs 0.192 af n=0.030 L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=2.07 cfs 0.192 af

Reach AP1: Analysis Point 1 (New CB)

Inflow=3.03 cfs 0.231 af
Outflow=3.03 cfs 0.231 af

Reach AP2: Analysis Point 2 Inflow=0.24 cfs 0.018 af
Outflow=0.24 cfs 0.018 af

Reach AP3: Analysis Point 3 Inflow=7.16 cfs 0.641 af
Outflow=7.16 cfs 0.641 af

Reach AP4: Analysis Point 4 Inflow=3.08 cfs 0.226 af Outflow=3.08 cfs 0.226 af

Pond 1P: Bioretention Pond

Peak Elev=61.60' Storage=924 cf Inflow=3.91 cfs 0.301 af

Discarded=0.68 cfs 0.122 af Primary=1.64 cfs 0.178 af Outflow=2.31 cfs 0.301 af

Pond 1PF: Sediment Forebay Peak Elev=0.00' Storage=0 cf

Pond 3P: Stone Under Deck
Peak Elev=66.20' Storage=0.008 af Inflow=0.23 cfs 0.021 af
Discarded=0.01 cfs 0.007 af Secondary=0.19 cfs 0.006 af Outflow=0.20 cfs 0.014 af

Pond 4P: Stone Under Deck
Peak Elev=67.20' Storage=0.008 af Inflow=0.34 cfs 0.017 af
Discarded=0.01 cfs 0.008 af Secondary=0.19 cfs 0.002 af Outflow=0.19 cfs 0.010 af

Pond 5P: Lined Stone Drip Edge Peak Elev=66.22' Storage=0.000 af Inflow=0.15 cfs 0.012 af Primary=0.13 cfs 0.012 af Secondary=0.00 cfs 0.000 af Outflow=0.13 cfs 0.012 af

Pond 6P: Lined Stone Drip Edge Peak Elev=67.01' Storage=0.001 af Inflow=0.15 cfs 0.012 af Primary=0.24 cfs 0.008 af Secondary=0.15 cfs 0.005 af Outflow=0.15 cfs 0.012 af

Pond CB101: Catch Basin 101 Peak Elev=67.27' Inflow=0.18 cfs 0.015 af 12.0" Round Culvert n=0.012 L=14.0' S=0.0071 '/' Outflow=0.18 cfs 0.015 af

Pond CB102: Catch Basin 102 Peak Elev=67.23' Inflow=0.38 cfs 0.032 af 12.0" Round Culvert n=0.012 L=15.0' S=0.0067 '/' Outflow=0.38 cfs 0.032 af

Pond CB103: Catch Basin 103 Peak Elev=67.15' Inflow=2.34 cfs 0.185 af

12.0" Round Culvert n=0.012 L=43.0' S=0.0070 '/' Outflow=2.34 cfs 0.185 af

Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

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Pond CB104: Catch Basin 104 Peak Elev=66.54' Inflow=2.40 cfs 0.190 af

12.0" Round Culvert n=0.012 L=31.0' S=0.0065 '/' Outflow=2.40 cfs 0.190 af

Pond YD1: Yard Drain 1 Peak Elev=67.30' Inflow=1.17 cfs 0.092 af

12.0" Round Culvert n=0.012 L=52.0' S=0.0058 '/' Outflow=1.17 cfs 0.092 af

Pond YD2: Yard Drain 2 Peak Elev=67.55' Inflow=0.61 cfs 0.045 af

8.0" Round Culvert n=0.012 L=13.0' S=0.0669 '/' Outflow=0.61 cfs 0.045 af

Total Runoff Area = 2.518 ac Runoff Volume = 1.250 af Average Runoff Depth = 5.96" 79.02% Pervious = 1.990 ac 20.98% Impervious = 0.528 ac Prepared by Jones & Beach Engineers Inc

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 2.81 cfs @ 12.09 hrs, Volume=

0.214 af, Depth> 6.84"

Routed to Reach 3R: Flow over Sagamore Ave

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Д	rea (sf)	CN I	Description		
		6,930	98 I	Paved park	ing, HSG C	
		7,938	74	>75% Gras	s cover, Go	ood, HSG C
		1,453	98	Roofs, HSC	G C	
		16,321	86 \	Weighted A	verage	
		7,938	4	48.64% Pe	rvious Area	
		8,383	!	51.36% Imp	pervious Ar	ea
	Tc	Length	Slope		Capacity	Description
((min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.5	50	0.1250	0.33		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.0	6	0.1250	2.47		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.3	30	0.0670	1.81		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.4	100	0.0360	3.85		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
	3.2	186	Total,	Increased t	to minimum	Tc = 6.0 min

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.24 cfs @ 12.09 hrs, Volume=

0.018 af, Depth> 5.40"

Routed to Reach AP2 : Analysis Point 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Aı	rea (sf)	CN	Description									
		1,728	74	74 >75% Grass cover, Good, HSG C									
		1,728		100.00% Pervious Area									
	Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	Description							
	1.3	20	0.1000	0.25		Sheet Flow,					_		
_						Grass: Short	n= 0.150	P2= 3.70"					
	4.0	00	T . 4 . 1	The same and a second of		T							

1.3 20 Total, Increased to minimum Tc = 6.0 min

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Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 5.17 cfs @ 12.16 hrs, Volume= 0.448 af, Depth> 5.27"

Routed to Reach AP3: Analysis Point 3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Α	rea (sf)	CN D	escription		
		16,641			•	ood, HSG C
		27,823	<u>73 V</u>	<u>Voods, Fai</u>	r, HSG C	
		44,464	73 V	Veighted A	verage	
		44,464	1	00.00% Pe	ervious Are	a
	Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	8.6	50	0.0415	0.10		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	0.7	62	0.0968	1.56		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.7	54	0.0741	1.36		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	1.3	122	0.1000	1.58		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.6	159	0.0189	4.55	18.20	Trap/Vee/Rect Channel Flow,
	0.0	.00	0.0.00		.0.20	Bot.W=1.00' D=1.00' Z= 3.0 '/' Top.W=7.00'
						n= 0.030 Short grass
	11.9	447	Total			0.000 0 9.2.00
		771	rotai			

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 3.08 cfs @ 12.09 hrs, Volume= 0.226 af, Depth> 5.64"

Routed to Reach AP4: Analysis Point 4

 Area (sf)	CN	Description			
11,135	74	>75% Grass cover, Good, HSG C			
8,169	73	Woods, Fair, HSG C			
 1,687	98	Roofs, HSG C			
20,991	76	Weighted Average			
19,304		91.96% Pervious Area			
1,687		8.04% Impervious Area			

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	_					
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.5	14	0.0357	0.16		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	1.9	14	0.1429	0.12		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	1.3	22	0.1333	0.29		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.3	50	0.1333	2.56		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	1.0	80	0.0750	1.37		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.2	30	0.2667	2.58		Shallow Concentrated Flow,
_						Woodland Kv= 5.0 fps
	6.2	210	Total			

Summary for Subcatchment 6S: Subcatchment 6S

Runoff = 0.20 cfs @ 12.09 hrs, Volume= 0

0.017 af, Depth> 8.28"

Routed to Pond CB102 : Catch Basin 102

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

_	Α	rea (sf)	CN I	Description								
		1,084	98 I	98 Paved parking, HSG C								
		1,084		100.00% Impervious Area								
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description						
_	6.0	,			, ,	Direct Entry.						

Summary for Subcatchment 7S: Subcatchment 7S

Runoff = 0.18 cfs @ 12.09 hrs, Volume= 0.015 af, Depth> 8.28"

Routed to Pond CB101: Catch Basin 101

A	rea (sf)	CN [CN Description								
	954	98 F	98 Paved parking, HSG C								
	954	1	100.00% Impervious Area								
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description						
6.0					Direct Entry,						

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Summary for Subcatchment 8S: Subcatchment 8S

Runoff = 0.57 cfs @ 12.09 hrs, Volume=

0.048 af, Depth> 8.28"

Routed to Pond CB103: Catch Basin 103

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description								
	2,554	98	Paved park	ing, HSG C							
	457	98	Roofs, HSC	Roofs, HSG C							
	3,011	98	Weighted A	verage							
	3,011		100.00% Impervious Area								
Тс	Length	Slop	e Velocity	Capacity	Description						
(min)	(feet)	(ft/fi	(ft/sec)	(cfs)							
6.0					Direct Entry,						

Summary for Subcatchment 9S: Subcatchment 9S

Runoff = 0.06 cfs @ 12.09 hrs, Volume=

0.005 af, Depth> 8.28"

Routed to Pond CB104: Catch Basin 104

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN [Description							
	325	98 F	Paved parking, HSG C							
	325	1	100.00% Impervious Area							
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
6.0		·			Direct Entry,					

Summary for Subcatchment 11S: Subcatchment 11S

Runoff = 0.79 cfs @ 12.09 hrs, Volume= 0.060 af, Depth> 6.84"

Routed to Pond YD1: Yard Drain 1

Area (sf)	CN	Description				
1,998	98	Roofs, HSG C				
2,312	74	>75% Grass cover, Good, HSG C				
261	98	Paved parking, HSG C				
4,571	86	Weighted Average				
2,312		50.58% Pervious Area				
2,259		49.42% Impervious Area				

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	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	4.0	50	0.0396	0.21		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.3	27	0.0396	1.39		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	4.0					T 00 :

4.3 77 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 12S: Subcatchment 12S

Runoff 0.61 cfs @ 12.09 hrs, Volume= 0.045 af, Depth> 6.36"

Routed to Pond YD2: Yard Drain 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

Α	rea (sf)	CN	Description					
•	1,318	98	Roofs, HSG	G C				
	2,416	74	>75% Gras	s cover, Go	ood, HSG C			
	3,734	82	Weighted A	verage				
	2,416		64.70% Per	vious Area				
	1,318		35.30% Imp	pervious Ar	ea			
Тс	Length	Slope	,	Capacity	Description			
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)				
4.3	50	0.0320	0.19		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.70"	
4.3	50	Total,	Increased t	o minimum	Tc = 6.0 min			

Summary for Subcatchment 13S: Subcatchment 14S

0.11 cfs @ 12.09 hrs, Volume= 0.009 af, Depth> 8.28"

Routed to Pond 3P: Stone Under Deck

A	rea (sf)	CN [Description		
	560	98 F	Roofs, HSC	G C	
	560	1	00.00% In	npervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

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Summary for Subcatchment 14S: Subcatchment 14S

Runoff = 0.11 cfs @ 12.09 hrs, Volume=

0.009 af, Depth> 8.28"

Routed to Pond 4P: Stone Under Deck

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Area (s	f)	CN	Description		
	56	60	98	Roofs, HSG	G C	
	56	0		100.00% In	npervious A	Area
T (mir	c Lenç	_	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.	0					Direct Entry,

Summary for Subcatchment 15S: Subcatchment 15S

Runoff = 0.15 cfs @ 12.09 hrs, Volume=

0.012 af, Depth> 8.28"

Routed to Pond 5P: Lined Stone Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description					
	590	98	Roofs, HSC	G C				
	189	98	Water Surfa	ace, 0% imp	ip, HSG C			
	779	98	8 Weighted Average					
	189		24.26% Pervious Area					
	590		75.74% lmp	pervious Ar	rea			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	,	(cfs)	2000p			
6.0					Direct Entry,			

Summary for Subcatchment 16S: Subcatchment 15S

Runoff = 0.15 cfs @ 12.09 hrs, Volume=

0.012 af, Depth> 8.28"

Routed to Pond 6P: Lined Stone Drip Edge

 Area (sf)	CN	Description
590	98	Roofs, HSG C
 189	98	Water Surface, 0% imp, HSG C
 779	98	Weighted Average
189		24.26% Pervious Area
590		75.74% Impervious Area

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6.0	(1001)	(10,10)	(14000)	(0.0)	Direct Entry	-
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
Tc	Length	Slope	Velocity	Capacity	Description	

Direct Entry,

Summary for Subcatchment 18S: Subcatchment 18S

1.50 cfs @ 12.09 hrs, Volume= Runoff

0.110 af, Depth> 5.88"

Routed to Pond 1P: Bioretention Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

_	Α	rea (sf)	CN	Description		
		8,136	74	>75% Gras	s cover, Go	ood, HSG C
		1,285	98	Roofs, HSC	G C	
		400	98	Paved park	ing, HSG C	
		9,821	78	Weighted A	verage	
		8,136		82.84% Pei	rvious Area	
		1,685		17.16% lmp	pervious Ar	ea
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	2.5	43	0.0930	0.29		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.4	7	0.3333	0.33		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.0	8	0.3333	4.04		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	2.0	58	Total	Increased t	o minimum	Tc = 6.0 min

Total, Increased to minimum Tc = 6.0 min 2.9

Summary for Reach 2R: Flow across Map 222 Lot 20

Inflow Area = 0.040 ac, 0.00% Impervious, Inflow Depth > 5.40" for 50 Yr 24 Hr +15% event

Inflow 0.24 cfs @ 12.09 hrs, Volume= 0.018 af

0.23 cfs @ 12.12 hrs, Volume= 0.018 af, Atten= 6%, Lag= 1.7 min Outflow

Routed to Reach 3R: Flow over Sagamore Ave

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.34 fps, Min. Travel Time= 2.6 min

Avg. Velocity = 0.12 fps, Avg. Travel Time= 7.5 min

Peak Storage= 35 cf @ 12.12 hrs

Average Depth at Peak Storage= 0.11', Surface Width= 9.36' Bank-Full Depth= 0.50' Flow Area= 6.7 sf, Capacity= 6.22 cfs

20.00' x 0.50' deep Parabolic Channel, n= 0.150 Sheet flow over Short Grass

Length= 52.0' Slope= 0.0385 '/'

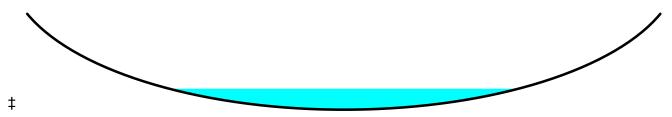
Inlet Invert= 66.00', Outlet Invert= 64.00'

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Summary for Reach 3R: Flow over Sagamore Ave

[90] Warning: Qout>Qin may require smaller dt or Finer Routing [62] Hint: Exceeded Reach 2R OUTLET depth by 0.08' @ 12.05 hrs

Inflow Area = 0.414 ac, 46.45% Impervious, Inflow Depth > 6.70" for 50 Yr 24 Hr +15% event

Inflow = 3.03 cfs @ 12.09 hrs, Volume= 0.231 af

Outflow = 3.03 cfs @ 12.10 hrs, Volume= 0.231 af, Atten= 0%, Lag= 0.4 min

Routed to Reach AP1 : Analysis Point 1 (New CB)

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.31 fps, Min. Travel Time= 0.5 min Avg. Velocity = 1.29 fps, Avg. Travel Time= 1.3 min

Peak Storage= 93 cf @ 12.10 hrs

Average Depth at Peak Storage= 0.19', Surface Width= 9.62' Bank-Full Depth= 0.50' Flow Area= 6.3 sf, Capacity= 39.77 cfs

0.00' x 0.50' deep channel, n= 0.016 Asphalt, rough Side Slope Z-value= 50.0 0.5 '/' Top Width= 25.25' Length= 101.0' Slope= 0.0297 '/' Inlet Invert= 64.00', Outlet Invert= 61.00'

‡

Summary for Reach 6R: Flow through 3S

Inflow = 0.51 cfs @ 12.16 hrs, Volume= 0.014 af

Outflow = 0.46 cfs @ 12.17 hrs, Volume= 0.014 af, Atten= 11%, Lag= 0.7 min

Routed to Reach 8R: Ditch on Tidewatch Property

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 2.25 fps, Min. Travel Time= 0.6 min

Avg. Velocity = 1.11 fps, Avg. Travel Time= 1.2 min

Peak Storage= 16 cf @ 12.17 hrs

Average Depth at Peak Storage= 0.03', Surface Width= 9.16'

Bank-Full Depth= 1.00' Flow Area= 33.3 sf, Capacity= 740.30 cfs

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50.00' x 1.00' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 81.0' Slope= 0.3457 '/' Inlet Invert= 66.00', Outlet Invert= 38.00'



Summary for Reach 7R: Flow Through 3S

Inflow Area = 0.539 ac, 45.26% Impervious, Inflow Depth = 3.97" for 50 Yr 24 Hr +15% event

Inflow = 1.64 cfs @ 12.21 hrs, Volume= 0.178 af

Outflow = 1.64 cfs @ 12.22 hrs, Volume= 0.178 af, Atten= 0%, Lag= 0.6 min

Routed to Reach 8R: Ditch on Tidewatch Property

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 3.60 fps, Min. Travel Time= 1.0 min Avg. Velocity = 1.21 fps, Avg. Travel Time= 3.0 min

Peak Storage= 100 cf @ 12.22 hrs

Average Depth at Peak Storage= 0.13', Surface Width= 3.80' Bank-Full Depth= 1.00' Flow Area= 6.0 sf, Capacity= 66.79 cfs

3.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 3.0 '/' Top Width= 9.00'

Length= 220.0' Slope= 0.0909 '/'

Inlet Invert= 58.00', Outlet Invert= 38.00'



Summary for Reach 8R: Ditch on Tidewatch Property

[62] Hint: Exceeded Reach 6R OUTLET depth by 0.34' @ 12.20 hrs [62] Hint: Exceeded Reach 7R OUTLET depth by 0.24' @ 12.20 hrs

Inflow Area = 0.539 ac, 45.26% Impervious, Inflow Depth = 4.28" for 50 Yr 24 Hr +15% event

Inflow = 2.08 cfs @ 12.17 hrs, Volume= 0.192 af

Outflow = 2.07 cfs @ 12.20 hrs, Volume= 0.192 af, Atten= 1%, Lag= 1.6 min

Routed to Reach AP3: Analysis Point 3

Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

18134-PROPOSED

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 2.60 fps, Min. Travel Time= 1.0 min Avg. Velocity = 0.92 fps, Avg. Travel Time= 2.9 min

Peak Storage= 126 cf @ 12.20 hrs

Average Depth at Peak Storage= 0.37', Surface Width= 3.25' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.18 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 3.0 '/' Top Width= 7.00'

Length= 159.0' Slope= 0.0189 '/'

Inlet Invert= 38.00', Outlet Invert= 35.00'



Summary for Reach AP1: Analysis Point 1 (New CB)

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.414 ac, 46.45% Impervious, Inflow Depth > 6.70" for 50 Yr 24 Hr +15% event

Inflow = 3.03 cfs @ 12.10 hrs, Volume= 0.231 af

Outflow = 3.03 cfs @ 12.10 hrs, Volume= 0.231 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.040 ac, 0.00% Impervious, Inflow Depth > 5.40" for 50 Yr 24 Hr +15% event

Inflow = 0.24 cfs @ 12.09 hrs, Volume= 0.018 af

Outflow = 0.24 cfs @ 12.09 hrs, Volume= 0.018 af, Atten= 0%, Lag= 0.0 min

Routed to Reach 2R: Flow across Map 222 Lot 20

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.560 ac, 15.65% Impervious, Inflow Depth > 4.93" for 50 Yr 24 Hr +15% event

Inflow = 7.16 cfs @ 12.17 hrs, Volume = 0.641 af

Outflow = 7.16 cfs @ 12.17 hrs, Volume= 0.641 af, Atten= 0%, Lag= 0.0 min

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.482 ac, 8.04% Impervious, Inflow Depth > 5.64" for 50 Yr 24 Hr +15% event

3.08 cfs @ 12.09 hrs, Volume= Inflow 0.226 af

Outflow 3.08 cfs @ 12.09 hrs, Volume= 0.226 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Bioretention Pond

Existing high contour within footprint of filter course = 61.0, SHWT depth = 35" per TP 10, so SHWT EI. = 58.08, which is 0.01' below the bottom of stone. However, in our experience, modelling the SHWTwith such a small separation to the bottom of stone causes an unrealistically high amount of infiltration to appear in the calculations. Therefore, the SHWT has been modelled 2" lower as a factor of safety.

Inflow Area = 0.539 ac. 45.26% Impervious, Inflow Depth > 6.69" for 50 Yr 24 Hr +15% event

Inflow 3.91 cfs @ 12.09 hrs, Volume= 0.301 af

2.31 cfs @ 12.21 hrs, Volume= 0.301 af, Atten= 41%, Lag= 7.1 min Outflow

Discarded = 0.68 cfs @ 12.21 hrs, Volume= 0.122 af 1.64 cfs @ 12.21 hrs, Volume= Primary 0.178 af

Routed to Reach 7R: Flow Through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 61.60' @ 12.21 hrs Surf.Area= 1,294 sf Storage= 924 cf

Plug-Flow detention time= 2.8 min calculated for 0.300 af (100% of inflow)

Center-of-Mass det. time= 2.4 min (783.5 - 781.0)

Volume	Invert Ava	il.Storage	Storage	Description		
#1	58.09'	2,677 cf	Custon	n Stage Data (Irreg	gular)Listed below	(Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
58.09	117	48.0	0.0	0	0	117
58.10	117	48.0	40.0	0	0	117
59.09	117	48.0	40.0	46	47	165
59.10	117	48.0	15.0	0	47	165
60.59	117	48.0	15.0	26	73	237
60.60	117	48.0	100.0	1	74	237
60.99	702	116.0	100.0	144	218	1,126
61.00	1,026	144.0	100.0	9	227	1,705
62.00	1,487	163.0	100.0	1,249	1,476	2,194
62.70	1,898	178.0	100.0	1,182	2,658	2,618
62.71	1,898	178.0	100.0	19	2,677	2,620

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Device	Routing	Invert	Outlet Devices
#1	Primary	58.35'	12.0" Round Culvert
	·		L= 20.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 58.35' / 58.00' S= 0.0175 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf
#2	Device 1	58.35'	6.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	61.70'	18.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Discarded	58.09'	7.400 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 57.92' Phase-In= 0.10'

Discarded OutFlow Max=0.68 cfs @ 12.21 hrs HW=61.60' (Free Discharge) **4=Exfiltration** (Controls 0.68 cfs)

Primary OutFlow Max=1.64 cfs @ 12.21 hrs HW=61.60' TW=58.13' (Dynamic Tailwater)

1=Culvert (Passes 1.64 cfs of 4.95 cfs potential flow)

2=Orifice/Grate (Orifice Controls 1.64 cfs @ 8.34 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 1PF: Sediment Forebay

[43] Hint: Has no inflow (Outflow=Zero)

olume	Invert	Avail.S	torage	Storage	Description	
#1	59.00'		231 cf	Custon	n Stage Data (Pi	rismatic)Listed below (Recalc)
Elevation (feet)					Cum.Store (cubic-feet)	
59.00 60.00 61.00		15 101 245		0 58 173	0 58 231	
	#1 Elevation (feet) 59.00 60.00	#1 59.00' Elevation Surf. (feet) (59.00 60.00	#1 59.00' Elevation Surf.Area (feet) (sq-ft) 59.00 15 60.00 101	#1 59.00' 231 cf Elevation Surf.Area Inc (feet) (sq-ft) (cubic 59.00 15 60.00 101	#1 59.00' 231 cf Custon Elevation Surf.Area Inc.Store (feet) (sq-ft) (cubic-feet) 59.00 15 0 60.00 101 58	#1 59.00' 231 cf Custom Stage Data (Picevation (feet) (sq-ft) (cubic-feet) (cubic-feet) (59.00 15 0 0 60.00 101 58 58

Summary for Pond 3P: Stone Under Deck

Ledge surface modelled 24" below original grade based on TP 13 (Bedrock found from 24" to 36". Proposed grade is approximately 3.2' above existing grade and therefore 5.2' above ledge.

Inflow Area = 0.031 ac, 85.88% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr +15% event
Inflow = 0.23 cfs @ 12.07 hrs, Volume= 0.021 af
Outflow = 0.20 cfs @ 12.17 hrs, Volume= 0.014 af, Atten= 15%, Lag= 6.3 min
Discarded = 0.19 cfs @ 12.15 hrs, Volume= 0.007 af
Secondary = 0.19 cfs @ 12.17 hrs, Volume= 0.006 af
Routed to Reach 6R : Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.20' @ 12.15 hrs Surf.Area= 0.006 ac Storage= 0.008 af

Plug-Flow detention time= 212.7 min calculated for 0.014 af (64% of inflow) Center-of-Mass det. time= 102.0 min (847.7 - 745.8)

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Volume	Invert	Avail.Storage	Storage Description
#1	62.90'	0.008 af	14.00'W x 20.00'L x 3.30'H Prismatoid 0.021 af Overall x 40.0% Voids
Device	Routing	Invert Ou	utlet Devices
#0	Secondary	66.20' A ı	utomatic Storage Overflow (Discharged without head)
#1	Discarded	62.90' 0. 3	300 in/hr Exfiltration over Surface area
		Co	onductivity to Groundwater Elevation = 61.00' Phase-In= 0.10'

Discarded OutFlow Max=0.01 cfs @ 12.15 hrs HW=66.20' (Free Discharge) 1=Exfiltration (Controls 0.01 cfs)

Secondary OutFlow Max=0.00 cfs @ 12.17 hrs HW=66.20' TW=66.03' (Dynamic Tailwater)

Summary for Pond 4P: Stone Under Deck

Ledge surface modelled 20" below original grade based on TP 12 (Bedrock ranging from 20" to 28". Proposed grade is approximately 3.2' above existing grade and therefore 4.87' above ledge.

[80] Warning: Exceeded Pond 6P by 0.20' @ 12.60 hrs (0.42 cfs 0.144 af)

Inflow Area = 0.031 ac, 85.88% Impervious, Inflow Depth > 6.63" for 50 Yr 24 Hr +15% event Inflow = 0.34 cfs @ 12.09 hrs, Volume= 0.017 af

Outflow = 0.19 cfs @ 12.16 hrs, Volume= 0.010 af, Atten= 43%, Lag= 3.9 min

Discarded = 0.19 cfs @ 12.15 hrs, Volume= 0.008 af

Secondary = 0.19 cfs @ 12.16 hrs, Volume= 0.002 af

Routed to Reach 6R : Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 67.20' @ 12.15 hrs Surf.Area= 0.006 ac Storage= 0.008 af

Plug-Flow detention time= 280.5 min calculated for 0.010 af (58% of inflow) Center-of-Mass det. time= 142.9 min (878.2 - 735.3)

<u>Volume</u>	Invert	Avail.Storage	Storage Description
#1	63.90'	0.008 af	14.00'W x 20.00'L x 3.30'H Prismatoid 0.021 af Overall x 40.0% Voids
Device	Routing	Invert Ou	utlet Devices
#0	Secondary	67.20' A ı	utomatic Storage Overflow (Discharged without head)
#1	Discarded	63.90' 0. 3	300 in/hr Exfiltration over Surface area
		Co	onductivity to Groundwater Elevation = 62.33' Phase-In= 0.10'

Discarded OutFlow Max=0.01 cfs @ 12.15 hrs HW=67.20' (Free Discharge) 1=Exfiltration (Controls 0.01 cfs)

Secondary OutFlow Max=0.00 cfs @ 12.16 hrs HW=67.20' TW=66.03' (Dynamic Tailwater)

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Summary for Pond 5P: Lined Stone Drip Edge

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=29)

Inflow Area = 0.018 ac, 75.74% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr +15% event

Inflow 0.15 cfs @ 12.09 hrs, Volume= 0.012 af

0.13 cfs @ 12.06 hrs, Volume= Outflow 0.012 af, Atten= 10%, Lag= 0.0 min

Primary 0.13 cfs @ 12.06 hrs, Volume= 0.012 af

Routed to Pond 3P : Stone Under Deck

0.00 hrs, Volume= 0.00 cfs @ 0.000 afSecondary =

Routed to Reach 6R: Flow through 3S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.22' @ 12.17 hrs Surf.Area= 0.003 ac Storage= 0.000 af

Plug-Flow detention time= 10.2 min calculated for 0.012 af (100% of inflow)

Center-of-Mass det. time= 9.9 min (749.9 - 740.0)

Volume	Invert	Avail.Storage	Storage Description
#1	66.00'	0.001 af	2.00'W x 63.00'L x 1.01'H Prismatoid
			0.003 af Overall x 40.0% Voids

Device	Routing	Invert	Outlet Devices			
#0	Secondary	67.01'	Automatic Storage Overflow (Discharged without head)			
#1	Primary	66.00'	6.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads			
#2	Secondary	67.00'	63.0' long x 1.0' breadth Broad-Crested Rectangular Weir			
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00			
			2.50 3.00			
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31			
			3.30 3.31 3.32			

Primary OutFlow Max=0.16 cfs @ 12.06 hrs HW=66.10' TW=65.88' (Dynamic Tailwater) -1=Orifice/Grate (Weir Controls 0.16 cfs @ 1.03 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=66.00' TW=66.00' (Dynamic Tailwater) -2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 6P: Lined Stone Drip Edge

[44] Hint: Outlet device #1 is below defined storage

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=87)

0.018 ac, 75.74% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr +15% event Inflow Area =

0.15 cfs @ 12.09 hrs, Volume= Inflow 0.012 af

0.15 cfs @ 12.14 hrs, Volume= 0.24 cfs @ 12.09 hrs, Volume= Outflow 0.012 af, Atten= 0%, Lag= 3.2 min

Primary 0.008 af

Routed to Pond 4P : Stone Under Deck

0.15 cfs @ 12.14 hrs, Volume= Secondary = 0.005 af

Routed to Reach 6R: Flow through 3S

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 67.01' @ 12.15 hrs Surf.Area= 0.003 ac Storage= 0.001 af

Plug-Flow detention time= 54.1 min calculated for 0.012 af (94% of inflow) Center-of-Mass det. time= 19.6 min (759.7 - 740.0)

<u>Volume</u>	Invert	Avail.Storage	e Storage Description		
#1	66.01'	0.001 af	2.00'W x 63.00'L x 1.01'H Prismatoid 0.003 af Overall x 40.0% Voids		
Device	Routing	Invert Ou	utlet Devices		
#1	Primary	66.00' 6. 0	D" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads		
#2	Secondary	67.00' 63	.0' long x 1.0' breadth Broad-Crested Rectangular Weir		
		He	ead (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00		
		2.5	50 3.00		
		Co	pef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31		
		3.3	30 3.31 3.32		

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=66.95' TW=67.09' (Dynamic Tailwater) 1=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.14 cfs @ 12.14 hrs HW=67.01' TW=66.03' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Weir Controls 0.14 cfs @ 0.25 fps)

Summary for Pond CB101: Catch Basin 101

Inflow Area = 0.022 ac,100.00% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr +15% event

Inflow = 0.18 cfs @ 12.09 hrs, Volume= 0.015 af

Outflow = 0.18 cfs @ 12.09 hrs, Volume= 0.015 af, Atten= 0%, Lag= 0.0 min

Primary = 0.18 cfs @ 12.09 hrs, Volume= 0.015 af

Routed to Pond CB102: Catch Basin 102

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 67.27' @ 12.13 hrs

Flood Elev= 70.10'

Device	Routing	Invert	Outlet Devices			
#1	Primary	66.60'	12.0" Round Culvert			
			L= 14.0' CPP, projecting, no headwall, Ke= 0.900			
			Inlet / Outlet Invert= 66.60' / 66.50' S= 0.0071 '/' Cc= 0.900			
			n= 0.012. Flow Area= 0.79 sf			

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=67.13' TW=67.18' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

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Summary for Pond CB102: Catch Basin 102

[80] Warning: Exceeded Pond CB101 by 0.07' @ 12.05 hrs (0.33 cfs 0.003 af)

Inflow Area = 0.047 ac,100.00% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr +15% event

Inflow = 0.38 cfs @ 12.09 hrs, Volume= 0.032 af

Outflow = 0.38 cfs @ 12.09 hrs, Volume= 0.032 af, Atten= 0%, Lag= 0.0 min

Primary = 0.38 cfs @ 12.09 hrs, Volume= 0.032 af

Routed to Pond yd1: Yard Drain 1

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 67.23' @ 12.10 hrs

Flood Elev= 70.10'

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=67.18' TW=67.25' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Pond CB103: Catch Basin 103

Inflow Area = 0.307 ac, 64.59% Impervious, Inflow Depth > 7.25" for 50 Yr 24 Hr +15% event

Inflow = 2.34 cfs @ 12.09 hrs, Volume= 0.185 af

Outflow = 2.34 cfs @ 12.09 hrs, Volume= 0.185 af, Atten= 0%, Lag= 0.0 min

Primary = 2.34 cfs @ 12.09 hrs, Volume= 0.185 af

Routed to Pond CB104: Catch Basin 104

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 67.15' @ 12.09 hrs

Flood Elev= 72.60'

Device	Routing	Invert	Outlet Devices			
#1	Primary	65.80'	12.0" Round Culvert			
			L= 43.0' CPP, projecting, no headwall, Ke= 0.900			
			Inlet / Outlet Invert= 65.80' / 65.50' S= 0.0070 '/' Cc= 0.900			
			n= 0.012, Flow Area= 0.79 sf			

Primary OutFlow Max=2.28 cfs @ 12.09 hrs HW=67.10' TW=66.52' (Dynamic Tailwater) 1=Culvert (Inlet Controls 2.28 cfs @ 2.91 fps)

Summary for Pond CB104: Catch Basin 104

Inflow Area = 0.314 ac, 65.44% Impervious, Inflow Depth > 7.28" for 50 Yr 24 Hr +15% event

Inflow = 2.40 cfs @ 12.09 hrs, Volume= 0.190 af

Outflow = 2.40 cfs @ 12.09 hrs, Volume= 0.190 af, Atten= 0%, Lag= 0.0 min

Primary = 2.40 cfs @ 12.09 hrs, Volume= 0.190 af

Routed to Pond 1P: Bioretention Pond

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.54' @ 12.09 hrs

Flood Elev= 71.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	65.40'	12.0" Round Culvert
			L= 31.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 65.40' / 65.20' S= 0.0065 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=2.34 cfs @ 12.09 hrs HW=66.52' TW=61.30' (Dynamic Tailwater) 1=Culvert (Inlet Controls 2.34 cfs @ 2.98 fps)

Summary for Pond YD1: Yard Drain 1

[80] Warning: Exceeded Pond CB102 by 0.07' @ 12.05 hrs (0.62 cfs 0.006 af)

Inflow Area = 0.152 ac, 65.02% Impervious, Inflow Depth > 7.29" for 50 Yr 24 Hr +15% event

Inflow 1.17 cfs @ 12.09 hrs, Volume= 0.092 af

Outflow 0.092 af, Atten= 0%, Lag= 0.0 min

1.17 cfs @ 12.09 hrs, Volume= 1.17 cfs @ 12.09 hrs, Volume= Primary 0.092 af

Routed to Pond CB103: Catch Basin 103

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 67.30' @ 12.09 hrs

Flood Elev= 69.30'

Device	Routing	Invert	Outlet Devices
#1	Primary	66.20'	12.0" Round Culvert
	-		L= 52.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 66.20' / 65.90' S= 0.0058 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=1.17 cfs @ 12.09 hrs HW=67.25' TW=67.10' (Dynamic Tailwater) 1=Culvert (Inlet Controls 1.17 cfs @ 1.48 fps)

Summary for Pond YD2: Yard Drain 2

Inflow Area = 0.086 ac, 35.30% Impervious, Inflow Depth > 6.36" for 50 Yr 24 Hr +15% event

Inflow 0.61 cfs @ 12.09 hrs, Volume= 0.045 af

0.61 cfs @ 12.09 hrs, Volume= Outflow 0.045 af, Atten= 0%, Lag= 0.0 min

0.61 cfs @ 12.09 hrs. Volume= Primary 0.045 af

Routed to Pond CB103: Catch Basin 103

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 67.55' @ 12.09 hrs

Flood Elev= 70.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	67.00'	8.0" Round Culvert

Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

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L= 13.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 67.00' / 66.13' S= 0.0669 '/' Cc= 0.900 n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.59 cfs @ 12.09 hrs HW=67.54' TW=67.11' (Dynamic Tailwater) —1=Culvert (Inlet Controls 0.59 cfs @ 1.97 fps)

APPENDIX III

Test Pit Logs



GOVE ENVIRONMENTAL SERVICES, INC. TEST PIT DATA

Project 635 Sagamore Ave

Client 635 Sagamore Development LLC

GES Project No. GES 2021307

MM/DD/YY Staff 3-18-2022 JPG

Test Pit No. 1

ESHWT: n/a

Termination @ 15"

Refusal: 15" SCS Soil: Hollis

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0-5" **NONE FSL** GR 10YR 3/2 FR **NONE** 5-15" 10YR 5/6 **FSL** GR FR

Test Pit No. 2

ESHWT: n/a

Termination @ 25"

Refusal: 25" SCS Soil: Chatfield

Obs. Water: none

Redox; Quantity/Contrast Depth Color Texture Structure Consistence 0-5" 10YR 3/2 **FSL** GR FR **NONE** 5-25" **FSL** GR FR **NONE** 10YR 5/6

Test Pit No. 3

ESHWT: n/a

Termination @ 25"

Refusal: 25" SCS Soil: Chatfield

Obs. Water: none

Depth Color **Texture** Structure Consistence Redox; Quantity/Contrast 0-6" 10YR 3/2 **FSL** GR FR **NONE** NONE 6-25" **FSL** GR FR 10YR 5/6

Hollis

Test Pit No. 4

ESHWT: n/a

Termination @ 15"

Refusal: 15" SCS Soil:

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0–15" 10YR 3/2 FSL GR FR NONE

Test Pit No. 5

ESHWT: 30"

Termination @ 36"

Refusal: 36" SCS Soil: Chatfield variant

Obs. Water: none

Depth Texture Structure Consistence Redox; Quantity/Contrast Color 0-8" **NONE** 10YR 3/2 **FSL** GR FR 8-30" 10YR 4/6 **FSL** GR FR **NONE** 30-36" 2.5Y 5/3 **FSL** GR FR 10% Distinct

Test Pit No. 6

ESHWT: n/a

Termination @ 12"

Refusal: 12" SCS Soil: Hollis

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0–12" 10YR 3/2 FSL GR FR NONE

Test Pit No. 7

ESHWT: n/a

Termination @ 27"

Refusal: 27" SCS Soil: Chatfield

Obs. Water: none

Depth Texture Structure Redox; Quantity/Contrast Color Consistence 0-4" 10YR 3/2 **FSL** GR FR **NONE** 4-27" 10YR 5/6 **FSL** GR FR **NONE**

Test Pit No. 8

ESHWT: 35"

Termination @ 40"

Refusal: 40" Obs. Water: none SCS Soil:

Chatfield variant

Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-6"	10YR 3/2	FSL	GR	FR	NONE
6-35"	10YR 5/6	FSL	GR	FR	NONE
35–40"	2.5Y 5/3	FSL	OM	FI	10% Distinct

Test Pit No. 9

ESHWT: n/a

Termination @ 27"

Refusal: 27" Obs. Water: none SCS Soil:

Chatfield

Scituate

Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-4"	10YR 3/2	FSL	GR	FR	NONE
4–27"	10YR 5/6	FSL	GR	FR	NONE

Test Pit No. 10

ESHWT: 35

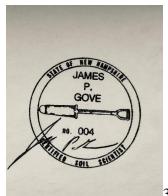
Termination @ 62"

Refusal: 62"

Obs. Water: none

Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-10"	10YR 3/2	FSL	GR	FR	NONE
10-35"	10YR 5/6	FSL	GR	FR	NONE
35–62"	2.5Y 5/3	FSL	PL	FI	10%. Distinct

SCS Soil:



Legend:

FSL = fine sandy loam GR = granular PL = platy FI = firm



GOVE ENVIRONMENTAL SERVICES, INC.

TEST PIT DATA

Project 635 Sagamore Ave., Portsmouth NH Client 635 Sagamore Development LLC

GES Project No. 2021308

MM/DD/YY Staff 07-24-2024 James Gove, CSS#004

Witnessed by: David Desfosses, City of Portsmouth

Test Pit No. Soils Series: Udorthents 11 ESHWT:: none Landscape: Paved Termination @ 32" Slope:

32" Parent Material: Refusal: Fill over till Obs. Water: None Hydrologic Soil Group: Impervious

Horizon Color (Munsell) Texture Structure-Consistence-Redox

Fill 1, 0-8" 10YR4/4 fine sandy loam massive-friable-none Fill 2, 8-19" 10YR2/1 ground pavement massive-firm-none Bw 18-32" 10YR5/6 fine sandy loam granular-friable-none

Test Pit No. **12** Soils Series: Chatfield ESHWT:: Hillside none Landscape: Termination @ 28" Slope: \mathbf{C}

Parent Material: Refusal: 28" Bedrock Till

Obs. Water: None Hydrologic Soil Group: В

Color (Munsell) Texture Structure-Consistence-Redox Horizon

A 0-6" 10YR3/2 fine sandy loam granular-friable-none granular-friable-none Bw 6-28" 10YR5/6 fine sandy loam

Bedrock ranges from 20" to 28" in test pit.

Test Pit No.13Soils Series:ChatfieldESHWT::noneLandscape:HillsideTermination @36"Slope:C

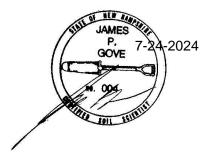
Refusal: 36" Parent Material: Bedrock Till

Obs. Water: None Hydrologic Soil Group: B

Horizon Color (Munsell) Texture Structure-Consistence-Redox fine sandy loam granular-friable-none A 0-6" 10YR3/2 Bw 6-24" 10YR4/6 fine sandy loam granular-friable-none C 24-36" fine sandy loam granular-friable-none 2.5Y5/3

Bedrock ranges from 24" to 36" in test pit.

Note: Site should be calculated as HSG C, due to the limited infiltration in thin soil layers above the bedrock.



Test Pit Data: 635 Sagamore Ave. 7-24-2024 —Page 4 of 4

APPENDIX IV

Site Specific Soil Survey Report and Map



GOVE ENVIRONMENTAL SERVICES, INC

SITE-SPECIFIC SOIL SURVEY REPORT
For
635 Sagamore Avenue, Portsmouth, NH
By
GES, Inc.
Project # 2021308

Date: 02-20-2024

1. MAPPING STANDARDS

Site-Specific Soil Mapping Standards for New Hampshire and Vermont. SSSNNE Special Publication No. 3, Version 7.0, July, 2021.

This map product is within the technical standards of the National Cooperative Soil Survey. It is a special purpose product, intended for infiltration requirements by the NH DES Alteration of Terrain Bureau. The soil map was produced by a professional soil scientist and is not a product of the USDA Natural Resources Conservation Service. This report accompanies the soil map.

The site-specific soil map (SSSM) was produced 2-20-2024; prepared by JP Gove, CSS #004, GES, Inc.

Soils were identified with the New Hampshire State-wide Numerical Soils Legend, USDA NRCS, Durham, NH. Issue # 10, January 2011.

Hydrologic Soil Group was determined using SSSNNE Special Publication No. 5, Ksat Values for New Hampshire Soils, September 2009.

High Intensity Soil Map symbols, based upon SSSNNE Special Publication 1, December 2017, were added to the Soil Legend.

Scale of soil map: Approximately 1'' = 20'.

Contours Interval: 2 feet

2. LANDFORMS & EXISTING CONDITIONS:

The site is located on sloping hillside that is bedrock controlled. Rock outcrops are numerous. At the top of the hill, adjacent Sagamore Avenue, is an existing commercial building and paved areas. Behind the impervious areas to the south, the hillside slopes downward. The area is forested in white pines. There are no wetlands on the site.

3. <u>DATE SOIL MAP PRODUCED</u>

Date(s) of on-site field work: 3-18-2022

Date(s) of test pits: 3-18-2922

Test pits recorded by: JP Gove, CSS # 004

4. GEOGRAPHIC LOCATION AND SIZE OF SITE

City or town where soil mapping was conducted: Portsmouth, NH

Location: Tax Map 222 Lot 19

Size of area: Approximately 2 acres

Was the map for the entire lot? Yes

If no, where was the mapping conducted on the parcel: n/a

5. PURPOSE OF THE SOIL MAP

Was the map prepared to meet the requirement of Alteration of Terrain? No

If no, what was the purpose of the map? City of Portsmouth requirements

Who was the map prepared for? Jones & Beach Engineers, Inc.



6. SOIL IDENTIFICATION LEGEND

Map	Unit Sym	ibol Map Unit N	lame		HISS Symb	ool	Hydrol	ogic Soil Group	
41	Chatfi	eld-Hollis-Rock C	outcrop complex		228		В		
289	Chatfi	eld Variant (mod	erately well drai	ned)	327		В		
699	Urban	Land			n/a		Imperv	rious	
SLOP	E PHASE:								
0-8%		В	8-15%	С		15-25%	,)	D	
25%-	50%	E	50%+	F					

7. NARRATIVE MAP UNIT DESCRIPTIONS

SITE-SPECIFIC MAP UNIT: 41

CORRELATED SOIL SERIES: Chatfield-Hollis-Rock Outcrop complex

LANDSCAPE SETTING: Sloping to very steep hillside.

CHARACTERISTIC SURFACE FEATURES: Numerous rock outcrops

DRAINAGE CLASS: Well drained

PARENT MATERIAL: Glacial Till

NATURE OF DISSIMILAR INCLUSIONS: With a complex, several similar soils are present. While the major soil is the moderately deep Chatfield, the shallow Hollis and the exposed ledge of the Rock Outcrop, are large minor components. Chatfield is 50%, Hollis is 25%, and Rock Outcrop is 25%. A few deeper soil areas are present in hollow in the bedrock.

ESTIMATED PERCENTAGE OF DISSIMILAR INCLUSIONS: less than 5%.

SOIL PROFILE DESCRIPTIONS- horizon designation, depth, soil texture, Munsell color notation, Munsell color of redox features, soil structure, soil consistence, estimated coarse fragments, estimated seasonal high water table (ESHWT), observed water table (OBSWT), kind of water table (perched, apparent, or both), depth to lithic or paralithic contact:

Test Pit No. 3

ESHWT: n/a

Termination @ 25"

Refusal: 25"

Obs. Water: none

SCS Soil: Chatfield

Structure Consistence Redox; Quantity/Contrast Depth Color Texture 0-6" 10YR 3/2 FSL GR FR **NONE** 6-25" 10YR 5/6 **FSL** GR FR **NONE**

No OBSWT, no ESHWT, lithic contact at 25", 20% rock fragments.

Test Pit No. 1

ESHWT: n/a

Termination @ 15"

Refusal: 15" SCS Soil: Hollis

Obs. Water: none

Depth Color Texture Structure Consistence Redox; Quantity/Contrast 0-5" 10YR 3/2 FSL GR FR **NONE** 5-15" 10YR 5/6 **FSL** GR FR NONE

No OBSWT, no ESHWT, lithic contact at 15", 20% rock fragments.

SITE-SPECIFIC MAP UNIT: 289

CORRELATED SOIL SERIES: Chatfield Variant (moderately well drained)



LANDSCAPE SETTING: At the top of the slope, a slightly deeper soil area on the northwest corner of the site.

CHARACTERISTIC SURFACE FEATURES: Fewer outcrops than the rest of the site.

DRAINAGE CLASS: Moderately well drained.

PARENT MATERIAL: Glacial till.

NATURE OF DISSIMILAR INCLUSIONS: Scituate soils with a hard pan above the bedrock,

ESTIMATED PERCENTAGE OF DISSIMILAR INCLUSIONS: 5%

SOIL PROFILE DESCRIPTIONS- horizon designation, depth, soil texture, Munsell color notation, Munsell color of redox features, soil structure, soil consistence, estimated coarse fragments, estimated seasonal high water table (ESHWT), observed water table (OBSWT), kind of water table (perched, apparent, or both), depth to lithic or paralithic contact:

Test Pit No. 5

ESHWT: 30"

Termination @ 36"

Refusal: 36" SCS Soil: Chatfield variant

Obs. Water: none

Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-8"	10YR 3/2	FSL	GR	FR	NONE
8-30"	10YR 4/6	FSL	GR	FR	NONE
30-36"	2.5Y 5/3	FSL	GR	FR	10% Distinct

ESHWT is 30", no OBSWT, lithic contact at 36", 20% rock fragments.

SITE-SPECIFIC MAP UNIT: 699

CORRELATED SOIL SERIES: Urban land

LANDSCAPE SETTING: Top of slope adjacent to Sagamore Avenue.

CHARACTERISTIC SURFACE FEATURES: Impervious.

DRAINAGE CLASS: N/A

PARENT MATERIAL: N/A

NATURE OF DISSIMILAR INCLUSIONS: N/A

ESTIMATED PERCENTAGE OF DISSIMILAR INCLUSIONS: N/A

SOIL PROFILE DESCRIPTIONS- horizon designation, depth, soil texture, Munsell color notation, Munsell color of redox features, soil structure, soil consistence, estimated coarse fragments, estimated seasonal high water table (ESHWT), observed water table (OBSWT), kind of water table (perched, apparent, or both), depth to lithic or paralithic contact:

N/A ---- Pavement and buildings.



8. RESPONSIBLE SOIL SCIENTIST

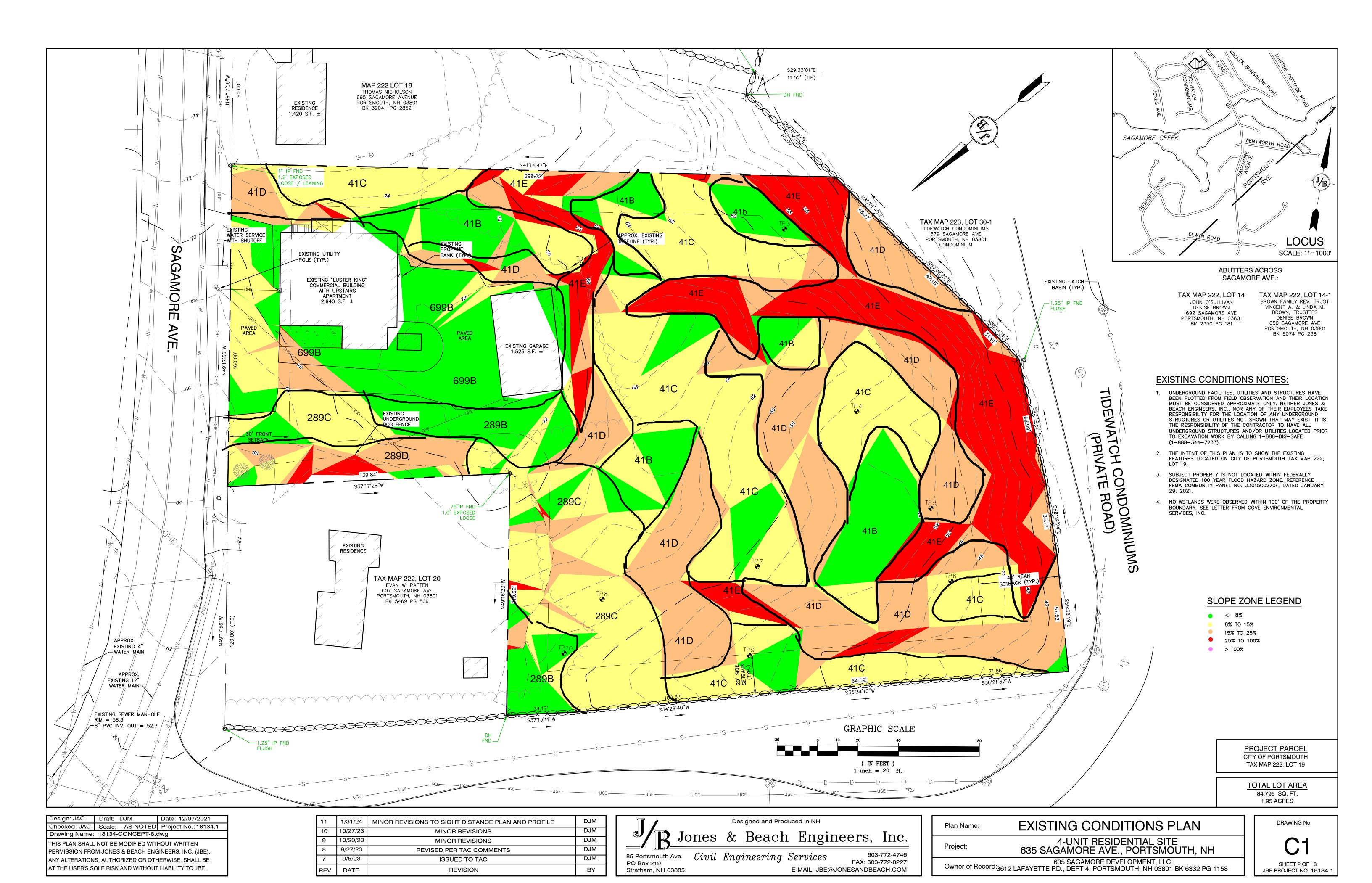
Name: James Gove

Certified Soil Scientist Number: 004

9. OTHER DISTINGUISHING FEATURES OF SITE

Is the site in a natural condition? Yes, with exception of existing development.

info@gesinc.biz



APPENDIX V

NRCS Soil Map



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons



Soil Map Unit Points

Special Point Features

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

+ Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot

Other

Special Line Features

Water Features

Δ

Streams and Canals

Transportation

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Rockingham County, New Hampshire Survey Area Data: Version 26, Aug 22, 2023

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Jun 19, 2020—Sep 20, 2020

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

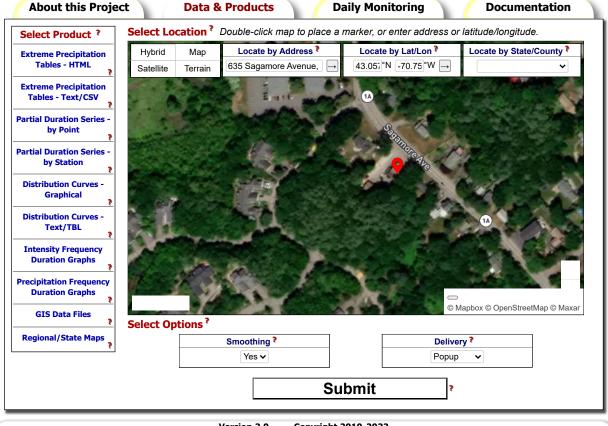
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
140B	Chatfield-Hollis-Canton complex, 0 to 8 percent slopes, rocky	0.7	30.5%
140D	Chatfield-Hollis-Canton complex, 15 to 35 percent slopes, rocky	1.6	69.5%
Totals for Area of Interest	•	2.3	100.0%

APPENDIX VI

Extreme Precipitation Estimates

Extreme Precipitation in New York & New England

An Interactive Web Tool for Extreme Precipitation Analysis



Version 2.0 Copyright 2010-2022
This project is a joint collaboration between:
Northeast Regional Climate Center (NRCC)
Natural Resources Conservation Service (NRCS)

SDA ONRCS
Contact: precip@cornell.edu

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Metadata for Point

Smoothing Yes

State Location

Latitude 43.058 degrees North Longitude 70.753 degrees West

Elevation 10 feet

Date/Time Wed Feb 21 2024 09:41:54 GMT-0500 (Eastern Standard

Time)

+15% due to location in Coastal/Great Bay Region

2yr: 3.22*1.15 = 3.70 in 10yr: 4.88*1.15 = 5.16 in 25yr: 6.19*1.15 = 7.12 in

50yr: 7.42*1.15 = 8.53 in

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day
1yr	0.26	0.40	0.50	0.65	0.82	1.04	1yr	0.70	0.98	1.21	1.56	2.03	2.67	2.94	1yr	2.36	2.82	3.24	3.96	4.57
2yr	0.32	0.50	0.62	0.82	1.03	1.30	2yr	0.89	1.18	1.52	1.94	2.49	3.22	3.58	2yr	2.85	3.45	3.95	4.70	5.35
5yr	0.37	0.58	0.73	0.98	1.25	1.61	5yr	1.08	1.47	1.89	2.44	3.15	4.08	4.60	5yr	3.61	4.42	5.07	5.96	6.73
10yr	0.41	0.65	0.82	1.12	1.46	1.90	10yr	1.26	1.73	2.24	2.90	3.76	4.88	5.55	10yr	4.32	5.34	6.12	7.14	8.01
25yr	0.48	0.76	0.97	1.34	1.78	2.35	25yr	1.54	2.15	2.79	3.65	4.76	6.19	7.13	25yr	5.48	6.86	7.85	9.07	10.09
50yr	0.54	0.86	1.11	1.55	2.08	2.77	50yr	1.80	2.54	3.31	4.35	5.69	7.42	8.62	50yr	6.57	8.29	9.48	10.87	12.02
100yr	0.60	0.97	1.25	1.78	2.43	3.28	100yr	2.10	2.99	3.93	5.19	6.80	8.89	10.42	100yr	7.87	10.02	11.46	13.04	14.33
200yr	0.68	1.11	1.44	2.06	2.85	3.86	200yr	2.46	3.54	4.65	6.17	8.12	10.65	12.60	200yr	9.43	12.12	13.85	15.64	17.09
500yr	0.81	1.33	1.73	2.51	3.51	4.80	500yr	3.03	4.41	5.81	7.76	10.28	13.54	16.21	500yr	11.98	15.59	17.81	19.90	21.58

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day
1yr	0.23	0.36	0.44	0.59	0.72	0.88	1yr	0.62	0.86	0.93	1.33	1.69	2.26	2.51	1yr	2.00	2.41	2.88	3.20	3.93
2yr	0.32	0.49	0.60	0.81	1.00	1.19	2yr	0.86	1.16	1.37	1.82	2.33	3.07	3.47	2yr	2.72	3.33	3.84	4.56	5.11
5yr	0.35	0.54	0.67	0.92	1.17	1.40	5yr	1.01	1.37	1.61	2.11	2.73	3.80	4.21	5yr	3.36	4.05	4.74	5.56	6.27
10yr	0.39	0.59	0.74	1.03	1.33	1.60	10yr	1.15	1.57	1.81	2.38	3.05	4.39	4.88	10yr	3.88	4.70	5.48	6.45	7.23
25yr	0.44	0.67	0.83	1.19	1.57	1.90	25yr	1.35	1.86	2.10	2.74	3.52	4.77	5.92	25yr	4.22	5.70	6.70	7.85	8.73
50yr	0.48	0.73	0.92	1.32	1.77	2.17	50yr	1.53	2.12	2.35	3.06	3.91	5.40	6.84	50yr	4.78	6.58	7.79	9.11	10.08
100yr	0.54	0.81	1.02	1.47	2.02	2.47	100yr	1.74	2.42	2.63	3.39	4.33	6.08	7.90	100yr	5.38	7.60	9.07	10.60	11.64
200yr	0.59	0.89	1.13	1.64	2.29	2.82	200yr	1.97	2.75	2.94	3.75	4.76	6.83	9.12	200yr	6.05	8.77	10.54	12.34	13.47
500yr	0.69	1.02	1.32	1.92	2.72	3.37	500yr	2.35	3.29	3.42	4.28	5.41	7.97	11.03	500yr	7.06	10.61	12.87	15.13	16.32

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day
1yr	0.29	0.44	0.54	0.72	0.89	1.08	1yr	0.77	1.06	1.26	1.74	2.20	2.99	3.18	1yr	2.64	3.05	3.59	4.38	5.06
2yr	0.34	0.52	0.64	0.87	1.07	1.27	2yr	0.92	1.24	1.48	1.96	2.51	3.43	3.72	2yr	3.03	3.57	4.10	4.86	5.64
5yr	0.40	0.62	0.77	1.05	1.34	1.63	5yr	1.16	1.59	1.89	2.54	3.25	4.36	4.98	5yr	3.85	4.79	5.40	6.40	7.18
10yr	0.47	0.72	0.89	1.25	1.61	1.98	10yr	1.39	1.94	2.29	3.11	3.96	5.36	6.22	10yr	4.74	5.98	6.84	7.87	8.78
25yr	0.58	0.88	1.09	1.56	2.06	2.58	25yr	1.77	2.52	2.96	4.08	5.17	7.77	8.36	25yr	6.87	8.04	9.18	10.37	11.44
50yr	0.67	1.03	1.28	1.84	2.48	3.15	50yr	2.14	3.08	3.61	5.01	6.35	9.71	10.48	50yr	8.60	10.08	11.48	12.76	14.00
100yr	0.80	1.20	1.51	2.17	2.98	3.83	100yr	2.57	3.75	4.39	6.18	7.80	12.14	13.13	100yr	10.74	12.62	14.35	15.74	17.13
200yr	0.93	1.40	1.78	2.57	3.58	4.69	200yr	3.09	4.58	5.36	7.61	9.60	15.22	16.46	200yr	13.47	15.83	17.96	19.40	20.96
500yr	1.16	1.72	2.22	3.22	4.58	6.09	500yr	3.95	5.95	6.96	10.07	12.65	20.54	22.22	500yr	18.18	21.36	24.18	25.57	27.38



APPENDIX VII

Rip Rap Calculations

RIP RAP CALCULATIONS

"Luster Cluster" 635 Sagamore Ave. Portsmouth, NH

Jones & Beach Engineers, Inc.

P.O. Box 219 Stratham, NH 03885 3/14/2024 REVISED 4/19/2024 REVISED 8/8/2024

Rip Rap equations were obtained from the *Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire.*Aprons are sized for the 10-Year storm event.

TAILWATER < HALF THE D_o

 $L_a = (1.8 \text{ x Q}) / D_0^{3/2} + (7 \text{ x D}_o)$

 $W = L_a + (3 \times D_o)$ or defined channel width

$$d_{50} = (0.02 \text{ x } Q^{4/3}) / (T_w \text{ x } D_0)$$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	d ₅₀ -Median Stone
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	Rip Rap
(Sta. No.)	$T_{\rm w}$	Q	D_{o}	L _a (feet)	W (feet)	d50 (feet)
1P Outlet Pipe	0.37	1.55	1	9.8	13	0.10

TAILWATER > HALF THE D_o

 $L_a = (3.0 \text{ x Q}) / D_0^{3/2} + (7 \text{ x D}_o)$

 $W = (0.4 \text{ x L}_a) + (3 \text{ x D}_o)$ or defined channel width

$$d_{50} = (0.02 \text{ x } Q^{4/3}) / (T_w \text{ x } D_0)$$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	d ₅₀ -Median Stone
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	Rip Rap
(Sta. No.)	$T_{ m w}$	Q	D_{o}	L_a (feet)	W (feet)	d50 (feet)
CB104 Outlet Pipe	0.59	1.96	1	12.9	8	0.08

d ₅₀ Size =	0.25	Feet	3	Inches
% of Weight Smaller		Size	e of Stone (In	ches)
Than the Given d ₅₀ Size		From		To
100%		5		6
85%		4		5
50%		3		5
15%		1		2

Table 7-24 Recommended Rip Rap Gradation Ranges											
d ₅₀ Size =	0.5	Feet	6	Inches							
% of Weight Smaller		Size	of Stone (Inc	ches)							
Than the Given d ₅₀ Size		From		To							
100%		9		12							
85%		8		11							
50%		6		9							
15%		2		3							

APPENDIX VIII

BMP Worksheets



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name: Bioretention Pond (1P)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

Yes	_	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.0	7(a).
0.54	ac	A = Area draining to the practice	
0.24	ac	A _I = Impervious area draining to the practice	
0.45	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.46	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
0.25	ac-in	WQV= 1" x Rv x A	
895	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
224	_	25% x WQV (check calc for sediment forebay volume)	
671		75% x WQV (check calc for surface sand filter volume)	
	t Forebay	_Method of Pretreatment? (not required for clean or roof runoff)	
231	cf	V _{SED} = Sediment forebay volume, if used for pretreatment	<u>></u> 25%WQV
Calculate ti	me to drain	if system IS NOT underdrained:	
	sf	A _{SA} = Surface area of the practice	
	iph	Ksat _{DESIGN} = Design infiltration rate ¹	
	-	If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?	
	Yes/No	(Use the calculations below)	
-	hours	$T_{DRAIN} = Drain time = V / (A_{SA} * I_{DESIGN})$	< 72-hrs
Calculate ti	me to drain	if system IS underdrained:	
61.61	ft	E _{WQV} = Elevation of WQV (attach stage-storage table)	
2.32	cfs	Q_{WQV} = Discharge at the E_{WQV} (attach stage-discharge table)	
0.21	hours	$T_{DRAIN} = Drain time = 2WQV/Q_{WQV}$	≤ 72-hrs
0.21 59.10		T_{DRAIN} = Drain time = $2WQV/Q_{WQV}$ E_{FC} = Elevation of the bottom of the filter course material ²	<u><</u> 72-hrs
	feet		<u><</u> 72-hrs
59.10	feet feet	E _{FC} = Elevation of the bottom of the filter course material ²	
59.10 58.35	feet feet feet	E_{FC} = Elevation of the bottom of the filter course material ² E_{UD} = Invert elevation of the underdrain (UD), if applicable	it)
59.10 58.35 58.08	feet feet feet feet	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p	it)
59.10 58.35 58.08 57.67	feet feet feet feet feet	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test	it) pit)
59.10 58.35 58.08 57.67 0.75	feet feet feet feet feet feet	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test D _{FC to UD} = Depth to UD from the bottom of the filter course	it) pit) > 1'
59.10 58.35 58.08 57.67 0.75 1.43	feet feet feet feet feet feet feet feet	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test $D_{FC \text{ to } UD}$ = Depth to UD from the bottom of the filter course $D_{FC \text{ to } ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC \text{ to } SHWT}$ = Depth to SHWT from the bottom of the filter course	it) pit) > 1' > 1'
59.10 58.35 58.08 57.67 0.75 1.43	feet feet feet feet feet feet feet ft	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test $D_{FC \text{ to } UD}$ = Depth to UD from the bottom of the filter course $D_{FC \text{ to } ROCK}$ = Depth to bedrock from the bottom of the filter course	it) pit) > 1' > 1'
59.10 58.35 58.08 57.67 0.75 1.43 1.02 61.60	feet feet feet feet feet feet feet ft	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test $D_{FC \text{ to } UD}$ = Depth to UD from the bottom of the filter course $D_{FC \text{ to } ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC \text{ to } SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis)	it) pit) > 1' > 1'
59.10 58.35 58.08 57.67 0.75 1.43 1.02 61.60 62.70 YES	feet feet feet feet feet feet ft ft	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test $D_{FC \text{ to UD}}$ = Depth to UD from the bottom of the filter course $D_{FC \text{ to ROCK}}$ = Depth to bedrock from the bottom of the filter course $D_{FC \text{ to SHWT}}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice	it) pit) ≥ 1' ≥ 1' ≥ 1'
59.10 58.35 58.08 57.67 0.75 1.43 1.02 61.60 62.70 YES	feet feet feet feet feet feet ft ft	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test $D_{FC \text{ to } UD}$ = Depth to UD from the bottom of the filter course $D_{FC \text{ to } ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC \text{ to } SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice 50 peak elevation \leq Elevation of the top of the practice	it) pit) ≥ 1' ≥ 1' ≥ 1'
59.10 58.35 58.08 57.67 0.75 1.43 1.02 61.60 62.70 YES	feet feet feet feet feet ft tt sand filter	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test $D_{FC \text{ to } UD}$ = Depth to UD from the bottom of the filter course $D_{FC \text{ to } ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC \text{ to } SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice 50 peak elevation \leq Elevation of the top of the practice or underground sand filter is proposed:	it) pit) ≥ 1' ≥ 1' ≥ 1'
59.10 58.35 58.08 57.67 0.75 1.43 1.02 61.60 62.70 YES	feet feet feet feet feet feet fet sand filter	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test $D_{FC \text{ to } UD}$ = Depth to UD from the bottom of the filter course $D_{FC \text{ to } ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC \text{ to } SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice 50 peak elevation \leq Elevation of the top of the practice or underground sand filter is proposed: Drainage Area check.	it) pit) ≥ 1' ≥ 1' ≥ 1'
59.10 58.35 58.08 57.67 0.75 1.43 1.02 61.60 62.70 YES	feet feet feet feet feet feet ft tt tt sand filter ac cf inches	E_{FC} = Elevation of the bottom of the filter course material 2 E_{UD} = Invert elevation of the underdrain (UD), if applicable E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test $D_{FC \text{ to } UD}$ = Depth to UD from the bottom of the filter course $D_{FC \text{ to } ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC \text{ to } SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice 50 peak elevation \leq Elevation of the top of the practice or underground sand filter is proposed: Drainage Area check. $V = Volume \text{ of storage}^3$ (attach a stage-storage table)	it) pit) ≥ 1' ≥ 1' ≥ 1' < yes < 10 ac ≥ 75%WQV 18", or 24" if

If a biorete	ntion a	rea i	is proposed:	
YES	ac		Drainage Area no larger than 5 ac?	← yes
992	cf		V = Volume of storage ³ (attach a stage-storage table)	<u>></u> WQV
18.0	inches		D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet		D4	Note what sheet in the plan set contains the filter course specification	
3.0	:1		Pond side slopes	<u>> 3</u> :1
Sheet		D4	Note what sheet in the plan set contains the planting plans and surface cover	
If porous p	avemen	t is	proposed:	
			Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acres		A _{SA} = Surface area of the pervious pavement	
	:1		Ratio of the contributing area to the pervious surface area	≤ 5:1
	inches		D _{FC} = Filter course thickness	12", or 18" if within GPA
Sheet			Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

- 1. Rate of the limiting layer (either the filter course or the underlying soil). Ksat_{design} includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
- 2. See lines 34, 40 and 48 for required depths of filter media.
- 3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:
SHWT elevation at high contour is only 0.01' below the bottom of the stone. However, we modelled it 2" lower in
the HydroCAD calculations as a factor of safety. Modelling such a small separation from the bottom of the stone
to the SHWT causes an unrealistically high amount of exfiltration to appear in the results.
Test Pits #8 and #10 used for design. Both test pits indicate a depth to SHWT of 35". TP 8 indicates a depth to
refusal of 40". Existing high contour in filter course area is 61, so SHWT and bedrock elevations were
derived accordingly.

Last Revised: January 2019

60.39

60.44

60.49

60.54

60.59

60.64

Printed 8/8/2024

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Stage-Area-Storage for Pond 1P: Bioretention Pond

Elevation Surface Storage (feet) Elevation (sq-ft) Surface (feet) Storage (feet) 58.09 117 0 60.69 208 89 58.14 117 2 60.74 270 101	
58.09 117 0 60.69 208 89	
58.19 117 5 60.79 341 116	
58.24 117 7 60.84 419 135	
58.29 117 9 60.89 505 158 Underdrain inv. = 58.35	
58.34 117 12 60.94 600 186 Vol. below = 12 cfs for	
58.39 117 14 60.99 702 218 GRV calculation	
58.44 117 16 61.04 1,043 268	
58.49 117 19 61.09 1,064 321	
58.54 117 21 61.14 1,085 374	
58.59 117 23 61.19 1,107 429	
58.64 117 26 61.24 1,129 485 Bottom of filter course = \$	59.1
58.69 117 28 61.29 1,151 542 Volume in stone voids be	
00.00	
·	
58.89 117 37 61.49 1,241 781 895+47 = 942 cf	
58.94 117 40 61.54 1,264 844 E(WQV) = 61.61 by	
58.99 117 42 61.59 1,288 908 interpolation	
59.04 117 44 <u>61.64 1,311 973</u>	
59.09 117 47 61.69 1,335 1,039 Overflow el. = 61.7	
59.14 117 48 61.74 1,359 1,106 Vol. below = 1,039 cf	
59.19 117 49 61.79 1,383 1,175	
59.24 117 49 61.84 1,408 1,244 WQV Provided = 1039-47	7 =
59.29 117 50 61.89 1,432 1,315 <u>992 cf</u> > 895 cf	
59.34 117 51 61.94 1,457 1,388	
59.39 117 52 61.99 1,482 1,461	
59.44 117 53 62.04 1,509 1,536	
59.49 117 54 62.09 1,537 1,612	
59.54 117 55 62.14 1,565 1,690	
59.59 117 56 62.19 1,594 1,769	
59.64 117 56 62.24 1,622 1,849	
59.69 117 57 62.29 1,651 1,931	
59.74 117 58 62.34 1,680 2,014	
59.79 117 59 62.39 1,710 2,099	
59.84 117 60 62.44 1,739 2,185	
59.89 117 61 62.49 1,769 2,273	
59.94 117 62 62.54 1,800 2,362	
59.99 117 63 62.59 1,830 2,453	
60.04 117 63 62.64 1,861 2,545	
60.09 117 64 62.69 1,892 2,639	
60.14 117 65	
60.19 117 66	
60.24 117 67	
60.29 117 68	
60.34 117 69	

60.29

60.34

60.39

60.44

60.49

60.54

60.59

60.64

1.51

1.53

1.56

1.58

1.60

1.63

1.65

1.68

0.28

0.29

0.29

0.30

0.30

0.31

0.31

0.33

1.23

1.25

1.26

1.28

1.30

1.32

1.33

1.35

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Stage-Discharge for Pond 1P: Bioretention Pond

Elevation	Discharge	Discarded	Primary	Elevation	Discharge	Discarded	Primary	
(feet)	(cfs)	(cfs)	(cfs)	(feet)	(cfs)	(cfs)	(cfs)	
58.09	0.00	0.00	0.00	60.69	1.71	0.34	1.37	
58.14	0.01	0.01	0.00	60.74	1.74	0.36	1.38	
58.19	0.03	0.03	0.00	60.79	1.78	0.38	1.40	
58.24	0.04	0.04	0.00	60.84	1.81	0.40	1.41	
58.29	0.04	0.04	0.00	60.89	1.85	0.42	1.43	
58.34	0.05	0.05	0.00	60.94	1.89	0.44	1.45	
58.39	0.06	0.06	0.01	60.99	1.93	0.47	1.46	
58.44	0.09	0.06	0.02	61.04	2.01	0.53	1.48	
58.49	0.12	0.07	0.06	61.09	2.04	0.55	1.49	
58.54	0.17	0.07	0.10	61.14	2.07	0.56	1.51	
58.59	0.23	0.08	0.16	61.19	2.09	0.57	1.52	
58.64	0.30	0.08	0.22	61.24	2.12	0.58	1.54	
58.69	0.37	0.09	0.28	61.29	2.15	0.60	1.55	
58.74	0.45	0.10	0.35	61.34	2.17	0.61	1.56	
58.79	0.52	0.10	0.41	61.39	2.20	0.62	1.58	
58.84	0.57	0.11	0.47	61.44	2.23	0.63	1.59	
58.89	0.62	0.11	0.51	61.49	2.25	0.65	1.61	
58.94	0.67	0.12	0.55	61.54	2.28	0.66	1.62	
58.99	0.72	0.13	0.59	61.59	2.31	0.67		E(WQV) = 61.61 per
59.04	0.76	0.13	0.63	61.64	2.33	0.69		stage storage table
59.09	0.80	0.14	0.66	61.69	2.36	0.70		Q(WQV) = 2.32 cfs
59.14	0.84	0.14	0.69	61.74	2.51	0.71	1.80	
59.19	0.88	0.15	0.73	61.79	2.83	0.73	2.10	
59.24	0.91	0.16	0.76	61.84	3.25	0.74	2.51	
59.29	0.95	0.16	0.79	61.89	3.74	0.75	2.99	
59.34	0.98	0.17	0.81	61.94	4.31	0.77	3.54	
59.39	1.01	0.17	0.84	61.99	4.93	0.78	4.15	
59.44	1.05	0.18	0.87	62.04	5.60	0.80	4.81	
59.49	1.08	0.19	0.89	62.09	6.18	0.81	5.37	
59.54	1.11	0.19	0.92	62.14	6.24	0.82	5.42	
59.59	1.14	0.20	0.94	62.19	6.30	0.84	5.46	
59.64	1.17	0.20	0.96	62.24	6.35	0.85	5.50	
59.69	1.20	0.21	0.99	62.29	6.41	0.87	5.54	
59.74	1.22	0.21	1.01	62.34	6.46	0.88	5.58	
59.79	1.25	0.22	1.03	62.39	6.52	0.90	5.62	
59.84	1.28	0.23	1.05	62.44	6.57	0.91	5.66	
59.89	1.31	0.23	1.07	62.49	6.63	0.93	5.70	
59.94	1.33	0.24	1.09	62.54	6.68	0.94	5.74	
59.99	1.36	0.24	1.11	62.59	6.73	0.96	5.77	
60.04	1.38	0.25	1.13	62.64	6.79	0.98	5.81	
60.09	1.41	0.26	1.15	62.69	6.84	0.99	5.85	
60.14	1.43	0.26	1.17					
60.19	1.46	0.27	1.19					
60.24	1.48	0.27	1.21					



GROUNDWATER RECHARGE VOLULME (GRV) CALCULATION (Env-Wq 1507.04)

	ac	Area of HSG A soil that was replaced by impervious cover	0.40"
0.12	ac	Area of HSG B soil that was replaced by impervious cover	0.25"
	ac	Area of HSG C soil that was replaced by impervious cover	0.10"
	ac	Area of HSG D soil or impervious cover that was replaced by impervious cover	0.0"
0.25 inches		Rd = Weighted groundwater recharge depth	
0.031	ac-in	GRV = AI * Rd	
113	cf	GRV conversion (ac-in x 43,560 sf/ac x 1ft/12")	

Provide calculations below showing that the project meets the groundwater recharge requirements (Env-Wq 1507.04):

Stone Beneath Units 3&4 decks: (14 ft * 20 ft *3 ft)*0.4*2 = 672 cf
Bioretention: 12 cf GRV provided below UD end cap orifice per stage storage table
GRV Provided = 672+12 = 684 cf > 113 cf

APPENDIX IX

Pollutant Removal Calculations

POLLUTANT REMOVAL CALCULATIONS

BMP	Drip Edge	Bioretention	None	Total	Required
Acres Impervious	0.053	0.244	0.039	0.335	
TSS Removal (%)	90%	90%	0%	80%	80%
TN Removal (%)	55%	65%	0%	67%	50%

Calculations are based on post-construction impervious surfaces directed toward AP3 and AP4. Post-construction impervious surfaces directed toward AP1 are handled offsite via the City's drainage system, and the amount of impervious surface directed toward AP1 is being decreased post-construction.

Stone underneath decks are assumed to provide similar treatment to a stone drip edge.

TSS removal of 80% provided meets 80% requirement

TN removal of 67% provided exceeds 50% requirement

Pollutant Ro	Values Accepted for Loading Analyses					
BMP Type	ВМР	Notes	Lit. Ref.	TSS	TN	TP
	Wet Pond		B, F	70%	35%	45%
01	Wet Extended Detention Pond		A, B	80%	55%	68%
Stormwater Ponds	Micropool Extended Detention Pond	TBA				
	Multiple Pond System	TBA				
	Pocket Pond	TBA				
	Shallow Wetland		A, B, F, I	80%	55%	45%
Stormwater	Extended Detention Wetland		A, B, F, I	80%	55%	45%
Wetlands	Pond/Wetland System	TBA				
	Gravel Wetland		Н	95%	85%	64%
	Infiltration Trench (≥75 ft from surface water)		B, D, I	90%	55%	60%
	Infiltration Trench (<75 ft from surface water)		B, D, I	90%	10%	60%
Infiltration Practices	Infiltration Basin (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%
	Infiltration Basin (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%
	Dry Wells			90%	55%	60%
	Drip Edges			90%	55%	60%
	Aboveground or Underground Sand Filter that infiltrates WQV (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%
	Aboveground or Underground Sand Filter that infiltrates WQV (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%
	Aboveground or Underground Sand Filter with underdrain		A, I, F, G, H	85%	10%	45%
Filtering	Tree Box Filter	TBA				
Practices	Bioretention System		I, G, H	90%	<mark>65%</mark>	<mark>65%</mark>
	Permeable Pavement that infiltrates WQV (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%
	Permeable Pavement that infiltrates WQV (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%
	Permeable Pavement with underdrain		Use TN and TP values for sand filter w/ underdrain and outlet pipe	90%	10%	45%

Pollutant R	Values Accepted for Loading Analyses					
BMP Type	ВМР	Notes	Lit. Ref.	TSS	TN	TP
Treatment Swales	Flow Through Treatment Swale	TBA				
Vegetated Buffers	Vegetated Buffers		A, B, I	73%	40%	45%
	Sediment Forebay	TBA				
	Vegetated Filter Strip		A, B, I	73%	40%	45%
	Vegetated Swale		A, B, C, F, H, I	65%	20%	25%
Pre-	Flow-Through Device - Hydrodynamic Separator		A, B, G, H	35%	10%	5%
Treatment Practices	Flow-Through Device - ADS Underground Multichamber Water Quality Unit (WQU)		G, H	72%	10%	9%
	Other Flow-Through Devices	TBA				
	Off-line Deep Sump Catch Basin		J, K, L, M	15%	5%	5%

APPENDIX X

Infiltration Testing Data

Front of Site - Test #1

Height	Constant	Tim	ne	Outflow	Rate (K _{sat})
cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
0						
6.2	105	0.5	0.008333	78120.0	82.4947	32.4782
9.9	105	1	0.016667	62370.0	65.8627	25.9302
13.5	105	1.5	0.025	56700.0	59.8752	23.5729

 Mean
 27.3271

 σ (Std. Dev.)
 3.7674

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 22.3 iph (Test #3)

With factor of safety of two = 11.15 iph

Constant	105 cm^2	
Glover Coefficient:	0.001056 1/cm ²	2

Front of Site - Test #2

	Height	Constant	Tim	ne	Outflow	Rate ((K _{sat})
	cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
	0						
Ī	6.7	105	0.5	0.008333	84420.0	89.1475	35.0974
	11.2	105	1	0.016667	70560.0	74.5114	29.3352
	16.1	105	1.5	0.025	67620.0	71.4067	28.1129

 Mean
 30.8485

 σ (Std. Dev.)
 3.0456

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 22.3 iph (Test #3)

With factor of safety of two = 11.15 iph

Constant	105 cm^2	
Glover Coefficient:	0.001056 1/cm ²	2

Front of Site - Test #3

	Height	Constant	Time		Outflow	Rate (K _{sat})
	cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
	0						
Ī	4.8	105	0.5	0.008333	60480.0	63.8669	25.1444
	8.3	105	1	0.016667	52290.0	55.2182	21.7395
	11.4	105	1.5	0.025	47880.0	50.5613	19.9060

 Mean
 22.2633

 σ (Std. Dev.)
 2.1704

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 22.3 iph (Test #3)

With factor of safety of two = 11.15 iph

Bioretention - Test #1

Height	Constant	Tim	ie	Outflow	Rate (K _{sat})	
cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
0						
2.9	105	0.5	0.008333	36540.0	38.5862	15.1914
5.7	105	1	0.016667	35910.0	37.9210	14.9295
8	105	1.5	0.025	33600.0	35.4816	13.9691
10.65	105	2	0.033333	33547.5	35.4262	13.9473
14.7	105	2.5	0.041667	37044.0	39.1185	15.4010
17.9	105	3	0.05	37590.0	39.6950	15.6280

 Mean
 14.8444

 σ (Std. Dev.)
 0.6611

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 14.8 iph (Test #1)

With factor of safety of two = 7.4 iph

Bioretention - Test #2

Height	Constant	Tim	ne	Outflow	Rate (K _{sat})	
cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
0						
6.8	105	0.5	0.008333	85680.0	90.4781	35.6213
13	105	1	0.016667	81900.0	86.4864	34.0498
17.5	105	1.5	0.025	73500.0	77.6160	30.5575

 Mean
 33.4095

 σ (Std. Dev.)
 2.1163

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 14.8 iph (Test #1)

With factor of safety of two = 7.4 iph

Bioretention - Test #3

	Height	Constant	Tim	ne	Outflow	Rate (K _{sat})	
	cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
	0						
Ī	12.6	105	0.5	0.008333	158760.0	167.6506	66.0042
	25	105	1	0.016667	157500.0	166.3200	65.4803

 Mean
 65.7422

 σ (Std. Dev.)
 0.2619

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 14.8 iph (Test #1)

With factor of safety of two = 7.4 iph

Unit 4 - Test #1

Height	Constant	Tim	ne	Outflow	Rate (K _{sat})	
cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
0						
6.5	105	0.5	0.008333	81900.0	86.4864	34.0498
11.7	105	1	0.016667	73710.0	77.8378	30.6448
15.6	105	1.5	0.025	65520.0	69.1891	27.2398

 Mean
 30.6448

 σ (Std. Dev.)
 2.7802

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 25.4 iph (Test #2)

With factor of safety of two = 12.7 iph

Unit 4 - Test #2

Height	Constant	Tim	ne	Outflow	Rate (Rate (K _{sat})	
cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr	
0							
5.6	105	0.5	0.008333	70560.0	74.5114	29.3352	
9.5	105	1	0.016667	59850.0	63.2016	24.8825	
12.6	105	1.5	0.025	52920.0	55.8835	22.0014	

 Mean
 25.4064

 σ (Std. Dev.)
 3.0168

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 25.4 iph (Test #2)

With factor of safety of two = 12.7 iph

Unit 4 - Test #3

	Height	Constant	Tim	ne	Outflow	Rate (K _{sat})	
	cm	cm ²	Minutes	Hours	cm³/hr	cm/hr	in/hr
	0						
Ī	8.4	105	0.5	0.008333	105840.0	111.7670	44.0028
	13.6	105	1	0.016667	85680.0	90.4781	35.6213
	18.5	105	1.5	0.025	77700.0	82.0512	32.3036

 Mean
 37.3092

 σ (Std. Dev.)
 4.9230

Calculations:

Constant = 20 cm² for one tube, 105 cm² for two tubes (two tubes used)

Hours = Minutes / 60

Outflow = (Height*Constant)/Hours

Ksat = Outflow*Glover Coefficient Lowest Mean Ksat = 25.4 iph (Test #2)

With factor of safety of two = 12.7 iph

Project #: 18134.1

Test Pit #: France - 18134.1

Permeameter Test #: 18134.1

Date: 7/7/24
Location: 635 549

Soil Map Unit Series:

Horizon: B/C (circle one)

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Test hole profile:

Set-Up Calculation

Hole Depth (cm):
Distance From Bottom of Bubble:
Tube to Soil Surface (cm):
Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on") (= 20.0cm²) Both ("2 on") (= 105.0 cm^2)

<-- "B'

Unit

Α	В				D	E	F		
Drop in Water	Outflow Chamber	Clock Time	Elapsed Time		Clapseu fillie		Outflow (Q)	Saturated Hydraulic	
Level				С	(4)	Conductiv	ity (Ksat)		
(cm)	(C.F.)	(hr : min)	(min)	(min/hr	(cm ³ /hr)	(cm/hr)	(in/hr)		
Example:	20	10:17	15	0.25	392	0.4139	0.1629		
Start (0)					-				
					No.				
	1								
	_								
	-								
	+								
					Mann Vact				
					Mean Ksat				

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

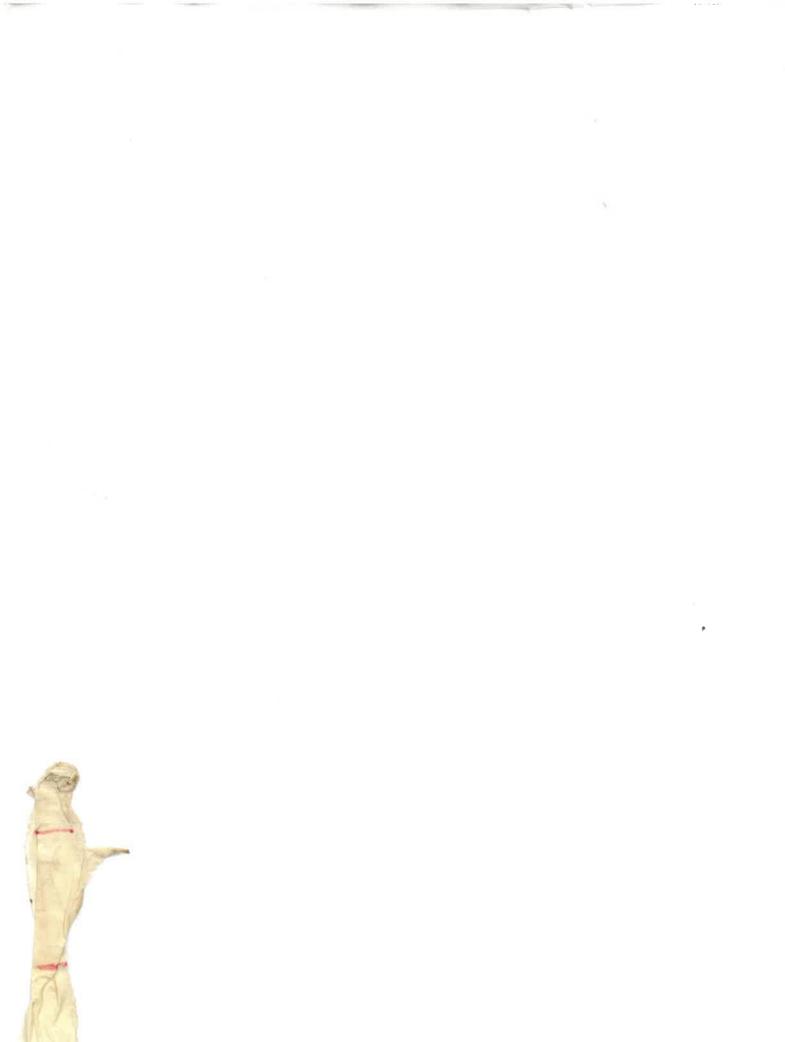
Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr







Project #:

Test Pit #:

From Fig. 1

Permeameter Test #:
Date: 7/7 /1

Location:

635 509

Soil Map Unit Series:

Horizon:

B/C (circle one)

JONES & BEACH ENGINEERS INC.

Test hole profile:

Unit

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6 "

Set-Up Calculation

Hole Depth (cm):

Distance From Bottom of Bubble:

Tube to Soil Surface (cm):

Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on")

 $(= 20.0 cm^2)$

Both ("2 on")

(= 105.0 cm/2)

<-- "B'

Α	В				D	E	F		
Drop In Water	Outflow Chamber	Clock Time	Elapsed Time		Elapsed Time		Outflow (Q)	Saturated Hydraulic	
Level				С		Conductiv	ty (Ksat)		
(cm)	(C.F.)	(hr : min)	(min)	(min/hr)	(cm³/hr)	(cm/hr)	(in/hr)		
Example:	20	10:17	15	0.25	392	0.4139	0.1629		
Start (0)									
					Mean Ksat				

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr

F:\Forms, Apps, Regs\Templates\Amoozemeter\Amoozemeter Data Sheet.xlsx

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Project #: 181341

Test Pit #: 4 F(0x)

Permeameter Test #: 3

Date: 7/2/24

Location: 635 569

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Location: 635 569
Soil Map Unit Series:
Horizon: B / C (circle one)

Set-Up Calculation

Hole Depth (cm):
Distance From Bottom of Bubble:
Tube to Soil Surface (cm):
Desired Water Depth In Hole (cm):
= CHT Tube Setting (cm):

Test hole profile:

Unit

9

1

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on") (= 20.0cm²) Both ("2 on") (= 105.0 cm^2)

<-- "B"

Α	В				D	E	F
Drop In Water	Outflow Chamber	Clock Time	Elapsed Time		Outflow (Q)	Saturated Hydraulic	
Level				С	(4)	Conductiv	ity (Ksat)
(cm)	(C.F.)	(hr : min)	(min)	(min/hr	(cm³/hr)	(cm/hr)	(in/hr)
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)							
					Mean Ksat		

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr





Project #:		18134.1	
Test Pit #:	Biores	ita	
Permeame	ter Test #:,	1	
Date:	7/2/1	4	
Location:	633 8	29	
Soil Map U	nit Series:		
Horizon:	B/C	(circle one)	

ONES& BEACH ENGINEERS INC.

Set-Up Calculation

Test hole profile: Unit

Hole Depth (cm): **Distance From Bottom of Bubble:** Tube to Soil Surface (cm): **Desired Water Depth In Hole (cm):** = CHT Tube Setting (cm):

Outflow Chamber(s) Used (circle one): Associated Conversion Factor:

Small ("1 on") $(= 20.0 cm^2)$

Both ("2 on") (= 105.0 cm^2)

Α	В				D	E	F
Drop In Water	Outflow Chamber	Clock Time	Elapsed Time		Outflow (Q)	Saturated Hydraulic	
Level				С	(4)	Conductiv	ity (Ksat)
(cm)	(C.F.)	(hr : min)	(min)	(min/hr	(cm³/hr)	(cm/hr)	(in/hr)
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)							
							×
						- 31	
					Mean Ksat		-

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr

Project #: Test Pit #:	18134 1 Bio 1886	192			
Permeameter Test #:					
Date:	7/2/1	1			
Location:	635 54	.9			
Soil Map Unit Series:					
Horizon:	B/C	(circle one)			

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Se	t-U	ln i	Cal	CU	lat	io	n
36	L-C	'P'	Cai	Cu	Iat	IU	

Hole Depth (cm):

Distance From Bottom of Bubble:

Tube to Soil Surface (cm):

Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

Test note	profile:
	Unit
	7"
	<u> 9 </u>

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on") (= 20.0cm²) Both ("2 on") (= 105.0 cm^2)

<-- "B

Α	В				D	E	F
Drop In Water Level	Outflow Chamber	Clock Time	Elapsed Time		Outflow (Q)	Saturated Hydraulic Conductiv	ity (Ksat)
(cm)	(C.F.)	(hr : min)	(min)	(min/hr)	(cm³/hr)	(cm/hr)	(in/hr)
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)							
					Mean Ksat		

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr



Project #: Test Pit #: Permeameter Test #: Date: Location:

Soil Map Unit Series:

Horizon: B/C (circle one)

Set-Up Calculation

Hole Depth (cm): **Distance From Bottom of Bubble:** Tube to Soil Surface (cm): Desired Water Depth In Hole (cm): **CHT Tube Setting (cm):**

Test hole profile: Unit

Outflow Chamber(s) Used (circle one): Associated Conversion Factor:

Small ("1 on") $(=20.0cm^2)$

Both ("2 on") $(= 105.0 \text{ cm}^2)$

A	В				D	E	F
Drop In Water	Outflow Chamber	Clock Time	Elapse	d Time	Outflow	Saturated Hydraulic	
Level	ļ			С	(Q)	Conductivi	ity (Ksat)
(cm)	(C.F.)	(hr : min)	(min)	(min/hr)	(cm ³ /hr)	(cm/hr)	(in/hr)
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)					332	0.4133	0.1029
10							
25							
					/lean Ksat		

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from ${\rm cm}^3/{\rm hr}$ to ${\rm cm/hr}$

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr

 $F: \label{lem:final_fi$

Project #:	18134	1
Test Pit #:	Unit	4
Permeamet	er Test #:	
Date:	7/2/20	21
Location:	635 Sa	9
Soil Map Ur	nit Series:	
Horizon:	B/C	(circle one)

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Set-Up Calculation

Hole Depth (cm):
Distance From Bottom of Bubble:
Tube to Soil Surface (cm):
Desired Water Depth In Hole (cm):
= CHT Tube Setting (cm):

Test hole	orofile:
	Unit
	6 "
	<u>//</u> "

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on") (= 20.0cm²) Both ("2 on") (= 105.0 cm^2)

<-- "B'

Α	В				D	E	F
Drop In Water	Outflow Chamber	Clock Time	Elapsed Time		Outflow (Q)	Saturated Hydraulic	
Level				С	(4)	Conductiv	ity (Ksat)
(cm)	(C.F.)	(hr : min)	(min)	(min/hr	(cm³/hr)	(cm/hr)	(in/hr)
Example:	20	10:17	15	0.25	392	0.4139	0.1629
Start (0)							
					Mean Ksat		

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr



Project #: Test Pit #: Permeameter Test #: Date: Location: Soil Map Unit Series:	JONES& BEACTENGINEERS IN
N	
Horizon: B/C (circle one)	Test hole profile:
	Unit
Set-Up Calculation	
Hole Depth (cm):	10
Distance From Bottom of Bubble:	<u>*</u>
Tube to Soil Surface (cm):	

Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

Small ("1 on") Both ("2 on") Outflow Chamber(s) Used (circle one): $(=20.0cm^2)$ (= 105.0 cm²) Associated Conversion Factor:

Unit

Α	В				D	E	F	
Drop In Water Level	Outflow Chamber	Clock Time	Elapse	Hyd		Saturated Hydraulic Conductivi		
(cm)	(C.F.)	(hr : min)	(min)	(min/hr)	(cm³/hr)	(cm/hr) (in/hr		
Example:	20	10:17	15	0.25	392	0.4139	0.1629	
Start (0)								
	A STATE OF THE PARTY OF THE PAR				Mean Ksat			

Calculation Formulas:

D = (AxB)/C

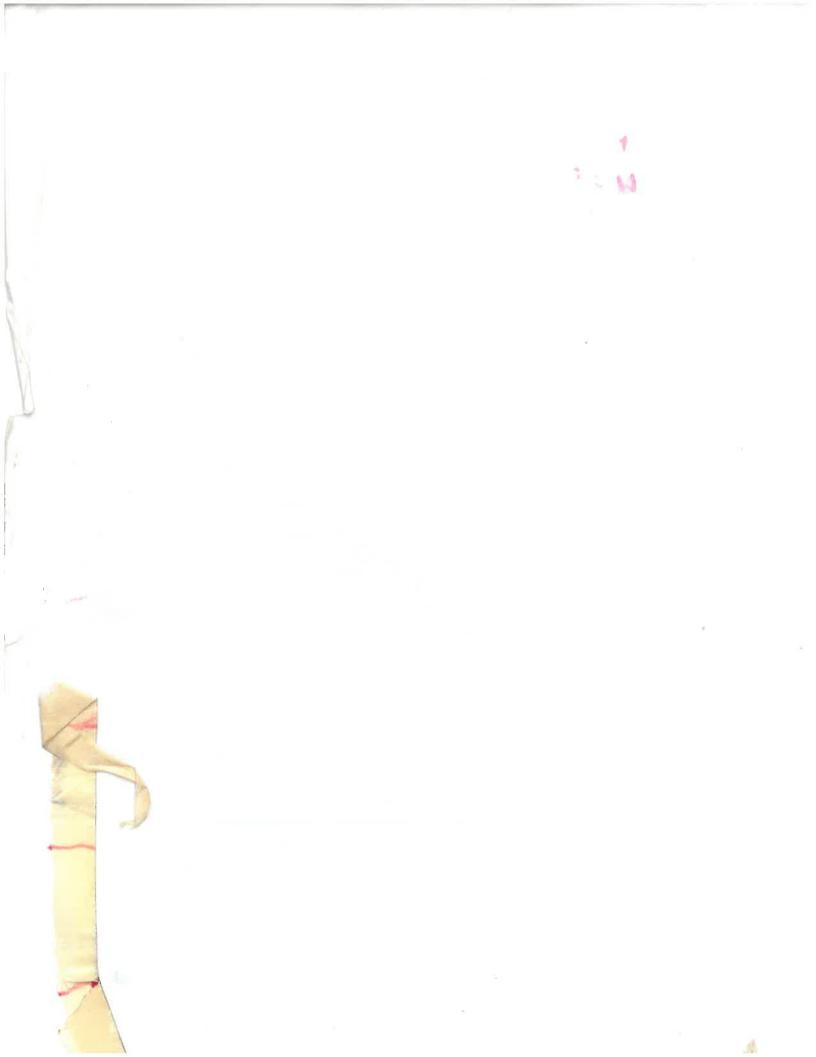
 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr



Project #:	18134.1
Test Pit #:	1/1/1 4
Permeamete	er Test #: 3
Date:	7/2/29
Location:	635 509

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Soil Map Unit Series:

Horizon: B / C (circle one)

Test hole profile:
Unit

Set-Up Calculation

Hole Depth (cm):
Distance From Bottom of Bubble:
Tube to Soil Surface (cm):
Desired Water Depth In Hole (cm):

= CHT Tube Setting (cm):

Both ("2 on") (= 105.0 cm^2)

<-- "B"

Outflow Chamber(s) Used (circle one) :
Associated Conversion Factor:

Small ("1 on") (= 20.0cm²)

Mean Ksat

Α	В				D	E	F	
Drop In Water Level	Outflow Chamber	Clock Time	Elapsed Time		Outflow (Q)	Saturated Hydraulic Conductiv		
(cm)	(C.F.)	(hr : min)	(min)	C (min/hr)	(cm³/hr)	(cm/hr) (in/hr)		
Example:	20	10:17	15	-	392	0.4139	0.1629	
Start (0)								

Calculation Formulas:

D = (AxB)/C

 $E = D \times 0.001056$

F = E / 2.54

Notes:

Mulitply "D" by 0.001056 for a conversion from cm³/hr to cm/hr

Multiply "E" by 0.393701 for conversion fro cm/hr to in/hr



APPENDIX XI

Stormwater Operations and Maintenance Manual



85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

STORMWATER MANAGEMENT OPERATIONS AND MAINTENANCE MANUAL

Luster Cluster 635 Sagamore Ave. Portsmouth, NH 03801 Tax Map 222, Lot 19

Prepared for:

635 Sagamore Development LLC 3612 Lafayette Rd., Dept 4 Portsmouth, NH 03801

Prepared by:

Jones & Beach Engineers, Inc.
85 Portsmouth Avenue
P.O. Box 219
Stratham, NH 03885
(603) 772-4746
March 18, 2024
Revised April 15, 2024
Revised August 8, 2024
JBE Project No. 18134.1

Inspection and Maintenance of Facilities and Property

A. Maintenance of Common Facilities or Property

1. The Condominium Association, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Association, future owners and assigns shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form and shall submit an Operations and Maintenance report on a yearly basis to the Portsmouth Planning Department by December 31st.

B. General Inspection and Maintenance Requirements

- 1. Permanent stormwater and sediment and erosion control facilities to be maintained on the site include, but are not limited to, the following:
 - a. Roadway and driveways
 - b. Vegetation and landscaping
 - c. Sediment Forebay
 - d. Bioretention system
 - e. Catch Basins & Yard Drains
 - f. Stone Drip Edges
 - g. Stone Underneath Decks
 - h. Culverts
 - i. Rip-Rap Outlet Protection Aprons
 - i. Swale
- 2. Maintenance of permanent measures shall follow the following schedule:
 - a. Normal winter roadway maintenance including plowing and snow removal. Road sweeping at the end of every winter, preferably before the start of the spring rain season.
 - b. **Annual inspection** of the site for erosion, destabilization, settling, and sloughing. Any needed repairs are to be conducted immediately. **Annual inspection** of site's vegetation and landscaping. Any areas that are bare shall be reseeded and mulched with hay or, if the case is extreme, loamed and seeded or sodded to ensure adequate vegetative cover. Landscape specimens shall be replaced in kind, if they are found to be dead or dying.
 - c. Cleaning Criteria for all Sedimentation Forebays: Sediment shall be removed from the sedimentation chamber (forebay) when it accumulates to a depth of more than 12 inches (30 cm) or 10 percent of the pretreatment volume. The sedimentation forebay shall be cleaned of vegetation if persistent standing water and wetland vegetation becomes dominant. The cleaning interval is once every year. A dry sedimentation forebay is the optimal condition while in practice this condition is rarely achieved. The sedimentation



chamber, forebay, and treatment cell outlet devices shall be cleaned when drawdown times exceed 60 to 72 hours. Materials can be removed with heavy construction equipment; however, this equipment shall not track on the wetland surface. Revegetate disturbed areas as necessary. Removed sediments shall be dewatered (if necessary) and disposed of in an acceptable manner.

d. Bioretention Systems:

- Visually inspect monthly and repair erosion. Use small stones to stabilize erosion along drainage paths.
- Check the pH once a year if grass is not surviving. Apply an alkaline product, such as limestone, if needed.
- Re-seed any bare areas by hand as needed.
- Immediately after the completion of cell construction, water grass for 14 consecutive days unless there is sufficient natural rainfall.
- Once a month (more frequently in the summer), the land owner or Association shall visually inspect vegetation for disease or pest problems and treat as required.
- During times of extended drought, look for physical features of stress. Water in the early morning as needed.
- Weed regularly, if needed.
- After rainstorms, inspect the cell and make sure that drainage paths are clear and that ponding water dissipates over 4-6 hours. (Water may pond for longer times during the winter and early spring.)
- Twice annually, inspect the outlet control structures to ensure that they are not clogged and correct any clogging found as needed.
- Any debris and sediment accumulations shall be removed from the outlet structures, overflow risers, and emergency spillways and disposed of properly.
- Inspect outlet structure for deterioration and or clogging.
- If erosion is evident on the berm or emergency spillway, stabilize the affected area by seeding. Trees must not be allowed to grow in these areas.
- KEEP IN MIND, THE BIORETENTION CELL IS NOT A POND. IT SHALL NOT PROVIDE A BREEDING GROUND FOR MOSQUITOES. MOSQUITOES NEED AT LEAST FOUR (4) DAYS OF STANDING WATER TO DEVELOP AS LARVA.
- e. Annual inspection of catch basins and yard drains to determine if they need to be cleaned. Catch basins and yard drains are to be cleaned if the depth of deposits is greater than one-half the depth from the basin bottom to the invert of the lowest pipe or opening into or out of the basin. If a catch basin or yard drain significantly exceeds the one-half depth standard during the inspection, then it shall be cleaned more frequently. If woody debris or trash accumulates in the catch basin or yard drain, then it shall be cleaned on a weekly basis. The catch basin or yard drain can be cleaned either manually or by specially designed equipment including, but not limited to, bucket loaders and vacuum pumps. Before any materials can be disposed, it is necessary to perform a detailed chemical analysis to determine if the materials meet the EPA criteria for hazardous waste. This will help determine



how the materials shall be stored, treated, and disposed. Grease hoods are to be wiped clean and the rags disposed of properly. Debris obscuring the grate inlet shall also be removed.

f. Stone drip edges:

Units 3 & 4 feature stone drip edges to collect roof runoff into a pipe in order to direct it into the stone areas underneath the unit decks. These practices shall be lined and are not intended for infiltration. The following course of action will help assure that the roof drip edges are maintained to preserve its effectiveness.

In the spring and fall, visually inspect the area around the edges and repair any erosion. Use small stones to stabilize erosion along drainage paths. Inspect stone area to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation shall not be allowed to become established in stone areas, and/or any debris removed from the void spaces between the stones

g. Stone underneath decks:

Units 3 and 4 feature stone areas underneath their associated rear decks for infiltration of roof runoff. The following guidelines will help ensure proper functioning of the system.

In the spring and fall, visually inspect the area around the edges and repair any erosion. Use small stones to stabilize erosion along drainage paths. Inspect stone area to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation shall not be allowed to become established in stone areas, and/or any debris removed from the void spaces between the stones.

- h. **Inspection** of culvert inlets and outlets at least **once per month** during the rainy season (March to November). Any debris is to be removed and disposed of properly.
 - i. Rock riprap shall be **inspected annually** in order to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation must not be allowed to become established in riprap areas, and/or any debris removed from the void spaces between the rocks. If the riprap is adjacent to a stream or other waterbody, the water shall be kept clear of obstructions, debris, and sediment deposits



j. Swale – There is a swale on the north side of Unit 3, leading to the bioretention pond. Inspect swale annually for erosion, sediment accumulation, vegetation loss, and presence of invasive species. Perform periodic mowing; frequency depends on location and type of grass. Remove debris and accumulated sediment, based on inspection. Repair eroded areas, remove invasive species and dead vegetation, and reseed as warranted by inspection

See attached sample forms as a guideline.

Any inquiries in regards to the design, function, and/or maintenance of any one of the above-mentioned facilities or tasks shall be directed to the project engineer:

Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885

T#: (603) 772-4746 F#: (603) 772-0227

Commitment to maintenance requirements

I agree to complete and/or observe all of the required schedules as outlined above.	maintenance practices and their respective
Signature	-
Print Name	_
	_
Title	
Date	_

Annual Operations and Maintenance Report

The Condominium Association, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Association, future owners and assigns shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form and shall submit an Operations and Maintenance report on a yearly basis to the Portsmouth Planning Department by December 31st.

Construction Activity	Date of Inspection	Who Inspected	Findings of Inspector
Roadway and Driveways			
Vegetation and Landscaping			
Sediment Forebay			
Bioretention Pond			
Catch Basins & Yard Drains			



Unit 3 Stone Drip Edge		
H : 40: B : E1		
Unit 4 Stone Drip Edge		
Stone underneath unit 3		
deck		
Stone underneath unit 4		
deck		
0.1		
Culverts		
Rip Rap Outlet Protection		
Swale	 	



Other (please note):			

Regular Inspection and Maintenance Guidance for Bioretention Systems / Tree Filters

Maintenance of bioretention systems and tree filters can typically be performed as part of standard landscaping. Regular inspection and maintenance is critical to the effective operation of bioretention systems and tree filters to insure they remain clear of leaves and debris and free draining. This page provides guidance on maintenance activities that are typically required for these systems, along with the suggested frequency for each activity. Individual systems may have more, or less, frequent maintenance needs, depending on a variety of factors including the occurrence of large storm events, overly wet or dry (I.E., drought), regional hydrologic conditions, and the upstream land use.

ACTIVITIES

The most common maintenance activity is the removal of leaves from the system and bypass structure. Visual inspections are routine for system maintenance. This includes looking for standing water, accumulated leaves, holes in the soil media, signs of plant distress, and debris and sediment accumulation in the system. Mulch and/or vegetation coverage is integral to the performance of the system, including infiltration rate and nutrient uptake. Vegetation care is important to system productivity and health.

ACTIVITY	FREQUENCY	
A record should be kept of the time to drain for the system completely after a storm event. The system should drain completely within 72 hours.		
Check to insure the filter surface remains well draining after storm event. Remedy: If filter bed is clogged, draining poorly, or standing water covers more than 15% of the surface 48 hours after a precipitation event, then remove top few inches of discolored material. Till or rake remaining material as needed.	After every major storm in the first few months, then biannually.	
Check inlets and outlets for leaves and debris. Remedy: Rake in and around the system to clear it of debris. Also, clear the inlet and overflow if obstructed.		
Check for animal burrows and short circuiting in the system Remedy: Soil erosion from short circuiting or animal boroughs should be repaired when they occur. The holes should be filled and lightly compacted.	Quarterly initially, biannually, frequency adjusted as needed after 3 inspections	
Check to insure the filter bed does not contain more than 2 inches accumulated material Remedy: Remove sediment as necessary. If 2 inches or more of filter bed has been removed, replace media with either mulch or a (50% sand, 20% woodchips, 20% compost, 10% soil) mixture.		
During extended periods without rainfall, inspect plants for signs of distress. Remedy: Plants should be watered until established (typical only for first few months) or as needed thereafter.		
Inspect inlets and outlets to ensure good condition and no evidence of deterioration. Check to see if high-flow bypass is functioning. Remedy: Repair or replace any damaged structural parts, inlets, outlets, sidewalls.	Annually	
Check for robust vegetation coverage throughout the system. Remedy : If at least 50% vegetation coverage is not established after 2 years, reinforcement planting should be performed.		
Check for dead or dying plants, and general long term plant health. Remedy : This vegetation should be cut and removed from the system. If woody vegetation is present, care should be taken to remove dead or decaying plant Material. Separation of Herbaceous vegetation rootstock should occur when overcrowding is observed.	As needed	

1/15/2011, University of New Hampshire Stormwater Center

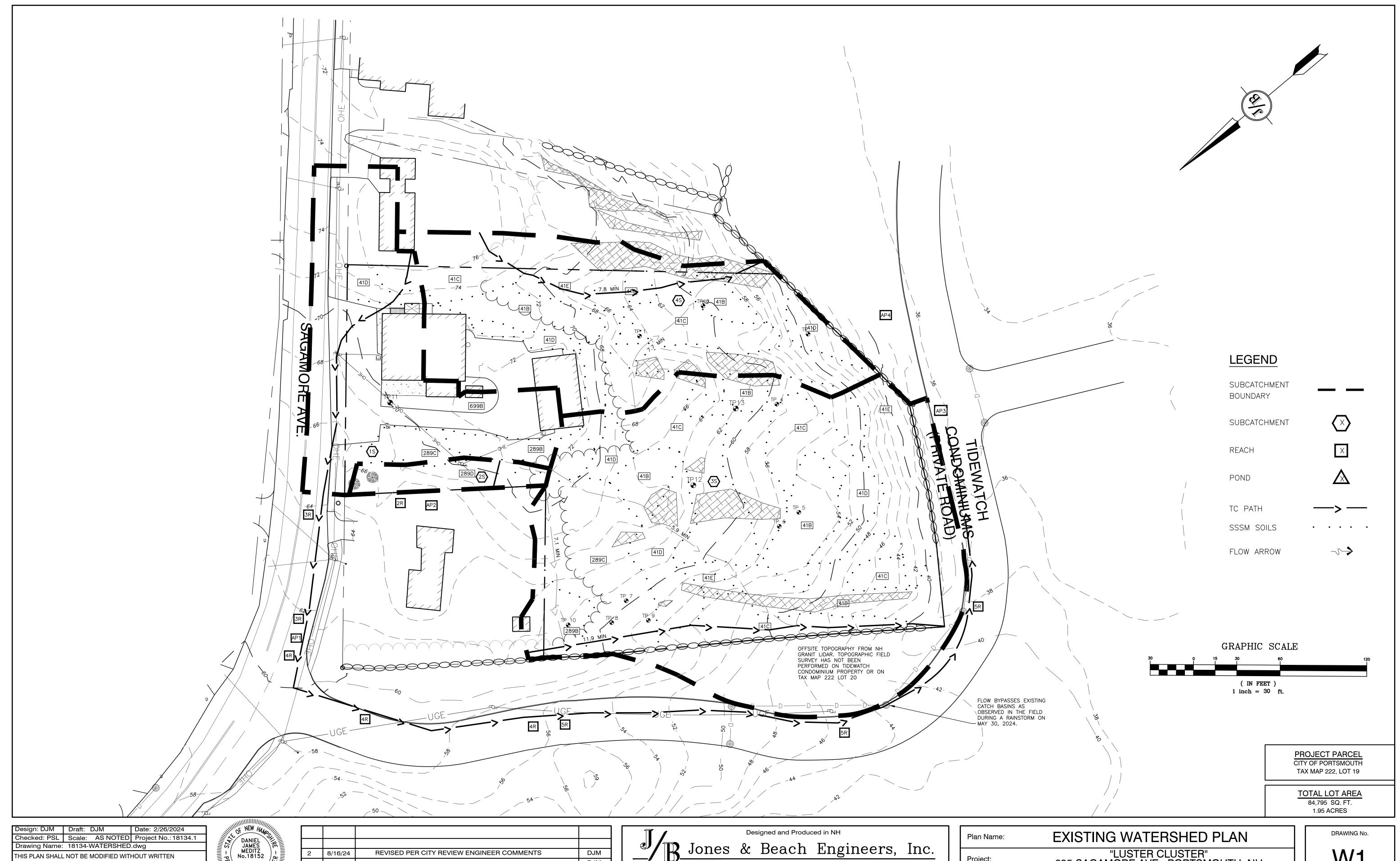
CHECKLIST FOR INSPECTION OF BIORETENTION SYSTEM / TREE FILTERS Location: Inspector: Date: Time: Site Conditions: Date Since Last Rain Event: Inspection Items Satisfactory (S) or Unsatisfactory (U) Comments/Corrective Action

spection Items Satisfactory (S) or Unsatisfactory (U)		Comments/Corrective Action	
1. Initial Inspection After Planting and Mulching			
Plants are stable, roots not exposed	S	U]
Surface is at design level, typically 4" below overpass	S	U	
Overflow bypass / inlet (if available) is functional	s	U	<u></u>
2. Debris Cleanup (2 times a year minimum, Spring & Fall)			
Litter, leaves, and dead vegetation removed from the system	S	U	7
Prune perennial vegetation	S	U	T
3. Standing Water (1 time a year, After large storm events)			
No evidence of standing water after 72 hours	S	U	
4. Short Circuiting & Erosion (1 time a year, After large storn	n events)		
No evidence of animal burrows or other holes	S	U	
No evidence of erosion	s	U	
5. Drought Conditions (As needed)			
Water plants as needed	S	U]
Dead or dying plants			
6. Overflow Bypass / Inlet Inspection (1 time a year, After lar	ge storm eve	ents)	
No evidence of blockage or accumulated leaves	S	U	
Good condition, no need for repair	S	U	
7. Vegetation Coverage (once a year)			
50% coverage established throughout system by first year	s	U	
Robust coverage by year 2 or later	s	U	
8. Mulch Depth (if applicable)(once every 2 years)			
Mulch at original design depth after tilling or replacement	s	U	
9. Vegetation Health (once every 3 years)			
Dead or decaying plants removed from the system	s	U	
10. Tree Pruning (once every 3 years)			
Prune dead, diseased, or crossing branches	S	U	
Corrective Action Needed			Due Date
1.			
2.			
3.			

1/15/2011, University of New Hampshire Stormwater Center

APPENDIX XII

Pre- and Post-Construction Watershed Plans



PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



2	8/16/24	REVISED PER CITY REVIEW ENGINEER COMMENTS	DJM
1	4/19/24	REVISED PER TAC COMMENTS	DJM
0	3/8/24	ISSUED FOR REVIEW	DJM
REV.	DATE	REVISION	BY

85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885

Civil Engineering Services
E-MAIL: JBE@3 603-772-4746

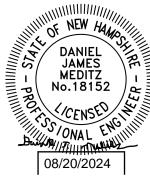
E-MAIL: JBE@JONESANDBEACH.COM

"LUSTER CLUSTER" 635 SAGAMORE AVE., PORTSMOUTH, NH Project: 635 SAGAMORE DEVELOPMENT LLC
Owner of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158 SHEET 1 OF 2 JBE PROJECT NO. 18134.1



Design: DJM Draft: DJM Date: 2/26/2024
Checked: PSL Scale: AS NOTED Project No.: 18134.1
Drawing Name: 18134-WATERSHED.dwg
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REV.	DATE	REVISION	BY

Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885

Civil Engineering Services

E-MAIL: JBE@JONESANDBEACH.COM

	Plan Name:	PROPOSED WATERSHED PLAN
	Project:	"LUSTER CLUSTER" 635 SAGAMORE AVE., PORTSMOUTH, NH
	Owner of Record	635 SAGAMORE DEVELOPMENT LLC d: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

DRAWING No.

W2

SHEET 2 OF 2

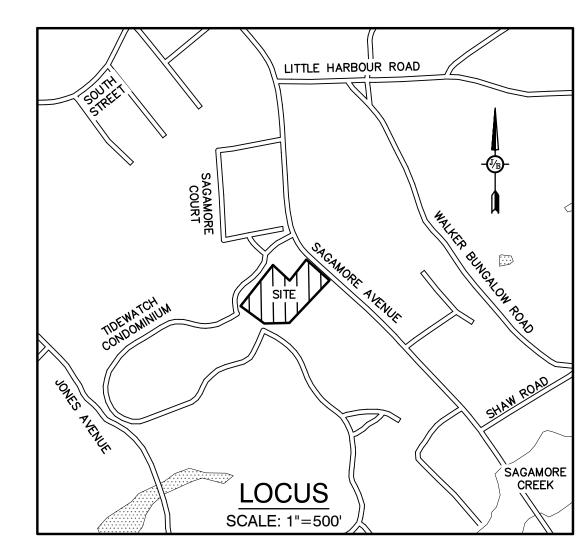
JBE PROJECT NO. 18134.1

GENERAL LEGEND **EASEMENT** MAJOR CONTOUR MINOR CONTOUR EDGE OF PAVEMENT VERTICAL GRANITE CURB UNDERDRAIN THRUST BLOCK IRON PIPE/IRON ROD DRILL HOLE IRON ROD/DRILL HOLE STONE/GRANITE BOUND 100x0 SPOT GRADE x 100.00 PAVEMENT SPOT GRADE CURB SPOT GRADE BENCHMARK (TBM) DOUBLE POST SIGN SINGLE POST SIGN TEST PIT TREES AND BUSHES UTILITY POLE DRAIN MANHOLE SEWER MANHOLE HYDRANT WATER GATE VALVE WATER SHUT OFF REDUCER SINGLE GRATE CATCH BASIN TRANSFORMER CULVERT W/FLARED END SECTION CULVERT W/STRAIGHT HEADWALL STONE CHECK DAM DRAINAGE FLOW DIRECTION PAVEMENT HATCH STABILIZED CONSTRUCTION **ENTRANCE** CONCRETE SNOW STORAGE

RETAINING WALL

SINGLE FAMILY CONDOMINIUM "LUSTER CLUSTER" TAX MAP 222, LOT 19 635 SAGAMORE AVE., PORTSMOUTH, NH





CIVIL ENGINEER / SURVEYOR

JONES & BEACH ENGINEERS, INC. 85 PORTSMOUTH AVENUE PO BOX 219 STRATHAM, NH 03885 (603) 772-4746 CONTACT: JOSEPH CORONATI EMAIL: JCORONATI@JONESANDBEACH.COM

TRAFFIC ENGINEER

STEPHEN G. PERNAW & COMPANY, INC. P.O. BOX 1721 CONCORD, NH 03302 (603) 731-8500 CONTACT: STEPHEN PERNAW

SOILS CONSULTANT

GOVE ENVIRONMENTAL SERVICES, INC. 8 CONTINENTAL DRIVE, BLDG 2, UNIT H EXETER, NH 03833-7507 (603) 418-7260 CONTACT: JAMES GOVE EMAIL: JGOVE@GESINC.BIZ

LANDSCAPE DESIGNER

LM LAND DESIGN, LLC 11 SOUTH ROAD BRENTWOOD, NH 03833 (603) 770-7728 CONTACT: LISE MCNAUGHTON

WATER

CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS WATER DIVISION 680 PEVERLY HILL ROAD PORTSMOUTH, NH 03801 (603) 427-1530

SEWER

Stratham, NH 03885

CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS **SEWER DIVISION** 680 PEVERLY HILL ROAD PORTSMOUTH, NH 03801 (603) 766-1421

LIGHTING DESIGN

EXPOSURE LIGHTING 501 ISLINGTON STREET, UNIT 1A PORTSMOUTH, NH 03801 **CONTACT: KEN SWEENEY**

EVERSOURCE 1700 LAFAYETTE ROAD PORTSMOUTH, NH 03801 (800) 662-7764

TELEPHONE

CONSOLIDATED COMMUNICATIONS 1575 GREENLAND ROAD GREENLAND, NH 03840 (800) 427-5525

CABLE TV

E-MAIL: JBE@JONESANDBEACH.COM

COMCAST COMMUNICATION CORPORATION 334-B CALEF HIGHWAY EPPING, NH 03042-2325 (603) 679-5695

SHEET INDEX

COVER SHEET

EXISTING CONDITIONS PLAN

DEMOLITION PLAN

SITE PLAN

CONDOMINIUM SITE PLAN

GRADING AND DRAINAGE PLAN

UTILITY PLAN

LIGHTING PLAN

LANDSCAPE PLAN

DRIVEWAY PLAN AND PROFILE

SEWER PLAN AND PROFILE

HIGHWAY ACCESS PLAN

TRUCK TURNING PLAN

DETAIL SHEET D1-D5

EROSION AND SEDIMENT CONTROL DETAILS

ARCHITECTURAL PLANS

PROJECT PARCEL CITY OF PORTSMOUTH TAX MAP 222, LOT 19

TOTAL LOT AREA 84,795 SQ. FT.

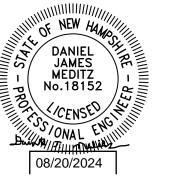
1.95 ACRES

CITY OF PORTSMOUTH PLANNING BOARD

CHAIRPERSON

DATE

Design: DJM Draft: KDR Date: 2/26/2024 Checked: JAC | Scale: AS NOTED | Project No.: 18134.1 Drawing Name: 18134.1-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



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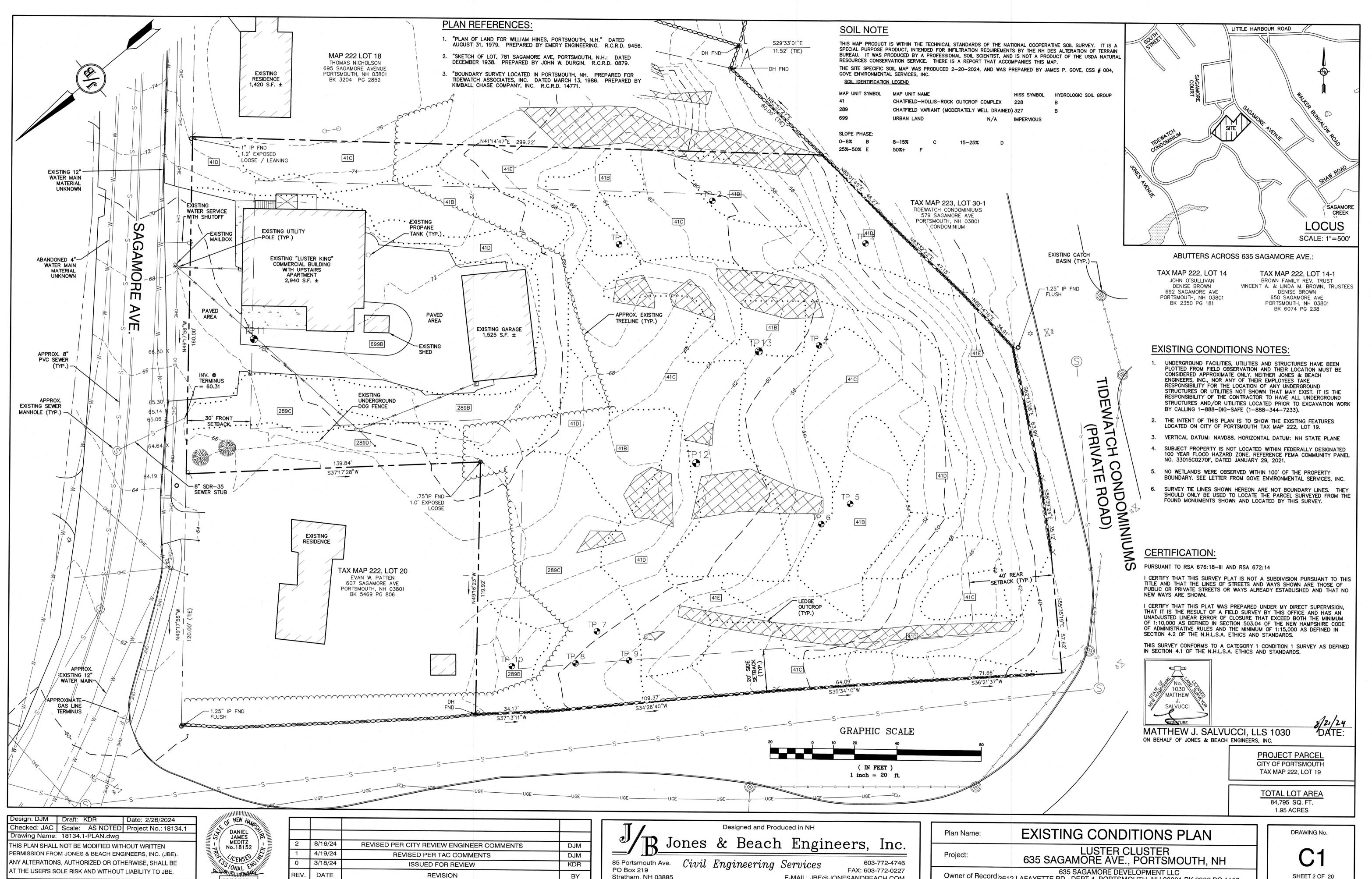
Designed and Produced in NH Jones & Beach Engineers, Inc. 603-772-4746 85 Portsmouth Ave. Civil Engineering Services PO Box 219

COVER SHEET Plan Name: LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH Project:

Owner of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

635 SAGAMORE DEVELOPMENT LLC

DRAWING No. JBE PROJECT NO. 18134.1



PO Box 219

Stratham, NH 03885

BY

FAX: 603-772-0227

E-MAIL: JBE@JONESANDBEACH.COM

AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE

REV. DATE

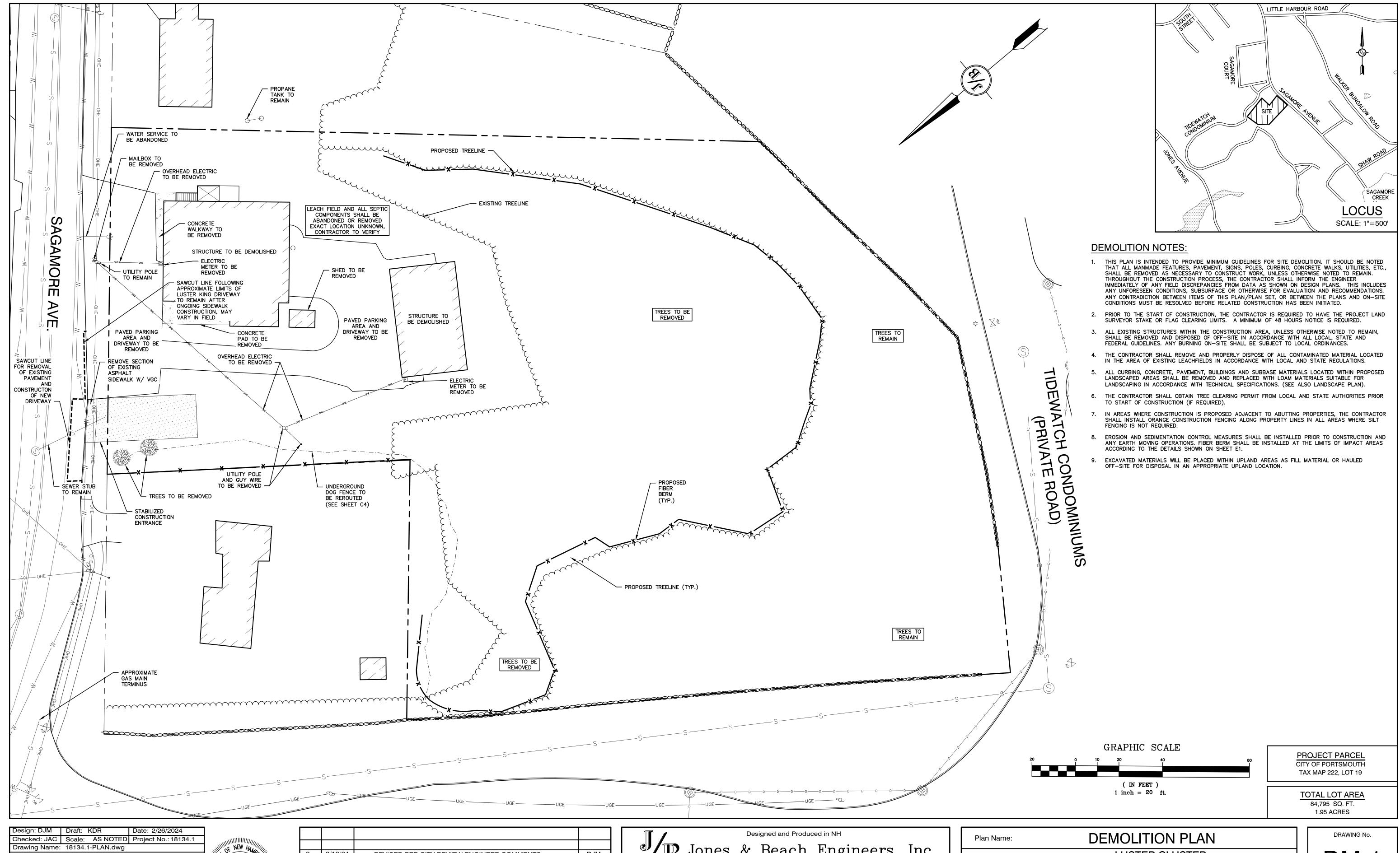
08/20/2024

REVISION

SHEET 2 OF 20 JBE PROJECT NO. 18134.1

635 SAGAMORE DEVELOPMENT LLC

Owner of Record:3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158



DANIEL JAMES MEDITZ No.18152

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REV.	DATE	REVISION	BY

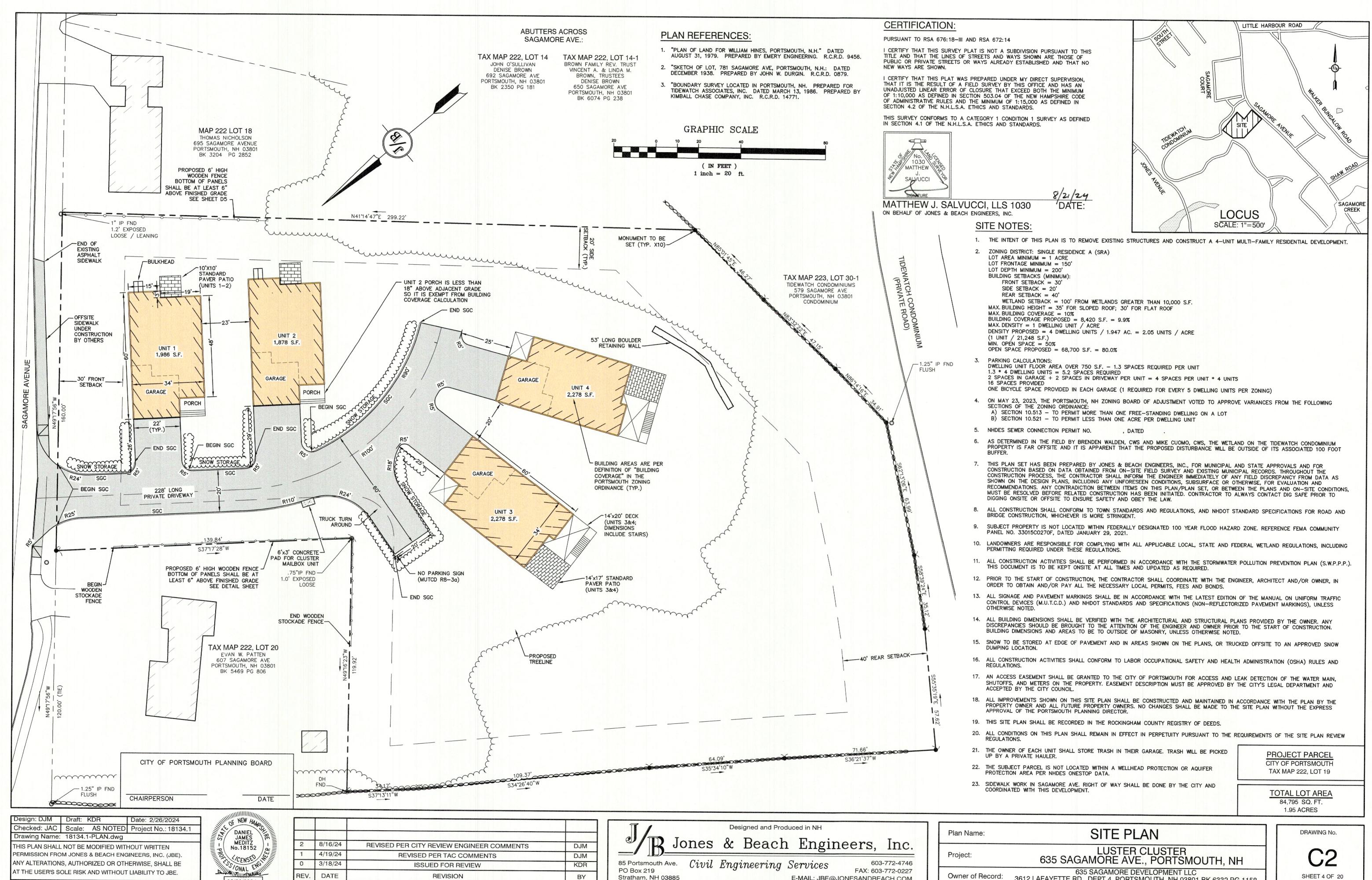
Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services PO Box 219 E-MAIL: JBE@JONESANDBEACH.COM Stratham, NH 03885

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Stratham, NH 03885

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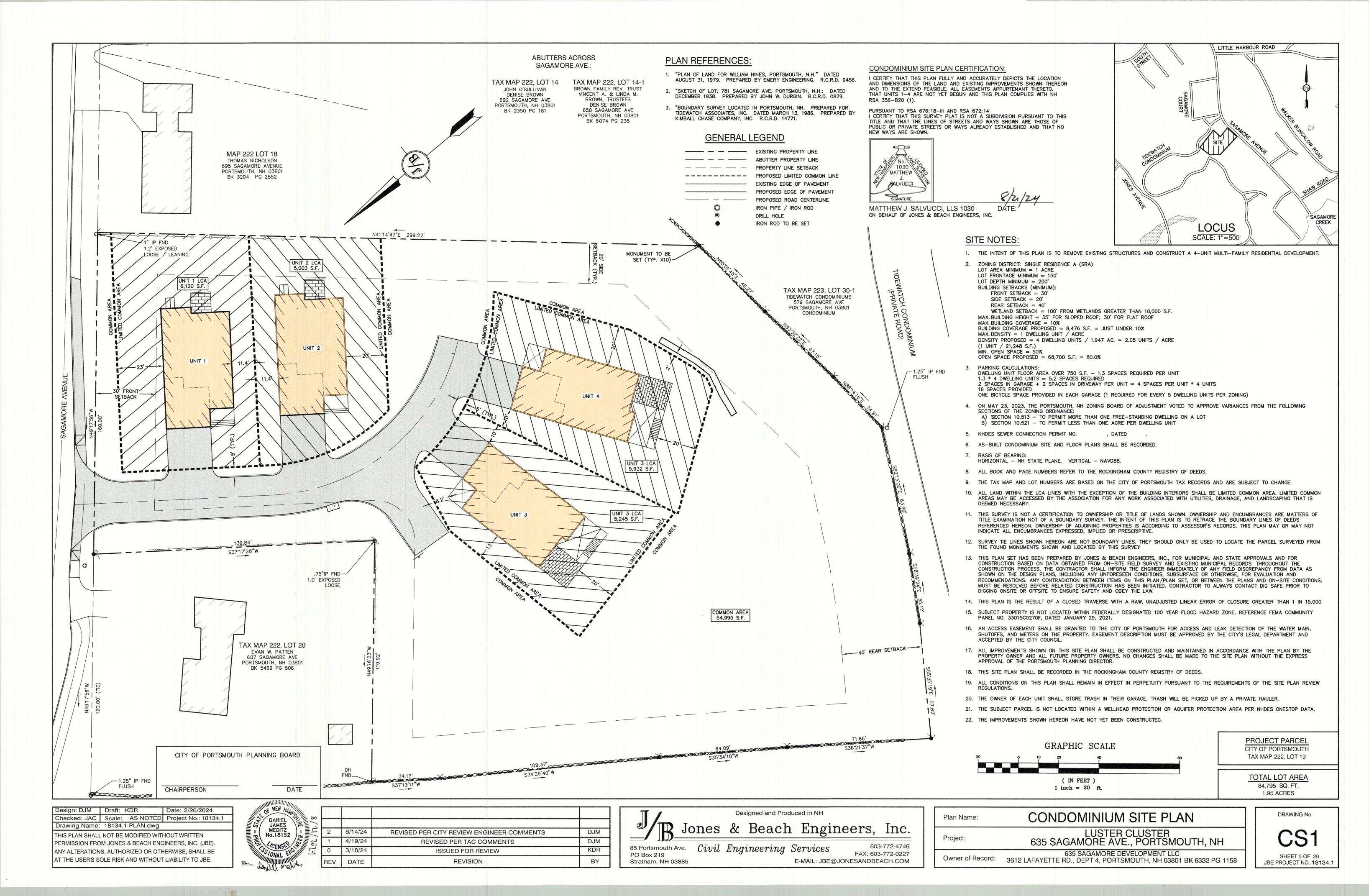
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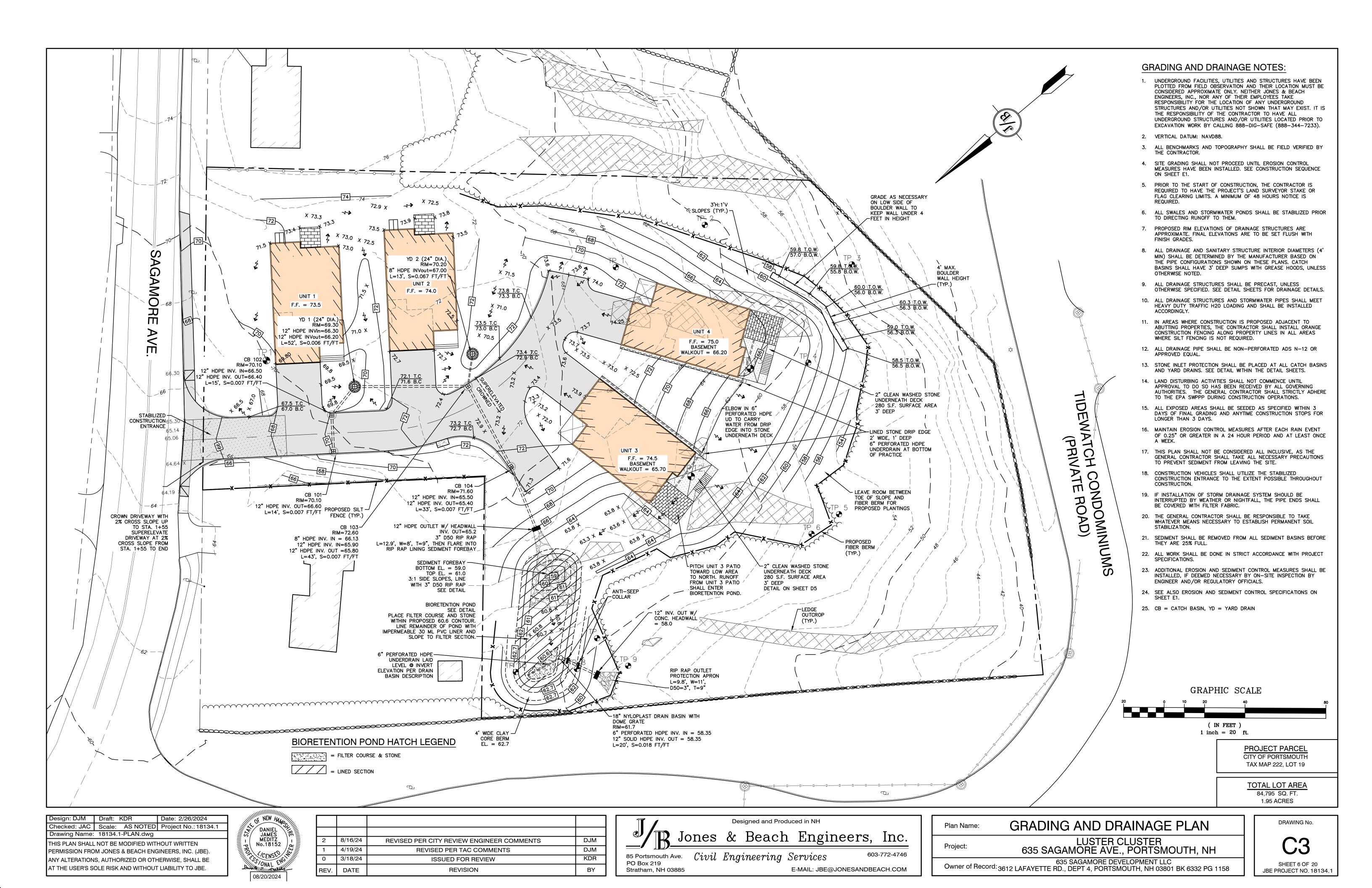
08/20/2024

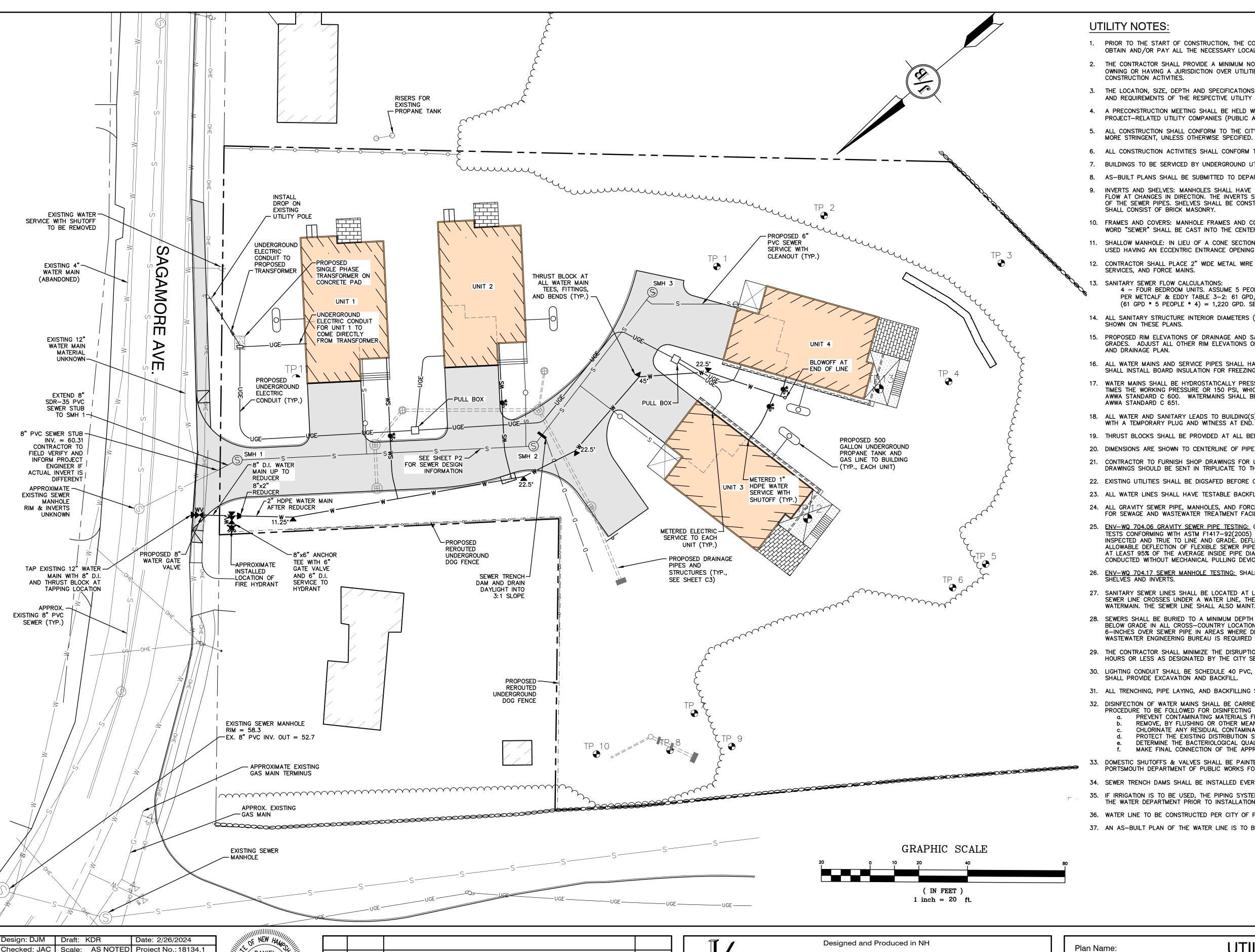
REVISION

SHEET 4 OF 20 JBE PROJECT NO. 18134.

3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158







UTILITY NOTES:

- PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR SHALL COORDINATE WITH THE ENGINEER, ARCHITECT AND/OR OWNER, IN ORDER TO OBTAIN AND/OR PAY ALL THE NECESSARY LOCAL PERMITS, CONNECTION FEES AND BONDS.
- 2. THE CONTRACTOR SHALL PROVIDE A MINIMUM NOTICE OF FOURTEEN (14) DAYS TO ALL CORPORATIONS, COMPANIES AND/OR LOCAL AUTHORITIES OWNING OR HAVING A JURISDICTION OVER UTILITIES RUNNING TO, THROUGH OR ACROSS PROJECT AREAS PRIOR TO DEMOLITION AND/OR
- 3. THE LOCATION, SIZE, DEPTH AND SPECIFICATIONS FOR CONSTRUCTION OF PROPOSED PRIVATE UTILITY SERVICES SHALL BE TO THE STANDARDS AND REQUIREMENTS OF THE RESPECTIVE UTILITY COMPANY (ELECTRIC, TELEPHONE, CABLE TELEVISION, WATER, AND SEWER).
- 4. A PRECONSTRUCTION MEETING SHALL BE HELD WITH THE OWNER, ENGINEER, ARCHITECT, CONTRACTOR, LOCAL OFFICIALS, AND ALL PROJECT-RELATED UTILITY COMPANIES (PUBLIC AND PRIVATE) PRIOR TO START OF CONSTRUCTION.
- 5. ALL CONSTRUCTION SHALL CONFORM TO THE CITY STANDARDS AND REGULATIONS, AND NHDES STANDARDS AND SPECIFICATIONS, WHICHEVER ARE
- 6. ALL CONSTRUCTION ACTIVITIES SHALL CONFORM TO LABOR OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA) RULES AND REGULATIONS
- 7. BUILDINGS TO BE SERVICED BY UNDERGROUND UTILITIES UNLESS OTHERWISE NOTED.
- 8. AS-BUILT PLANS SHALL BE SUBMITTED TO DEPARTMENT OF PUBLIC WORKS.
- 9. INVERTS AND SHELVES: MANHOLES SHALL HAVE A BRICK PAVED SHELF AND INVERT, CONSTRUCTED TO CONFORM TO THE SIZE OF PIPE AND FLOW AT CHANGES IN DIRECTION. THE INVERTS SHALL BE LAID OUT IN CURVES OF THE LONGEST RADIUS POSSIBLE TANGENT TO THE CENTER LIN OF THE SEWER PIPES. SHELVES SHALL BE CONSTRUCTED TO THE ELEVATION OF THE THROUGH CHANNEL UNDERLAYMENT OF INVERT, AND SHELF SHALL CONSIST OF BRICK MASONRY.
- 10. FRAMES AND COVERS: MANHOLE FRAMES AND COVERS SHALL BE OF HEAVY DUTY DESIGN AND PROVIDE A 30 INCH DIA, CLEAR OPENING. THE WORD "SEWER" SHALL BE CAST INTO THE CENTER OF THE UPPER FACE OF EACH COVER WITH RAISED, 3" LETTERS.
- 11. SHALLOW MANHOLE: IN LIEU OF A CONE SECTION, WHEN MANHOLE DEPTH IS LESS THAN 6 FEET, A REINFORCED CONCRETE SLAB COVER MAY BE USED HAVING AN ECCENTRIC ENTRANCE OPENING AND CAPABLE OF SUPPORTING H20 LOADS. (THIS APPLIES TO SMH 1)
- 12. CONTRACTOR SHALL PLACE 2" WIDE METAL WIRE IMPREGNATED RED PLASTIC WARNING TAPE OVER ENTIRE LENGTH OF ALL GRAVITY SEWERS, SERVICES, AND FORCE MAINS.
- SANITARY SEWER FLOW CALCULATIONS:
 - 4 FOUR BEDROOM UNITS. ASSUME 5 PEOPLE IN 4-BEDROOM UNITS. PER METCALF & EDDY TABLE 3-2: 61 GPD/PERSON IN 5 PERSON HOUSE
 - (61 GPD * 5 PEOPLE * 4) = 1,220 GPD. SEE SHEET 2 FOR BEDROOM NUMBER DESIGNATION.
- 14. ALL SANITARY STRUCTURE INTERIOR DIAMETERS (4' MIN) SHALL BE DETERMINED BY THE MANUFACTURER BASED ON THE PIPE CONFIGURATIONS
- 15. PROPOSED RIM ELEVATIONS OF DRAINAGE AND SANITARY MANHOLES ARE APPROXIMATE. FINAL ELEVATIONS ARE TO BE SET FLUSH WITH FINISH GRADES. ADJUST ALL OTHER RIM ELEVATIONS OF MANHOLES, WATER GATES, AND OTHER UTILITIES TO FINISH GRADE AS SHOWN ON THE GRADING
- 16. ALL WATER MAINS AND SERVICE PIPES SHALL HAVE A MINIMUM 12" VERTICAL AND 24" HORIZONTAL SEPARATION TO MANHOLES, OR CONTRACTOR SHALL INSTALL BOARD INSULATION FOR FREEZING PROTECTION.
- 17. WATER MAINS SHALL BE HYDROSTATICALLY PRESSURE TESTED FOR LEAKAGE PRIOR TO ACCEPTANCE. WATERMAINS SHALL BE TESTED AT 1.5 TIMES THE WORKING PRESSURE OR 150 PSI, WHICH EVER IS GREATER. TESTING SHALL BE CONDUCTED IN ACCORDANCE WITH SECTION 4 OF AWWA STANDARD C 600. WATERMAINS SHALL BE DISINFECTED AFTER THE ACCEPTANCE OF THE PRESSURE AND LEAKAGE TESTS ACCORDING TO AWWA STANDARD C 651.
- 18. ALL WATER AND SANITARY LEADS TO BUILDING(S) SHALL END 5' OUTSIDE THE BUILDING LIMITS AS SHOWN ON PLANS AND SHALL BE PROVIDED WITH A TEMPORARY PLUG AND WITNESS AT END.
- 19. THRUST BLOCKS SHALL BE PROVIDED AT ALL BENDS, TEES, MECHANICAL JOINTS AND FIRE HYDRANTS.
- 20. DIMENSIONS ARE SHOWN TO CENTERLINE OF PIPE OR FITTING.
- 21. CONTRACTOR TO FURNISH SHOP DRAWINGS FOR UTILITY RELATED ITEMS TO ENSURE CONFORMANCE WITH THE PLANS AND SPECIFICATIONS. SHOP DRAWINGS SHOULD BE SENT IN TRIPLICATE TO THE DESIGN ENGINEER FOR REVIEW AND APPROVAL PRIOR TO INSTALLATION.
- 22. EXISTING UTILITIES SHALL BE DIGSAFED BEFORE CONSTRUCTION.
- 23. ALL WATER LINES SHALL HAVE TESTABLE BACKFLOW PREVENTERS AT THE ENTRANCE TO EACH BUILDING.
- 24. ALL GRAVITY SEWER PIPE, MANHOLES, AND FORCE MAINS SHALL BE TESTED ACCORDING TO NHDES STANDARDS OF DESIGN AND CONSTRUCTION FOR SEWAGE AND WASTEWATER TREATMENT FACILITIES, CHAPTER ENV-WQ 700. ADOPTED ON 10-15-14.
- 25. ENV-WQ 704.06 GRAVITY SEWER PIPE TESTING: GRAVITY SEWERS SHALL BE TESTED FOR WATER TIGHTNESS BY USE OF LOW-PRESSURE AIR TESTS CONFORMING WITH ASTM F1417-92(2005) OR UNI-BELL PVC PIPE ASSOCIATION UNI-B-6. LINES SHALL BE CLEANED AND VISUALLY INSPECTED AND TRUE TO LINE AND GRADE. DEFLECTION TESTS SHALL TAKE PLACE AFTER 30 DAYS FOLLOWING INSTALLATION AND THE MAXIMUM ALLOWABLE DEFLECTION OF FLEXIBLE SEWER PIPE SHALL BE 5% OF AVERAGE INSIDE DIAMETER. A RIGID BALL OR MANDREL WITH A DIAMETER OF AT LEAST 95% OF THE AVERAGE INSIDE PIPE DIAMETER SHALL BE USED FOR TESTING PIPE DEFLECTION. THE DEFLECTION TEST SHALL BE
- 26. <u>ENV-WQ 704.17 SEWER MANHOLE TESTING:</u> SHALL BE TESTED FOR LEAKAGE USING A VACUUM TEST PRIOR TO BACKFILLING AND PLACEMENT OF SHELVES AND INVERTS.
- 27. SANITARY SEWER LINES SHALL BE LOCATED AT LEAST TEN (10) FEET HORIZONTALLY FROM AN EXISTING OR PROPOSED WATER LINE. WHEN A SEWER LINE CROSSES UNDER A WATER LINE, THE SEWER PIPE JOINTS SHALL BE LOCATED AT LEAST 6 FEET HORIZONTALLY FROM THE WATERMAIN. THE SEWER LINE SHALL ALSO MAINTAIN A VERTICAL SEPARATION OF NOT LESS THAN 18 INCHES.
- 28. SEWERS SHALL BE BURIED TO A MINIMUM DEPTH OF 6 FEET BELOW GRADE IN ALL ROADWAY LOCATIONS, AND TO A MINIMUM DEPTH OF 4 FEET BELOW GRADE IN ALL CROSS-COUNTRY LOCATIONS. PROVIDE TWO-INCHES OF R-10 FOAM BOARD INSULATION 2-FOOT WIDE TO BE INSTALLED 6-INCHES OVER SEWER PIPE IN AREAS WHERE DEPTH IS NOT ACHIEVED. A WAIVER FROM THE DEPARTMENT OF ENVIRONMENTAL SERVICES WASTEWATER ENGINEERING BUREAU IS REQUIRED PRIOR TO INSTALLING SEWER AT LESS THAN MINIMUM COVER.
- 29. THE CONTRACTOR SHALL MINIMIZE THE DISRUPTIONS TO THE EXISTING SEWER FLOWS AND THOSE INTERRUPTIONS SHALL BE LIMITED TO FOUR (4) HOURS OR LESS AS DESIGNATED BY THE CITY SEWER DEPARTMENT.
- 30. LIGHTING CONDUIT SHALL BE SCHEDULE 40 PVC, AND SHALL BE INSTALLED IN CONFORMANCE WITH THE NATIONAL ELECTRIC CODE. CONTRACTOR SHALL PROVIDE EXCAVATION AND BACKFILL.
- 31. ALL TRENCHING, PIPE LAYING, AND BACKFILLING SHALL BE IN ACCORDANCE WITH FEDERAL OSHA REGULATIONS.
- 32. DISINFECTION OF WATER MAINS SHALL BE CARRIED OUT IN STRICT ACCORDANCE WITH AWWA STANDARD C651, LATEST EDITION. THE BASIC PROCEDURE TO BE FOLLOWED FOR DISINFECTING WATER MAINS IS AS FOLLOWS:
 - PREVENT CONTAMINATING MATERIALS FROM ENTERING THE WATER MAIN DURING STORAGE, CONSTRUCTION, OR REPAIR. REMOVE, BY FLUSHING OR OTHER MEANS, THOSE MATERIALS THAT MAY HAVE ENTERED THE WATER MAINS.
 - CHLORINATE ANY RESIDUAL CONTAMINATION THAT MAY REMAIN, AND FLUSH THE CHLORINATED WATER FROM THE MAIN. PROTECT THE EXISTING DISTRIBUTION SYSTEM FROM BACKFLOW DUE TO HYDROSTATIC PRESSURE TEST AND DISINFECTION PROCEDURES.
 - DETERMINE THE BACTERIOLOGICAL QUALITY BY LABORATORY TEST AFTER DISINFECTION. MAKE FINAL CONNECTION OF THE APPROVED NEW WATER MAIN TO THE ACTIVE DISTRIBUTION SYSTEM
- 33. DOMESTIC SHUTOFFS & VALVES SHALL BE PAINTED BLUE. FIRE SERVICE SHUTOFFS & VALVES SHALL BE PAINTED RED. COORDINATE WITH CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS FOR EXACT COLORS.
- 34. SEWER TRENCH DAMS SHALL BE INSTALLED EVERY 75' ALONG GRAVITY SEWER PIPE.
- 35. IF IRRIGATION IS TO BE USED, THE PIPING SYSTEM SHALL BE REVIEWED AND APPROVED BY THE PORTSMOUTH CITY PLANNER, CITY ENGINEER, AND THE WATER DEPARTMENT PRIOR TO INSTALLATION.
- 36. WATER LINE TO BE CONSTRUCTED PER CITY OF PORTSMOUTH SPECIFICATIONS.
- 37. AN AS-BUILT PLAN OF THE WATER LINE IS TO BE PREPARED AND SUBMITTED TO THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS.

PROJECT PARCEL CITY OF PORTSMOUTH TAX MAP 222, LOT 19

TOTAL LOT AREA 84,795 SQ. FT. 1.95 ACRES

Checked: JAC | Scale: AS NOTED | Project No.: 18134.1 Drawing Name: 18134.1-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE T THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

DANIEL JAMES No.18152 CENSE 08/20/2024

| 8/16/24 REVISED PER CITY REVIEW ENGINEER COMMENTS DJM DJM 4/19/24 **REVISED PER TAC COMMENTS** KDR 3/18/24 ISSUED FOR REVIEW REV. DATE **REVISION** BY

PO Box 219

Stratham, NH 03885

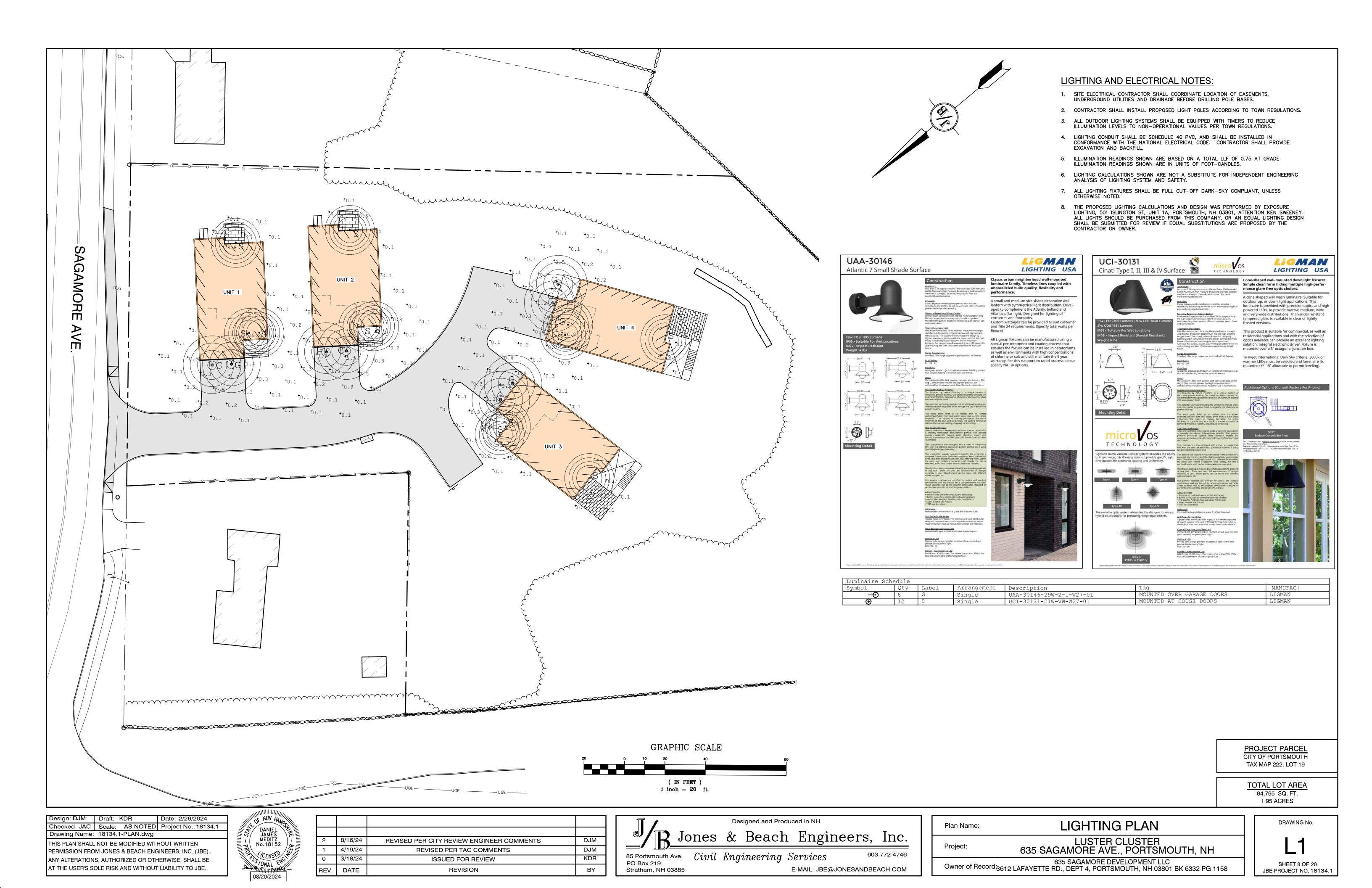
603-772-4746 85 Portsmouth Ave. Civil Engineering Services FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

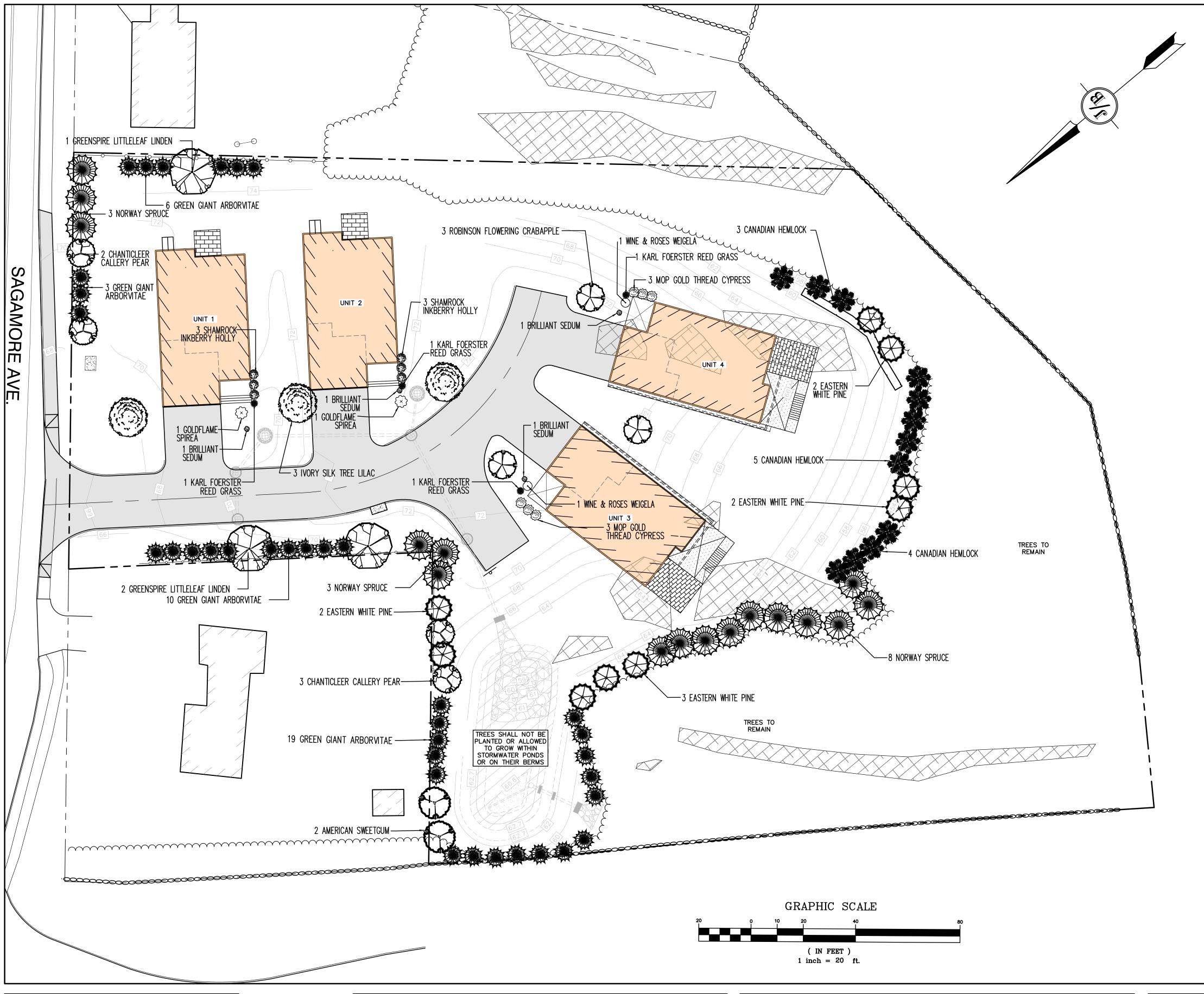
UTILITY PLAN

Project:

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH

635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158 JBE PROJECT NO. 18134.1





LANDSCAPE NOTES:

- 1. THE CONTRACTOR SHALL LOCATE AND VERIFY THE EXISTENCE OF ALL UTILITIES PRIOR TO STARTING WORK.
- THE CONTRACTOR SHALL SUPPLY ALL PLANT MATERIALS IN QUANTITIES SUFFICIENT TO COMPLETE THE PLANTINGS SHOWN ON THE
- ALL MATERIAL SHALL CONFORM TO THE GUIDELINES ESTABLISHED BY THE CURRENT AMERICAN STANDARD FOR NURSERY STOCK PUBLISHED BY THE AMERICAN ASSOCIATION OF NURSERYMEN.
- 4. PLANTS SHALL BE SUBJECT TO INSPECTION AND APPROVAL AT THE PLACE OF GROWTH, UPON DELIVERY OR AT THE JOB SITE WHILE WORK IS ON-GOING FOR CONFORMITY TO SPECIFIED QUALITY, SIZE AND VARIETY.
- PLANTS FURNISHED IN CONTAINERS SHALL HAVE THE ROOTS WELL ESTABLISHED IN THE SOIL MASS AND SHALL HAVE AT LEAST ONE (1) GROWING SEASON. ROOT-BOUND PLANTS OR INADEQUATELY SIZED CONTAINERS TO SUPPORT THE PLANT MAY BE
- DEEMED UNACCEPTABLE. 6. NO PLANT SHALL BE PUT IN THE GROUND BEFORE GRADING HAS BEEN COMPLETED.
- 7. ALL WORK AND PLANTS SHALL BE DONE, INSTALLED AND DETAILED IN STRICT ACCORDANCE WITH PROJECT SPECIFICATIONS.
- 8. ALL PLANTS SHALL BE WATERED THOROUGHLY TWICE DURING THE FIRST 24-HOUR PERIOD AFTER PLANTING. ALL PLANTS SHALL BE WATERED WEEKLY, OR MORE OFTEN IF NECESSARY, DURING THE FIRST GROWING SEASON.
- 9. ALL LANDSCAPE AREAS TO BE GRASS COMMON TO REGION, EXCEPT FOR INTERIOR LANDSCAPED ISLANDS OR WHERE OTHER PLANT MATERIAL IS SPECIFIED.
- 10. ALL TREES AND SHRUBS SHALL BE PLANTED IN MULCH BEDS WITH EDGE STRIPS TO SEPARATE TURF GRASS AREAS.
- 11. THE CONTRACTOR SHALL REMOVE WEEDS, ROCKS, CONSTRUCTION ITEMS, ETC. FROM ANY LANDSCAPE AREA SO DESIGNATED TO
- REMAIN, WHETHER ON OR OFF-SITE. GRASS SEED OR PINE BARK MULCH SHALL BE APPLIED AS DEPICTED ON PLANS.
- 12. EXISTING TREES TO REMAIN SHALL BE PROTECTED WITH TEMPORARY SNOW FENCING AT THE DRIPLINE OF THE TREE. THE CONTRACTOR SHALL NOT STORE VEHICLES OR MATERIALS WITHIN THE LANDSCAPED AREAS. ANY DAMAGE TO EXISTING TREES, SHRUBS OR LAWN SHALL BE REPAIRED BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.
- 13. ALL MULCH AREAS SHALL RECEIVE A 3" LAYER OF SHREDDED PINE BARK MULCH OVER A 10 MIL WEED MAT EQUAL TO 'WEEDBLOCK' BY EASY GARDENER OR DEWITT WEED BARRIER.
- 14. ALL LANDSCAPED AREAS SHALL HAVE SELECT MATERIALS REMOVED TO A DEPTH OF AT LEAST 9" BELOW FINISH GRADE. THE RESULTING VOID IS TO BE FILLED WITH A MINIMUM OF 9" HIGH-QUALITY SCREENED LOAM AMENDED WITH 3" OF AGED ORGANIC
- 15. THIS PLAN IS INTENDED FOR LANDSCAPING PURPOSES ONLY. REFER TO CIVIL/SITE DRAWINGS FOR OTHER SITE CONSTRUCTION INFORMATION.
- 16. IRRIGATION PIPING SYSTEM SHALL BE REVIEWED AND APPROVED BY OWNER AND ENGINEER PRIOR TO INSTALLATION.
- 17. WITH AUTHORIZATION OF THE PROJECT ENGINEER, PROPOSED TREES ALONG EDGE OF WOODED BUFFER SHALL BE PLACED WHEREVER NECESSARY IN ORDER TO COVER GAPS IN EXISTING WOODED BUFFER IN ORDER TO BLOCK VISIBILITY FROM TIDEWATCH CONDOMINIUM PROPERTY.
- 18. TREES SHALL NOT BE PLANTED ON BERMS OF STORMWATER PONDS.
- 19. ALL PLANTING SHALL ADHERE TO THE GENERAL REQUIREMENTS OUTLINED IN SECTION 6.3 AND THE PLANTING REQUIREMENTS OUTLINED IN SECTION 6.4 OF THE PORTSMOUTH SITE PLAN REVIEW REGULATIONS.
- 20. ALL PLANTING SHALL FOLLOW THE ANSI A300 PART 6 STANDARD PRACTICES FOR PLANTING AND TRANSPLANTING (AS AMENDED).

Quantity	Botanical Name	Common Name	Size
4	Calamagrostis x acutiflora 'Karl Foerster'	KARL FOERSTER REED GRASS **	2 Gallon
6	Chamaecyparis pisifera 'Mop'	MOP GOLD THREAD CYPRESS **	5 Gallon
6	llex glabra 'Shamrock'	SHAMROCK INKBERRY HOLLY **	5 Gallon
2	Liquidambar styraciflua	AMERICAN SWEETGUM **	3" Caliper
3	Malus x 'Robinson'	ROBINSON FLOWERING CRABAPPLE **	2" Caliper
16	Picea abies	NORWAY SPRUCE	8-9 Ft. Ht.
9	Pinus strobus	EASTERN WHITE PINE	8-9 Ft. Ht.
4	Pyrus calleryana 'Chanticleer'	CHANTICLEER CALLERY PEAR **	2.5" Caliper
4	Sedum spectabile 'Brilliant'	BRILLIANT SEDUM **	1 Gallon
2	Spiraea japonica 'Goldflame'	GOLDFLAME SPIREA **	5 Gallon
3	Syringa reticulata 'Ivory Silk'	IVORY SILK TREE LILAC	2" Caliper
38	Thuja plicata 'Green Giant'	GREEN GIANT ARBORVITAE **	7-8 Ft. Ht.
3	Tilia cordata 'Greenspire'	GREENSPIRE LITTLELEAF LINDEN **	3" Caliper
12	Tsuga canadensis	CANADIAN HEMLOCK	8-9 Ft. Ht.
2	Weigela florida 'Alexandra'	WINE & ROSES WEIGELA	5 Gallon
**	Denotes plants that are tolerant of urban conditions including road salt, soil compaction, drought, heat, and air pollution.		

PROJECT PARCEL CITY OF PORTSMOUTH TAX MAP 222, LOT 19

TOTAL LOT AREA 84,795 SQ. FT. 1.95 ACRES

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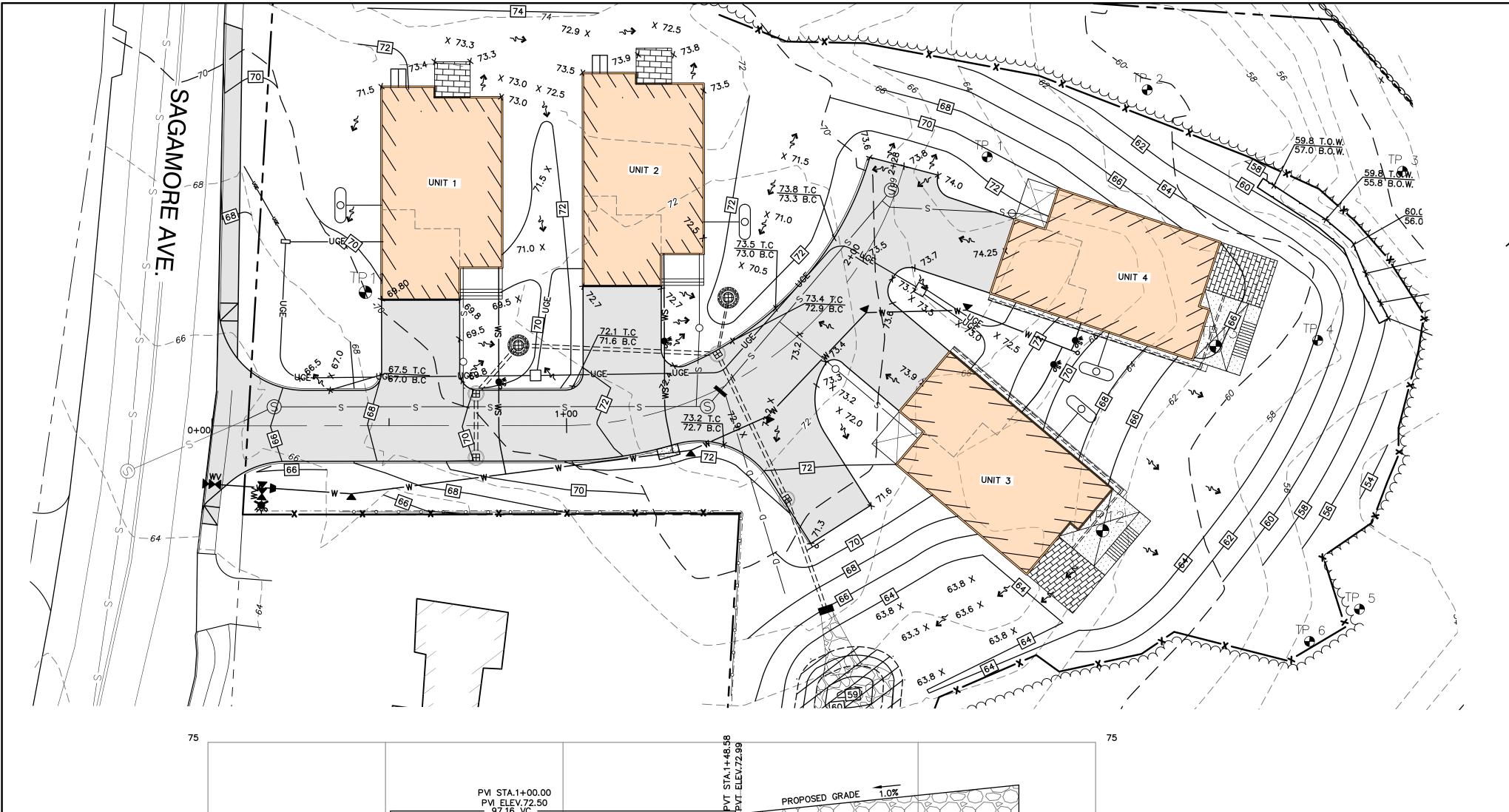
Stratham, NH 03885

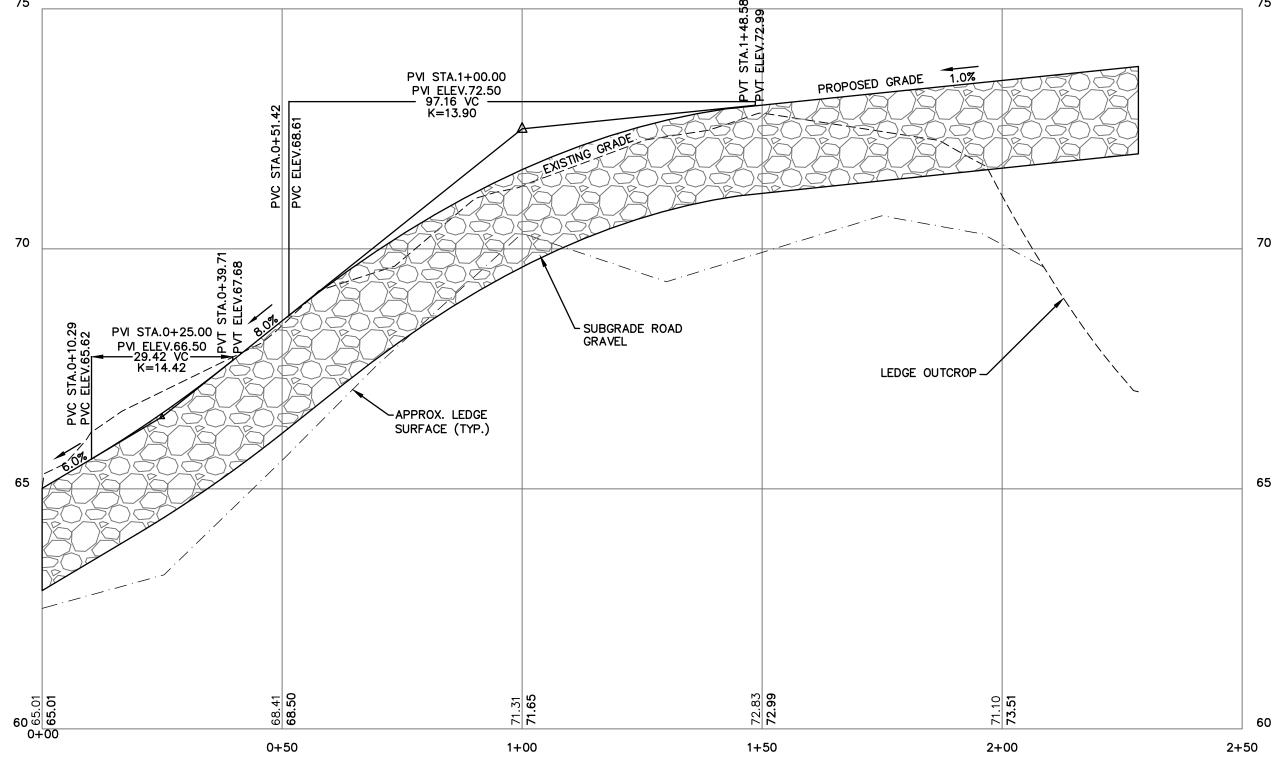
LANDSCAPE PLAN Plan Name:

Project:

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH 635 SAGAMORE DEVELOPMENT LLC
Owner of Record;3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

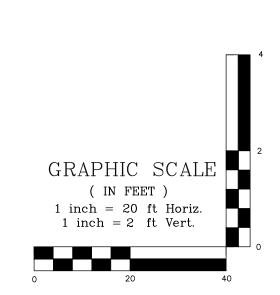
SHEET 9 OF 20 JBE PROJECT NO. 18134.1





NOTES:

- THIS SITE WILL REQUIRE A USEPA NPDES PERMIT FOR STORMWATER DISCHARGE FOR THE CONSTRUCTION SITE. THE CONSTRUCTION SITE OPERATOR SHALL DEVELOP AND IMPLEMENT A CONSTRUCTION STORM WATER POLLUTION PREVENTION PLAN (SWPPP), WHICH SHALL REMAIN ON SITE AND BE MADE ACCESSIBLE TO THE PUBLIC. THE CONSTRUCTION SITE OPERATOR SHALL SUBMIT A NOTICE OF INTENT (NOI) TO THE EPA REGIONAL OFFICE SEVEN DAYS PRIOR TO COMMENCEMENT OF ANY WORK ON SITE. EPA WILL POST THE NOI AT HTTP://CFPUB1.EPA.GOV/NPDES/STORMWATER/NOI/NOISEARCH.CFM. AUTHORIZATION IS GRANTED UNDER THE PERMIT ONCE THE NOI IS SHOWN IN "ACTIVE" STATUS ON THIS WEBSITE. A COMPLETED NOTICE OF TERMINATION SHALL BE SUBMITTED TO THE NPDES PERMITTING AUTHORITY WITHIN 30 DAYS AFTER EITHER OF THE FOLLOWING CONDITIONS HAVE BEEN MET:
 - A. FINAL STABILIZATION HAS BEEN ACHIEVED ON ALL PORTIONS OF THE SITE FOR WHICH THE PERMITTEE IS RESPONSIBLE;
 - B. ANOTHER OPERATOR/PERMITTEE HAS ASSUMED CONTROL OVER ALL AREAS OF THE SITE THAT HAVE NOT BEEN FINALLY STABILIZED. PROVIDE DPW WITH A COPY OF THE NOTICE OF TERMINATION (NOT).
- 2. ALL ROAD AND DRAINAGE WORK SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE STANDARD SPECIFICATIONS FOR THE CITY, AND NHDOT SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION, WHICHEVER IS MORE STRINGENT.
- 3. AS-BUILT PLANS TO BE SUBMITTED TO THE CITY PRIOR TO ACCEPTANCE OF THE ROADWAY.
- CONTRACTOR TO COORDINATE AND COMPLETE ALL WORK REQUIRED FOR THE RELOCATION AND/OR INSTALLATION OF ELECTRIC, CATV, TELEPHONE, PER UTILITY DESIGN AND STANDARDS. LOCATIONS SHOWN ARE APPROXIMATE. LOW PROFILE STRUCTURES SHALL BE USED TO THE GREATEST EXTENT POSSIBLE.
- 5. THIS PLAN HAS BEEN PREPARED BY JONES & BEACH ENGINEERS, INC. FOR MUNICIPAL AND STATE APPROVALS AND FOR CONSTRUCTION BASED ON DATA OBTAINED FROM ON—SITE FIELD SURVEY AND EXISTING MUNICIPAL RECORDS. THROUGHOUT THE CONSTRUCTION PROCESS, THE CONTRACTOR SHALL INFORM THE ENGINEER IMMEDIATELY OF ANY FIELD DISCREPANCY FROM DATA SHOWN ON THE DESIGN PLANS. THIS INCLUDES ANY UNFORESEEN CONDITIONS, SUBSURFACE OR OTHERWISE, FOR EVALUATION AND RECOMMENDATIONS. ANY CONTRADICTION BETWEEN ITEMS OF THIS PLAN/PLAN SET, OR BETWEEN THE PLANS AND ON—SITE CONDITIONS MUST BE RESOLVED BEFORE RELATED CONSTRUCTION HAS BEEN INITIATED.
- 6. SILTATION AND EROSION CONTROLS SHALL BE INSTALLED PRIOR TO CONSTRUCTION, SHALL BE MAINTAINED DURING CONSTRUCTION, AND SHALL REMAIN UNTIL SITE HAS BEEN STABILIZED WITH PERMANENT VEGETATION. SEE DETAIL SHEET E1 FOR ADDITIONAL NOTES ON EROSION CONTROL.
- 7. ALL DISTURBED AREAS NOT STABILIZED BY OCTOBER 15TH SHALL BE COVERED WITH AN EROSION CONTROL BLANKET. PRODUCT TO BE SPECIFIED BY THE ENGINEER.
- 8. FINAL DRAINAGE, GRADING AND EROSION PROTECTION MEASURES SHALL CONFORM TO REGULATIONS OF THE PUBLIC WORKS DEPARTMENT.
- 9. CONTRACTOR TO VERIFY EXISTING UTILITIES AND TO NOTIFY ENGINEER OF ANY DISCREPANCY IMMEDIATELY.
- 10. DRAINAGE INSPECTION AND MAINTENANCE SCHEDULE: SILT FENCING WILL BE INSPECTED DURING AND AFTER STORM EVENTS TO ENSURE THAT THE FENCE STILL HAS INTEGRITY AND IS NOT ALLOWING SEDIMENT TO PASS. SEDIMENT BUILD UP IN SWALES WILL BE REMOVED IF IT IS DEEPER THAN SIX INCHES, AND IS TO BE REMOVED FROM SUMPS BELOW THE INLET OF CULVERTS SEMIANNUALLY, AS WELL AS FROM CATCH BASINS. FOLLOWING MAJOR STORM EVENTS, THE STAGE DISCHARGE OUTLET STRUCTURES ARE TO BE INSPECTED AND ANY DEBRIS REMOVED FROM THE ORIFICE, TRASH TRACK AND EMERGENCY SPILL WAY. INFREQUENTLY, SEDIMENT MAY ALSO HAVE TO BE REMOVED FROM THE SUMP OF THE STRUCTURE.
- 11. ALL DRAINAGE INFRASTRUCTURE SHALL BE INSTALLED AND STABILIZED PRIOR TO DIRECTING ANY RUNOFF TO IT.
- 12. BIORETENTION PONDS REQUIRE TIMELY MAINTENANCE AND SHOULD BE INSPECTED AFTER EVERY MAJOR STORM EVENT, AS WELL AS FREQUENTLY DURING THE FIRST YEAR OF OPERATION, AND ANNUALLY THEREAFTER. EVERY FIVE YEARS, THE SERVICES OF A PROFESSIONAL ENGINEER SHOULD BE RETAINED TO PERFORM A THOROUGH INSPECTION OF THE BIORETENTION POND AND ITS INFRASTRUCTURE. ANY DEBRIS AND SEDIMENT ACCUMULATIONS SHOULD BE REMOVED FROM THE OUTLET STRUCTURE(S) AND EMERGENCY SPILLWAY(S) AND DISPOSED OF PROPERLY. BIORETENTION POND BERMS SHOULD BE MOWED AT LEAST ONCE ANNUALLY SO AS TO PREVENT THE ESTABLISHMENT OF WOODY VEGETATION. TREES SHOULD NEVER BE ALLOWED TO GROW ON A BIORETENTION POND BERM, AS THEY MAY DESTABILIZE THE STRUCTURE AND INCREASE THE POTENTIAL FOR FAILURE. AREAS SHOWING SIGNS OF EROSION OR THIN OR DYING VEGETATION SHOULD BE REPAIRED IMMEDIATELY BY WHATEVER MEANS NECESSARY, WITH THE EXCEPTION OF FERTILIZER. RODENT BORROWS SHOULD BE REPAIRED IMMEDIATELY AND THE ANIMALS SHOULD BE TRAPPED AND RELOCATED IF THE PROBLEM PERSISTS.
- 13. IN THOSE AREAS WHERE THE BERMS OF THE BIORETENTION SYSTEMS MUST BE CONSTRUCTED BY THE PLACEMENT OF FILL, THE ENTIRE EMBANKMENT AREA OF THE BIORETENTION PONDS SHALL BE EXCAVATED TO PROPOSED GRADE, STRIPPED OF ALL ORGANIC MATERIALS, COMPACTED TO AT LEAST 95% AND SCARIFIED PRIOR TO THE PLACEMENT OF THE EMBANKMENT MATERIAL. IN THE EVENT THE FOUNDATION MATERIAL EXPOSED DOES NOT ALLOW THE SPECIFIED COMPACTION, AN ADDITIONAL ONE FOOT (1') OF EXCAVATION AND THE PLACEMENT OF A ONE FOOT (1') THICK, TWELVE FOOT (12') WIDE PAD OF THE MATERIAL DESCRIBED IN THE NOTE BELOW, COMPACTED TO 95% OF ASTM D-1557 MAY BE NECESSARY. PLACEMENT AND COMPACTION SHOULD OCCUR AT A MOISTURE CONTENT OF OPTIMUM PLUS OR MINUS 3%, AND NO FROZEN OR ORGANIC MATERIAL SHOULD BE PLACED WITHIN FOR ANY REASON.
- 14. EMBANKMENT IS TO HAVE 3:1 SIDE SLOPES (MAX.) AND IS TO BE BROUGHT TO SPECIFIED GRADES PRIOR TO THE ADDITION OF LOAM (4" MINIMUM) SO AS TO ALLOW FOR THE COMPACTION OF THE STRUCTURE OVER TIME WHILE MAINTAINING THE PROPER BERM FLEXATION
- 15. COMPACTION TESTING SERVICES (I.E. NUCLEAR DENSITY TESTS) ARE TO BE PERFORMED BY AN INDEPENDENT GEOTECHNICAL ENGINEER RETAINED BY THE CONTRACTOR FOR ROADWAY CONSTRUCTION, AND ON THE FOUNDATION OF THE BERM AND ON EVERY



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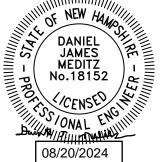
Drawing Name: 18134.1-PLAN.dwg

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Civil Engineering Services

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FAX: 603-772-0227
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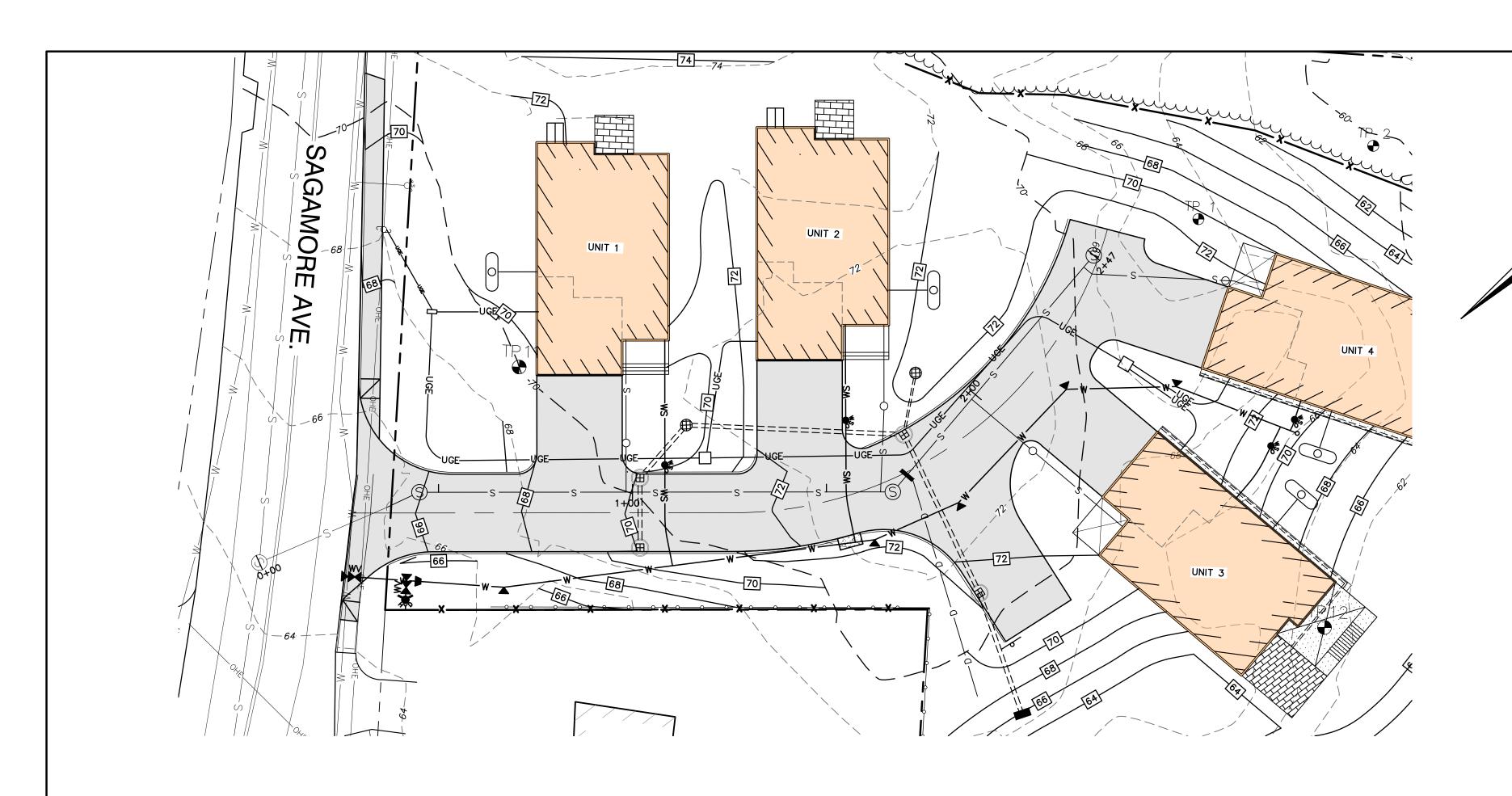
Plan Name: DRIVEWAY PLAN AND PROFILE

LUSTER CLUSTER
635 SAGAMORE AVE., PORTSMOUTH, NH

635 SAGAMORE DEVELOPMENT LLC Owner of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158 DRAWING No.

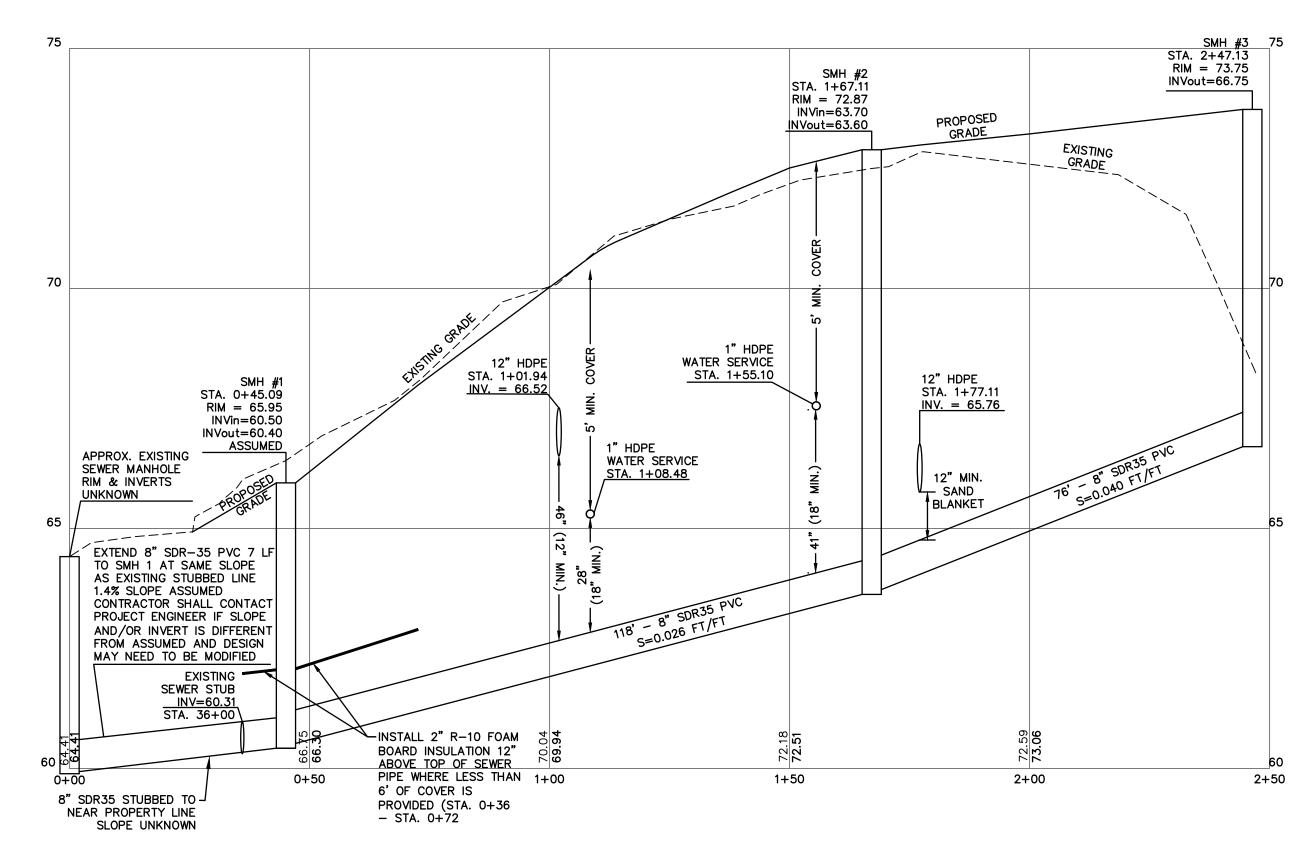
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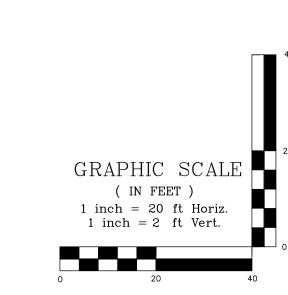
SHEET 10 OF 20
JBE PROJECT NO. 18134.1



NOTES:

- 1. PROPOSED GRADES SHOWN HEREON ARE APPROXIMATE. REFER TO SHEETS C3 AND P1 FOR GRADING OF SITE AND DRIVEWAY. SET RIM ELEVATIONS OF SEWER STRUCTURES FLUSH WITH PROPOSED GRADE.
- 2. STATIONS REFER TO CENTERLINE OF SEWER STRUCTURE OR CROSSING DRAINAGE/WATER PIPE.
- CONTRACTOR TO CONFIRM ACTUAL EXISTING INVERT OF STUB IN THE FIELD AND NOTIFY ENGINEER IF IT IS MORE THAN 0.1'
 DIFFERENT FROM THE STATED INVERT.





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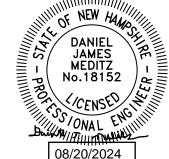
Plan Name:	SEWER PLAN AND PROFILE
Project:	LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH

635 SAGAMORE DEVELOPMENT LLC
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P2
SHEET 11 OF 20
JBE PROJECT NO. 18134.1



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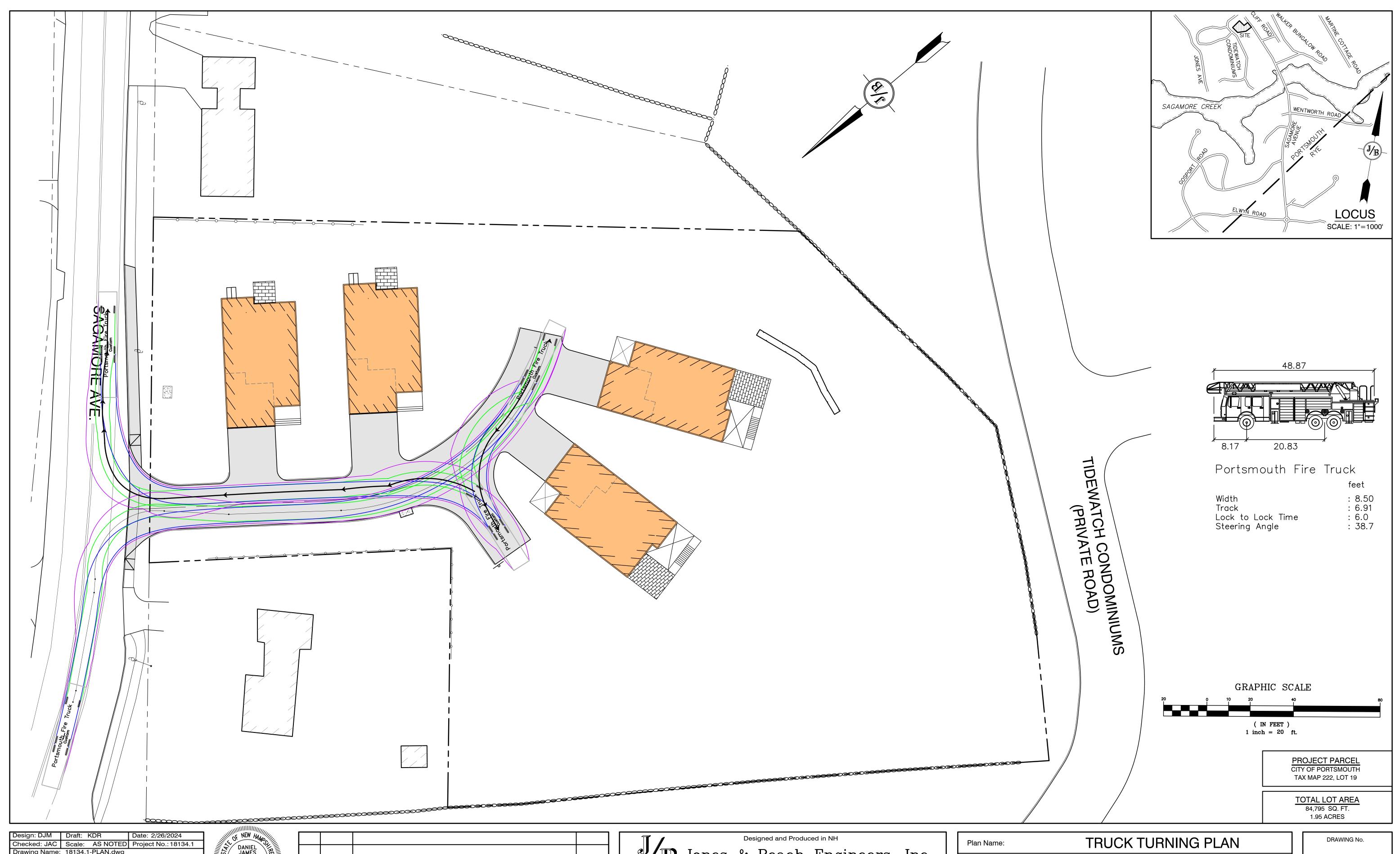
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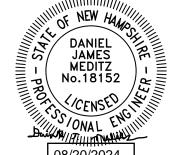
Plan Name:	HIGHWAY ACCESS PLAN
Project:	LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH
Owner of Record:	635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

SHEET 12 OF 20

JBE PROJECT NO. 18134.1



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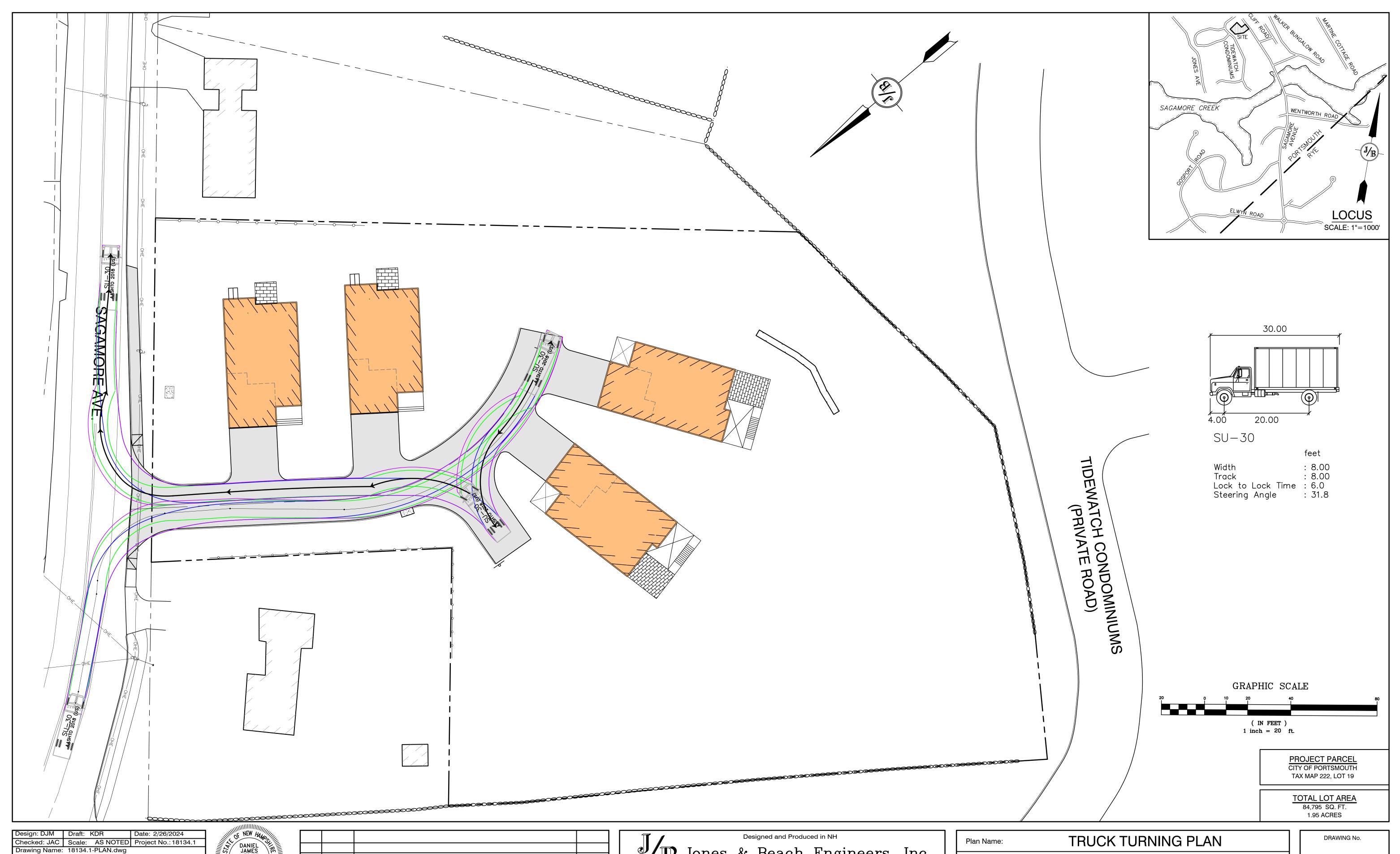
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PO Box 219 603-772-4 FAX: 603-772-0

Stratham, NH 03885

		Project:
Services	603-772-4746	
Dervices	FAX: 603-772-0227	0
E-MAIL: JBE@J	ONESANDBEACH.COM	Owner c

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH 635 SAGAMORE DEVELOPMENT LLC r of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158 SHEET 13 OF 20 JBE PROJECT NO. 18134.1



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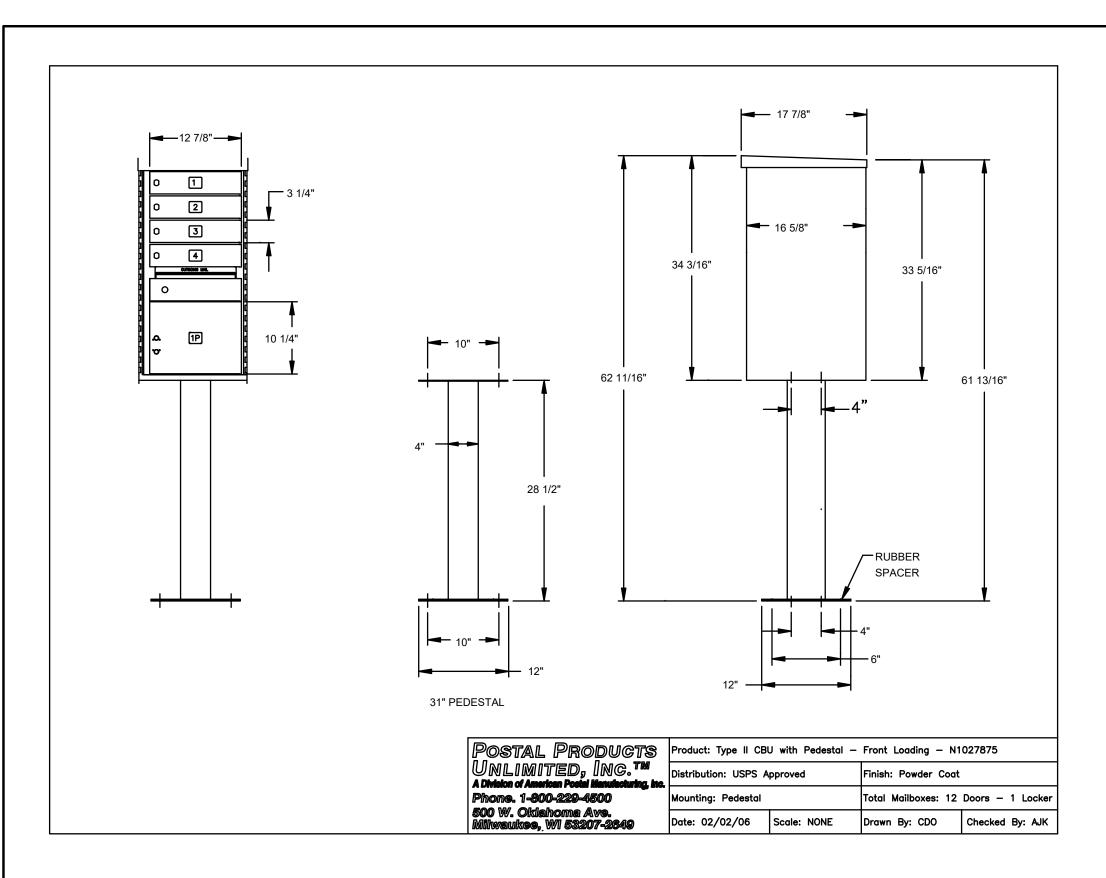
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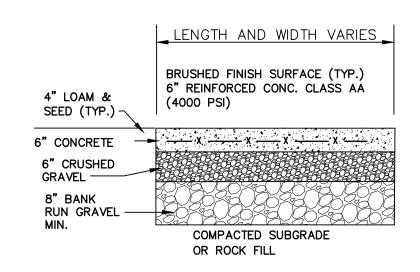
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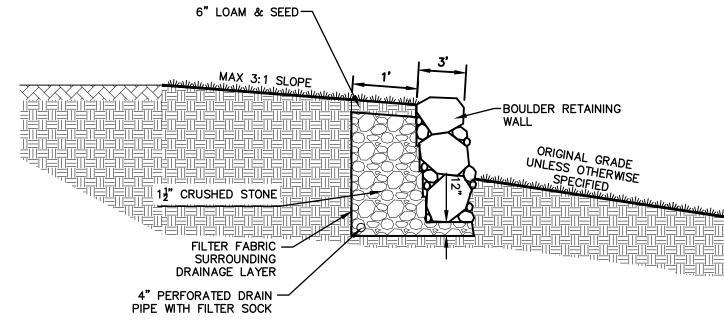
CLUSTER MAILBOX UNIT DETAIL

NOT TO SCALE



CONCRETE PAD DETAIL

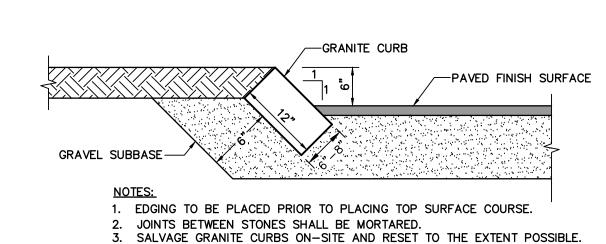
NOT TO SCALE



THE CONTRACTOR IS RESPONSIBLE FOR RETAINING THE SERVICES OF A STRUCTURAL ENGINEER LISENCED IN THE STATE OF NEW HAMPSHIRE TO DESIGN ANY WALL THAT HAS A HEIGHT OVER 4.0'. JONES & BEACH ENGINEERS, INC. DOES NOT ACCEPT ANY LIABILITY FOR THE STRUCTURAL DESIGN AND/OR INSTALLATION OF ANY RETAINING WALL OF ANY TYPE ABOVE THIS HEIGHT. THIS DETAIL IS INTENDED TO PROVIDE AN EXAMPLE OF THE RETAINING WALL FOR PLANNING PURPOSES ONLY AND IS SPECIFICALLY NOT INTENDED FOR USE BY THE CONTRACTOR IN ANY CONSTRUCTION-RELATED ACTIVITY FOR A WALL GREATER THAN 4.0' IN HEIGHT.

BOULDER RETAINING WALL CROSS SECTION

NOT TO SCALE



-SAWCUT AND REMOVE EXIST. PAVEMENT.

WITH BIT. EMULSION PRIOR TO PLACING

ABUTTING PAVEMENT

KEYWAY

9-79-79-79-79-79-

TO EXISTING PAVEMENT

KEYWAY DETAIL FOR CONNECTION

BINDER COURSE -

BASE COURSE-

NOT TO SCALE

COAT EXPOSED EDGES OF EXISTING PVMT.

—1" TOP COURSE

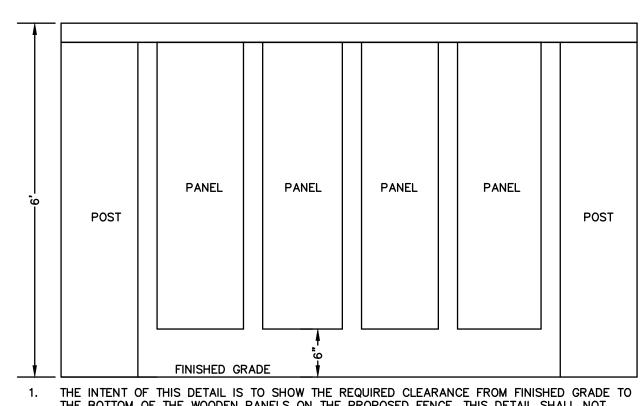
12" MIN. GRAVEL

/-- 2" BINDER COURSE

←6" CRUSHED GRAVEL

SLOPED GRANITE CURB

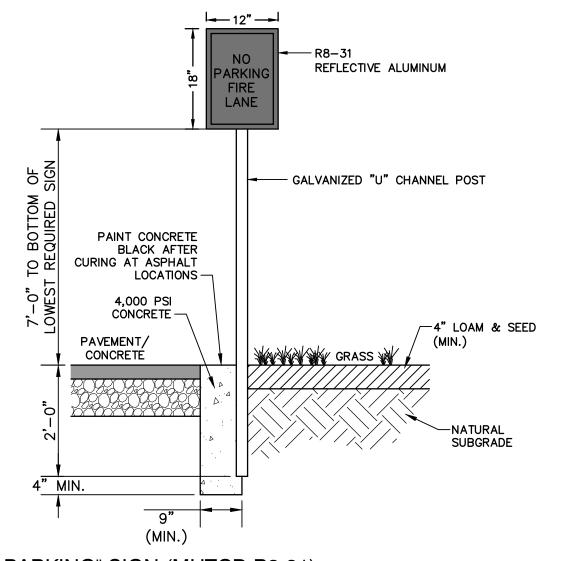
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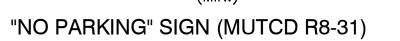


THE BOTTOM OF THE WOODEN PANELS ON THE PROPOSED FENCE. THIS DETAIL SHALL NOT CONSTRUE A REQUIREMENT WITH REGARDS TO POST OR PANEL PLACEMENT ALONG THE LENGTH

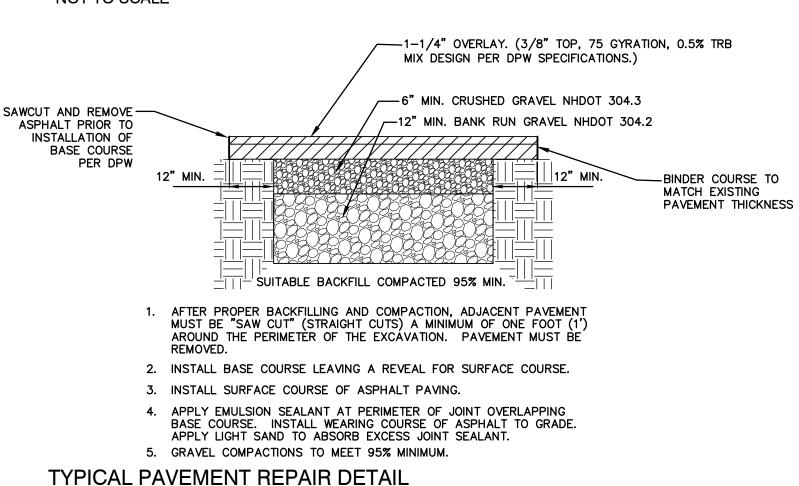
6' HIGH WOODEN STOCKADE FENCE DETAIL

NOT TO SCALE





NOT TO SCALE



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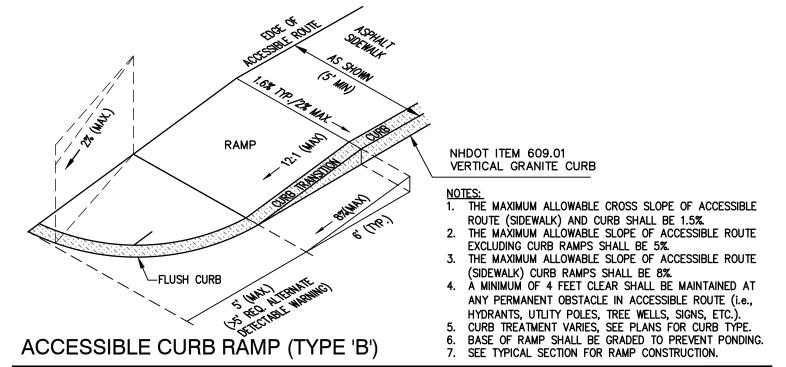
85 Portsmouth Ave. Civil Engineering Services

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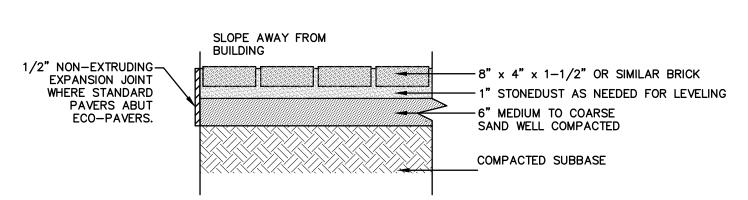
Stratham, NH 03885

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NOT TO SCALE



-2.5" -3/4" HOT BIT PAVEMENT

6" NHDOT ITEM 304.3 CRUSHED

GRAVEL 95% MIN. COMPACTION INCLUDING RECLAIMED MATERIAL

-12" - NHDOT ITEM 304.2 BANK

(NHDOT 19mm SUPERPAVE)

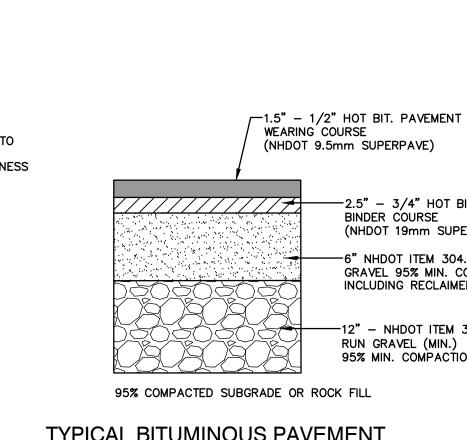
BINDER COURSE

RUN GRAVEL (MIN.)

95% MIN. COMPACTION

STANDARD BRICK PAVER

NOT TO SCALE



TYPICAL BITUMINOUS PAVEMENT

635 SAGAMORE DEVELOPMENT LLC

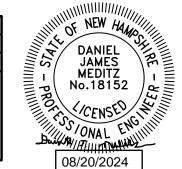
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DETAIL SHEET Plan Name: LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH Project:

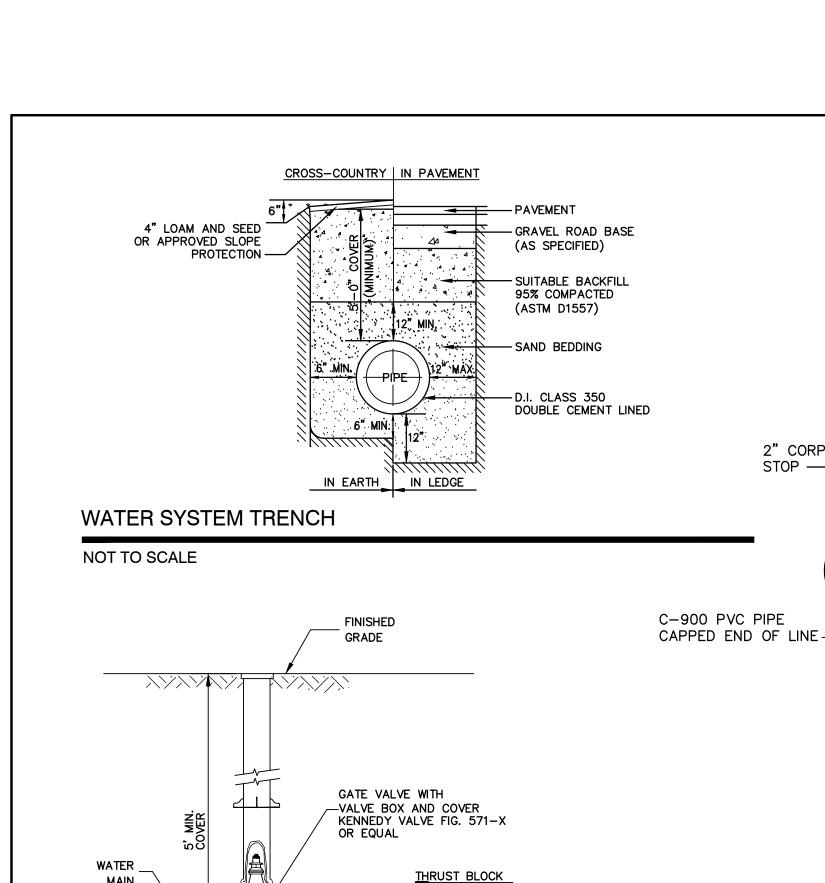
Owner of Record 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

DRAWING No. SHEET 15 OF 20 JBE PROJECT NO. 18134.1

Design: DJM	Draft:	KDR	Date: 2/26/2024
Checked: JAC	Scale:	AS NOTED	Project No.: 18134.1
Drawing Name:	18134.	1-PLAN.dwg	
THIS PLAN SHALL	NOT BE	MODIFIED WITH	HOUT WRITTEN
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ANY ALTERATION	S, AUTHO	RIZED OR OTH	IERWISE, SHALL BE
			LIABILITY TO JBE.



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REV.	DATE	REVISION	BY



BURIED GATE VALVE DETAIL

RODDING 5/8" MIN.

NOT TO SCALE

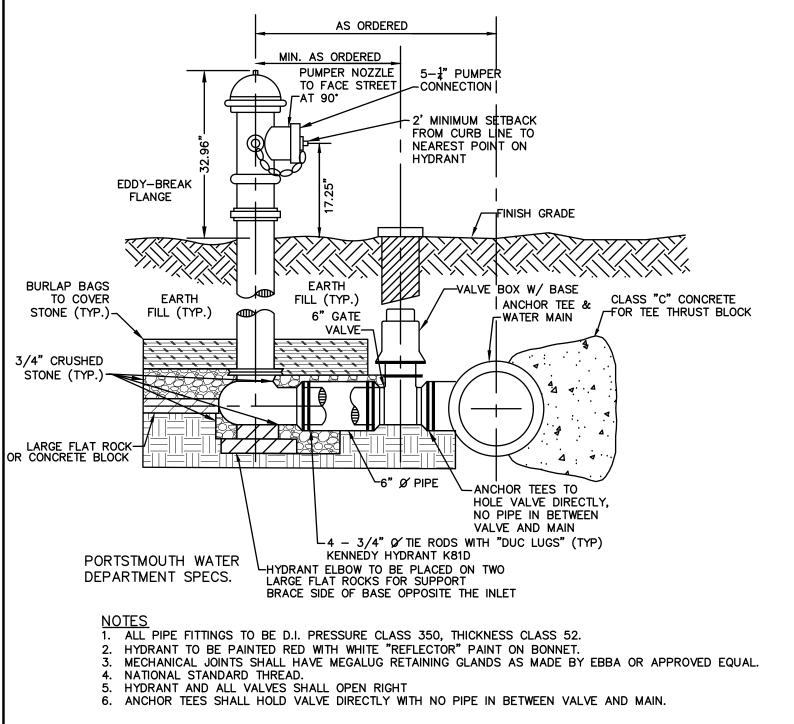
Design: DJM | Draft: KDR

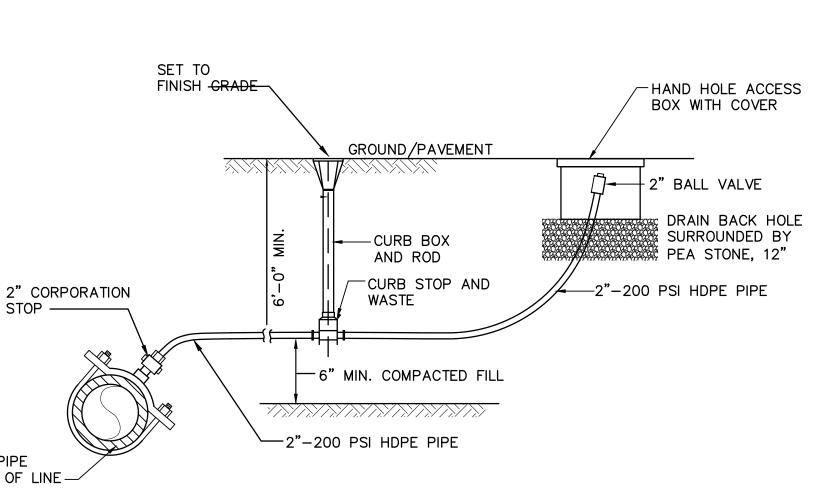
Drawing Name: 18134.1-PLAN.dwg

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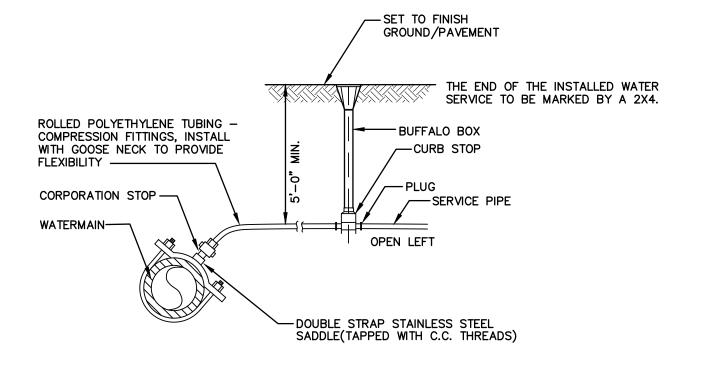
MAIN





TYPICAL WATER MAIN BLOWOFF

NOT TO SCALE



WATER SERVICE CONNECTION-POLYETHYLENE

NOT TO SCALE

NOT TO SCALE

BACKFILL MATERIAL EXISTING GRADE-- EXCAVATION AND BACKFILL IN ACCORDANCE WITH UTILITY WARNING TAPE -COMPANY STANDARDS GAS PIPELINE MATERIAL AND INSTALLATION BY UTILITY COMPANY CONTRACTOR TO COORDINATE WITH UTILITY COMPANY AND TRACER WIRE PROVIDE EXCAVATION AND BACKFILL FOR PIPE INSTALLATION GRANULAR BACKFILL SAND NHDOT 209.3 (OR AS SPECIFIED BY UTILITY COMPANY) -**GAS TRENCH**

NOT TO SCALE

1. CONTRACTOR TO INSTALL 2" RIGID INSULATION BETWEEN THE PROPOSED WATERMAIN(S) AND DRAINAGE LINES IN ALL AREAS WHERE SEPARATION IS TO BE IN 4' OR LESS.

2. ALL PIPE, FITTINGS, HYDRANTS, AND WORKMANSHIP SHALL BE INSPECTED AND APPROVED BY THE MUNICIPAL WATER/SEWER DEPARTMENT.

4. ALL CONSTRUCTION AND TESTING SHALL COMPLY WITH THE REGULATIONS OF THE MUNICIPAL, THE STATE, AND THE AMERICAN WATER WORKS ASSOCIATION.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING AND DETERMINING THE LOCATION, SIZE, AND ELEVATION OF ALL EXISTING UTILITIES PRIOR TO THE START OF CONSTRUCTION. THE ENGINEER SHALL BE NOTIFIED IN WRITING OF ANY UNFORESEEN UTILITY FOUND INTERFERING WITH THE PROPOSED CONSTRUCTION. ANY APPROPRIATE REMEDIAL ACTION MUST BE AGREED TO BY THE ENGINEER PRIOR TO THE COMMENCEMENT OF WORK. THE CONTRACTOR SHALL BE RESPONSIBLE FOR CONTACTING "DIG-SAFE" AT 1-888-344-7233 AT LEAST 72 HOURS BEFORE DIGGING.

6. ALL CONCRETE SHALL HAVE A COMPRESSIVE STRENGTH OF NOT LESS THAN 2000 PSI AFTER 28 DAYS.

7. CONTRACTOR TO INSTALL CORPORATION FITTINGS AT EACH CONNECTION TO THE WATER MAIN FOR TESTING PURPOSES. CORPORATIONS SHALL BE REMOVED AND PLUGGED AT THE COMPLETION OF TESTING.

8. CONTRACTOR TO OBSERVE ALL APPROPRIATE BEST MANAGEMENT PRACTICES.

9. ALL GATE VALVES TO BE MUELLER RESILIENT WEDGE (OPEN RIGHT).

10. ALL TEES TO BE ANCHOR TEES.

11. THE TERMINAL 36' OF ALL "DEAD END" WATERMAINS AND ALL BENDS AND TEES ARE TO BE FITTED WITH MECHANICAL RESTRAINING JOINTS, "MEGALUG" OR APPROVED EQUAL AND THRUST BLOCKS.

12. INSTALL THRUST BLOCKS AT ALL TEES, BENDS, AND FITTINGS.

-SELECT BACKFILL COMPACTED IN 6" LAYERS - 95% STANDARD PROCTOR DENSITY **SEPARATION NOTES:** 1. WATER MAINS SHALL BE LAID AT LEAST 10 FEET HORIZONTALLY FROM ANY

-WATER MAIN

EXISTING OR PROPOSED SEWERS. THE DISTANCE SHALL BE MEASURED EDGE TO EDGE. 2. WATER MAINS CROSSING SEWERS SHALL BE LAID TO PROVIDE A MINIMUM VERTICAL DISTANCE OF 18 INCHES BETWEEN PIPES. SEWER PIPE JOINTS SHALL BE LOCATED AT LEAST 6 FEET HORIZONTALLLY FROM THE WATER MAIN.

CONCRETE THRUST BLOCK DIMENSIONS

90° BEND | 45° BEND | 22.5° BEND

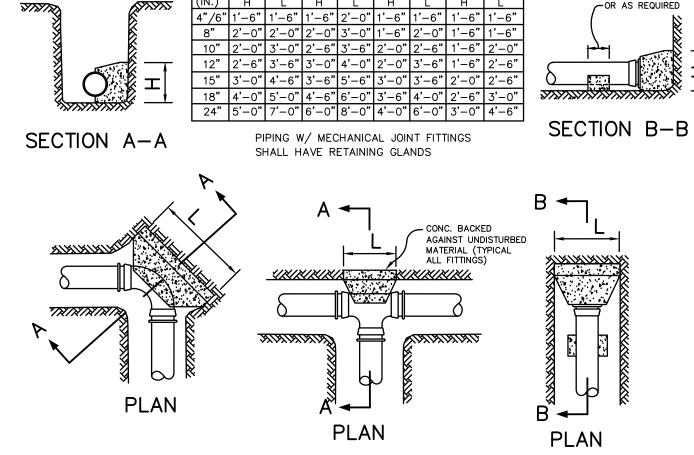
1'-6" CONC. CRADLE

ONE STANDARD FULL

LENGTH OF WATER MAIN TO

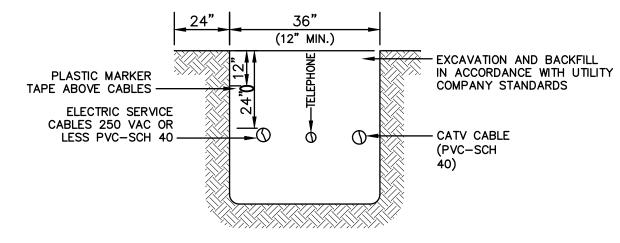
BE CENTERED OVER SEWER

TYPICAL WATER / SEWER SEPARATION



THRUST BLOCK DETAILS

NOT TO SCALE



NOTE: ALL UTILITIES SHALL BE REVIEWED AND APPROVED BY APPROPRIATE UTILITY COMPANY.

UTILITY TRENCH

NOT TO SCALE

Plan Name:

Project:

DETAIL SHEET

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH

DRAWING No. JBE PROJECT NO. 18134.1

SUBMITTALS
SHOP DRAWINGS, INCLUDING SPECIFICATIONS, CATALOG CUTS, DATA SHEETS, DRAWINGS AND OTHER DESCRIPTIVE MATERIAL SHALL BE SUPPLIED TO THE ENGINEER FOR REVIEW PRIOR TO INSTALLATION. A CERTIFICATE OF COMPLIANCE FROM THE MANUFACTURER INDICATING CONFORMANCE WITH THE SPECIFIED REQUIREMENTS FOR DUCTILE IRON PIPE SHALL BE SUBMITTED TO THE ENGINEER FOR REVIEW AND APPROVAL.

<u>DELIVERY, HANDLING, AND STORAGE</u>
ALL PIPE AND APPURTENANCES ARE SUBJECT TO INSPECTION BY THE ENGINEER AT THE POINT OF DELIVERY. MATERIAL FOUND TO BE DEFECTIVE DUE TO MANUFACTURE OR DAMAGE IN SHIPMENT SHALL BE REJECTED OR RECORDED ON THE BILL OF LADING AND REMOVED FROM THE JOB SITE. ALL MATERIALS, IF STORED, SHALL BE KEPT SAFE FROM ANY POTENTIAL DAMAGE.

SAND BEDDING SAND BLANKET SHALL CONSIST OF CLEAN SAND THAT IS FREE FROM ORGANIC MATTER AND GRADED SO THAT 90-100% PASSES A 1/2" SIEVE AND NOT MORE THAN 15% WILL PASS A #200

BACKFILL SUITABLE MATERIAL FOR BACKFILL IN ROADS, ROAD SHOULDERS, AND WALKWAYS SHALL BE THE NATURAL MATERIAL REMOVED DURING THE COURSE OF TRENCH EXCAVATION, BUT SHALL EXCLUDE ANY DEBRIS, PAVEMENT, ORGANIC MATTER, LOAM, WET OR SOFT MUCK, PEAT, OR CLAY. BACKFILL MATERIAL SHALL BE PLACED IN 6" LIFTS AND SHALL BE COMPACTED TO 95% OF ASTM-1557 AT OPTIMUM MOISTURE CONTENT.

DUCTILE IRON PIPE-CLASS 52 JOINTS SHALL BE OF "PUSH-ON" TYPE UNLESS OTHERWISE SPECIFIED. PIPE SHALL HAVE A DOUBLE CEMENT LINING WITH SEAL COATING INSIDE AND BITUMINOUS COATING OUTSIDE THAT MEETS OR EXCEEDS THE REQUIREMENTS OF AWWA/ANSI C104/A21.4. GASKETS FOR DUCTILE IRON PIPE SHALL BE OIL-RESISTANT RUBBER WHICH MEETS OR EXCEEDS THE REQUIREMENTS OF AWWA/ANSI C111/A21.11. PIPE SHALL BE FURNISHED COMPLETE WITH ALL GASKETS AND

WATERMAIN TESTING
ALL WATER MAINS WILL BE CLEANED AND HYDROSTATICALLY TESTED AT A MINIMUM PRESSURE OF 150psi AT THE HIGHEST POINT ALONG THE TEST SECTION. THE HYDROSTATIC TEST SHALL BE CONDUCTED FOR A MINIMUM OF TWO HOURS DURING WHICH TEST PRESSURE SHALL NOT VARY MORE THAN ±5psi. LEAKAGE CALCULATIONS WILL BE COMPLETED IN ACCORDANCE WITH THE REQUIREMENTS OF THE AMERICAN WATER WORKS ASSOCIATION. DISINFECTION WILL BE REQUIRED PER THE SPECIFICATIONS OF ANSI/AWWA C651. WITHIN 24 HOURS OF DISINFECTION, ALL NEWLY INSTALLED MAINS SHALL BE FLUSHED.

WATER LINE TECHNICAL SPECIFICATIONS HYDRANT INSTALLATION NOT TO SCALE

OF NEW HAMP Date: 2/26/2024 Checked: JAC | Scale: AS NOTED | Project No.: 18134.1 DANIEL JAMES THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN No.18152 DE CENSED LA CHOMPANA PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).

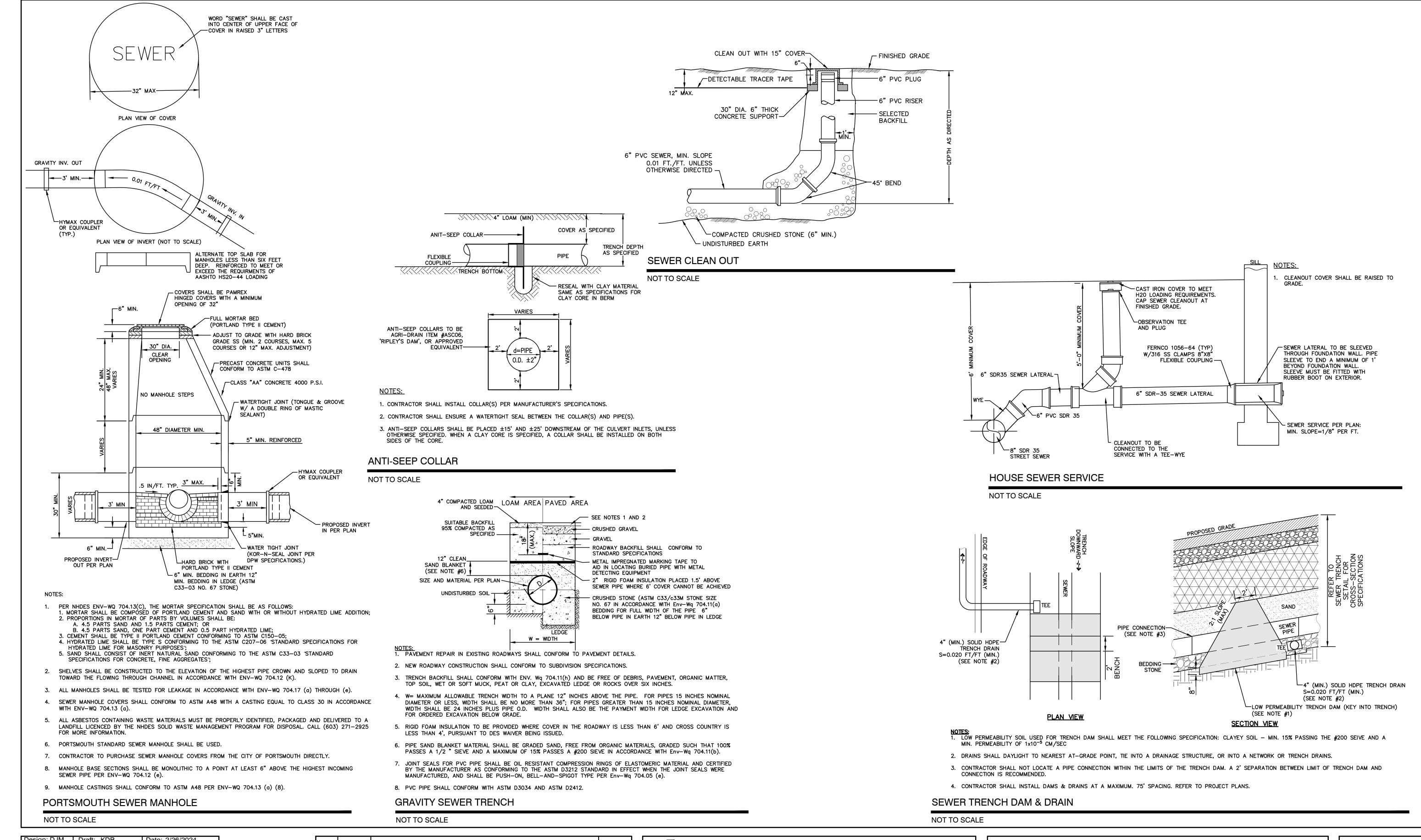
08/20/2024

8/16/24 REVISED PER CITY REVIEW ENGINEER COMMENTS DJM 4/19/24 DJM **REVISED PER TAC COMMENTS** KDR 3/18/24 ISSUED FOR REVIEW **REVISION** BY REV. DATE

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PO Box 219 E-MAIL: JBE@JONESANDBEACH.COM Stratham, NH 03885

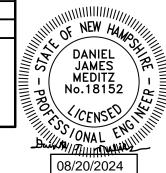
635 SAGAMORE DEVELOPMENT LLC Owner of Record 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158



Design: DJM Draft: KDR Date: 2/26/2024
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REV.	DATE	REVISION	BY

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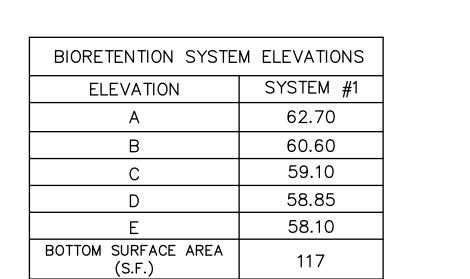
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Stratham, NH 03885

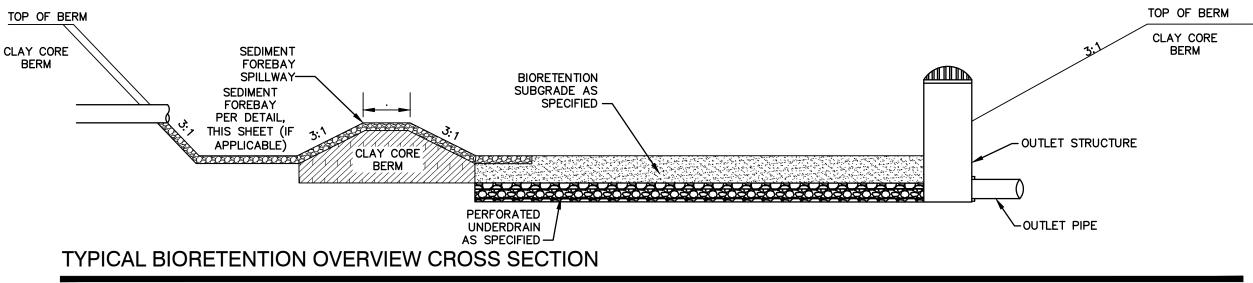
E-MAIL: JBE@JONESANDBEACH.COM

Plan Name:	DETAIL SHEET
Project:	LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH
Owner of Record;	635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

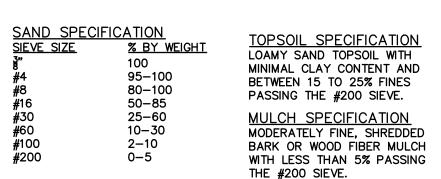
D3

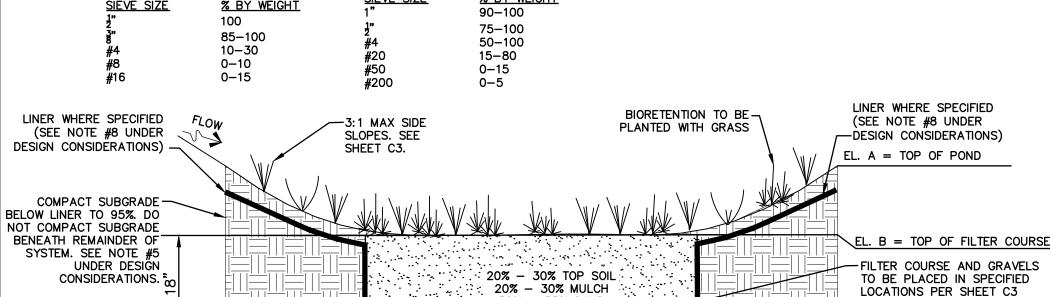
SHEET 17 OF20
JBE PROJECT NO. 18134.1





NOT TO SCALE





50% - 55% SAND

-6" PERFORATED

HDPE UNDERDRAIN

(INVERT PER PLAN)

PEA GRAVEL
COARSE
CRAVEL

% BY WEIGHT

COARSE GRAVEL SPECIFICATION

SIEVE SIZE

DESIGN CONSIDERATIONS

- DO NOT PLACE BIORETENTION SYSTEMS INTO SERVICE UNTIL THE BMP HAS BEEN SEEDED AND ITS CONTRIBUTING AREAS HAVE BEEN FULLY STABILIZED.
- 2. DO NOT DISCHARGE SEDIMENT-LADEN WATERS FROM CONSTRUCTION ACTIVITIES (RUN-OFF, WATER FROM EXCAVATIONS) TO THE BIORETENTION AREA DURING ANY STAGE OF CONSTRUCTION.
- 3. DO NOT TRAFFIC EXPOSED SOIL SURFACE WITH CONSTRUCTION EQUIPMENT. IF FEASIBLE, PERFORM EXCAVATIONS WITH EQUIPMENT OUTSIDE THE LIMITS OF THE INFILTRATION COMPONENTS OF THE SYSTEM.
- 4. REMOVE LEDGE TO AT LEAST TWO FEET BELOW BOTTOM OF COARSE GRAVEL LAYER IF ENCOUNTERED.
- 5. IN ADDITION TO DESIGN CRITERIA LISTED HERE, REFER TO GUIDELINES LISTED IN UNIVERSITY OF NEW
- HAMPSHIRE (UNH) STORMWATER CENTER BIORETENTION SOIL SPECIFICATION. UPSTREAM DEEP SUMP CATCH BASINS PROVIDE PRE-TREATMENT IN LIEU OF A SEDIMENT FOREBAY.
- 8. ONLY PLACE FILTER MEDIA AND STONE BENEATH DOTTED HATCH AREA ON SHEET C3. REMAINDER OF POND TO BE LINED WITH 30ML LINER 6" BELOW SURFACE. FILTER MEDIA AND STONE SECTIONS ARE NOT TO BE LINED. LINER SHALL CONTINUE DOWN THE SIDES OF THE FILTER COURSE BUT MUST NOT BE PLACED ON THE SIDES OF THE PEA GRAVEL OR COARSE GRAVEL OR PLACED BENEATH THE FILTER COURSE AND/OR GRAVELS.
- THE EXISTING NATIVE SUBGRADE MATERIAL SHALL NOT BE COMPACTED OR SUBJECT TO EXCESSIVE CONSTRUCTION EQUIPMENT TRAFFIC PRIOR TO STONE PLACEMENT. IF SOIL MEDIA OR SUBGRADE IS OVER COMPACTED, DISTURBED, OR CONTAMINATED BY FOREIGN OR DELETERIOUS MATERIALS OR LIQUIDS, REMOVE THE SOIL MEDIA AND CONTAMINATION; RESTORE THE SUBGRADE AS DIRECTED BY ENGINEER AND REPLACE CONTAMINATED SOIL MEDIA WITH NEW SOIL MEDIA.

MAINTENANCE REQUIREMENTS:

- SYSTEMS SHALL BE INSPECTED AT LEAST TWICE ANNUALLY, AND FOLLOWING ANY RAINFALL EVENT EXCEEDING 2.5 INCHES IN A 24 HOUR PERIOD, WITH MAINTENANCE OR REHABILITATION CONDUCTED AS WARRANTED BY SUCH
- PRETREATMENT MEASURES SHALL BE INSPECTED AT LEAST TWICE ANNUALLY, AND CLEANED OF ACCUMULATED SEDIMENT AS WARRANTED BY INSPECTION, BUT NO LESS THAN ONCE ANNUALLY.
- TRASH AND DEBRIS SHALL BE REMOVED AT EACH INSPECTION.
- AT LEAST ONCE ANNUALLY, SYSTEM SHALL BE INSPECTED FOR DRAWDOWN TIME. IF BIORETENTION SYSTEM DOES NOT DRAIN WITHIN 72 HOURS FOLLOWING A RAINFALL EVENT, THEN A QUALIFIED PROFESSIONAL SHALL ASSESS THE CONDITION OF THE FACILITY TO DETERMINE MEASURES REQUIRED TO RESTORE FILTRATION FUNCTION, INCLUDING BUT NOT LIMITED TO REMOVAL OF ACCUMULATED SEDIMENTS OR RECONSTRUCTION OF THE FILTER
- 8. VEGETATION SHALL BE INSPECTED AT LEAST ANNUALLY, AND MAINTAINED IN HEALTHY CONDITION, INCLUDING PRUNING, REMOVAL AND REPLACEMENT OF DEAD OR DISEASED VEGETATION, AND REMOVAL OF INVASIVE SPECIES.
- COMPACTION AND MATERIALS TESTING SERVICES SHALL BE PERFORMED BY AN INDEPENDENT GEOTECHNICAL ENGINEER RETAINED BY THE OWNER.

Durky / FILLING THATHALL 08/20/2024

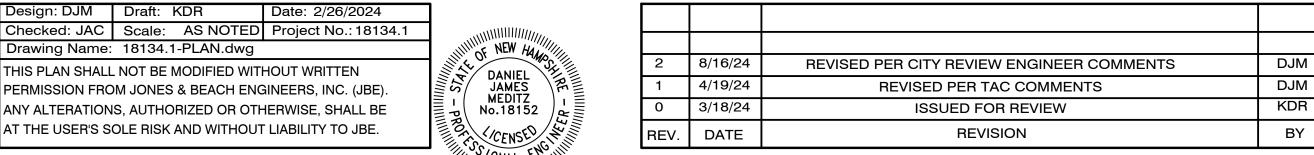
BIORETENTION SYSTEM WITH UNDERDRAIN

NOT TO SCALE

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Drawing Name: 18134.1-PLAN.dwg

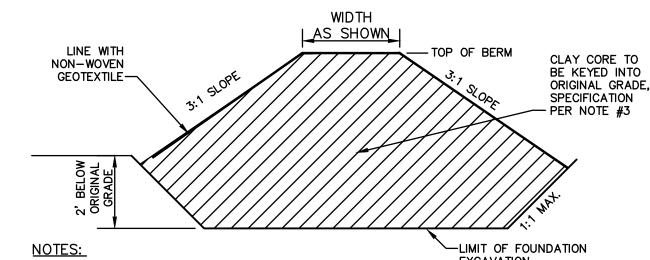
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EL. C = FILTER COURSE

EL. D = PEA GRAVEL

RIP RAP -D50 = 3" - PROPEX GEOTEX WS-200ST GEOTEXTILE FABRIC OR APPROVED EQUAL 6" THICK IMPERVIOUS One ha ha ha ha ha -CLAY LINER SPILLWAY SECTION RIP RAP $D50 = 3" \neg$ WATER FLOW ~**~**→ 220220220220220 SEDIMENT FOREBAY 046046046046046046046046046046 CLAY CORE BERM POND AREA PROPEX GEOTEX WS-200ST GEOTEXTILE FABRIC OR APPROVED EQUAL CLAY LINER LEXTEND RIP RAP 5' MIN. INTO POND AREA SPILLWAY PROFILE SEDIMENT FOREBAY SPILLWAY NOT TO SCALE



EXCAVATION BERM SHALL BE CONSTRUCTED WITH A CLAY CORE TO BE KEYED INTO ORIGINAL GRADE, AS WELL AS A FINE GEOTEXTILE, TO AVOID WATER SEEPAGE AND SOIL PIPING THROUGH THE EARTHEN DIVIDER

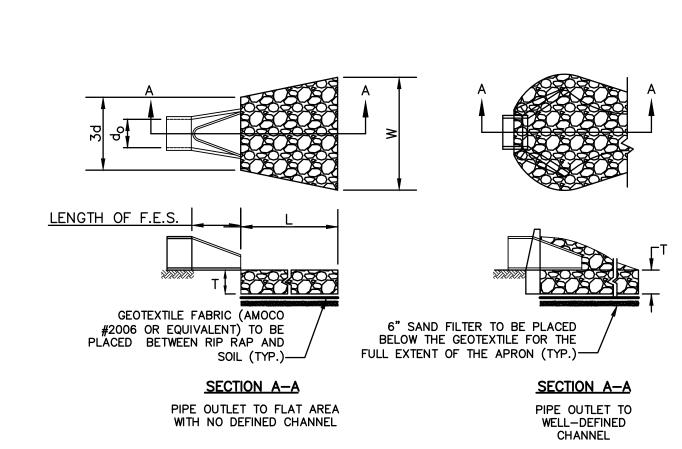
- 2. THE ENTIRE EMBANKMENT AREA OF THE BIORETENTION AREA SHALL BE EXCAVATED A MINIMUM 2 BELOW THE ORIGINAL GRADE, STRIPPED OF ALL ORGANIC MATERIALS, COMPACTED TO AT LEAST 92% OF ASTM D-1557, AND SCARIFIED PRIOR TO THE PLACEMENT OF THE EMBANKMENT MATERIAL. PLACEMENT AND COMPACTION SHOULD OCCUR AT A MOISTURE CONTENT OF OPTIMUM PLUS OR MINUS 3%, AND NO FROZEN OR ORGANIC MATERIAL SHALL BE PLACED FOR ANY REASON.
- 3. CLAY CORE MATERIAL SHALL BE CLEAN SILTY-CLAY BORROW FREE OF ROOTS, ORGANIC MATTER, AND OTHER DELETERIOUS SUBSTANCES, AND SHALL CONTAIN NO ROCKS OR LUMPS OVER THREE INCHES (3") IN DIAMETER. THIS MATERIAL SHALL BE INSTALLED IN 6" LIFTS COMPACTED TO 92% OF ASTM D-1557. AND SHALL MEET THE FOLLOWING SPECIFICATIONS: 6" PASSING 100%, #4 SIEVE 95-100%, #40 SIEVE 60-90%, #100 SIEVE 40-60%, #200 SIEVE 25-45% (OF THE FRACTION PASSING THE #4 SIEVE). THE CLAY COMPONENT SHALL HAVE A PLASTICITY INDEX OF AT LEAST 8 AND A HYDRAULIC CONDUCTIVITY OF 10 TO THE -6 CM/SEC.

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- 4. COMPACTION AND MATERIALS TESTING SERVICES SHALL BE PERFORMED BY AN INDEPENDENT GEOTECHNICAL ENGINEER RETAINED BY THE OWNER.
- 5. REMOVE LEDGE TO AT LEAST 2' OUTSIDE OF AND BELOW LIMITS OF CLAY CORE.

CLAY CORE BERM

NOT TO SCALE



- 8" - 30" DOME GRATES SHALL BE DUCTILE IRON PER ASTM A536

OF A PVC BODY TOP. SEE DRAWING NO. 7001-110-045.

4 - DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO

RESTRICTIONS. SEE DRAWING NO. 7001-110-065.

N-12 HP, & PVC SEWER (4" - 24").

RIM ELAVTION OF STRUCTURE

(5) ADAPTER ANGLES VARIABLE

0° - 360° ACCORDING TO PLANS

4" MIN ON 8"-24"

6" MIN ON 30"

REFERS TO THIS POINT

6 - 8" - 30" DOME GRATES HAVE NO LOAD RATING.

- DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN

8" & 10" DOME GRATES FIT ONTO THE DRAIN BASINS WITH THE USE

DETAILS. RISERS ARE NEEDED FOR BASINS OVER 84" DUE TO SHIPPING

ASTM D3212 FOR CORRUGATED HDPE (ADS N-12/HANCOR DUAL WALL),

(3) VARIABLE SUMP DEPTH

ACCORDING TO PLANS

(6" MIN. ON 8"-24", 10" MIN. ON 30"

BASED ON MANUFACTURING REQ.)

THE BACKFILL MATERIAL SHALL BE CRUSHED STONE

REQUIREMENTS OF CLASS I, CLASS II, OR CLASS III

INTLETS SHALL BE PLACED & COMPACTED UNIFORMLY

OR OTHER GRANULAR MATERIAL MEETING THE

BEDDING & BACKFILL FOR SURFACE DRAINAGE

MATERIAL AS DEFINED IN ASTM D2321.

IN ACCORDANCE WITH ASTM D2321.

- ADAPTERS CAN BE MOUNTED ON ANY ANGLE 0° TO 360°. TO DETERMINE MINIMUM ANGLE BETWEEN ADAPTERS SEE DRAWING NO. 7001-110-012.

GRADE 70-50-05.

(1, 2) INTEGRATED DUCTILE IRON

MINIMUM PIPE BURIAL DEPTH PER PIPE

MANUFACTURER

RECOMMENDATION

(MIN. MANUFACTURING

REQ. SAME AS MIN. SUMP)

WATERTIGHT JOINT -

24" DIA. NYLOPLAST DRAIN BASIN (YARD DRAIN & POND OUTLET STRUCTURE SPECIFICATION)

(CORRUGATED HDPE SHOWN)

(4) VARIOUS TYPES OF INLET & OUTLET ADAPTERS -

AVAILABLE: 4" - 30" FOR CORRUGATED HDPE

(ADS N-12/HANCOR DUAL WALL, ADS/HANCOR

(EX: SDR 35), PVC DWV (EX: SCH 40), PVC

C900/C905, CORRUGATED & RIBBED PVC

SINGLE WALL), N-12 HP, PVC SEWER

(3) VARIABLE INVERT HEIGHTS

AVAILABLE (ACCORDING TO

PLANS/TAKE OFF)

NOT TO SCALE

GRATE TO MATCH BASIN O.D. -

TABLE 7-24RE	COMMENDED	RIP RAP GRAI	DATIC	ON RANGES
THICKNESS OF RI	P RAP = 0.	75 FEET		
d50 SIZE=	0.25	FEET	3	INCHES
% OF WEIGHT SMATHAN THE GIVEN		SIZE OF S FROM	STON	E (INCHES) TO
100%		5		6
85%		4		5
50%		3		5
15%		1		2

- 1. THE SUBGRADE FOR THE GEOTEXTILE FABRIC AND RIP RAP SHALL BE PREPARED TO THE LINES AND GRADES SHOWN ON THE PLANS.
- 2. THE RIP RAP SHALL CONFORM TO THE SPECIFIED GRADATION.
- 3. GEOTEXTILE FABRICS SHALL BE PROTECTED FROM PUNCTURE OR TEARING DURING THE PLACEMENT OF THE ROCK RIP. DAMAGED AREAS IN THE FABRIC SHALL BE REPAIRED BY PLACING A PIECE OF FABRIC OVER THE DAMAGED AREA OR BY COMPLETE REPLACEMENT OF THE FABRIC. ALL OVERLAPS REQUIRED FOR REPAIRS OR JOINING TWO PIECES OF FABRIC SHALL BE A MINIMUM OF 12 INCHES.
- 4. STONE FOR THE RIP RAP MAY BE PLACED BY EQUIPMENT AND SHALL BE CONSTRUCTED TO THE FULL LAYER THICKNESS IN ONE OPERATION AND IN SUCH A MANNER AS TO PREVENT SEGREGATION OF THE
- 5. OUTLETS TO A DEFINED CHANNEL SHALL HAVE 2:1 OR FLATTER SIDE SLOPES AND SHOULD BEGIN AT THE TOP OF THE CULVERT AND TAPER DOWN TO THE CHANNEL BOTTOM THROUGH THE LENGTH OF THE
- 6. <u>MAINTENANCE</u>; THE OUTLET PROTECTION SHOULD BE CHECKED AT LEAST ANNUALLY AND AFTER EVERY MAJOR STORM. IF THE RIP RAP HAS BEEN DISPLACED, UNDERMINED OR DAMAGED, IT SHOULD BE REPAIRED IMMEDIATELY. THE CHANNEL IMMEDIATELY BELOW THE OUTLET SHOULD BE CHECKED TO SEE THAT EROSION IS NOT OCCURRING. THE DOWNSTREAM CHANNEL SHOULD BE KEPT CLEAR OF OBSTRUCTIONS SUCH AS FALLEN TREES, DEBRIS, AND SEDIMENT THAT COULD CHANGE FLOW PATTERNS AND/OR TAILWATER DEPTHS ON THE PIPES. REPAIRS MUST BE CARRIED OUT IMMEDIATELY TO AVOID ADDITIONAL DAMAGE TO OUTLET PROTECTION.

RIP RAP OUTLET PROTECTION APRON

NOT TO SCALE

		Designed and Produced in NH
		D Jones & Rosch Engineers
REVISED PER CITY REVIEW ENGINEER COMMENTS	DJM	🎱 🖊 🏲 Jones & Beach Engineers
REVISED PER TAC COMMENTS	DJM	
ISSUED FOR REVIEW	KDR	85 Portsmouth Ave. Civil Engineering Services

PO Box 219

Stratham, NH 03885

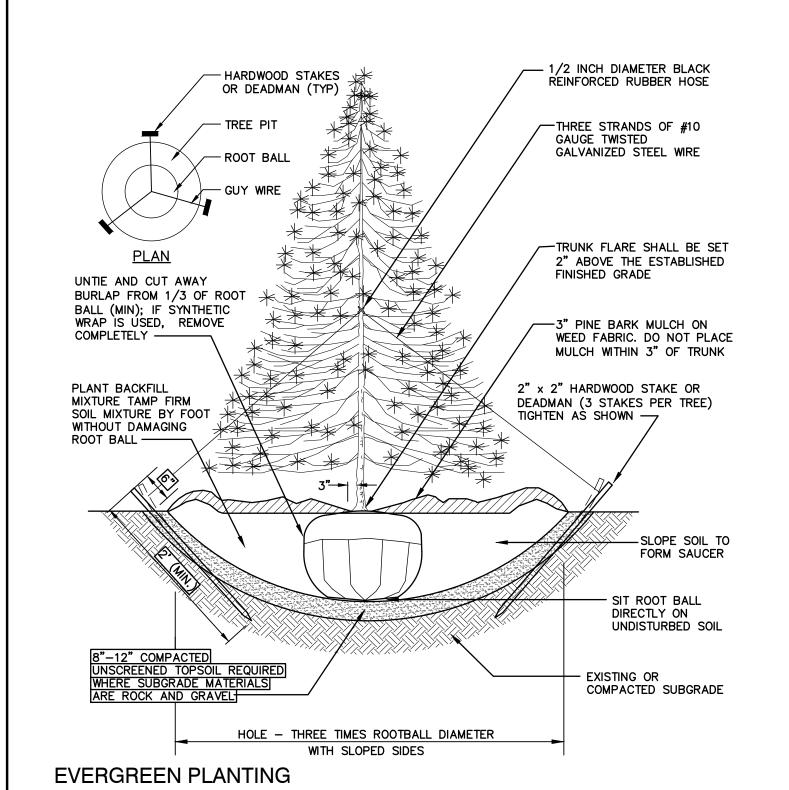
s, Inc. Project: 603-772-4746

Plan Name:

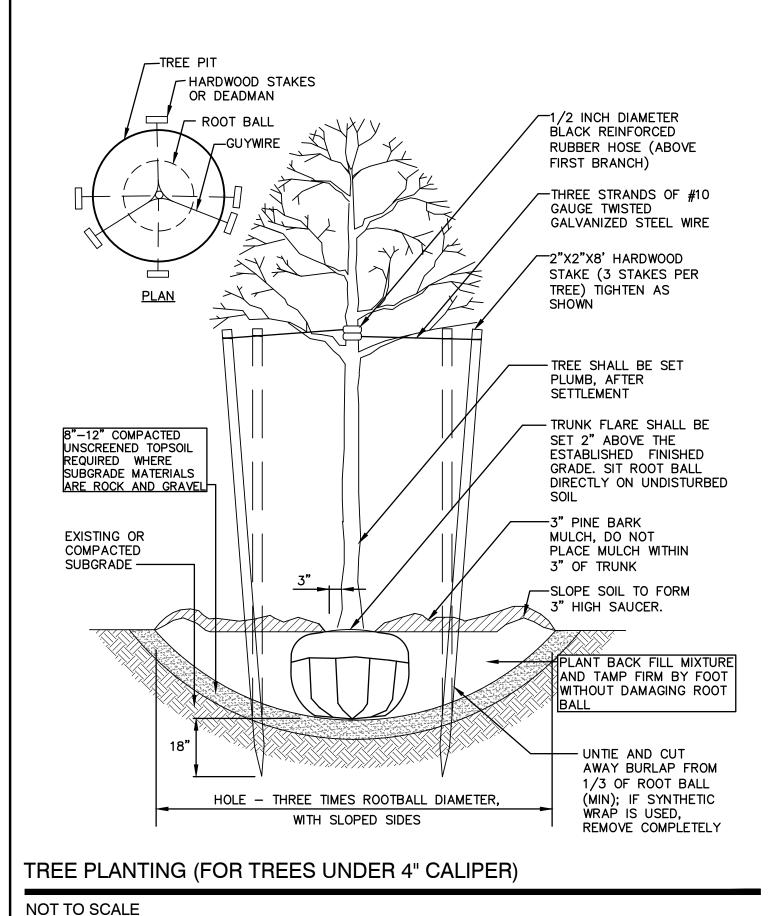
DETAIL SHEET LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH 635 SAGAMORE DEVELOPMENT LLC

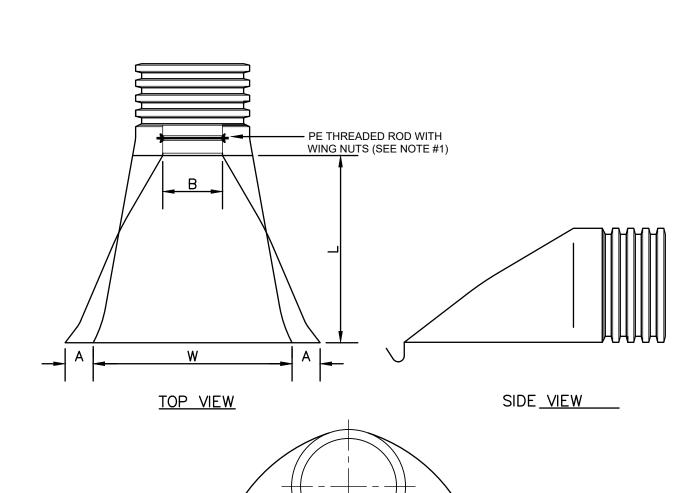
Owner of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

SHEET 18 OF 20 JBE PROJECT NO. 18134.1



NOT TO SCALE





PART NO.	PIPE SIZE	А	B (MAX)	Н	L	W
1210-NP	12"	6.5"	10"	6.5"	25"	29"
1510-NP	15"	6.5"	10"	6.5"	25"	29"
1810-NP	18"	7.5"	15"	6.5"	32"	35"
2410-NP	24"	7.5"	18"	6.5"	36"	45"
3010-NP	30"	10.5"	N/A	7.0"	53"	68"
3610-NP	36"	10.5"	N/A	7.0"	53"	68"

FRONT VIEW

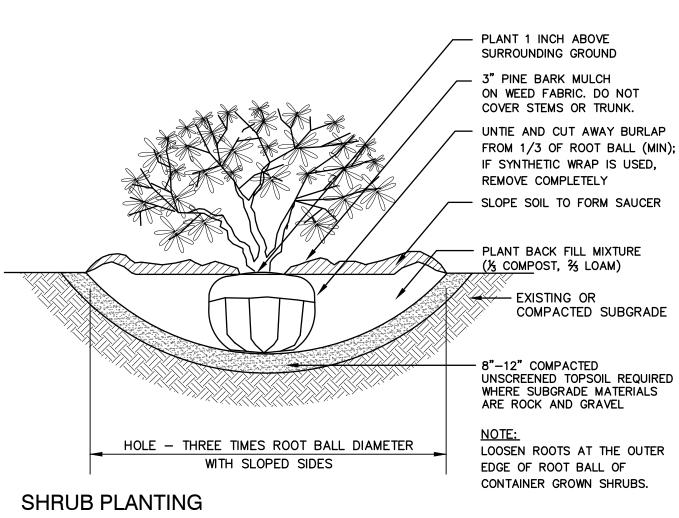
NOTES:

- 1. PE THREADED ROD WITH WING NUTS PROVIDED FOR END SECTIONS 12"-24".

 30" AND 36" END SECTIONS TO BE WELDED PER MANUFACTURER'S RECOMMENDATIONS.
- 2. ALL DIMENSIONS ARE NOMINAL.

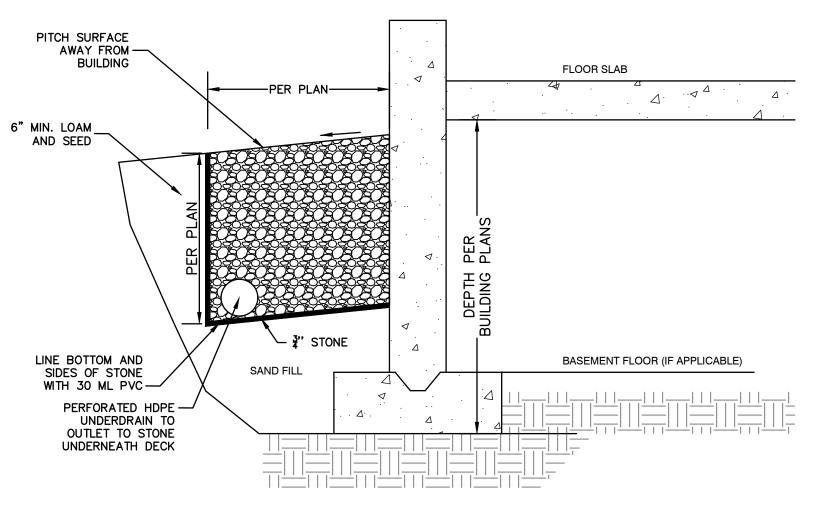
ADS N-12 FLARED END SECTION

NOT TO SCALE



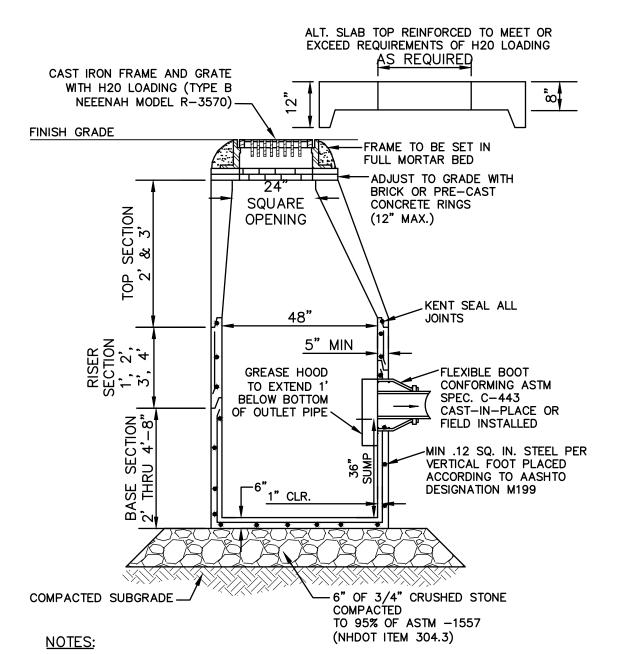
SHRUB PLANTING

NOT TO SCALE



LINED STONE DRIP EDGE DETAIL

NOT TO SCALE



- 1. BASE SECTION SHALL BE MONOLITHIC WITH 48" INSIDE DIAMETER.
- 2. ALL SECTIONS SHALL BE DESIGNED FOR H20 LOADING.
- 3. CONCRETE SHALL BE COMPRESSIVE STRENGTH 4000 PSI, TYPE II CEMENT.
- 4. FRAMES AND GRATES SHALL BE HEAVY DUTY AND DESIGNED FOR H20 LOADING
- 5. PROVIDE "V" KNOCKOUTS FOR PIPES WITH 2" MAX. CLEARANCE TO OUTSIDE OF PIPE. MORTAR ALL PIPE CONNECTIONS SO AS TO BE WATERTIGHT.
- 6. JOINT SEALANT BETWEEN PRECAST SECTIONS SHALL BE BUTYL RUBBER.
- 7. STANDARD CATCH BASIN FRAME AND GRATE(S) SHALL BE SET IN FULL MORTAR BED. ADJUST TO GRADE WITH CLAY BRICK AND MORTAR (2 BRICK COURSES TYPICALLY, 5 BRICK COURSES MAXIMUM, BUT NO MORE THAN 12"), OR PRECAST CONCRETE 'DONUTS'.
- 8. CATCH BASINS SHALL HAVE A 36" MINIMUM SUMP AS SHOWN.

 CATCH BASIN

NOT TO SCALE

HOUSE PER ARCHITECTURAL / STRUCTURAL PLÁNS DECK PER ARCHITECTURAL PLANS F.F. PER SHEET C3 EXTERNAL WALL SHOWN STAIRS HEREON IS FOR ILLUSTRATIVE PURPOSES ONLY. REFER TO WATER TO SEEP THROUGH SLOTTED OPENINGS IN BUILDING PLANS FOR WOODEN DECK -WALL DESIGN. -WOODEN WALL AT LEAST MINIMUM EXPOSED CONCRETE AT WALKOUT PER CODE -BASEMENT FLOOR SURFACE AWAY FROM 2" CLEAN CONTROL WASHED STONE CONTROL OF CON CONCRETE FROST WALL CONTINUE STONE UNDERNEATH STAIRS - UNDERDRAIN FROM DRIP ~BACKFILL MATERIAL NON-WOVEN GEOTEXTILE ON BOTTOM AND SIDES OF OPEN-GRADED BASE SHALL BE SUITABLE * INFILTRATION STONE SHALL BE PLACED UNDER FOR BOTH INFILTRATION AND DECK POSTS DECKS AND STAIRS AS SHOWN ON SHEET C3 INFILTRATION STONE UNDERNEATH DECK NOT TO SCALE SECTION A-A

12"	
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	DIA.	HEADWALL LENGTH	HEADWALL HEIGHT	FILL HEIGHT	PIPE COVER	HEADWALL BOTTOM WIDTH
	D	L	Н	FH	h	W
	12"	4'-2"	3'-9"	1'-6"	1'-3"	1'-11"
	15"	5'-11"	4'-2"	1'-6"	1'-5"	2'-0"
	18"	6'-11"	4'-5"	1'-6"	1'-5"	2'-1"
	24"	8'-10"	4'-11"	1'-6"	1'-5"	2'-3"
•						

LONGITUDINAL SECTION

1. ALL DIMENSIONS GIVEN IN FEET & INCHES.

- 2. PROVIDE BELL END AT INLET HEADWALL, AND SPIGOT END AT OUTLET END HEADWALL. 3. CONCRETE: 5,000 PSI MINIMUM AFTER 28 DAYS. CEMENT TO BE TYPE III PER ASTM
- C-150. REINFORCING TO MEET OR EXCEED ASTM A-615 GRADE 60 DEFORMED BARS.

 4. 1" THREADED INSERTS PROVED FOR FINAL ATTACHMENT IN FIELD BY OTHERS.

PRECAST CONCRETE HEADWALL

NOT TO SCALE

Design: DJM Draft: KDR Date: 2/26/2024
Checked: JAC Scale: AS NOTED Project No.: 18134.1
Drawing Name: 18134.1-PLAN.dwg
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN
PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).
ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE

AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

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		08/20/2024	

2	8/16/24	REVISED PER CITY REVIEW ENGINEER COMMENTS	DJM
1	4/19/24	REVISED PER TAC COMMENTS	DJM
0	3/18/24	ISSUED FOR REVIEW	KDR
REV.	DATE	REVISION	BY

Designed and Produced in NH Jones & Beach Engineers, Inc.

85 Portsmouth Ave. PO Box 219
Stratham, NH 03885

Civil Engineering Services

E-MAIL: JBE@JONESANDBEACH.COM

Plan Name:	DETAIL SHEET				
Project:	LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH				
635 SAGAMORE DEVELOPMENT LLC Owner of Record;3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 115					

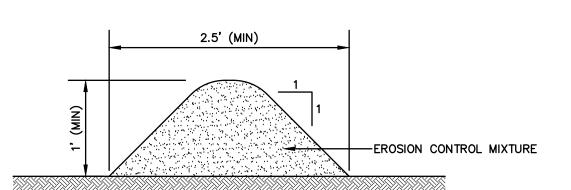
DRAWING No.

D5

SHEET 19 OF 20
JBE PROJECT NO. 18134.1

TEMPORARY EROSION CONTROL NOTES

- THE SMALLEST PRACTICAL AREA OF LAND SHALL BE EXPOSED AT ANY ONE TIME. AT NO TIME SHALL AN AREA IN EXCESS OF 5 ACRES BE EXPOSED AT ANY ONE TIME BEFORE DISTURBED AREAS ARE STABILIZED.
- EROSION, SEDIMENT AND DETENTION MEASURES SHALL BE INSTALLED AS SHOWN ON THE PLANS AND AT LOCATIONS AS REQUIRED, DIRECTED BY THE ENGINEER.
- 3. ALL DISTURBED AREAS (INCLUDING POND AREAS BELOW THE PROPOSED WATERLINE) SHALL BE RETURNED TO PROPOSED GRADES AND ELEVATIONS. DISTURBED AREAS SHALL BE LOAMED WITH A MINIMUM OF 6" OF SCREENED ORGANIC LOAM AND SEEDED WITH SEED MIXTURE 'C' AT A RATE NOT LESS THAN 1.10 POUNDS OF SEED PER 1,000 S.F. OF AREA (48 LBS. / ACRE).
- SILT FENCES AND OTHER BARRIERS SHALL BE INSPECTED EVERY SEVEN CALENDAR DAYS AND WITHIN 24 HOURS OF A RAINFALL OF 0.5" OR GREATER. ALL DAMAGED AREAS SHALL BE REPAIRED, AND SEDIMENT DEPOSITS SHALL PERIODICALLY BE REMOVED
- AFTER ALL DISTURBED AREAS HAVE BEEN STABILIZED, THE TEMPORARY EROSION CONTROL MEASURES SHALL BE REMOVED AND THE AREA DISTURBED BY THE REMOVAL SMOOTHED AND RE-VEGETATED.
- AREAS MUST BE SEEDED AND MULCHED OR OTHERWISE PERMANENTLY STABILIZED WITHIN 3 DAYS OF FINAL GRADING, OR TEMPORARILY STABILIZED WITHIN 14 DAYS OF THE INITIAL DISTURBANCE OF SOIL. ALL AREAS SHALL BE STABILIZED WITHIN 45
- ALL PROPOSED VEGETATED AREAS THAT DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED BY SEEDING AND INSTALLING NORTH AMERICAN GREEN S75 EROSION CONTROL BLANKETS (OR AN EQUIVALENT APPROVED IN WRITING BY THE ENGINEER) ON SLOPES GREATER THAN 3:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT EVENTS.
- ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15. OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS.
- AFTER OCTOBER 15th, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3" OF CRUSHED GRAVEL PER NHDOT ITEM 304.3.
- 10. AN AREA SHALL BE CONSIDERED STABLE IF ONE OF THE FOLLOWING HAS OCCURRED:
 - a. BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED;
 - b. A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED;
 - c. A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH STONE OR RIPRAP HAS BEEN INSTALLED; OR
 - d. EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.
- 11. FUGITIVE DUST CONTROL IS REQUIRED TO BE CONTROLLED IN ACCORDANCE WITH ENV-A 1000, AND THE PROJECT IS TO MEET THE REQUIREMENTS AND INTENT OF RSA 430:53 AND AGR 3800 RELATIVE TO INVASIVE SPECIES.



- 1. ORGANIC FILTER BERMS SHALL BE UTILIZED IN LIEU OF SILT FENCE.
- 2. THE EROSION CONTROL MIX USED IN THE FILTER BERMS SHALL BE A WELL-GRADED MIXTURE OF PARTICLE SIZES. MAY CONTAIN ROCKS LESS THAN 4" IN DIAMETER. STUMP GRINDINGS. SHREDDED OR COMPOSTED BARK, OR ACCEPTABEL MANUFACTURED PRODUCTS, AND SHALL BE FREE OF REFUSE, PHYSICAL CONTAMINANTS, AND MATERIAL TOXIC TO PLANT GROWTH, AND SHALL MEET THE FOLLOWING STANDARDS:
- a) THE ORGANIC CONTENT SHALL BE 25-65% OF DRY WEIGHT.
- b) PARTICLE SIZE BY WEIGHT SHALL BE 100% PASSING A 3" SCREEN, 90-100% PASSING A 1" SCREEN, 70-100& PASSING A 0.75" SCREEN, AND 30-75% PASSING A 0.25"
- c) THE ORGANIC PORTION SHALL BE FIBROUS AND ELONGATED. d) LARGE PORTIONS OF SILTS, CLAYS, OR FINE SANDS SHALL NOT BE INCLUDED IN THE
- e) SOLUBLE SALTS CONTENT SHALL BE >4.0mmhos/cm. f) THE pH SHALL BE BETWEEN 5.0 AND 8.0.
- 3. ORGANIC FILTER BERMS SHALL BE INSTALLED ALONG A RELATIVELY LEVEL CONTOUR. IT MAY BE NECESSARY TO CUT TALL GRASSES OR WOODY VEGETATION TO AVOID CREATING VOIDS AND BRIDGES THAT WOULD ENABLE FINES TO WASH UNDER THE BERM.
- 4. ON SLOPES LESS THAN 5%, OR AT THE BOTTOM OF SLOPES STEEPER THAN 3:1, UP TO 20' LONG, THE BERM SHALL BE A MINIMUM OF 12" HIGH (AS MEASURED ON THE UPHILL SIDE), AND A MINIMUM OF 36" WIDE. ON LONGER OR STEEPER SLOPES, THE BERM SHALL BE WIDER TO ACCOMMODATE THE POTENTIAL ADDITIONAL RUNOFF.
- 5. FROZEN GROUND, OUTCROPS OF BEDROCK, AND VERY ROOTED FORESTED AREAS PRESENT THE MOST PRACTICAL AND EFFECTIVE LOCATIONS FOR ORGANIC FILTER BERMS. OTHER BMP'S SHOULD BE USED AT LOW POINTS OF CONCENTRATED RUNOFF, BELOW CULVERT OUTLET APRONS, AROUND CATCH BASINS, AND AT THE BOTTOM OF STEEP PERIMETER SLOPES THAT HAVE A LARGE CONTRIBUTING AREA.
- 6. SEDIMENT SHALL BE REMOVED FROM BEHIND THE STRUCTURES WHEN IT HAS ACCUMULATED TO ONE HALF THE ORIGINAL HEIGHT OF THE STRUCTURE.
- 7. STRUCTURES MAY BE LEFT IN PLACE ONCE THE SITE IS STABILIZED.

ORGANIC FILTER BERM / FIBER BERM

OF NEW HAMP DANIEL JAMES No.18152 CENSED MAL. Durky / ATHINT NAMEDY

| 8/16/24 REVISED PER CITY REVIEW ENGINEER COMMENTS DJM DJM 4/19/24 **REVISED PER TAC COMMENTS** KDR 3/18/24 ISSUED FOR REVIEW **REVISION** BY REV. DATE

SEEDING SPECIFICATIONS

- GRADING AND SHAPING A. SLOPES SHALL NOT BE STEEPER THAN 2:1 WITHOUT APPROPRIATE EROSION CONTROL MEASURES AS
- SPECIFIED ON THE PLANS (3:1 SLOPES OR FLATTER ARE PREFERRED). B. WHERE MOWING WILL BE DONE, 3:1 SLOPES OR FLATTER ARE RECOMMENDED.

2. <u>SEEDBED PREPARATION</u>

- A. SURFACE AND SEEPAGE WATER SHOULD BE DRAINED OR DIVERTED FROM THE SITE TO PREVENT DROWNING
- OR WINTER KILLING OF THE PLANTS. B. STONES LARGER THAN 4 INCHES AND TRASH SHOULD BE REMOVED BECAUSE THEY INTERFERE WITH SEEDING AND FUTURE MAINTENANCE OF THE AREA. WHERE FEASIBLE, THE SOIL SHOULD BE TILLED TO A DEPTH OF ABOUT 4 INCHES TO PREPARE A SEEDBED AND FERTILIZER AND LIME MIXED INTO THE SOIL. THE SEEDBED SHOULD BE LEFT IN A REASONABLY FIRM AND SMOOTH CONDITION. THE LAST TILLAGE OPERATION SHOULD BE PERFORMED ACROSS THE SLOPE WHEREVER PRACTICAL.

3. ESTABLISHING A STAND

- A. LIME AND FERTILIZER SHOULD BE APPLIED PRIOR TO OR AT THE TIME OF SEEDING AND INCORPORATED INTO THE SOIL. TYPES AND AMOUNTS OF LIME AND FERTILIZER SHOULD BE BASED ON AN EVALUATION OF SOIL TESTS. WHEN A SOIL TEST IS NOT AVAILABLE, THE FOLLOWING MINIMUM AMOUNTS SHOULD BE
- AGRICULTURAL LIMESTONE, 2 TONS PER ACRE OR 100 LBS. PER 1,000 SQ.FT. NITROGEN(N), 50 LBS. PER ACRE OR 1.1 LBS. PER 1,000 SQ.FT.
- PHOSPHATE(P205), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT.
- POTASH(K20), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT. (NOTE: THIS IS THE EQUIVALENT OF 500 LBS. PER ACRE OF 10-20-20 FERTILIZER OR 1,000 LBS. PER
- ACRE OF 5-10-10.) B. SEED SHOULD BE SPREAD UNIFORMLY BY THE METHOD MOST APPROPRIATE FOR THE SITE. METHODS INCLUDE BROADCASTING, DRILLING AND HYDROSEEDING. WHERE BROADCASTING IS USED, COVER SEED WITH
- .25 INCH OF SOIL OR LESS, BY CULTIPACKING OR RAKING. C. REFER TO THE 'SEEDING GUIDE' AND 'SEEDING RATES' TABLES ON THIS SHEET FOR APPROPRIATE SEED MIXTURES AND RATES OF SEEDING. ALL LEGUMES (CROWNVETCH, BIRDSFOOT, TREFOIL AND FLATPEA) MUST BE INOCULATED WITH THEIR SPECIFIC INOCULANT PRIOR TO THEIR INTRODUCTION TO THE SITE.
- D. WHEN SEEDED AREAS ARE MULCHED, PLANTINGS MAY BE MADE FROM EARLY SPRING TO EARLY OCTOBER WHEN SEEDED AREAS ARE NOT MULCHED, PLANTINGS SHOULD BE MADE FROM EARLY SPRING TO MAY 20th OR FROM AUGUST 10th TO SEPTEMBER 1st.

EXISTING

BERM (OPTIONAL)

- EXISTING

PAVEMENT-

-MOUNTABLE

PAVEMENT

50' MINIMUM

(75 W/O MOUNTABLE BERM)

6" MIN.-

(75' W/O MOUNTABLE BERM)

1. STONE FOR STABILIZED CONSTRUCTION ENTRANCE SHALL BE 3 INCH STONE, RECLAIMED

WITHOUT A MOUNTABLE BERM, AND EXCEPT FOR A SINGLE RESIDENTIAL LOT WHERE A 30

3. THICKNESS OF THE STONE FOR THE STABILIZED ENTRANCE SHALL NOT BE LESS THAN 6

ENTRANCE WHERE INGRESS OR EGRESS OCCURS, OR 10 FEET, WHICHEVER IS GREATER.

6. ALL SURFACE WATER THAT IS FLOWING TO OR DIVERTED TOWARD THE CONSTRUCTION ENTRANCE SHALL BE PIPED BENEATH THE ENTRANCE. IF PIPING IS IMPRACTICAL, A STONE

5. GEOTEXTILE FILTER FABRIC SHALL BE PLACED OVER THE ENTIRE AREA PRIOR TO PLACING THE STONE. FILTER FABRIC IS NOT REQUIRED FOR A SINGLE FAMILY RESIDENTIAL LOT.

BERM WITH 5:1 SLOPES THAT CAN BE CROSSED BY VEHICLES MAY BE SUBSTITUTED FOR

FLOWING OF SEDIMENT ONTO THE PUBLIC RIGHT-OF-WAY. THIS MAY REQUIRE PERIODIC TOP

7. THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION THAT WILL PREVENT TRACKING OR

DRESSING WITH ADDITIONAL STONE AS CONDITIONS DEMAND AND REPAIR AND/OR CLEAN OUT OF ANY MEASURES USED TO TRAP SEDIMENT. ALL SEDIMENT SPILLED, WASHED, OR

TRACKED ONTO THE PUBLIC RIGHT-OF-WAY MUST BE REMOVED PROMPTLY.

STABILIZED CONSTRUCTION ENTRANCE

2. THE LENGTH OF THE STABILIZED ENTRANCE SHALL NOT BE LESS THAN 50 FEET, 75'

4. THE WIDTH OF THE ENTRANCE SHALL NOT BE LESS THAN THE FULL WIDTH OF THE

PLAN VIEW

PROFILE

EXISTING GROUND

WOVEN GEOTEXTILE

FILTER FABRIC-

STONE, OR RECYCLED CONCRETE EQUIVALENT.

FOOT MINIMUM LENGTH WOULD APPLY.

NOT TO SCALE

- A. HAY, STRAW, OR OTHER MULCH, WHEN NEEDED, SHOULD BE APPLIED IMMEDIATELY AFTER SEEDING. B. MULCH WILL BE HELD IN PLACE USING APPROPRIATE TECHNIQUES FROM THE BEST MANAGEMENT PRACTICE FOR MULCHING. HAY OR STRAW MULCH SHALL BE PLACED AT A RATE OF 90 LBS PER 1000 S.F.
- 5. MAINTENANCE TO ESTABLISH A STAND
- A. PLANTED AREAS SHOULD BE PROTECTED FROM DAMAGE BY FIRE, GRAZING, TRAFFIC, AND DENSE WEED
- B. FERTILIZATION NEEDS SHOULD BE DETERMINED BY ONSITE INSPECTIONS. SUPPLEMENTAL FERTILIZER IS USUALLY THE KEY TO FULLY COMPLETE THE ESTABLISHMENT OF THE STAND BECAUSE MOST PERENNIALS TAKE 2 TO 3 YEARS TO BECOME FULLY ESTABLISHED.
- C. IN WATERWAYS, CHANNELS, OR SWALES WHERE UNIFORM FLOW CONDITIONS ARE ANTICIPATED, ANNUAL MOWING MAY BE NECESSARY TO CONTROL GROWTH OF WOODY VEGETATION.

USE	SEEDING MIXTURE 1/	DROUGHTY	WELL DRAINED	MODERATELY WELL DRAINED	POORLY DRAINED
STEEP CUTS AND FILLS, BORROW AND DISPOSAL AREAS	A B C	FAIR POOR POOR FAIR	GOOD GOOD GOOD EXCELLENT	GOOD FAIR EXCELLENT EXCELLENT	FAIR FAIR GOOD POOR
WATERWAYS, EMERGENC SPILLWAYS, AND OTHER CHANNELS WITH FLOWING WATER.		GOOD GOOD	GOOD EXCELLENT	GOOD EXCELLENT	FAIR FAIR
LIGHTLY USED PARKING LOTS, ODD AREAS, UNUSED LANDS, AND LOW INTENSITY USE RECREATION SITES.	A B C	GOOD GOOD GOOD	GOOD GOOD EXCELLENT	GOOD FAIR EXCELLENT	FAIR POOR FAIR
PLAY AREAS AND ATHLETIC FIELDS. (TOPSOIL IS ESSENTIAL FOR GOOD TURF.)	E F	FAIR FAIR	EXCELLENT EXCELLENT	EXCELLENT EXCELLENT	<u>2/</u> 2/

GRAVEL PIT, SEE NH-PM-24 IN APPENDIX FOR RECOMMENDATION REGARDING RECLAMATION OF SAND AND GRAVEL PITS.

/ REFER TO SEEDING MIXTURES AND RATES IN TABLE BELOW. 27 POORLY DRAINED SOILS ARE NOT DESIRABLE FOR USE AS PLAYING AREA AND ATHLETIC FIELDS.

NOTE: TEMPORARY SEED MIX FOR STABILIZATION OF TURF SHALL BE WINTER RYE OR OATS AT A RATE OF 2.5 LBS. PER 1000 S.F. AND SHALL BE PLACED PRIOR TO OCTOBER 15th, IF PERMANENT SEEDING NOT

SEEDING GUIDE

MIXTURE	POUNDS PER ACRE	POUNDS PER 1.000 Sq. Ft.,
A. TALL FESCUE CREEPING RED FESCUE RED TOP TOTAL	20 20 <u>2</u> 42	0.45 0.45 <u>0.05</u> 0.95
B. TALL FESCUE CREEPING RED FESCUE CROWN VETCH OR FLAT PEA TOTAL	15 10 15 30 40 OR 55	0.35 0.25 0.35 0.75 0.95 OR 1.35
C. TALL FESCUE CREEPING RED FESCUE BIRDS FOOT TREFOIL TOTAL	20 20 <u>8</u> 48	0.45 0.45 <u>0.20</u> 1.10
D. TALL FESCUE FLAT PEA TOTAL	20 <u>30</u> 50	0.45 <u>0.75</u> 1.20
E. CREEPING RED FESCUE 1/ KENTUCKY BLUEGRASS 1/ TOTAL	50 50 100	1.15 1.15 2.30
F. TALL FESCUE 1	150	3.60
1/FOR HEAVY USE ATHLETIC FIE NEW HAMPSHIRE COOPERATIVE EXCURRENT VARIETIES AND SEEDING	XTENSION TURF SPE	

STONE FILTER RUNOFF WATER WITH SEDIMENT

—CONCRETE BLOCKS

WIRE SCREEN SHALL BE PLACED BETWEEN STONE AND BLOCKS TO

PREVENT THE AGGREGATE FROM BEING WASHED INTO THE STRUCTURE

- WIRE SCREEN

-FILTERED WATER

- DROP INLET WITH GRATE

MAINTENANCE NOTE:

1. ALL STRUCTURES SHOULD BE INSPECTED AFTER EVERY RAINFALL AND REPAIRS MADE AS NECESSARY. SEDIMENT SHOULD BE REMOVED FROM TRAPPING DEVICES AFTER THE SEDIMENT HAS REACHED A MAXIMUM OF ONE HALF THE DEPTH OF THE TRAP. THE SEDIMENT SHOULD BE DISPOSED IN A SUITABLE UPLAND AREA AND PROTECTED FROM EROSION BY EITHER STRUCTURE OR VEGETATIVE MEANS. THE TEMPORARY TRAPS SHOULD BE REMOVED AND THE AREA REPAIRED AS SOON AS THE CONTRIBUTING DRAINAGE AREA TO THE INLET HAS BEEN COMPLETELY STABILIZED.

TEMPORARY CATCH BASIN INLET PROTECTION (Block and Gravel Drop Inlet Sediment Filter)

-SUBGRADE

NOT TO SCALE

CONSTRUCTION SEQUENCE

- PRIOR TO THE START OF ANY ACTIVITY, IT IS THE RESPONSIBILITY OF THE SITE'S SITE DEVELOPER (OR OWNER) TO FILE A NOTICE OF INTENT (NOI) FORM WITH THE ENVIRONMENTAL PROTECTION AGENCY (EPA) IN ORDER TO GAIN COVERAGE UNDER THE NPDES GENERAL PERMIT FOR STORM WATER DISCHARGES FROM CONSTRUCTION ACTIVITIES. A PRE CONSTRUCTION MEETING IS TO BE HELD WITH ALL DEPARTMENT HEADS PRIOR TO THE START OF CONSTRUCTION.
- 2. CUT AND REMOVE TREES IN CONSTRUCTION AREA AS REQUIRED OR DIRECTED.
- 3. INSTALL FIBER BERM, HAY BALES AND CONSTRUCTION ENTRANCES PRIOR TO THE START OF CONSTRUCTION. THESE ARE TO BE MAINTAINED UNTIL THE FINAL PAVEMENT SURFACING AND LANDSCAPING AREAS ARE ESTABLISHED.
- CLEAR, CUT, GRUB AND DISPOSE OF DEBRIS IN APPROVED FACILITIES. THIS INCLUDES ANY REQUIRED DEMOLITION OF EXISTING STRUCTURES, UTILITIES, ETC.
- 5. CONSTRUCT AND/OR INSTALL TEMPORARY OR PERMANENT SEDIMENT AND/OR DETENTION BASIN(S) AS REQUIRED. THESE FACILITIES SHALL BE INSTALLED AND STABILIZED PRIOR TO DIRECTING RUN-OFF TO THEM.
- 6. STRIP LOAM AND PAVEMENT PER THE RECOMMENDATIONS OF THE PROJECT ENGINEER AND STOCKPILE EXCESS MATERIAL. STABILIZE STOCKPILE AS NECESSARY.
- 7. PERFORM PRELIMINARY SITE GRADING IN ACCORDANCE WITH THE PLANS.
- 8. INSTALL THE SEWER AND DRAINAGE SYSTEMS FIRST, THEN ANY OTHER UTILITIES IN ACCORDANCE WITH THE PLAN AND DETAILS, ANY CONFLICTS BETWEEN UTILITIES ARE TO BE RESOLVED WITH THE INVOLVEMENT AND APPROVAL OF THE ENGINEER.
- 9. INSTALL INLET PROTECTION AT ALL CATCH BASINS AS THEY ARE CONSTRUCTED IN ACCORDANCE WITH DETAILS.
- 10. ALL SWALES AND DRAINAGE STRUCTURES ARE TO BE CONSTRUCTED AND STABILIZED PRIOR TO HAVING RUN-OFF DIRECTED TO THEM.
- 11. DAILY, OR AS REQUIRED, CONSTRUCT TEMPORARY BERMS, DRAINAGE DITCHES, CHECK DAMS, SEDIMENT TRAPS, ETC., TO PREVENT EROSION ON THE SITE AND PREVENT ANY SILTATION OF ABUTTING WATERS AND/OR PROPERTY.
- 12. PERFORM FINAL FINE GRADING, INCLUDING PLACEMENT OF 'SELECT' SUBGRADE MATERIALS.
- 13. PAVE ROADWAY AND DRIVEWAYS WITH INITIAL 'BASE COURSE'.
- 14. PERFORM ALL REMAINING SITE CONSTRUCTION (i.e. BUILDING, CURBING, UTILITY CONNECTIONS, ETC.).
- 15. LOAM AND SEED ALL DISTURBED AREAS AND INSTALL ANY REQUIRED SEDIMENT AND EROSION CONTROL FACILITIES (i.e. RIP RAP, EROSION CONTROL BLANKETS, ETC.).
- 16. FINISH PAVING ROADWAY AND DRIVEWAYS WITH 'FINISH' COURSE.
- 17. ROADWAY AND DRIVEWAYS SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- 18. ALL CUT AND FILL SLOPES SHALL BE SEEDED/LOAMED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- 19. COMPLETE PERMANENT SEEDING AND LANDSCAPING.
- 20. REMOVE TEMPORARY EROSION CONTROL MEASURES AFTER SEEDING AREAS HAVE BEEN 75%-85% ESTABLISHED AND SITE IMPROVEMENTS ARE COMPLETE. SMOOTH AND RE-VEGETATE ALL DISTURBED AREAS.
- 21. CLEAN SITE AND ALL DRAINAGE STRUCTURES, PIPES AND SUMPS OF ALL SILT AND DEBRIS.
- 22. INSTALL ALL PAINTED PAVEMENT MARKINGS AND SIGNAGE PER THE PLANS AND DETAILS.
- 23. ALL EROSION CONTROLS SHALL BE INSPECTED WEEKLY AND AFTER EVERY QUARTER-INCH OF RAINFALL
- 24. UPON COMPLETION OF CONSTRUCTION, IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO NOTIFY ANY RELEVANT PERMITTING AGENCIES THAT THE CONSTRUCTION HAS BEEN FINISHED IN A SATISFACTORY MANNER.

SEEDING RATES

Designed and Produced in NH

PO Box 219

603-772-4746 85 Portsmouth Ave. Civil Engineering Services E-MAIL: JBE@JONESANDBEACH.COM Stratham, NH 03885

EROSION AND SEDIMENT CONTROL DETAILS

635 SAGAMORE DEVELOPMENT LLC

LUSTER CLUSTER Project: 635 SAGAMORE AVE., PORTSMOUTH, NH

DRAWING No.

SHEET 20 OF 20 Owner of Record 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158 JBE PROJECT NO. 18134.1

NOT TO SCALE

Design: DJM | Draft: KDR Date: 2/26/2024 Checked: JAC | Scale: AS NOTED | Project No.: 18134.1 Drawing Name: 18134.1-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).

ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE

T THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

08/20/2024

August 19, 2024

Portsmouth Technical Advisory Committee Attn: Peter Stith 1 Junkins Avenue, Suite 3rd Floor Portsmouth, NH 03801

RE: Lot Line Adjustment – 100 Borthwick Ave, Portsmouth, NH

Dear Mr. Peter Stith:

On behalf of the Applicant, Stonefish, LLC, Apex Design Build respectfully submits an application to the adjust of the Lot-Line between the existing neighbor (Liberty Mutual) to the north and 100 Borthwick Ave, Portsmouth, NH. The Applicant is proposing this adjustment as part of the sale of an existing parking lot which features an addition of (264) parking spots for Liberty Mutual. This parking lot was previously designed, permitted, and constructed by Liberty Mutual as part of an agreement between NECU and Liberty Mutual. Now that NECU is relocating their corporate headquarters to Dover, NH, this presents a viable opportunity to Liberty Mutual to purchase the aforementioned parking lot which has been leased back to them for 5+ years. As a result of this lot-line adjustment, there will be no change in usage, no change in surface drainage, and the existing infrastructure complies with required runoff rates employed by Portsmouth. Additionally, all current needs of the site remain in compliance for the intended mixed-use tenancy at 100 Borthwick Ave and associated parking requirements.

This Lot-Line Adjustment will ensure that Liberty Mutual continues to provide a strong presence in Portsmouth for their Corporate Headquarters, and will also be a strong advocate for continuing that presence for the foreseeable future. This, in turn, will continue to solidify thousands of local employment opportunities for the Portsmouth, NH area.

Should there be any questions or concerns about the aforementioned application, please feel free to contact me directly.

Sincerely,

Jeff Kilburg

Project Director

JAPS a Vien

Encl: Application Materials



Authorization Form

This Authorization Form (this "<u>Authorization</u>"), effective upon the date of signature below (the "<u>Effective Date</u>"), is by and among Northeast Credit Union dba Lighthouse Credit Union and its successors or assigns ("<u>Lighthouse</u>"), Apex Design Build ("<u>Apex</u>") and Allen & Major Associates, Inc. (collectively with Apex, the "<u>ATDG Borthwick Team</u>"), to act as an agent on behalf of Lighthouse for the purposes and upon the limitations listed herein:

Effective upon the Effective Date, this Authorization, relative strictly to Lighthouse's property located at 100 Borthwick Avenue, Portsmouth, New Hampshire 03801 (the "Property") and the ATDG Borthwick Team's ongoing project on behalf of ATDG, LLC at the Property (the "Project"), is limited to: 1) permitting and land use matters relative to the Project that are before governing boards, committees or other authority bodies or individuals authorized and acting on behalf of the City of Portsmouth, New Hampshire or the State of New Hampshire (collectively, the "Project Governmental Bodies") and 2) authorizes the ATDG Borthwick Team to: a) apply for and sign permits and ancillary documents relative to the Project as needed from the Project Governmental Bodies and individuals working on behalf of the same, as representative of Lighthouse in conjunction with the Project. This Authorization is contingent upon copy of all applications and submissions relative to the Project that are submitted to the Project Governmental Bodies being sent to Lighthouse, contemporaneously with or before their time of submission, as follows:

Lighthouse Credit Union

Attn: Lee Schafer, SVP, General Counsel & Chief Operating Officer

Via email to: lschafer@lighthousecu.org & Neil Gordon, SVP & Chief Financial Officer Via email to: ngordon@lighthousecu.org

With a copy to

Sheehan Phinney Bass & Green, PA Attn: Eric T. Kilchenstein, Esq.

Via email to: ckilchenstein@sheehan.com

This Authorization is fully revocable without cause and upon written notice from Lighthouse.

[Signature Page Follows]

Northeast Credit Union dba Lighthouse Credit Union

By: Neil Gordon,

Title: SVP and Chief Financial Officer

Duly Authorized

[Signature Page to Authorization Form]

Date:



City of Portsmouth, New Hampshire Subdivision Application Checklist

This subdivision application checklist is a tool designed to assist the applicant in the planning process and for preparing the application for Planning Board review. A pre-application conference with a member of the planning department is strongly encouraged as additional project information may be required depending on the size and scope. The applicant is cautioned that this checklist is only a guide and is not intended to be a complete list of all subdivision review requirements. Please refer to the Subdivision review regulations for full details.

Applicant Responsibilities (Section III.C): Applicable fees are due upon application submittal along with required number of copies of the Preliminary or final plat and supporting documents and studies. Please consult with Planning staff for submittal requirements.

Owner: Northeast Credit Union & ATTN: Accounting		Date Submitted: 08/19	/2024		
Applicant: Raquelle Kemnitz - Apex Design Build					
Phone Number: 847-288-0100	_E-mail: _	raquellek@apexdesignbui	ld.net		
Site Address 1: 100 Borthwick Ave, Portsmouth, NH 038	01		Map:	259	Lot:
Site Address 2:			Map:		Lot:

	Application Requirements				
Ø	Required Items for Submittal	Item Location (e.g. Page or Plan Sheet/Note #)	Waiver Requested		
V	Completed Application form. (III.C.2-3)	Separate Form	N/A		
V	All application documents, plans, supporting documentation and other materials provided in digital Portable Document Format (PDF) on compact disc, DVD or flash drive. (III.C.4)	All documents to be submitted via the Portsmouth online portal	N/A		

Requirements for Preliminary/Final Plat				
M	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
7	Name and address of record owner, any option holders, descriptive name of subdivision, engineer and/or surveyor or name of person who prepared the plat. (Section IV.1/V.1)	See title block for owner name and address, subdivision name, and surveyor/company.	☑ Preliminary Plat ☑ Final Plat	N/A

	Requirements for Pr	eliminary/Final Plat		
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
	Preliminary Plat Names and addresses of all adjoining property owners. (Section IV.2) Final Plat Names and addresses of all abutting property owners, locations of buildings within one hundred (100) feet of the parcel, and any new house numbers within the subdivision. (Section V.2)		☑ Preliminary Plat ☑ Final Plat	N/A
V	North point, date, and bar scale. (Section IV.3/V3)	Required on all Plan Sheets	☑ Preliminary Plat ☑ Final Plat	N/A
V	Zoning classification and minimum yard dimensions required. (Section IV.4/V.4)		☑ Preliminary Plat ☑ Final Plat	N/A
7	Preliminary Plat Scale (not to be smaller than one hundred (100) feet = 1 inch) and location map (at a scale of 1" = 1000'). (Section IV.5) Final Plat Scale (not to be smaller than 1"=100'), Location map (at a scale of 1"=1,000') showing the property being subdivided and its relation to the surrounding area within a radius of 2,000 feet. Said location map shall delineate all streets and other major physical features that my either affect or be affected by the proposed development. (Section V.5) Location and approximate dimensions of all existing and proposed property lines including the entire area proposed to be subdivided, the areas of proposed lots, and any adjacent parcels in the same ownership. (Section IV.6)		☑ Preliminary Plat ☑ Preliminary Plat ☑ Preliminary Plat ☑ Final Plat	N/A
~	Dimensions and areas of all lots and any and all property to be dedicated or reserved for schools, parks, playgrounds, or other public purpose. Dimensions shall include radii and length of all arcs and calculated bearing for all straight lines. (Section V.6/ IV.7)		☑ Preliminary Plat ☑ Final Plat	N/A
V	Location, names, and present widths of all adjacent streets, with a designation as to whether public or private and approximate location of existing utilities to be used. Curbs and sidewalks shall be shown. (Section IV.8/V.7)		☑ Preliminary Plat ☑ Final Plat	

		reliminary/Final Plat	Popuired for	Waiver
<u> </u>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Requested
V	Location of significant physical features, including bodies of water, watercourses, wetlands, railroads, important vegetation, stone walls and soils types that my influence the design of the subdivision. (Section IV.9/V.8)		☑ Preliminary Plat ☑ Final Plat	
	Preliminary Plat Proposed locations, widths and other dimensions of all new streets and utilities, including water mains, storm and sanitary sewer mains, catch basins and culverts, street lights, fire hydrants, sewerage pump stations, etc. (Section IV.10) Final Plat Proposed locations and profiles of all proposed streets and utilities, including water mains, storm and sanitary sewer mains, catchbasins and culverts, together with typical cross sections. Profiles shall be drawn to a horizontal scale of 1"=50" and a vertical scale of 1"=5", showing existing centerline grade, existing left and right sideline grades, and proposed centerline grade. (Section V.9)	No proposed new streets / utilities.	☑ Preliminary Plat ☑ Final Plat	
	When required by the Board, the plat shall be accompanied by profiles of proposed street grades, including extensions for a reasonable distance beyond the subject land; also grades and sizes of proposed utilities. (Section IV.10)	No proposed new streets / utilities	☑ Preliminary Plat ☑ Final Plat	
V	Base flood elevation (BFE) for subdivisions involving greater than five (5) acres or fifty (50) lots. (Section IV.11)	No BFE within the parcel or vicinity.	☑ Preliminary Plat ☑ Final Plat	
7	For subdivisions of five (5) lots or more, or at the discretion of the Board otherwise, the preliminary plat shall show contours at intervals no greater than two (2) feet. Contours shall be shown in dotted lines for existing natural surface and in solid lines for proposed final grade, together with the final grade elevations shown in figures at all lot corners. If existing grades are not to be changed, then the contours in these areas shall be solid lines. (Section IV.12/ V.12)	Not applicable. This is a two lot subdivision.	☑ Preliminary Plat ☑ Final Plat	

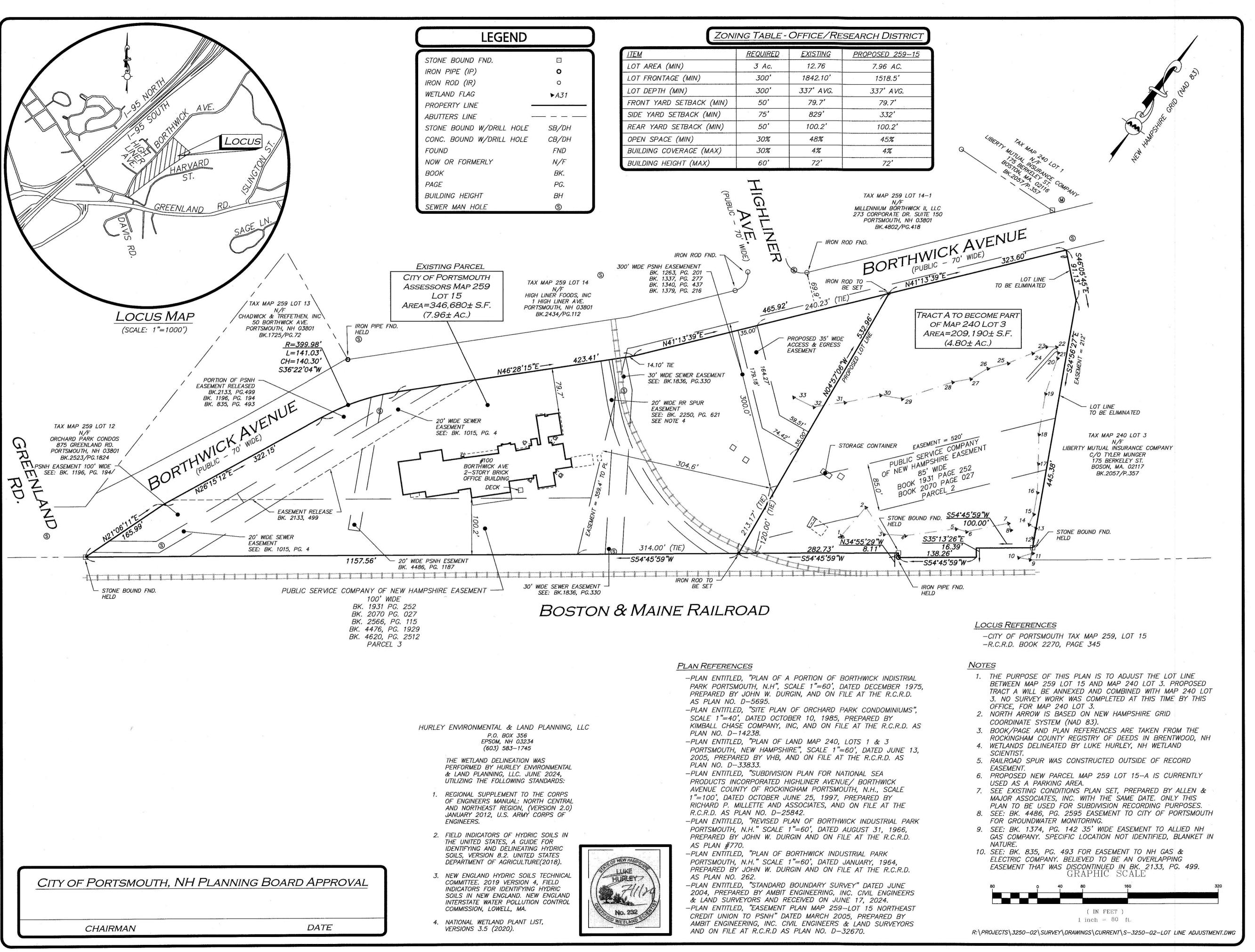
Requirements for Preliminary/Final Plat				
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
	Dates and permit numbers of all necessary permits from governmental agencies from which approval is required by Federal or State law. (Section V.10)	N/A	☐ Preliminary Plat ☑ Final Plat	
8	For subdivisions involving greater than five (5) acres or fifty (50) lots, the final plat shall show hazard zones and shall include elevation data for flood hazard zones. (Section V.11)	No BFE within the parcel or vicinity	☐ Preliminary Plat ☑ Final Plat	
V	Location of all permanent monuments. (Section V.12)		☐ Preliminary Plat ☑ Final Plat	

	General Requirements ¹				
	Required Items for Submittal	Item Location	Waiver		
	Required Items for Submittal	(e.g. Page/line or Plan Sheet/Note #)	Requested		
	1. Basic Requirements: (VI.1) a. Conformity to Official Plan or Map b. Hazards c. Relation to Topography d. Planned Unit Development	Not applicable, this is a two lot subdivision of previously developed area using existing frontage.			
2222	2. Lots: (VI.2) a. Lot Arrangement b. Lot sizes c. Commercial and Industrial Lots				
	a. Relation to adjoining Street System b. Street Rights-of-Way c. Access d. Parallel Service Roads e. Street Intersection Angles f. Merging Streets g. Street Deflections and Vertical Alignment h. Marginal Access Streets i. Cul-de-Sacs j. Rounding Street Corners k. Street Name Signs l. Street Names m. Block Lengths n. Block Widths o. Grade of Streets p. Grass Strips	Some items are not applicable. No new right-of-way is proposed. Lots will use existing frontage.			
	4. Curbing: (VI.4)	Not applicable, no new street proposed			
IT	5. Driveways: (VI.5)	Existing driveways are maintained			
后	6. Drainage Improvements: (VI.6)	Existing drainage to remain.			
	7. Municipal Water Service: (VI.7)	Existing water service to remain			
一	8. Municipal Sewer Service: (VI.8)	Existing sewer service to remain			
	9. Installation of Utilities: (VI.9) a. All Districts b. Indicator Tape	No new utilities proposed			
	10. On-Site Water Supply: (VI.10)	No new on-site water supply proposed.			
	11. On-Site Sewage Disposal Systems: (VI.11)	No on-site sewage disposal proposed/required			
	12. Open Space: (VI.12) a. Natural Features b. Buffer Strips c. Parks d. Tree Planting	No changes proposed to existing site			
	13. Flood Hazard Areas: (VI.13) a. Permits b. Minimization of Flood Damage c. Elevation and Flood-Proofing Records d. Alteration of Watercourses	No BFE on the parcel or within the vicinity			
	14. Erosion and Sedimentation Control (VI.14)	No site work proposed			

	Required Items for Submittal	Item Location	Waiver
"	isadanca isanis na ananima.	(e.g. Page/line or	Requested
		Plan Sheet/Note #)	
V	15. Easements (VI.15)	Existing easements are	
	a. Utilities	shown. Proposed	
	b. Drainage	access easement is	
V	16. Monuments: (VI.16)		
H	17. Benchmarks: (VI.17)	No site work is proposed	
7	18. House Numbers (VI.18)	Existing address to remain.	
ابنا	10. House families (41120)		
	<u></u>		
	Design Standards		
	Required Items for Submittal	Indicate compliance and/or	Waiver
	,	provide explanation as to	Requested
		alternative design	
	Streets have been designed according to the design	No new streets are	
	standards required under Section (VII.1).	proposed.	
	a. Clearing		
	b. Excavation		
	c. Rough Grade and Preparation of Sub-Grade		
	d. Base Course		
	e. Street Paving	:	
	f. Side Slopes	•	
	g. Approval Specifications		
	h. Curbing		
	i. Sidewalks		
	j. Inspection and Methods		
╙	2. Storm water Sewers and Other Drainage Appurtenances	No new storm water or	
	have been designed according to the design standards	drainage work is	1
	required under Section (VII.2).	proposed. Existing	
	a. Design	drainage is to remain.	
_	b. Standards of Construction		
	3. Sanitary Sewers have been designed according to the	No new sanitary sewer	
	design standards required under Section (VII.3).	work is proposed.	
	a. Design	Existing sewer is to	
	b. Lift Stations	remain.	
	c. Materials		
 	d. Construction Standards		
	4. Water Mains and Fire Hydrants have been designed	No new water mains or	
	according to the design standards required under	hydrants are proposed.	
	Section (VII.4).	Existing water is to	
	a. Connections to Lots	remain.	
1	b. Design and Construction		
	c. Materials		
	d. Notification Prior to Construction		<u> </u>
	/ /		
	/ ~/		

Applicant's/Representative's Signature: _______ Date: __08/19/2024

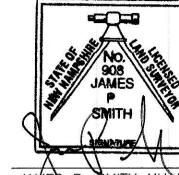
¹ See City of Portsmouth, NH Subdivision Rules and Regulations for details. Subdivision Application Checklist/January 2018



THIS PLAN IS THE RESULT OF AN ACTUAL ON THE GROUND SURVEY PERFORMED ON OR BETWEEN JUNE 14, 2024 AND JULY 2, 2024 AND HAD AN ERROR OF CLOSURE OF NO GREATER THAN 1/10,000.

THE SUBJECT PREMISES IS LOCATED IN FLOOD ZONE X — "AREA OF MINIMAL FLOOD HAZARD" AS SHOWN ON THE FLOOD INSURANCE RATE MAP FOR THE CITY OF PORTSMOUTH NEW HAMPSHIRE ROCKINGHAM COUNTY COMMUNITY PANEL NUMBER 33015C0270F HAVING AN EFFECTIVE DATE OF JANUARY 1, 2021.

ALLEN & MAJOR ASSOCIATES, INC.



P. SMITH NH LLS #908

REV DATE DESCRIPTION

STONEFISH, LLC 875 GREENLAND RD. UNIT C8 PORTSMOUTH, NH 03801

OWN

APPLICANT:

NORTH EAST CREDIT UNION PO BOX 1240 PORTSMOUTH, NH 03802

PROJECT:

TM 259 LOT 15
100 BORTHWICK AVE.
PORTSMOUTH, NH

 PROJECT NO.
 3250-02
 DATE:
 08-19-2024

 SCALE: 1" = 80'
 DWG. NAME:
 S-3250-02-LLA

 DRAFTED BY:
 CTP
 CHECKED BY:
 JPS

PREPARED BY:

ALLEN & MAJOR
ASSOCIATES, INC.
civil engineering • land surveying

environmental consulting de landscape architecture www.allenmajor.com 400 HARVEY ROAD MANCHESTER, NH 03103

MANCHESTER, NH 03103 TEL: (603) 627-5500 FAX: (603) 627-5501

WOBURN, MA

◆ LAKEVILLE, MA

◆ MANCHESTER, NI

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SHEET No.

LOT LINE ADJUSTMENT PLAN

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DRAWING TITLE: