#### SITE PLAN REVIEW TECHNICAL ADVISORY COMMITTEE PORTSMOUTH, NEW HAMPSHIRE

#### CONFERENCE ROOM A CITY HALL, MUNICIPAL COMPLEX, 1 JUNKINS AVENUE

Members of the public also have the option to join the meeting over Zoom (See below for more details)\*

#### 2:00 PM

June 4, 2024

#### **AGENDA**

#### I. APPROVAL OF MINUTES

**A.** Approval of minutes from the May 7, 2024 Site Plan Review Technical Advisory Committee Meeting.

#### II. OLD BUSINESS

- A. The request of RIGZ Enterprises LLC (Owner), for property located at 806 us Route 1 Bypass requesting an Amended Site Plan Approval and a second 1-year extension of the previously approved site plan approval granted on June 23, 2022. Said property is located on Assessor Map 161 Lot 43 and lies within the Business (B) District. (LU-22-81)
- **B.** The request of **635 Sagamore Development LLC (Owner)**, For property located at **635 Sagamore Avenue** requesting Site Plan approval for the removal of the existing structures and construction of 4 single-family dwellings on one lot with associated site improvements. Said property is located on Assessor Map 222 Lot 19 and lies within the Single Residence A (SRA) District. (LU-22-209)
- C. REQUEST TO POSTPONE The request of Oak Street Real Estate Capital (Owner), 100 Durgin Lane Owner, LLC (Applicant), for property located at 100 Durgin Lane requesting Subdivision approval of a lot line adjustment and Site Plan Review approval for the demolition of the existing buildings and the construction of 360 rental housing units in a mix of 3-story and 4-story buildings with associated site improvements including parking, pedestrian access, community spaces, utilities, stormwater management, lighting, and landscaping. Said property is located on Assessor Map 239 Lot 18 and lies within the Gateway Corridor (G1) District. (LU-24-62) REQUEST TO POSTPONE

#### **III. NEW BUISINESS**

- A. The request of Christ Church Parish, (Owner), Portsmouth Housing Authority (Applicant), for property located at 1035 Lafayette Road seeking Conditional Use Permits from Section 10.5B41.10 for a Development Site, from Section 10.5B72 for density bonus incentive for increased dwelling units per building and a Conditional Use Permit from Section 10.1112.14 to provide less than the required parking and Site Plan Review Approval for construction of a 4-story, 44-unit multi-family residential building to the south of the existing church building, conversion of the first-floor of the existing church into office space and construction of a 7-unit transitional housing addition. The lower level of the existing rectory building on the site. The project will include associated site improvements such as parking, pedestrian connections, access to public transportation, utilities, stormwater management, lighting, and landscaping. Said property is located on Assessor Map 246 Lot 1 and lies within the Gateway Center (G2) District. (LU-24-92)
- **B.** The request of Lonza Biologics (Owner), for property located at 5 Technology Drive (*Formerly 70 Corporate Drive*) requesting Amended Site Plan approval for the addition of Phase Photovoltaic Cell (PV) Solar canopies over the previously approved temporary surface parking lot. Said property is located on Assessor Map 305 Lot 6 and lies within the Airport Business Commercial (ABC) District. (LU-23-108)

#### **IV. ADJOURNMENT**

\*Members of the public also have the option to join this meeting over Zoom, a unique meeting ID and password will be provided once you register. To register, click on the link below or copy and paste this into your web browser:

https://us06web.zoom.us/webinar/register/WN\_M2P-hnHSRcysYNP\_175zhw

#### SITE PLAN REVIEW TECHNICAL ADVISORY COMMITTEE PORTSMOUTH, NEW HAMPSHIRE

#### CONFERENCE ROOM A CITY HALL, MUNICIPAL COMPLEX, 1 JUNKINS AVENUE

2:00 PM

May 7, 2024

#### **MINUTES**

#### **MEMBERS PRESENT:**

Peter Stith, Chairperson, Planning Manager; David Desfosses, Construction Technician Supervisor; Chad Putney, Fire Prevention Officer; Shanti Wolph, Chief Building Inspector; Peter Britz, Director of Planning & Sustainability; Zachary Cronin, Assistant City Engineer, Eric Eby, Parking and Transportation Engineer; Mike Maloney; Deputy Police Chief, Vincent Hayes; Land Use Compliance Agent/Associate Planner

**MEMBERS ABSENT:** 

Patrick Howe, Deputy Fire Chief

#### ADDITIONAL STAFF PRESENT:

Stefanie Casella, Planner II; Kate Homet, Associate Environmental Planner

[3:56] Chairman Stith opened the meeting.

#### I. APPROVAL OF MINUTES

A. Approval of minutes from the April 2, 2024 Site Plan Review Technical Advisory Committee Meeting.

[4:116] S. Wolph made a motion to approve the minutes as presented. Z. Cronin seconded the motion. The motion passed unanimously.

#### II. OLD BUSINESS

A. REQUEST TO POSTPONE The request of 635 Sagamore Development LLC (Owner), For property located at 635 Sagamore Avenue requesting Site Plan approval for the removal of the existing structures and construction of 4 single-family dwellings on one lot with associated site improvements. Said property is located on Assessor Map 222 Lot 19 and lies within the Single Residence A (SRA) District. (LU-22-209) REQUEST TO POSTPONE

[4:26] Chairman Stith noted the applicants had requested to postpone as they are still working on third party reviews.

#### III. NEW BUISINESS

a. The request of **Friends of Lafayette House (Owner)**, for property located at **413 Lafayette Road** requesting Site Plan Review Approval for a 635 square foot addition with associated site improvements. Said property is located on Assessor Map 230 Lot 23A and lies within the Single Residence B (SRB) District. (LU-24-61)

[4:37] Chairman Stith introduced this application.

#### SPEAKING TO THE APPLICATION

[4:57] Joe Coronati of Jones & Beach Engineering, came to present this application. He noted that the last time he was before the Committee, it was requested that the utilities be located, which has been done. There will be no utilities in the way of the new addition, it will all be interior. The newest site plan set has been submitted which has their requests for waivers in it. They will provide a green building statement and they will request the two waivers as noted by the staff comments.

[7:30] C. Putney noted that the applicant will have to extend the sprinkler and fire alarm system. Mr. Coronati agreed.

#### **PUBLIC HEARING**

[7:38] Chairman Stith opened the public hearing. No one spoke. The hearing was closed.

#### **DISCUSSION AND DECISION OF THE BOARD**

[7:59] D. Desfosses made a motion to send this application to the Planning Board. P. Britz seconded the motion. The motion passed unanimously.

b. The request of **Oak Street Real Estate Capital (Owner) 100 Durgin Lane Owner, LLC (Applicant)**, for property located at **100 Durgin Lane** requesting Subdivision approval of a lot line adjustment and Site Plan Review approval for the demolition of the existing buildings and the construction of 360 rental housing units in a mix of 3story and 4-story buildings with associated site improvements including parking, pedestrian access, community spaces, utilities, stormwater management, lighting, and landscaping. Said property is located on Assessor Map 239 Lot 18 and lies within the Gateway Corridor (G1) District. (LU-24-62)

[9:29] Chairman Stith introduced this application.

#### SPEAKING TO THE APPLICATION

[10:14] Brett Benson (architect), Patrick Crimmins (engineer), Andrew Hayes (owner representative), and Nick Aceto (landscape architect) came to present this application. Mr. Benson proceeded to explain the proposed development with a slideshow. This highlighted the project objectives and project summary, which detailed the proposed 360 residential apartments, a clubhouse building, 567 parking spaces and three acres of community space. He also reviewed the main points heard at their previous Planning Board, TAC and Conservation Commission work sessions.

[14:05] Mr. Crimmins listed the required permits the project would need to meet, including a lot line revision, a site plan review permit, a conditional use permit for site development standards, a conditional use permit for noise and a wetland conditional use permit. He went into the existing conditions on site and how the lots are proposed to be rearranged with easements relocated. He proceeded to go through different sections of zoning requirements that this project complies with and how the site reduces existing impervious surfaces and attempts to reduce wetland buffer impacts. A fire truck turning plan was shown as well as a grading and drainage plan for the proposed site which describes the stormwater and sewer plans in greater detail. The buildings will be heated with electricity, which should reduce their demand for natural gas.

[24:48] Mr. Aceto went on to describe the community space exhibit, layout and materials, the proposed planting plan, and the photometric plan.

[28:57] Mr. Benson addressed previous wayfinding comments, EV parking, the noise overlay district, potential solar locations, and the proposed floor plans.

[34:54] P. Britz asked if they had considered doing more of a townhouse design for the buildings. Mr. Benson responded that some of the buildings are centered around an entry courtyard but in discussions with the team, they want the sidewalks to feel public and bustling and open to the public to feel like a neighborhood. This pointed them towards feeling as if they needed to create layers of semi-private and semi-public spaces so that it does not feel like a front door is right on top of a busy sidewalk.

[37:45] Chairman Stith asked the six parking spaces that are in the shared community space. The committee will need to look at that more closely to make sure it still meets the definition of a community space. Mr. Hayes responded that their intention with those parking spaces was the ability to program that space for the community at large, for example hosting food trucks. From a traditional parking perspective, they would be open to limiting the use of those spaces there.

[38:50] P. Britz noted that he could not see the full outline of the lot depicted on any plans. Mr. Crimmins responded that it was not depicted in these exhibits, but it would be a part of the lot line revision plan coming up. P. Britz asked if they were counting their frontage off Gosling Road for this project. Mr. Crimmins responded that they were using their Durgin Lane frontage. P. Britz asked if they would build out the proposed circle shown on the plans. Mr. Crimmins noted that it was there due to a staff comment about needing a truck turnaround. They had looked into it but the lot lines constrain it to half a cul de sac, and not a full cul de sac. The implementation of a turnaround there would also mean more impervious surface in the wetland buffer. They would be open to installing it if the staff feels like they will need one. P. Britz asked

about trash would be delivered and circulated through the site. Mr. Benson mentioned that they were still working on this but they imagined that a trash truck or the staff will collect trash from each building. Package delivery will be delivered to a central location within the community building and delivery vans will have designated parking nearby. Mr. Hayes mentioned that they are evaluating a potential partnership with a trash valet system which would be localized to each building.

[42:09] P. Britz asked if the intention of the solar canopy was to reduce noise. Mr. Benson responded that they are continuing to study the covered parking (two sided facing the west and south) and how it could help with the acoustics.

[42:59] E. Eby asked bout the parking spaces on the main street, the head-in parking and parallel parking. He wanted to know if they intended to flip those as the current configuration constrains which direction cars need to come from to park. Mr. Aceto noted that they considered this configuration to reduce headlights into the windows on buildings.

[44:33] Chairman Stith noted that the applicants would need a wetland third party review, a traffic third party and stormwater third party analysis.

#### **PUBLIC HEARING**

[45:13] Chairman Stith opened the public comment.

[45:35] Liz Bratter of 159 McDonough Street came to speak. Ms. Bratter voiced her concern about the sound barriers, the need for more signs and not circles, the narrow roadway that currently exists on the way to Motel 6, the proximity of the dog park to wetlands and storm drains, the proximity of buildings to the wetlands, and the height of the proposed light poles.

[53:07] Chairman Stith closed the public hearing.

#### DISCUSSION AND DECISION OF THE BOARD

[53:22] Chairman Stith noted that he would entertain a motion to postpone.

[53:26] D. Desfosses made a motion to postpone. Z. Cronin seconded the motion. The motion passed unanimously.

#### **IV. ADJOURNMENT**

[53:45] Z. Cronin made a motion to adjourn. D. Desfosses seconded the motion. The motion passed unanimously.

The meeting adjourned at 2:50 p.m.

Respectfully submitted,

Kate E. Homet Secretary for the Technical Advisory Committee

#### Ross Engineering, LLC Civil / Structural Engineering

909 Islington Street Portsmouth, NH 03801 603-433-7560 alexross@comcast.net

### 806 US Route 1 Bypass Project Description

May 17, 2024

806 US Rte. 1 bypass is the current location for the City Tobacco business. 822 US Rte. 1 bypass is a vacant gas station, and was just approved for the new City Tobacco business last night at the Planning Board meeting. The City Tobacco business will be moved to 822 after a new building is constructed.

We are requesting administration approval for the minor changes to the 806 site plan, which is necessary because of the drainage and site design for 822. 822 Rte. 1 By-Pass was just approved by the planning board last night, and the drainage configuration has been revised on 806 to match. We are also requesting the second extension to the original approval, since that deadline is fast approaching. 822 has existing drainage that needed extensive design to re-configure and this took extra time, which is why we need the extension for 806.

#### **Project History**

- The Technical Advisory Committee voted to recommend approval to the Planning Board at their May 3, 2022 meeting.
- The Planning Board granted Site Plan approval at the June 23, 2022 meeting.
- At the June 15, 2023 Planning Board meeting a 1-year extension of the Site Plan Approval granted on June 23, 2022 was approved so that the extension goes to June 23, 2024.

#### **Revisions include:**

#### **Drawing 1 – Existing Conditions Plan**

- Revised existing catch basin elevations
- Added note 6 outlining PB approval and extension of approval.

#### Drawing 2 – Site Plan

- Landscaping removed in NHDOT right of way, as per NHDOT request. This is shown on drawings 2-4.
- Drainage has been changed to depict new proposed drainage system. New drainage system is depicted to match proposed drainage on lot 29, which is connected to drainage system on lot 43. This is shown on drawings 2 & 3.
- Revised lighting callouts on the plan.

#### **Ross Engineering, LLC Civil / Structural Engineering**

909 Islington Street Portsmouth, NH 03801 603-433-7560 alexross@comcast.net

#### **Drawing 3 – Utility Plan**

- Landscaping removed in NHDOT right of way, as per NHDOT request. This is shown on drawings 2-4.
- Drainage has been changed to depict new proposed drainage system. New drainage system is depicted to match proposed drainage on lot 29, which is connected to drainage system on lot 43.
- Stormwater notes for drainage system on drawing 3 "Utility Plan".
- Revised existing and proposed drainage structure elevations on drawing 3 "Utility Plan".
- Revised lighting on drawing 3. Note 3 and the Lighting Specification Table have been revised. Lighting notes on the plan have been revised and are shown on drawings 2 & 3.

#### **Drawing 4 – Landscape Plan**

- Landscaping removed in NHDOT right of way as per NHDOT request.
- Drawing 4 "Landscape Plan" has been changed to depict new proposed manhole and catch basin locations.
- Planting notes have been changed to reflect landscaping that has been changed to reflect landscaping that has been removed in the NHDOT right of way.

#### **Drawing 5**–Easement Plan

• Easement Plan has been added as drawing 5 showing a drainage easement across Lot 43.

#### **Drawing 6 – Notes & Details**

• Revised manhole & catch basin details.

These minor amendments along with the improvements on the abutting property are an improvement from the previous proposed drainage system.

Sincerely,

Alex Ross, P.E.

# Site Plan 806 Route 1 Bypass Portsmouth, New Hampshire

# LIST OF PROJECT PLANS:

# SITE PLAN SET

- 1 Existing Conditions Plan
- 2 Site Plan
- 3 Utility Plan
- 4 Landscape Plan
- 5 Easement Plan
- 6 Notes & Details
- 7 Sewer Notes

PREPARED FOR:

# RIGZ ENTERPRISES LLC

PREPARED BY:

# ROSS ENGINEERING, LLC Civil/Structural Engineering & Surveying

909 Islington St. Portsmouth, NH 03801 (603) 433-7560

May 17, 2024







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MONUMENT FOUND

6' STOCKADE FENCE

6' CHAIN LINK FENCE

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# <u>LEGEND</u>

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REVISIONS

REVISIONS

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VERTICAL GRANITE CURE
6' CHAIN LINK FENCE
UTILITY POLE
CATCH BASIN
DRAIN MANHOLE
DRAIN LINE

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TRENCH NOTES - STORM DRAIN:



## **NOTES**

INLET

COMPACT

SUBGRADE

N.T.S.

I) ALL SECTIONS SHALL BE DESIGNED FOR H20 LOADING.

2) CONCRETE SHALL BE COMPRESSIVE STRENGTH 4000 PSI, TYPE II CEMENT.

PROPOSED DRAIN MANHOLE (TYP)

CONCRETE

INVERT

3) JOINT SEALANT BETWEEN PRECAST SECTIONS SHALL BE BUTYL RUBBER.

4) CIRCUMFERENTIAL REINFORCEMENT SHALL BE 0.12 SQ. IN PER LINEAR FT. IN ALL SECTIONS & SHALL BE PLACED IN THE CENTER THIRD OF WALL.

5) THE TONGUE OR THE GROOVE OF THE JOINT SHALL CONTAIN ONE LINE OF CIRCUMFERENTIAL REINFORCEMENT EQUAL TO 0.12 SQ IN PER LINEAR FT.

6) EACH CASTING TO HAVE LIFTING HOLES CAST IN.

## **NOTES**

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OUTLET

6" CRUSHED STONE

BEDDING (12" REQUIRED

AT LEDGE) (NHDOT 304.4)



## **GRAVITY SEWER TRENCH NOTES:**

- 1) <u>ORDERED EXCAVATION OF UNSUITABLE MATERIAL BELOW GRADE</u>: BACKFILL AS STATED IN THE TECHNICAL SPECIFICATIONS OR AS SHOWN ON THE DRAWINGS.
- 2) <u>BEDDING</u>: SCREENED GRAVEL AND/OR CRUSHED STONE FREE FROM CLAY, LOAM, ORGANIC MATTER AND MEETING ASTM C33. STONE SIZE NO. 67.
  - 100% PASSING 1 INCH SCREEN
  - 0-10% PASSING #4 SIEVE 90-100% PASSING 3/4 INCH SCREEN
  - 0-5% PASSING #8 SIEVE
  - 20-55% PASSING 3/8 INCH SCREEN
- WHERE ORDERED BY THE ENGINEER TO STABILIZE THE BASE, SCREENED GRAVEL OR CRUSHED STONE 1-1/2 INCH TO 1/2 INCH SHALL BE USED.
- 3) <u>SAND BLANKET</u>: CLEAN SAND FREE FROM ORGANIC MATTER, SO GRADED THAT 90-100% PASSES A 1/2 INCH SIEVE AND NOT MORE THAN 15% WILL PASS A #200 SIEVE. NO STONE LARGER THAN 2" SHOULD BE IN CONTACT WITH THE PIPE.
- 4) <u>SUITABLE MATERIAL:</u> IN ROADS, ROAD SHOULDERS, WALKWAYS AND TRAVELED WAYS, SUITABLE MATERIAL FOR TRENCH BACKFILL SHALL BE THE NATURAL MATERIAL 9) <u>CONCRETE FOR ENCASEMENT</u> SHALL CONFORM TO THE REQUIREMENTS OF SECTION 520, EXCAVATED DURING THE COURSE OF CONSTRUCTION, BUT SHALL EXCLUDE DEBRIS; (NHDDT STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION, LATEST PIECES OF PAVEMENT; ORGANIC MATTER; TOP SOIL; ALL WET OR SOFT MUCK, PEAT, EDITION. DR CLAY; ALL EXCAVATED LEDGE MATERIAL; ALL ROCKS OVER 6 INCHES IN LARGEST DIMENSION; AND ANY MATERIAL WHICH, AS DETERMINED BY THE ENGINEER, WILL NOT 10) <u>CONCRETE FULL ENCASEMENT</u>: IF FULL ENCASEMENT IS UTILIZED, DEPTH OF CONCRETE PROVIDE SUFFICIENT SUPPORT OR MAINTAIN THE COMPLETED CONSTRUCTION IN A BELOW PIPE SHALL BE 1/4 I.D. (4" MINIMUM). BLOCK SUPPORT SHALL BE SOLID STABLE CONDITION. IN CROSS-COUNTRY CONSTRUCTION, SUITABLE MATERIAL SHALL BE CONCRETE BLOCKS. AS DESCRIBED ABOVE, EXCEPT THAT THE ENGINEER MAY PERMIT THE USE OF TOP SOIL, LOAM, MUCK, OR PEAT, IF HE IS SATISFIED THAT THE COMPLETED CONSTRUCTION 11) GRAVEL DRIVEWAY AND SHOULDER RESTORATION: CRUSHED GRAVEL IN DRIVEWAYS AND WILL BE ENTIRELY STABLE AND PROVIDED THAT EASY ACCESS TO THE SEWER FOR RDAD SHOULDERS SHALL MATCH EXISTING WITH A MINIMUM DF 12". GRAVEL MAINTENANCE AND POSSIBLY RECONSTRUCTION, WILL BE PRESERVED. REPLACEMENT SHALL BE SUBSIDIARY TO SEWER CONSTRUCTION AND WILL NOT BE MEASURED FOR PAYMENT.

- 5) BASE COURSE AND PAVEMENT SHALL MEET THE REQUIREMENTS OF THE NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION'S LATEST EDITION OF THE STANDARD SPECIFICATIONS FOR HIGHWAYS AND BRIDGES - DIVISIONS 300 AND 400 RESPECTIVELY AND LOCAL REGULATION.
- WOOD SHEATHING, IF REQUIRED: WHERE SHEETING IS PLACED ALONGSIDE THE PIPE 6) AND EXTENDS BELOW MID-DIAMETER, IT SHALL BE CUT OFF AND LEFT IN PLACE TO AN ELEVATION 1 FOOT ABOVE THE TOP OF PIPE. WHERE SHEETING IS ORDERED BY THE ENGINEER TO BE LEFT IN PLACE, IT SHALL BE CUT DFF AT LEAST 3 FEET BELOW FINISHED GRADE, NUT NOT LESS THAN 1 FOOT ABOVE THE TOP OF THE PIPE.
- 7) <u>W = MAXIMUM ALLOWABLE TRENCH PAYMENT WIDTH</u> FOR LEDGE EXCAVATION AND FOR ORDERED EXCAVATION BELOW GRADE. FOR PIPES 15 INCHES NOMINAL DIAMETER OR LESS, W SHALL BE NO MORE THAN 36 INCHES. FOR PIPES GREATER THAN 12 INCHES IN NOMINAL DIAMETER, W SHALL BE 24 INCHES PLUS PIPE DUTSIDE DIAMETER (D. D. ) ALSO, W SHALL BE THE PAYMENT WIDTH.
- 8) <u>FOR CROSS COUNTRY CONSTRUCTION,</u> BACKFILL OR FILL SHALL BE MOUNDED TO A HEIGHT DF 6 INCHES ABOVE THE DRIGINAL GROUND SURFACE.

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**CITY OF PORTSMOUTH** 

Planning Department 1 Junkins Avenue Portsmouth, New Hampshire 03801 (603) 610-7216

#### **TECHNICAL ADVISORY COMMITTEE**

May 9, 2022

RIGZ Enterprises LLC 18 Dixon Lane Derry, New Hampshire 03801

RE: Site Review request for property located at 806 US Route 1 Bypass (LU-22-81)

Dear Property Owner:

The Technical Advisory Committee, at its regularly scheduled meeting of Tuesday, May 3, 2022, considered your application for Site Plan Review for construction of 400 square feet of additional commercial space and site improvements. Said property is shown on Assessor Map 161 Lot 43 and lies within the Business (B) District. As a result of said consideration, the Committee voted to **recommend approval** to the Planning Board with the following stipulations:

#### Items to be addressed prior to Planning Board approval:

1. Dumpsters will be relocated to parking spaces 24 and 23 with a 20 foot setback from rear lot line and at least 10 feet from side lot line. Applicant will request a waiver from the Planning Board for Section 9.3 of the Site Plan regulations to have the dumpsters located within 20' of the side lot line.

2. A note will be added to the plans regarding the use of non-combustible mulch.

3. Applicant will work with DPW to correct the sewer lateral connection and location.

4. Applicant will work with DPW staff (Eric Eby) to reconfigure handicap parking and accessibility (two spaces needed).

5. Applicant will extend landscaping and curbing at the front lot line.

6. Parking spaces 18 and 19 will be relocated and be replaced with landscaping and 3 bike racks.

7. Entryway will be striped.

8. Raised sidewalk will be extended to connect to front entryway.

9. Light Pole 3 (LP3) located at the rear of the building shall be limited to a height of 16' with cut off shields.

10. Lighting on the rear wall will not exceed a height of 9'.

11. Curbing is added to proposed landscape islands.

This matter will be placed on the agenda for the Planning Board meeting scheduled for **Thursday, June 16, 2022**. One (1) hard copy of all plans and supporting reports and exhibits as well as an updated electronic file (in a PDF format) must be filed in the Planning Department and uploaded to the online permit system no later than **Wednesday, May 25, 2022**.

Per Section 2.5 of the Site Plan Regulations, a site plan review application to the Planning Board must include all applicable information and supporting materials including but not limited to the following items:

- Full updated plan set
- Draft Easements
- Drainage Analysis
- Traffic Studies
- Etc.

All comments, corrections, and conditions identified as "Items to be addressed before Planning Board submittal' must be resolved/corrected for the Planning Board application submittal to be deemed complete.

The minutes and audio recording of this meeting are available by contacting the Planning Department.

Very truly yours,

Benerey Mon-zalt

Beverly Mesa-Zendt, Planning Director

cc:

Alex Ross, Ross Engineering



**CITY OF PORTSMOUTH** 

Planning Department 1 Junkins Avenue Portsmouth, New Hampshire 03801

(603) 610-7216

#### PLANNING BOARD

June 29, 2022

RIGZ Enterprises LLC 18 Dixon Lane Derry, New Hampshire 03801

RE: Site Review request for property located at 806 US Route 1 Bypass (LU-22-81)

Dear Property Owner:

The Planning Board, at its regularly scheduled meeting of **Thursday**, **June 23**, **2022**, considered your application for Site Plan Review for construction of 400 square feet of additional commercial space and site improvements Said property is shown on Assessor Map 161 Lot 43 and lies within the Business (B) District. As a result of said consideration, the Board voted 1) to determine the requested waiver does not nullify the spirit and intent of the City's Master Plan of the Site Plan Regulations and to grant the following waiver: *Waiver of Site Plan Review regulations* section 4.3.5 to locate a dumpster 12.2 feet from the property line where 20 feet is required; and 2) to **grant** Site Plan approval with the following stipulations:

# <u>Conditions to be satisfied subsequent to final approval of site plan but prior to commencement of any site work or construction activity:</u>

2.1 The site plan and any easement plans and deeds shall be recorded at the Registry of Deeds by the City or as deemed appropriate by the Planning Department.

2.2 Associated recording fees shall be paid to the City prior to recordation.

2.3 Light pole labels on the utility plan will be correct to reflect appropriate numbering and include LP3 and LP5 consistent with stipulation requiring light Pole 3 (LP3) located at the rear of the building to be limited to a height of 16' with cut off shields.

The Board's decision may be appealed up to thirty (30) days after the vote. Any action taken by the applicant pursuant to the Board's decision during this appeal period shall be at the applicant's risk. Please contact the Planning Department for more details about the appeals process.

This site plan approval shall not be effective until a site plan review agreement has been signed satisfying the requirements of Section 2.12 of the City's Site Review Approval Regulations.

Unless otherwise indicated above, applicant is responsible for applying for and securing a building permit from the Inspection Department prior to starting any project work.

The Planning Director must certify that all outstanding stipulations of approval have been completed prior to issuance of a building permit unless otherwise indicated above.

This site plan approval shall expire unless a building permit is issued within a period of one (1) year from the date granted by the Planning Board unless an extension is granted by the Planning Board in accordance with Section 2.14 of the Site Review Regulations.

The minutes and audio recording of this meeting are available by contacting the Planning Department.

Very truly yours,

Rick Chellman, Chairman of the Planning Board

cc: Shanti Wolph, Chief Building Inspector Rosann Maurice-Lentz, City Assessor

Peter H. Rice, Director of Public Works

Alex Ross, Ross Engineering



**CITY OF PORTSMOUTH** 

Planning Department 1 Junkins Avenue Portsmouth, New Hampshire 03801 (603) 610-7216

#### PLANNING BOARD

June 22, 2023

RIGZ Enterprises LLC 18 Dixon Lane Derry, New Hampshire 03801

RE: 1-Year Extension request for Site Plan and CUP approvals for property located at 806 US Route 1 Bypass (LU-22-81)

Dear Property Owner:

The Planning Board, at its meeting of Thursday, June 15, 2023, considered your request for

a 1-Year Extension of the Site Plan Approval granted on June 23, 2022.

As a result of said consideration, the Board voted

to grant a one-year extension to the Planning Board Approval of the Site Plan and Conditional Use Permits to June 23, 2024.

The Board's decision may be appealed up to thirty (30) days after the vote. Any action taken by the applicant pursuant to the Board's decision during this appeal period shall be at the applicant's risk. Please contact the Planning Department for more details about the appeals process.

The minutes and audio recording of this meeting are available by contacting the Planning Department.

Very truly yours,

Rick Chellman, Chairman of the Planning Board

cc: Shanti Wolph, Chief Building Inspector Rosann Maurice-Lentz, City Assessor

Alex Ross, Ross Engineering



85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

April 19, 2024

Portsmouth Technical Advisory Committee Attn: Board Members 1 Junkins Avenue, Suite 3<sup>rd</sup> Floor Portsmouth, NH 03801

#### RE: Response Letter - LU-22-209 635 Sagamore Ave, Portsmouth, NH Tax Map 222, Lot 19 JBE Project No. 18134.1

Dear Board Members,

We are in receipt of comments from the Technical Advisory Committee, provided by Stefanie Casella, City Planner, dated March 29, 2024. Review comments are listed below with our responses in bold.

- The city is finalizing roadway improvement design. City to work with applicant on CB location in relation to new sidewalk location.
   RESPONSE: No response necessary at this time.
- Sight lines at driveway are slightly shorter than required based on existing roadway profile. Sight lines will need to be rechecked once the City's roadway design is finalized. Possible mitigation measures needed if sight lines remain below minimums.
   RESPONSE: Prior to the initial TAC submission, we had discussed the sight lines with Eric Eby. It was understood that we were under the minimum stopping sight distance and that mitigation measures would be necessary, such as a "blind driveway" warning sight or 25 MPH posted speed limit over the crest of the hill to the south as Mr. Eby suggested via email on February 23, 2024.
- 3. Water work needs to be out of right of way prior to Sagamore road work. This includes extending new water to property and cut & cap of the previous water. RESPONSE: A water line stub will be extended to the right of way line prior to the Sagamore Ave road work.
- 4. Move water to driveway location. RESPONSE: Water has been moved to the driveway location.
- Remove label for 4" water main on far side of Sagamore Road. 4" water main has been abandoned.
   RESPONSE: The word "Abandoned" has been added to the label for the 4" water main on Sheets C1 and C4.

- 6. Are there plans to extend gas to the site? Stub gas main label on overhead wires south of site.' Sheet C4 Utility Plan.
  RESPONSE: We are not planning to extend the gas main to the site. The units will have propane tanks as shown on Sheet C4. The "stub gas main" label was a holdover from when natural gas service was being considered and has been removed.
- 7. How will this site deal with trash pickup? RESPONSE: The owner of each unit shall store trash in their garage. Trash will be picked up by a private hauler. Seet Note #21 on Sheet C2.
- 8. Remove stop bar and stop sign leaving site. This is not a road it is a driveway. **RESPONSE: The stop sign and stop bar have been removed from the plan.**
- 9. Change SMH2 inlet to a drop manhole connection to flatten out sewer run. RESPONSE: The sewer layout has been revised so this is no longer necessary. Previously, a drop inlet would have been helpful in order to flatten the sewer run and reduce the depth of the trench, but we have rearranged the sewer layout to eliminate the drainage crossing that made this sewer manhole necessary in the first place. Therefore, we now have only three sewer manholes proposed rather than four and we are placing a flatter 3.2% run between SMH 1 and SMH 2, which more nearly follows proposed grade than what was previously proposed and requires a shallower trench.
- 10. Drainage Concerns:
  - The drainage study needs to be revisited. We do not agree that these are type B soils due to the shallow ledge. The study also uses very long time of concentration sheet flow lengths that are inaccurate due to the steepness and type of terrain. Because of this, we believe that the runoff generation calculations are not accurate.

**RESPONSE:** See attached letter from the soil scientist. The soils on site are represented as HSG B because Chatfield, which is classified as HSG B, is the dominant soil type within the Chatfield-Hollis-Canton soil complex that makes up most of the subject parcel. Modelling the site as HSG B rather than C or D is a conservative approach. The addition of impervious surface causes more of a change to the curve number (CN) with the site represented as HSG B than with the site represented as HSG C or D and therefore this provides a safety factor for the requirement to reduce off-site peak flows to below the existing.

Tc paths are taken from the most hydraulically distant point and this is what we did. Each modelled Tc path is broken into several different sections to analyze each slope and land cover segment separately. We have double checked to make sure that we are modelling the correct slopes and land covers. Furthermore, modelling a long Tc path in the existing conditions is a conservative approach as this increases the difference in peak flows that needs to be attenuated.



We also believe that the applicant should have added the 3S and 4S hydrographs together in both the pre and post conditions because they combine along the Tidewatch road about 130' past AP3. There is evidence that there is in fact historic flooding or at a minimum, poor drainage conditions, in this location at the base of the hill adjacent to the Tidewatch road in the predevelopment condition so we are suspect of the calculations.

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**RESPONSE:** Subcatchments 3S and 4S need to be separate. 3S represents the runoff that reaches the ditch along the Tidewatch Condominium road while 4S represents the runoff that directly enters the catch basin adjacent to the Tidewatch Condominium mailbox structure, modelled as AP3. However, we agree that both subcatchments ultimately drain toward one analysis point; therefore, we have removed AP4 from the analysis and AP3 represents the catch basin on the Tidewatch Condominium property that the runoff from 3S and 4S ultimately drains into in the existing condition. 3S and 4S both ultimately drain toward Analysis Point 3, but 3S drains toward a shallow drainage ditch on the Tidewatch property before reaching AP3 while 4S drains directly over land to the analysis point.

- We also feel that perhaps the engineer should explore moving the outlet of 0 Bioretention Pond #1 southeast so that the flow leaving the pond is closest to its ultimate discharge point but this must be vetted during the calculations. **RESPONSE:** We are no longer proposing a bioretention pond where Pond #1 was previously proposed. All site runoff is now directed toward a single pond, now referred to as Bioretention Pond #1, where Bioretention Pond #2 was previously. The area where this pond is proposed is the only part of the site with enough depth to ledge to allow infiltration according to the results of test pits 8 and 10. Small infiltration practices are also proposed adjacent to units 3&4 where ledge is shallower, but we are providing enough fill at these locations to facilitate infiltration. The discharge from this pond will be directed over land toward the existing drainage ditch on the Tidewatch Condominium property, from where it will be directed to the ultimate discharge point (Analysis Point 3). Having the discharge flow through the ditch first rather than being outletted directly on to the Tidewatch property downstream of the ditch will help to better maintain or improve upon existing hydrologic patterns and prevent an increase in flooding at the ultimate discharge point. The swale has been modelled to ensure that an increase in runoff is not proposed to flow to it and the peak elevation stays the same or decreases.
- An off-site drainage improvement on Tidewatch property may be necessary to shed the stormwater via a new culvert under the private Tidewatch road and into one of the Tidewatch wetland areas directly as the flow from this development seems to be directed toward a single catch basin located near Tidewatch's mailbox structure.

**RESPONSE:** We are not opposed to this, however we would need permission from Tidewatch and would need more survey detail as well. If a culvert is added it should be cored into the catch basin that the runoff from the subject parcel is draining toward in the existing condition rather than across the street into the wetland, in order to mimic existing drainage patterns and not increase peak rates of runoff upon the wetland.



- We are therefore recommending a third-party Engineer review the design and the stormwater report.
   RESPONSE: John Chagnon of Haley Ward is already reviewing the design on behalf of Tidewatch Condominium, however we understand that the City will also be sending the plans and drainage report to their own review consultant.
- 11. Please demonstrate how you can reduce flow entering into AP3 to meet or be reduced by pre-development numbers [Section 6.1 (d) and Section 7.6 in Site Plan Review Regs]. While there is ledge across the site, please provide a low impact development method for reducing flow in this area as infiltration does not appear to be viable.
  RESPONSE: The peak flow was already being reduced with the previous design, however the volume of runoff directed toward Analysis Point 3 was being slightly increased as we acknowledged in our drainage report due to the lack of infiltration at the former pond location. With the increased infiltration capacity in the revised design, post-development runoff volumes will be less than pre-development runoff volumes toward all analysis points during the 2-, 10-, 25-, and 50-Year 24 Hour storms.
- 12. Please demonstrate how this project will conserve stormwater on site and practice low impact development stormwater practices (drip edges, rain barrels, stormwater filtration with vegetation, etc.). [Section 6.3, Section 6.6 and Section 7.1] RESPONSE: All of the stormwater management devices that we are proposing are Low Impact Development (LID) devices. Rain gardens are listed as an example of an LID device in Section 7.1 of the Site Plan Review Regulations and pre-treatment is achieved through the use of deep sump catch basins rather than a sediment function.

forebay. Where practicable, roof runoff is being captured and directly infiltrated through the use of stone drip edges and a permeable paver patio. These devices are only being proposed where the basement slab will be above the groundwater table.

- Please provide a green statement that addresses the sustainable and energy efficient practices that you intend to pursue in this development. [Section 2.5.3 (b)]
   RESPONSE: A green building statement is included with this submission.
- 14. Please update landscaping plans to acknowledge planting requirements [Section 6.2.2 (d-f), and Section 6.4] and to demonstrate adherence to Section 6.3 in the Site Plan Review Regulations.
  RESPONSE: The landscape designer has denoted on the planting schedule on Sheet L2 which plants are tolerant of urban conditions and also added Notes 19 and 20 to this sheet stipulating the requirements that need to be followed.
- 15. Please include in stormwater management operations and maintenance manual that an annual report will be submitted to the City of Portsmouth Department of Public Works. RESPONSE: This requirement has been added to Section A.1 of the O&M Manual.
- 16. Please indicate if, and/or where, snow storage will be located on site. If located on site, please demonstrate compliance with Section 7.6.1 (10).
   RESPONSE: Snow storage is shown on Sheet C2. The snow storage locations have been revised so that it is only shown in areas where snowmelt will drain toward a treatment BMP in accordance with the cited requirement.



17. Please provide a condo plan.

**RESPONSE:** A draft condominium site plan has been added as Sheet CS1 of the plan set.

18. How high are the buildings from the existing grade vs the proposed grade?

RESPONSE: See below table. In accordance with the definition of "building height" provided in Article 15 of the Zoning Ordinance, we measured the height of each building from average existing grade or average finished grade, whichever is lower, to the midpoint between the level of the roof eaves and the highest point of the roof. Based on this definition, all units are under the maximum height of 35' per the Zoning Regulations.

	Unit 1	Unit 2	Unit 3	Unit 4
<b>Finished Floor elevation</b>	73.5	74.0	74.5	75.0
FF to midpoint of ridge (ft.)	27.67	27.67	23.89	23.89
<b>Ridge midpoint elevation</b>	101.17	101.67	98.39	98.89
Average existing grade	71.0	72.0	65.5	66.0
elevation				
Average finished grade	72.0	73.0	69.0	68.0
elevation				
Building Height (ft.) based	30.17	29.67	32.89	32.89
on lower of average existing				
and proposed grade				

Included with this response letter are the following:

- 1. One (1) Full Size Plan Set (Folded).
- 2. One (1) Drainage Analysis.
- 3. One (1) Stormwater Operations & Maintenance Manual.
- 4. One (1) Green Building Statement.
- 5. Letter from Soil Scientist.

If you have any questions or need any additional information, please feel free to contact our office. Thank you very much for your time.

Very truly yours, JONES & BEACH ENGINEERS, INC.

## Joseph Coronati

Joseph A. Coronati Vice President

cc: Michael Garrepy (via email) Christopher Ward (via email) John Chagnon, P.E., Haley Hard (reviewer on behalf of Tidewatch Condominium, via email and U.S. Mail.)
Eric Weinrieb, Altus Engineering (via email & Hard Copy Delivered)





Architecture | Planning 22 Jady Hill Avenue Exeter, NH 03833 207.347.1504

City of Portsmouth Planning Department Attn: Peter Stith, Principal Planner 1 Junkins Ave, 3<sup>rd</sup> Floor Portsmouth, NH 03801

April 1, 2024

Dear Mr. Stith,

The residential units proposed for the project at 635 Sagamore Avenue are being designed to meet or exceed the applicable green building standards as set forth in the 2018 set of Codes adopted by the State of New Hampshire, along with associated amendments codified by the City of Portsmouth.

In an effort promote the buildings' efficiency, longevity, and health of their occupants, close attention shall be given to the following building categories:

- Tight building enclosures
  - Watertightness (though moisture barriers)
  - Vapor permeability
  - Airtightness
  - Aire quality, environmental controls, and whole-house ventilation
- Thermal control for reduced energy usage
  - o Enhanced envelope assembly R-Values and window/door U-Values
  - $\circ$  ~ Solar Heat Gain Coefficient and orientation of windows and doors
- High-efficiency water heating & HVAC equipment
- ENERGY STAR appliances
- High-efficiency lighting
- Low-flow water fixtures

Assemblies and systems for the proposed residences shall be specified during the Building Permit Application phase.

Thank you,

Margaret Randolph, RA, NCARB, AIA, LEED AP ND

635 Sagamore Avenue (LU-24-34) Staff Comments for TAC Meeting

"not type B soils due to shallow ledge"

The dominant soil unit mapped on the site was 41- a complex of soil types so intermixed that no one soil can be separated into a single consociation or soil type. The complex is named Chatfield-Hollis-Rock Outcrop. Based upon the test pits (3 Hollis, 6 Chatfield (Chatfield well drained and Chatfield moderately well drained) and one deep soil), the percentage of each soil type was 50% Chatfield, 25% Hollis, and 25% Rock Outcrop. The standard protocol is to utilize the dominant soil type for Hydrologic Soil Group, which is Chatfield (well drained and moderately well drained) with a Hydrologic Soil Group of B. Chatfield has a depth of 20 to 40 inches to bedrock. The Hydrologic Soil Groups are assigned to soil units by Publication Number 5 of the Society of Soil Scientists of Northern New England and adopted by NH DES Alteration of Terrain.

Hollis has a soil depth of 10 to 20 inches to bedrock. It also has a combined Hydrologic Soil Group of C/D. Rock Outcrop is any area that has surface exposed bedrock to 10 inches deep.

Typically for drainage analysis, the dominant hydrologic soil group is used, in this case B. Conversely, a weighted average could be used to mimic the complex: 50% B, 25% C/D, and 25% D-virtually impervious.

Complexes are difficult to interpret given that multiple soil types are present and randomly intermixed. It becomes even more difficult when the multiple soil types have differing characteristics.

Jim Gove, CSS #004

4-1-2024

## **DRAINAGE ANALYSIS**

## SEDIMENT AND EROSION CONTROL PLAN

"Luster Cluster" 635 Sagamore Ave. Portsmouth, NH 03801 Tax Map 222, Lot 19

**Prepared for:** 

635 Sagamore Development LLC 3612 Lafayette Rd., Dept 4 Portsmouth, NH 03801



Prepared by: Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885 (603) 772-4746 March 14, 2024 Revised April 18, 2024 JBE Project No. 18134.1

#### **EXECUTIVE SUMMARY**

635 Sagamore Development LLC proposes to demolish an existing commercial development and construct a 4-unit multi-family residential site on the subject parcel located at 635 Sagamore Ave. in Portsmouth, NH. In the existing condition, the subject parcel is home to two buildings and a paved parking area that used to comprise the "Luster King," a former auto detailing business that has since closed.

A drainage analysis of the entire site as well as offsite contributing watershed area was conducted for the purpose of estimating the peak rate of stormwater runoff and to subsequently design adequate drainage structures. Two models were compiled, one for the area in its existing (pre-construction) condition, and a second for its proposed (post-construction) condition. The analysis was conducted using data for the 2 Year – 24 Hour (3.70"), 10 Year – 24 Hour (5.61"), 25 Year – 24 Hour (7.12"), and 50 Year – 24 Hour (8.53") storm events using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment. This data was taken from the Extreme Precipitation Tables developed by the Northeast Regional Climate Center (NRCC), and the values have been increased by 15% due to the project being within the Coastal/Great Bay Region. A summary of the existing and proposed conditions peak rates of runoff toward the three analysis points and toward the existing drainage ditch on the Tidewatch Condominium property (Reach 1R) in units of cubic feet per second (cfs) is as follows:

<b>Analysis Point</b>	2 Y	ear	10 Y	'ear	25 Year		50 Y	lear
	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Analysis Point #1	0.75	0.35	1.33	0.67	1.78	0.93	2.21	1.17
Analysis Point #2	0.20	0.02	0.44	0.08	0.65	0.12	0.84	0.17
Analysis Point #3	0.91	0.71	2.86	2.12	4.73	3.47	6.61	5.03
Reach #1R	0.51	0.48	1.75	1.47	2.94	2.41	4.17	3.98

A similar summary of the existing and proposed peak volumes in units of acre-feet is as follows:

<b>Analysis Point</b>	2 Y	ear	10 Y	'ear	ar 25 Y		50 Y	Year
	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Analysis Point #1	0.054	0.025	0.098	0.048	0.133	0.068	0.167	0.087
Analysis Point #2	0.015	0.002	0.032	0.006	0.047	0.009	0.061	0.013
Analysis Point #3	0.118	0.118	0.302	0.279	0.477	0.436	0.656	0.629
Reach #1R	0.069	0.086	0.187	0.200	0.300	0.312	0.418	0.460

Although the volume of runoff directed toward Reach 1R is slightly increasing, the flow toward this reach is being reduced and the peak elevation will remain the same or be decreased in the proposed condition and the volume of runoff directed toward the downstream analysis point (AP3) is being reduced as well. A comparison of the peak elevations within the ditch pre- to post-construction is below:

<b>Peak Elevation</b>	2 Year		10 Year		25 Year		50 Year	
	Pre	Post	Pre Post		Pre	Post	Pre	Post
Reach #1R	0.18'	0.18'	0.34'	0.32'	0.44'	0.40'	0.52'	0.51'

Peak flows and volumes are being reduced in the post-construction condition toward all analysis points during all analyzed storm events. The subject parcel is located in the Single Residence A (SRA) Zoning District. The subject parcel currently consists of the aforementioned former commercial site which is proposed to be demolished. Despite impervious surface existing on the subject parcel now, the proposed development results in an increase in impervious surface on the subject parcel. The addition of the proposed impervious surfaces causes an increase in the curve number ( $C_n$ ) and a decrease in the time of concentration (T<sub>c</sub>), and if a stormwater management system were not implemented, the net result of this would be a potential increase in peak rates of runoff from the site. In order to avoid this potential, a stormwater management system has been designed, consisting of a bioretention system with deep sump catch basins for pre-treatment of runoff, and stone drip edges. Due to the use of these stormwater management features, the peak flow and volume of runoff will be reduced toward all analysis points during all analyzed storm events in the proposed condition as compared to the existing condition, and the treatment requirements of the City of Portsmouth are met. Additionally, the NHDES Alteration of Terrain Bureau's groundwater recharge volume and channel protection requirements are met with the proposed development. The stormwater management system as designed meets all requirements of the City of Portsmouth stormwater regulations per Section 7.1 and 7.4-7.6 of the Site Plan Review Regulations. Additionally, the stormwater management system as designed meets all requirements of the NHDES Alteration of Terrain (AOT) Bureau, even though an AOT permit is not necessary for this project due to the area of disturbance.

The use of Best Management Practices per the NHDES <u>Stormwater Manual</u> have been applied to the design of this stormwater management system and will be observed during all stages of construction. All land disturbed during construction will be stabilized within thirty days of groundbreaking and abutting property owners will suffer minimal adversity resultant to this development.

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#### 1.0 RAINFALL CHARACTERISTICS

This drainage report includes an existing conditions analysis of the area involved in the proposed development, as well as a proposed condition, or post-construction analysis, of the same area. These analyses were accomplished using the USDA SCS TR-20 Method within the HydroCAD 10.20-3c Stormwater Modeling System. The curve numbers were developed using the SCS TR-55 Runoff Curve numbers for Urban Areas. A Type III SCS 24-hour rainfall distribution was utilized in analyzing the data for the 2 Year – 24 Hour (3.70"), 10 Year – 24 Hour (5.61"), 25 Year – 24 Hour (7.12"), and 50 Year – 24 Hour (8.53") storm events. This data was taken from the Extreme Precipitation Tables developed by the Northeast Regional Climate Center (NRCC), and the values have been increased by 15% due to the project being within the Coastal/Great Bay Region.

The peak rates of runoff will be reduced from the existing condition, thereby minimizing any potential for a negative impact on abutting properties. This is accomplished through treatment of stormwater runoff and attenuation of peak flows and volumes resulting from storm events.

#### 2.0 EXISTING CONDITIONS ANALYSIS

In the existing condition, the site consists of two commercial buildings as well as a shed and a paved parking area that comprise the former Luster King auto detailing business, which has since closed. Most of the area behind the existing commercial development is wooded with light underbrush and large ledge outcrops. Due to these features of the woodlands, the woods area has been modelled as "fair" rather than "good" for the purposes of stormwater runoff calculations. There is some lawn space around the existing developed area as well.

The existing topography and roof ridges divide the subject parcel and offsite contributing watershed areas into four subcatchments, draining toward three analysis points. Subcatchment 1 represents the front of the subject parcel as well as a stretch of the northbound lane of Sagamore Avenue. This subcatchment is entirely developed in the existing condition, and it drains directly into the Sagamore Ave. right of way, modelled as Analysis Point 1.

Subcatchment 2S represents a small section of the developed portion of the property which drains to the north and on to abutting Tax Map 222, Lot 20, modelled as Analysis Point 2. It is very important that peak flows and volumes draining toward Analysis Points 1 and 2 are reduced in the post-construction condition, as these two analysis points represent a highway and a house lot, respectively.

The largest subcatchment is Subcatchment 3S. Subcatchment 3S is roughly the western quarter of the property and it consists primarily of woodland with large ledge outcrops. Subcatchment 3S drains toward an existing drainage ditch alongside and below the grade of the Tidewatch Condominium private roadway, which is curbed so that no runoff from the roadway itself enters the ditch. This drainage ditch is modelled as Reach 1R and it drains toward Analysis Point 3. Analysis Point 3 is an existing catch basin adjacent to the community mailbox structure for Tidewatch Condominiums.

Finally, a section of both developed and undeveloped land in the western end of the property drains into abutting woodland on the Tidewatch Condominium property and ultimately toward the aformemntioned catch basin that is modelled as Analysis Point 3.

Existing soil types were determined through a Site Specific Soil Survey conducted by a Certified Soil Scientist. The pervious soils are categorized into Hydrologic Soil Group (HSG) B while the

impervious areas of the subject parcel are categorized as Urban Land (SSS Symbol 699). The pervious sections of the property are represented as Chatfield-Hollis-Rock Outcrop complex and Chatfield Variant (moderately well drained). According to "Ksat Values for New Hampshire Soils," Special Publication No. 5 sponsored by the Society of Soil Scientists of Northern New England (SSSNNE), Chatfield, Chatfield Variant, and Hollis soils all have identical saturated hydraulic conductivity ranges in the B and C horizons. The saturated hydraulic conductivity (Ksat) value for these soils ranges from 0.6 to 6.0 inches/hour within both the B and C horizons. Therefore, in accordance with standard engineering practice, the lowest published Ksat of 0.6 in/hr for these soils types was divided by two in order to determine an appropriate Ksat of **0.3 in/hr** to use for design.

#### 3.0 PROPOSED CONDITIONS ANALYSIS

The addition of the proposed impervious surfaces causes an increase in the curve number (C<sub>n</sub>) and a decrease in the time of concentration  $(T_c)$ , and if a stormwater management system were not implemented, the net result of this would be a potential increase in peak rates of runoff from the site. A stormwater management system was designed in order to avoid this potential. The proposed development, consisting of the aforementioned four (4) residential units with associated paved roadway and driveways as well as stormwater management features divide the subject parcel into fifteen (15) subcatchments. Subcatchments 1S, 2S, and 4S drain directly toward Analysis Points 1-3, respectively, as previously outlined. Subcatchment 3S drains toward the existing drainage ditch on the Tidewatch Condominium property, modelled as Reach 1R, which ultimately outlets toward AP3, the same as in the existing condition. Subcatchment 5S has been removed from the drainage analysis as it was the subcatchment associated with a stormwater pond that has since been removed from the drainage design. Subcatchments 6S-9S drain through deep sump catch basins into a closed drainage system which outlets toward a bioretention pond modelled as Pond 1P. The deep sump catch basins provide pre-treatment of runoff reaching the bioretention pond in lieu of a sediment forebay. The bioretention pond is designed to treat and infiltrate runoff directed toward it during smaller storms, or in larger storms, infiltrate as much as possible and attenuate and slowly discharge outflow. Any discharge from Pond 1P follows a path through Subcatchment 3S represented as Reach 4R, toward Reach 1R, the existing ditch on the Tidewatch condominium property leading to Analysis Point 3.

Subcatchments 10S-12S consist of lawn and roof areas that drain toward yard drains 1-3, respectively. The runoff that is caught by these yard drains additionally enters the previously described closed drainage system that outlets toward Pond 1P.

Subcatchments 13S, 14S, and 15S represent roof and deck areas on Units 3-4 which are routed toward infiltration systems adjacent to the units such as stone drip edges and stone underneath a deck. These devices are only featured in areas where the basement grade will be above the seasonal high water table and the top of ledge. These devices are modelled as Ponds 2P-4P.

Finally, Subcatchment 18S represents the grassed and roof area that drains directly toward Pond 1P without passing through the closed drainage system in the proposed condition.

As a result of the implementation of this stormwater management system, peak flows and runoff volumes are reduced toward all three analysis points during all analyzed storm events in the proposed condition as compared with the existing condition. The NHDES Alteration of Terrain Bureau allows an increase in runoff volume of up to 0.1 acre-feet during the 2-year 24-hour storm event. We are decreasing runoff volumes and therefore this would be approvable by the AOT Bureau if the project needed an AOT permit (which it does not as the area of disturbance is below 100,000 SF).

Furthermore, the project as designed exceeds the AOT Bureau's groundwater recharge volume requirement. A GRV worksheet is contained within the appendix of this report in order to illustrate this. Therefore, we have designed the drainage system to avoid adverse impacts to abutting infrastructure and the requirement per Section 7.1 of the Site Plan Review Regulations to "design practices to the maximum extent practical (MEP) to reduce stormwater runoff volumes, maintain predevelopment site hydrology, and protect water quality in receiving waters" is met. Furthermore, rain gardens (also known as bioretention systems) are recommended as a Low Impact Development practice in this same section of the regulations. We are using bioretention systems to treat and attenuate runoff from paved areas of the subject parcel in the proposed condition.

According to the NH Stormwater Manual, bioretention systems provide a pollutant removal efficiency of 90% for TSS and 65% for nitrogen, and drip edges provide a removal efficiency of 90% for TSS and 55% for nitrogen. The City of Portsmouth Site Plan Review Regulations stipulate that stormwater BMPs shall either be designed for 80% TSS removal and 50% nitrogen removal of stormwater runoff from impervious surfaces. This plan exceeds the requirements for pollutant removal because appropriate treatment / groundwater recharge systems are proposed and the Water Quality Volume is retained and treated. A breakdown of pollutant removal efficiencies for the entire site is contained within the appendix of this report.

#### 5.0 CONCLUSION

This proposed site development will have minimal adverse effect on abutting infrastructures, properties, and downstream wetlands by way of stormwater runoff or siltation. Appropriate steps will be taken to eliminate erosion and sedimentation; these will be accomplished through the construction of a drainage system consisting of site grading, catch basins, yard drains, a bioretention system, stone drip edges, and temporary erosion control measures including but not limited to silt fence and the use of a stabilized construction entrance. Best Management Practices developed by the State of New Hampshire have been utilized in the design of this system and their application will be enforced throughout the construction process. Peak rates of runoff from the site will be reduced toward all analysis points during all analyzed storm events.

This project disturbs less than 100,000 S.F. and does <u>not</u> require a NHDES Alteration of Terrain Permit.

Respectfully Submitted, JONES & BEACH ENGINEERS. INC.

Meelit

Daniel Meditz, P.E Project Engineer
# APPENDIX I

# EXISTING CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Complete 10 YEAR Summary 25 YEAR Complete 50 YEAR



# Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.547	61	>75% Grass cover, Good, HSG B (1S, 2S, 3S, 4S)
0.230	98	Paved parking, HSG B (1S, 2S, 4S)
0.114	98	Roofs, HSG B (1S, 2S, 3S, 4S)
1.538	60	Woods, Fair, HSG B (2S, 3S, 4S)
2.429	66	TOTAL AREA

# Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
2.429	HSG B	1S, 2S, 3S, 4S
0.000	HSG C	
0.000	HSG D	
0.000	Other	
2.429		TOTAL AREA

18134-EXISTING	Type III 24-hr	2 Yr 24 Hr +15% Rainfall=3.70"
Prepared by Jones & Beach Engineers Inc		Printed 4/19/2024
HydroCAD® 10.20-3c s/n 00762 © 2023 HydroCAD Softwar	e Solutions LLC	Page 4

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=13,001 sf 64.94% Impervious Runoff Depth>2.19" Flow Length=187' Tc=6.0 min CN=85 Runoff=0.75 cfs 0.054 af
Subcatchment2S: Subcatchment2S	Runoff Area=6,082 sf 32.08% Impervious Runoff Depth>1.31" Flow Length=114' Tc=6.0 min CN=73 Runoff=0.20 cfs 0.015 af
Subcatchment3S: Subcatchment3S	Runoff Area=58,629 sf 0.32% Impervious Runoff Depth>0.62" Flow Length=291' Tc=17.0 min CN=60 Runoff=0.51 cfs 0.069 af
Subcatchment4S: Subcatchment4S	Runoff Area=28,091 sf 15.59% Impervious Runoff Depth>0.91" Flow Length=216' Tc=11.5 min CN=66 Runoff=0.49 cfs 0.049 af
Reach 1R: Ditch on Tidewatch Proper n=0.030	<b>ty</b> Avg. Flow Depth=0.18' Max Vel=1.77 fps Inflow=0.51 cfs 0.069 af L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=0.51 cfs 0.069 af
Reach AP1: Analysis Point 1	Inflow=0.75 cfs 0.054 af Outflow=0.75 cfs 0.054 af
Reach AP2: Analysis Point 2	Inflow=0.20 cfs 0.015 af Outflow=0.20 cfs 0.015 af
Reach AP3: Analysis Point 3	Inflow=0.91 cfs 0.118 af Outflow=0.91 cfs 0.118 af
Total Dunoff Area - 2	420 co. Bunoff Volume = 0.499 of Average Bunoff Denth = 0.0

Total Runoff Area = 2.429 ac Runoff Volume = 0.188 af Average Runoff Depth = 0.93" 85.86% Pervious = 2.085 ac 14.14% Impervious = 0.343 ac

18134-EXISTING	Type III 24-hr	10 Yr 24 Hr +15% Rainfall=5.61"
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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=13,001 sf 64.94% Impervious Runoff Depth>3.93" Flow Length=187' Tc=6.0 min CN=85 Runoff=1.33 cfs 0.098 af
Subcatchment2S: Subcatchment2S	Runoff Area=6,082 sf 32.08% Impervious Runoff Depth>2.77" Flow Length=114' Tc=6.0 min CN=73 Runoff=0.44 cfs 0.032 af
Subcatchment3S: Subcatchment3S	Runoff Area=58,629 sf 0.32% Impervious Runoff Depth>1.66" Flow Length=291' Tc=17.0 min CN=60 Runoff=1.75 cfs 0.187 af
Subcatchment4S: Subcatchment4S	Runoff Area=28,091 sf 15.59% Impervious Runoff Depth>2.15" Flow Length=216' Tc=11.5 min CN=66 Runoff=1.31 cfs 0.116 af
Reach 1R: Ditch on Tidewatch Proper n=0.030	<b>ty</b> Avg. Flow Depth=0.34' Max Vel=2.48 fps Inflow=1.75 cfs 0.187 af L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=1.74 cfs 0.186 af
Reach AP1: Analysis Point 1	Inflow=1.33 cfs 0.098 af Outflow=1.33 cfs 0.098 af
Reach AP2: Analysis Point 2	Inflow=0.44 cfs 0.032 af Outflow=0.44 cfs 0.032 af
Reach AP3: Analysis Point 3	Inflow=2.86 cfs 0.302 af Outflow=2.86 cfs 0.302 af
Total Dunoff Area - 2	420 co. Bunoff Volume = 0.422 of Average Bunoff Douth = 2.4

Total Runoff Area = 2.429 ac Runoff Volume = 0.432 af Average Runoff Depth = 2.14" 85.86% Pervious = 2.085 ac 14.14% Impervious = 0.343 ac

#### Summary for Subcatchment 1S: Subcatchment 1S

Runoff 1.33 cfs @ 12.09 hrs, Volume= 0.098 af, Depth> 3.93" = Routed to Reach AP1 : Analysis Point 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	Area (sf)	CN	Description						
	1,476	98	98 Roofs, HSG B						
	6,967	98	8 Paved parking, HSG B						
	4,558	61	>75% Gras	s cover, Go	bod, HSG B				
	13,001	85	Weighted A	verage					
	4,558		35.06% Per	vious Area	l de la constante d				
	8,443		64.94% Imp	pervious Ar	ea				
Т	c Length	Slope	e Velocity	Capacity	Description				
(mir	i) (feet)	(ft/ft	) (ft/sec)	(cfs)					
2.	5 46	0.109	0.31		Sheet Flow,				
					Grass: Short n= 0.150 P2= 3.70"				
0.	4 45	0.067	0 2.04		Sheet Flow,				
					Smooth surfaces n= 0.011 P2= 3.70"				
0.	4 96	0.036	0 3.85		Shallow Concentrated Flow,				
					Paved Kv= 20.3 fps				
3	3 197	Total	Increased t	o minimum	$T_{c} = 6.0 \text{ min}$				

Lotal, Increased to minimum Ic = 6.0 min 3.3 107

#### Summary for Subcatchment 2S: Subcatchment 2S

0.032 af, Depth> 2.77" Runoff 0.44 cfs @ 12.09 hrs, Volume= = Routed to Reach AP2 : Analysis Point 2

Area (sf)	CN	Description		
482	98	Roofs, HSG B		
1,469	98	Paved parking, HSG B		
3,981	3,981 61 >75% Grass cover, Good, HSG B			
150	60	Woods, Fair, HSG B		
6,082	73	Weighted Average		
4,131 67.92% Pervious		67.92% Pervious Area		
1,951		32.08% Impervious Area		

#### 18134-EXISTING

Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

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Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.7	53	0.0200	1.30		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.70"
2.8	47	0.0810	0.28		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
0.1	14	0.2100	3.21		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
3.6	114	Total, I	ncreased t	o minimum	Tc = 6.0 min

# Summary for Subcatchment 3S: Subcatchment 3S

Runoff	=	1.75 cfs @	12.26 hrs,	Volume=	0.187 af,	Depth>	1.66"
Routed	to Read	ch 1R : Ditch o	on Tidewate	ch Property			

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

	A	rea (sf)	CN [	Description		
		187	98 F	Roofs, HSC	БB	
		9,391	61 >	75% Gras	s cover, Go	ood, HSG B
_		49,051	60 V	Voods, Fai	r, HSG B	
		58,629	60 V	Veighted A	verage	
		58,442	ç	9.68% Pei	vious Area	
		187	C	).32% Impe	ervious Area	a
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	9.0	53	0.0415	0.10		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	5.8	47	0.0968	0.13		Sheet Flow,
				4 50		Woods: Light underbrush n= 0.400 P2= 3.70"
	0.2	15	0.0968	1.56		Shallow Concentrated Flow,
	07	<b>F</b> 4	0 0744	4.00		Woodland KV= 5.0 fps
	0.7	54	0.0741	1.30		Shallow Concentrated Flow,
	1 2	100	0 1000	1 50		woodland KV= 5.0 lps
	1.5	122	0.1000	1.00		Woodland Ky= 5.0 fps
-	47.0	204	Tatal			
	17.0	291	TO(a)			

#### Summary for Subcatchment 4S: Subcatchment 4S

Runoff	=	1.31 cfs @	12.17 hrs,	Volume=	0.116 af,	Depth>	2.15"
Routed	to Rea	ch AP3 : Anal	ysis Point 3	5			

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

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Α	rea (sf)	CN	Description					
	2,809	98	Roofs, HSG B					
	1,571	98	Paved park	ing, HSG B	3			
	5,912	61	>75% Ġras	s cover, Go	bod, HSG B			
	17,799	60	Noods, Fai	r, HSG B				
	28,091	66	Neighted A	verage				
	23,711	1	34.41% Pe	rvious Area				
	4,380		15.59% Imp	pervious Ar	ea			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
1.9	14	0.0210	0.13		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.70"			
8.4	86	0.1280	0.17		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 3.70"			
1.0	87	0.0800	1.41		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
0.2	29	0.2860	2.67		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
11.5	216	Total						

#### Summary for Reach 1R: Ditch on Tidewatch Property

 Inflow Area =
 1.346 ac,
 0.32% Impervious, Inflow Depth >
 1.66" for 10 Yr 24 Hr +15% event

 Inflow =
 1.75 cfs @
 12.26 hrs, Volume=
 0.187 af

 Outflow =
 1.74 cfs @
 12.27 hrs, Volume=
 0.186 af, Atten= 0%, Lag= 0.7 min

 Routed to Reach AP3 : Analysis Point 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 2.48 fps, Min. Travel Time= 1.1 min Avg. Velocity = 1.11 fps, Avg. Travel Time= 2.4 min

Peak Storage= 112 cf @ 12.27 hrs Average Depth at Peak Storage= 0.34', Surface Width= 3.07' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.18 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 7.00' Length= 159.0' Slope= 0.0189 '/' Inlet Invert= 38.00', Outlet Invert= 35.00'

## Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	0.298 ac, 6	64.94% Impe	ervious,	Inflow Depth >	3.93"	for 10	Yr 24 Hr +15%	event
Inflow	=	1.33 cfs @	12.09 hrs,	Volume	= 0.098	3 af			
Outflow	=	1.33 cfs @	12.09 hrs,	Volume	= 0.098	3 af, Atte	en= 0%,	Lag= 0.0 min	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

#### Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	Area =	0.140 ac, 32.08% Impervious, Inflow	v Depth > 2.77" for 10 Yr 24 Hr +15% ever	٦t
Inflow	=	0.44 cfs @ 12.09 hrs, Volume=	0.032 af	
Outflow	v =	0.44 cfs @ 12.09 hrs, Volume=	0.032 af, Atten= 0%, Lag= 0.0 min	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

#### Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow /	Area =	1.991 ac,	5.27% Impervious, Inflow	v Depth > 1.82"	for 10 Yr 24 Hr +15% event
Inflow	=	2.86 cfs @	12.23 hrs, Volume=	0.302 af	
Outflov	v =	2.86 cfs @	12.23 hrs, Volume=	0.302 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

18134-EXISTING	Type III 24-hr 25 Yr 24 Hr +15% Rainfall=7.12'
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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=13,001 sf 64.94% Impervious Runoff Depth>5.36" Flow Length=187' Tc=6.0 min CN=85 Runoff=1.78 cfs 0.133 af
Subcatchment2S: Subcatchment2S	Runoff Area=6,082 sf 32.08% Impervious Runoff Depth>4.04" Flow Length=114' Tc=6.0 min CN=73 Runoff=0.65 cfs 0.047 af
Subcatchment3S: Subcatchment3S	Runoff Area=58,629 sf 0.32% Impervious Runoff Depth>2.68" Flow Length=291' Tc=17.0 min CN=60 Runoff=2.94 cfs 0.300 af
Subcatchment4S: Subcatchment4S	Runoff Area=28,091 sf 15.59% Impervious Runoff Depth>3.29" Flow Length=216' Tc=11.5 min CN=66 Runoff=2.05 cfs 0.177 af
Reach 1R: Ditch on Tidewatch Proper n=0.030	<b>ty</b> Avg. Flow Depth=0.44' Max Vel=2.85 fps Inflow=2.94 cfs 0.300 af L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=2.94 cfs 0.300 af
Reach AP1: Analysis Point 1	Inflow=1.78 cfs 0.133 af Outflow=1.78 cfs 0.133 af
Reach AP2: Analysis Point 2	Inflow=0.65 cfs 0.047 af Outflow=0.65 cfs 0.047 af
Reach AP3: Analysis Point 3	Inflow=4.73 cfs 0.477 af Outflow=4.73 cfs 0.477 af
Total Dunoff Area - 2	420 co. Dunoff Volume = 0.050 cf. Average Dunoff Donth = 2.2

Total Runoff Area = 2.429 acRunoff Volume = 0.658 afAverage Runoff Depth = 3.25"85.86% Pervious = 2.085 ac14.14% Impervious = 0.343 ac

18134-EXISTING	Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"
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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=13,001 sf 64.94% Impervious Runoff Depth>6.72" Flow Length=187' Tc=6.0 min CN=85 Runoff=2.21 cfs 0.167 af
Subcatchment2S: Subcatchment2S	Runoff Area=6,082 sf 32.08% Impervious Runoff Depth>5.28" Flow Length=114' Tc=6.0 min CN=73 Runoff=0.84 cfs 0.061 af
Subcatchment3S: Subcatchment3S	Runoff Area=58,629 sf 0.32% Impervious Runoff Depth>3.72" Flow Length=291' Tc=17.0 min CN=60 Runoff=4.17 cfs 0.418 af
Subcatchment4S: Subcatchment4S	Runoff Area=28,091 sf 15.59% Impervious Runoff Depth>4.44" Flow Length=216' Tc=11.5 min CN=66 Runoff=2.78 cfs 0.238 af
Reach 1R: Ditch on Tidewatch Proper n=0.030	<b>ty</b> Avg. Flow Depth=0.52' Max Vel=3.12 fps Inflow=4.17 cfs 0.418 af L=159.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=4.17 cfs 0.417 af
Reach AP1: Analysis Point 1	Inflow=2.21 cfs 0.167 af Outflow=2.21 cfs 0.167 af
Reach AP2: Analysis Point 2	Inflow=0.84 cfs 0.061 af Outflow=0.84 cfs 0.061 af
Reach AP3: Analysis Point 3	Inflow=6.61 cfs 0.656 af Outflow=6.61 cfs 0.656 af
Total Dupoff Area = 2	420 co. Bunoff Valuma = 0.994 of Average Bunoff Donth = 4.2

Total Runoff Area = 2.429 ac Runoff Volume = 0.884 af Average Runoff Depth = 4.37" 85.86% Pervious = 2.085 ac 14.14% Impervious = 0.343 ac

#### Summary for Subcatchment 1S: Subcatchment 1S

2.21 cfs @ 12.09 hrs, Volume= Runoff 0.167 af, Depth> 6.72" = Routed to Reach AP1 : Analysis Point 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description						
	1,476	98	Roofs, HSG B						
	6,967	98	Paved park	Paved parking, HSG B					
	4,558	61	>75% Gras	s cover, Go	bod, HSG B				
	13,001	85	Weighted A	verage					
	4,558		35.06% Per	vious Area					
	8,443		64.94% Imp	pervious Ar	ea				
Tc	Length	Slope	e Velocity	Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft	) (ft/sec)	(cfs)					
2.5	46	0.109	0 0.31		Sheet Flow,				
					Grass: Short n= 0.150 P2= 3.70"				
0.4	45	0.067	0 2.04		Sheet Flow,				
					Smooth surfaces n= 0.011 P2= 3.70"				
0.4	96	0.036	0 3.85		Shallow Concentrated Flow,				
					Paved Kv= 20.3 fps				
23	187	Total	Increased t	o minimum	$T_{c} = 6.0 \text{ min}$				

Lotal, Increased to minimum 1c = 6.0 min 3.3 107

#### Summary for Subcatchment 2S: Subcatchment 2S

Runoff 0.84 cfs @ 12.09 hrs, Volume= 0.061 af, Depth> 5.28" = Routed to Reach AP2 : Analysis Point 2

Area (sf)	CN	Description					
482	98	Roofs, HSG B					
1,469	98	Paved parking, HSG B					
3,981	61	>75% Grass cover, Good, HSG B					
150	60	Woods, Fair, HSG B					
6,082	73	Weighted Average					
4,131		67.92% Pervious Area					
1,951		32.08% Impervious Area					

#### 18134-EXISTING

Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53" Printed 4/19/2024

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.7	53	0.0200	1.30		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.70"
2.8	47	0.0810	0.28		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
0.1	14	0.2100	3.21		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
3.6	114	Total, I	ncreased t	o minimum	Tc = 6.0 min

#### Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 4.17 cfs @ 12.24 hrs, Volume= 0.418 af, Depth> 3.72" Routed to Reach 1R : Ditch on Tidewatch Property

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	A	rea (sf)	CN [	Description		
		187	98 F	Roofs, HSC	БB	
9,391 61 >75% Grass cover, Good, H					s cover, Go	ood, HSG B
_		49,051	60 V	Voods, Fai	r, HSG B	
		58,629	60 V	Veighted A	verage	
		58,442	ç	9.68% Pei	vious Area	
		187	C	).32% Impe	ervious Area	a
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	9.0	53	0.0415	0.10		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.70"
	5.8	47	0.0968	0.13		Sheet Flow,
				4 50		Woods: Light underbrush n= 0.400 P2= 3.70"
	0.2	15	0.0968	1.56		Shallow Concentrated Flow,
	07	<b>F</b> 4	0 0744	4.00		Woodland KV= 5.0 fps
	0.7	54	0.0741	1.30		Shallow Concentrated Flow,
	1 2	100	0 1000	1 50		woodland KV= 5.0 lps
	1.5	122	0.1000	1.00		Woodland Ky= 5.0 fps
-	47.0	204	Tatal			
	17.0	291	TO(a)			

#### Summary for Subcatchment 4S: Subcatchment 4S

Runoff	=	2.78 cfs @	12.16 hrs,	Volume=	0.238 af,	Depth>	4.44"
Routed	l to R	Reach AP3 : Anal	ysis Point 3			-	

Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

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A	rea (sf)	CN I	Description		
	2,809	98	Roofs, HSG	βB	
	1,571	98	Paved park	ing, HSG B	
	5,912	61 :	>75% Ġras	s cover, Go	ood, HSG B
	17,799	60	Noods, Fai	r, HSG B	
	28,091	66	Neighted A	verage	
	23,711	8	34.41% Pe	rvious Area	
	4,380		15.59% Imp	pervious Ar	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
1.9	14	0.0210	0.13		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
8.4	86	0.1280	0.17		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
1.0	87	0.0800	1.41		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.2	29	0.2860	2.67		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
11.5	216	Total			

#### Summary for Reach 1R: Ditch on Tidewatch Property

 Inflow Area =
 1.346 ac,
 0.32% Impervious, Inflow Depth >
 3.72" for 50 Yr 24 Hr +15% event

 Inflow =
 4.17 cfs @
 12.24 hrs, Volume=
 0.418 af

 Outflow =
 4.17 cfs @
 12.26 hrs, Volume=
 0.417 af, Atten= 0%, Lag= 0.7 min

 Routed to Reach AP3 : Analysis Point 3
 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 3.12 fps, Min. Travel Time= 0.8 min Avg. Velocity = 1.34 fps, Avg. Travel Time= 2.0 min

Peak Storage= 212 cf @ 12.26 hrs Average Depth at Peak Storage= 0.52', Surface Width= 4.12' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.18 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 7.00' Length= 159.0' Slope= 0.0189 '/' Inlet Invert= 38.00', Outlet Invert= 35.00'

### Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	a =	0.298 ac, 64.94% Impervious, Inflow	Depth > 6.72" for 50 Yr 24 Hr	+15% event
Inflow	=	2.21 cfs @ 12.09 hrs, Volume=	0.167 af	
Outflow	=	2.21 cfs @ 12.09 hrs, Volume=	0.167 af, Atten= 0%, Lag= 0.0	min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

#### Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	Area =	0.140 ac, 32.08% Impervious, Inflo	w Depth > 5.28" for 50 Yr 24 Hr +15% ever	nt
Inflow	=	0.84 cfs @ 12.09 hrs, Volume=	0.061 af	
Outflow	/ =	0.84 cfs @ 12.09 hrs, Volume=	0.061 af, Atten= 0%, Lag= 0.0 min	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

#### Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	Area =	1.991 ac,	5.27% Impervious, In	flow Depth > 3.95"	for 50 Yr 24 Hr +15% event
Inflow	=	6.61 cfs @	12.22 hrs, Volume=	0.656 af	
Outflow	v =	6.61 cfs @	12.22 hrs, Volume=	0.656 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

# APPENDIX II

# PROPOSED CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Complete 10 YEAR Summary 25 YEAR Complete 50 YEAR



# Area Listing (all nodes)

	Area	CN	Description
(	acres)		(subcatchment-numbers)
	1.116	61	>75% Grass cover, Good, HSG B (1S, 2S, 3S, 4S, 10S, 11S, 12S, 18S)
	0.253	98	Paved parking, HSG B (1S, 6S, 7S, 8S, 9S, 10S, 11S, 18S)
	0.226	98	Roofs, HSG B (3S, 4S, 8S, 10S, 11S, 12S, 13S, 14S, 15S, 18S)
	0.008	98	Water Surface, HSG B (13S, 15S)
	0.826	60	Woods, Fair, HSG B (3S, 4S)
	2.429	68	TOTAL AREA

# Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
2.429	HSG B	1S, 2S, 3S, 4S, 6S, 7S, 8S, 9S, 10S, 11S, 12S, 13S, 14S, 15S, 18S
0.000	HSG C	
0.000	HSG D	
0.000	Other	
2.429		TOTAL AREA

18134-PROPOSED	Type III 24-hr	2 Yr 24 Hr +15% Rair	nfall=3.70"
Prepared by Jones & Beach Engineers Inc		Printed	4/19/2024
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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=7,392 sf 50.61% Impervious Runoff Depth>1.79" Flow Length=186' Tc=6.0 min CN=80 Runoff=0.35 cfs 0.025 af
Subcatchment2S: Subcatchment2S Flow Length=20	Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>0.66" Slope=0.0500 '/' Tc=6.0 min CN=61 Runoff=0.02 cfs 0.002 af
Subcatchment3S: Subcatchment3S	Runoff Area=45,177 sf 1.54% Impervious Runoff Depth>0.66" Flow Length=291' Tc=17.0 min CN=61 Runoff=0.44 cfs 0.057 af
Subcatchment4S: Subcatchment4S	Runoff Area=20,991 sf 8.04% Impervious Runoff Depth>0.81" Flow Length=210' Tc=7.9 min CN=64 Runoff=0.35 cfs 0.032 af
Subcatchment6S: Subcatchment6S	Runoff Area=1,952 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.16 cfs 0.013 af
Subcatchment7S: Subcatchment7S	Runoff Area=1,516 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.12 cfs 0.010 af
Subcatchment8S: Subcatchment8S	Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.24 cfs 0.020 af
Subcatchment9S: Subcatchment9S	Runoff Area=325 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.03 cfs 0.002 af
Subcatchment10S: Subcatchment10S	Runoff Area=3,630 sf 29.12% Impervious Runoff Depth>1.25" Flow Length=142' Tc=6.3 min CN=72 Runoff=0.11 cfs 0.009 af
Subcatchment11S: Subcatchment11S Flow Length=77	Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>1.72" Slope=0.0396 '/' Tc=6.0 min CN=79 Runoff=0.21 cfs 0.015 af
Subcatchment12S: Subcatchment12S Flow Length=51	Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>1.38" Slope=0.0320 '/' Tc=6.0 min CN=74 Runoff=0.13 cfs 0.010 af
Subcatchment13S: Subcatchment13S	Runoff Area=876 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment14S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment15S: Subcatchment15S	Runoff Area=876 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment18S: Subcatchment18S	Runoff Area=9,474 sf 14.12% Impervious Runoff Depth>0.91" Flow Length=58' Tc=6.0 min CN=66 Runoff=0.20 cfs 0.016 af
Reach 1R: Ditch on Tidewatch Property A n=0.030 L=15	vg. Flow Depth=0.18' Max Vel=1.74 fps Inflow=0.48 cfs 0.086 af 59.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=0.48 cfs 0.086 af

18134-PROPOSED	Type III 24-hr 2 Yr 24 Hr +15% Rainf	all=3.70"
Prepared by Jones & Beach Engineers Inc	Printed 4	/19/2024
HydroCAD® 10.20-3c s/n 00762 © 2023 HydroCAD	) Software Solutions LLC	Page 5
Reach 2R: Flow through 3S Avg. F n=0.030 L=81.0' S	Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs S=0.3457 '/' Capacity=740.30 cfs Outflow=0.00 cfs	0.000 af 0.000 af
Reach 4R: Flow Through 3S Avg. F n=0.030 L=220.0'	Flow Depth=0.01' Max Vel=0.94 fps Inflow=0.04 cfs S=0.0909 '/' Capacity=66.79 cfs Outflow=0.04 cfs	0.029 af 0.029 af
Reach AP1: Analysis Point 1	Inflow=0.35 cfs Outflow=0.35 cfs	0.025 af 0.025 af
Reach AP2: Analysis Point 2	Inflow=0.02 cfs Outflow=0.02 cfs	0.002 af 0.002 af
Reach AP3: Analysis Point 3	Inflow=0.71 cfs Outflow=0.71 cfs	0.118 af 0.118 af
Pond 1P: Bioretention Pond Discarded=0.08 cfs 0.0	Peak Elev=61.42' Storage=1,704 cf Inflow=1.20 cfs 063 af Primary=0.04 cfs 0.029 af Outflow=0.12 cfs	0.095 af 0.092 af
Pond 2P: Stone Drip Edge Discarded=0.00 cfs 0.003	Peak Elev=64.62' Storage=0.004 af Inflow=0.07 cfs af Secondary=0.00 cfs 0.000 af Outflow=0.00 cfs	0.006 af 0.003 af
Pond 3P: Stone Under Deck Discarded=0.00 cfs 0.003	Peak Elev=65.44' Storage=0.002 af Inflow=0.05 cfs af Secondary=0.00 cfs 0.000 af Outflow=0.00 cfs	0.004 af 0.003 af
Pond 4P: Stone Drip Edge Discarded=0.00 cfs 0.004	Peak Elev=63.39' Storage=0.003 af Inflow=0.07 cfs af Secondary=0.00 cfs 0.000 af Outflow=0.00 cfs	0.006 af 0.004 af
Pond CB101: Catch Basin 101 12.0" Round Culv	Peak Elev=62.62' Inflow=0.27 cfs vert n=0.012 L=19.0' S=0.0053 '/' Outflow=0.27 cfs	0.022 af 0.022 af
Pond CB102: Catch Basin 102 12.0" Round Culve	Peak Elev=62.47' Inflow=0.39 cfs ert n=0.012 L=147.0' S=0.0054 '/' Outflow=0.39 cfs	0.032 af 0.032 af
Pond CB103: Catch Basin 103 12.0" Round Culv	Peak Elev=66.74' Inflow=0.58 cfs vert n=0.012 L=43.0' S=0.0070 '/' Outflow=0.58 cfs	0.045 af 0.045 af
Pond CB104: Catch Basin 104 12.0" Round Culv	Peak Elev=61.79' Inflow=1.00 cfs vert n=0.012 L=45.0' S=0.0067 '/' Outflow=1.00 cfs	0.079 af 0.079 af
Pond YD1: Yard Drain 1 8.0" Round Cul	Peak Elev=63.01' Inflow=0.11 cfs Ivert n=0.012 L=9.0' S=0.0189 '/' Outflow=0.11 cfs	0.009 af 0.009 af
Pond YD2: Yard Drain 2 8.0" Round Culv	Peak Elev=67.39' Inflow=0.21 cfs vert n=0.012 L=52.0' S=0.0058 '/' Outflow=0.21 cfs	0.015 af 0.015 af
Pond YD3: Yard Drain 3 8.0" Round Culv	Peak Elev=68.23' Inflow=0.13 cfs vert n=0.012 L=13.0' S=0.0923 '/' Outflow=0.13 cfs	0.010 af 0.010 af
Total Runoff Area = 2.429 ac	Runoff Volume = 0.228 af Average Runoff De	pth = 1.12"

79.95% Pervious = 1.942 ac 20.05% Impervious = 0.487 ac

# **18134-PROPOSED** Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61" Prepared by Jones & Beach Engineers Inc Printed 4/19/2024 HydroCAD® 10.20-3c s/n 00762 © 2023 HydroCAD Software Solutions LLC

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=7,392 sf 50.61% Impervious Runoff Depth>3.43" Flow Length=186' Tc=6.0 min CN=80 Runoff=0.67 cfs 0.048 af
Subcatchment2S: Subcatchment2S Flow Length=20	Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>1.75" V Slope=0.0500 '/' Tc=6.0 min CN=61 Runoff=0.08 cfs 0.006 af
Subcatchment3S: Subcatchment3S	Runoff Area=45,177 sf 1.54% Impervious Runoff Depth>1.74" Flow Length=291' Tc=17.0 min CN=61 Runoff=1.42 cfs 0.151 af
Subcatchment4S: Subcatchment4S	Runoff Area=20,991 sf 8.04% Impervious Runoff Depth>1.99" Flow Length=210' Tc=7.9 min CN=64 Runoff=1.00 cfs 0.080 af
Subcatchment6S: Subcatchment6S	Runoff Area=1,952 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.24 cfs 0.020 af
Subcatchment7S: Subcatchment7S	Runoff Area=1,516 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.19 cfs 0.016 af
Subcatchment8S: Subcatchment8S	Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.37 cfs 0.031 af
Subcatchment9S: Subcatchment9S	Runoff Area=325 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.04 cfs 0.003 af
Subcatchment10S: Subcatchment10S	Runoff Area=3,630 sf 29.12% Impervious Runoff Depth>2.67" Flow Length=142' Tc=6.3 min CN=72 Runoff=0.25 cfs 0.019 af
Subcatchment11S: Subcatchment11S Flow Length=77	Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>3.33" " Slope=0.0396 '/' Tc=6.0 min CN=79 Runoff=0.40 cfs 0.029 af
Subcatchment12S: Subcatchment12S Flow Length=51	Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>2.86" ' Slope=0.0320 '/' Tc=6.0 min CN=74 Runoff=0.28 cfs 0.020 af
Subcatchment13S: Subcatchment13S	Runoff Area=876 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.11 cfs 0.009 af
Subcatchment14S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment15S: Subcatchment15S	Runoff Area=876 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.11 cfs 0.009 af
Subcatchment18S: Subcatchment18S	Runoff Area=9,474 sf 14.12% Impervious Runoff Depth>2.15" Flow Length=58' Tc=6.0 min CN=66 Runoff=0.53 cfs 0.039 af
Reach 1R: Ditch on Tidewatch Property n=0.030 L=1	Avg. Flow Depth=0.32' Max Vel=2.37 fps Inflow=1.47 cfs 0.200 af 59.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=1.47 cfs 0.199 af

18134-PROPOSED	Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61	"
Prepared by Jones & Beach Engineers Inc	Printed 4/19/2024	
HydroCAD® 10.20-3c s/n 00762 © 2023 HydroC	AD Software Solutions LLC Page 7	
Reach 2R: Flow through 3S Avg n=0.030 L=81.0	g. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af V S=0.3457 '/' Capacity=740.30 cfs Outflow=0.00 cfs 0.000 af	
Reach 4R: Flow Through 3S Avg n=0.030 L=220.	g. Flow Depth=0.02' Max Vel=0.98 fps Inflow=0.05 cfs 0.049 af .0' S=0.0909 '/' Capacity=66.79 cfs Outflow=0.05 cfs 0.049 af	
Reach AP1: Analysis Point 1	Inflow=0.67 cfs 0.048 af Outflow=0.67 cfs 0.048 af	
Reach AP2: Analysis Point 2	Inflow=0.08 cfs 0.006 af Outflow=0.08 cfs 0.006 af	
Reach AP3: Analysis Point 3	Inflow=2.12 cfs 0.279 af Outflow=2.12 cfs 0.279 af	
Pond 1P: Bioretention Pond Discarded=0.10 cfs	Peak Elev=62.21' Storage=3,721 cf Inflow=2.30 cfs 0.177 af 0.106 af Primary=0.05 cfs 0.049 af Outflow=0.15 cfs 0.155 af	
Pond 2P: Stone Drip Edge Discarded=0.00 cfs 0.0	Peak Elev=65.98' Storage=0.006 af Inflow=0.11 cfs 0.009 af 004 af Secondary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.004 af	
Pond 3P: Stone Under Deck Discarded=0.00 cfs 0.0	Peak Elev=65.97' Storage=0.003 af Inflow=0.07 cfs 0.006 af 004 af Secondary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.004 af	
Pond 4P: Stone Drip Edge Discarded=0.01 cfs 0.0	Peak Elev=64.56' Storage=0.005 af Inflow=0.11 cfs 0.009 af 006 af Secondary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.006 af	
Pond CB101: Catch Basin 101 12.0" Round C	Peak Elev=62.78' Inflow=0.49 cfs 0.039 af ulvert n=0.012 L=19.0' S=0.0053 '/' Outflow=0.49 cfs 0.039 af	
Pond CB102: Catch Basin 102 12.0" Round Cu	Peak Elev=62.63' Inflow=0.68 cfs 0.054 af Ivert n=0.012 L=147.0' S=0.0054 '/' Outflow=0.68 cfs 0.054 af	
Pond CB103: Catch Basin 103 12.0" Round C	Peak Elev=66.91' Inflow=1.05 cfs 0.080 af ulvert n=0.012 L=43.0' S=0.0070 '/' Outflow=1.05 cfs 0.080 af	
Pond CB104: Catch Basin 104 12.0" Round C	Peak Elev=62.21' Inflow=1.77 cfs 0.138 af ulvert n=0.012 L=45.0' S=0.0067 '/' Outflow=1.77 cfs 0.138 af	
Pond YD1: Yard Drain 1 8.0" Round (	Peak Elev=63.12' Inflow=0.25 cfs 0.019 af Culvert n=0.012 L=9.0' S=0.0189 '/' Outflow=0.25 cfs 0.019 af	
Pond YD2: Yard Drain 2 8.0" Round C	Peak Elev=67.52' Inflow=0.40 cfs 0.029 af ulvert n=0.012 L=52.0' S=0.0058 '/' Outflow=0.40 cfs 0.029 af	
Pond YD3: Yard Drain 3 8.0" Round C	Peak Elev=68.34' Inflow=0.28 cfs 0.020 af ulvert n=0.012 L=13.0' S=0.0923 '/' Outflow=0.28 cfs 0.020 af	
Total Runoff Area = 2.429 ad	c Runoff Volume = 0.485 af Average Runoff Depth = 2.4	10"

79.95% Pervious = 1.942 ac 20.05% Impervious = 0.487 ac

#### Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 0.67 cfs @ 12.09 hrs, Volume= 0.048 af, Depth> 3.43" Routed to Reach AP1 : Analysis Point 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN E	Description						
	3,741 3,651	98 F	98 Paved parking, HSG B						
	7 302	80 \	Veighted A						
	3.651	4	9.39% Per	vious Area					
	3,741	5	50.61% Imp	pervious Ar	ea				
Tc	Length	Slope	Velocity	Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
2.8	56	0.1250	0.34		Sheet Flow,				
					Grass: Short n= 0.150 P2= 3.70"				
2.1	30	0.0670	0.23		Sheet Flow,				
			4.00		Grass: Short n= 0.150 P2= 3.70"				
0.2	14	0.0360	1.26		Sheet Flow,				
0.4	96	0.0260	2.05		Smooth surfaces h= 0.011 P2= 3.70"				
0.4	00	0.0360	3.00		Shahow Concentrated Flow, Poved Ky= 20.3 fps				
5.5	186	Total, I	ncreased t	o minimum	1 c = 6.0 min				

#### Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.08 cfs @ 12.10 hrs, Volume= 0.006 af, Depth> 1.75" Routed to Reach AP2 : Analysis Point 2

A	rea (sf)	CN	Description					
	1,728	61	>75% Gras	s cover, Go	od, HSG B			
	1,728		100.00% Pe	ervious Area	а			
Tc (min)	Length (feet)	Slope (ft/ft)	e Velocity ) (ft/sec)	Capacity (cfs)	Description			
1.7	20	0.0500	0.19		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.70"	
1.7	20	Total,	Increased t	o minimum	Tc = 6.0 min			

#### Summary for Subcatchment 3S: Subcatchment 3S

Runoff	=	1.42 cfs @	12.26 hrs,	Volume=	0.151 af,	Depth> 1.74"
Routed	I to Read	ch 1R : Ditch (	on Tidewato	ch Property		-

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN D	escription		
	695	98 F	Roofs, HSC	ЭB	
	16,659	61 >	75% Gras	s cover, Go	ood, HSG B
	27,823	60 V	Voods, Fai	r, HSG B	
	45,177	61 V	Veighted A	verage	
	44,482	9	8.46% Pei	vious Area	
	695	1	.54% Impe	ervious Area	a
_					
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
9.0	53	0.0415	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
5.8	47	0.0968	0.13		Sheet Flow,
			4 - 0		Woods: Light underbrush n= 0.400 P2= 3.70"
0.2	15	0.0968	1.56		Shallow Concentrated Flow,
07	<b>F</b> 4	0.0744	4 0 0		Woodland KV= 5.0 fps
0.7	54	0.0741	1.36		Shallow Concentrated Flow,
10	400	0 1000	4 50		woodland KV= 5.0 fps
1.3	122	0.1000	1.58		Shallow Concentrated Flow,
		<b>-</b> · ·			
17.0	291	Iotal			

#### Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 1.00 cfs @ 12.12 hrs, Volume= 0.080 af, Depth> 1.99" Routed to Reach AP3 : Analysis Point 3

Area (sf)	CN	Description						
11,135	61	>75% Grass cover, Good, HSG B						
8,169	60	oods, Fair, HSG B						
 1,687	98	Roofs, HSG B						
20,991	64	Weighted Average						
19,304		91.96% Pervious Area						
1,687		8.04% Impervious Area						

#### 18134-PROPOSED

Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

Printed 4/19/2024

Prepared by Jones	& Beach	Engineer	s Inc			
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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
1.5	14	0.0357	0.16		Sheet Flow,	
					Grass: Short n= 0.150 P2= 3.70"	
1.9	14	0.1429	0.12		Sheet Flow,	
					Woods: Light underbrush n= 0.400 P2= 3.7	0"
3.3	72	0.1333	0.37		Sheet Flow,	
					Grass: Short n= 0.150 P2= 3.70"	
1.0	80	0.0750	1.37		Shallow Concentrated Flow,	
					Woodland Kv= 5.0 fps	
0.2	30	0.2667	2.58		Shallow Concentrated Flow,	

7.9 210 Total

#### Summary for Subcatchment 6S: Subcatchment 6S

Woodland Kv= 5.0 fps

Runoff	=	0.24 cfs @	12.09 hrs,	Volume=
Routed	to Pond	CB101 : Ca	tch Basin 10	01

0.020 af, Depth> 5.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

Area (s	f) CN	D	Description					
1,95	2 98	P	aved park	ing, HSG B	3			
1,95	2	100.00% Impervious Area						
Tc Leng (min) (fee	jth Sl et) (f	ope t/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

### Summary for Subcatchment 7S: Subcatchment 7S

Runoff = 0.19 cfs @ 12.09 hrs, Volume= 0.016 af, Depth> 5.37" Routed to Pond CB102 : Catch Basin 102

A	rea (sf)	CN	CN Description					
	1,516	98	Paved park	ing, HSG B	В			
	1,516		100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

#### Summary for Subcatchment 8S: Subcatchment 8S

Runoff = 0.37 cfs @ 12.09 hrs, Volume= 0.031 af, Depth> 5.37" Routed to Pond CB103 : Catch Basin 103

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN	Description		
	2,554	98	Paved park	ing, HSG B	В
	457	98	Roofs, HSC	Β́Β	
	3,011	98	Weighted A	verage	
	3,011		100.00% In	npervious A	Area
Тс	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)	
6.0					Direct Entry,
					-

#### **Summary for Subcatchment 9S: Subcatchment 9S**

0.003 af, Depth> 5.37"

Runoff = 0.04 cfs @ 12.09 hrs, Volume= Routed to Pond CB104 : Catch Basin 104

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

Ar	rea (sf)	CN	Description					
	325	98	3 Paved parking, HSG B					
	325		100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft	e Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

#### Summary for Subcatchment 10S: Subcatchment 10S

Runoff = 0.25 cfs @ 12.10 hrs, Volume= 0.019 af, Depth> 2.67" Routed to Pond YD1 : Yard Drain 1

Area (sf)	CN	Description
796	98	Roofs, HSG B
2,573	61	>75% Grass cover, Good, HSG B
261	98	Paved parking, HSG B
3,630	72	Weighted Average
2,573		70.88% Pervious Area
1,057		29.12% Impervious Area

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*Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"* Printed 4/19/2024

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.2	42	0.1190	0.31		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
3.7	58	0.0650	0.26		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
0.4	42	0.0650	1.78		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
6.2	140	Total			

6.3 142 Total

#### Summary for Subcatchment 11S: Subcatchment 11S

Runoff = 0.40 cfs @ 12.09 hrs, Volume= 0.029 af, Depth> 3.33" Routed to Pond YD2 : Yard Drain 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN	Description	l				
	1,998	98	Roofs, HSC	ЭB				
	2,312	61	>75% Gras	s cover, Go	ood, HSG B			
	261	98	Paved park	ting, HSG B	3			
	4,571	79	Weighted A	verage				
	2,312		50.58% Pe	rvious Area	l			
	2,259		49.42% Im	pervious Ar	ea			
Tc	Length	Slop	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft	i) (ft/sec)	(cfs)				
5.6	77	0.039	6 0.23		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.70"	
5.6	77	Total,	Increased	to minimum	n Tc = 6.0 min			

#### Summary for Subcatchment 12S: Subcatchment 12S

Runoff = 0.28 cfs @ 12.09 hrs, Volume= 0.020 af, Depth> 2.86" Routed to Pond YD3 : Yard Drain 3

Area (sf)	CN	Description
1,318	98	Roofs, HSG B
2,416	61	>75% Grass cover, Good, HSG B
3,734	74	Weighted Average
2,416		64.70% Pervious Area
1,318		35.30% Impervious Area

18134-PROPOSED					Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"
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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.4	51	0.0320	0.19		Sheet Flow, Grass: Short n= 0.150 P2= 3.70"
4.4	51	Total, I	ncreased t	o minimum	Tc = 6.0 min
		Sum	mary fo	r Subcato	chment 13S: Subcatchment 13S
Runoff Route	= ed to Pone	0.11 cfs d 2P : Ste	s @ 12.09 one Drip E	9 hrs, Volu dge	me= 0.009 af, Depth> 5.37"
Runoff b Type III 2	y SCS TF 24-hr 10	R-20 met Yr 24 Hr	hod, UH=S +15% Rai	SCS, Weigh nfall=5.61"	nted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
A	rea (sf)	CN D	escription		
	696 180	98 F 98 V	loofs, HSG Vater Surfa	3 B ace, HSG B	l
	876 876	98 V 1	Veighted A 00.00% Im	verage pervious A	rea
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,
		Sum	mary fo	r Subcato	chment 14S: Subcatchment 14S
Runoff Route	= ed to Pone	0.07 cfs d 3P : Ste	s @ 12.09 one Under	9 hrs, Volu <sup>-</sup> Deck	me= 0.006 af, Depth> 5.37"
	000 T				

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN	Description		
	560	98	Roofs, HSC	βB	
	560		100.00% In	npervious A	Area
Tc (min)	Length (feet)	Slop (ft/fl	e Velocity ) (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

## Summary for Subcatchment 15S: Subcatchment 15S

Runoff = 0.11 cfs @ 12.09 hrs, Volume= 0.009 af, Depth> 5.37" Routed to Pond 4P : Stone Drip Edge

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A	rea (sf)	CN	Description		
	696	98	Roofs, HSC	βB	
	180	98	Water Surfa	ace, HSG B	3
	876	98	Weighted A	verage	
	876		100.00% In	npervious A	Area
_					
Тс	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
6.0					Direct Entry,

#### Summary for Subcatchment 18S: Subcatchment 18S

Runoff = 0.53 cfs @ 12.10 hrs, Volume= 0.039 af, Depth> 2.15" Routed to Pond 1P : Bioretention Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr +15% Rainfall=5.61"

A	rea (sf)	CN	Description					
	8,136	61	>75% Gras	s cover, Go	ood, HSG B			
	938	98	Roofs, HSC	βB				
	400	98	Paved park	ing, HSG B	5			
	9,474	66	Weighted A	verage				
	8,136		85.88% Pe	rvious Area				
	1,338		14.12% Im	pervious Ar	ea			
Tc	Length	Slop	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)				
2.5	43	0.093	0 0.29		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.70"	
0.6	15	0.333	3 0.39		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.70"	
3.1	58	Total.	Increased	to minimum	Tc = 6.0 min			

#### Summary for Reach 1R: Ditch on Tidewatch Property

[62] Hint: Exceeded Reach 2R OUTLET depth by 0.32' @ 12.25 hrs
[62] Hint: Exceeded Reach 4R OUTLET depth by 0.30' @ 12.25 hrs
Inflow Area = 1.685 ac, 18.36% Impervious, Inflow Depth > 1.42" for 10 Yr 24 Hr +15% event
Inflow = 1.47 cfs @ 12.26 hrs, Volume= 0.200 af
Outflow = 1.47 cfs @ 12.27 hrs, Volume= 0.199 af, Atten= 0%, Lag= 0.8 min
Routed to Reach AP3 : Analysis Point 3
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 2.37 fps, Min. Travel Time= 1.1 min Avg. Velocity = 1.12 fps, Avg. Travel Time= 2.4 min

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Peak Storage= 98 cf @ 12.27 hrs Average Depth at Peak Storage= 0.32', Surface Width= 2.90' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.18 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 7.00' Length= 159.0' Slope= 0.0189 '/' Inlet Invert= 38.00', Outlet Invert= 35.00'

#### Summary for Reach 2R: Flow through 3S

Inflow Outflow	= =	0.00 cfs @ 0.00 cfs @	0.00 hrs, 0.00 hrs,	Volume= Volume=	0.000 af 0.000 af,	Atten= 0%,	Lag= 0.0 min
Routed	to Reac	h 1R : Ditch or	n Tidewato	ch Property			0

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs Average Depth at Peak Storage= 0.00' Bank-Full Depth= 1.00' Flow Area= 33.3 sf, Capacity= 740.30 cfs

50.00' x 1.00' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 81.0' Slope= 0.3457 '/' Inlet Invert= 66.00', Outlet Invert= 38.00'



#### Summary for Reach 4R: Flow Through 3S

Inflow Area = 0.648 ac, 45.28% Impervious, Inflow Depth > 0.92" for 10 Yr 24 Hr +15% event 0.05 cfs @ 13.96 hrs, Volume= 0.05 cfs @ 14.00 hrs, Volume= Inflow = 0.049 af Outflow = 0.049 af, Atten= 0%, Lag= 2.5 min Routed to Reach 1R : Ditch on Tidewatch Property

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 0.98 fps, Min. Travel Time= 3.7 min Avg. Velocity = 0.92 fps, Avg. Travel Time= 4.0 min

Peak Storage= 11 cf @ 14.00 hrs Average Depth at Peak Storage= 0.02' , Surface Width= 3.10' Bank-Full Depth= 1.00' Flow Area= 6.0 sf, Capacity= 66.79 cfs

3.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 9.00' Length= 220.0' Slope= 0.0909 '/' Inlet Invert= 58.00', Outlet Invert= 38.00'

‡

## Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	0.170 ac, 5	0.61% Imp	ervious,	Inflow Dep	oth > 3	3.43"	for 10	Yr 24 Hr +	-15% event
Inflow	=	0.67 cfs @	12.09 hrs,	Volume	= 0	).048 a <sup>.</sup>	f			
Outflow	=	0.67 cfs @	12.09 hrs,	Volume	= 0	).048 a <sup>.</sup>	f, Atte	n= 0%,	Lag= 0.0	min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

#### Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	rea =	0.040 ac,	0.00% Impervious, Inflow	Depth > 1.75"	for 10 Yr 24 Hr +15% event
Inflow	=	0.08 cfs @	12.10 hrs, Volume=	0.006 af	
Outflow	=	0.08 cfs @	12.10 hrs, Volume=	0.006 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

#### Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	ea =	2.167 ac, 16.06% Impervious, Inf	low Depth > 1.55" for	10 Yr 24 Hr +15% event
Inflow	=	2.12 cfs @ 12.22 hrs, Volume=	0.279 af	
Outflow	=	2.12 cfs @ 12.22 hrs, Volume=	0.279 af, Atten= 0	%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

# Summary for Pond 1P: Bioretention Pond

Existing high contour within footprint of filter course = 61.0, SHWT depth = 35" per TP 10, so SHWT EI. = 58.08, which is 0.01' below the bottom of stone. However, in our experience, modelling the SHWT with such a small separation to the bottom of stone causes an unrealistically high amount of infiltration to appear in the calculations. Therefore, the SHWT has been modelled 2" lower as a factor of safety.

Inflow Area	ı =	0.648 ac, 4	45.28% Impe	ervious,	Inflow Depth >	3.28"	for 10 Y	r 24 Hr +15% event
Inflow	=	2.30 cfs @	12.09 hrs,	Volume	= 0.177	af		
Outflow	=	0.15 cfs @	13.96 hrs,	Volume	= 0.155	af, Atte	en= 93%,	Lag= 111.9 min
Discarded	=	0.10 cfs @	13.96 hrs,	Volume	= 0.106	af		
Primary	=	0.05 cfs @	13.96 hrs,	Volume	= 0.049	af		
Routed	to Reac	h 4R : Flow	Through 3S					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 62.21' @ 13.96 hrs Surf.Area= 2,793 sf Storage= 3,721 cf

Plug-Flow detention time= 260.5 min calculated for 0.155 af (88% of inflow) Center-of-Mass det. time= 203.0 min (1,003.3 - 800.3)

Volume	Invert	Avail	.Storage	Storage	Description		
#1	58.09'		6,166 cf	Custom	n Stage Data (Irregu	<b>llar)</b> Listed below	(Recalc)
Elevatio	on Su	urf.Area	Perim.	Voids	Inc.Store	Cum.Store	Wet.Area
(fee	et)	(sq-ft)	(feet)	(%)	(cubic-feet)	(cubic-feet)	<u>(sq-ft)</u>
58.0	)9	466	106.0	0.0	0	0	466
58.1	0	466	106.0	40.0	2	2	467
59.0	)9	466	106.0	40.0	185	186	572
59.1	0	466	106.0	15.0	1	187	573
60.5	59	466	106.0	15.0	104	291	731
60.6	60	466	106.0	100.0	5	296	732
61.0	00	2,114	176.0	100.0	476	772	2,304
62.0	00	2,672	195.0	100.0	2,388	3,160	2,895
63.0	00	3,285	215.0	100.0	2,973	6,133	3,579
63.0	)1	3,285	215.0	100.0	33	6,166	3,581
Device	Routing	Inv	ert Outle	et Device	S		
#1	Primary	58.	60' <b>12.0</b>	" Round	l Culvert		
			L= 1	8.0' CP	P, projecting, no hea	adwall, Ke= 0.90	0
			Inlet	/ Outlet I	nvert= 58.60' / 58.00	D' S= 0.0333 '/'	Cc= 0.900
			n= 0	.012, Flo	ow Area= 0.79 sf		
#2	Device 1	58.	90' <b>1.0''</b>	Vert. Or	ifice/Grate C= 0.60	00 Limited to we	eir flow at low heads
#3	Device 1	62.	65' <b>15.0</b>	" Horiz.	Orifice/Grate C= 0	.600	
			Limit	ted to we	ir flow at low heads		
#4	Discarded	58.	09' <b>0.30</b>	0 in/hr E	xfiltration over Sur	face area	
			Cone	ductivity f	o Groundwater Elev	ation = 57.92'	Phase-In= 0.10'

**Discarded OutFlow** Max=0.10 cfs @ 13.96 hrs HW=62.21' (Free Discharge) **4=Exfiltration** (Controls 0.10 cfs)

**Primary OutFlow** Max=0.05 cfs @ 13.96 hrs HW=62.21' TW=58.02' (Dynamic Tailwater) **1=Culvert** (Passes 0.05 cfs of 5.26 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.05 cfs @ 8.70 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

## Summary for Pond 2P: Stone Drip Edge

Ledge surface modelled 15" below original grade based on TP 1 and TP 4. Proposed grade is approximately 4' above existing grade and therefore 5.25' above ledge.

Inflow Area =	0.020 ac,10	0.00% Impervious,	Inflow Depth >	5.37" for	10 Yr 24 Hr +15% event	
Inflow =	0.11 cfs @	12.09 hrs, Volume	e= 0.009 a	af		
Outflow =	0.00 cfs @	15.49 hrs, Volume	e= 0.004 a	af, Atten= 9	7%, Lag= 204.3 min	
Discarded =	0.00 cfs @	15.49 hrs, Volume	e 0.004 a	af	-	
Secondary =	0.00 cfs @	0.00 hrs, Volume	e= 0.000 a	af		
Routed to Reach 2R : Flow through 3S						

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 65.98' @ 15.49 hrs Surf.Area= 0.004 ac Storage= 0.006 af

Plug-Flow detention time= 332.3 min calculated for 0.004 af (50% of inflow) Center-of-Mass det. time= 201.5 min (947.3 - 745.7)

Invert	Avail.Storage	Storage Description
62.50'	0.006 af	<b>3.00'W x 60.00'L x 3.51'H Prismatoid</b> 0.015 af Overall x 40.0% Voids
Routing	Invert O	utlet Devices
Secondary	66.01' <b>A</b> i	utomatic Storage Overflow (Discharged without head)
Discarded	62.50' <b>0.</b>	300 in/hr Exfiltration over Surface area
	Co	onductivity to Groundwater Elevation = 60.75' Phase-In= 0.10'
	Invert 62.50' Routing Secondary Discarded	InvertAvail.Storage62.50'0.006 afRoutingInvertOSecondary66.01'ArDiscarded62.50'O.ContractContract

**Discarded OutFlow** Max=0.00 cfs @ 15.49 hrs HW=65.98' (Free Discharge) **1=Exfiltration** (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=62.50' TW=66.00' (Dynamic Tailwater)

## Summary for Pond 3P: Stone Under Deck

Ledge surface modelled 15" below original grade based on TP 1 and TP 4. Proposed grade is approximately 3.2' above existing grade and therefore 4.45' above ledge.

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			-			
Inflow A	rea = C	.013 ac,100.0	0% Impervious, Infl	ow Depth > 5.37	" for 10 ነ	r 24 Hr +15% event
Inflow	= 0	.07 cfs @ 12	.09 hrs, Volume=	0.006 af		
Outflow	= 0	.00 cfs 🥘 15	.02 hrs, Volume=	0.004 af, A	tten= 96%,	Lag= 176.3 min
Discarde	ed = 0	.00 cfs @15	.02 hrs, Volume=	0.004 af		0
Seconda	ary = 0	.00 cfs 🥘 0	.00 hrs, Volume=	0.000 af		
Rout	ed to Reach :	2R : Flow thro	ugh 3S			
			-			
Routing	by Dyn-Stor-	Ind method, T	ime Span= 0.00-24	.00 hrs, dt= 0.05 h	rs / 3	
Peak El	ev= 65.97' @	15.02 hrs S	urf.Area= 0.006 ac	Storage= 0.003 a	f	
Plug-Flc	w detention	time= 294.9 m	in calculated for 0.0	04 af (62% of inflo	w)	
Center-o	of-Mass det. 1	time= 187.7 m	in(933.4 - 745.7)			
Volume	Invert	Avail.Stora	ge Storage Descri	ption		
#1	64.70'	0.004	af 14.00'W x 20.0	0'L x 1.50'H Prisi	natoid	
			0.010 af Overa	ll x 40.0% Voids		
Device	Routing	Invert	Outlet Devices			
#0	Secondary	66.20'	<b>Automatic Storage</b>	e Overflow (Disch	narged with	out head)
#1	Discarded	64.70'	0.300 in/hr Exfiltra	tion over Surface	e area	·
			Conductivity to Gro	undwater Elevatio	n = 61.75'	Phase-In= 0.10'
			-			
Discard	ed OutFlow	Max=0.00 cfs	@ 15.02 hrs HW=0	65.97' (Free Disc	harge)	
T—1=Ex	t <b>filtration</b> (C	ontrols 0.00 c	fs)			
Second	ary OutFlow	v Max=0.00 cfs	s @ 0.00 hrs HW=6	4.70' TW=66.00'	(Dynamic	Tailwater)

# Summary for Pond 4P: Stone Drip Edge

Ledge surface modelled 15" below original grade based on TP 1 and TP 4. Proposed grade is approximately 4' above existing grade and therefore 5.25' above ledge.

Inflow Area Inflow Outflow Discarded	= = = -	0.020 ac,100.00% 0.11 cfs @ 12.09 0.01 cfs @ 13.80 0.01 cfs @ 13.80	Impervious, Inflow Depth > 5.37"         for 10 Yr 24 Hr +15% event           hrs, Volume=         0.009 af           hrs, Volume=         0.006 af, Atten= 94%, Lag= 103.0 min           hrs, Volume=         0.006 af			
Routed	= to Reach	n 2R : Flow through	as 0.000 ai			
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 64.56' @ 13.80 hrs Surf.Area= 0.004 ac Storage= 0.005 af						
Plug-Flow detention time= 301.8 min calculated for 0.006 af (71% of inflow) Center-of-Mass det. time= 209.5 min(955.2 - 745.7)						
Volume	Inver	t Avail.Storage	Storage Description			
#1	61.50	' 0.007 af	<b>3.00'W x 60.00'L x 4.51'H Prismatoid</b> 0.019 af Overall x 40.0% Voids			
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Device	Routing	Invert	Outlet Devices	
#0	Secondary	66.01'	Automatic Storage Overflow (Discharged with	out head)
#1	Discarded	61.50'	<b>0.300 in/hr Exfiltration over Surface area</b> Conductivity to Groundwater Elevation = 60.75'	Phase-In= 0.10'

**Discarded OutFlow** Max=0.01 cfs @ 13.80 hrs HW=64.56' (Free Discharge) **1=Exfiltration** (Controls 0.01 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=61.50' TW=66.00' (Dynamic Tailwater)

## Summary for Pond CB101: Catch Basin 101

 Inflow Area =
 0.128 ac, 53.91% Impervious, Inflow Depth > 3.62" for 10 Yr 24 Hr +15% event

 Inflow =
 0.49 cfs @ 12.09 hrs, Volume=
 0.039 af

 Outflow =
 0.49 cfs @ 12.09 hrs, Volume=
 0.039 af, Atten= 0%, Lag= 0.0 min

 Primary =
 0.49 cfs @ 12.09 hrs, Volume=
 0.039 af

 Routed to Pond CB102 : Catch Basin 102
 0.039 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 62.78' @ 12.09 hrs Flood Elev= 65.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	62.30'	<b>12.0" Round Culvert</b> L= 19.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 62.30' / 62.20' S= 0.0053 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.48 cfs @ 12.09 hrs HW=62.77' TW=62.62' (Dynamic Tailwater) -1=Culvert (Outlet Controls 0.48 cfs @ 1.94 fps)

#### Summary for Pond CB102: Catch Basin 102

 Inflow Area =
 0.163 ac, 63.75% Impervious, Inflow Depth > 3.99" for 10 Yr 24 Hr +15% event

 Inflow =
 0.68 cfs @ 12.09 hrs, Volume=
 0.054 af

 Outflow =
 0.68 cfs @ 12.09 hrs, Volume=
 0.054 af, Atten= 0%, Lag= 0.0 min

 Primary =
 0.68 cfs @ 12.09 hrs, Volume=
 0.054 af

 Routed to Pond CB104 : Catch Basin 104
 0.054 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 62.63' @ 12.09 hrs Flood Elev= 65.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	62.10'	<b>12.0" Round Culvert</b> L= 147.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 62.10' / 61.30' S= 0.0054 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.67 cfs @ 12.09 hrs HW=62.62' TW=62.04' (Dynamic Tailwater) -1=Culvert (Outlet Controls 0.67 cfs @ 2.34 fps)

# Summary for Pond CB103: Catch Basin 103

 Inflow Area =
 0.260 ac, 58.22% Impervious, Inflow Depth > 3.72" for 10 Yr 24 Hr +15% event

 Inflow =
 1.05 cfs @ 12.09 hrs, Volume=
 0.080 af

 Outflow =
 1.05 cfs @ 12.09 hrs, Volume=
 0.080 af, Atten= 0%, Lag= 0.0 min

 Primary =
 1.05 cfs @ 12.09 hrs, Volume=
 0.080 af

 Routed to Pond CB104 : Catch Basin 104
 0.080 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.91' @ 12.09 hrs Flood Elev= 73.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	66.30'	<b>12.0" Round Culvert</b> L= 43.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 66.30' / 66.00' S= 0.0070 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=1.03 cfs @ 12.09 hrs HW=66.90' TW=62.04' (Dynamic Tailwater) -1=Culvert (Inlet Controls 1.03 cfs @ 2.09 fps)

# Summary for Pond CB104: Catch Basin 104

 Inflow Area =
 0.430 ac, 61.04% Impervious, Inflow Depth > 3.85" for 10 Yr 24 Hr +15% event

 Inflow =
 1.77 cfs @ 12.09 hrs, Volume=
 0.138 af

 Outflow =
 1.77 cfs @ 12.09 hrs, Volume=
 0.138 af, Atten= 0%, Lag= 0.0 min

 Primary =
 1.77 cfs @ 12.09 hrs, Volume=
 0.138 af

 Routed to Pond 1P : Bioretention Pond
 0.138 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 62.21' @ 13.94 hrs Flood Elev= 70.80'

Device	Routing	Invert	Outlet Devices
#1	Primary	61.20'	<b>12.0" Round Culvert</b> L= 45.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 61.20' / 60.90' S= 0.0067 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=1.74 cfs @ 12.09 hrs HW=62.04' TW=61.45' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 1.74 cfs @ 2.46 fps)

# Summary for Pond YD1: Yard Drain 1

Inflow Area	ı =	0.083 ac,	29.12% Imp	ervious,	Inflow Depth >	2.67"	for 10	Yr 24 Hr +1	5% event
Inflow	=	0.25 cfs @	2 12.10 hrs,	Volume	= 0.019	9 af			
Outflow	=	0.25 cfs @	2 12.10 hrs,	Volume	= 0.019	9 af, Atte	en= 0%,	Lag= 0.0 m	nin
Primary	=	0.25 cfs @	2 12.10 hrs,	Volume	= 0.019	9 af		-	
Routed	to Pond	CB101 : C	atch Basin 10	D1					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

## 18134-PROPOSED

Peak Elev= 63.12' @ 12.10 hrs Flood Elev= 65.80'

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Device Routing Invert Outlet Devices 8.0" Round Culvert #1 Primary 62.80' L= 9.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 62.80' / 62.63' S= 0.0189 '/' Cc= 0.900 n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.25 cfs @ 12.10 hrs HW=63.12' TW=62.78' (Dynamic Tailwater) ↓ 1=Culvert (Inlet Controls 0.25 cfs @ 1.52 fps)

#### Summary for Pond YD2: Yard Drain 2

Inflow Area = 0.105 ac, 49.42% Impervious, Inflow Depth > 3.33" for 10 Yr 24 Hr +15% event 0.40 cfs @ 12.09 hrs, Volume= Inflow 0.029 af = 0.029 af, Atten= 0%, Lag= 0.0 min 0.40 cfs @ 12.09 hrs, Volume= Outflow = 0.40 cfs @ 12.09 hrs, Volume= Primarv = 0.029 af Routed to Pond CB103 : Catch Basin 103

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 67.52' @ 12.09 hrs Flood Elev= 69.30'

Device	Routing	Invert	Outlet Devices
#1	Primary	67.10'	<b>8.0" Round Culvert</b> L= 52.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 67.10' / 66.80' S= 0.0058 '/' Cc= 0.900 n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.39 cfs @ 12.09 hrs HW=67.52' TW=66.90' (Dynamic Tailwater) ←1=Culvert (Barrel Controls 0.39 cfs @ 2.43 fps)

#### Summary for Pond YD3: Yard Drain 3

Inflow Area = 0.086 ac, 35.30% Impervious, Inflow Depth > 2.86" for 10 Yr 24 Hr +15% event Inflow 0.28 cfs @ 12.09 hrs, Volume= 0.020 af = 0.28 cfs @ 12.09 hrs, Volume= 0.28 cfs @ 12.09 hrs, Volume= 0.020 af, Atten= 0%, Lag= 0.0 min Outflow = Primarv = 0.020 af Routed to Pond CB103 : Catch Basin 103

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 68.34' @ 12.09 hrs Flood Elev= 70.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	68.00'	<b>8.0" Round Culvert</b> L= 13.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 68.00' / 66.80' S= 0.0923 '/' Cc= 0.900 n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.28 cfs @ 12.09 hrs HW=68.34' TW=66.90' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 0.28 cfs @ 1.56 fps)

# **18134-PROPOSED** Type III 24-hr 25 Yr 24 Hr +15% Rainfall=7.12" Prepared by Jones & Beach Engineers Inc Printed 4/19/2024 HydroCAD® 10.20-3c s/n 00762 © 2023 HydroCAD Software Solutions LLC Page 24

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=7,392 sf 50.61% Impervious Runoff Depth>4.80" Flow Length=186' Tc=6.0 min CN=80 Runoff=0.93 cfs 0.068 af
Subcatchment2S: Subcatchment2S Flow Length=20	Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>2.79" Slope=0.0500 '/' Tc=6.0 min CN=61 Runoff=0.12 cfs 0.009 af
Subcatchment3S: Subcatchment3S	Runoff Area=45,177 sf 1.54% Impervious Runoff Depth>2.78" Flow Length=291' Tc=17.0 min CN=61 Runoff=2.36 cfs 0.240 af
Subcatchment4S: Subcatchment4S	Runoff Area=20,991 sf 8.04% Impervious Runoff Depth>3.09" Flow Length=210' Tc=7.9 min CN=64 Runoff=1.60 cfs 0.124 af
Subcatchment6S: Subcatchment6S	Runoff Area=1,952 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.31 cfs 0.026 af
Subcatchment7S: Subcatchment7S	Runoff Area=1,516 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.24 cfs 0.020 af
Subcatchment8S: Subcatchment8S	Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.47 cfs 0.040 af
Subcatchment9S: Subcatchment9S	Runoff Area=325 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment10S: Subcatchment10S	Runoff Area=3,630 sf 29.12% Impervious Runoff Depth>3.93" Flow Length=142' Tc=6.3 min CN=72 Runoff=0.37 cfs 0.027 af
Subcatchment11S: Subcatchment11S Flow Length=77	Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>4.69" '' Slope=0.0396 '/' Tc=6.0 min CN=79 Runoff=0.56 cfs 0.041 af
Subcatchment12S: Subcatchment12S Flow Length=51	Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>4.14" ' Slope=0.0320 '/' Tc=6.0 min CN=74 Runoff=0.41 cfs 0.030 af
Subcatchment13S: Subcatchment13S	Runoff Area=876 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.14 cfs 0.012 af
Subcatchment14S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af
Subcatchment15S: Subcatchment15S	Runoff Area=876 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.14 cfs 0.012 af
Subcatchment18S: Subcatchment18S	Runoff Area=9,474 sf 14.12% Impervious Runoff Depth>3.30" Flow Length=58' Tc=6.0 min CN=66 Runoff=0.82 cfs 0.060 af
Reach 1R: Ditch on Tidewatch Property n=0.030 L=1	Avg. Flow Depth=0.40' Max Vel=2.71 fps Inflow=2.41 cfs 0.312 af 59.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=2.41 cfs 0.312 af

18134-PROPOSED	Type III 24-hr  25 Yr 24 Hr +15% Rain	fall=7.12"
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Reach 2R: Flow through 3S Av	g. Flow Depth=0.01' Max Vel=1.19 fps Inflow=0.05 cfs	0.003 af
n=0.030 L=81.	0' S=0.3457 '/' Capacity=740.30 cfs Outflow=0.05 cfs	0.003 af
Reach 4R: Flow Through 3S Av	g. Flow Depth=0.04' Max Vel=1.69 fps Inflow=0.21 cfs	0.070 af
n=0.030 L=220	0.0' S=0.0909 '/' Capacity=66.79 cfs Outflow=0.21 cfs	0.070 af
Reach AP1: Analysis Point 1	Inflow=0.93 cfs	0.068 af
	Outflow=0.93 cfs	0.068 af
Reach AP2: Analysis Point 2	Inflow=0.12 cfs	0.009 af
	Outflow=0.12 cfs	0.009 af
Reach AP3: Analysis Point 3	Inflow=3.47 cfs	0.436 af
	Outflow=3.47 cfs	0.436 af
Pond 1P: Bioretention Pond	Peak Elev=62.70' Storage=5,186 cf Inflow=3.23 cfs	0.247 af
Discarded=0.12 cfs	0.125 af Primary=0.21 cfs 0.070 af Outflow=0.33 cfs	0.195 af
Pond 2P: Stone Drip Edge	Peak Elev=66.01' Storage=0.006 af Inflow=0.14 cfs	0.012 af
Discarded=0.00 cfs_0.	005 af Secondary=0.05 cfs 0.002 af Outflow=0.05 cfs	0.007 af
Pond 3P: Stone Under Deck	Peak Elev=66.20' Storage=0.004 af Inflow=0.09 cfs	0.007 af
Discarded=0.00 cfs 0.	004 af Secondary=0.01 cfs 0.001 af Outflow=0.01 cfs	0.005 af
Pond 4P: Stone Drip Edge	Peak Elev=65.51' Storage=0.007 af Inflow=0.14 cfs	0.012 af
Discarded=0.01 cfs_0.	008 af Secondary=0.00 cfs 0.000 af Outflow=0.01 cfs	0.008 af
Pond CB101: Catch Basin 101	Peak Elev=62.92' Inflow=0.68 cfs	0.053 af
12.0" Round (	Culvert n=0.012 L=19.0' S=0.0053 '/' Outflow=0.68 cfs	0.053 af
Pond CB102: Catch Basin 102	Peak Elev=62.85' Inflow=0.92 cfs	0.073 af
12.0" Round Co	ulvert n=0.012 L=147.0' S=0.0054 '/' Outflow=0.92 cfs	0.073 af
Pond CB103: Catch Basin 103	Peak Elev=67.04' Inflow=1.44 cfs	0.110 af
12.0" Round (	Culvert n=0.012 L=43.0' S=0.0070 '/' Outflow=1.44 cfs	0.110 af
Pond CB104: Catch Basin 104	Peak Elev=62.71' Inflow=2.41 cfs	0.187 af
12.0" Round (	Culvert n=0.012 L=45.0' S=0.0067 '/' Outflow=2.41 cfs	0.187 af
Pond YD1: Yard Drain 1	Peak Elev=63.20' Inflow=0.37 cfs	0.027 af
8.0" Round	Culvert n=0.012 L=9.0' S=0.0189 '/' Outflow=0.37 cfs	0.027 af
Pond YD2: Yard Drain 2	Peak Elev=67.62' Inflow=0.56 cfs	0.041 af
8.0" Round (	Culvert n=0.012 L=52.0' S=0.0058 '/' Outflow=0.56 cfs	0.041 af
Pond YD3: Yard Drain 3	Peak Elev=68.42' Inflow=0.41 cfs	0.030 af
8.0" Round (	Culvert n=0.012 L=13.0' S=0.0923 '/' Outflow=0.41 cfs	0.030 af
Total Runoff Area = 2.429 a	c Runoff Volume = 0.719 af Average Runoff De	epth = 3.55"

79.95% Pervious = 1.942 ac 20.05% Impervious = 0.487 ac

18134-PROPOSED	Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"
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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=7,392 sf 50.61% Impervious Runoff Depth>6.12" Flow Length=186' Tc=6.0 min CN=80 Runoff=1.17 cfs 0.087 af
Subcatchment2S: Subcatchment2S Flow Length=20	Runoff Area=1,728 sf 0.00% Impervious Runoff Depth>3.85" ' Slope=0.0500 '/' Tc=6.0 min CN=61 Runoff=0.17 cfs 0.013 af
Subcatchment3S: Subcatchment3S	Runoff Area=45,177 sf 1.54% Impervious Runoff Depth>3.84" Flow Length=291' Tc=17.0 min CN=61 Runoff=3.32 cfs 0.332 af
Subcatchment4S: Subcatchment4S	Runoff Area=20,991 sf 8.04% Impervious Runoff Depth>4.20" Flow Length=210' Tc=7.9 min CN=64 Runoff=2.19 cfs 0.169 af
Subcatchment6S: Subcatchment6S	Runoff Area=1,952 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.37 cfs 0.031 af
Subcatchment7S: Subcatchment7S	Runoff Area=1,516 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.28 cfs 0.024 af
Subcatchment8S: Subcatchment8S	Runoff Area=3,011 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.57 cfs 0.048 af
Subcatchment9S: Subcatchment9S	Runoff Area=325 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment10S: Subcatchment10S	Runoff Area=3,630 sf 29.12% Impervious Runoff Depth>5.16" Flow Length=142' Tc=6.3 min CN=72 Runoff=0.49 cfs 0.036 af
Subcatchment11S: Subcatchment11S Flow Length=77	Runoff Area=4,571 sf 49.42% Impervious Runoff Depth>6.00" ' Slope=0.0396 '/' Tc=6.0 min CN=79 Runoff=0.71 cfs 0.052 af
Subcatchment12S: Subcatchment12S Flow Length=51	Runoff Area=3,734 sf 35.30% Impervious Runoff Depth>5.40" ' Slope=0.0320 '/' Tc=6.0 min CN=74 Runoff=0.53 cfs 0.039 af
Subcatchment13S: Subcatchment13S	Runoff Area=876 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.16 cfs 0.014 af
Subcatchment14S: Subcatchment14S	Runoff Area=560 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.11 cfs 0.009 af
Subcatchment15S: Subcatchment15S	Runoff Area=876 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.16 cfs 0.014 af
Subcatchment18S: Subcatchment18S	Runoff Area=9,474 sf 14.12% Impervious Runoff Depth>4.44" Flow Length=58' Tc=6.0 min CN=66 Runoff=1.11 cfs 0.081 af
Reach 1R: Ditch on Tidewatch Property n=0.030 L=1	Avg. Flow Depth=0.51' Max Vel=3.08 fps Inflow=3.98 cfs 0.460 af 59.0' S=0.0189 '/' Capacity=18.18 cfs Outflow=3.98 cfs 0.460 af

18134-PROPOSED	Type III 24-hr  50 Yr 24 Hr +15% Rain	fall=8.53"
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Reach 2P: Flow through 3S Avg. Flow I	Denth=0.02' Max Vel=1.55 fps_Inflow=0.12 cfs	: 0.006 af
n=0.030 L=81.0' S=0.1	3457 '/' Capacity=740.30 cfs Outflow=0.12 cfs	0.006 af
		0.000 4
Reach 4R: Flow Through 3S Avg. Flow I	Depth=0.11' Max Vel=3.19 fps Inflow=1.18 cfs	0.122 af
n=0.030 L=220.0' S=0	0.0909 '/' Capacity=66.79 cfs Outflow=1.17 cfs	6 0.122 af
Reach AP1: Analysis Point 1	Inflow=1.17 cfs	s 0.087 af
	Outflow=1.17 cts	s 0.087 af
Reach AP2: Analysis Point 2	Inflow=0.17 cfs	s 0.013 af
Neach Ar 2. Analysis roint 2	Outflow=0.17 cfs	s 0.013 af
Reach AP3: Analysis Point 3	Inflow=5.03 cfs	s 0.629 af
	Outflow=5.03 cfs	s 0.629 af
Pond 1P: Bioretention Pond Peak	Elev=62.85' Storage=5,639 cf Inflow=4.12 cfs	0.315 af
Discarded-0.12 cis 0.152 a	1 Phinary-1.16 cis 0.122 al Outlow-1.30 cis	0.204 ai
Pond 2P: Stone Drin Edge Peak	Elev=66.01' Storage=0.006.af Inflow=0.16.cfs	0 014 af
Discarded=0.00 cfs 0.005 af	Secondary=0.11 cfs 0.004 af Outflow=0.11 cfs	0.009 af
Pond 3P: Stone Under Deck Peak	Elev=66.20' Storage=0.004 af Inflow=0.11 cfs	s 0.009 af
Discarded=0.00 cfs 0.004 af	Secondary=0.04 cfs 0.002 af Outflow=0.05 cfs	0.006 af
Dand (D: Ctana Drin Edua	Elevence 01' Starage=0.007 of Inflow=0.16 of	0.014 of
Discarded=0.01 cfs_0.009 af	Secondary=0.02 cfs 0.001 at 11110w=0.10 cfs	0.014 ai
		0.010 al
Pond CB101: Catch Basin 101	Peak Elev=63.28' Inflow=0.86 cfs	s 0.067 af
12.0" Round Culvert r	1=0.012 L=19.0' S=0.0053 '/' Outflow=0.86 cfs	6 0.067 af
Pond CB102: Catch Basin 102	Peak Elev=63.42' Inflow=1.14 cfs	s 0.091 af
12.0° Round Culvert n=	=0.012 L=147.0 S=0.0054 7 Outflow=1.14 cfs	6 0.091 af
Pond CB103: Catch Basin 103	Peak Flev=67 16' Inflow=1 81 cfs	s 0 139 af
12.0" Round Culvert r	=0.012 L=43.0' S=0.0070 '/' Outflow=1.81 cfs	0.139 af
Pond CB104: Catch Basin 104	Peak Elev=63.25' Inflow=3.01 cfs	s 0.235 af
12.0" Round Culvert r	1=0.012 L=45.0' S=0.0067 '/' Outflow=3.01 cfs	0.235 af
David VD4. Vand Duain 4		0.020 -f
Pond YD1: Yard Drain 1 8 0" Round Culvert	Peak Elev=03.50 Inilow=0.49 cls	5 0.036 af
	11-0.012 L-9.0 3-0.0109 / Outilow-0.49 cis	0.000 ai
Pond YD2: Yard Drain 2	Peak Elev=67.72' Inflow=0.71 cfs	s 0.052 af
8.0" Round Culvert r	1=0.012 L=52.0' S=0.0058 '/' Outflow=0.71 cfs	6 0.052 af
Pond YD3: Yard Drain 3	Peak Elev=68.50' Inflow=0.53 cfs	0.039 af
8.0" Round Culvert r	1=0.012 L=13.0' S=0.0923 '/' Outflow=0.53 cfs	6 0.039 af
Total Runoff Area = $2.420$ ac Pun	off Volume = 0.952 af Average Punoff D	enth = 4 70"
79.95%	Pervious = 1.942 ac 20.05% Impervious	c = 0.487 ac

#### Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 1.17 cfs @ 12.09 hrs, Volume= 0.087 af, Depth> 6.12" Routed to Reach AP1 : Analysis Point 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN E	Description		
	3,741 3,651	98 F	Paved park	ing, HSG B	and HSG B
	7 302	80 \	Veighted A	verade	
	3.651	4	9.39% Per	vious Area	
	3,741	5	50.61% Imp	pervious Ar	ea
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.8	56	0.1250	0.34		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
2.1	30	0.0670	0.23		Sheet Flow,
			4.00		Grass: Short n= 0.150 P2= 3.70"
0.2	14	0.0360	1.26		Sheet Flow,
0.4	96	0.0260	2.05		Smooth surfaces h= 0.011 P2= 3.70"
0.4	00	0.0360	3.00		Shahow Concentrated Flow, Poved Ky= 20.3 fps
5.5	186	Total, I	ncreased t	o minimum	1 c = 6.0 min

#### Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 0.17 cfs @ 12.10 hrs, Volume= 0.013 af, Depth> 3.85" Routed to Reach AP2 : Analysis Point 2

A	rea (sf)	CN	Description					
	1,728	61	>75% Gras	s cover, Go	od, HSG B			
	1,728		100.00% P	ervious Are	а			
Tc (min)	Length (feet)	Slope (ft/ft)	velocity (ft/sec)	Capacity (cfs)	Description			
1.7	20	0.0500	0.19		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.70"	
1.7	20	Total,	Increased t	o minimum	Tc = 6.0 min			

#### Summary for Subcatchment 3S: Subcatchment 3S

Runoff	=	3.32 cfs @	12.24 hrs,	Volume=	0.332 af,	Depth>	3.84"
Routed	to Read	ch 1R : Ditch	on Tidewate	ch Property		-	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

	Area (sf)	CN E	Description		
	695	98 F	Roofs, HSC	βB	
	16,659	61 >	>75% Gras	s cover, Go	bod, HSG B
	27,823	60 V	Voods, Fai	r, HSG B	
	45,177	61 V	Veighted A	verage	
	44,482	ç	98.46% Pe	rvious Area	
	695	1	l.54% Impe	ervious Are	а
Т	c Length	Slope	Velocity	Capacity	Description
(mir	n) (feet)	(ft/ft)	(ft/sec)	(cfs)	
9.	0 53	0.0415	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
5.	8 47	0.0968	0.13		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
0.	2 15	0.0968	1.56		Shallow Concentrated Flow,
0		0.0744	4.00		Woodland Kv= 5.0 fps
0.	7 54	0.0741	1.36		Shallow Concentrated Flow,
4	2 400	0 4000	4 50		Woodland KV= 5.0 fps
1.	3 122	0.1000	1.58		Shallow Concentrated Flow,
		<b>—</b> ( )			
17.	.0 291	Total			

#### Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 2.19 cfs @ 12.12 hrs, Volume= 0.169 af, Depth> 4.20" Routed to Reach AP3 : Analysis Point 3

Area (sf)	CN	Description			
11,135	61	>75% Grass cover, Good, HSG B			
8,169	60	Voods, Fair, HSG B			
 1,687	98	Roofs, HSG B			
20,991	64	Weighted Average			
19,304		91.96% Pervious Area			
1,687		8.04% Impervious Area			

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Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.5	14	0.0357	0.16		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
1.9	14	0.1429	0.12		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
3.3	72	0.1333	0.37		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
1.0	80	0.0750	1.37		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.2	30	0.2667	2.58		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps

7.9 210 Total

## Summary for Subcatchment 6S: Subcatchment 6S

Runoff	=	0.37	cfs @	12.09 hrs,	Volume=
Routed	to Pond	CB1	01 : Čat	ch Basin 10	)1

0.031 af, Depth> 8.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

Area (sf)	CN	Description				
1,952	98	Paved park	ing, HSG B	В		
1,952		100.00% Impervious Area				
Tc Lengtł (min) (feet	n Slop ) (ft/i	e Velocity t) (ft/sec)	Capacity (cfs)	Description		
6.0				Direct Entry,		

# Summary for Subcatchment 7S: Subcatchment 7S

Runoff = 0.28 cfs @ 12.09 hrs, Volume= 0.024 af, Depth> 8.28" Routed to Pond CB102 : Catch Basin 102

Α	rea (sf)	CN	Description			
	1,516	98	Paved park	ing, HSG B	3	
	1,516		100.00% Impervious Area			
Tc (min)	Length (feet)	Slope (ft/ft	velocity (ft/sec)	Capacity (cfs)	Description	
6.0					Direct Entry,	

## Summary for Subcatchment 8S: Subcatchment 8S

Runoff = 0.57 cfs @ 12.09 hrs, Volume= 0.048 af, Depth> 8.28" Routed to Pond CB103 : Catch Basin 103

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description			
	2,554	98	Paved park	ing, HSG B	В	
	457	98	Roofs, HSC	βΒ		
	3,011	98	Weighted A	verage		
	3,011		100.00% In	npervious A	Area	
Тс	Length	Slop	e Velocity	Capacity	Description	
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)		
6.0					Direct Entry,	

## **Summary for Subcatchment 9S: Subcatchment 9S**

0.005 af, Depth> 8.28"

Runoff = 0.06 cfs @ 12.09 hrs, Volume= Routed to Pond CB104 : Catch Basin 104

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

Are	ea (sf)	CN	Description					
	325	98	98 Paved parking, HSG B					
	325		100.00% In	npervious A	Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

#### Summary for Subcatchment 10S: Subcatchment 10S

Runoff = 0.49 cfs @ 12.10 hrs, Volume= 0.036 af, Depth> 5.16" Routed to Pond YD1 : Yard Drain 1

Area (sf)	CN	Description
796	98	Roofs, HSG B
2,573	61	>75% Grass cover, Good, HSG B
261	98	Paved parking, HSG B
3,630	72	Weighted Average
2,573		70.88% Pervious Area
1,057		29.12% Impervious Area

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*Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"* Printed 4/19/2024

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.2	42	0.1190	0.31		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
3.7	58	0.0650	0.26		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
0.4	42	0.0650	1.78		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
6.2	140	Total			

6.3 142 I otal

#### Summary for Subcatchment 11S: Subcatchment 11S

Runoff = 0.71 cfs @ 12.09 hrs, Volume= 0.052 af, Depth> 6.00" Routed to Pond YD2 : Yard Drain 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description	l				
	1,998	98	Roofs, HSC	ЭB				
	2,312	61	>75% Gras	s cover, Go	ood, HSG B			
	261	98	Paved park	ting, HSG B	3			
	4,571	79	Weighted A	verage				
	2,312		50.58% Pe	rvious Area	l			
	2,259		49.42% Im	pervious Ar	ea			
Tc	Length	Slop	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft	i) (ft/sec)	(cfs)				
5.6	77	0.039	6 0.23		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.70"	
5.6	77	Total,	Increased	to minimum	n Tc = 6.0 min			

#### Summary for Subcatchment 12S: Subcatchment 12S

Runoff = 0.53 cfs @ 12.09 hrs, Volume= 0.039 af, Depth> 5.40" Routed to Pond YD3 : Yard Drain 3

Area (sf)	CN	Description
1,318	98	Roofs, HSG B
2,416	61	>75% Grass cover, Good, HSG B
3,734	74	Weighted Average
2,416		64.70% Pervious Area
1,318		35.30% Impervious Area

18134-PROPOSED					Type III 24-hr  50 Yr 24 Hr +15% Rainfall=8.53'				
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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
4.4	51	0.0320	0.19		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.70"				
4.4	51	Total, I	ncreased t	o minimum	n Tc = 6.0 min				
		Sum	mary fo	r Subcato	chment 13S: Subcatchment 13S				
Runoff Route	= ed to Pone	0.16 cf d 2P : St	s @ 12.0 one Drip E	9 hrs, Volu dge	ume= 0.014 af, Depth> 8.28"				
Runoff by Type III 2	y SCS TF 24-hr 50	R-20 met Yr 24 Hr	hod, UH=S +15% Rai	SCS, Weigh nfall=8.53"	hted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs '				
AI									
	696 180	98 F 98 V	Vater Surfa	ace. HSG B	3				
	876 876	98 V 1	Veighted A 00.00% In	verage pervious A	Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
6.0					Direct Entry,				
		Sum	mary fo	r Subcato	chment 14S: Subcatchment 14S				
Runoff Route	= ed to Pone	0.11 cf d 3P : St	s @ 12.0 one Under	9 hrs, Volu Deck	ume= 0.009 af, Depth> 8.28"				

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description		
	560	98	Roofs, HSC	βB	
	560		100.00% In	npervious A	Area
Tc (min)	Length (feet)	Slop (ft/fl	e Velocity ) (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

# Summary for Subcatchment 15S: Subcatchment 15S

Runoff = 0.16 cfs @ 12.09 hrs, Volume= 0.014 af, Depth> 8.28" Routed to Pond 4P : Stone Drip Edge

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Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53" Printed 4/19/2024

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A	rea (sf)	CN	Description		
	696	98	Roofs, HSC	βB	
	180	98	Water Surfa	ace, HSG B	3
	876	98	Weighted A	verage	
	876		100.00% In	npervious A	Area
Tc	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
6.0					Direct Entry,

## Summary for Subcatchment 18S: Subcatchment 18S

Runoff = 1.11 cfs @ 12.09 hrs, Volume= 0.081 af, Depth> 4.44" Routed to Pond 1P : Bioretention Pond

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"

A	rea (sf)	CN	Description					
	8,136	61	>75% Gras	s cover, Go	ood, HSG B			
	938	98	Roofs, HSC	βB				
	400	98	Paved park	ing, HSG B	5			
	9,474	66	Weighted A	verage				
	8,136		85.88% Pe	rvious Area				
	1,338		14.12% Im	pervious Ar	ea			
Tc	Length	Slop	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)				
2.5	43	0.093	0 0.29		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.70"	
0.6	15	0.333	3 0.39		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.70"	
3.1	58	Total.	Increased	to minimum	Tc = 6.0 min			

# Summary for Reach 1R: Ditch on Tidewatch Property

[62] Hint: Exceeded Reach 2R OUTLET depth by 0.49' @ 12.35 hrs
[62] Hint: Exceeded Reach 4R OUTLET depth by 0.45' @ 12.20 hrs
Inflow Area = 1.685 ac, 18.36% Impervious, Inflow Depth > 3.28" for 50 Yr 24 Hr +15% event
Inflow = 3.98 cfs @ 12.34 hrs, Volume= 0.460 af
Outflow = 3.98 cfs @ 12.35 hrs, Volume= 0.460 af, Atten= 0%, Lag= 0.7 min
Routed to Reach AP3 : Analysis Point 3

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 3.08 fps, Min. Travel Time= 0.9 min Avg. Velocity = 1.30 fps, Avg. Travel Time= 2.0 min

# **18134-PROPOSED** Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53" Prepared by Jones & Beach Engineers Inc Printed 4/19/2024 HydroCAD® 10.20-3c s/n 00762 © 2023 HydroCAD Software Solutions LLC Page 35

Peak Storage= 205 cf @ 12.35 hrs Average Depth at Peak Storage= 0.51', Surface Width= 4.06' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 18.18 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 7.00' Length= 159.0' Slope= 0.0189 '/' Inlet Invert= 38.00', Outlet Invert= 35.00'

Summary for Reach 2R: Flow through 3S

Inflow	=	0.12 cfs @ 12.26 hrs, Volume=	
Outflow	=	0.12 cfs @ 12.20 hrs, Volume=	
Routed	to	Reach 1R : Ditch on Tidewatch Property	V

0.006 af 0.006 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 1.55 fps, Min. Travel Time= 0.9 min Avg. Velocity = 1.07 fps, Avg. Travel Time= 1.3 min

Peak Storage= 6 cf @ 12.20 hrs Average Depth at Peak Storage= 0.02', Surface Width= 6.47' Bank-Full Depth= 1.00' Flow Area= 33.3 sf, Capacity= 740.30 cfs

50.00' x 1.00' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 81.0' Slope= 0.3457 '/' Inlet Invert= 66.00', Outlet Invert= 38.00'



# Summary for Reach 4R: Flow Through 3S

Inflow Area = 0.648 ac, 45.28% Impervious, Inflow Depth > 2.27" for 50 Yr 24 Hr +15% event Inflow = 1.18 cfs @ 12.42 hrs, Volume= 0.122 af Outflow = 1.17 cfs @ 12.43 hrs, Volume= 0.122 af, Atten= 1%, Lag= 0.8 min Routed to Reach 1R : Ditch on Tidewatch Property

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 3.19 fps, Min. Travel Time= 1.1 min Avg. Velocity = 1.09 fps, Avg. Travel Time= 3.4 min

Peak Storage= 81 cf @ 12.43 hrs Average Depth at Peak Storage= 0.11', Surface Width= 3.66' Bank-Full Depth= 1.00' Flow Area= 6.0 sf, Capacity= 66.79 cfs

3.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 9.00' Length= 220.0' Slope= 0.0909 '/' Inlet Invert= 58.00', Outlet Invert= 38.00'

‡

# Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	0.170 ac, 5	50.61% Imp	ervious,	Inflow Dept	th > 6	.12"	for 50 \	∕r 24 Hr ·	+15% event
Inflow	=	1.17 cfs @	12.09 hrs,	Volume	= 0.	.087 af				
Outflow	=	1.17 cfs @	12.09 hrs,	Volume	= 0.	.087 af	, Atter	n= 0%,	Lag= 0.0	min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

# Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	0.040 ac,	0.00% Impervious, Inflow D	epth > 3.85"	for 50 Yr 24 Hr +15% event
Inflow	=	0.17 cfs @	12.10 hrs, Volume=	0.013 af	
Outflow	=	0.17 cfs @	12.10 hrs, Volume=	0.013 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

# Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	ea =	2.167 ac, 16.06% Impervious, I	nflow Depth > 3.48" for 50 Yr 24 Hr +	15% event
Inflow	=	5.03 cfs @ 12.33 hrs, Volume=	0.629 af	
Outflow	=	5.03 cfs @ 12.33 hrs, Volume=	0.629 af, Atten= 0%, Lag= 0.0	min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

# Summary for Pond 1P: Bioretention Pond

Existing high contour within footprint of filter course = 61.0, SHWT depth = 35" per TP 10, so SHWT EI. = 58.08, which is 0.01' below the bottom of stone. However, in our experience, modelling the SHWT with such a small separation to the bottom of stone causes an unrealistically high amount of infiltration to appear in the calculations. Therefore, the SHWT has been modelled 2" lower as a factor of safety.

Inflow Area	ı =	0.648 ac,	45.28% Impe	ervious,	Inflow Depth >	5.84"	for 50 Yr	24 Hr +15% event
Inflow	=	4.12 cfs @	12.09 hrs,	Volume	= 0.315	af		
Outflow	=	1.30 cfs @	12.42 hrs,	Volume	= 0.254	af, Atte	n= 68%, L	.ag= 19.6 min
Discarded	=	0.12 cfs @	12.42 hrs,	Volume	= 0.132	af		
Primary	=	1.18 cfs @	12.42 hrs,	Volume	= 0.122	af		
Routed	to Reac	h 4R : Flow	Through 3S					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 62.85' @ 12.42 hrs Surf.Area= 3,187 sf Storage= 5,639 cf

Plug-Flow detention time= 216.2 min calculated for 0.254 af (81% of inflow) Center-of-Mass det. time= 139.8 min ( 930.8 - 791.0 )

Volume	Invert	Avail	.Storage	Storage	Description		
#1	58.09'		6,166 cf	Custom	Stage Data (Irregu	<b>Ilar)</b> Listed below	/ (Recalc)
Elevatio	on Su	urf.Area	Perim.	Voids	Inc.Store	Cum.Store	Wet.Area
	)() )()	466		( /0 )			(39-11)
58.0	19	400	106.0	0.0	0	0	400
58.1	10	466	106.0	40.0	2	2	467
59.0	)9	466	106.0	40.0	185	186	572
59.1	10	466	106.0	15.0	1	187	573
60.5	59	466	106.0	15.0	104	291	731
60.6	60	466	106.0	100.0	5	296	732
61.0	00	2,114	176.0	100.0	476	772	2,304
62.0	00	2,672	195.0	100.0	2,388	3,160	2,895
63.0	)0	3,285	215.0	100.0	2,973	6,133	3,579
63.0	)1	3,285	215.0	100.0	33	6,166	3,581
Device	Routing	١nv	vert Outle	et Device	s		
#1	Primary	58.	60' <b>12.0</b>	" Round	l Culvert		
	-		L= 1	8.0' CPI	P, projecting, no hea	dwall, Ke= 0.90	00
			Inlet	/ Outlet I	nvert= 58.60' / 58.00	)' S= 0.0333 '/'	Cc= 0.900
			n= 0	.012. Flo	w Area= 0.79 sf		
#2	Device 1	58.	90' <b>1.0</b> "	Vert. Or	ifice/Grate C= 0.60	0 Limited to w	eir flow at low heads
#3	Device 1	62	65' <b>15 0</b>	"Horiz (	Orifice/Grate C= 0	600	
	201100 1	52.	l imit	ted to we	ir flow at low heads		
<b>#</b> Δ	Discarded	58	09' <b>0 30</b>	0 in/hr F	vfiltration over Sur	face area	
<i>1</i> 1-1	Conductivity to Groundwater Elevation = 57.92' Phase-In= 0.10'						

**Discarded OutFlow** Max=0.12 cfs @ 12.42 hrs HW=62.85' (Free Discharge) **4=Exfiltration** (Controls 0.12 cfs)

Primary OutFlow Max=1.16 cfs @ 12.42 hrs HW=62.85' TW=58.11' (Dynamic Tailwater) 1=Culvert (Passes 1.16 cfs of 5.78 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.05 cfs @ 9.51 fps)

-3=Orifice/Grate (Weir Controls 1.11 cfs @ 1.45 fps)

# Summary for Pond 2P: Stone Drip Edge

Ledge surface modelled 15" below original grade based on TP 1 and TP 4. Proposed grade is approximately 4' above existing grade and therefore 5.25' above ledge.

Inflow Area	=	0.020 ac,10	0.00% Impe	ervious, Ir	nflow Depth >	8.28"	for 50 Y	′r 24 Hr +15% ev	ent
Inflow :	=	0.16 cfs @	12.09 hrs,	Volume=	0.014	af			
Outflow :	=	0.11 cfs @	12.20 hrs,	Volume=	0.009	af, Atte	en= 32%,	Lag= 6.6 min	
Discarded :	=	0.00 cfs @	12.15 hrs,	Volume=	0.005	5 af		•	
Secondary :	=	0.11 cfs @	12.20 hrs,	Volume=	0.004	af			
Routed t	o Reacl	h 2R : Flow t	hrough 3S						

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.01' @ 12.15 hrs Surf.Area= 0.004 ac Storage= 0.006 af

Plug-Flow detention time= 220.2 min calculated for 0.009 af (64% of inflow) Center-of-Mass det. time= 113.7 min (853.7 - 740.0)

Volume	Invert	Avail.Storage	Storage Description				
#1	62.50'	0.006 af	<b>3.00'W x 60.00'L x 3.51'H Prismatoid</b> 0.015 af Overall x 40.0% Voids				
Device	Routing	Invert Ou	utlet Devices				
#0	Secondary	66.01' <b>A</b> ı	Itomatic Storage Overflow (Discharged without head)				
#1	Discarded	62.50' <b>0.</b> 3	300 in/hr Exfiltration over Surface area				
		Co	onductivity to Groundwater Elevation = 60.75' Phase-In= 0.10'				

**Discarded OutFlow** Max=0.00 cfs @ 12.15 hrs HW=66.01' (Free Discharge) **1=Exfiltration** (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 12.20 hrs HW=66.01' TW=66.02' (Dynamic Tailwater)

# Summary for Pond 3P: Stone Under Deck

Ledge surface modelled 15" below original grade based on TP 1 and TP 4. Proposed grade is approximately 3.2' above existing grade and therefore 4.45' above ledge.

18134-		Beach En	nineers Inc	Type III 24-hr 50	Yr 24 Hi	r +15% Raii Printed	nfall=8.53" 4/19/2024
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	D® 10.20-30	3/11 007 02 @ 2					Fage 39
Inflow An Inflow Outflow Discarde Seconda Route	rea = ( = 0 = 0 ed = 0 ary = 0 ed to Reach	0.013 ac,100.0 .11 cfs @ 12 .05 cfs @ 12 .00 cfs @ 12 .04 cfs @ 12 2R : Flow thro	0% Impervious, Infl .09 hrs, Volume= .30 hrs, Volume= .25 hrs, Volume= .30 hrs, Volume= ugh 3S	ow Depth > 8.28" 0.009 af 0.006 af, Atte 0.004 af 0.002 af	for 50 Y en= 56%,	′r 24 Hr +159 Lag= 13.1 r	% event nin
Routing Peak Ele Plug-Elo	by Dyn-Stor- ev= 66.20' @ w detention :	Ind method, 1 12.25 hrs S	Time Span= 0.00-24 urf.Area= 0.006 ac in calculated for 0.0	.00 hrs, dt= 0.05 hrs Storage= 0.004 af 06 af (66% of inflow	/ 3		
Center-c	of-Mass det	time= 122 1 m	in (862 1 - 740 0 )		/		
e enter e							
Volume	Invert	Avail.Stora	ge Storage Descri	otion			
#1	64.70'	0.004	af <b>14.00'W x 20.0</b> 0.010 af Overal	<b>0'L x 1.50'H Prisma</b> Il x 40.0% Voids	itoid		
Device	Routina	Invert	Outlet Devices				
#0 #1	Secondary Discarded	66.20' 64.70'	Automatic Storage 0.300 in/hr Exfiltra	e Overflow (Dischar tion over Surface a	rged witho area	out head)	
			Conductivity to Gro	undwater Elevation =	= 61.75'	Phase-In=	0.10'
Discard Î──1=Ex	ed OutFlow filtration(C	Max=0.00 cfs Controls 0.00 c	@ 12.25 hrs HW=6 fs)	66.20' (Free Discha	arge)		
Second	ary OutFlow	/ Max=0.00 cf	s @ 12.30 hrs HW=	66.20' TW=66.02'	(Dynamic	c Tailwater)	

# Summary for Pond 4P: Stone Drip Edge

Ledge surface modelled 15" below original grade based on TP 1 and TP 4. Proposed grade is approximately 4' above existing grade and therefore 5.25' above ledge.

Inflow Area Inflow Outflow	= = =	0.020 ac,100. 0.16 cfs @ 12 0.03 cfs @ 12	00% Impervic 2.09 hrs, Vol 2.55 hrs, Vol	us, Inflow De ime= ime=	epth > 8.28 0.014 af 0.010 af, <i>A</i>	" for 50 Yr 24 Hr + Atten= 81%, Lag= 27.	15% event 8 min
Discarded	=	0.01 cfs @ 12	2.50 hrs, Vol	ime=	0.009 af		
Secondary	=	0.02 cfs @ 12	2.55 hrs, Vol	ime=	0.001 af		
Routed	to Reac	n 2R : Flow thr	ough 3S				
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 66.01' @ 12.50 hrs Surf.Area= 0.004 ac Storage= 0.007 af Plug-Flow detention time= 297.2 min calculated for 0.010 af (70% of inflow) Center-of-Mass det. time= 201.2 min ( 941.2 - 740.0 )							
Volume	Inve	t Avail.Stora	age Storage	Description			
#1	61.50	)' 0.007	7 af <b>3.00'W</b> 0.019 a	<b>60.00'L x 4</b> Overall x 40	. <b>51'H Prism</b> ).0% Voids	atoid	

#### 18134-PROPOSED

*Type III 24-hr 50 Yr 24 Hr +15% Rainfall=8.53"* Printed 4/19/2024

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Prepared by Jones & Beach Engineers Inc HydroCAD® 10.20-3c s/n 00762 © 2023 HydroCAD Software Solutions LLC

Device	Routing	Invert	Outlet Devices	
#0 #1	Secondary Discarded	66.01' 61.50'	Automatic Storage Overflow (Discharged without head)0.300 in/hr Exfiltration over Surface areaConductivity to Groundwater Elevation = 60.75'Phase-In= 0.10'	-
Discard	led OutFlow Ma	x=0.01 cf	s @ 12.50 hrs HW=66.01' (Free Discharge)	

**1=Exfiltration** (Controls 0.01 cfs)

Secondary OutFlow Max=0.00 cfs @ 12.55 hrs HW=66.01' TW=66.01' (Dynamic Tailwater)

# Summary for Pond CB101: Catch Basin 101

 Inflow Area =
 0.128 ac, 53.91% Impervious, Inflow Depth > 6.25" for 50 Yr 24 Hr +15% event

 Inflow =
 0.86 cfs @
 12.09 hrs, Volume=
 0.067 af

 Outflow =
 0.86 cfs @
 12.09 hrs, Volume=
 0.067 af, Atten= 0%, Lag= 0.0 min

 Primary =
 0.86 cfs @
 12.09 hrs, Volume=
 0.067 af

 Routed to Pond CB102 : Catch Basin 102
 0.067 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 63.28' @ 12.10 hrs Flood Elev= 65.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	62.30'	<b>12.0" Round Culvert</b> L= 19.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 62.30' / 62.20' S= 0.0053 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=63.24' TW=63.35' (Dynamic Tailwater)

# Summary for Pond CB102: Catch Basin 102

[80] Warning: Exceeded Pond CB101 by 0.14' @ 12.10 hrs (1.10 cfs 0.017 af)

 Inflow Area =
 0.163 ac, 63.75% Impervious, Inflow Depth > 6.69" for 50 Yr 24 Hr +15% event

 Inflow =
 1.14 cfs @ 12.09 hrs, Volume=
 0.091 af

 Outflow =
 1.14 cfs @ 12.09 hrs, Volume=
 0.091 af, Atten= 0%, Lag= 0.0 min

 Primary =
 1.14 cfs @ 12.09 hrs, Volume=
 0.091 af

 Routed to Pond CB104 : Catch Basin 104
 0.091 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 63.42' @ 12.11 hrs Flood Elev= 65.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	62.10'	<b>12.0" Round Culvert</b> L= 147.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 62.10' / 61.30' S= 0.0054 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

**Primary OutFlow** Max=1.17 cfs @ 12.09 hrs HW=63.34' TW=63.16' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 1.17 cfs @ 1.54 fps)

# Summary for Pond CB103: Catch Basin 103

Inflow Area	a =	0.260 ac, 5	58.22% Impe	ervious,	Inflow Depth >	6.41"	for 50	Yr 24 Hr +15%	% event
Inflow	=	1.81 cfs @	12.09 hrs,	Volume	= 0.139	af			
Outflow	=	1.81 cfs @	12.09 hrs,	Volume	= 0.139	af, Att	en= 0%,	Lag= 0.0 min	1
Primary	=	1.81 cfs @	12.09 hrs,	Volume	= 0.139	af		•	
Routed	to Pond	CB104 : Ca	tch Basin 10	)4					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 67.16' @ 12.09 hrs Flood Elev= 73.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	66.30'	12.0" Round Culvert
			L= 43.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 66.30' / 66.00' S= 0.0070 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=1.76 cfs @ 12.09 hrs HW=67.15' TW=63.15' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 1.76 cfs @ 2.48 fps)

# Summary for Pond CB104: Catch Basin 104

Inflow Area	ı =	0.430 ac, 6	61.04% Impe	ervious,	Inflow Depth >	6.55"	for 50	Yr 24 Hr +15%	event
Inflow	=	3.01 cfs @	12.09 hrs,	Volume	= 0.235	af			
Outflow	=	3.01 cfs @	12.09 hrs,	Volume	= 0.235	af, Atter	ו= 0%,	Lag= 0.0 min	
Primary	=	3.01 cfs @	12.09 hrs,	Volume	= 0.235	af			
Routed	to Pond	1P : Biorete	ntion Pond						

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 63.25' @ 12.11 hrs Flood Elev= 70.80'

Device	Routing	Invert	Outlet Devices
#1	Primary	61.20'	<b>12.0" Round Culvert</b> L= 45.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 61.20' / 60.90' S= 0.0067 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=2.94 cfs @ 12.09 hrs HW=63.15' TW=62.18' (Dynamic Tailwater) -1=Culvert (Inlet Controls 2.94 cfs @ 3.74 fps)

# Summary for Pond YD1: Yard Drain 1

 Inflow Area =
 0.083 ac, 29.12% Impervious, Inflow Depth > 5.16" for 50 Yr 24 Hr +15% event

 Inflow =
 0.49 cfs @
 12.10 hrs, Volume=
 0.036 af

 Outflow =
 0.49 cfs @
 12.10 hrs, Volume=
 0.036 af, Atten= 0%, Lag= 0.0 min

 Primary =
 0.49 cfs @
 12.10 hrs, Volume=
 0.036 af

 Routed to Pond CB101 : Catch Basin 101
 0.036 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 63.50' @ 12.15 hrs Flood Elev= 65.80'

Device	Routing	Invert	Outlet Devices
#1	Primary	62.80'	<b>8.0" Round Culvert</b> L= 9.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 62.80' / 62.63' S= 0.0189 '/' Cc= 0.900 n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.34 cfs @ 12.10 hrs HW=63.34' TW=63.25' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 0.34 cfs @ 1.12 fps)

# Summary for Pond YD2: Yard Drain 2

 Inflow Area =
 0.105 ac, 49.42% Impervious, Inflow Depth > 6.00" for 50 Yr 24 Hr +15% event

 Inflow =
 0.71 cfs @ 12.09 hrs, Volume=
 0.052 af

 Outflow =
 0.71 cfs @ 12.09 hrs, Volume=
 0.052 af, Atten= 0%, Lag= 0.0 min

 Primary =
 0.71 cfs @ 12.09 hrs, Volume=
 0.052 af

 Routed to Pond CB103 : Catch Basin 103
 0.052 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 67.72' @ 12.09 hrs Flood Elev= 69.30'

Device	Routing	Invert	Outlet Devices
#1	Primary	67.10'	8.0" Round Culvert L= 52.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 67.10' / 66.80' S= 0.0058 '/' Cc= 0.900 n= 0.012, Flow Area= 0.35 sf

Primary OutFlow Max=0.70 cfs @ 12.09 hrs HW=67.71' TW=67.15' (Dynamic Tailwater) -1=Culvert (Inlet Controls 0.70 cfs @ 2.09 fps)

# Summary for Pond YD3: Yard Drain 3

Inflow Area	a =	0.086 ac,	35.30% Imp	ervious,	Inflow Depth >	5.40"	for 50	Yr 24 Hr +15% ev	/ent
Inflow	=	0.53 cfs @	12.09 hrs,	Volume	= 0.039	af			
Outflow	=	0.53 cfs @	12.09 hrs,	Volume	= 0.039	af, Atte	en= 0%,	Lag= 0.0 min	
Primary	=	0.53 cfs @	12.09 hrs,	Volume	= 0.039	af		-	
Routed	to Pond	CB103 : C	atch Basin 10	03					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 68.50' @ 12.09 hrs Flood Elev= 70.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	68.00'	<b>8.0" Round Culvert</b> L= 13.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 68.00' / 66.80' S= 0.0923 '/' Cc= 0.900 n= 0.012, Flow Area= 0.35 sf
Primary <sup>€</sup> —1=Cu	• OutFlow M Ivert (Inlet C	ax=0.52 cfs @ Controls 0.52 (	0 12.09 hrs HW=68.49' TW=67.15' (Dynamic Tailwater) cfs @ 1.88 fps)

# APPENDIX III

**Test Pit Logs** 



GOVE ENVIRONMENTAL SERVICES, INC.

TEST PIT DATA

Project Client GES Proje MM/DD/Y	635 Sagam 635 Sagam ct No. GE YY Staff 3-1	ore Ave ore Developm S 2021307 8-2022 JPC	ent LLC G		
Test Pit N ESHWT: 1 Terminatio Refusal: 1 Obs. Wate	lo. 1 n/a on @ 15" 15" or: none		SCS	Soil:	Hollis
Depth 0–5" 5–15"	Color 10YR 3/2 10YR 5/6	Texture FSL FSL	Structure GR GR	Consistence FR FR	Redox; Quantity/Contrast NONE NONE
<b>Test Pit N</b> ESHWT: 1 Terminatio Refusal: 2 Obs. Wate	H <b>o. 2</b> n/a pn @ 25" 25" pr: none		SCS	Soil:	Chatfield
Depth 0–5" 5–25"	Color 10YR 3/2 10YR 5/6	Texture FSL FSL	Structure GR GR	Consistence FR FR	Redox; Quantity/Contrast NONE NONE
<b>Test Pit N</b> ESHWT: 1 Terminatio Refusal: 2 Obs. Wate	<b>10. 3</b> n/a on @ 25" 25" er: none		SCS	Soil:	Chatfield
Depth 0–6" 6–25"	Color 10YR 3/2 10YR 5/6	Texture FSL FSL	Structure GR GR	Consistence FR FR	Redox; Quantity/Contrast NONE NONE

<b>Test Pit N</b> ESHWT: n Terminatio Refusal: 1 Obs. Water	<b>o. 4</b> 1/a on @ 15" 5" r: none		SCS	Soil:	Hollis
Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0–15"	10YR 3/2	FSL	GR	FR	NONE
<b>Test Pit N</b> ESHWT: 3 Terminatic Refusal: 3 Obs. Water	<b>o. 5</b> 60'' on @ 36'' 6'' r: none		SCS	Soil:	Chatfield variant
Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0–8"	10YR 3/2	FSL	GR	FR	NONE
8–30"	10YR 4/6	FSL	GR	FR	NONE
30–36"	2.5Y 5/3	FSL	GR	FR	10% Distinct
<b>Test Pit N</b> ESHWT: n Terminatio Refusal: 1 Obs. Water	<b>o. 6</b> //a on @ 12" 2" r: none		SCS	Soil:	Hollis
Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0–12"	10YR 3/2	FSL	GR	FR	NONE
<b>Test Pit N</b> ESHWT: n Terminatic Refusal: 2 Obs. Water	<b>o. 7</b> //a on @ 27" 7" r: none		SCS	Soil:	Chatfield
Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0–4"	10YR 3/2	FSL	GR	FR	NONE
4–27"	10YR 5/6	FSL	GR	FR	NONE

<b>Test Pit N</b> ESHWT: 3 Termination Refusal: 4 Obs. Wate	<b>6. 8</b> 35" on @ 40" .0" r: none		SCS	Soil:	Chatfield variant
Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0–6"	10YR 3/2	FSL	GR	FR	NONE
6–35"	10YR 5/6	FSL	GR	FR	NONE
35–40"	2.5Y 5/3	FSL	OM	FI	10% Distinct
<b>Test Pit N</b> ESHWT: r Terminatic Refusal: 2 Obs. Wate	<b>6. 9</b> n/a on @ 27" 7" r: none		SCS	Soil:	Chatfield
Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0–4"	10YR 3/2	FSL	GR	FR	NONE
4–27"	10YR 5/6	FSL	GR	FR	NONE

Test Pit N	lo. 10				
ESHWT:	35				
Terminatio	on @ 62"				
Refusal: 6	52"		SCS	Soil:	Scituate
Obs. Wate	er: none				
Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0–10"	10YR 3/2	FSL	GR	FR	NONE
10–35"	10YR 5/6	FSL	GR	FR	NONE
35–62"	2.5Y 5/3	FSL	PL	FI	10%, Distinct



3-21-2022

Legend:

FSL = fine sandy loam GR = granular PL = platy FI = firm

# APPENDIX IV

Site Specific Soil Survey Report and Map



# GOVE ENVIRONMENTAL SERVICES, INC

SITE-SPECIFIC SOIL SURVEY REPORT For 635 Sagamore Avenue, Portsmouth, NH By GES, Inc. Project # 2021308 Date: 02-20-2024

#### 1. MAPPING STANDARDS

*Site-Specific Soil Mapping Standards for New Hampshire and Vermont.* SSSNNE Special Publication No. 3, Version 7.0, July, 2021.

This map product is within the technical standards of the National Cooperative Soil Survey. It is a special purpose product, intended for infiltration requirements by the NH DES Alteration of Terrain Bureau. The soil map was produced by a professional soil scientist and is not a product of the USDA Natural Resources Conservation Service. This report accompanies the soil map.

The site-specific soil map (SSSM) was produced 2-20-2024; prepared by JP Gove, CSS #004, GES, Inc.

Soils were identified with the New Hampshire State-wide Numerical Soils Legend, USDA NRCS, Durham, NH. Issue # 10, January 2011.

Hydrologic Soil Group was determined using SSSNNE Special Publication No. 5, Ksat Values for New Hampshire Soils, September 2009.

High Intensity Soil Map symbols, based upon SSSNNE Special Publication 1, December 2017, were added to the Soil Legend.

Scale of soil map: Approximately 1'' = 20'.

Contours Interval: 2 feet

#### 2. LANDFORMS & EXISTING CONDITIONS:

The site is located on sloping hillside that is bedrock controlled. Rock outcrops are numerous. At the top of the hill, adjacent Sagamore Avenue, is an existing commercial building and paved areas. Behind the impervious areas to the south, the hillside slopes downward. The area is forested in white pines. There are no wetlands on the site.

#### 3. DATE SOIL MAP PRODUCED

Date(s) of on-site field work:3-18-2022Date(s) of test pits:3-18-2922

Test pits recorded by: JP Gove, CSS # 004

#### 4. GEOGRAPHIC LOCATION AND SIZE OF SITE

City or town where soil mapping was conducted: Portsmouth, NH Location: Tax Map 222 Lot 19 Size of area: Approximately 2 acres Was the map for the entire lot? Yes If no, where was the mapping conducted on the parcel: n/a

#### 5. <u>PURPOSE OF THE SOIL MAP</u>

Was the map prepared to meet the requirement of Alteration of Terrain? No If no, what was the purpose of the map? City of Portsmouth requirements Who was the map prepared for? Jones & Beach Engineers, Inc.



#### 6. <u>SOIL IDENTIFICATION LEGEND</u>

Map L	Jnit Symbol	Map Unit N	ame		HISS Symb	ol	Hydrologic S	oil Group
41	Chatfield-H	Iollis-Rock O	utcrop complex		228		В	
289	Chatfield V	ariant (mode	erately well drai	ned)	327		В	
699	Urban Land				n/a		Impervious	
SLOPE	PHASE:							
0-8%	В		8-15%	С		15-25%	D	
25%-50	)% E		50%+	F				

## 7. NARRATIVE MAP UNIT DESCRIPTIONS

SITE-SPECIFIC MAP UNIT: 41

CORRELATED SOIL SERIES: Chatfield-Hollis-Rock Outcrop complex

LANDSCAPE SETTING: Sloping to very steep hillside.

CHARACTERISTIC SURFACE FEATURES: Numerous rock outcrops

DRAINAGE CLASS: Well drained

PARENT MATERIAL: Glacial Till

NATURE OF DISSIMILAR INCLUSIONS: With a complex, several similar soils are present. While the major soil is the moderately deep Chatfield, the shallow Hollis and the exposed ledge of the Rock Outcrop, are large minor components. Chatfield is 50%, Hollis is 25%, and Rock Outcrop is 25%. A few deeper soil areas are present in hollow in the bedrock.

ESTIMATED PERCENTAGE OF DISSIMILAR INCLUSIONS: less than 5%.

SOIL PROFILE DESCRIPTIONS- horizon designation, depth, soil texture, Munsell color notation, Munsell color of redox features, soil structure, soil consistence, estimated coarse fragments, estimated seasonal high water table (ESHWT), observed water table (OBSWT), kind of water table (perched, apparent, or both), depth to lithic or paralithic contact:

3				
@ 25"				
Refusal: 25"		SCS Soil:		Chatfield
none				
Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
10YR 3/2	FSL	GR	FR	NONE
10YR 5/6	FSL	GR	FR	NONE
	3 @ 25" none Color 10YR 3/2 10YR 5/6	<b>3</b> (a) 25" none Color Texture 10YR 3/2 FSL 10YR 5/6 FSL	<b>3</b> (a) 25" SCS none Color Texture Structure 10YR 3/2 FSL GR 10YR 5/6 FSL GR	<b>3</b> (a) 25" SCS Soil: none Color Texture Structure Consistence 10YR 3/2 FSL GR FR 10YR 5/6 FSL GR FR

No OBSWT, no ESHWT, lithic contact at 25", 20% rock fragments.

Test Pit N	lo. 1				
ESHWT:	n/a				
Terminati	on @ 15"				
Refusal: 15"		SCS Soil:		Hollis	
Obs. Wate	er: none				
Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-5"	10YR 3/2	FSL	GR	FR	NONE
5–15"	10YR 5/6	FSL	GR	FR	NONE

No OBSWT, no ESHWT, lithic contact at 15", 20% rock fragments.

SITE-SPECIFIC MAP UNIT: 289

CORRELATED SOIL SERIES: Chatfield Variant (moderately well drained)



LANDSCAPE SETTING: At the top of the slope, a slightly deeper soil area on the northwest corner of the site.

CHARACTERISTIC SURFACE FEATURES: Fewer outcrops than the rest of the site.

DRAINAGE CLASS: Moderately well drained.

PARENT MATERIAL: Glacial till.

NATURE OF DISSIMILAR INCLUSIONS: Scituate soils with a hard pan above the bedrock,

ESTIMATED PERCENTAGE OF DISSIMILAR INCLUSIONS: 5%

SOIL PROFILE DESCRIPTIONS- horizon designation, depth, soil texture, Munsell color notation, Munsell color of redox features, soil structure, soil consistence, estimated coarse fragments, estimated seasonal high water table (ESHWT), observed water table (OBSWT), kind of water table (perched, apparent, or both), depth to lithic or paralithic contact:

Test Pit N ESHWT: 3	<b>0.</b> 5 30"				
Terminatio	on @ 36"				
Refusal: 36"		SCS Soil:		Chatfield variant	
Obs. Wate	r: none				
Depth	Color	Texture	Structure	Consistence	Redox; Quantity/Contrast
0-8"	10YR 3/2	FSL	GR	FR	NONE
8–30"	10YR 4/6	FSL	GR	FR	NONE
30–36"	2.5Y 5/3	FSL	GR	FR	10% Distinct

ESHWT is 30", no OBSWT, lithic contact at 36", 20% rock fragments.

SITE-SPECIFIC MAP UNIT: 699

CORRELATED SOIL SERIES: Urban land

LANDSCAPE SETTING: Top of slope adjacent to Sagamore Avenue.

CHARACTERISTIC SURFACE FEATURES: Impervious.

DRAINAGE CLASS: N/A

PARENT MATERIAL: N/A

NATURE OF DISSIMILAR INCLUSIONS: N/A

ESTIMATED PERCENTAGE OF DISSIMILAR INCLUSIONS: N/A

SOIL PROFILE DESCRIPTIONS- horizon designation, depth, soil texture, Munsell color notation, Munsell color of redox features, soil structure, soil consistence, estimated coarse fragments, estimated seasonal high water table (ESHWT), observed water table (OBSWT), kind of water table (perched, apparent, or both), depth to lithic or paralithic contact:

N/A ---- Pavement and buildings.


#### 8. <u>RESPONSIBLE SOIL SCIENTIST</u>

Name: James Gove

Certified Soil Scientist Number: 004

#### 9. OTHER DISTINGUISHING FEATURES OF SITE

Is the site in a natural condition? Yes, with exception of existing development.



## APPENDIX V

### NRCS Soil Map



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey 3/8/2024 Page 1 of 3



# Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
140B	Chatfield-Hollis-Canton complex, 0 to 8 percent slopes, rocky	0.7	30.5%
140D	Chatfield-Hollis-Canton complex, 15 to 35 percent slopes, rocky	1.6	69.5%
Totals for Area of Interest		2.3	100.0%



# APPENDIX VI

### **Extreme Precipitation Estimates**



## **Extreme Precipitation Tables**

#### Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

#### **Metadata for Point**

Smoothing	Yes
State	
Location	
Latitude	43.058 degrees North
Longitude	70.753 degrees West
Elevation	10 feet
Date/Time	Wed Feb 21 2024 09:41:54 GMT-0500 (Eastern Standard Time)

+15% due to location in Coastal/Great Bay Region 2yr: 3.22\*1.15 = 3.70 in 10yr: 4.88\*1.15 = 5.16 in 25yr: 6.19\*1.15 = 7.12 in 50yr: 7.42\*1.15 = 8.53 in

#### **Extreme Precipitation Estimates**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day
1yr	0.26	0.40	0.50	0.65	0.82	1.04	1yr	0.70	0.98	1.21	1.56	2.03	2.67	2.94	1yr	2.36	2.82	3.24	3.96	4.57
2yr	0.32	0.50	0.62	0.82	1.03	1.30	2yr	0.89	1.18	1.52	1.94	2.49	<mark>3.22</mark>	3.58	2yr	2.85	3.45	3.95	4.70	5.35
5yr	0.37	0.58	0.73	0.98	1.25	1.61	5yr	1.08	1.47	1.89	2.44	3.15	4.08	4.60	5yr	3.61	4.42	5.07	5.96	6.73
10yr	0.41	0.65	0.82	1.12	1.46	1.90	10yr	1.26	1.73	2.24	2.90	3.76	<mark>4.88</mark>	5.55	10yr	4.32	5.34	6.12	7.14	8.01
25yr	0.48	0.76	0.97	1.34	1.78	2.35	25yr	1.54	2.15	2.79	3.65	4.76	<mark>6.19</mark>	7.13	25yr	5.48	6.86	7.85	9.07	10.09
50yr	0.54	0.86	1.11	1.55	2.08	2.77	50yr	1.80	2.54	3.31	4.35	5.69	<mark>7.42</mark>	8.62	50yr	6.57	8.29	9.48	10.87	12.02
100yr	0.60	0.97	1.25	1.78	2.43	3.28	100yr	2.10	2.99	3.93	5.19	6.80	8.89	10.42	100yr	7.87	10.02	11.46	13.04	14.33
200yr	0.68	1.11	1.44	2.06	2.85	3.86	200yr	2.46	3.54	4.65	6.17	8.12	10.65	12.60	200yr	9.43	12.12	13.85	15.64	17.09
500yr	0.81	1.33	1.73	2.51	3.51	4.80	500yr	3.03	4.41	5.81	7.76	10.28	13.54	16.21	500yr	11.98	15.59	17.81	19.90	21.58

### **Lower Confidence Limits**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day
1yr	0.23	0.36	0.44	0.59	0.72	0.88	1yr	0.62	0.86	0.93	1.33	1.69	2.26	2.51	1yr	2.00	2.41	2.88	3.20	3.93
2yr	0.32	0.49	0.60	0.81	1.00	1.19	2yr	0.86	1.16	1.37	1.82	2.33	3.07	3.47	2yr	2.72	3.33	3.84	4.56	5.11
5yr	0.35	0.54	0.67	0.92	1.17	1.40	5yr	1.01	1.37	1.61	2.11	2.73	3.80	4.21	5yr	3.36	4.05	4.74	5.56	6.27
10yr	0.39	0.59	0.74	1.03	1.33	1.60	10yr	1.15	1.57	1.81	2.38	3.05	4.39	4.88	10yr	3.88	4.70	5.48	6.45	7.23
25yr	0.44	0.67	0.83	1.19	1.57	1.90	25yr	1.35	1.86	2.10	2.74	3.52	4.77	5.92	25yr	4.22	5.70	6.70	7.85	8.73
50yr	0.48	0.73	0.92	1.32	1.77	2.17	50yr	1.53	2.12	2.35	3.06	3.91	5.40	6.84	50yr	4.78	6.58	7.79	9.11	10.08
100yr	0.54	0.81	1.02	1.47	2.02	2.47	100yr	1.74	2.42	2.63	3.39	4.33	6.08	7.90	100yr	5.38	7.60	9.07	10.60	11.64
200yr	0.59	0.89	1.13	1.64	2.29	2.82	200yr	1.97	2.75	2.94	3.75	4.76	6.83	9.12	200yr	6.05	8.77	10.54	12.34	13.47
500yr	0.69	1.02	1.32	1.92	2.72	3.37	500yr	2.35	3.29	3.42	4.28	5.41	7.97	11.03	500yr	7.06	10.61	12.87	15.13	16.32

#### **Upper Confidence Limits**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day
1yr	0.29	0.44	0.54	0.72	0.89	1.08	1yr	0.77	1.06	1.26	1.74	2.20	2.99	3.18	1yr	2.64	3.05	3.59	4.38	5.06
2yr	0.34	0.52	0.64	0.87	1.07	1.27	2yr	0.92	1.24	1.48	1.96	2.51	3.43	3.72	2yr	3.03	3.57	4.10	4.86	5.64
5yr	0.40	0.62	0.77	1.05	1.34	1.63	5yr	1.16	1.59	1.89	2.54	3.25	4.36	4.98	5yr	3.85	4.79	5.40	6.40	7.18
10yr	0.47	0.72	0.89	1.25	1.61	1.98	10yr	1.39	1.94	2.29	3.11	3.96	5.36	6.22	10yr	4.74	5.98	6.84	7.87	8.78
25yr	0.58	0.88	1.09	1.56	2.06	2.58	25yr	1.77	2.52	2.96	4.08	5.17	7.77	8.36	25yr	6.87	8.04	9.18	10.37	11.44
50yr	0.67	1.03	1.28	1.84	2.48	3.15	50yr	2.14	3.08	3.61	5.01	6.35	9.71	10.48	50yr	8.60	10.08	11.48	12.76	14.00
100yr	0.80	1.20	1.51	2.17	2.98	3.83	100yr	2.57	3.75	4.39	6.18	7.80	12.14	13.13	100yr	10.74	12.62	14.35	15.74	17.13
200yr	0.93	1.40	1.78	2.57	3.58	4.69	200yr	3.09	4.58	5.36	7.61	9.60	15.22	16.46	200yr	13.47	15.83	17.96	19.40	20.96
500yr	1.16	1.72	2.22	3.22	4.58	6.09	500yr	3.95	5.95	6.96	10.07	12.65	20.54	22.22	500yr	18.18	21.36	24.18	25.57	27.38



# APPENDIX VII

### **Rip Rap Calculations**

#### **RIP RAP CALCULATIONS**

"Luster Cluster" 635 Sagamore Ave. Portsmouth, NH

#### Jones & Beach Engineers, Inc.

P.O. Box 219 Stratham, NH 03885 3/14/2024 REVISED 4/19/2024

Rip Rap equations were obtained from the *Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire.* Aprons are sized for the 10-Year storm event.

#### TAILWATER < HALF THE $D_0$

$$\begin{split} & L_a = (1.8 \text{ x } \text{Q}) \ / \ D_0^{-3/2} + (7 \text{ x } D_o) \\ & W = L_a + (3 \text{ x } D_o) \text{ or defined channel width} \\ & d_{50} = (0.02 \text{ x } \text{Q}^{4/3}) \ / \ (T_w \text{ x } D_0) \end{split}$$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	d <sub>50</sub> -Median Stone
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	Rip Rap
(Sta. No.)	$T_w$	Q	$D_{o}$	L <sub>a</sub> (feet)	W (feet)	d50 (feet)
1P Outlet Pipe	0.12	0.21	1	7.4	10	0.02

#### TAILWATER > HALF THE D<sub>o</sub>

$$\begin{split} &L_a = (3.0 \ x \ Q) \ / \ {D_0}^{3/2} + (7 \ x \ D_o) \\ &W = (0.4 \ x \ L_a) + (3 \ x \ D_o) \ \text{or defined channel width} \\ &d_{50} = (0.02 \ x \ Q^{4/3}) \ / \ (T_w \ x \ D_0) \end{split}$$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	d <sub>50</sub> -Median Stone
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	Rip Rap
(Sta. No.)	$T_w$	Q	D <sub>o</sub>	$L_{a}$ (feet)	W (feet)	d50 (feet)
CB4 Outlet Pipe	0.66	2.41	1	14.2	9	0.10

Table 7-24 Recommended Rip Rap Gradation Ranges										
$d_{50}$ Size =	0.25	Feet	3	Inches						
% of Weight Smaller		Siz	ze of Stone (Inc	ches)						
Than the Given d <sub>50</sub> Size		From		То						
100%		5		6						
85%		4		5						
50%		3		5						
15%		1		2						

Table 7-24 Recommended Rip Rap Gradation Ranges										
$d_{50}$ Size =	0.5	Feet	6	Inches						
% of Weight Smaller		Siz	ze of Stone (Ind	ches)						
Than the Given d <sub>50</sub> Size		From		То						
100%		9		12						
85%		8		11						
50%		6		9						
15%		2		3						

## APPENDIX VIII

### **BMP Worksheets**



### FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

### Type/Node Name:

#### **Bioretention Pond (1P)**

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

		Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.07	7(a).
0.65	ас	A = Area draining to the practice	
0.29	ас	A <sub>I</sub> = Impervious area draining to the practice	
0.45	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.46	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x l)	
0.30	ac-in	WQV= 1" x Rv x A	
1,076	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
269	cf	25% x WQV (check calc for sediment forebay volume)	
807	cf	75% x WQV (check calc for surface sand filter volume)	
Deep Su	ump CBs	Method of Pretreatment? (not required for clean or roof runoff)	
	cf	V <sub>SED</sub> = Sediment forebay volume, if used for pretreatment	<u>&gt;</u> 25%WQV
Calculate ti	me to drair	n if system IS NOT underdrained:	
	sf	A <sub>SA</sub> = Surface area of the practice	
	iph	Ksat <sub>DESIGN</sub> = Design infiltration rate <sup>1</sup>	
	-	If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?	
	Yes/No	(Use the calculations below)	
-	hours	$T_{DRAIN} = Drain time = V / (A_{SA} * I_{DESIGN})$	<u>&lt;</u> 72-hrs
Calculate ti	me to drair	if system IS underdrained:	
61.15	ft	E <sub>WQV</sub> = Elevation of WQV (attach stage-storage table)	
0.11	-		
0.11	cfs	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table)	
5.44	hours	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) T <sub>DRAIN</sub> = Drain time = 2WQV/Q <sub>WQV</sub>	<u>&lt;</u> 72-hrs
5.44 59.10	cfs hours feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) T <sub>DRAIN</sub> = Drain time = 2WQV/Q <sub>WQV</sub> $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup>	<u>&lt;</u> 72-hrs
0.11 5.44 59.10 58.60	feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = 2WQV/ $Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable	<u>&lt;</u> 72-hrs
0.11 5.44 59.10 58.60 58.08	cts hours feet feet feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = 2WQV/ $Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pi	<u>≤ <b>72-hrs</b></u>
0.11 5.44 59.10 58.60 58.08 55.83	cts hours feet feet feet feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilter E <sub>ROCK</sub> = Elevation of bedrock (if none found, enter the lowest elevation of the test	<b>≤ 72-hrs</b> t) pit)
0.11 5.44 59.10 58.60 58.08 55.83 0.50	cts hours feet feet feet feet feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = 2WQV/ $Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilter E <sub>ROCK</sub> = Elevation of bedrock (if none found, enter the lowest elevation of the test D <sub>FC to UD</sub> = Depth to UD from the bottom of the filter course	≤ 72-hrs it) ≥ 1'
0.11 5.44 59.10 58.60 58.08 55.83 0.50 3.27	cts hours feet feet feet feet feet feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = 2WQV/ $Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilt $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test pilt $D_{FC to UD}$ = Depth to UD from the bottom of the filter course $D_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course	≤ 72-hrs t) pit) ≥ 1' ≥ 1'
0.11 5.44 59.10 58.60 58.08 55.83 0.50 3.27 1.02	cts hours feet feet feet feet feet feet feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilt $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test pilt $D_{FC to UD}$ = Depth to UD from the bottom of the filter course $D_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course	≤ 72-hrs t) pit) ≥ 1' ≥ 1' ≥ 1' ≥ 1'
0.11 5.44 59.10 58.60 58.08 55.83 0.50 3.27 1.02 62.85	cts hours feet feet feet feet feet feet feet fee	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilt $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test pilt $D_{FC to UD}$ = Depth to UD from the bottom of the filter course $D_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis)	≤ 72-hrs it) ≥ 1' ≥ 1' ≥ 1' ≥ 1'
0.11 5.44 59.10 58.60 58.08 55.83 0.50 3.27 1.02 62.85 63.00	cts hours feet feet feet feet feet feet feet ft	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilter EROCK = Elevation of bedrock (if none found, enter the lowest elevation of the test pilter to UD from the bottom of the filter course $D_{FC to UD}$ = Depth to UD from the bottom of the filter course $D_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice	≤ 72-hrs t) pit) ≥ 1' ≥ 1' ≥ 1' ≥ 1'
0.11 5.44 59.10 58.60 58.08 55.83 0.50 3.27 1.02 62.85 63.00 YES	cts hours feet feet feet feet feet feet ft ft	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilt $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test pilt $D_{FC to UD}$ = Depth to UD from the bottom of the filter course $D_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice 50 peak elevation $\leq$ Elevation of the top of the practice	≤ 72-hrs it) ≥ 1' ≥ 1' ≥ 1' ≥ 1'
0.11 5.44 59.10 58.60 58.08 55.83 0.50 3.27 1.02 62.85 63.00 YES If a surface	cts hours feet feet feet feet feet feet ft ft sand filter	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = 2WQV/ $Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilter E $R_{OCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test pilter to UD from the bottom of the filter course $D_{FC to UD}$ = Depth to UD from the bottom of the filter course $D_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice 50 peak elevation $\leq$ Elevation of the top of the practice or underground sand filter is proposed:	≤ 72-hrs t) pit) ≥ 1' ≥ 1' ≥ 1' ≥ 1'
0.11 5.44 59.10 58.60 58.08 55.83 0.50 3.27 1.02 62.85 63.00 YES If a surface YES	cts hours feet feet feet feet feet feet ft ft sand filter ac	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = 2WQV/ $Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilter EROCK = Elevation of bedrock (if none found, enter the lowest elevation of the test pilter to UD from the bottom of the filter course $D_{FC to UD}$ = Depth to UD from the bottom of the filter course $D_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice 50 peak elevation < Elevation of the top of the practice or underground sand filter is proposed: Drainage Area check.	<pre>≤ 72-hrs t) pit) ≥ 1' ≥ 1' ≥ 1' </pre> ← yes  < 10 ac
0.11 5.44 59.10 58.60 58.08 55.83 0.50 3.27 1.02 62.85 63.00 YES If a surface YES	cts hours feet feet feet feet feet feet ft ft sand filter ac cf	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = 2WQV/ $Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilter to UD form the bottom of the filter course $D_{FC to UD}$ = Depth to UD from the bottom of the filter course $D_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $P_{eak}$ elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice 50 peak elevation $\leq$ Elevation of the top of the practice or underground sand filter is proposed: P = Volume of storage <sup>3</sup> (attach a stage-storage table)	<pre> &lt; 72-hrs  t) pit)  ≥ 1'  ≥ 1'  ≥ 1'  </pre>
0.11 5.44 59.10 58.60 58.08 55.83 0.50 3.27 1.02 62.85 63.00 YES If a surface YES	cts hours feet feet feet feet feet feet ft ft sand filter ac cf inches	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilter course elevation of bedrock (if none found, enter the lowest elevation of the test pilter to UD from the bottom of the filter course $D_{FC to UD}$ = Depth to UD from the bottom of the filter course $D_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice 50 peak elevation < Elevation of the top of the practice or underground sand filter is proposed: Drainage Area check. V = Volume of storage <sup>3</sup> (attach a stage-storage table) $D_{FC}$ = Filter course thickness	<pre>≤ 72-hrs it) pit) ≥ 1' ≥ 1' ≥ 1' </pre> ← yes <pre>&lt; 10 ac </pre> <pre>&gt; 75%WQV 18", or 24" if within GPA</pre>
0.11 5.44 59.10 58.60 58.08 55.83 0.50 3.27 1.02 62.85 63.00 YES If a surface YES Sheet	cts hours feet feet feet feet feet feet ft ft sand filter ac cf inches	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test pilt $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test pilt $D_{FC to UD}$ = Depth to UD from the bottom of the filter course $D_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course Peak elevation of the 50-year storm event (infiltration can be used in analysis) Elevation of the top of the practice 50 peak elevation $\leq$ Elevation of the top of the practice or underground sand filter is proposed: Drainage Area check. V = Volume of storage <sup>3</sup> (attach a stage-storage table) $D_{FC}$ = Filter course thickness Note what sheet in the plan set contains the filter course specification.	<pre>≤ 72-hrs t) pit) ≥ 1' ≥ 1' ≥ 1' ≥ 1' </pre> (10 ac) 275%WQV 18", or 24" if within GPA

If a biorete	ntion a	rea i	is proposed:	
YES	ас		Drainage Area no larger than 5 ac?	← yes
4,806	cf		V = Volume of storage <sup>3</sup> (attach a stage-storage table)	<u>&gt;</u> WQV
18.0	inches		D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA
Sheet		D4	Note what sheet in the plan set contains the filter course specification	
3.0	:1		Pond side slopes	<u>&gt; 3</u> :1
Sheet		D4	Note what sheet in the plan set contains the planting plans and surface cover	
If porous p	avemei	nt is	proposed:	
			Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acres		A <sub>SA</sub> = Surface area of the pervious pavement	
	:1		Ratio of the contributing area to the pervious surface area	≤ 5:1
	inches		D <sub>FC</sub> = Filter course thickness	12", or 18" if within GPA
	-			mod. 304.1 (see
Sheet			Note what sheet in the plan set contains the filter course spec.	spec)

1. Rate of the limiting layer (either the filter course or the underlying soil). Ksat<sub>design</sub> includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.

2. See lines 34, 40 and 48 for required depths of filter media.

3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

#### Designer's Notes:

SHWT elevation at high contour is only 0.01' below the bottom of the stone. However, we modelled it 2" lower in the HydroCAD calculations as a factor of safety. Modelling such a small separation from the bottom of the stone to the SHWT causes an unrealistically high amount of exfiltration to appear in the results.

NHDES Alteration of Terrain

Last Revised: January 2019

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### Stage-Area-Storage for Pond 1P: Bioretention Pond

Elevation	Surface	Storage	Elevation	Surface	Storage	
<u> </u>	(54-11)			(34-11)	(Cubic-leet)	
58.09	400	0	60.09	733	300	
59 10	400	9 10	60.74	1 100	390	
59.19	400	19	60.79	1,100	440 501	
50.24	400	20	60.04	1,312	501	End cap in $x = 58.0$
00.29 50.24	400	37	00.09	1,342	07Z	End cap inv. = $56.9$
58.34	400	47	60.94	1,791	000	vol. below = 149 cl lor GRV
58.39	466	56	60.99	2,058	/51	calculation
58.44	466	65	61.04	2,135	857	
58.49	466	75	61.09	2,162	965	WQV Required = 1,076 cf
58.54	466	84	61.14	2,188	1,073	WQV EI. = 61.15
58.59	466	93	61.19	WQV EI. 2,215	1,183	
58.64	466	103	61.24	2,242	1,295	Overflow el. $= 62.65$
58.69	466	112	61.29	2,269	1,408	Vol. below = $4,992$ cf
58.74	466	121	61.34	2,296	1,522	
58.79	466	130	61.39	2,324	1,637	Bottom of filter course el. =
58.84	466	140	61.44	2,351	1,754	59 1
<mark>58.89</mark>	466	149	61.49	2,379	1,872	
58.94	End cap 466	158	61.54	2,407	1,992	4002 - 186 - 4.806  cf
58.99	invert 466	168	61.59	2,435	2,113	4992-100 = 4,000 Cl
59.04	466	177	61.64	2,464	2,236	MOV Dravidad 4 000 of
<b>59.09</b>	466	186	61.69	2,492	2,360	VQV Provided = 4,806 cf
59.14	466	190	61.74	2,521	2,485	<u>&gt;&gt; 1,076 cf</u>
59.19	466	193	61.79	2,549	2,612	
59.24	466	197	61.84	2,578	2,740	
59.29	466	200	61.89	2,607	2,869	
59.34	466	204	61.94	2.637	3.001	
59.39	466	207	61.99	2,666	3,133	
59 44	466	211	62.04	2 695	3 267	
59 49	466	214	62.09	2 725	3 403	
59 54	466	218	62.00	2,720	3 540	
59 59	466	210	62.14	2,704	3 678	
59.64	400	225	62.10	2,707	3 818	
50.60	400	223	62.24	2,013	3 050	
59.09	400	220	62.23	2,043	3,959	
50.74	400	232	62.34	2,073	4,102	
59.79	400	200	62.39	2,904	4,247	
59.04	400	239	02.44	2,934	4,393	
59.89	400	242	62.49	2,904	4,540	
59.94	400	240	02.54	2,995	4,089	
59.99	466	249	62.59	3,026	4,840	
60.04	466	253	62.64	3,057	4,992	
60.09	466	256	62.69	Overflow 3,088	5,145	
60.14	466	260	62.74	3,120	5,301	
60.19	466	263	62.79	3,151	5,457	
60.24	466	267	62.84	3,183	5,616	
60.29	466	270	62.89	3,214	5,776	
60.34	466	274	62.94	3,246	5,937	
60.39	466	277	62.99	3,279	6,100	
60.44	466	281				
60.49	466	284				
60.54	466	288				
60.59	466	291				
60.64	577	317				

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Prepared by Jones & Beach Engineers Inc HydroCAD® 10.20-3c s/n 00762 © 2023 HydroCAD Software Solutions LLC

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### Stage-Discharge for Pond 1P: Bioretention Pond

Elevation	Discharge	Discarded	Primary	Elevation	Discharge	Discarded	Primary	
(feet)	(cfs)	(cfs)	(cfs)	(feet)	(cfs)	(cfs)	(cfs)	
58.09	0.00	0.00	0.00	60.69	0.09	0.05	0.03	
58.14	0.00	0.00	0.00	60.74	0.09	0.06	0.04	
58.19	0.01	0.01	0.00	60.79	0.09	0.06	0.04	
58.24	0.01	0.01	0.00	60.84	0.10	0.06	0.04	
58.29	0.01	0.01	0.00	60.89	0.10	0.06	0.04	
58.34	0.01	0.01	0.00	60.94	0.10	0.07	0.04	
58.39	0.01	0.01	0.00	60.99	0.11	0.07	0.04	
58.44	0.01	0.01	0.00	61.04	0.11	0.07	0.04	
58.49	0.01	0.01	0.00	61.09	0.11	0.07	0.04	
58.54	0.01	0.01	0.00	<mark>61.14</mark>	0.11	0.07	0.04	WQV EI. = 61.15
58.59	0.01	0.01	0.00	61.19	0.12	0.08	0.04	Q(WQV) = 0.11  cfs
58.64	0.01	0.01	0.00	61.24	0.12	0.08	0.04	
58.69	0.01	0.01	0.00	61.29	0.12	0.08	0.04	
58.74	0.02	0.02	0.00	61.34	0.12	0.08	0.04	
58.79	0.02	0.02	0.00	61.39	0.12	0.08	0.04	
58.84	0.02	0.02	0.00	61.44	0.12	0.08	0.04	
58.89	0.02	0.02	0.00	61.49	0.13	0.08	0.04	
58.94	0.02	0.02	0.00	61.54	0.13	0.09	0.04	
58.99	0.03	0.02	0.01	61.59	0.13	0.09	0.04	
59.04	0.03	0.02	0.01	61.64	0.13	0.09	0.04	
59.09	0.03	0.02	0.01	61.69	0.13	0.09	0.04	
59.14	0.03	0.02	0.01	61.74	0.13	0.09	0.04	
59.19	0.04	0.02	0.01	61.79	0.14	0.09	0.04	
59.24	0.04	0.03	0.01	61.84	0.14	0.09	0.04	
59.29	0.04	0.03	0.02	61.89	0.14	0.09	0.05	
59.34	0.04	0.03	0.02	61.94	0.14	0.10	0.05	
59.39	0.05	0.03	0.02	61.99	0.14	0.10	0.05	
59.44	0.05	0.03	0.02	62.04	0.15	0.10	0.05	
59.49	0.05	0.03	0.02	62.09	0.15	0.10	0.05	
59.54	0.05	0.03	0.02	62.14	0.15	0.10	0.05	
59.59	0.05	0.03	0.02	62.19	0.15	0.10	0.05	
59.64	0.05	0.03	0.02	62.24	0.15	0.10	0.05	
59.69	0.06	0.03	0.02	62.29	0.15	0.11	0.05	
59.74	0.06	0.03	0.02	62.34	0.16	0.11	0.05	
59.79	0.06	0.04	0.02	62.39	0.16	0.11	0.05	
59.84	0.06	0.04	0.02	62.44	0.16	0.11	0.05	
59.89	0.06	0.04	0.03	62.49	0.16	0.11	0.05	
59.94	0.06	0.04	0.03	62.54	0.16	0.11	0.05	
59.99	0.07	0.04	0.03	62.59	0.16	0.11	0.05	
60.04	0.07	0.04	0.03	62.64	0.17	0.12	0.05	
60.09	0.07	0.04	0.03	62.69	0.27	0.12	0.15	
60.14	0.07	0.04	0.03	62.74	0.52	0.12	0.40	
60.19	0.07	0.04	0.03	62.79	0.84	0.12	0.72	
60.24	0.07	0.04	0.03	62.84	1.24	0.12	1.12	
60.29	0.08	0.05	0.03	62.89	1.69	0.12	1.56	
60.34	0.08	0.05	0.03	62.94	2.18	0.13	2.06	
60.39	0.08	0.05	0.03	62.99	2.73	0.13	2.60	
60.44	0.08	0.05	0.03					
60.49	0.08	0.05	0.03					
60.54	0.08	0.05	0.03					
60.59	0.08	0.05	0.03					
60.64	0.09	0.05	0.03					



## GROUNDWATER RECHARGE VOLULME (GRV) CALCULATION (Env-Wq 1507.04)

	ас	Area of HSG A soil that was replaced by impervious cover	0.40"
0.12	ac	Area of HSG B soil that was replaced by impervious cover	0.25"
	ac	Area of HSG C soil that was replaced by impervious cover	0.10"
	ac	Area of HSG D soil or impervious cover that was replaced by impervious cover	0.0"
0.25	inches	Rd = Weighted groundwater recharge depth	
0.031	ac-in	GRV = AI * Rd	
113	cf	GRV conversion (ac-in x 43,560 sf/ac x 1ft/12")	

#### Provide calculations below showing that the project meets the groundwater recharge requirements (Env-Wq 1507.04):

 Stone Drip Edges, 40% Stone Voids:

 ((3 ft \* 60 ft \* 3.5 ft)+(3 ft \* 60 ft \* 4.5 ft)+)\*0.4 = 576 cf

 Eco Paver, 40% Voids: (13 ft \* 17 ft \* 1 ft)\*0.4 = 88 cf

 Stone Beneath Deck: (14 ft \* 20 ft \*1.5 ft)\*0.4 = 168 cf

 Bioretention: 149 cf GRV provided below UD end cap orifice per stage storage table

 GRV Provided = 576+88+168+149 = 981 cf >> 113 cf

## APPENDIX IX

### **Pollutant Removal Calculations**

# POLLUTANT REMOVAL CALCULATIONS

BMP	Drip Edge	Bioretention	None	Total	Required
Acres Impervious	0.032	0.293	0.036	0.361	
TSS Removal (%)	90%	90%	0%	81%	80%
TN Removal (%)	55%	65%	0%	68%	50%

Calculations are based on post-construction impervious surfaces on the subject parcel.

TSS removal of 86% provided exceeds 80% requirement

TN removal of 65% provided exceeds 50% requirement

Pollutant R	Values Accepted for Loading Analyses					
ВМР Туре	ВМР	Notes	Lit. Ref.	TSS	TN	ТР
	Wet Pond		B, F	70%	35%	45%
Chammunatan	Wet Extended Detention Pond		А, В	80%	55%	68%
Ponds	Micropool Extended Detention Pond	TBA				
	Multiple Pond System	TBA				
	Pocket Pond	TBA				
	Shallow Wetland		A, B, F, I	80%	55%	45%
Stormwater	Extended Detention Wetland		A, B, F, I	80%	55%	45%
Wetlands	Pond/Wetland System	TBA				
	Gravel Wetland		Н	95%	85%	64%
	Infiltration Trench (≥75 ft from surface water)		B, D, I	90%	55%	60%
	Infiltration Trench (<75 ft from surface water)		B, D, I	90%	10%	60%
Infiltration Practices	Infiltration Basin (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%
	Infiltration Basin (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%
	Dry Wells			90%	55%	60%
	Drip Edges			90%	55%	60%
	Aboveground or Underground Sand Filter that infiltrates WQV (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%
	Aboveground or Underground Sand Filter that infiltrates WQV (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%
	Aboveground or Underground Sand Filter with underdrain		A, I, F, G, H	85%	10%	45%
Filtering	Tree Box Filter	TBA				
Practices	Bioretention System		I, G, H	90%	65%	65%
	Permeable Pavement that infiltrates WQV (≥75 ft from surface water)		A, F, B, D, I	90%	60%	65%
	Permeable Pavement that infiltrates WQV (<75 ft from surface water)		A, F, B, D, I	90%	10%	65%
	Permeable Pavement with underdrain		Use TN and TP values for sand filter w/ underdrain and outlet pipe	90%	10%	45%

Pollutant R	Values Accepted for Loading Analyses					
ВМР Туре	ВМР	Notes	Lit. Ref.	TSS	TN	ТР
Treatment Swales	Flow Through Treatment Swale	TBA				
Vegetated Buffers	Vegetated Buffers		A, B, I	73%	40%	45%
	Sediment Forebay	TBA				
	Vegetated Filter Strip		A, B, I	73%	40%	45%
	Vegetated Swale		A, B, C, F, H, I	65%	20%	25%
Pre-	Flow-Through Device - Hydrodynamic Separator		A, B, G, H	35%	10%	5%
Treatment Practices	Flow-Through Device - ADS Underground Multichamber Water Quality Unit (WQU)		G, H	72%	10%	9%
	Other Flow-Through Devices	TBA				
	Off-line Deep Sump Catch Basin		J, K, L, M	15%	5%	5%

# APPENDIX X

Stormwater Operations and Maintenance Manual



85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

# STORMWATER MANAGEMENT OPERATIONS AND MAINTENANCE MANUAL

Luster Cluster 635 Sagamore Ave. Portsmouth, NH 03801 Tax Map 222, Lot 19

**Prepared for:** 

635 Sagamore Development LLC 3612 Lafayette Rd., Dept 4 Portsmouth, NH 03801

> Prepared by: Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885 (603) 772-4746 March 18, 2024 Revised April 15, 2024 JBE Project No. 18134.1

## **Inspection and Maintenance of Facilities and Property**

### A. Maintenance of Common Facilities or Property

1. The Condominium Association, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Association, future owners and assigns shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form and shall submit an Operations and Maintenance report on a yearly basis to the Portsmouth Planning Department by December 31<sup>st</sup>.

#### **B.** General Inspection and Maintenance Requirements

- 1. Permanent stormwater and sediment and erosion control facilities to be maintained on the site include, but are not limited to, the following:
  - a. Roadway and driveways
  - b. Vegetation and landscaping
  - c. Bioretention systems
  - d. Catch Basins & Yard Drains
  - e. Permeable Paver Patio
  - f. Stone Drip Edges
  - g. Culverts
  - h. Rip-Rap Outlet Protection Aprons
  - i. Swale
- 2. Maintenance of permanent measures shall follow the following schedule:
  - a. Normal winter roadway maintenance including plowing and snow removal. Road sweeping at the end of every winter, preferably before the start of the spring rain season.
  - b. **Annual inspection** of the site for erosion, destabilization, settling, and sloughing. Any needed repairs are to be conducted immediately. **Annual inspection** of site's vegetation and landscaping. Any areas that are bare shall be reseeded and mulched with hay or, if the case is extreme, loamed and seeded or sodded to ensure adequate vegetative cover. Landscape specimens shall be replaced in kind, if they are found to be dead or dying.
  - c. Bioretention Systems:
    - Visually inspect monthly and repair erosion. Use small stones to stabilize erosion along drainage paths.
    - Check the pH once a year if grass is not surviving. Apply an alkaline product, such as limestone, if needed.
    - Re-seed any bare areas by hand as needed.



- Immediately after the completion of cell construction, water grass for 14 consecutive days unless there is sufficient natural rainfall.
- Once a month (more frequently in the summer), the land owner or Association shall visually inspect vegetation for disease or pest problems and treat as required.
- During times of extended drought, look for physical features of stress. Water in the early morning as needed.
- Weed regularly, if needed.
- After rainstorms, inspect the cell and make sure that drainage paths are clear and that ponding water dissipates over 4-6 hours. (Water may pond for longer times during the winter and early spring.)
- Twice annually, inspect the outlet control structures to ensure that they are not clogged and correct any clogging found as needed.
- Any debris and sediment accumulations shall be removed from the outlet structures, overflow risers, and emergency spillways and disposed of properly.
- Inspect outlet structure for deterioration and or clogging.
- If erosion is evident on the berm or emergency spillway, stabilize the affected area by seeding. Trees must not be allowed to grow in these areas.
- KEEP IN MIND, THE BIORETENTION CELL IS NOT A POND. IT SHALL NOT PROVIDE A BREEDING GROUND FOR MOSQUITOES. MOSQUITOES NEED AT LEAST FOUR (4) DAYS OF STANDING WATER TO DEVELOP AS LARVA.
- d. **Annual inspection** of catch basins and yard drains to determine if they need to be cleaned. Catch basins and yard drains are to be cleaned if the depth of deposits is greater than one-half the depth from the basin bottom to the invert of the lowest pipe or opening into or out of the basin. If a catch basin or yard drain significantly exceeds the one-half depth standard during the inspection, then it shall be cleaned more frequently. If woody debris or trash accumulates in the catch basin or yard drain, then it shall be cleaned on a weekly basis. The catch basin or yard drain can be cleaned either manually or by specially designed equipment including, but not limited to, bucket loaders and vacuum pumps. Before any materials can be disposed, it is necessary to perform a detailed chemical analysis to determine if the materials meet the EPA criteria for hazardous waste. This will help determine how the materials shall be stored, treated, and disposed. Grease hoods are to be wiped clean and the rags disposed of properly. Debris obscuring the grate inlet shall also be removed.
- e. Permeable Paver Patio:

Units 4 features a permeable paver patio for stormwater management while Units 1-3 feature standard paver patios. The following course of action will help assure that the pavers are maintained to preserve its hydrologic effectiveness for their special purpose.

#### Winter maintenance:



- Sanding for winter traction is prohibited. Deicing is permitted (NaCl, MgCl<sub>2</sub>, or equivalent). Reduced salt application is possible and can be a cost savings for winter maintenance. Nontoxic, organic deicers, applied either as blended, magnesium chloride-based liquid products or as pretreated salt, are preferable.
- Plow after each storm. Special plow blades may be used to prevent scarring. Do not raise blade of plow. Ice and light snow accumulation are generally not as problematic as for standard asphalt. Snow will accumulate during heavier storms and should be plowed after 2 to 4 inches of snow accumulate. Alternatively, snow may be blown or shoveled off of paver surface

#### **Routine maintenance:**

- Seal coating is absolutely forbidden. Surface seal coating is not reversible.
- The paver surface shall be vacuumed 2 or 3 times per year, and at any additional times sediment is spilled, eroded, or tracked onto the surface.
- Planted areas adjacent to permeable pavers shall be well maintained to prevent soil washout onto the pavers. If any bare spots or eroded areas are observed within the planted areas, they shall be replanted and/or stabilized at once.
- Immediately clean any soil deposited on pavers. Superficial dirt does not necessarily clog the paver voids. However, dirt that is ground in repeatedly by tires can lead to clogging. Therefore, trucks or other heavy vehicles shall be prevented from tracking or spilling dirt onto the pavers.
- Do not allow construction staging, soil/mulch storage, etc. on unprotected paver surface. Contractor to lay down tarps, plywood or removable item and take care not to track material onto unprotected pavers.
- Repairs: Potholes or other surface blemishes shall be replaced in kind. Any required repair of drainage structures shall be done promptly to ensure continued proper functioning of the system.
- Written and verbal communication to the future owner shall make clear the pavers' special purpose and special maintenance requirements such as those listed here.
- f. Stone Drip Edges:

In the spring and fall, visually inspect the area around the edges and repair any erosion. Use small stones to stabilize erosion along drainage paths. Inspect stone area to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation shall not be allowed to become established in stone areas, and/or any debris removed from the void spaces between the stones.

g. **Inspection** of culvert inlets and outlets at least **once per month** during the rainy season (March to November). Any debris is to be removed and disposed of properly.



- h. Rock riprap shall be **inspected annually** in order to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation must not be allowed to become established in riprap areas, and/or any debris removed from the void spaces between the rocks. If the riprap is adjacent to a stream or other waterbody, the water shall be kept clear of obstructions, debris, and sediment deposits
- i. Swales Inspect swales annually for erosion, sediment accumulation, vegetation loss, and presence of invasive species. Perform periodic mowing; frequency depends on location and type of grass. Remove debris and accumulated sediment, based on inspection. Repair eroded areas, remove invasive species and dead vegetation, and reseed as warranted by inspection

See attached sample forms as a guideline.

Any inquiries in regards to the design, function, and/or maintenance of any one of the abovementioned facilities or tasks shall be directed to the project engineer:

Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885

T#: (603) 772-4746 F#: (603) 772-0227



### **Commitment to maintenance requirements**

I agree to complete and/or observe all of the required maintenance practices and their respective schedules as outlined above.

Signature

Print Name

Title

Date



#### **Annual Operations and Maintenance Report**

The Condominium Association, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Association, future owners and assigns shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form and shall submit an Operations and Maintenance report on a yearly basis to the Portsmouth Planning Department by December 31<sup>st</sup>.

Construction Activity	Date of Inspection	Who Inspected	Findings of Inspector
Roadway and Driveways			
Vegetation and Landscaping			
Bioretention #1			
Bioretention #2			
Catch Basins & Yard Drains			



Permeable Paver Patios		
(Unit 4)		
(Oline I)		
Stone Drin Edge		
Stone Drip Edge		
Culverte		
Culverts		
Rip Rap Outlet Protection		
Tup tup contribution		
Swalas		
Swales		
Other (plaga note):		
Other (please note):		
1		



### Regular Inspection and Maintenance Guidance for Bioretention Systems / Tree Filters

Maintenance of bioretention systems and tree filters can typically be performed as part of standard landscaping. Regular inspection and maintenance is critical to the effective operation of bioretention systems and tree filters to insure they remain clear of leaves and debris and free draining. This page provides guidance on maintenance activities that are typically required for these systems, along with the suggested frequency for each activity. Individual systems may have more, or less, frequent maintenance needs, depending on a variety of factors including the occurrence of large storm events, overly wet or dry (I.E., drought), regional hydrologic conditions, and the upstream land use.

### ACTIVITIES

The most common maintenance activity is the removal of leaves from the system and bypass structure. Visual inspections are routine for system maintenance. This includes looking for standing water, accumulated leaves, holes in the soil media, signs of plant distress, and debris and sediment accumulation in the system. Mulch and/or vegetation coverage is integral to the performance of the system, including infiltration rate and nutrient uptake. Vegetation care is important to system productivity and health.

ACTIVITY	FREQUENCY		
A record should be kept of the time to drain for the system completely after a storm event. The system should drain completely within 72 hours.	After every major storm in the first few months, then biannually.		
Check to insure the filter surface remains well draining after storm event. <b>Remedy</b> : If filter bed is clogged, draining poorly, or standing water covers more than 15% of the surface 48 hours after a precipitation event, then remove top few inches of discolored material. Till or rake remaining material as needed			
Check inlets and outlets for leaves and debris			
<b>Remedy</b> : Rake in and around the system to clear it of debris. Also, clear the inlet and overflow if obstructed.			
Check for animal burrows and short circuiting in the system <b>Remedy</b> : Soil erosion from short circuiting or animal boroughs should be repaired when they occur. The holes should be filled and lightly compacted.	Quarterly initially, biannually, frequency adjusted as needed after 3 inspections		
Check to insure the filter bed does not contain more than 2 inches accumulated material			
been removed, replace media with either mulch or a (50% sand, 20% woodchips, 20% compost, 10% soil) mixture.			
During extended periods without rainfall, inspect plants for signs of distress.			
<b>Remedy</b> : Plants should be watered until established (typical only for first few months) or as needed thereafter.			
Inspect inlets and outlets to ensure good condition and no evidence of deterioration. Check to see if high-flow bypass is functioning. <b>Remedy</b> : Repair or replace any damaged structural parts, inlets, outlets, sidewalls.	Annually		
Check for robust vegetation coverage throughout the system. <b>Remedy</b> : If at least 50% vegetation coverage is not established after 2 years, reinforcement planting should be performed.			
Check for dead or dying plants, and general long term plant health. <b>Remedy</b> : This vegetation should be cut and removed from the system. If woody vegetation is present, care should be taken to remove dead or decaying plant Material. Separation of Herbaceous vegetation rootstock should occur when overcrowding is observed.	As needed		

1/15/2011, University of New Hampshire Stormwater Center



CHECKLIST FOR INSPECTION OF BIORETENTION SYSTEM / TREE FILTERS						
Location:		Inspect	or:			
Date: Time:	ate: Time: Site					
Date Since Last Rain Event:						
Inspection Items	Satisfac Unsatisf	tory (S) or actory (U)	Comments/Corrective Action			
1. Initial Inspection After Planting and Mulching						
Plants are stable, roots not exposed	S	U				
Surface is at design level, typically 4" below overpass	S	U				
Overflow bypass / inlet ( if available) is functional	S	U				
2. Debris Cleanup (2 times a year minimum, Spring & Fall)						
Litter, leaves, and dead vegetation removed from the system	S	U				
Prune perennial vegetation	S	U				
3. Standing Water (1 time a year, After large storm events)						
No evidence of standing water after 72 hours	S	U	1			
4. Short Circuiting & Erosion (1 time a year, After large storm	events)					
No evidence of animal burrows or other holes	S	U				
No evidence of erosion	S	U	1			
5. Drought Conditions (As needed)						
Water plants as needed	s	U				
Dead or dying plants						
6. Overflow Bypass / Inlet Inspection (1 time a year, After large	storm ev	ents)				
No evidence of blockage or accumulated leaves	S	U				
Good condition, no need for repair	S	U				
7. Vegetation Coverage (once a year)						
50% coverage established throughout system by first year	S	U				
Robust coverage by year 2 or later	S	U				
8. Mulch Depth (if applicable)(once every 2 years)						
Mulch at original design depth after tilling or replacement	s	U				
9. Vegetation Health (once every 3 years)						
Dead or decaying plants removed from the system	s	U				
10. Tree Pruning (once every 3 years)						
Prune dead, diseased, or crossing branches	S	U				
Corrective Action Needed			Due Date			
1.						
2.						
3.						

1/15/2011, University of New Hampshire Stormwater Center



## APPENDIX XI

Pre- and Post-Construction Watershed Plans




GENERAL	LEGEND
EXISTING	PROPOSED
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**DESCRIPTION** PROPERTY LINES SETBACK LINES CENTERLINE TREE LINE STONEWALL BARBED WIRE FENCE SOIL BOUNDARY EASEMENT MAJOR CONTOUR MINOR CONTOUR EDGE OF PAVEMENT VERTICAL GRANITE CURB SLOPE GRANITE CURB FIBER BERM DRAINAGE LINE SEWER LINE SEWER FORCE MAIN GAS LINE WATER LINE WATER SERVICE OVERHEAD ELECTRIC UNDERGROUND ELECTRIC UNDERDRAIN THRUST BLOCK IRON PIPE/IRON ROD DRILL HOLE IRON ROD/DRILL HOLE STONE/GRANITE BOUND SPOT GRADE PAVEMENT SPOT GRADE CURB SPOT GRADE BENCHMARK (TBM) DOUBLE POST SIGN SINGLE POST SIGN WELL TEST PIT TREES AND BUSHES UTILITY POLE DRAIN MANHOLE SEWER MANHOLE HYDRANT WATER GATE VALVE WATER SHUT OFF REDUCER SINGLE GRATE CATCH BASIN TRANSFORMER CULVERT W/FLARED END SECTION CULVERT W/STRAIGHT HEADWALL STONE CHECK DAM DRAINAGE FLOW DIRECTION RIPRAP PAVEMENT HATCH STABILIZED CONSTRUCTION ENTRANCE CONCRETE GRAVEL

# SNOW STORAGE

# RETAINING WALL

# "LUSTER CLUSTER" TAX MAP 222, LOT 19

# SINGLE FAMILY CONDOMINIUM 635 SAGAMORE AVE., PORTSMOUTH, NH

# 85 PORTSMOUTH AVENUE PO BOX 219 STRATHAM, NH 03885 (603) 772-4746 CONTACT: JOSEPH CORONATI

# **TRAFFIC ENGINEER**

P.O. BOX 1721 CONCORD, NH 03302 (603) 731-8500 CONTACT: STEPHEN PERNAW

# SOILS CONSULTANT

8 CONTINENTAL DRIVE, BLDG 2, UNIT H EXETER, NH 03833-7507 (603) 418-7260 CONTACT: JAMES GOVE EMAIL: JGOVE@GESINC.BIZ

Design: DJM Draft: KDR Date: 2/26/2024 Checked: JAC Scale: AS NOTED Project No.: 18134.1 Drawing Name: 18134.1-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN

PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



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0	3/18/24	ISSUED FOR REVIEW
REV.	DATE	REVISION
REV.	DATE	REVISION



**CIVIL ENGINEER / SURVEYOR** JONES & BEACH ENGINEERS, INC.

EMAIL: JCORONATI@JONESANDBEACH.COM

STEPHEN G. PERNAW & COMPANY, INC.

GOVE ENVIRONMENTAL SERVICES, INC.

# LANDSCAPE DESIGNER LM LAND DESIGN, LLC 11 SOUTH ROAD BRENTWOOD, NH 03833

(603) 770-7728 CONTACT: LISE MCNAUGHTON

WATER CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS WATER DIVISION 680 PEVERLY HILL ROAD PORTSMOUTH, NH 03801 (603) 427-1530

SEWER CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS SEWER DIVISION 680 PEVERLY HILL ROAD PORTSMOUTH, NH 03801 (603) 766-1421

LIGHTING DESIGN **EXPOSURE LIGHTING 501 ISLINGTON STREET, UNIT 1A** PORTSMOUTH, NH 03801 CONTACT: KEN SWEENEY

# **ELECTRIC**

**EVERSOURCE** 1700 LAFAYETTE ROAD PORTSMOUTH, NH 03801 (800) 662-7764

**TELEPHONE** 

CONSOLIDATED COMMUNICATIONS 1575 GREENLAND ROAD GREENLAND, NH 03840 (800) 427-5525

CABLE TV

COMCAST COMMUNICATION CORPORATION 334-B CALEF HIGHWAY EPPING, NH 03042-2325 (603) 679-5695

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11		Des	signed and Pro	duced in NH		
_/B_	Jones	&	Beach	ı Engi	neers,	Inc.
85 Portsmouth Av	e. Civil	Eng	ineering	Services	603	3-772-4746
Stratham, NH 038	85			E-MAIL: JBE@	JONESANDBE	ACH.COM

Plan Name:

Project:



Know what's **below** 811 before you dig

# SHEET INDEX

CS	COVER SHEET
C1	EXISTING CONDITIONS PLAN
DM1	DEMOLITION PLAN
C2	SITE PLAN
CS1	CONDOMINIUM SITE PLAN
C3	GRADING AND DRAINAGE PLAN
C4	UTILITY PLAN
L1	LIGHTING PLAN
L2	LANDSCAPE PLAN
P1	DRIVEWAY PLAN AND PROFILE
P2	SEWER PLAN AND PROFILE
H1	HIGHWAY ACCESS PLAN
T1-T2	TRUCK TURNING PLAN
D1-D5	DETAIL SHEET
E1	EROSION AND SEDIMENT CONTROL DETAILS
	ARCHITECTURAL PLANS





SONAL ENGIN 04/19/2024

REVISION





# **DEMOLITION NOTES:**

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- THIS PLAN IS INTENDED TO PROVIDE MINIMUM GUIDELINES FOR SITE DEMOLITION. IT SHOULD BE NOTED THAT ALL MANMADE FEATURES, PAVEMENT, SIGNS, POLES, CURBING, CONCRETE WALKS, UTILITIES, ETC., SHALL BE REMOVED AS NECESSARY TO CONSTRUCT WORK, UNLESS OTHERWISE NOTED TO REMAIN. THROUGHOUT THE CONSTRUCTION PROCESS, THE CONTRACTOR SHALL INFORM THE ENGINEER IMMEDIATELY OF ANY FIELD DISCREPANCIES FROM DATA AS SHOWN ON DESIGN PLANS. THIS INCLUDES ANY UNFORESEEN CONDITIONS, SUBSURFACE OR OTHERWISE FOR EVALUATION AND RECOMMENDATIONS. ANY CONTRADICTION BETWEEN ITEMS OF THIS PLAN/PLAN SET, OR BETWEEN THE PLANS AND ON-SITE CONDITIONS MUST BE RESOLVED BEFORE RELATED CONSTRUCTION HAS BEEN INITIATED.
- PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR IS REQUIRED TO HAVE THE PROJECT LAND SURVEYOR STAKE OR FLAG CLEARING LIMITS. A MINIMUM OF 48 HOURS NOTICE IS REQUIRED. 2.
- 3. ALL EXISTING STRUCTURES WITHIN THE CONSTRUCTION AREA, UNLESS OTHERWISE NOTED TO REMAIN, SHALL BE REMOVED AND DISPOSED OF OFF-SITE IN ACCORDANCE WITH ALL LOCAL, STATE AND FEDERAL GUIDELINES. ANY BURNING ON-SITE SHALL BE SUBJECT TO LOCAL ORDINANCES.
- 4. THE CONTRACTOR SHALL REMOVE AND PROPERLY DISPOSE OF ALL CONTAMINATED MATERIAL LOCATED IN THE AREA OF EXISTING LEACHFIELDS IN ACCORDANCE WITH LOCAL AND STATE REGULATIONS.
- 5. ALL CURBING, CONCRETE, PAVEMENT, BUILDINGS AND SUBBASE MATERIALS LOCATED WITHIN PROPOSED LANDSCAPED AREAS SHALL BE REMOVED AND REPLACED WITH LOAM MATERIALS SUITABLE FOR LANDSCAPING IN ACCORDANCE WITH TECHNICAL SPECIFICATIONS. (SEE ALSO LANDSCAPE PLAN).
- 6. THE CONTRACTOR SHALL OBTAIN TREE CLEARING PERMIT FROM LOCAL AND STATE AUTHORITIES PRIOR TO START OF CONSTRUCTION (IF REQUIRED).
- IN AREAS WHERE CONSTRUCTION IS PROPOSED ADJACENT TO ABUTTING PROPERTIES, THE CONTRACTOR 7. SHALL INSTALL ORANGE CONSTRUCTION FENCING ALONG PROPERTY LINES IN ALL AREAS WHERE SILT FENCING IS NOT REQUIRED.
- EROSION AND SEDIMENTATION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO CONSTRUCTION AND ANY EARTH MOVING OPERATIONS. FIBER BERM SHALL BE INSTALLED AT THE LIMITS OF IMPACT AREAS 8. ACCORDING TO THE DETAILS SHOWN ON SHEET E1.
- EXCAVATED MATERIALS WILL BE PLACED WITHIN UPLAND AREAS AS FILL MATERIAL OR HAULED 9 OFF-SITE FOR DISPOSAL IN AN APPROPRIATE UPLAND LOCATION.

GRAPHIC SCALE 0 10 20 40 80 ( IN FEET ) 1 inch = 20 ft.	PROJECT PARCEL CITY OF PORTSMOUTH TAX MAP 222, LOT 19 <u>TOTAL LOT AREA</u> 84,795 SQ. FT.
	1.95 ACRES
DEMOLITION PLAN	DRAWING No.

635 SAGAMORE AVE., PORTSMOUTH, NH 635 SAGAMORE DEVELOPMENT LLC Owner of Record:3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158







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04/19/2024

PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR SHALL COORDINATE WITH THE ENGINEER, ARCHITECT AND/OR OWNER, IN ORDER TO OBTAIN AND/OR PAY ALL THE NECESSARY LOCAL PERMITS, CONNECTION FEES AND BONDS.

2. THE CONTRACTOR SHALL PROVIDE A MINIMUM NOTICE OF FOURTEEN (14) DAYS TO ALL CORPORATIONS, COMPANIES AND/OR LOCAL AUTHORITIES OWNING OR HAVING A JURISDICTION OVER UTILITIES RUNNING TO, THROUGH OR ACROSS PROJECT AREAS PRIOR TO DEMOLITION AND/OR

3. THE LOCATION, SIZE, DEPTH AND SPECIFICATIONS FOR CONSTRUCTION OF PROPOSED PRIVATE UTILITY SERVICES SHALL BE TO THE STANDARDS AND REQUIREMENTS OF THE RESPECTIVE UTILITY COMPANY (ELECTRIC, TELEPHONE, CABLE TELEVISION, WATER, AND SEWER).

4. A PRECONSTRUCTION MEETING SHALL BE HELD WITH THE OWNER, ENGINEER, ARCHITECT, CONTRACTOR, LOCAL OFFICIALS, AND ALL PROJECT-RELATED UTILITY COMPANIES (PUBLIC AND PRIVATE) PRIOR TO START OF CONSTRUCTION.

5. ALL CONSTRUCTION SHALL CONFORM TO THE CITY STANDARDS AND REGULATIONS, AND NHDES STANDARDS AND SPECIFICATIONS, WHICHEVER ARE MORE STRINGENT, UNLESS OTHERWISE SPECIFIED.

6. ALL CONSTRUCTION ACTIVITIES SHALL CONFORM TO LABOR OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA) RULES AND REGULATIONS 7. BUILDINGS TO BE SERVICED BY UNDERGROUND UTILITIES UNLESS OTHERWISE NOTED.

8. AS-BUILT PLANS SHALL BE SUBMITTED TO DEPARTMENT OF PUBLIC WORKS.

9. INVERTS AND SHELVES: MANHOLES SHALL HAVE A BRICK PAVED SHELF AND INVERT, CONSTRUCTED TO CONFORM TO THE SIZE OF PIPE AND FLOW AT CHANGES IN DIRECTION. THE INVERTS SHALL BE LAID OUT IN CURVES OF THE LONGEST RADIUS POSSIBLE TANGENT TO THE CENTER LIN OF THE SEWER PIPES. SHELVES SHALL BE CONSTRUCTED TO THE ELEVATION OF THE THROUGH CHANNEL UNDERLAYMENT OF INVERT, AND SHELF SHALL CONSIST OF BRICK MASONRY.

10. FRAMES AND COVERS: MANHOLE FRAMES AND COVERS SHALL BE OF HEAVY DUTY DESIGN AND PROVIDE A 30 INCH DIA, CLEAR OPENING. THE WORD "SEWER" SHALL BE CAST INTO THE CENTER OF THE UPPER FACE OF EACH COVER WITH RAISED, 3" LETTERS.

11. SHALLOW MANHOLE: IN LIEU OF A CONE SECTION, WHEN MANHOLE DEPTH IS LESS THAN 6 FEET, A REINFORCED CONCRETE SLAB COVER MAY BE USED HAVING AN ECCENTRIC ENTRANCE OPENING AND CAPABLE OF SUPPORTING H20 LOADS. (THIS APPLIES TO SMH 1)

12. CONTRACTOR SHALL PLACE 2" WIDE METAL WIRE IMPREGNATED RED PLASTIC WARNING TAPE OVER ENTIRE LENGTH OF ALL GRAVITY SEWERS,

SANITARY SEWER FLOW CALCULATIONS: 4 - FOUR BEDROOM UNITS. ASSUME 5 PEOPLE IN 4-BEDROOM UNITS. PER METCALF & EDDY TABLE 3-2: 61 GPD/PERSON IN 5 PERSON HOUSE

(61 GPD \* 5 PEOPLE \* 4) = 1,220 GPD. SEE SHEET 2 FOR BEDROOM NUMBER DESIGNATION.

14. ALL SANITARY STRUCTURE INTERIOR DIAMETERS (4' MIN) SHALL BE DETERMINED BY THE MANUFACTURER BASED ON THE PIPE CONFIGURATIONS

15. PROPOSED RIM ELEVATIONS OF DRAINAGE AND SANITARY MANHOLES ARE APPROXIMATE. FINAL ELEVATIONS ARE TO BE SET FLUSH WITH FINISH GRADES. ADJUST ALL OTHER RIM ELEVATIONS OF MANHOLES, WATER GATES, AND OTHER UTILITIES TO FINISH GRADE AS SHOWN ON THE GRADING

16. ALL WATER MAINS AND SERVICE PIPES SHALL HAVE A MINIMUM 12" VERTICAL AND 24" HORIZONTAL SEPARATION TO MANHOLES, OR CONTRACTOR SHALL INSTALL BOARD INSULATION FOR FREEZING PROTECTION.

17. WATER MAINS SHALL BE HYDROSTATICALLY PRESSURE TESTED FOR LEAKAGE PRIOR TO ACCEPTANCE. WATERMAINS SHALL BE TESTED AT 1.5 TIMES THE WORKING PRESSURE OR 150 PSI, WHICH EVER IS GREATER. TESTING SHALL BE CONDUCTED IN ACCORDANCE WITH SECTION 4 OF AWWA STANDARD C 600. WATERMAINS SHALL BE DISINFECTED AFTER THE ACCEPTANCE OF THE PRESSURE AND LEAKAGE TESTS ACCORDING TO

18. ALL WATER AND SANITARY LEADS TO BUILDING(S) SHALL END 5' OUTSIDE THE BUILDING LIMITS AS SHOWN ON PLANS AND SHALL BE PROVIDED WITH A TEMPORARY PLUG AND WITNESS AT END.

19. THRUST BLOCKS SHALL BE PROVIDED AT ALL BENDS, TEES, MECHANICAL JOINTS AND FIRE HYDRANTS.

20. DIMENSIONS ARE SHOWN TO CENTERLINE OF PIPE OR FITTING.

21. CONTRACTOR TO FURNISH SHOP DRAWINGS FOR UTILITY RELATED ITEMS TO ENSURE CONFORMANCE WITH THE PLANS AND SPECIFICATIONS. SHOP DRAWINGS SHOULD BE SENT IN TRIPLICATE TO THE DESIGN ENGINEER FOR REVIEW AND APPROVAL PRIOR TO INSTALLATION.

22. EXISTING UTILITIES SHALL BE DIGSAFED BEFORE CONSTRUCTION.

23. ALL WATER LINES SHALL HAVE TESTABLE BACKFLOW PREVENTERS AT THE ENTRANCE TO EACH BUILDING.

24. ALL GRAVITY SEWER PIPE, MANHOLES, AND FORCE MAINS SHALL BE TESTED ACCORDING TO NHDES STANDARDS OF DESIGN AND CONSTRUCTION FOR SEWAGE AND WASTEWATER TREATMENT FACILITIES, CHAPTER ENV-WQ 700. ADOPTED ON 10-15-14.

25. ENV-WQ 704.06 GRAVITY SEWER PIPE TESTING: GRAVITY SEWERS SHALL BE TESTED FOR WATER TIGHTNESS BY USE OF LOW-PRESSURE AIR TESTS CONFORMING WITH ASTM F1417-92(2005) OR UNI-BELL PVC PIPE ASSOCIATION UNI-B-6. LINES SHALL BE CLEANED AND VISUALLY INSPECTED AND TRUE TO LINE AND GRADE. DEFLECTION TESTS SHALL TAKE PLACE AFTER 30 DAYS FOLLOWING INSTALLATION AND THE MAXIMUM ALLOWABLE DEFLECTION OF FLEXIBLE SEWER PIPE SHALL BE 5% OF AVERAGE INSIDE DIAMETER. A RIGID BALL OR MANDREL WITH A DIAMETER OF AT LEAST 95% OF THE AVERAGE INSIDE PIPE DIAMETER SHALL BE USED FOR TESTING PIPE DEFLECTION. THE DEFLECTION TEST SHALL BE CONDUCTED WITHOUT MECHANICAL PULLING DEVICES.

26. ENV-WQ 704.17 SEWER MANHOLE TESTING: SHALL BE TESTED FOR LEAKAGE USING A VACUUM TEST PRIOR TO BACKFILLING AND PLACEMENT OF SHELVES AND INVERTS.

27. SANITARY SEWER LINES SHALL BE LOCATED AT LEAST TEN (10) FEET HORIZONTALLY FROM AN EXISTING OR PROPOSED WATER LINE. WHEN A SEWER LINE CROSSES UNDER A WATER LINE, THE SEWER PIPE JOINTS SHALL BE LOCATED AT LEAST 6 FEET HORIZONTALLY FROM THE WATERMAIN. THE SEWER LINE SHALL ALSO MAINTAIN A VERTICAL SEPARATION OF NOT LESS THAN 18 INCHES.

28. SEWERS SHALL BE BURIED TO A MINIMUM DEPTH OF 6 FEET BELOW GRADE IN ALL ROADWAY LOCATIONS, AND TO A MINIMUM DEPTH OF 4 FEET BELOW GRADE IN ALL CROSS-COUNTRY LOCATIONS. PROVIDE TWO-INCHES OF R-10 FOAM BOARD INSULATION 2-FOOT WIDE TO BE INSTALLED 6-INCHES OVER SEWER PIPE IN AREAS WHERE DEPTH IS NOT ACHIEVED. A WAIVER FROM THE DEPARTMENT OF ENVIRONMENTAL SERVICES WASTEWATER ENGINEERING BUREAU IS REQUIRED PRIOR TO INSTALLING SEWER AT LESS THAN MINIMUM COVER.

29. THE CONTRACTOR SHALL MINIMIZE THE DISRUPTIONS TO THE EXISTING SEWER FLOWS AND THOSE INTERRUPTIONS SHALL BE LIMITED TO FOUR (4) HOURS OR LESS AS DESIGNATED BY THE CITY SEWER DEPARTMENT.

30. LIGHTING CONDUIT SHALL BE SCHEDULE 40 PVC, AND SHALL BE INSTALLED IN CONFORMANCE WITH THE NATIONAL ELECTRIC CODE. CONTRACTOR SHALL PROVIDE EXCAVATION AND BACKFILL.

31. ALL TRENCHING, PIPE LAYING, AND BACKFILLING SHALL BE IN ACCORDANCE WITH FEDERAL OSHA REGULATIONS.

32. DISINFECTION OF WATER MAINS SHALL BE CARRIED OUT IN STRICT ACCORDANCE WITH AWWA STANDARD C651, LATEST EDITION. THE BASIC PROCEDURE TO BE FOLLOWED FOR DISINFECTING WATER MAINS IS AS FOLLOWS:

PREVENT CONTAMINATING MATERIALS FROM ENTERING THE WATER MAIN DURING STORAGE, CONSTRUCTION, OR REPAIR.

REMOVE, BY FLUSHING OR OTHER MEANS, THOSE MATERIALS THAT MAY HAVE ENTERED THE WATER MAINS. CHLORINATE ANY RESIDUAL CONTAMINATION THAT MAY REMAIN, AND FLUSH THE CHLORINATED WATER FROM THE MAIN.

PROTECT THE EXISTING DISTRIBUTION SYSTEM FROM BACKFLOW DUE TO HYDROSTATIC PRESSURE TEST AND DISINFECTION PROCEDURES. DETERMINE THE BACTERIOLOGICAL QUALITY BY LABORATORY TEST AFTER DISINFECTION. MAKE FINAL CONNECTION OF THE APPROVED NEW WATER MAIN TO THE ACTIVE DISTRIBUTION SYSTEM

33. DOMESTIC SHUTOFFS & VALVES SHALL BE PAINTED BLUE. FIRE SERVICE SHUTOFFS & VALVES SHALL BE PAINTED RED. COORDINATE WITH CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS FOR EXACT COLORS.

34. SEWER TRENCH DAMS SHALL BE INSTALLED EVERY 75' ALONG GRAVITY SEWER PIPE.

35. IF IRRIGATION IS TO BE USED, THE PIPING SYSTEM SHALL BE REVIEWED AND APPROVED BY THE PORTSMOUTH CITY PLANNER, CITY ENGINEER, AND THE WATER DEPARTMENT PRIOR TO INSTALLATION.

36. WATER LINE TO BE CONSTRUCTED PER CITY OF PORTSMOUTH SPECIFICATIONS.

37. AN AS-BUILT PLAN OF THE WATER LINE IS TO BE PREPARED AND SUBMITTED TO THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS.



TOTAL LOT AREA 84,795 SQ. FT. 1.95 ACRES



DRAWING No.



635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158





THE CONTRACTOR SHALL SUPPLY ALL PLANT MATERIALS IN QUANTITIES SUFFICIENT TO COMPLETE THE PLANTINGS SHOWN ON THE

ALL MATERIAL SHALL CONFORM TO THE GUIDELINES ESTABLISHED BY THE CURRENT AMERICAN STANDARD FOR NURSERY STOCK

4. PLANTS SHALL BE SUBJECT TO INSPECTION AND APPROVAL AT THE PLACE OF GROWTH, UPON DELIVERY OR AT THE JOB SITE

PLANTS FURNISHED IN CONTAINERS SHALL HAVE THE ROOTS WELL ESTABLISHED IN THE SOIL MASS AND SHALL HAVE AT LEAST ONE (1) GROWING SEASON. ROOT-BOUND PLANTS OR INADEQUATELY SIZED CONTAINERS TO SUPPORT THE PLANT MAY BE

8. ALL PLANTS SHALL BE WATERED THOROUGHLY TWICE DURING THE FIRST 24-HOUR PERIOD AFTER PLANTING. ALL PLANTS SHALL

9. ALL LANDSCAPE AREAS TO BE GRASS COMMON TO REGION, EXCEPT FOR INTERIOR LANDSCAPED ISLANDS OR WHERE OTHER

11. THE CONTRACTOR SHALL REMOVE WEEDS, ROCKS, CONSTRUCTION ITEMS, ETC. FROM ANY LANDSCAPE AREA SO DESIGNATED TO REMAIN, WHETHER ON OR OFF-SITE. GRASS SEED OR PINE BARK MULCH SHALL BE APPLIED AS DEPICTED ON PLANS.

12. EXISTING TREES TO REMAIN SHALL BE PROTECTED WITH TEMPORARY SNOW FENCING AT THE DRIPLINE OF THE TREE. THE CONTRACTOR SHALL NOT STORE VEHICLES OR MATERIALS WITHIN THE LANDSCAPED AREAS. ANY DAMAGE TO EXISTING TREES, SHRUBS OR LAWN SHALL BE REPAIRED BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.

13. ALL MULCH AREAS SHALL RECEIVE A 3" LAYER OF SHREDDED PINE BARK MULCH OVER A 10 MIL WEED MAT EQUAL TO

14. ALL LANDSCAPED AREAS SHALL HAVE SELECT MATERIALS REMOVED TO A DEPTH OF AT LEAST 9" BELOW FINISH GRADE. THE RESULTING VOID IS TO BE FILLED WITH A MINIMUM OF 9" HIGH-QUALITY SCREENED LOAM AMENDED WITH 3" OF AGED ORGANIC

15. THIS PLAN IS INTENDED FOR LANDSCAPING PURPOSES ONLY. REFER TO CIVIL/SITE DRAWINGS FOR OTHER SITE CONSTRUCTION

16. IRRIGATION PIPING SYSTEM SHALL BE REVIEWED AND APPROVED BY OWNER AND ENGINEER PRIOR TO INSTALLATION.

17. WITH AUTHORIZATION OF THE PROJECT ENGINEER, PROPOSED TREES ALONG EDGE OF WOODED BUFFER SHALL BE PLACED WHEREVER NECESSARY IN ORDER TO COVER GAPS IN EXISTING WOODED BUFFER IN ORDER TO BLOCK VISIBILITY FROM TIDEWATCH

19. ALL PLANTING SHALL ADHERE TO THE GENERAL REQUIREMENTS OUTLINED IN SECTION 6.3 AND THE PLANTING REQUIREMENTS

20. ALL PLANTING SHALL FOLLOW THE ANSI A300 PART 6 STANDARD PRACTICES FOR PLANTING AND TRANSPLANTING (AS AMENDED).

Botanical Name	Common Name	Size
Calamagrostis x acutiflora 'Karl Foerster'	KARL FOERSTER REED GRASS **	2 Gallon
Chamaecyparis pisifera 'Mop'	MOP GOLD THREAD CYPRESS **	5 Gallon
llex glabra 'Shamrock'	SHAMROCK INKBERRY HOLLY **	5 Gallon
Liquidambar styraciflua	AMERICAN SWEETGUM **	3" Caliper
Malus x 'Robinson'	ROBINSON FLOWERING CRABAPPLE **	2" Caliper
Picea abies	NORWAY SPRUCE	8-9 Ft. Ht.
Pinus strobus	EASTERN WHITE PINE	8-9 Ft. Ht.
Pyrus calleryana 'Chanticleer'	CHANTICLEER CALLERY PEAR **	2.5" Caliper
Sedum spectabile 'Brilliant'	BRILLIANT SEDUM **	1 Gallon
Spiraea japonica 'Goldflame'	GOLDFLAME SPIREA **	5 Gallon
Syringa reticulata 'Ivory Silk'	IVORY SILK TREE LILAC	2" Caliper
Thuja plicata 'Green Giant'	GREEN GIANT ARBORVITAE **	7-8 Ft. Ht.
Tilia cordata 'Greenspire'	GREENSPIRE LITTLELEAF LINDEN **	3" Caliper
Tsuga canadensis	CANADIAN HEMLOCK	8-9 Ft. Ht.
Weigela florida 'Alexandra'	WINE & ROSES WEIGELA	5 Gallon
Denotes plants that are tolerant of urban conditions including road salt, soil compaction, drought, heat, and air pollution.		

**PROJECT PARCEL** CITY OF PORTSMOUTH TAX MAP 222, LOT 19

TOTAL LOT AREA 84,795 SQ. FT. 1.95 ACRES

DRAWING No.

SHEET 9 OF 20

JBE PROJECT NO. 18134.1



ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE T THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

SS IONAL with AMITIM MANA 04/19/2024

1	4/19/24	REVISED PER TAC COMMENT
0	3/18/24	ISSUED FOR REVIEW
REV.	DATE	REVISION

ΒY

FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

THIS SITE WILL REQUIRE A USEPA NPDES PERMIT FOR STORMWATER DISCHARGE FOR THE CONSTRUCTION SITE. THE CONSTRUCTION SITE OPERATOR SHALL DEVELOP AND IMPLEMENT A CONSTRUCTION STORM WATER POLLUTION PREVENTION PLAN (SWPPP), WHICH SHALL REMAIN ON SITE AND BE MADE ACCESSIBLE TO THE PUBLIC. THE CONSTRUCTION SITE OPERATOR SHALL SUBMIT A NOTICE OF INTENT (NOI) TO THE EPA REGIONAL OFFICE SEVEN DAYS PRIOR TO COMMENCEMENT OF ANY WORK ON SITE. EPA WILL POST THE NOI AT HTTP: //CFPUB1.EPA.GOV/NPDES/STORMWATER/NOI/NOISEARCH.CFM. AUTHORIZATION IS GRANTED UNDER THE PERMIT ONCE THE NOI IS SHOWN IN "ACTIVE" STATUS ON THIS WEBSITE. A COMPLETED NOTICE OF TERMINATION SHALL BE SUBMITTED TO THE NPDES PERMITTING AUTHORITY WITHIN 30 DAYS AFTER EITHER OF THE FOLLOWING CONDITIONS HAVE BEEN MET: A. FINAL STABILIZATION HAS BEEN ACHIEVED ON ALL PORTIONS OF THE SITE FOR WHICH THE PERMITTEE IS RESPONSIBLE;

ANOTHER OPERATOR/PERMITTEE HAS ASSUMED CONTROL OVER ALL AREAS OF THE SITE THAT HAVE NOT BEEN FINALLY STABILIZED. PROVIDE DPW WITH A COPY OF THE NOTICE OF TERMINATION (NOT).

2. ALL ROAD AND DRAINAGE WORK SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE STANDARD SPECIFICATIONS FOR THE CITY, AND NHDOT SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION, WHICHEVER IS MORE STRINGENT.

3. AS-BUILT PLANS TO BE SUBMITTED TO THE CITY PRIOR TO ACCEPTANCE OF THE ROADWAY.

CONTRACTOR TO COORDINATE AND COMPLETE ALL WORK REQUIRED FOR THE RELOCATION AND/OR INSTALLATION OF ELECTRIC, CATV, TELEPHONE, PER UTILITY DESIGN AND STANDARDS. LOCATIONS SHOWN ARE APPROXIMATE. LOW PROFILE STRUCTURES SHALL BE USED TO THE GREATEST EXTENT POSSIBLE.

5. THIS PLAN HAS BEEN PREPARED BY JONES & BEACH ENGINEERS, INC. FOR MUNICIPAL AND STATE APPROVALS AND FOR CONSTRUCTION BASED ON DATA OBTAINED FROM ON-SITE FIELD SURVEY AND EXISTING MUNICIPAL RECORDS. THROUGHOUT THE CONSTRUCTION PROCESS, THE CONTRACTOR SHALL INFORM THE ENGINEER IMMEDIATELY OF ANY FIELD DISCREPANCY FROM DATA SHOWN ON THE DESIGN PLANS. THIS INCLUDES ANY UNFORESEEN CONDITIONS, SUBSURFACE OR OTHERWISE, FOR EVALUATION AND RECOMMENDATIONS. ANY CONTRADICTION BETWEEN ITEMS OF THIS PLAN/PLAN SET, OR BETWEEN THE PLANS AND ON-SITE CONDITIONS MUST BE RESOLVED BEFORE RELATED CONSTRUCTION HAS BEEN INITIATED.

6. SILTATION AND EROSION CONTROLS SHALL BE INSTALLED PRIOR TO CONSTRUCTION, SHALL BE MAINTAINED DURING CONSTRUCTION, AND SHALL REMAIN UNTIL SITE HAS BEEN STABILIZED WITH PERMANENT VEGETATION. SEE DETAIL SHEET E1 FOR ADDITIONAL

7. ALL DISTURBED AREAS NOT STABILIZED BY OCTOBER 15TH SHALL BE COVERED WITH AN EROSION CONTROL BLANKET. PRODUCT TO

FINAL DRAINAGE, GRADING AND EROSION PROTECTION MEASURES SHALL CONFORM TO REGULATIONS OF THE PUBLIC WORKS

9. CONTRACTOR TO VERIFY EXISTING UTILITIES AND TO NOTIFY ENGINEER OF ANY DISCREPANCY IMMEDIATELY.

10. DRAINAGE INSPECTION AND MAINTENANCE SCHEDULE: SILT FENCING WILL BE INSPECTED DURING AND AFTER STORM EVENTS TO ENSURE THAT THE FENCE STILL HAS INTEGRITY AND IS NOT ALLOWING SEDIMENT TO PASS. SEDIMENT BUILD UP IN SWALES WILL BE REMOVED IF IT IS DEEPER THAN SIX INCHES, AND IS TO BE REMOVED FROM SUMPS BELOW THE INLET OF CULVERTS SEMIANNUALLY, AS WELL AS FROM CATCH BASINS. FOLLOWING MAJOR STORM EVENTS, THE STAGE DISCHARGE OUTLET STRUCTURES ARE TO BE INSPECTED AND ANY DEBRIS REMOVED FROM THE ORIFICE, TRASH TRACK AND EMERGENCY SPILL WAY. INFREQUENTLY, SEDIMENT MAY ALSO HAVE TO BE REMOVED FROM THE SUMP OF THE STRUCTURE.

11. ALL DRAINAGE INFRASTRUCTURE SHALL BE INSTALLED AND STABILIZED PRIOR TO DIRECTING ANY RUNOFF TO IT.

12. BIORETENTION PONDS REQUIRE TIMELY MAINTENANCE AND SHOULD BE INSPECTED AFTER EVERY MAJOR STORM EVENT, AS WELL AS FREQUENTLY DURING THE FIRST YEAR OF OPERATION, AND ANNUALLY THEREAFTER. EVERY FIVE YEARS, THE SERVICES OF A PROFESSIONAL ENGINEER SHOULD BE RETAINED TO PERFORM A THOROUGH INSPECTION OF THE BIORETENTION POND AND ITS INFRASTRUCTURE. ANY DEBRIS AND SEDIMENT ACCUMULATIONS SHOULD BE REMOVED FROM THE OUTLET STRUCTURE(S) AND EMERGENCY SPILLWAY(S) AND DISPOSED OF PROPERLY. BIORETENTION POND BERMS SHOULD BE MOWED AT LEAST ONCE ANNUALLY SO AS TO PREVENT THE ESTABLISHMENT OF WOODY VEGETATION. TREES SHOULD NEVER BE ALLOWED TO GROW ON A BIORETENTION POND BERM, AS THEY MAY DESTABILIZE THE STRUCTURE AND INCREASE THE POTENTIAL FOR FAILURE. AREAS SHOWING SIGNS OF EROSION OR THIN OR DYING VEGETATION SHOULD BE REPAIRED IMMEDIATELY BY WHATEVER MEANS NECESSARY, WITH THE EXCEPTION OF FERTILIZER. RODENT BORROWS SHOULD BE REPAIRED IMMEDIATELY AND THE ANIMALS SHOULD BE TRAPPED

13. IN THOSE AREAS WHERE THE BERMS OF THE BIORETENTION SYSTEMS MUST BE CONSTRUCTED BY THE PLACEMENT OF FILL, THE ENTIRE EMBANKMENT AREA OF THE BIORETENTION PONDS SHALL BE EXCAVATED TO PROPOSED GRADE, STRIPPED OF ALL ORGANIC MATERIALS. COMPACTED TO AT LEAST 95% AND SCARIFIED PRIOR TO THE PLACEMENT OF THE EMBANKMENT MATERIAL. IN THE EVENT THE FOUNDATION MATERIAL EXPOSED DOES NOT ALLOW THE SPECIFIED COMPACTION, AN ADDITIONAL ONE FOOT (1') OF EXCAVATION AND THE PLACEMENT OF A ONE FOOT (1') THICK, TWELVE FOOT (12') WIDE PAD OF THE MATERIAL DESCRIBED IN THE NOTE BELOW, COMPACTED TO 95% OF ASTM D-1557 MAY BE NECESSARY. PLACEMENT AND COMPACTION SHOULD OCCUR AT A MOISTURE CONTENT OF OPTIMUM PLUS OR MINUS 3%, AND NO FROZEN OR ORGANIC MATERIAL SHOULD BE PLACED WITHIN FOR ANY

14. EMBANKMENT IS TO HAVE 3:1 SIDE SLOPES (MAX.) AND IS TO BE BROUGHT TO SPECIFIED GRADES PRIOR TO THE ADDITION OF LOAM (4" MINIMUM) SO AS TO ALLOW FOR THE COMPACTION OF THE STRUCTURE OVER TIME WHILE MAINTAINING THE PROPER BERM

15. COMPACTION TESTING SERVICES (I.E. NUCLEAR DENSITY TESTS) ARE TO BE PERFORMED BY AN INDEPENDENT GEOTECHNICAL ENGINEER RETAINED BY THE CONTRACTOR FOR ROADWAY CONSTRUCTION, AND ON THE FOUNDATION OF THE BERM AND ON EVERY

# DRIVEWAY PLAN AND PROFILE

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH

635 SAGAMORE DEVELOPMENT LLC Owner of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158 DRAWING No.





Stratham, NH 03885

AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

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1. PROPOSED GRADES SHOWN HEREON ARE APPROXIMATE. REFER TO SHEETS C3 AND P1 FOR GRADING OF SITE AND DRIVEWAY. SET RIM ELEVATIONS OF SEWER STRUCTURES FLUSH WITH PROPOSED GRADE. 2. STATIONS REFER TO CENTERLINE OF SEWER STRUCTURE OR CROSSING DRAINAGE/WATER PIPE.

3. CONTRACTOR TO CONFIRM ACTUAL EXISTING INVERT OF STUB IN THE FIELD AND NOTIFY ENGINEER IF IT IS MORE THAN 0.1' DIFFERENT FROM THE STATED INVERT.

# SEWER PLAN AND PROFILE

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH

635 SAGAMORE DEVELOPMENT LLC Owner of Record: 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

DRAWING No. **P2** 

SHEET 11 OF 20 JBE PROJECT NO. 18134.1



ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

3/18/24 ISSUED FOR REVIEW 0 REV. DATE REVISION

			Designed and Pro	duced in NH			Plan Name:
		nes	& Beach	ı Engin	eers. Inc.		
DJM					603-772-4746		Project:
KDR	PO Box 219	เาบน	Engineering	Services	FAX: 603-772-0227		Owner of Record:



635 SAGAMORE DEVELOPMENT LLC 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

H<sup>1</sup> SHEET 12 OF 20 JBE PROJECT NO. 18134.1



Owner of Record:	3612





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Portsmouth Ave.	Civil	Enc
Box 219	00000	
tham NIL 02885		

04/19/2024





04/19/2024

REV.



		Designed and Produced in NH Plan Name:
		D Ionog & Boach Engineers Inc
		Jones & Deach Engineers, Inc.
NTS	DJM	
	KDR	85 Portsmouth Ave. Civil Engineering Services
	BY	Stratham, NH 03885 E-MAIL: JBE@JONESANDBEACH.COM Owner of Record: 3







# NOTES:

1. PE THREADED ROD WITH WING NUTS PROVIDED FOR END SECTIONS 12"-24". 30" AND 36" END SECTIONS TO BE WELDED PER MANUFACTURER'S RECOMMENDATIONS.

2. ALL DIMENSIONS ARE NOMINAL.

# ADS N-12 FLARED END SECTION

NOT TO SCALE



SHRUB PLANTING

# NOT TO SCALE

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10" 6.5" 10" 6.5" 15" 6.5" 18" 6.5" N/A 7.0" 7.0" N/A

1. BASE SECTION SHALL BE MONOLITHIC WITH 48" INSIDE DIAMETER.

2. ALL SECTIONS SHALL BE DESIGNED FOR H20 LOADING.

3. CONCRETE SHALL BE COMPRESSIVE STRENGTH 4000 PSI, TYPE II CEMENT.

GREASE HOOD

TO EXTEND 1'

1" CLR.

BELOW BOTTOM

OF OUTLET PIPE \

-FLEXIBLE BOOT

CAST-IN-PLACE OR

VERTICAL FOOT PLACED

ACCORDING TO AASHTO

DESIGNATION M199

-MIN .12 SQ. IN. STEEL PER

FIELD INSTALLED

CONFORMING ASTM 7 SPEC. C-443

6" OF 3/4" CRUSHED STONE

TO 95% OF ASTM -1557

(NHDOT ITEM 304.3)

COMPACTED

- 4. FRAMES AND GRATES SHALL BE HEAVY DUTY AND DESIGNED FOR H20 LOADING
- 5. PROVIDE "V" KNOCKOUTS FOR PIPES WITH 2" MAX. CLEARANCE TO OUTSIDE OF PIPE. MORTAR ALL PIPE CONNECTIONS SO AS TO BE WATERTIGHT.
- 6. JOINT SEALANT BETWEEN PRECAST SECTIONS SHALL BE BUTYL RUBBER.
- 7. STANDARD CATCH BASIN FRAME AND GRATE(S) SHALL BE SET IN FULL MORTAR BED. ADJUST TO GRADE WITH CLAY BRICK AND MORTAR (2 BRICK COURSES TYPICALLY, 5 BRICK COURSES MAXIMUM, BUT NO MORE THAN 12"), OR PRECAST CONCRETE 'DONUTS'.
- 8. CATCH BASINS SHALL HAVE A 48" SUMP AS SHOWN.

# CATCH BASIN

A 2, 2, 4

05

Ш °

COMPACTED SUBGRADE -

NOTES:

# NOT TO SCALE





# STONE DRIP EDGE DETAIL

NOT TO SCALE



- 1. ALL DIMENSIONS GIVEN IN FEET & INCHES.
- PROVIDE BELL END AT INLET HEADWALL, AND SPIGOT END AT OUTLET END HEADWALL. . CONCRETE: 5,000 PSI MINIMUM AFTER 28 DAYS. CEMENT TO BE TYPE III PER ASTM
- C-150. REINFORCING TO MEET OR EXCEED ASTM A-615 GRADE 60 DEFORMED BARS. 4. 1" THREADED INSERTS PROVED FOR FINAL ATTACHMENT IN FIELD BY OTHERS.

PRECAST CONCRETE HEADWALL

NOT TO SCALE

# DETAIL SHEET

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH 635 SAGAMORE DEVELOPMENT LLC

DRAWING No. **D**5

SHEET 19 OF 20 JBE PROJECT NO. 18134.1

Owner of Record 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158

# TEMPORARY EROSION CONTROL NOTES

- THE SMALLEST PRACTICAL AREA OF LAND SHALL BE EXPOSED AT ANY ONE TIME. AT NO TIME SHALL AN AREA IN EXCESS OF 5 ACRES BE EXPOSED AT ANY ONE TIME BEFORE DISTURBED AREAS ARE STABILIZED.
- EROSION, SEDIMENT AND DETENTION MEASURES SHALL BE INSTALLED AS SHOWN ON THE PLANS AND AT LOCATIONS AS REQUIRED, DIRECTED BY THE ENGINEER.
- 3. ALL DISTURBED AREAS (INCLUDING POND AREAS BELOW THE PROPOSED WATERLINE) SHALL BE RETURNED TO PROPOSED GRADES AND ELEVATIONS. DISTURBED AREAS SHALL BE LOAMED WITH A MINIMUM OF 6" OF SCREENED ORGANIC LOAM AND SEEDED WITH SEED MIXTURE 'C' AT A RATE NOT LESS THAN 1.10 POUNDS OF SEED PER 1,000 S.F. OF AREA (48 LBS. / ACRE).
- SILT FENCES AND OTHER BARRIERS SHALL BE INSPECTED EVERY SEVEN CALENDAR DAYS AND WITHIN 24 HOURS OF A RAINFALL OF 0.5" OR GREATER. ALL DAMAGED AREAS SHALL BE REPAIRED, AND SEDIMENT DEPOSITS SHALL PERIODICALLY BE REMOVED AND DISPOSED OF
- AFTER ALL DISTURBED AREAS HAVE BEEN STABILIZED. THE TEMPORARY EROSION CONTROL MEASURES SHALL BE REMOVED AND THE AREA DISTURBED BY THE REMOVAL SMOOTHED AND RE-VEGETATED.
- AREAS MUST BE SEEDED AND MULCHED OR OTHERWISE PERMANENTLY STABILIZED WITHIN 3 DAYS OF FINAL GRADING, OR TEMPORARILY STABILIZED WITHIN 14 DAYS OF THE INITIAL DISTURBANCE OF SOIL. ALL AREAS SHALL BE STABILIZED WITHIN 45 DAYS OF INITIAL DISTURBANCE.
- ALL PROPOSED VEGETATED AREAS THAT DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED BY SEEDING AND INSTALLING NORTH AMERICAN GREEN S75 EROSION CONTROL BLANKETS (OR AN EQUIVALENT APPROVED IN WRITING BY THE ENGINEER) ON SLOPES GREATER THAN 3:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT EVENTS.
- ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15. OR WHICH 8. ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS.
- 9. AFTER OCTOBER 15th, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3" OF CRUSHED GRAVEL PER NHDOT ITEM 304.3.
- 10. AN AREA SHALL BE CONSIDERED STABLE IF ONE OF THE FOLLOWING HAS OCCURRED:
  - a. BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED;
  - b. A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED;
  - c. A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH STONE OR RIPRAP HAS BEEN INSTALLED; OR
  - d. EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.
- 11. FUGITIVE DUST CONTROL IS REQUIRED TO BE CONTROLLED IN ACCORDANCE WITH ENV-A 1000, AND THE PROJECT IS TO MEET THE REQUIREMENTS AND INTENT OF RSA 430:53 AND AGR 3800 RELATIVE TO INVASIVE SPECIES.





- NOTES: 1. STONE FOR STABILIZED CONSTRUCTION ENTRANCE SHALL BE 3 INCH STONE, RECLAIMED STONE, OR RECYCLED CONCRETE EQUIVALENT. 2. THE LENGTH OF THE STABILIZED ENTRANCE SHALL NOT BE LESS THAN 50 FEET, 75' WITHOUT A MOUNTABLE BERM, AND EXCEPT FOR A SINGLE RESIDENTIAL LOT WHERE A 30 FOOT MINIMUM LENGTH WOULD APPLY. 3. THICKNESS OF THE STONE FOR THE STABILIZED ENTRANCE SHALL NOT BE LESS THAN 6
- THE PIPE

# STABILIZED CONSTRUCTION ENTRANCE

NOT TO SCALE



2.5' (MIN)

NOTES:

- 1. ORGANIC FILTER BERMS SHALL BE UTILIZED IN LIEU OF SILT FENCE.
- 2. THE EROSION CONTROL MIX USED IN THE FILTER BERMS SHALL BE A WELL-GRADED MIXTURE OF PARTICLE SIZES, MAY CONTAIN ROCKS LESS THAN 4" IN DIAMETER, STUMP GRINDINGS, SHREDDED OR COMPOSTED BARK, OR ACCEPTABEL MANUFACTURED PRODUCTS, AND SHALL BE FREE OF REFUSE, PHYSICAL CONTAMINANTS, AND MATERIAL TOXIC TO PLANT GROWTH, AND SHALL MEET THE FOLLOWING STANDARDS:
- a) THE ORGANIC CONTENT SHALL BE 25-65% OF DRY WEIGHT. b) PARTICLE SIZE BY WEIGHT SHALL BE 100% PASSING A 3" SCREEN, 90-100% PASSING A 1" SCREEN, 70-100& PASSING A 0.75" SCREEN, AND 30-75% PASSING A 0.25" SCREEN.
- c) THE ORGANIC PORTION SHALL BE FIBROUS AND ELONGATED. d) LARGE PORTIONS OF SILTS, CLAYS, OR FINE SANDS SHALL NOT BE INCLUDED IN THE
- MIXTURE.
- e) SOLUBLE SALTS CONTENT SHALL BE >4.0mmhos/cm. f) THE pH SHALL BE BETWEEN 5.0 AND 8.0.
- 3. ORGANIC FILTER BERMS SHALL BE INSTALLED ALONG A RELATIVELY LEVEL CONTOUR. IT MAY BE NECESSARY TO CUT TALL GRASSES OR WOODY VEGETATION TO AVOID CREATING VOIDS AND BRIDGES THAT WOULD ENABLE FINES TO WASH UNDER THE BERM.
- 4. ON SLOPES LESS THAN 5%, OR AT THE BOTTOM OF SLOPES STEEPER THAN 3:1, UP TO 20' LONG, THE BERM SHALL BE A MINIMUM OF 12" HIGH (AS MEASURED ON THE UPHILL SIDE), AND A MINIMUM OF 36" WIDE. ON LONGER OR STEEPER SLOPES, THE BERM SHALL BE WIDER TO ACCOMMODATE THE POTENTIAL ADDITIONAL RUNOFF.
- 5. FROZEN GROUND, OUTCROPS OF BEDROCK, AND VERY ROOTED FORESTED AREAS PRESENT THE MOST PRACTICAL AND EFFECTIVE LOCATIONS FOR ORGANIC FILTER BERMS. OTHER BMP'S SHOULD BE USED AT LOW POINTS OF CONCENTRATED RUNOFF, BELOW CULVERT OUTLET APRONS, AROUND CATCH BASINS, AND AT THE BOTTOM OF STEEP PERIMETER SLOPES THAT HAVE A LARGE CONTRIBUTING AREA.
- 6. SEDIMENT SHALL BE REMOVED FROM BEHIND THE STRUCTURES WHEN IT HAS ACCUMULATED TO ONE HALF THE ORIGINAL HEIGHT OF THE STRUCTURE.
- 7. STRUCTURES MAY BE LEFT IN PLACE ONCE THE SITE IS STABILIZED.

ORGANIC FILTER BERM / FIBER BERM

NOT TO SCALE

Design: DJM | Draft: KDR Date: 2/26/2024 Checked: JAC Scale: AS NOTED Project No.: 18134.1 Drawing Name: 18134.1-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE T THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



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- 1. <u>GRADING AND SHAPING</u> A. SLOPES SHALL NOT BE STEEPER THAN 2:1 WITHOUT APPROPRIATE EROSION CONTROL MEASURES AS SPECIFIED ON THE PLANS (3:1 SLOPES OR FLATTER ARE PREFERRED).
- B. WHERE MOWING WILL BE DONE, 3:1 SLOPES OR FLATTER ARE RECOMMENDED.

# 2. <u>SEEDBED PREPARATION</u>

- A. SURFACE AND SEEPAGE WATER SHOULD BE DRAINED OR DIVERTED FROM THE SITE TO PREVENT DROWNING OR WINTER KILLING OF THE PLANTS. B. STONES LARGER THAN 4 INCHES AND TRASH SHOULD BE REMOVED BECAUSE THEY INTERFERE WITH
- SEEDING AND FUTURE MAINTENANCE OF THE AREA. WHERE FEASIBLE, THE SOIL SHOULD BE TILLED TO A DEPTH OF ABOUT 4 INCHES TO PREPARE A SEEDBED AND FERTILIZER AND LIME MIXED INTO THE SOIL. THE SEEDBED SHOULD BE LEFT IN A REASONABLY FIRM AND SMOOTH CONDITION. THE LAST TILLAGE OPERATION SHOULD BE PERFORMED ACROSS THE SLOPE WHEREVER PRACTICAL.

## 3. ESTABLISHING A STAND

- A. LIME AND FERTILIZER SHOULD BE APPLIED PRIOR TO OR AT THE TIME OF SEEDING AND INCORPORATED INTO THE SOIL. TYPES AND AMOUNTS OF LIME AND FERTILIZER SHOULD BE BASED ON AN EVALUATION OF SOIL TESTS. WHEN A SOIL TEST IS NOT AVAILABLE, THE FOLLOWING MINIMUM AMOUNTS SHOULD BE **APPLIED:**
- AGRICULTURAL LIMESTONE, 2 TONS PER ACRE OR 100 LBS. PER 1,000 SQ.FT.
- NITROGEN(N), 50 LBS. PER ACRE OR 1.1 LBS. PER 1,000 SQ.FT. PHOSPHATE(P205), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT.
- POTASH(K20), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT.
- (NOTE: THIS IS THE EQUIVALENT OF 500 LBS. PER ACRE OF 10-20-20 FERTILIZER OR 1,000 LBS. PER ACRE OF 5-10-10.)
- B. SEED SHOULD BE SPREAD UNIFORMLY BY THE METHOD MOST APPROPRIATE FOR THE SITE. METHODS INCLUDE BROADCASTING, DRILLING AND HYDROSEEDING. WHERE BROADCASTING IS USED, COVER SEED WITH .25 INCH OF SOIL OR LESS, BY CULTIPACKING OR RAKING.
- C. REFER TO THE 'SEEDING GUIDE' AND 'SEEDING RATES' TABLES ON THIS SHEET FOR APPROPRIATE SEED MIXTURES AND RATES OF SEEDING. ALL LEGUMES (CROWNVETCH, BIRDSFOOT, TREFOIL AND FLATPEA)
- MUST BE INOCULATED WITH THEIR SPECIFIC INOCULANT PRIOR TO THEIR INTRODUCTION TO THE SITE. D. WHEN SEEDED AREAS ARE MULCHED, PLANTINGS MAY BE MADE FROM EARLY SPRING TO EARLY OCTOBER WHEN SEEDED AREAS ARE NOT MULCHED, PLANTINGS SHOULD BE MADE FROM EARLY SPRING TO MAY 20th
- OR FROM AUGUST 10th TO SEPTEMBER 1st.

4. MULCH

- A. HAY, STRAW, OR OTHER MULCH. WHEN NEEDED, SHOULD BE APPLIED IMMEDIATELY AFTER SEEDING. B. MULCH WILL BE HELD IN PLACE USING APPROPRIATE TECHNIQUES FROM THE BEST MANAGEMENT PRACTICE FOR MULCHING. HAY OR STRAW MULCH SHALL BE PLACED AT A RATE OF 90 LBS PER 1000 S.F.
- 5. MAINTENANCE TO ESTABLISH A STAND
- A. PLANTED AREAS SHOULD BE PROTECTED FROM DAMAGE BY FIRE, GRAZING, TRAFFIC, AND DENSE WEED B. FERTILIZATION NEEDS SHOULD BE DETERMINED BY ONSITE INSPECTIONS. SUPPLEMENTAL FERTILIZER IS
- USUALLY THE KEY TO FULLY COMPLETE THE ESTABLISHMENT OF THE STAND BECAUSE MOST PERENNIALS TAKE 2 TO 3 YEARS TO BECOME FULLY ESTABLISHED.
- C. IN WATERWAYS, CHANNELS, OR SWALES WHERE UNIFORM FLOW CONDITIONS ARE ANTICIPATED, ANNUAL MOWING MAY BE NECESSARY TO CONTROL GROWTH OF WOODY VEGETATION.

USE	SEEDING MIXTURE 1/	DROUGHTY	WELL DRAINED	MODERATELY WELL DRAINED	POORLY DRAINED
STEEP CUTS AND FILLS, BORROW AND DISPOSAL	A B C	FAIR POOR POOR	GOOD GOOD GOOD	GOOD FAIR EXCELLENT	FAIR FAIR GOOD
AREAS	D	FAIR	EXCELLENT	EXCELLENT	POOR
WATERWAYS, EMERGENC` SPILLWAYS, AND OTHER CHANNELS WITH FLOWING WATER.	Y A C	GOOD GOOD	GOOD EXCELLENT	GOOD EXCELLENT	FAIR FAIR
LIGHTLY USED PARKING LOTS, ODD AREAS, UNUSED LANDS, AND LOW INTENSITY USE RECREATION SITES.	A B C	GOOD GOOD GOOD	GOOD GOOD EXCELLENT	GOOD FAIR EXCELLENT	FAIR POOR FAIR
PLAY AREAS AND ATHLETIC FIELDS. (TOPSOIL IS ESSENTIAL FOR GOOD TURF.)	E F	FAIR FAIR	EXCELLENT EXCELLENT	EXCELLENT EXCELLENT	<u>2/</u> 2/

GRAVEL PIT, SEE NH-PM-24 IN APPENDIX FOR RECOMMENDATION REGARDING RECLAMATION OF SAND AND GRAVEL PITS.

/ REFER TO SEEDING MIXTURES AND RATES IN TABLE BELOW.  $\overline{27}$  poorly drained soils are not desirable for use as playing area and athletic fields.

NOTE: TEMPORARY SEED MIX FOR STABILIZATION OF TURF SHALL BE WINTER RYE OR OATS AT A RATE OF 2.5 LBS. PER 1000 S.F. AND SHALL BE PLACED PRIOR TO OCTOBER 15th, IF PERMANENT SEEDING NOT YET COMPLETE.

# SEEDING GUIDE

	MIXTURE	POUNDS PER ACRE	POUNDS PER <u>1.000 Sq. Ft</u>
	A. TALL FESCUE CREEPING RED FESCUE RED TOP TOTAL	20 20 <u>2</u> 42	0.45 0.45 <u>0.05</u> 0.95
	B. TALL FESCUE CREEPING RED FESCUE CROWN VETCH OR	15 10 15	0.35 0.25 0.35
	FLAT PEA TOTAL	<u> </u>	0.75 0.95 OR 1.35
<	C. TALL FESCUE CREEPING RED FESCUE BIRDS FOOT TREFOIL TOTAL	20 20 <u>8</u> 48	0.45 0.45 <u>0.20</u> 1.10
	D. TALL FESCUE FLAT PEA TOTAL	20 <u>30</u> 50	0.45 <u>0.75</u> 1.20
	E. CREEPING RED FESCUE 1/ KENTUCKY BLUEGRASS 1/ TOTAL	50 <u>50</u> 100	1.15 <u>1.15</u> 2.30
	F. TALL FESCUE 1	150	3.60
	1/FOR HEAVY USE ATHLETIC FIEL NEW HAMPSHIRE COOPERATIVE EXT CURRENT VARIETIES AND SEEDING	DS CONSULT THE U ENSION TURF SPEC RATES.	JNIVERSITY OF CIALIST FOR

# SEEDING RATES



4. THE WIDTH OF THE ENTRANCE SHALL NOT BE LESS THAN THE FULL WIDTH OF THE ENTRANCE WHERE INGRESS OR EGRESS OCCURS, OR 10 FEET, WHICHEVER IS GREATER. 5. GEOTEXTILE FILTER FABRIC SHALL BE PLACED OVER THE ENTIRE AREA PRIOR TO PLACING THE STONE. FILTER FABRIC IS NOT REQUIRED FOR A SINGLE FAMILY RESIDENTIAL LOT. 6. ALL SURFACE WATER THAT IS FLOWING TO OR DIVERTED TOWARD THE CONSTRUCTION ENTRANCE SHALL BE PIPED BENEATH THE ENTRANCE. IF PIPING IS IMPRACTICAL, A STONE

7. THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION THAT WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO THE PUBLIC RIGHT-OF-WAY. THIS MAY REQUIRE PERIODIC TOP DRESSING WITH ADDITIONAL STONE AS CONDITIONS DEMAND AND REPAIR AND/OR CLEAN

BERM WITH 5:1 SLOPES THAT CAN BE CROSSED BY VEHICLES MAY BE SUBSTITUTED FOR

OUT OF ANY MEASURES USED TO TRAP SEDIMENT. ALL SEDIMENT SPILLED, WASHED, OR TRACKED ONTO THE PUBLIC RIGHT-OF-WAY MUST BE REMOVED PROMPTLY.



6. STRIP LOAM AND PAVEMENT PER THE RECOMMENDATIONS OF THE PROJECT ENGINEER AND STOCKPILE EXCESS MATERIAL. STABILIZE STOCKPILE AS NECESSARY.

7. PERFORM PRELIMINARY SITE GRADING IN ACCORDANCE WITH THE PLANS. 8. INSTALL THE SEWER AND DRAINAGE SYSTEMS FIRST. THEN ANY OTHER UTILITIES IN ACCORDANCE WITH THE PLAN AND DETAILS. ANY CONFLICTS BETWEEN UTILITIES ARE TO BE RESOLVED WITH THE INVOLVEMENT AND APPROVAL OF THE ENGINEER.

9. INSTALL INLET PROTECTION AT ALL CATCH BASINS AS THEY ARE CONSTRUCTED IN ACCORDANCE WITH DETAILS.

10. ALL SWALES AND DRAINAGE STRUCTURES ARE TO BE CONSTRUCTED AND STABILIZED PRIOR TO HAVING RUN-OFF DIRECTED TO THEM. 11. DAILY, OR AS REQUIRED, CONSTRUCT TEMPORARY BERMS, DRAINAGE DITCHES, CHECK DAMS, SEDIMENT TRAPS, ETC., TO PREVENT EROSION ON THE SITE AND PREVENT ANY SILTATION OF ABUTTING WATERS AND/OR PROPERTY.

12. PERFORM FINAL FINE GRADING, INCLUDING PLACEMENT OF 'SELECT' SUBGRADE MATERIALS.

13. PAVE ROADWAY AND DRIVEWAYS WITH INITIAL 'BASE COURSE'.

14. PERFORM ALL REMAINING SITE CONSTRUCTION (i.e. BUILDING, CURBING, UTILITY CONNECTIONS, ETC.).

15. LOAM AND SEED ALL DISTURBED AREAS AND INSTALL ANY REQUIRED SEDIMENT AND EROSION CONTROL FACILITIES (i.e. RIP RAP, EROSION CONTROL BLANKETS, ETC.).

16. FINISH PAVING ROADWAY AND DRIVEWAYS WITH 'FINISH' COURSE.

17. ROADWAY AND DRIVEWAYS SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.

18. ALL CUT AND FILL SLOPES SHALL BE SEEDED/LOAMED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.

19. COMPLETE PERMANENT SEEDING AND LANDSCAPING.

20. REMOVE TEMPORARY EROSION CONTROL MEASURES AFTER SEEDING AREAS HAVE BEEN 75%-85% ESTABLISHED AND SITE IMPROVEMENTS ARE COMPLETE. SMOOTH AND RE-VEGETATE ALL DISTURBED AREAS.

21. CLEAN SITE AND ALL DRAINAGE STRUCTURES, PIPES AND SUMPS OF ALL SILT AND DEBRIS.

22. INSTALL ALL PAINTED PAVEMENT MARKINGS AND SIGNAGE PER THE PLANS AND DETAILS.

23. ALL EROSION CONTROLS SHALL BE INSPECTED WEEKLY AND AFTER EVERY QUARTER-INCH OF RAINFALL

24. UPON COMPLETION OF CONSTRUCTION, IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO NOTIFY ANY RELEVANT PERMITTING AGENCIES THAT THE CONSTRUCTION HAS BEEN FINISHED IN A SATISFACTORY MANNER.

# **EROSION AND SEDIMENT CONTROL DETAILS**

LUSTER CLUSTER 635 SAGAMORE AVE., PORTSMOUTH, NH SHEET 20 OF 20

JBE PROJECT NO. 18134.1

DRAWING No.

635 SAGAMORE DEVELOPMENT LLC Owner of Record 3612 LAFAYETTE RD., DEPT 4, PORTSMOUTH, NH 03801 BK 6332 PG 1158



1-INC\2024\0aks Wal



TOTAL HEATED =3,557 G.F.



# Tighe&Bond

P5118-001 May 20, 2024

Mr. Peter Britz, Director of Planning & Sustainability City of Portsmouth Planning & Sustainability Department 1 Junkins Avenue Portsmouth NH, 03801 Portsmouth, New Hampshire 03801

## Re: Request for Site Plan Review & Conditional Use Permits Review Proposed Mixed-Use Development, 1035 Lafayette Road, Portsmouth, NH

Dear Peter:

On behalf of Christ Church Parish (Owner), and Portsmouth Housing Authority (Applicant), we are pleased to submit one (1) set of hard copies of the following information to support a request for a Site Review Permit for the above referenced project:

- One (1) full size & one (1) half size copy of the Site Plan Set, dated May 20, 2024;
- Owner Authorization, dated March 25, 2024;
- Applicant Authorization, dated March 24, 2024;
- Parking Conditional Use Permit Request, dated May 20, 2024;
- Drainage Analysis, dated May 20, 2024;
- Long-Term Operation & Maintenance Plan, dated May 20, 2024;
- Truck Turning Exhibit, dated May 20, 2024;
- Trip Generation Memorandum, dated May 20, 2024;
- Site Review Checklist, dated May 20, 2024;
- Application fee calculation form for the Site Review Permit;

## **PROJECT SUMMARY**

## **Existing Conditions**

The proposed project is located at 1035 Lafayette Road on a parcel of land identified as Map 246 Lot 1 on the City of Portsmouth Tax Maps and is located in the Gateway Neighborhood Mixed Use Corridor, G2 District. The existing parcel is approximately 3.5 acres and is bound to the west by Route 1 and to the North, East, and South by a State of New Hampshire Conservation Urban Forestry Center parcel. The sites current uses include the Christ Episcopal Church and Little Blessings Child Care Center. The site is accessed by two driveways on Route 1, a right in / right out at the center of the property and a signalized intersection at Mirona Road on the north side of property.

## **Proposed Redevelopment**

For the proposed project, the Portsmouth Housing Authority will construct a 4-story, 44-unit multi-family residential building to the south of the existing church building. In addition, HAVEN will convert and renovate the first-floor of the existing church into office space and will construct a 7-unit transitional housing addition to the north of their new office. The lower level of the existing church will be renovated for Little Blessings Child Care Center. The Christ Episcopal Church will be relocated to the existing rectory building on the southern portion of

the site. The project will include associated site improvements such as parking, pedestrian connections, access to public transportation, utilities, stormwater management, lighting, and landscaping. The site will continue to be accessed via the existing driveways on Route 1.

# LAND USE PERMIT APPLICATIONS

The proposed project will require the following site-related approvals from the Planning Board:

- Site Plan Review Permit
- Conditional Use Permit for Development Site
- Conditional Use Permit for Density Bonus Incentives
- Conditional Use Permit for Parking

The applicant met with the Planning Board on April 18, 2024, for conceptual consultation. The enclosed information which has been prepared to address comments and feedback received to date from this meeting.

The project will also require the following approvals from the New Hampshire Department of Environmental Services (NHDES):

- Alteration of Terrain Permit
- Shoreland Permit
- Sewer Connection Permit

## **Site Plan Review Permit**

The project will require a Site Plan Review Permit for the site improvements described above in the project summary. The project has previously met with the Planning Board for Conceptual Consultation.

## Traffic Impact Study

A Traffic Impact Study is currently being prepared for the development project and will be completed and submitted for review by NHDOT once the NHDOT continuous count station data from April is available. Enclosed in this package is a Trip Generation Memorandum showing the net tips for the proposed uses.

## CONDITIONAL USE PERMITS

## **Development Site Conditional Use Permit**

Under Section 10.5B41.10 Development Site Standards are "allowed by Conditional Use Permit approval from the Planning Board, a development site is any lot or group of contiguous lots owned or controlled by the same person or entity, assembled for the purpose of a single development and including more than one principal building or building type". The proposed project meets the definition of a Development Site, as such a CUP to allow the use of the Development Site Standards is being requested for this proposed project.

## **Conditional Use Permit Criteria**

Based on the above-described and enclosed materials, the following addresses how the Project warrants the granting of a Conditional Use Permit for a Development Site by satisfying the following four (4) criteria for approval in Section 10.5B43.10 of the Zoning Ordinance:



### (1) The development project is consistent with the Portsmouth Master Plan.

The Project along with the existing site as a whole is consistent with several goals identified in the Master Plan.

- Goal 1.2 is to encourage walkable mixed-use development along existing commercial corridors. The proposed project has been designed to promote alternative modes of transportation such as walking, bicycling, and public transportation by incorporating bicycle storage spaces on-site, pedestrian connections to Lafayette Rd, and the applicant is working with COAST for the addition of an on-site COAST bus stop.
- Goal 2.1 is to ensure that new development complements and enhances its surroundings. The proposed residential, office and day care uses of the proposed development will further enhance the commercial, retail, and restaurants located at the Lafayette Plaza Shopping Centers to the West and North of the property.
- Goal 3.1 and Goal 3.2 are to adapt housing stock to accommodate changing demographics and to accommodate the housing needs of low- and moderate-income residents. The Project will add 51 residential units to the local housing stock all of which 44 will be workforce housing and 7 will be transitional housing units.

# (2) The development project has been designed to allow uses that are appropriate for its context and consistent with City's planning goals and objectives for the area.

The Project has been designed to be consistent with the surrounding uses already in the neighborhood. Residential buildings are an allowed use with the zone and the addition of housing stock and workforce housing is consistent with goals laid out in the City's Master Plan as described in criteria item 1.

# (3) The project includes measures to mitigate or eliminate anticipated impacts on traffic safety and circulation, demand on municipal services, stormwater runoff, natural resources, and adjacent neighborhood character.

The Project will have a minimal impact on traffic due to the existing large traffic volumes on Lafayette Road. A traffic study will be prepared and submitted to NHDOT for review.

The development site has been designed to mitigate stormwater runoff with the use of a surface Bioretention Internal Storage Reservoir (ISR) and an infiltration basin stormwater treatment practices. The proposed project is a significant improvement over existing conditions as there is no stormwater treatment on site.

# (4) The project is consistent with the purpose and intent set forth in Section 10.5B11.

Section 10.5B11.10 states that "The purpose of Article 5B is to implement and support the goals of the City's Master Plan and Housing Policy to encourage walkable mixed-use development and continued economic vitality in the City's primary gateway areas, ensure that new development complements and enhances its surroundings, provide housing stock that is suited for changing demographics, and accommodate the housing needs of the City's current and future workforce."

The Project meets the standards outlined in Section 10.5B11.20 which are to:

- a. Promote development that is consistent with the goals of the Master Plan to create vibrant, authentic, diverse, connected and resilient neighborhoods; Criteria 1 details that the proposed project is consistent with the goals of the Master Plan.
- b. Encourage high quality housing for a variety of household types and income ranges. All of the proposed units will be workforce and transitional housing units ensuring that the Project will provide high quality housing for a variety of income ranges.
- c. Guide the physical character of development by providing a menu of building and site development types that are based on established community design principles; The proposed project maintains the existing church building on site with the addition of a new code compliant modern building on site which will enhance the parcel.
- d. **Create quality places by allowing for whole site development with meaningful public spaces and neighborhood centers.** The Project will enhance the whole-site development approach by maintaining and enhancing the existing historic features which include the addition of the Memorial and Cemetery Fence surrounding the existing burial grounds.

## **Density Bonus Conditional Use Permit**

Under Section 10.5B72 Density Bonus Incentives "A conditional use permit may be granted by the Planning Board for increased housing density or for increased building height. Such conditional use permit shall be contingent upon satisfying the requirements of Section 10.5B73". The Project is requesting a CUP for increased dwelling units per building allowed under Section 10.5B72.10.

## **Conditional Use Permit Criteria**

Based on the above-described and enclosed materials, the following addresses how the Project warrants the granting of a Conditional Use Permit for a Development Site by satisfying the following requirements for approval in Section 10.5B73.10 of the Zoning Ordinance:

**10.5B73.10** Workforce Housing Requirement: At least 20% of the dwelling units in the development, but no less than three units, shall be workforce housing units for sale or rent complying with the following criteria:

1) For sale units shall be at least the average gross floor area of the proposed units in the building or 1,000 sq. ft., whichever is greater.

All the proposed dwelling units will be for rent units.

# 2) Rental units shall be at least the average gross floor area of the proposed units in the building or 800 sq. ft., whichever is greater.

All the proposed dwelling units will be for rent units which will be at least the average gross floor area of the proposed units in the building.

# 3) The workforce housing units shall be distributed throughout the building wherever dwelling units are located.

All the proposed units will be workforce housing units therefore will be distributed throughout the building.

## **Parking Conditional Use Permit**

Under Section 10.1112.14 Number of Required Parking Spaces "The Planning Board may grant a conditional use permit to allow a building or use to provide less than the minimum number of off-street parking spaces required by Section 10.1112.30, Section 10.1112.61 or Section 10.1115.20, as applicable." The project is requesting a CUP for a reduction in off-street parking spaces. A Parking Conditional Use Permit Request has been included in the package.

## CONCLUSION

We respectfully request to be placed on the TAC meeting agenda for June 4, 2024. If you have any questions or need any additional information, please contact me by phone at (603) 294-9213 or by email at <u>NAHansen@tighebond.com</u>.

Sincerely,

TIGHE & BOND, INC.

Patrick M. Crimmins, PE Vice President

Neil A. Hansen, PE Project Manager

Cc: Portsmouth Housing Authority Christ Church Parish

# 1035 LAFAYETTE ROAD PROPOSED MULTI-FAMILY DEVELOPMENT PORTSMOUTH, NEW HAMPSHIRE DATE: May 20, 2024

SHEET NO.	SHEET TITLE	LAST REVISED
	COVER SHEET	5/20/2024
1 OF 1	TOPOGRAPHIC PLAN	4/2/2024
G-100	GENERAL NOTES AND LEGEND	5/20/2024
C-101	EXISTING CONDITIONS & DEMOLITION PLAN	5/20/2024
C-102	SITE PLAN	5/20/2024
C-103	GRADING, DRAINAGE, & EROSION CONTROL PLAN	5/20/2024
C-104	UTILITY PLAN	5/20/2024
C-105	PHOTOMETRIC PLAN	5/20/2024
C-501	EROSION CONTROL NOTES AND DETAILS SHEET	5/20/2024
C-502	DETAILS SHEET	5/20/2024
C-503	DETAILS SHEET	5/20/2024
C-504	DETAILS SHEET	5/20/2024
C-505	DETAILS SHEET	5/20/2024
C-506	DETAILS SHEET	5/20/2024
C-507	DETAILS SHEET	5/20/2024
L-1	LANDSCAPE PLAN	5/20/2024
TAC-01	COVER SHEET	5/20/2024
LS-01	CODE SEARCH AND LIFE SAFETY DRAWINGS	5/20/2024
TAC-02	FIRST FLOOR PLAN	5/20/2024
TAC-03	SECOND FLOOR PLAN	5/20/2024
TAC-04	THIRD FLOOR PLAN	5/20/2024
TAC-05	FOURTH FLOOR PLAN	5/20/2024
TAC-06	ROOF PLAN	5/20/2024
TAC-07	EXTERIOR ELEVATIONS	5/20/2024
TAC-08	EXTERIOR ELEVATIONS	5/20/2024
PR1.01	LEVEL 1 FLOOR PLAN	5/20/2024
PR1.04	NORTH AND WEST ELEVATION	5/20/2024
PR1.05	EAST AND SOUTH ELEVATION	5/20/2024

LIST OF PERM	ITS	
LOCAL	STATUS	DATE
SITE PLAN REVIEW PERMIT	PENDING	
CONDITIONAL USE PERMIT - DEVELOPMENT SITE	PENDING	
CONDITIONAL USE PERMIT - DENSITY BONUS	PENDING	
CONDITIONAL USE PERMIT - PARKING	PENDING	
STATE		
NHDES - SEWER CONNECTION PERMIT	PENDING	
NHDES - ALTERATION OF TERRAIN PERMIT	PENDING	
NHDES - SHORELAND PERMIT	PENDING	
FEDERAL		
NPDES - CONSTRUCTION GENERAL PERMIT	PENDING	





- ONSTRUCTION NOTES: THE CONTRACTOR SHALL NOT RELY ON SCALED DIMENSIONS AND SHALL CONTACT THE ENGINEER FOR CLARIFICATION IF A REOUIRED DIMENSION IS NOT PROVIDED ON THE PLANS
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR CONSTRUCTION MEANS AND METHODS. AND JIRED FOR THE SAFETY OF THE CONTRACTOR, THEIR EMPLOYEES, AGENTS OR REPRESENTATIVES IN THE PERFORMANCE OF THE WORK. THE CONTRACTOR SHALL BE RESPONSIBLE FOR DETERMINING AND IMPLEMENTING SAFETY PROCEDURES AND SYSTEMS AS REQUIRED BY THE UNITED STATES OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA), AND ANY STATE OR LOCAL SAFETY REGULATIONS.
- TIGHE & BOND ASSUMES NO RESPONSIBILITY FOR ANY ISSUES LEGAL OR OTHERWISE RESULTING FROM CHANGES MADE TO THESE DRAWINGS WITHOUT WRITTEN AUTHORIZATION OF TIGHE & BOND.

PREPARED BY: **Tighe&Bond** 

**177 CORPORATE DRIVI** PORTSMOUTH, NH 03801 603-433-8818

**APPLICANT:** 

PORTSMOUTH HOUSING AUTHORITY 245 Middle Street Portsmouth, NH 03801

OWNER:

CHRIST CHURCH PARISH 1035 Lafayette Rd Portsmouth, NH 03801

# LANDSCAPE ARCHITECT:

WOODBURN & COMPANY 103 Kent Place Newmarket, NH 03857

# **ARCHITECT:**

JSA DESIGN 273 Corporate Dr Suite 100 Portsmouth, NH 03801

# SURVEYOR:

JAMES VERRA & ASSOCIATES, INC. 101 Shattuck Way, Suite 8 Newington, NH 03801

# TAC SUBMISSION **COMPLETE SET 28 SHEETS**



LASSEL ARCHITECTS 370 Main St South Berwick, ME 03908











# NOTES:

FRONT YARD SETBACK ......30'\* SIDE YARD SETBACK ......10' REAR YARD SETBACK ......30'

- \* SEE PORTSMOUTH ZONING SECTION 10.533 FOR SPECIAL YARD REQUIREMENTS ON LAFAYETTE ROAD. (80' FROM CENTERLINE OF LAFAYETTE ROAD.)
- 3. THE INTENT OF THIS PLAN IS TO SHOW THE EXISTING CONDITIONS OF THE SUBJECT PARCEL AND THE IMPROVEMENTS THEREON FOR FUTURE SITE REDEVELOPMENT.
- 4. THE LOCATION OF ALL UNDERGROUND UTILITIES SHOWN HEREON ARE APPROXIMATE AND ARE BASED UPON THE FIELD LOCATION OF ALL VISIBLE STRUCTURES (IE CATCH BASINS, MANHOLES, WATER GATES ETC.) AND INFORMATION COMPILED FROM PLANS PROVIDED BY UTILITY COMPANIES AND GOVERNMENTAL AGENCIES. ALL CONTRACTORS SHOULD NOTIFY, IN WRITING, SAID AGENCIES PRIOR TO ANY EXCAVATION WORK AND CALL DIG-SAFE @ 1-888-DIG-SAFE.
- 5. HORIZONTAL DATUM: NAD83, VERTICAL DATUM: NAVD88. ESTABLISHED BY SURVEY GRADE GPS OBSERVATION AND PROCESSED BY OPUS. UNITS: US SURVEY FOOT.
- 6. THE PLAN IS BASED UPON A FIELD SURVEY COMPLETED IN JULY AUGUST OF 2023 & MARCH 2024 WITH TRIMBLE S5 ROBOTIC TOTAL STATION, CARLSON BRX7 RTK GPS UNITS, PANASONIC FZ-M1/TRIMBLE TSC7 DATA COLLECTORS.
- 7. THE PARCEL SHOWN HEREON LIES WITHIN ZONE X (AREA OF MINIMAL FLOOD HAZARD) AS IDENTIFIED ON FLOOD INSURANCE RATE MAP, ROCKINGHAM COUNTY, NEW HAMPSHIRE, MAP NUMBER 33015C0270F, EFFECTIVE DATE 1/29/2021 BY THE FEDERAL EMERGENCY MANAGEMENT AGENCY.
- 8. WETLANDS WERE DELINEATED BY JOSEPH NOEL, CWS #86 ON 6/22/2023 AND WERE FIELD LOCATED BY JVA.
- 9. CONTRACTOR TO VERIFY SITE BENCHMARKS BY LEVELING BETWEEN 2 BENCHMARKS PRIOR TO THE ESTABLISHMENT OF ANY GRADES OR ELEVATIONS. DISCREPANCIES ARE TO BE REPORTED TO JAMES VERRA AND ASSOCIATES, INC.
- 10. IT IS BELIEVED THAT THE "MEMORIAL GARDEN" DOES NOT HAVE ANY REMAINS OR URNS BURIED THERE BASED ON INFORMATION PROVIDED BY REPRESENTATIVES AT THE EPISCOPAL CHURCH OF NEW HAMPSHIRE. THERE IS A POSSIBILITY THAT ASHES HAVE BEEN SPRINKLED IN THE GARDEN. BASED ON THE INFORMATION PROVIDED THE MEMORIAL GARDEN MAY NOT BE CONSIDERED A CEMETERY AND WOULD NOT BE SUBJECT TO THE 25' BUFFER. FURTHER EXPLORATION SHOULD BE CONDUCTED TO CONFIRM NO HUMAN REMAINS ARE LOCATED IN THE GARDEN, EXTREME CAUTION SHOULD BE USED IN ANY EXCAVATION WITHIN 25' OF THE MEMORIAL GARDEN.
- 11. SHORELAND PROTECTION BUFFER SHOWN IS BASED ON THE CHANNEL LOCATION TAKEN FROM AERIAL PHOTOGRAPHY.

# **REFERENCE PLANS:**

- 1. "PLAN OF LAND, PORTSMOUTH, N.H., FOR CHRIST EPSICOPOL CHURCH." REVISED SEPT. 1964, AND PREPARED BY JOHN W. DURGIN (JWD). JWD FILE NO. 2320S, PLAN NO. 8393. NOT RECORDED AND ON FILE WITH THIS OFFICE.
- 2. "LOT LINE ADJUSTMENT OF THE LANDS OF: D.R.E.D. & THE PARISH OF CHRIST CHURCH." LAST REVISED JUNE 22, 1999 AND PREPARED BY RICHARD D. BARTLETT & ASSOCIATES, INC. NOT RECORDED, AND ON FILE WITH THE STATE OF NEW HAMPSHIRE DEPARTMENT OF NATURAL & CULTURAL RESOURCES, DIVISION OF FORESTS & LANDS. BARTLET JOB #298.111.
- 3. "STATE OF NEW HAMPSHIRE, DEPARTMENT OF TRANSPORTATION, RIGHT-OF-WAY, PLANS OF PROPOSED FEDERAL AID PROJECT, STP-X-T-001-1(90), N.H. PROJECT NO. 11855, US ROUTE 1 OVER SAGAMORE CREEK." DATED MARCH 14, 2000 AND PREPARED BY NHDOT & KIMBALL CHASE. RCRD PLAN #D-28308.

#1	5/3/24	COMMENTS PER I	PHAN & TEAM		RMF	
REV. NO.	DATE	DESCRIF	TION		APPR'D	
		TOPOGRAPH	HIC PLAN			
		1035 LAFAY	ETTE RO	AD		
	POR	TSMOUTH, N	EW HAM	(PSHI	RE	
		TAX MAP	#246-01			
		LAND	OF:			
	THE PARISH OF CHRIST CHURCH IN PORTSMOUTH					
		PREPARE	D FOR:			
		PORTSMOUTH HOU	SING AUTH	ORITY		
			RMF	DATE:	4/2/2024	
			DRAWN BY	JOB NO:	24–2012	
	$\frac{\text{RMF}}{\text{SCALE:}}  1'' = 50^{\circ}$					
	DWG NAME: 24-2012					
	JA	AMES VERRA & ASSOCIATES, INC.		PLAN NO:	24-2012	
101	SHATTUCK WA	Y, SUITE 8, NEWINGTON, N.H., 03801-78	376 603-436-3557	SHEET:	1 of 1	

# **GENERAL NOTES**

- 1. THE LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE NOT GUARANTEED BY THE OWNER OR THE ENGINEER. IT IS THE CONTRACTOR'S RESPONSIBILITY TO LOCATE ALL UTILITIES, ANTICIPATE CONFLICTS, REPAIR EXISTING UTILITIES AND RELOCATE EXISTING UTILITIES REQUIRED TO COMPLETE THE WORK.
- COORDINATE ALL WORK WITHIN PUBLIC RIGHT OF WAYS WITH THE CITY OF PORTSMOUTH. THE CONTRACTOR SHALL EMPLOY A NEW HAMPSHIRE LICENSED LAND SURVEYOR TO
- DETERMINE ALL LINES AND GRADES.
- 4. THE CONTRACTOR SHALL VERIFY LOCATION OF ALL EXISTING UTILITIES. CALL DIG SAFE AT LEAST 72 HOURS PRIOR TO THE COMMENCEMENT OF ANY DEMOLITION/CONSTRUCTION ACTIVITIES.
- 5. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FAMILIARIZE THEMSELVES AND COMPLY WITH THE CONDITIONS OF ALL OF THE PERMIT APPROVALS.
- 6. THE CONTRACTOR SHALL OBTAIN AND PAY FOR AND COMPLY WITH ADDITIONAL PERMITS NOTICES AND FEES NECESSARY TO COMPLETE THE WORK AND ARRANGE FOR AND PAY FOR NECESSARY INSPECTIONS AND APPROVALS FROM THE AUTHORITIES HAVING JURISDICTION.
- 7. THE CONTRACTOR SHALL PHASE DEMOLITION AND CONSTRUCTION AS REQUIRED TO PROVIDE CONTINUOUS SERVICE TO EXISTING BUSINESSES AND HOMES THROUGHOUT THE CONSTRUCTION PERIOD. EXISTING BUSINESS AND HOME SERVICES INCLUDE, BUT ARE NOT LIMITED TO ELECTRICAL, COMMUNICATION, FIRE PROTECTION, DOMESTIC WATER AND SEWER SERVICES. TEMPORARY SERVICES, IF REQUIRED, SHALL COMPLY WITH ALL FEDERAL, STATE, LOCAL AND UTILITY COMPANY STANDARDS. CONTRACTOR SHALL PROVIDE DETAILED CONSTRUCTION SCHEDULE TO OWNER PRIOR TO ANY DEMOLITION/CONSTRUCTION ACTIVITIES AND SHALL COORDINATE TEMPORARY SERVICES TO ABUTTERS WITH THE UTILITY COMPANY AND AFFECTED ABUTTER.
- 8. ALL MATERIALS AND CONSTRUCTION SHALL CONFORM WITH APPLICABLE FEDERAL, STATE, AND LOCAL CODES & SPECIFICATIONS.
- ALL WORK SHALL CONFORM TO THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS, STANDARD SPECIFICATIONS AND WITH THE STATE OF NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION, "STANDARD SPECIFICATIONS OF ROAD AND BRIDGE CONSTRUCTION", CURRENT EDITION
- 10. CONTRACTOR TO SUBMIT AS-BUILT PLANS IN DIGITAL FORMAT (.DWG AND .PDF FILES) ON DISK TO THE OWNER AND ENGINEER UPON COMPLETION OF THE PROJECT. AS-BUILTS SHALL BE PREPARED AND CERTIFIED BY A NEW HAMPSHIRE LICENSED LAND SURVEYOR.
- 11. CONTRACTOR SHALL THOROUGHLY CLEAN ALL CATCH BASINS AND DRAIN LINES, WITHIN THE LIMIT OF WORK, OF SEDIMENT IMMEDIATELY UPON COMPLETION OF CONSTRUCTION.
- 12. SEE EXISTING CONDITIONS PLAN FOR BENCH MARK INFORMATION

# **DEMOLITION NOTES:**

- 1. EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO THE START OF ANY CLEARING OR DEMOLITION ACTIVITIES.
- 2. ALL MATERIALS SCHEDULED TO BE REMOVED SHALL BECOME THE PROPERTY OF THE CONTRACTOR UNLESS OTHERWISE SPECIFIED. THE CONTRACTOR SHALL DISPOSE OF ALL MATERIALS OFF-SITE IN ACCORDANCE WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS, ORDINANCES AND CODES.
- 3. COORDINATE REMOVAL, RELOCATION, DISPOSAL OR SALVAGE OF UTILITIES WITH THE OWNER AND APPROPRIATE UTILITY COMPANY. ANY EXISTING WORK OR PROPERTY DAMAGED OR DISRUPTED BY CONSTRUCTION/
- DEMOLITION ACTIVITIES SHALL BE REPLACED OR REPAIRED TO MATCH ORIGINAL EXISTING CONDITIONS BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.
- 5. SAW CUT AND REMOVE PAVEMENT ONE (1) FOOT OFF PROPOSED EDGE OF PAVEMENT OR EXISTING CURB LINE IN ALL AREAS WHERE PAVEMENT TO BE REMOVED ABUTS EXISTING PAVEMENT OR CONCRETE TO REMAIN.
- 6. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL DEMOLITION AND OFF-SITE DISPOSAL OF MATERIALS REQUIRED TO COMPLETE THE WORK, EXCEPT FOR WORK NOTED TO BE COMPLETED BY OTHERS.
- 7. UTILITIES SHALL BE TERMINATED AT THE MAIN LINE PER UTILITY COMPANY AND CITY OF PORTSMOUTH STANDARDS. THE CONTRACTOR SHALL REMOVE ALL ABANDONED UTILITIES LOCATED WITHIN THE LIMITS OF WORK UNLESS OTHERWISE NOTED.
- CONTRACTOR SHALL VERIFY ORIGIN OF ALL DRAINS AND UTILITIES PRIOR TO REMOVAL/TERMINATION TO DETERMINE IF DRAINS OR UTILITY IS ACTIVE, AND SERVICES ANY ON OR OFF-SITE STRUCTURE TO REMAIN. THE CONTRACTOR SHALL NOTIFY ENGINEER IMMEDIATELY OF ANY SUCH UTILITY FOUND AND SHALL MAINTAIN THESE UTILITIES UNTIL PERMANENT SOLUTION IS IN PLACE.
- 9. PAVEMENT REMOVAL LIMITS ARE SHOWN FOR CONTRACTOR'S CONVENIENCE. ADDITIONAL PAVEMENT REMOVAL MAY BE REQUIRED DEPENDING ON THE CONTRACTOR'S OPERATION CONTRACTOR TO VERIFY FULL LIMITS OF PAVEMENT REMOVAL PRIOR TO BID.
- 10. THE CONTRACTOR SHALL REMOVE AND DISPOSE OF ALL EXISTING STRUCTURES, CONCRETE PADS, UTILITIES AND PAVEMENT WITHIN THE WORK LIMITS SHOWN UNLESS SPECIFICALLY IDENTIFIED TO REMAIN. ITEMS TO BE REMOVED INCLUDE BUT ARE NOT LIMITED TO: CONCRETE, PAVEMENT, CURBS, LIGHTING, MANHOLES, CATCH BASINS, UNDER GROUND PIPING, POLES, STAIRS, SIGNS, FENCES, RAMPS, WALLS, BOLLARDS, BUILDING SLABS, FOUNDATION, TREES AND LANDSCAPING.
- 11. REMOVE TREES AND BRUSH AS REQUIRED FOR COMPLETION OF WORK. CONTRACTOR SHALL GRUB AND REMOVE ALL STUMPS WITHIN LIMITS OF WORK AND DISPOSE OF OFF SITE IN ACCORDANCE WITH FEDERAL, STATE, AND LOCAL LAWS AND REGULATIONS.
- 12. CONTRACTOR SHALL PROTECT ALL PROPERTY MONUMENTATION THROUGHOUT DEMOLITION AND CONSTRUCTION OPERATIONS. SHOULD ANY MONUMENTATION BE DISTURBED BY THE CONTRACTOR, THE CONTRACTOR SHALL EMPLOY A NEW HAMPSHIRE LICENSED SURVEYOR TO REPLACE DISTURBED MONUMENTS.
- 13. PROVIDE INLET PROTECTION BARRIERS AT ALL CATCH BASINS/CURB INLETS WITHIN CONSTRUCTION LIMITS AS WELL AS CATCH BASINS/CURB INLETS THAT RECEIVE RUNOFF FROM CONSTRUCTION ACTIVITIES. INLET PROTECTION BARRIERS SHALL BE MAINTAINED FOR THE DURATION OF THE PROJECT. INLET PROTECTION BARRIERS SHALL BE "HIGH FLOW SILT SACK" BY ACF ENVIRONMENTAL OR EQUAL. INSPECT BARRIERS WEEKLY AND AFTER EACH RAIN EVENT OF 0.25 INCHES OR GREATER. CONTRACTOR SHALL COMPLETE A MAINTENANCE INSPECTION REPORT AFTER EACH INSPECTION. SEDIMENT DEPOSITS SHALL BE REMOVED AFTER EACH STORM EVENT OR MORE OFTEN IF THE FABRIC BECOMES CLOGGED OR SEDIMENT HAS ACCUMULATED TO 1/3 THE DESIGN DEPTH OF THE BARRIER.
- 15. THE CONTRACTOR SHALL PAY ALL COSTS NECESSARY FOR TEMPORARY PARTITIONING, BARRICADING, FENCING, SECURITY AND SAFETY DEVICES REQUIRED FOR THE MAINTENANCE OF A CLEAN AND SAFE CONSTRUCTION SITE.
- 16. SAW CUT AND REMOVE PAVEMENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL UTILITIES TO BE REMOVED AND PROPOSED UTILITIES LOCATED IN EXISTING PAVEMENT AREAS TO REMAIN

## SITE NOTES:

- 1. PAVEMENT MARKINGS SHALL BE INSTALLED AS SHOWN, INCLUDING PARKING SPACES, STOP BARS, ADA SYMBOLS, PAINTED ISLANDS, FIRE LANES, CROSS WALKS, ARROWS, LEGENDS AND CENTERLINES. ALL MARKINGS EXCEPT CENTERLINE AND MEDIAN ISLANDS TO BE CONSTRUCTED USING WHITE PAVEMENT MARKINGS. ALL THERMOPLASTIC PAVEMENT MARKINGS INCLUDING LEGENDS, ARROWS, CROSSWALKS AND STOP BARS SHALL MEET THE REQUIREMENTS OF AASHTO M249. ALL PAINTED PAVEMENT MARKINGS INCLUDING CENTERLINES, LANE LINES AND PAINTED MEDIANS SHALL MEET THE REQUIREMENTS OF AASHTO M248 TYPE "F".
- ALL PAVEMENT MARKINGS AND SIGNS TO CONFORM TO "MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES", "STANDARD ALPHABETS FOR HIGHWAY SIGNS AND PAVEMENT MARKINGS", AND THE AMERICANS WITH DISABILITIES ACT REQUIREMENTS, LATEST EDITIONS.
- 3. SEE DETAILS FOR PAVEMENT MARKINGS, ADA SYMBOLS, SIGNS AND SIGN POSTS.
- 4. CENTERLINES SHALL BE FOUR (4) INCH WIDE YELLOW LINES.
- PAINTED ISLANDS SHALL BE FOUR (4) INCH WIDE DIAGONAL LINES AT 3'-0" O.C. BORDERED BY FOUR (4) INCH WIDE LINES.
  - STOP BARS SHALL BE EIGHTEEN (18) INCHES WIDE, WHITE THERMOPLASTIC AND CONFORM TO CURRENT MUTCD STANDARDS.

- EMULSION IMMEDIATELY PRIOR TO PLACING NEW BITUMINOUS CONCRETE.
- 8. SEE ARCHITECTURAL/BUILDING DRAWINGS FOR ALL CONCRETE PADS & SIDEWALKS ADJACENT TO BUILDING.
- CONTRACTOR.
- 11. COORDINATE ALL WORK ADJACENT TO BUILDING WITH BUILDING CONTRACTOR.
- 12. ALL DIMENSIONS ARE TO THE FACE OF CURB UNLESS OTHERWISE NOTED.

# **GRADING AND DRAINAGE NOTES:**

- COMPACTION REQUIREMENTS: BELOW PAVED OR CONCRETE AREAS TRENCH BEDDING MATERIAL AND SAND BLANKET BACKFILL
- BELOW LOAM AND SEED AREAS ASTM D-1557, METHOD C FIELD DENSITY TESTS SHALL BE MADE IN ACCORDANCE WITH ASTM D-1556 OR ASTM-2922.
- N-12 OR EQUAL) OR RCP CLASS IV, UNLESS OTHERWISE SPECIFIED.
- FINISH GRADE. 4. CONTRACTOR SHALL PROVIDE A FINISH PAVEMENT SURFACE AND LAWN AREAS FREE OF LOW
- RAMPS AND LOADING DOCK AREAS ADJACENT TO THE BUILDING. ALL DISTURBED AREAS NOT TO BE PAVED OR OTHERWISE TREATED SHALL RECEIVE 6" LOAM,
- SEED FERTILIZER AND MULCH.
- SPECIFICATIONS FOR HIGHWAYS AND BRIDGES, LATEST EDITION.
- SUMPS.

1. SEE SHEET C-501 FOR GENERAL EROSION CONTROL NOTES AND DETAILS.

- COORDINATE ALL UTILITY WORK WITH APPROPRIATE UTILITY COMPANY. • NATURAL GAS - UNITIL
- WATER CITY OF PORTSMOUTH
- SEWER CITY OF PORTSMOUTH • ELECTRIC - EVERSOURCE
- COMMUNICATIONS CONSOLIDATED COMM/FAIRPOINT/COMCAST
- 4. ALL SEWER PIPE SHALL BE PVC SDR 35 UNLESS OTHERWISE STATED. 5. CONNECTION TO EXISTING WATER MAIN SHALL BE CONSTRUCTED TO CITY OF PORTSMOUTH
- DPW STANDARDS. 6. EXISTING UTILITIES TO BE REMOVED SHALL BE CAPPED AT THE MAIN AND MEET THE
- CODE, LATEST EDITION, AND ALL APPLICABLE STATE AND LOCAL CODES.
- COORDINATED WITH THE BUILDING DRAWINGS AND THE APPLICABLE UTILITY COMPANIES. CABLES.
- 10. THE CONTRACTOR SHALL PROVIDE AND INSTALL ALL MANHOLES, BOXES, FITTINGS OPERATIONAL
- NATURAL GAS SERVICES.
- CROSSINGS
- PROPOSED UTILITIES LOCATED IN EXISTING PAVEMENT AREAS TO REMAIN 14. HYDRANTS, GATE VALVES, FITTINGS, ETC. SHALL MEET THE REQUIREMENTS OF THE CITY OF
- PORTSMOUTH. 15. COORDINATE TESTING OF SEWER CONSTRUCTION WITH THE CITY OF PORTSMOUTH
- IN UNPAVED AREAS SHALL BE INSULATED.
- ENGINEER.
- 19. CONTRACTOR SHALL CONSTRUCT ALL UTILITIES AND DRAINS TO WITHIN 10' OF THE
- BE NECESSARY BASED ON THE OBSERVED EXISTING CONDITIONS.
- NHDOT RIGHT OF WAY ACTIVITIES PERMIT.
- 22. EXISTING SEWER LINE IS ASSUMED TO BE ASBESTOS CEMENT PIPE. CONSTRICTOR SHALL

# **EXISTING CONDITIONS PLAN NOTES:**

DATED 5/3/2024.

7. CLEAN AND COAT VERTICAL FACE OF EXISTING PAVEMENT AT SAW CUT LINE WITH RS-1

10. CONTRACTOR TO PROVIDE BACKFILL AND COMPACTION AT CURB LINE AFTER CONCRETE FORMS FOR SIDEWALKS AND PADS HAVE BEEN STRIPPED. COORDINATE WITH BUILDING

13. THE PROPERTY MANAGER WILL BE RESPONSIBLE FOR TIMELY SNOW REMOVAL FROM ALL PRIVATE SIDEWALKS, DRIVEWAYS, AND PARKING AREAS. SNOW REMOVAL WILL BE HAULED OFF-SITE AND LEGALLY DISPOSED OF WHEN SNOW BANKS EXCEED 6 FEET IN HEIGHT.

95%

95% 90%

\* ALL PERCENTAGES OF COMPACTION SHALL BE OF THE MAXIMUM DRY DENSITY AT THE OPTIMUM MOISTURE CONTENT AS DETERMINED AND CONTROLLED IN ACCORDANCE WITH

ALL STORM DRAINAGE PIPES SHALL BE HIGH DENSITY POLYETHYLENE (HANCOR HI-Q, ADS

3. ADJUST ALL MANHOLES, CATCH BASINS, CURB BOXES, ETC. WITHIN LIMITS OF WORK TO

SPOTS AND PONDING AREAS. CRITICAL AREAS INCLUDE BUILDING ENTRANCES, EXITS,

6. ALL STORM DRAIN CONSTRUCTION SHALL BE IN ACCORDANCE WITH THE NHOOT STANDARD

7. ALL PROPOSED CATCH BASINS SHALL BE EQUIPPED WITH OIL/GAS SEPARATOR HOODS AND 4'

EROSION CONTROL NOTES:

**UTILITY NOTES:** 

ALL WATER MAIN INSTALLATIONS SHALL BE CLASS 52, CEMENT LINED DUCTILE IRON PIPE. ALL WATER MAIN INSTALLATIONS SHALL BE PRESSURE TESTED AND CHLORINATED AFTER CONSTRUCTION PRIOR TO ACTIVATING THE SYSTEM. CONTRACTOR SHALL COORDINATE CHLORINATION AND TESTING WITH THE CITY OF PORTSMOUTH WATER DEPARTMENT.

DEPARTMENT OF PUBLIC WORKS STANDARDS FOR CAPPING OF WATER AND SEWER SERVICES. 7. ALL ELECTRICAL MATERIAL WORKMANSHIP SHALL CONFORM TO THE NATIONAL ELECTRIC 8. THE EXACT LOCATION OF NEW UTILITY SERVICES AND CONNECTIONS SHALL BE

9. ALL UNDERGROUND CONDUITS SHALL HAVE NYLON PULL ROPES TO FACILITATE PULLING

CONNECTORS, COVER PLATES, AND OTHER MISCELLANEOUS ITEMS NOT NECESSARILY DETAILED ON THESE DRAWINGS TO RENDER INSTALLATION OF UTILITIES COMPLETE AND

11. CONTRACTOR SHALL PROVIDE EXCAVATION, BEDDING, BACKFILL AND COMPACTION FOR

12. A 10-FOOT MINIMUM EDGE TO EDGE HORIZONTAL SEPARATION SHALL BE PROVIDED BETWEEN ALL WATER AND SANITARY SEWER LINES. AN 18-INCH MINIMUM OUTSIDE TO OUTSIDE VERTICAL SEPARATION SHALL BE PROVIDED AT ALL WATER/SANITARY SEWER

13. SAW CUT AND REMOVE PAVEMENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL

16. ALL SEWER PIPE WITH LESS THAN 6' OF COVER IN PAVED AREAS OR LESS THAT 4' OF COVER

17. CONTRACTOR SHALL COORDINATE ALL ELECTRIC WORK INCLUDING BUT NOT LIMITED TO: CONDUIT CONSTRUCTION, MANHOLE CONSTRUCTION, UTILITY POLE CONSTRUCTION, OVERHEAD WIRE RELOCATION, AND TRANSFORMER CONSTRUCTION WITH POWER COMPANY. 18. SITE LIGHTING SPECIFICATIONS, CONDUIT LAYOUT AND CIRCUITRY FOR PROPOSED SITE LIGHTING AND SIGN ILLUMINATION SHALL BE PROVIDED BY THE PROJECT ELECTRICAL

FOUNDATION WALLS AND CONNECT THESE TO SERVICE STUBS FROM THE BUILDING. 20. CONTRACTOR SHALL FIELD VERIFY EXISTING SEWER LINE LOCATION, INVERT AND DIAMETER PRIOR TO CONSTRUCTION AND SHALL SUBMIT FIELD INFORMATION TO ENGINEER FOR REVIEW. MODIFICATIONS TO THE NEW SEWER CONNECTION LOCATION AND ELEVATION MAY

21. EACH UTILITY CONNECTION WITHIN THE LAFAYETTE ROAD RIGHT OF WAY WILL REQUIRE A

UTILIZE A LICENSED ASBESTOS SPECIALIST FOR THE REMOVAL OF ANY ASBESTOS PIPE.

1. EXISTING CONDITIONS ARE BASED ON A FIELD SURVEY BY JAMES VERRA & ASSOCIATES, INC.

AMERICAN ASSOCIATION OF AASHTO STATE HIGHWAY & TRANSPORTATION OFFICIALS ACRES AMERICANS WITH DISABILITIES AGGREGATE BUTI DING BOTTOM OF CURB CATCH BASIN CONSTRUCT COORD COORDINATE DIAMETER DUCTILE IRON PIPE DRAINAGE MANHOLE DRAWING ELEVATION EDGE OF PAVEMEN ELECTRIC VEHICLE FINISHED FLOOR FLUSH GRANITE CURB HIGH DENSITY POLYETHYLENE HOT MIX ASPHALT HYDRANT INSIDE DIAMETER INVER LENGTH

## LEGEND

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ADA

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DMH

DWG

ELEV

EV

FGC

HDPE

HMA

HYD

ID

INV

APPROXIMATE LIMIT OF SAWCUT LIMIT OF WORK

APPROXIMATE LIMIT OF PAVEMENT & CONCRETE TO BE REMOVED

EXISTING TREES TO BE REMOVED

EXISTING BUILDING TO BE REMOVED

APPROXIMATE LIMIT OF PAVEMENT TO RECEIVE MILL & OVERLAY

LOCATION OF PROPOSED BUILDING

PROPERTY LINE PROPOSED EDGE OF PAVEMENT PROPOSED CURB

PROPOSED GRAVEL PAVEMENT SECTION

PROPOSED PAVEMENT SECTION

PROPOSED CONCRETE

PROPOSED MAJOR CONTOUR LINE PROPOSED MINOR CONTOUR LINE EXISTING STORM DRAIN

EXISTING DRAIN CATCH BASIN APPROXIMATE SANITARY SEWER

EXISTING WATER EXISTING GAS EXISTING OVERHEAD UTILITY EXISTING APPROXIMATE SEWER MANHOLE EXISTING SEWER MANHOLE EXISTING HYDRANT EXISTING UTILITY POLE PROPOSED DRAIN MANHOLE PROPOSED CATCH BASIN PROPOSED INLET PROTECTION BARRIER PROPOSED DRAINLINE PROPOSED SEWER MANHOLE PROPOSED SEWER LINE PROPOSED GAS LINE PROPOSED WATER LINE PROPOSED WATER VALVE PROPOSED THRUST BLOCK PROPOSED UNDERGROUND ELECTRIC LINE

PROPOSED TRANSFORMER 100' WETLAND BUFFER 50' LIMITED CUT BUFFER 25' VEGETATIVE BUFFER 250' TIDAL BUFFER 150' WOODLAND BUFFER 100' TIDAL BUFFER 50' TIDAL BUFFER

# ABBREVIATIONS

IF

MAX

MIN

OC

PCB

PDMH

POS

PROP

PSMH

PVC

PVMT

R

RCP

ROW

SGC

SF

STD

TBR

TC

TYP

UD

W

W/

YD

LINEAR FEET MAXIMUM MINIMUM ON CENTER PROPOSED CATCH BASIN PROPOSED DRAINAGE MANHOLE PROPOSED OUTLET STRUCTURE PROPOSED PROPOSED SEWER MANHOLE POLYVINYL CHLORIDE PAVEMENT RADIUS REINFORCED CONCRETE PIPE RIGHT OF WAY SLOPED GRANITE CURB SQUARE FEET STANDARD TO BE REMOVED TOP OF CURB TYPICAL UNDERDRAIN WIDTH WITH YARD DRAIN



# Proposed **Mixed-Use** Development

Portsmouth Housing Authority

1035 Lafayette Rd Portsmouth, NH

# NOT FOR CONSTRUCTION

MARK	DATE	DESCRIPTION	
PROJE	CT NO:	P5118-001	
DATE:		May 20, 2024	
FILE:		P5118-001-C-DSGN.DWG	
DRAW	N BY:	CJK/NHW	
CHECK	ED:	NAH	
APPRO	VED:	РМС	
GENERAL NOTES			
SCAI	_E:	AS SHOWN	
G-100			











# **GENERAL PROJECT INFORMATION**

PROJECT APPLICANT: PORTSMOUTH HOUSING AUTHORITY PROJECT NAME: PROPOSED MIXED USED DEVELOPMENT PROJECT ADDRESS: 1035 LAFAYETTE ROAD, PORTSMOUTH NH PROJECT MAP / LOT: TAX MAP 246, LOT 1 PROJECT LATITUDE: 42°-03'-53"N PROJECT LONGITUDE: 70°-46'-15"W

# PROJECT DESCRIPTION

THE PROPOSED PROJECT CONSISTS OF RENOVATING THE PORTION OF THE EXISTING CHURCH TO REMAIN, CONSTRUCTING A NEW ADDITION TO THE NORTH SIDE OF THE EXISTING CHURCH, AS WELL AS A FOUR STORY APARTMENT BUILDING IN THE CENTRAL PORTION OF THE SITE.

# DISTURBED AREA

THE TOTAL AREA TO BE DISTURBED IS APPROXIMATELY 3.0 ACRES.

# SOIL CHARACTERISTICS

BASED ON THE NRCS WEB SOIL SURVEY FOR STRAFFORD COUNTY - NEW HAMPSHIRE, THE SOILS ON SITE CONSIST OF URBAN LAND-CANTON GRAVELLY FINE SANDY LOAM SOILS WHICH HAVE A FAST INFILTRATION RATE WHEN THOROUGHLY WET. THESE SOILS HAVE A HYDROLOGIC SOIL GROUP RATING OF D.

# NAME OF RECEIVING WATERS

THE STORM WATER RUNOFF WILL ULTIMATELY DISCHARGE INTO THE SAGAMORE CREEK TO THE SOUTH OF THE SITE.

## CONSTRUCTION SEQUENCE OF MAJOR ACTIVITIES:

- CUT AND CLEAR TREES. CONSTRUCT TEMPORARY AND PERMANENT SEDIMENT, EROSION AND DETENTION CONTROL FACILITIES. EROSION, SEDIMENT AND DETENTION MEASURES SHALL BE INSTALLED PRIOR TO ANY EARTH MOVING OPERATIONS THAT WILL INFLUENCE STORMWATER RUNOFF SUCH AS: NEW CONSTRUCTION
  - CONTROL OF DUST
  - NEARNESS OF CONSTRUCTION SITE TO RECEIVING WATERS
- CONSTRUCTION DURING LATE WINTER AND EARLY SPRING ALL PERMANENT DITCHES, SWALES, DETENTION, RETENTION AND SEDIMENTATION BASINS TO
- BE STABILIZED USING THE VEGETATIVE AND NON-STRUCTURAL BMPS PRIOR TO DIRECTING RUNOFF TO THEM
- CLEAR AND DISPOSE OF DEBRIS.
- CONSTRUCT TEMPORARY CULVERTS AND DIVERSION CHANNELS AS REQUIRED
- GRADE AND GRAVEL ROADWAYS AND PARKING AREAS ALL ROADS AND PARKING AREA SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE
- BEGIN PERMANENT AND TEMPORARY SEEDING AND MULCHING. ALL CUT AND FILL SLOPES
- SHALL BE SEEDED AND MULCHED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- DAILY, OR AS REQUIRED, CONSTRUCT TEMPORARY BERMS, DRAINS, DITCHES, PERIMETER
- EROSION CONTROL MEASURES, SEDIMENT TRAPS, ETC., MULCH AND SEED AS REQUIRED. SEDIMENT TRAPS AND/OR BASINS SHALL BE USED AS NECESSARY TO CONTAIN RUNOFF UNTIL SOILS ARE STABILIZED
- 0. FINISH PAVING ALL ROADWAYS AND PARKING LOTS.
- INSPECT AND MAINTAIN ALL EROSION AND SEDIMENT CONTROL MEASURES.
- 12. COMPLETE PERMANENT SEEDING AND LANDSCAPING. REMOVE TRAPPED SEDIMENTS FROM COLLECTOR DEVICES AS APPROPRIATE AND THEN REMOVE TEMPORARY EROSION CONTROL MEASURES.

# SPECIAL CONSTRUCTION NOTES:

THE CONSTRUCTION SEQUENCE MUST LIMIT THE DURATION AND AREA OF DISTURBANCE. THE PROJECT IS TO BE MANAGED IN A MANNER THAT MEETS THE REQUIREMENTS AND INTENT OF RSA 430:53 AND CHAPTER AGR 3800 RELATIVE TO INVASIVE SPECIES.

## EROSION CONTROL NOTES:

- ALL EROSION CONTROL MEASURES AND PRACTICES SHALL CONFORM TO THE "NEW HAMPSHIRE STORMWATER MANUAL VOLUME 3: EROSION AND SEDIMENT CONTROLS DURING CONSTRUCTION" PREPARED BY THE NHDES
- PRIOR TO ANY WORK OR SOIL DISTURBANCE, CONTRACTOR SHALL SUBMIT SHOP DRAWINGS FOR EROSION CONTROL MEASURES AS REQUIRED IN THE PROJECT MANUAL
- CONTRACTOR SHALL INSTALL TEMPORARY EROSION CONTROL BARRIERS, INCLUDING HAY BALES, SILT FENCES, MULCH BERMS, SILT SACKS AND SILT SOCKS AS SHOWN IN THESE DRAWINGS AS THE FIRST ORDER OF WORK.
- SILT SACK INLET PROTECTION SHALL BE INSTALLED IN ALL EXISTING AND PROPOSED CATCH BASIN INLETS WITHIN THE WORK LIMITS AND BE MAINTAINED FOR THE DURATION OF THE PROJECT.
- PERIMETER CONTROLS INCLUDING SILT FENCES, MULCH BERM, SILT SOCK, AND/OR HAY BALE BARRIERS SHALL BE MAINTAINED FOR THE DURATION OF THE PROJECT UNTIL NON-PAVED AREAS HAVE BEEN STABILIZED.
- THE CONTRACTOR SHALL REMOVE AND PROPERLY DISPOSE OF ALL TEMPORARY EROSION CONTROL DEVICES UPON COMPLETION OF CONSTRUCTION.
- ALL DISTURBED AREAS NOT OTHERWISE BEING TREATED SHALL RECEIVE 6" LOAM, SEED AND FERTILIZER. INSPECT ALL INLET PROTECTION AND PERIMETER CONTROLS WEEKLY AND AFTER EACH RAIN STORM OF 0.25 INCH OR GREATER. REPAIR/MODIFY PROTECTION AS NECESSARY TO
- MAXIMIZE EFFICIENCY OF FILTER. REPLACE ALL FILTERS WHEN SEDIMENT IS 1/3 THE FILTER HEIGHT. CONSTRUCT EROSION CONTROL BLANKETS ON ALL SLOPES STEEPER THAN 3:1.

# STABILIZATION:

- AN AREA SHALL BE CONSIDERED STABLE WHEN ONE OF THE FOLLOWING HAS OCCURRED: A. BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED;
- B. A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED; C. A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH AS STONE OR RIPRAP HAS BEEN INSTALLED;
- D. EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.;
- E. IN AREAS TO BE PAVED, "STABLE" MEANS THAT BASE COURSE GRAVELS MEETING THE REQUIREMENTS OF NHDOT STANDARD FOR ROAD AND BRIDGE CONSTRUCTION, 2016, ITEM 304.2 HAVE BEEN INSTALLED.
- WINTER STABILIZATION PRACTICES: A. ALL PROPOSED VEGETATED AREAS THAT DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED BY SEEDING AND INSTALLING EROSION CONTROL BLANKETS ON SLOPES GREATER THAN 3:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT EVENTS;
- ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS;
- AFTER OCTOBER 15, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3 INCHES OF CRUSHED GRAVEL PER NHDOT ITEM 304.3, OR IF CONSTRUCTION IS TO CONTINUE THROUGH THE WINTER SEASON BE CLEARED OF ANY ACCUMULATED SNOW AFTER EACH STORM EVENT;
- STABILIZATION SHALL BE INITIATED ON ALL LOAM STOCKPILES, AND DISTURBED AREAS, WHERE CONSTRUCTION ACTIVITY SHALL NOT OCCUR FOR MORE THAN TWENTY-ONE (21) CALENDAR DAYS BY THE FOURTEENTH (14TH) DAY AFTER CONSTRUCTION ACTIVITY HAS PERMANENTLY OR TEMPORARILY CEASED IN THAT AREA. STABILIZATION MEASURES TO BE USED INCLUDE:
- A. TEMPORARY SEEDING;
- B. MULCHING.
- . ALL AREAS SHALL BE STABILIZED WITHIN 45 DAYS OF INITIAL DISTURBANCE. WHEN CONSTRUCTION ACTIVITY PERMANENTLY OR TEMPORARILY CEASES WITHIN 100 FEET OF NEARBY SURFACE WATERS OR DELINEATED WETLANDS, THE AREA SHALL BE STABILIZED WITHIN SEVEN (7) DAYS OR PRIOR TO A RAIN EVENT. ONCE CONSTRUCTION ACTIVITY CEASES

PERMANENTLY IN AN THESE AREAS, SILT FENCES, MULCH BERMS, HAY BALE BARRIERS AND

ANY EARTH/DIKES SHALL BE REMOVED ONCE PERMANENT MEASURES ARE ESTABLISHED. 6. DURING CONSTRUCTION, RUNOFF WILL BE DIVERTED AROUND THE SITE WITH EARTH DIKES, PIPING OR STABILIZED CHANNELS WHERE POSSIBLE. SHEET RUNOFF FROM THE SITE WILL BE FILTERED THROUGH SILT FENCES, MULCH BERMS, HAY BALE BARRIERS, OR SILT SOCKS. ALL STORM DRAIN BASIN INLETS SHALL BE PROVIDED WITH FLARED END SECTIONS AND TRASH RACKS. THE SITE SHALL BE STABILIZED FOR THE WINTER BY NOVEMBER 15.

# DUST CONTROL:

- 1. THE CONTRACTOR SHALL BE RESPONSIBLE TO CONTROL DUST THROUGHOUT THE CONSTRUCTION PERIOD.
- 2. DUST CONTROL METHODS SHALL INCLUDE, BUT BE NOT LIMITED TO SPRINKLING WATER ON EXPOSED AREAS, COVERING LOADED DUMP TRUCKS LEAVING THE SITE, AND TEMPORARY MULCHING.
- 3. DUST CONTROL MEASURES SHALL BE UTILIZED SO AS TO PREVENT THE MIGRATION OF DUST FROM THE SITE TO ABUTTING AREAS.

# STOCKPILES:

- CULVERTS.
- 2. ALL STOCKPILES SHOULD BE SURROUNDED WITH TEMPORARY EROSION CONTROL MEASURES
- PRIOR TO THE ONSET OF PRECIPITATION. 3. PERIMETER BARRIERS SHOULD BE MAINTAINED AT ALL TIMES, AND ADJUSTED AS NEEDED TO ACCOMMODATE THE DELIVERY AND REMOVAL OF MATERIALS FROM THE STOCKPILE. THE INTEGRITY OF THE BARRIER SHOULD BE INSPECTED AT THE END OF EACH WORKING DAY 4. PROTECT ALL STOCKPILES FROM STORMWATER RUN-OFF USING TEMPORARY EROSION CONTROL MEASURES SUCH AS BERMS, SILT SOCK, OR OTHER APPROVED PRACTICE TO
- PREVENT MIGRATION OF MATERIAL BEYOND THE IMMEDIATE CONFINES OF THE STOCKPILES

# OFF SITE VEHICLE TRACKING:

1. THE CONTRACTOR SHALL CONSTRUCT STABILIZED CONSTRUCTION ENTRANCE(S) PRIOR TO ANY EXCAVATION ACTIVITIES.

# VEGETATION:

- 1. TEMPORARY GRASS COVER:
- A. SEEDBED PREPARATION: a. APPLY FERTILIZER AT THE RATE OF 600 POUNDS PER ACRE OF 10-10-10. APPLY LIMESTONE (EQUIVALENT TO 50 PERCENT CALCIUM PLUS MAGNESIUM OXIDE) AT A RATE OF THREE (3) TONS PER ACRE;
- B. SEEDING:
- a. UTILIZE ANNUAL RYE GRASS AT A RATE OF 40 LBS/ACRE; b. WHERE THE SOIL HAS BEEN COMPACTED BY CONSTRUCTION OPERATIONS, LOOSEN SOIL TO A DEPTH OF TWO (2) INCHES BEFORE APPLYING FERTILIZER, LIME AND SEED; c. APPLY SEED UNIFORMLY BY HAND, CYCLONE SEEDER, OR HYDROSEEDER (SLURRY INCLUDING SEED AND FERTILIZER). HYDROSEEDINGS, WHICH INCLUDE MULCH, MAY BE
- LEFT ON SOIL SURFACE. SEEDING RATES MUST BE INCREASED 10% WHEN
- HYDROSEEDING;
- C. MAINTENANCE: a. TEMPORARY SEEDING SHALL BE PERIODICALLY INSPECTED. AT A MINIMUM, 95% OF THE SOIL SURFACE SHOULD BE COVERED BY VEGETATION. IF ANY EVIDENCE OF EROSION OR SEDIMENTATION IS APPARENT, REPAIRS SHALL BE MADE AND OTHER TEMPORARY MEASURES USED IN THE INTERIM (MULCH, FILTER BARRIERS, CHECK DAMS, ETC.).
- 2. VEGETATIVE PRACTICE:
  - a. LIMESTONE SHALL BE THOROUGHLY INCORPORATED INTO THE LOAM LAYER AT A RATE OF THREE (3) TONS PER ACRE IN ORDER TO PROVIDE A PH VALUE OF 5.5 TO 7.6; b. FERTILIZER SHALL BE SPREAD ON THE TOP LAYER OF LOAM AND WORKED INTO THE SURFACE. FERTILIZER APPLICATION RATE SHALL BE 800 POUNDS PER ACRE OF 10-20-20
- A. FOR PERMANENT MEASURES AND PLANTINGS:
- FERTILIZER
- c. SOIL CONDITIONERS AND FERTILIZER SHALL BE APPLIED AT THE RECOMMENDED RATES AND SHALL BE THOROUGHLY WORKED INTO THE LOAM. LOAM SHALL BE RAKED UNTIL THE SURFACE IS FINELY PULVERIZED, SMOOTH AND EVEN, AND THEN COMPACTED TO AN EVEN SURFACE CONFORMING TO THE REQUIRED LINES AND GRADES WITH APPROVED ROLLERS WEIGHING BETWEEN 4-1/2 POUNDS AND 5-1/2 POUNDS PER INCH OF WIDTH; d. SEED SHALL BE SOWN AT THE RATE SHOWN BELOW. SOWING SHALL BE DONE ON A CALM, DRY DAY, PREFERABLY BY MACHINE, BUT IF BY HAND, ONLY BY EXPERIENCED WORKMEN. IMMEDIATELY BEFORE SEEDING, THE SOIL SHALL BE LIGHTLY RAKED. ONE HALF THE SEED SHALL BE SOWN IN ONE DIRECTION AND THE OTHER HALF AT RIGHT ANGLES TO THE ORIGINAL DIRECTION. IT SHALL BE LIGHTLY RAKED INTO THE SOIL TO A DEPTH NOT OVER 1/4 INCH AND ROLLED WITH A HAND ROLLER WEIGHING NOT OVER
- 100 POUNDS PER LINEAR FOOT OF WIDTH;
- e. HAY MULCH SHALL BE APPLIED IMMEDIATELY AFTER SEEDING AS INDICATED ABOVE; f. THE SURFACE SHALL BE WATERED AND KEPT MOIST WITH A FINE SPRAY AS REQUIRED, WITHOUT WASHING AWAY THE SOIL, UNTIL THE GRASS IS WELL ESTABLISHED. ANY AREAS WHICH ARE NOT SATISFACTORILY COVERED WITH GRASS SHALL BE RESEEDED, AND ALL NOXIOUS WEEDS REMOVED;
- THE CONTRACTOR SHALL PROTECT AND MAINTAIN THE SEEDED AREAS UNTIL ACCEPTED; h. A GRASS SEED MIXTURE CONTAINING THE FOLLOWING SEED REQUIREMENTS SHALL BE APPLIED AT THE INDICATED RATE. CATION RATE

SEED MIX	APPLI
CREEPING RED FESCUE	20 LBS
TALL FESCUE	20 LBS
REDTOP	2 LBS/

3. DORMANT SEEDING (SEPTEMBER 15 TO FIRST SNOWFALL)

A. FOLLOW PERMANENT MEASURES SLOPE, LIME, FERTILIZER AND GRADING REQUIREMENTS. APPLY SEED MIXTURE AT TWICE THE INDICATED RATE. APPLY MULCH AS INDICATED FOR PERMANENT MEASURES.

## **CONCRETE WASHOUT AREA:**

- THE FOLLOWING ARE THE ONLY NON-STORMWATER DISCHARGES ALLOWED. ALL OTHER NON-STORMWATER DISCHARGES ARE PROHIBITED ON SITE:
- A. THE CONCRETE DELIVERY TRUCKS SHALL, WHENEVER POSSIBLE, USE WASHOUT FACILITIES AT THEIR OWN PLANT OR DISPATCH FACILITY;
- B. IF IT IS NECESSARY, SITE CONTRACTOR SHALL DESIGNATE SPECIFIC WASHOUT AREAS AND DESIGN FACILITIES TO HANDLE ANTICIPATED WASHOUT WATER;
- C. CONTRACTOR SHALL LOCATE WASHOUT AREAS AT LEAST 150 FEET AWAY FROM STORM
- DRAINS, SWALES AND SURFACE WATERS OR DELINEATED WETLANDS; D. INSPECT WASHOUT FACILITIES DAILY TO DETECT LEAKS OR TEARS AND TO IDENTIFY WHEN MATERIALS NEED TO BE REMOVED.

# **ALLOWABLE NON-STORMWATER DISCHARGES:**

- 1. FIRE-FIGHTING ACTIVITIES FIRE HYDRANT FLUSHING;
- 3. WATERS USED TO WASH VEHICLES WHERE DETERGENTS ARE NOT USED:
- 4. WATER USED TO CONTROL DUST; 5. POTABLE WATER INCLUDING UNCONTAMINATED WATER LINE FLUSHING;
- 6. ROUTINE EXTERNAL BUILDING WASH DOWN WHERE DETERGENTS ARE NOT USED;
- 7. PAVEMENT WASH WATERS WHERE DETERGENTS ARE NOT USED;
- 8. UNCONTAMINATED AIR CONDITIONING/COMPRESSOR CONDENSATION;
- 9. UNCONTAMINATED GROUND WATER OR SPRING WATER; 10. FOUNDATION OR FOOTING DRAINS WHICH ARE UNCONTAMINATED;
- 11. LANDSCAPE IRRIGATION.

# WASTE DISPOSAL:

2. HAZARDOUS WASTE:

- 1. WASTE MATERIAL A. ALL WASTE MATERIALS SHALL BE COLLECTED AND STORED IN SECURELY LIDDED RECEPTACLES. ALL TRASH AND CONSTRUCTION DEBRIS FROM THE SITE SHALL BE DEPOSITED IN A DUMPSTER;
- B. NO CONSTRUCTION WASTE MATERIALS SHALL BE BURIED ON SITE; C. ALL PERSONNEL SHALL BE INSTRUCTED REGARDING THE CORRECT PROCEDURE FOR WASTE
- DISPOSAL BY THE SUPERINTENDENT.

- 1. LOCATE STOCKPILES A MINIMUM OF 50 FEET AWAY FROM CATCH BASINS, SWALES, AND

- S/ACRE
- S/ACRE
- /ACRE IN NO CASE SHALL THE WEED CONTENT EXCEED ONE (1) PERCENT BY WEIGHT. ALL SEED SHALL COMPLY WITH STATE AND FEDERAL SEED LAWS. SEEDING SHALL BE DONE NO LATER THAN SEPTEMBER 15. IN NO CASE SHALL SEEDING TAKE PLACE OVER SNOW.

- A. ALL HAZARDOUS WASTE MATERIALS SHALL BE DISPOSED OF IN THE MANNER SPECIFIED BY LOCAL OR STATE REGULATION OR BY THE MANUFACTURER; B. SITE PERSONNEL SHALL BE INSTRUCTED IN THESE PRACTICES BY THE SUPERINTENDENT. 3. SANITARY WASTE: A. ALL SANITARY WASTE SHALL BE COLLECTED FROM THE PORTABLE UNITS A MINIMUM OF ONCE PER WEEK BY A LICENSED SANITARY WASTE MANAGEMENT CONTRACTOR. SPILL PREVENTION 1. CONTRACTOR SHALL BE FAMILIAR WITH SPILL PREVENTION MEASURES REQUIRED BY LOCAL, STATE AND FEDERAL AGENCIES. AT A MINIMUM, CONTRACTOR SHALL FOLLOW THE BEST MANAGEMENT SPILL PREVENTION PRACTICES OUTLINED BELOW. 2. THE FOLLOWING ARE THE MATERIAL MANAGEMENT PRACTICES THAT SHALL BE USED TO
- REDUCE THE RISK OF SPILLS OR OTHER ACCIDENTAL EXPOSURE OF MATERIALS AND SUBSTANCES DURING CONSTRUCTION TO STORMWATER RUNOFF: A. GOOD HOUSEKEEPING - THE FOLLOWING GOOD HOUSEKEEPING PRACTICE SHALL BE
- FOLLOWED ON SITE DURING CONSTRUCTION: a. ONLY SUFFICIENT AMOUNTS OF PRODUCTS TO DO THE JOB SHALL BE STORED ON SITE;
- b. ALL MATERIALS STORED ON SITE SHALL BE STORED IN A NEAT, ORDERLY MANNER IN THEIR PROPER (ORIGINAL IF POSSIBLE) CONTAINERS AND, IF POSSIBLE, UNDER A ROOF OR OTHER ENCLOSURE; c. MANUFACTURER'S RECOMMENDATIONS FOR PROPER USE AND DISPOSAL SHALL BE
- FOLLOWED; d. THE SITE SUPERINTENDENT SHALL INSPECT DAILY TO ENSURE PROPER USE AND
- DISPOSAL OF MATERIALS; e. SUBSTANCES SHALL NOT BE MIXED WITH ONE ANOTHER UNLESS RECOMMENDED BY THE
- MANUFACTURER; f. WHENEVER POSSIBLE ALL OF A PRODUCT SHALL BE USED UP BEFORE DISPOSING OF THE
- CONTAINER, B. HAZARDOUS PRODUCTS - THE FOLLOWING PRACTICES SHALL BE USED TO REDUCE THE RISKS ASSOCIATED WITH HAZARDOUS MATERIALS:
- g. PRODUCTS SHALL BE KEPT IN THEIR ORIGINAL CONTAINERS UNLESS THEY ARE NOT RESEALABLE h. ORIGINAL LABELS AND MATERIAL SAFETY DATA SHALL BE RETAINED FOR IMPORTANT
- PRODUCT INFORMATION SURPLUS PRODUCT THAT MUST BE DISPOSED OF SHALL BE DISCARDED ACCORDING TO
- THE MANUFACTURER'S RECOMMENDED METHODS OF DISPOSAL PRODUCT SPECIFIC PRACTICES - THE FOLLOWING PRODUCT SPECIFIC PRACTICES SHALL BE C. FOLLOWED ON SITE:
- a. PETROLEUM PRODUCTS:
- ALL ON SITE VEHICLES SHALL BE MONITORED FOR LEAKS AND RECEIVE REGULAR PREVENTIVE MAINTENANCE TO REDUCE LEAKAGE;
- PETROLEUM PRODUCTS SHALL BE STORED IN TIGHTLY SEALED CONTAINERS WHICH ARE CLEARLY LABELED. ANY ASPHALT BASED SUBSTANCES USED ON SITE SHALL BE APPLIED ACCORDING TO THE MANUFACTURER'S RECOMMENDATIONS. b. FERTILIZERS
- FERTILIZERS USED SHALL BE APPLIED ONLY IN THE MINIMUM AMOUNTS DIRECTED BY THE SPECIFICATIONS;
- ONCE APPLIED FERTILIZER SHALL BE WORKED INTO THE SOIL TO LIMIT EXPOSURE TO STORMWATER;
- STORAGE SHALL BE IN A COVERED SHED OR ENCLOSED TRAILERS. THE CONTENTS OF ANY PARTIALLY USED BAGS OF FERTILIZER SHALL BE TRANSFERRED TO A SEALABLE PLASTIC BIN TO AVOID SPILLS. c. PAINTS:
- ALL CONTAINERS SHALL BE TIGHTLY SEALED AND STORED WHEN NOT REQUIRED FOR USE:
- EXCESS PAINT SHALL NOT BE DISCHARGED TO THE STORM SEWER SYSTEM EXCESS PAINT SHALL BE DISPOSED OF PROPERLY ACCORDING TO MANUFACTURER'S
- INSTRUCTIONS OR STATE AND LOCAL REGULATIONS D. SPILL CONTROL PRACTICES - IN ADDITION TO GOOD HOUSEKEEPING AND MATERIAL
- MANAGEMENT PRACTICES DISCUSSED IN THE PREVIOUS SECTION, THE FOLLOWING PRACTICES SHALL BE FOLLOWED FOR SPILL PREVENTION AND CLEANUP:
- a. MANUFACTURER'S RECOMMENDED METHODS FOR SPILL CLEANUP SHALL BE CLEARLY POSTED AND SITE PERSONNEL SHALL BE MADE AWARE OF THE PROCEDURES AND THE LOCATION OF THE INFORMATION AND CLEANUP SUPPLIES;
- b. MATERIALS AND EQUIPMENT NECESSARY FOR SPILL CLEANUP SHALL BE KEPT IN THE MATERIAL STORAGE AREA ON SITE. EQUIPMENT AND MATERIALS SHALL INCLUDE BUT NOT BE LIMITED TO BROOMS, DUSTPANS, MOPS, RAGS, GLOVES, GOGGLES, KITTY LITTER, SAND, SAWDUST AND PLASTIC OR METAL TRASH CONTAINERS SPECIFICALLY FOR THIS PURPOSE
- c. ALL SPILLS SHALL BE CLEANED UP IMMEDIATELY AFTER DISCOVERY AND REPORTED TO PEASE DEVELOPMENT AUTHORITY;
- d. THE SPILL AREA SHALL BE KEPT WELL VENTILATED AND PERSONNEL SHALL WEAR APPROPRIATE PROTECTIVE CLOTHING TO PREVENT INJURY FROM CONTACT WITH A HAZARDOUS SUBSTANCE;
- e. SPILLS OF TOXIC OR HAZARDOUS MATERIAL SHALL BE REPORTED TO THE APPROPRIATE LOCAL, STATE OR FEDERAL AGENCIES AS REQUIRED;
- f. THE SITE SUPERINTENDENT RESPONSIBLE FOR DAY-TO-DAY SITE OPERATIONS SHALL BE THE SPILL PREVENTION AND CLEANUP COORDINATOR. E. VEHICLE FUELING AND MAINTENANCE PRACTICE:
- a. CONTRACTOR SHALL MAKE AN EFFORT TO PERFORM EQUIPMENT/VEHICLE FUELING AND
- MAINTENANCE AT AN OFF-SITE FACILITY b. CONTRACTOR SHALL PROVIDE AN ON-SITE FUELING AND MAINTENANCE AREA THAT IS

- e. CONTRACTOR SHALL REGULARLY INSPECT VEHICLES FOR LEAKS AND DAMAGE;
- REPLACING SPENT FLUID.

# **EROSION CONTROL OBSERVATIONS AND MAINTENANCE PRACTICES**

THIS PROJECT EXCEEDS ONE (1) ACRE OF DISTURBANCE AND THUS REQUIRES A SWPPP. THE FOLLOWING REPRESENTS THE GENERAL OBSERVATION AND REPORTING PRACTICES THAT

- SHALL BE FOLLOWED AS PART OF THIS PROJECT: 1. AN OBSERVATION REPORT SHALL BE MADE AFTER EACH OBSERVATION AND DISTRIBUTED TO THE ENGINEER, THE OWNER, AND THE CONTRACTOR;
- 2. A REPRESENTATIVE OF THE SITE CONTRACTOR, SHALL BE RESPONSIBLE FOR MAINTENANCE AND REPAIR ACTIVITIES:
- 3. IF A REPAIR IS NECESSARY, IT SHALL BE INITIATED WITHIN 24 HOURS OF REPORT; 4. AN NPDES NOTICE OF INTENT SHALL BE SUBMITTED.

# **CITY OF PORTSMOUTH BUFFER VEGETATION NOTES**

- 1. REMOVAL OR CUTTING OF VEGETATION 1.1. CHEMICAL CONTROL OF VEGETATION IS PROHIBITED IN ALL AREAS OF A WETLAND OR WETLAND BUFFER.
- THE REMOVAL OR CUTTING OF VEGETATION IS PROHIBITED IN A WETLAND OR 1.2. VEGETATED BUFFER STRIP, EXCEPT THAT NON-CHEMICAL CONTROL OF PLANTS DESIGNATED BY THE STATE OF NEW HAMPSHIRE AS "NEW HAMPSHIRE PROHIBITED
- INVASIVE SPECIES" IS PERMITTED. 1.3. THE REMOVAL OF MORE THAN 50% OF TREES GREATER THAN 6" DIAMETER AT BREAST HEIGHT (DBH) IS PROHIBITED IN THE LIMITED CUT AREA.
- 2. FERTILIZERS 2.1. THE USE OF ANY FERTILIZER IS PROHIBITED IN A WETLAND, VEGETATED BUFFER STRIP OR LIMITED CUT AREA.
- THE USE OF FERTILIZERS OTHER THAN LOW PHOSPHATE AND SLOW RELEASE NITROGEN 2.2. FERTILIZERS IS PROHIBITED IN ANY PART OF A WETLAND BUFFER.
- 3. PESTICIDES AND HERBICIDES 3.1. THE USE OF PESTICIDES OR HERBICIDES IS PROHIBITED IN A WETLAND OR WETLAND BUFFER, EXCEPT THAT APPLICATION OF PESTICIDES BY A PUBLIC AGENCY FOR PUBLIC HEALTH PURPOSES IS PERMITTED.











- CLEAN AND DRY; c. IF POSSIBLE THE CONTRACTOR SHALL KEEP AREA COVERED; d. CONTRACTOR SHALL KEEP A SPILL KIT AT THE FUELING AND MAINTENANCE AREA;
- f. CONTRACTOR SHALL USE DRIP PANS, DRIP CLOTHS, OR ABSORBENT PADS WHEN






### **4' DIAMETE**

- HOLES, NO MORE THAN 75% OF A HORIZNTAL
- 10. ALL STRUCTURES WITH MULTIPLE PIPES SHAL

- THE WIDTH OF THE WALL AND SHALL BE ASSE

- 9. PRECAST SECTIONS SHALL HAVE A TONGUE A

- 8. OUTSIDE EDGES OF PIPES SHALL PROJECT NO
- PIPE ELEVATIONS SHOWN ON PLANS SHALL B
- THE TONGUE AND GROOVE JOINT SHALL BE S

- CONSTRUCT CRUSHED STONE BEDDING AND E

- 4. THE STRUCTURES SHALL BE DESIGNED FOR

- REINFORCEMENT EQUAL TO 0.12 SQUARE INC
- 3. THE TONGUE AND THE GROOVE OF THE JOINT
- AND SHALL BE PLACED IN THE CENTER THIRD
- 2. CIRCUMFERENTIAL REINFORCEMENT SHALL B

P RESISTANT RFACE /2" FLAT FACE THIC FLUSH	<b>Tighe&amp;Bond</b>
NOTES: NOTES: NOTES: NANHOLE FRAME AND COVER SHALL BE 32" HINGED ERGO XL BY EJ CO. ALL DIMENSIONS ARE NOMINAL. SOLT SLOTS 1" SOLT SLOTS 1" ARE ALLOWED PROVIDED: A. THE FRAMES WEET OR EXCEED THE SPECIFIED LOAD RATING. B. THE INTERIOR PERIMETER (SEAT AREA) DIMENSIONS OF THE FRAMES REMAIN THE SAME TO ALLOW CONTINUED USE OF EXISTING GRATES/COVERS AS THE EXISTING FRAMES ALLOW, WITHOUT SHIMS OR OTHER MODIFICATIONS OR ACCOMMODATIONS. C. ALL OTHER PERTINENT REQUIREMENTS OF THE SPECIFICATIONS ARE MET. LABEL TYPE OF MANHOLE WITH 3" HIGH LETTERS IN HE CENTER OF THE COVER. 4-1/2"	Image: Non-Standing of New Hardson in the New Hardson in t
MANHOLE FRAMES AND COVERS SHALL BE OF HEAVY DUTY DESIGN AND PROVIDE A 30-INCH CLEAR OPENING. A 3-INCH	
(MINIMUM HEIGHT) WORD DRAIN SHALL BE PLAINLY CAST INTO THE CENTER OF EACH COVER. ADJUST TO GRADE WITH CONCRETE GRADE RINGS OR CLAY BRICKS, FRAME TO BE SET IN FULL BED OF MORTAR. (2 COURSES MAX). SEE STRUCTURE JOINTS DETAIL (TYP.) MORTAR ALL JOINTS MIN. 0.12 sq. in. STEEL PER VERTICAL FOOT, PLACED ACCORDING TO AASHTO DESIGNATION M199 48" ± 1" DIA. PIPE OPENING TO BE PRECAST IN RISER SECTION 1 - #3 BAR AROUND OPENING FOR PIPES 18" DIAMETER AND OVER, 1" COVER INVERT OF STRUCTURE TO BE CONCRETE CLASS "B" -3/4" CRUSHED STONE	Proposed Mixed-Use DevelopmentPortsmouth Housing Authority1035 Lafayette Rd Portsmouth, NH
BEDDING 6" MIN. 6" MIN. FINISH SUBGRADE 6" TYP.	NOT FOR CONSTRUCTION
ICRETE. ALL BE 0.12 SQUARE INCHES PER LINEAR FOOT IN ALL SECTIONS THIRD OF THE WALL. JOINT SHALL CONTAIN ONE LINE OF CIRCUMFERENTIAL & INCHES PER LINEAR FOOT. FOR H20 LOADING. G AND BACKFILL UNDER (6" MINIMUM THICKNESS) L BE SEALED WITH ONE STRIP OF BUTYL RUBBER SEALANT. HALL BE FIELD VERIFIED PRIOR TO PRECASTING. CT NO MORE THAN 3" BEYOND INSIDE WALL OF STRUCTURE. IGUE AND GROOVE JOINT 4" HIGH AT AN 11° ANGLE CENTERED IN E ASSEMBLED USING AN APPROVED FLEXIBLE SEALANT IN JOINTS. G SHALL HAVE A MINIMUM OF 12" OF INSIDE SURFACE BETWEEN IZNTAL CROSS SECTION SHALL BE HOLES, AND THERE SHALL BE	MARK DATE DESCRIPTION PROJECT NO: P5118-001 DATE: May 20, 2024 FILE: P5118-001-C-DTLS.DWG DRAWN BY: CJK/NHW CHECKED: NAH APPROVED: PMC
<u>IETER DRAIN MANHOLE</u> NO SCALE	SCALE: AS SHOWN



entities	
	dund

"ELIMINATOR" OIL FLOATING DEBRIS TRAP



<b>⊢►</b> A	<b>Tighe&amp;Bond</b>
POLYETHYLENE THREADED ROD WITH WING NUTS AND SPACERS B B C C C C C C C C C C C C C C C C C	NEW HAMO HANSEN No. 15227 S/20/2024
PIPE DIA.         S         B         H         L         W           12"         6.5"         10"         6.5"         25"         29"           15"         6.5"         10"         6.5"         25"         29"           15"         6.5"         10"         6.5"         25"         29"           18"         7.5"         15"         6.5"         32"         35"           24"         7.5"         18"         6.5"         36"         45"	
24         7.5         10         6.5         50         45           30"         7.5"         12"         8.6"         58"         63"           36"         7.5"         25"         8.6"         58"         63"           36"         7.5"         25"         8.6"         58"         63"	
	Proposed Mixed-Use Development Portsmouth Housing Authority
	NOT FOR CONSTRUCTION
	Image: Image
	SCALE: AS SHOWN





### Landscape Notes

- 1. Design is based on drawings by Tighe & Bond Engineering dated 2024-05-13 and Lassel Architects dated 2024-05-14 and may require adjustment due to actual field conditions.
- 2. The contractor shall follow best management practices during construction and shall take all means necessary to stabilize and protect the site from erosion.
- 3. Erosion Control shall be in place prior to construction. 4. Erosion Control shall be as illustrated in the Engineer's drawings
- 5. The Contractor shall verify layout and grades and inform the Landscape Architect or Client's Representative of
- any discrepancies or changes in layout and/or grade relationships prior to construction. 6. It is the contractor's responsibility to verify drawings provided are to the correct scale prior to any bid, estimate or installation. A graphic scale bar has been provided on each sheet for this purpose. If it is determined that the
- scale of the drawing is incorrect, the landscape architect will provide a set of drawings at the correct scale, at the request of the contractor. 7. Trees to Remain within the construction zone shall be protected from damage for the duration of the project by
- snow fence or other suitable means of protection to be approved by Landscape Architect or Client's Representative. Snow fence shall be located at the drip line at a minimum and shall include any and all surface roots. Do not fill or mulch on the trunk flare. Do not disturb roots. In order to protect the integrity of the roots, branches, trunk and bark of the tree(s) no vehicles or construction equipment shall drive or park in or on the area within the drip line(s) of the tree(s). Do not store any refuse or construction materials or portalets within the tree protection area.
- 8. This plan is for review purposes only, NOT for Construction. Construction Documents will be provided upon request.
- 9. Location, support, protection, and restoration of all existing utilities and appurtenances shall be the responsibility of the Contractor. 10. The Contractor shall verify exact location and elevation of all utilities with the respective utility owners prior
- to construction. Call DIGSAFE at 811 or 888-DIG-SAFE.
- 11. The Contractor shall procure any required permits prior to construction. 12.Prior to any landscape construction activities Contractor shall test all existing loam and loam from off-site intended to be used for lawns and plant beds using a thorough sampling throughout the supply. Soil testing shall indicate levels of pH, nitrates, macro and micro nutrients, texture, soluble salts, and organic matter. Contractor shall provide Landscape Architect with test results and recommendations from the testing facility along with soil amendment plans as necessary for the proposed plantings to thrive. All loam to be used on site shall be amended as approved by the Landscape Architect prior to placement.
- 13.Contractor shall notify landscape architect or owner's representative immediately if at any point during demolition or construction a site condition is discovered which may negatively impact the completed project. This includes, but is not limited to, unforeseen drainage problems, unknown subsurface conditions, and discrepancies between the plan and the site. If a Contractor is aware of a potential issue and does not bring it to the attention of the Landscape Architect or Owner's Representative immediately, they may be responsible for the labor and materials associated with correcting the problem.
- 14. The Contractor shall furnish and plant all plants shown on the drawings and listed thereon. All plants shall be nursery-grown under climatic conditions similar to those in the locality of the project. Plants shall conform to the botanical names and standards of size, culture, and quality for the highest grades and standards as adopted by the American Association of Nurserymen, Inc. in the American Standard of Nursery Stock, American Standards Institute, Inc. 230 Southern Building, Washington, D.C. 20005.
- 15.A complete list of plants, including a schedule of sizes, quantities, and other requirements is shown on the drawings. In the event that quantity discrepancies or material omissions occur in the plant materials list, the planting plans shall govern.
- 16.All plants shall be legibly tagged with proper botanical name. 17. The Contractor shall guarantee all plants including seeding, for not less than one year from time of
- acceptance.
- 18.Owner or Owner's Representative will inspect plants upon delivery for conformity to Specification requirements. Such approval shall not affect the right of inspection and rejection during or after the progress of the work. The Owner reserves the right to inspect and/or select all trees at the place of growth and reserves the right to approve a representative sample of each type of shrub, herbaceous perennial, annual, and ground cover at the place of growth. Such sample will serve as a minimum standard for all plants of the same species used in this work.
- 19.No substitutions of plants may be made without prior approval of the Owner or the Owner's Representative for any reason. 20. All landscaping shall be provided with the following:
- a. Outside hose attachments spaced a maximum of 150 feet apart, and
- b. An underground irrigation system, or
- c. A temporary irrigation system designed for a two-year period of plant establishment. 21. If an automatic irrigation system is installed, all irrigation valve boxes shall be located within planting bed areas
- 22. The contractor is responsible for all plant material from the time their work commences until final acceptance. This includes but is not limited to maintaining all plants in good condition, the security of the plant material once delivered to the site, watering of plants, including seeding and weeding. Plants shall be appropriately watered prior to, during, and after planting. It is the Contractor's responsibility to provide clean water suitable for plant health from off site, should it not be available on site.
- 23. All disturbed areas will be dressed with 6" of loam and planted as noted on the plans or seeded except plant beds. Plant beds shall be prepared to a depth of 12" with 75% loam and 25% compost.
- 24. Trees, ground cover, and shrub beds shall be mulched to a depth of 2" with one-year-old, well-composted, shredded native bark not longer than 4" in length and ½" in width, free of woodchips and sawdust. Mulch for ferns and herbaceous perennials shall be no longer than 1" in length. Trees in lawn areas shall be mulched in a 5' diameter min. saucer. Color of mulch shall be dark brown.
- 25. Drip strip/Maintenance Strip shall extend to 6" beyond roof overhang and shall be edged with 3/16" thick black metal edger. 26. In no case shall mulch touch the stem of a plant nor shall mulch ever be more than 3" thick total (including
- previously applied mulch) over the root ball of any plant. 27. Secondary lateral branches of deciduous trees overhanging vehicular and pedestrian travel ways shall be
- pruned up to a height of 6' to allow clear and safe passage of vehicles and pedestrians under tree canopy. Within the sight distance triangles at vehicle intersections the canopies shall be raised to 8' min. 28. Snow shall be stored a minimum of 5' from shrubs and trunks of trees.
- 29. Landscape Architect is not responsible for the means and methods of the Contractor.

Standard Tree Planting Detail







Proposed Memorial and Cemetery Fence - 8x8 granite posts with 2.5" diameter metal rails.

TREES						
Symbol	Botanical Name	Common Name	Native	Current Plan Quantity	Future Planting Quatity	Size
Am	Amelanchier granidflora 'Autumn Brilliance'	Autumn Brilliance Serviceberry	Y	3	2	8-10' ht.
Bn	Betula nigra 'Dura Heat'	Dura Heat River Birch	Y	6	2	10-12' h
Ham	Hamamelis intermedia 'Arnold Promise'	Arnold Promise Witch Hazel	Y	1	0	7-8' ht
Jv1	Juniperus virginiana 'Manhattan Blue'	Manhattan Blue Eastern Red Cedar	Y	4	0	7-8' ht.
Ls	Liquidambar styraciflua	Sweet Gum	Y	4	0	3.5" cal.
Qr	Quercus rubra	Northern Red Oak	Y	4	0	3.5" cal.
Th	Thuja plicata 'Green Giant'	Green Giant Western Red Cedar		11	0	8-10' ht.
Ua	Ulmus americana 'Princeton'	Princeton Elm	Y	6	0	3.5" cal.
SHRUBS						
Symbol	Botanical Name	Common Name	Native	Quantity		Size
Cf	Calycanthus floridus 'Aphrodite'	Aphrodite Sweetshrub	Y	0	2	7 gal.
HyL	Hydrangea paniculata 'Little Lime'	Little Lime Hydrangea		11	11	3 gal.
HyQ	Hydrangea Little Quick Fire'	Little Quick Fire Hydrangea		7	18	3 gal.
lg	Ilex glabra 'Shamrock'	Shamrock Inkberry	Y	4	20	3 gal.
K	Kalmia latifolia 'Olympic Fire'	Olympic Fire Mountain Laurel	Y	2	0	2.5'3' ht
Rh	Rhododendron 'Roseum Pink'	Roseum Pink Rhododendron		3	0	3-4' ht.
Pros	Rosa 'Apricot Drift'	Apricot Drift Rose		6	0	3 gal.
Rhus	Rhus aromatica 'Grow Low'	Grow Low Sumac	Y	0	23	3 gal.
PERENNIA	ALS, GROUNDCOVERS, VINES and A	NNUALS				
Cumula al	Deteried News	Common Name	Notice	Current Plan	Future Planting	Cine
Symbol	Botanical Name		Native	Quantity	Quatity	Size
Н	HOSTA VARIETIES					
	Hosta 'Frances Williams'	Frances Williams Hosta		3	5	1 gal.
	Hosta sieboldiana 'Elegans'	Elegans Hosta		3	5	1 gal.
	Hosta 'Sum and Substance'	Sum and Substance Hosta		3	0	1 gal.
	Hosta 'Guacamole'	Guacamole Hosta		0	5	1 gal.
Vm	Vinca minor 'Bowles'	Bowles Periwinkle		285	380	2.5" Pot



Bike Rack nts

See Engineer's

Specifications for

Concrete

Footing

Pavement sections

BB

Comments

BB

BB

Comments

© 2024 Woodburn & Company Landscape Architecture, LLC

*CycleSafe Vintage* 

Plymouth Rack

9"

 $\boldsymbol{\omega}$ 

4





# TAC SUBMISSION



TOTAL:	43,555
OVERALL APARTMENT BREAKDOWN	
FIRST FLOOR:	7
SECOND FLOOR:	14
THIRD FLOOR:	14
FOURTH FLOOR:	<u>9</u>
TOTAL:	44

OVERALL SF BREAKDOWN

FIRST FLOOR:

THIRD FLOOR:

FOURTH FLOOR:

SECOND FLOOR:

PROJECT NUM	BER:
	23.30
DATE:	
	MAY 2024
SCALE:	
	AS NOTED
REVISION:	

COVER SHEET

DRAWING NAME:

DRAWING NUMBER:

### PORTSMOUTH HOUSING AUTHORITY

CLIENT:

10,556

11,413

11,413

<u>10,173</u>

1035 LAFAYETTE ROAD

ADDRESS:

REV: DATE: NOTES:

PROJECT:

PROPOSED MIXED-USE DEVELOPMENT





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TAC - 01





 $1 \frac{\text{FIRST FLOOR - LIFE SAFETY}}{1" = 20'-0"}$ 



# TAC SUBMISSION

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DRAWING NAME: CODE SEARCH AND LIFE SAFETY DRAWINGS

PROJECT NUMBER: 23.30 DATE: MAY 2024 SCALE: AS NOTED **REVISION:** 

Exterior walls will be rated within 10' horizontally off the corners of stairways, where required per IBC 1023.7 - where

exposed by other parts of the building at an angle less than 180 degrees - EXTERIOR WALL OF STAIRWELL SHALL

Exterior walls have a fire separation distance of more than 20 feet therefore openings are unlimited in size.

PORTSMOUTH HOUSING AUTHORITY

**1035 LAFAYETTE ROAD** 

(Second floor + third floor + fourth floor) / 2 stairwells = (58 + 58 + 68) / 2 92 OCCUPANTS

Per requirements of 1011.2, when OCL over 50, minimum 44" required: 44" WIDE STAIRS PROVIDED

PROJECT:

58 occupants 11 414 s.f. / 200 = 57 160 s.f. / 300 = 1 58 occupants 11 414 s.f. / 200 = 57 160 s.f. / 300 = 1 68 occupants 9735 s.f. / 200 = 49

88 occupants 603 s.f. / 15 = 40

FOUR STORIES -12 000 SQ. FT. -

8 899 s.f. / 200 = 40 1054 s.f. / 300 = 4

REQ. MET REQ. MET

CONNECTED V-A

48 FT; (four stories)

10 546 SQ.FT.

11 574 SQ.FT.

11 574 SQ.FT.

10 173 SQ.FT.

43 875 SQ.FT.

YES, NFPA 13 R

3R system, and per o	constructio	on type V A
0 FT.	-	REQ. MET

YES, A MANUAL FIRE ALARM WITH AUTOMATIC SPRINKLER SYSTEM AND SMOKE DETECTORS





class C

class C

CLIENT: REV: DATE: NOTES

ADDRESS:

PROPOSED MIXED-USE DEVELOPMENT

279 s.f. / 15 = 19 160 s.f. / 300 = 1





- PUBLIC ACCESSIBLE ENTRANCES TO HAVE ADA
- DOOR OPERATOR AND PUSH BUTTON
  ALL STAIRWELLS TO BE 2 HOUR FIRE RATED
- ALL EGRESS DOORS TO HAVE PANIC HARDWARE
- BUILDING TO MEET ALL APPLICABLE BUILDING
   CODES AT TIME OF CONSTRUCTION
- EGRESS AND SEPARATION REGULATIONS:
- MINIMUM NUMBER OF EXITS FROM EACH STORY: 2
  MAX TRAVEL DISTANCE: 250'
- DEAD END CORRIDOR DISTANCE: 20'
- FIRE SEPARATION BETWEEN OCCUPANCY GROUPS
   TO MEET IBC AND NFPA REQUIREMENTS





### PROJECT:

### PROPOSED MIXED-USE DEVELOPMENT

ADDRESS:

1035 LAFAYETTE ROAD

### CLIENT:

### PORTSMOUTH HOUSING AUTHORITY

REV: DATE: NOTES:

B/(IE.	HOTEO.



DRAWING NAME:

FIRST FLOOR PLAN



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# EXIT SIGNS

### SF BREAKDOWN: FIRST FLOOR

	APARTMENTS:	6,710
	MECHANICAL / UTILITIES:	1,054
	CIRCULATION:	2,189
	COMMUNITY SPACES:	603
TOTA	AL:	10,556

### APARTMENT BREAKDOWN: FIRST FLOOR

ONE BEDROOM:	2
TWO BEDROOM:	3
THREE BEDROOM:	2
TOTAL:	7









- PUBLIC ACCESSIBLE ENTRANCES TO HAVE ADA
- DOOR OPERATOR AND PUSH BUTTON ALL STAIRWELLS TO BE 2 HOUR FIRE RATED
- ALL EGRESS DOORS TO HAVE PANIC HARDWARE •
- BUILDING TO MEET ALL APPLICABLE BUILDING • CODES AT TIME OF CONSTRUCTION
- EGRESS AND SEPARATION REGULATIONS:
- MINIMUM NUMBER OF EXITS FROM EACH STORY: 2 • MAX TRAVEL DISTANCE: 250' •
- DEAD END CORRIDOR DISTANCE: 20' •
- FIRE SEPARATION BETWEEN OCCUPANCY GROUPS • TO MEET IBC AND NFPA REQUIREMENTS





### PROJECT:

### PROPOSED MIXED-USE DEVELOPMENT

ADDRESS:

1035 LAFAYETTE ROAD

### CLIENT:

### PORTSMOUTH HOUSING AUTHORITY

REV: DATE: NOTES:

PROJECT NUMBER: NORTH 23.30 DATE: MAY 2024 SCALE: AS NOTED **REVISION:** 

DRAWING NAME:

SECOND FLOOR PLAN



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## EXIT SIGNS

### SF BREAKDOWN: SECOND FLOOR

	APARTMENTS:	10,012
	MECHANICAL / UTILITIES:	160
	CIRCULATION:	1,401
	COMMUNITY SPACES:	0
TOTA	L:	11,413
<u>APAR</u>	TMENT BREAKDOWN: SECOND	<u>FLOOR</u>

ONE BEDROOM:	12
TWO BEDROOM:	2
THREE BEDROOM:	0
TOTAL:	14





- PUBLIC ACCESSIBLE ENTRANCES TO HAVE ADA
- DOOR OPERATOR AND PUSH BUTTON ALL STAIRWELLS TO BE 2 HOUR FIRE RATED
- ALL EGRESS DOORS TO HAVE PANIC HARDWARE •
- BUILDING TO MEET ALL APPLICABLE BUILDING • CODES AT TIME OF CONSTRUCTION
- EGRESS AND SEPARATION REGULATIONS:
- MINIMUM NUMBER OF EXITS FROM EACH STORY: 2 • MAX TRAVEL DISTANCE: 250' •
- DEAD END CORRIDOR DISTANCE: 20' •
- FIRE SEPARATION BETWEEN OCCUPANCY GROUPS • TO MEET IBC AND NFPA REQUIREMENTS





### PROJECT:

### PROPOSED MIXED-USE DEVELOPMENT

ADDRESS:

1035 LAFAYETTE ROAD

CLIENT:

### PORTSMOUTH HOUSING AUTHORITY

REV: DATE: NOTES:



DRAWING NAME:

THIRD FLOOR PLAN



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EXIT SIGNS

### SF BREAKDOWN: THIRD FLOOR

	APARTMENTS:	10,012			
	MECHANICAL / UTILITIES:	160			
	CIRCULATION:	1,401			
	COMMUNITY SPACES:	0			
ΤΟΤΑ	11,413				
APARTMENT BREAKDOWN: THIRD FLOOR					

ONE BEDROOM:	12
TWO BEDROOM:	2
THREE BEDROOM:	0
TOTAL:	14











- PUBLIC ACCESSIBLE ENTRANCES TO HAVE ADA
- DOOR OPERATOR AND PUSH BUTTON ALL STAIRWELLS TO BE 2 HOUR FIRE RATED
- ALL EGRESS DOORS TO HAVE PANIC HARDWARE
- BUILDING TO MEET ALL APPLICABLE BUILDING • CODES AT TIME OF CONSTRUCTION
- EGRESS AND SEPARATION REGULATIONS:
- MINIMUM NUMBER OF EXITS FROM EACH STORY: 2 • MAX TRAVEL DISTANCE: 250' •
- DEAD END CORRIDOR DISTANCE: 20' •
- FIRE SEPARATION BETWEEN OCCUPANCY GROUPS • TO MEET IBC AND NFPA REQUIREMENTS





### PROJECT:

### PROPOSED MIXED-USE DEVELOPMENT

ADDRESS:

1035 LAFAYETTE ROAD

### CLIENT:

### PORTSMOUTH HOUSING AUTHORITY

REV: DATE: NOTES:

PROJECT NUMBER: NORTH 23.30 DATE: MAY 2024 SCALE: AS NOTED **REVISION:** 

DRAWING NAME:

FOURTH FLOOR PLAN



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### EXIT SIGNS

### SF BREAKDOWN: FOURTH FLOOR

	APARTMENTS:	6,495
	MECHANICAL / UTILITIES:	160
	CIRCULATION:	1,862
	COMMUNITY SPACES:	1,656
TOTAL:		10,173

### APARTMENT BREAKDOWN: FOURTH FLOOR

ONE BEDROOM:	7
TWO BEDROOM:	2
THREE BEDROOM:	0
TOTAL:	9



1 ROOF PLAN 1/8" = 1'-0"

ELEVATOR OVERRUN PV PANELS TAC - 08 2 ROOF HATCH

PV PANELS



TAC - 08

(TAC - 07

# TAC SUBMISSION

**GRAPHIC SCALE** 

0' 4' 8' 16'

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### ROOF PLAN

DRAWING NAME:

PROJECT NUM	1BER:	NORTH:
	23.30	
DATE:		$\bigwedge$
	MAY 2024	
SCALE:		
	AS NOTED	
REVISION:		



REV: DATE: NOTES:

### PORTSMOUTH HOUSING AUTHORITY

CLIENT:

1035 LAFAYETTE ROAD

ADDRESS:

DEVELOPMENT

PROPOSED MIXED-USE

PROJECT:



207 384 2049 lasselarchitects.com SARAH E HOUL HAN











- VERTICAL WOOD PRODUCT SIDING TBD

\_\_\_\_\_

- CEMENTICIOUS SIDING TBD

PROJECT:

PROPOSED MIXED-USE DEVELOPMENT

ADDRESS:

1035 LAFAYETTE ROAD

CLIENT:

DATE:

SCALE:

**REVISION:** 

DRAWING NAME:

DRAWING NUMBER:

PORTSMOUTH HOUSING AUTHORITY

REV: DATE: NOTES:

PROJECT NUMBER: 23.30

MAY 2024

AS NOTED

EXTERIOR ELEVATIONS

# TAC SUBMISSION

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TAC - 07







- CEMENTICIOUS SIDING TBD

- VERTICAL WOOD PRODUCT SIDING TBD

- CEMENTICIOUS SIDING TBD

PROJECT:

### PROPOSED MIXED-USE DEVELOPMENT

ADDRESS:

1035 LAFAYETTE ROAD

CLIENT:

### PORTSMOUTH HOUSING AUTHORITY

REV: DATE: NOTES:

PROJECT NUMBER: 23.30 DATE: MAY 2024 SCALE: AS NOTED **REVISION:** 

EXTERIOR ELEVATIONS

DRAWING NAME:

DRAWING NUMBER:

# TAC SUBMISSION

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TAC - 08







ARCHITECTS INTERIORS PLANNERS

273 CORPORATE DRIVE PORTSMOUTH, NH 03801 T 603.436.2551 www.jsainc.com

\_\_\_\_\_

CIVIL ENGINEER & LAND SURVEYOR TIGHE & BOND 177 CORPORATE DR PORTSMOUTH, NH 03801 (603) 433 - 8818

LANDSCAPE ARCHITECT WOODBURN & COMPANY 130 KENT PLACE NEWMARKET, NH 03857

STRUCTURAL ENGINEER

MECHANICAL, ELECTRICAL, PLUMBING & FIRE PROTECTION ENGINEERS

### HAVEN

273 CORPORATE DRIVE PORTSMOUTH, NH, 03801

JSA DESIGN

Scale: Date: Project Number: 1/8" = 1'-0" 05/20/2024 24064.00



PROGRESS PRINT

LEVEL 1 FLOOR PLAN











ARCHITECTS INTERIORS PLANNERS

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CIVIL ENGINEER & LAND SURVEYOR TIGHE & BOND 177 CORPORATE DR PORTSMOUTH, NH 03801 (603) 433 - 8818

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STRUCTURAL ENGINEER

MECHANICAL, ELECTRICAL, PLUMBING & FIRE PROTECTION ENGINEERS

### HAVEN

273 CORPORATE DRIVE PORTSMOUTH, NH, 03801

JSA DESIGN

Scale:

1/8" = 1'-0" 05/20/2024 24064.00

Date:

Project Number:

PROGRESS PRINT

NORTH AND WEST ELEVATION



<u>40.600</u> <u>ENTRY LEVEL - NEW</u> 40' - 7 1/4"







ARCHITECTS INTERIORS PLANNERS

273 CORPORATE DRIVE PORTSMOUTH, NH 03801 T 603.436.2551 www.jsainc.com

CIVIL ENGINEER & LAND SURVEYOR TIGHE & BOND 177 CORPORATE DR PORTSMOUTH, NH 03801 (603) 433 - 8818

LANDSCAPE ARCHITECT WOODBURN & COMPANY 130 KENT PLACE NEWMARKET, NH 03857

STRUCTURAL ENGINEER

MECHANICAL, ELECTRICAL, PLUMBING & FIRE PROTECTION ENGINEERS

### HAVEN

273 CORPORATE DRIVE PORTSMOUTH, NH, 03801

JSA DESIGN

Scale:

1/8" = 1'-0" 05/20/2024 24064.00

Date: Project Number:

### PROGRESS PRINT

EAST AND SOUTH ELEVATION



### **Owner Letter of Authorization**

This letter is to authorize <u>Portsmouth Housing Authority</u> (Applicant), to represent the interest of <u>Christ Church Parish</u> (Owner), in all site design and permitting matters for the proposed redevelopment project located at 1035 Lafayette Road in Portsmouth, New Hampshire on parcel of land identified as Map 246 Lot 1. This project includes the construction of multifamily buildings, repurposing of an existing church for office and daycare uses, and associated onsite improvements. This authorization shall relate to those activities that are required for local, state and federal permitting for the above project and include any required signatures for those applications.

Signature

Benge Ambrogi, CFO 3/25/24 Print Name Episcopal Diocese of NH Date

(P5118-001 (owner auth form).docx)

### **Agent Letter of Authorization**

This letter is to authorize Tighe & Bond, Inc. (Civil Engineer), to represent and submit on behalf of Portsmouth Housing Authority (Applicant), applications and materials in all site design and permitting matters for the proposed redevelopment project located at 1035 Lafayette Road in Portsmouth, New Hampshire on parcel of land identified as Map 246 Lot 1. This project includes the construction of multifamily buildings, repurposing of an existing church for office and daycare uses, and associated on-site improvements. This authorization shall relate to those activities that are required for local, state and federal permitting for the above project and include any required signatures for those applications.

Signature

M. Craig W. Welch 3/24/24 Print Name Date

(P5118-001 (eng auth form).docx)



P5118-001 May 20, 2024

Mr. Peter Britz, Director of Planning & Sustainability City of Portsmouth Planning & Sustainability Department 1 Junkins Avenue Portsmouth NH, 03801 Portsmouth, New Hampshire 03801

### Parking Conditional Use Permit Request Re: Proposed Mixed-Use Development, 1035 Lafayette Road, Portsmouth, NH

Dear Peter:

On behalf of Christ Church Parish (Owner), and Portsmouth Housing Authority (Applicant), we are pleased to submit the following information relative to a request for a Conditional Use Permit (CUP) to provide less than the minimum number of off-street parking spaces for the above-referenced project:

• One (1) copy of the Parking Demand Analysis, dated May 20, 2024;

Pursuant Section 10.1112.14, the applicant is respectfully requesting that a CUP be granted by the Planning Board to allow the Project to provide less than the minimum off-street parking spaces required by Section 10.1112.30 or Section 10.1112.61:

- Section 10.1112.141 The enclosed Parking Demand Analysis has been provided as • required by this section. The Parking Demand Analysis demonstrates the off-street parking provided by the Project is sufficient for its Uses.
- Section 10.1112.142 This section indicates an application for a CUP shall identify permanent evidence-based measures to reduce parking demand. As described in the enclosed Parking Demand Analysis, the Project provides measures that promotes alternative modes of transportation such as walking, bicycling, and public transportation.

We trust the enclosed information is sufficient to support a Request for a CUP. As per Section 10.1112.141 the City's Technical Advisory Committee (TAC) shall review the Parking Demand Analysis prior to submission to the Planning Board. We respectfully request to be placed on the TAC meeting agenda for June 4, 2024. If you have any questions, please feel free to contact me by phone at (603) 433-8818 or by email at NAHansen@tighebond.com.

Sincerely,

**TIGHE & BOND, INC.** 

Patrick M. Crimmins, PE Vice President Portsmouth Housing Authority Cc:

Neil A. Hansen, PE **Project Manager** 

177 Corporate Drive

Portsmouth, NH 03801-6825 • Tel 603.433.8818

www.tighebond.com

### **1035 Lafayette Rd Redevelopment – Parking Demand Memo**

то:	City of Portsmouth Planning Board
FROM:	Patrick M. Crimmins, PE Neil A. Hansen, PE
Сору:	Portsmouth Housing Authority
DATE:	May 20, 2024

Tighe & Bond, Inc. (Tighe & Bond) has prepared this Parking Demand Memo to summarize the parking demand calculations related to the proposed redevelopment of the parcel located at 1035 Lafayette Road (Route 1) in Portsmouth, New Hampshire.

The proposed project includes 4 proposed uses consisting of residential, office space, daycare facility, and a place of worship. The residential building and addition to the existing church include 51 total units consisting of a mix of 500-750 SF and >750 SF units. The existing Church is proposed to be converted to 6,900 SF of first-floor office space and 6,900 SF of lower-level daycare which has a max licensed enrollment capacity of 71 students. The existing single-family dwelling located in the southern portion of the lot would be converted to a chapel and place of assembly with an anticipated maximum occupancy of 40 people. This chapel has been calculated utilizing the place of assembly use identified as Use No. 3.10 from Portsmouth Zoning Ordinance Section 10.1112.32.

To calculate the project's parking requirement, parking demand was first calculated by the minimum parking requirements defined in the City of Portsmouth Zoning Ordinance Section 10.1112.30.

Due to the mix in uses, a shared parking calculation was then applied as allowed by Section 10.1112.61 of the Zoning Ordinance. The shared parking occupancy rate for the residential, office space, and place of worship proposed uses have utilized the standard rates identified in section 10.1112.61. The daycare parking occupancy rates have been modified from the standard Retail/Service Use to better reflect the anticipated working hours of the proposed daycare of Monday through Friday 8 AM to 5PM. We have modified the weekday daytime rate to be 100%, weekday evening to be 10% and weekend and nighttime rates to be 0%.

Lastly, a 20% reduction was applied to the parking requirement calculation as allowed by Section 10.5B82.10 of the Zoning Ordinance when public transportation is within a ¼-mile of the property. The public transit reduction requirement states that "*For developments located on a public transit route with year-round, 5-days-per-week, fixed-route service and where at least 50% of the building(s) are within ¼ mile of a transit stop, the minimum offstreet parking required for motor vehicles shall be reduced by 20% of the total required for all uses."* The proposed parcel is located along the COAST route 41, Portsmouth-Lafayette Trolley, that runs along Lafayette Rd from Downtown Portsmouth to the Lafayette Road Residence Association at Bluefish Blvd. The applicant is currently working with COAST to provide a bus stop onsite along this route which would allow the project to utilize the 20% reduction.

Based on the above-described zoning requirements, the minimum required parking for the project is calculated at 83 spaces. The proposed project provides 84 spaces, which exceeds the minimum parking requirement. In addition, the project is promoting alternative modes of transportation such as walking, bicycling, and public transportation by incorporating pedestrian connections, bicycle storage, and a bus stop.

	MINIMUM PARKING REQUIRED PER CITY ZONING ORDINANCE						
		We	ekday	Weekend		Nighttime	
	Type of Use	Daytime (8:00 AM - 5:00 PM)	Evening (6:00 PM– Midnight)	Daytime (8:00 AM- 5:00 PM)	Evening (6:00 PM– Midnight)	(Midnight- 6:00 AM)	
	Residential	60%	100%	80%	100%	100%	
	Daycare <sup>(1)</sup>	100%	10%	0%	0%	0%	
	Office Space	100%	20%	10%	5%	5%	
	Place of Worship	10%	5%	100%	50%	5%	
Use	Required Spaces per Section 10.1112.30	Required Sha		red Spaces per Section 10.1112.61			
PROPOSED RESIDENTIAL UNITS < 500 SF	0	0	0	0	0	0	
PROPOSED RESIDENTIAL UNITS 500 - 750 SF	11	7	11	9	11	11	
PROPOSED RESIDENTIAL UNITS >750 SF	52	32	52	42	52	52	
SPACES FOR RESIDENTIAL VISITORS	11	7	11	9	11	11	
PROPOSED OFFICE	20	20	4	2	1	1	
PROPOSED DAYCARE	36	36	4	0	0	0	
RELOCATED EXISTING CHAPEL	10	1	1	10	5	1	
	Total Required Shared Spaces:	103	83	72	80	76	
	Public Transit 20% Reduction Spaces: (Per Section 10.5B82.10)	83	67	58	64	61	
	Total Provided:			84			

<sup>(1)</sup> Daycare has been modified from the Retail/Service use based on conservative estimates of the business hours (M-F 8 am-5 pm) of the proposed daycare.



Proposed Multi-Family Development 1035 Lafayette Road Portsmouth, NH

### **Drainage Analysis**

### **Portsmouth Housing Authority**





100% Recyclable

### **Section 1 Project Description**

1.1	On-Site Soil Description1-1
1.2	Pre- and Post-Development Comparison1-2
1.3	Calculation Methods1-2

### **Section 2 Pre-Development Conditions**

2.1	Pre-Development Calculations2-2
2.2	Pre-Development Watershed Plan2-3

### **Section 3 Post-Development Conditions**

3.1	Post-Development Calculations	3-3
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### Section 4 Peak Rate Comparison

### **Section 5 Mitigation Description**

5.1	Pre-Treatm	nent	Metho	ds for	• Protecting	Water Quality	55-	2

5.2 Treatment Methods for Protecting Water Quality. .....5-2

### Section 6 BMP Worksheet

### Appendices

- A Web Soil Survey Report
- B Extreme Precipitation Tables

### Section 1 Project Description

The project is located at 1035 Lafayette Road identified as Map 246 Lot 1 on the City of Portsmouth Tax Maps. The existing property is approximately 3.5 acres in size and is bound to the west by Route 1, the north by Sagamore Creek, and east & south by conservation land.

The proposed project consists of converting the existing church on site to office/day care space, converting an existing single family dwelling unit to a chapel and constructing two (2) additional buildings on site. The first proposed building (Building 1) will be a 4-story, 44-unit residential building. The second proposed building on site (Building 2) will be a 2-story, 7-unit residential building that will be connected to the existing church. The project will include associated site improvements such as parking, pedestrian access, utilities, stormwater management, lighting, and landscaping.

### **1.1 On-Site Soil Description**

The project site consists of terrain that is sloping in all directions due to the center of the site consisting of the higher elevations. The site has an approximate high point of elevation 45 located at the location of the existing single family dwelling unit.

A web soil survey was completed for the project and can be found in Appendix A of this report. Based on the soil survey, the runoff analyzed within this study has been modeled using Hydrologic Soil Group A soils.

### **1.2 Pre- and Post-Development Comparison**

The pre-development and post-development watershed areas have been analyzed using four (4) distinct points of analysis (PA-1, PA-2, PA-2.1 & PA-3.) While the points of analysis have remained unchanged, the contributing sub-catchment areas varied between pre-development and post-development conditions. These adjustments were made to reflect the differences in drainage patterns between the existing and proposed conditions. The overall area analyzed as part of this drainage analysis was held constant. PA-1 is located just off site to the south of the development. This area is undisturbed conservation land and will remain undisturbed throughout construction. PA-2 is also located just off site to the west of the development at Lafayette Road - US-Route 1. PA-2.1 is located just off site and is defined as the point where the existing catch basin between the sites northern most entrance and US-Route 1 discharges into the closed drainage system under Lafayette Road - US-Route 1. The last point of analysis, PA-3, is located off site to the north of the development at the Sagamore Creek, which is a tidal body of water.

The peak discharge rates at these points of analysis were determined by analyzing Type III, 24-hour storm events. The rainfall data for these storm events were obtained from the data published by the Northeast Regional Climate Center at Cornell University, which can be found in Appendix B.

Furthermore, the site is located within a Coastal and Great Bay Community, therefore an added factor of safety of 15% was included as required by Env-Wq 1503.08(I).

### **1.3 Calculation Methods**

The design storms analyzed in this study are the 2-year, 10-year, 25-year and 50-year 24-hour duration storm events. The stormwater modeling system, HydroCAD 10.0 was utilized to predict the peak runoff rates from these storm events. The peak discharge rates were determined by analyzing Type III 24-hour storm events. The rainfall data for these storm events were obtained from the data published by the Northeast Regional Climate Center at Cornell University, with an additional 15% added factor of safety as required by Env-Wq 1503.08(I).

The time of concentration was computed using the TR-55 Method, which provides a means of determining the time for an entire watershed to contribute runoff to a specific location via sheet flows, shallow concentrated flow, and channel flow. Runoff curve numbers were calculated by estimating the coverage areas and then summing the curve number for the coverage area as a percent of the entire watershed.

### References:

- 1. HydroCAD Stormwater Modeling System, by HydroCAD Software Solutions LLC, Chocorua, New Hampshire.
- New Hampshire Stormwater Management Manual, Volume 2, Post-Construction Best Management Practices Selection and Design, December 2008.
- "Extreme Precipitation in New York & New England." Extreme Precipitation in New York & New England by Northeast Regional Climate Center (NRCC), 26 June 2012.

### Section 2 Pre-Development Conditions

To analyze the pre-development condition, the site has been modeled utilizing (4) distinct points of analysis (PA-1, PA-2, PA-2.1 & PA-3.) These points of analysis and watershed areas are depicted on the plan entitled "Pre-Development Watershed Plan", Sheet C-801.

The points of analysis and their contributing watershed areas are described below:

### Point of Analysis (PA-1)

Point of analysis 1 (PA-1) is comprised of one subcatchment area (PRE 1.0). This subcatchment is comprised of mostly impervious surfaces, grass, and woods with a small portion of roof area made up by an existing shed and existing single-family dwelling. Runoff from this subcatchment sheet flows untreated stormwater directly into the conservation lands abutting the southern and eastern portions of the site.

### Point of Analysis (PA-2)

Point of analysis 2 (PA-2) is also comprised of one subcatchment area (PRE 2.0). This subcatchment is comprised of mostly impervious surfaces, grass, and a small portion of roof area made up by a small portion of both the existing single-family dwelling and church on site. Runoff from this watershed sheet flows untreated stormwater directly onto Lafayette Road - US-Route 1.

### Point of Analysis (PA-2.1)

Point of analysis 2.1 (PA-2.1) is also comprised of one subcatchment area (PRE 2.1). This subcatchment is comprised of mostly grass with a small portion of impervious surface. Runoff from this watershed sheet flows stormwater directly into an existing catch basin on site, which ties into a closed drainage system along US-Route 1. The point at which the pipe connected to the catch basin on site discharges into the closed drainage system under Lafayette Road - US-Route 1 is depicted on the plans as PA-2.1. This catch basin has an existing DOT Drainage Easement that will remain.

### Point of Analysis (PA-3)

Point of analysis 3 (PA-3) is the last point of analysis and is also comprised of one subcatchment area (PRE 3.0). This subcatchment is comprised of mostly impervious surfaces, grass, woods, and roof made up by an existing shed and the majority of the existing Church on site. Runoff from this watershed sheet flows untreated stormwater directly into Sagamore Creek and ultimately to the Piscataqua River.

### 2.1 Pre-Development Calculations



### Area Listing (selected nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
63,435	39	>75% Grass cover, Good, HSG A (PRE-1.0, PRE-2.0, PRE-2.1, PRE-3.0)
32,277	98	Paved parking, HSG A (PRE-1.0, PRE-2.0, PRE-2.1, PRE-3.0)
9,187	98	Unconnected roofs, HSG A (PRE-1.0, PRE-2.0, PRE-3.0)
47,183	30	Woods, Good, HSG A (PRE-1.0, PRE-2.0, PRE-3.0)
152,082	52	TOTAL AREA
### Soil Listing (selected nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
152,082	HSG A	PRE-1.0, PRE-2.0, PRE-2.1, PRE-3.0
0	HSG B	
0	HSG C	
0	HSG D	
0	Other	
152,082		TOTAL AREA

P5118-001_PRE	7
Prepared by Tighe & Bond Consulting	
HvdroCAD® 10.20-4b s/n 01453 © 2023 HvdroCAD Software Solutions	LLC

SubcatchmentPRE-1.0:	Runoff Area=61,649 sf 17.89% Impervious Runoff Depth>0.12" Flow Length=218' Tc=8.6 min CN=45 Runoff=0.02 cfs 598 cf
SubcatchmentPRE-2.0:	Runoff Area=24,290 sf 39.91% Impervious Runoff Depth>0.71" Flow Length=266' Tc=7.3 min CN=62 Runoff=0.34 cfs 1,438 cf
SubcatchmentPRE-2.1:	Runoff Area=7,081 sf 22.82% Impervious Runoff Depth>0.31" Flow Length=213' Tc=5.0 min CN=52 Runoff=0.02 cfs 183 cf
SubcatchmentPRE-3.0:	Runoff Area=59,062 sf 32.39% Impervious Runoff Depth>0.45" Flow Length=237' Tc=7.3 min CN=56 Runoff=0.38 cfs 2,228 cf
Link PA-1:	Inflow=0.02 cfs 598 cf Primary=0.02 cfs 598 cf
Link PA-2:	Inflow=0.36 cfs 1,620 cf Primary=0.36 cfs 1,620 cf
Link PA-2.1:	Inflow=0.02 cfs 183 cf Primary=0.02 cfs 183 cf
Link PA-3:	Inflow=0.38 cfs 2,228 cf Primary=0.38 cfs 2,228 cf

Total Runoff Area = 152,082 sf Runoff Volume = 4,446 cf Average Runoff Depth = 0.35" 72.74% Pervious = 110,618 sf 27.26% Impervious = 41,464 sf

P5118-001_PRE	Тур
Prepared by Tighe & Bond Consulting	
HvdroCAD® 10.20-4b s/n 01453 © 2023 HvdroCAD Software Solut	ions LLC

SubcatchmentPRE-1.0:	Runoff Area=61,649 sf 17.89% Impervious Runoff Depth>0.65" Flow Length=218' Tc=8.6 min CN=45 Runoff=0.51 cfs 3,355 cf
SubcatchmentPRE-2.0:	Runoff Area=24,290 sf 39.91% Impervious Runoff Depth>1.83" Flow Length=266' Tc=7.3 min CN=62 Runoff=1.07 cfs 3,708 cf
SubcatchmentPRE-2.1:	Runoff Area=7,081 sf 22.82% Impervious Runoff Depth>1.09" Flow Length=213' Tc=5.0 min CN=52 Runoff=0.17 cfs 645 cf
SubcatchmentPRE-3.0:	Runoff Area=59,062 sf 32.39% Impervious Runoff Depth>1.37" Flow Length=237' Tc=7.3 min CN=56 Runoff=1.81 cfs 6,764 cf
Link PA-1:	Inflow=0.51 cfs 3,355 cf Primary=0.51 cfs 3,355 cf
Link PA-2:	Inflow=1.24 cfs 4,354 cf Primary=1.24 cfs 4,354 cf
Link PA-2.1:	Inflow=0.17 cfs 645 cf Primary=0.17 cfs 645 cf
Link PA-3:	Inflow=1.81 cfs 6,764 cf Primary=1.81 cfs 6,764 cf

Total Runoff Area = 152,082 sf Runoff Volume = 14,473 cf Average Runoff Depth = 1.14" 72.74% Pervious = 110,618 sf 27.26% Impervious = 41,464 sf

#### **Summary for Subcatchment PRE-1.0:**

Runoff = 0.51 cfs @ 12.21 hrs, Volume= 3,355 cf, Depth> 0.65" Routed to Link PA-1 :

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Yr Rainfall=5.62"

A	rea (sf)	CN	Description					
	1,523	98	Unconnected roofs, HSG A					
	9,504	98	Paved park	ing, HSG A	N Contraction of the second seco			
	29,181	30	Woods, Go	od, HSG A				
	21,441	39	>75% Gras	s cover, Go	bod, HSG A			
	61,649	45	Weighted A	verage				
	50,622		82.11% Pe	rvious Area				
	11,027		17.89% Imp	pervious Ar	ea			
	1,523		13.81% Un	connected				
Тс	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	) (ft/sec)	(cfs)				
4.5	50	0.0300	0.19		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.68"			
0.3	15	0.0180	0.94		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
3.8	153	0.0180	0.67		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
8.6	218	Total						

#### Summary for Subcatchment PRE-2.0:

Runoff	=	1.07 cfs @	12.12 hrs,	Volume=	3,708 cf,	Depth>	1.83"
Routed	d to Link	PA-2 :				•	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Yr Rainfall=5.62"

Area	(sf)	CN	Description
2,	,697	98	Unconnected roofs, HSG A
6,	,996	98	Paved parking, HSG A
	933	30	Woods, Good, HSG A
13,	,664	39	>75% Grass cover, Good, HSG A
24,	,290	62	Weighted Average
14,	,597		60.09% Pervious Area
9,	,693		39.91% Impervious Area
2,	,697		27.82% Unconnected

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 Type III 24-hr
 10-Yr Rainfall=5.62"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.8	50	0.0250	0.17		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.68"
1.7	103	0.0220	1.04		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.4	63	0.0200	2.87		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
0.4	50	0.1150	2.37		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps

7.3 266 Total

#### Summary for Subcatchment PRE-2.1:

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.17 cfs @ 12.10 hrs, Volume= Routed to Link PA-2.1 :

645 cf, Depth> 1.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Yr Rainfall=5.62"

A	rea (sf)	CN	Description		
	0	98	Unconnecte	ed roofs, HS	SG A
	1,616	98	Paved park	ing, HSG A	N
	0	30	Woods, Go	od, HSG A	
	5,465	39	>75% Gras	s cover, Go	ood, HSG A
	7,081	52	Weighted A	verage	
	5,465		77.18% Pe	rvious Area	
	1,616		22.82% Imp	pervious Ar	ea
Тс	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
0.7	97	0.0618	3 2.30		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.68"
0.6	83	0.1200	) 2.42		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.1	33	0.0150	) 7.62	9.35	Pipe Channel,
					15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
					n= 0.011
1.4	213	Total,	Increased	to minimum	Tc = 5.0 min

#### Summary for Subcatchment PRE-3.0:

Runoff = 1.81 cfs @ 12.12 hrs, Volume= 6,764 cf, Depth> 1.37" Routed to Link PA-3 :

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Yr Rainfall=5.62"

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 Type III 24-hr
 10-Yr Rainfall=5.62"

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A	rea (sf)	CN	Description						
	4,967	98	Unconnected roofs, HSG A						
	14,161	98	Paved park	ing, HSG A	N				
	17,069	30	Woods, Go	od, HSG A					
	22,865	39	>75% Gras	s cover, Go	bod, HSG A				
	59,062	56	Weighted A	verage					
	39,934		67.61% Pe	rvious Area					
	19,128		32.39% Imp	pervious Ar	ea				
	4,967		25.97% Un	connected					
Тс	Length	Slope	<ul> <li>Velocity</li> </ul>	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
5.1	50	0.0220	0.16		Sheet Flow,				
					Grass: Short n= 0.150 P2= 3.68"				
1.2	89	0.0300	1.21		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
0.7	60	0.0380	1.36		Shallow Concentrated Flow,				
	00	0 4 5 0 6			Short Grass Pasture Kv= 7.0 fps				
0.3	38	0.1500	1.94		Shallow Concentrated Flow,				
					vvoodiand KV= 5.0 tps				
7.3	237	Total							

#### Summary for Link PA-1:

Inflow A	Area =	61,649 sf,	17.89% Impervious,	Inflow Depth >	0.65"	for 10-Yr event
Inflow	=	0.51 cfs @	12.21 hrs, Volume=	3,355 cf		
Primary	/ =	0.51 cfs @	12.21 hrs, Volume=	3,355 cf	, Atten=	= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

#### Summary for Link PA-2:

Inflow A	Area	=		31,371 sf	,36.05% Ir	npervious,	Inflow Depth >	1.67"	for 10	)-Yr event	t
Inflow		=	1.1	24 cfs @	12.11 hrs,	Volume=	4,354 c	f			
Primar	у	=	1.1	24 cfs @	12.11 hrs,	Volume=	4,354 c	f, Atte	n= 0%,	Lag= 0.0	min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

#### Summary for Link PA-2.1:

Inflow Area	a =	7,081 sf,	22.82% In	npervious,	Inflow Depth >	1.09"	for 10	-Yr event	
Inflow	=	0.17 cfs @	12.10 hrs,	Volume=	645 c	f			
Primary	=	0.17 cfs @	12.10 hrs,	Volume=	645 c	f, Atten	= 0%,	Lag= 0.0	min
Routed	to Link	PA-2 :							

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

### **Summary for Link PA-3:**

Inflow A	Area =	59,062 s	f, 32.39% Impervious,	Inflow Depth > 2	1.37" for	10-Yr event
Inflow	=	1.81 cfs @	12.12 hrs, Volume=	6,764 cf		
Primary	/ =	1.81 cfs @	12.12 hrs, Volume=	6,764 cf,	Atten= 0	%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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SubcatchmentPRE-1.0:	Runoff Area=61,649 sf 17.89% Impervious Runoff Depth>1.30" Flow Length=218' Tc=8.6 min CN=45 Runoff=1.48 cfs 6,655 cf
SubcatchmentPRE-2.0:	Runoff Area=24,290 sf 39.91% Impervious Runoff Depth>2.89" Flow Length=266' Tc=7.3 min CN=62 Runoff=1.75 cfs 5,856 cf
SubcatchmentPRE-2.1:	Runoff Area=7,081 sf 22.82% Impervious Runoff Depth>1.92" Flow Length=213' Tc=5.0 min CN=52 Runoff=0.34 cfs 1,134 cf
SubcatchmentPRE-3.0:	Runoff Area=59,062 sf 32.39% Impervious Runoff Depth>2.30" Flow Length=237' Tc=7.3 min CN=56 Runoff=3.27 cfs 11,318 cf
Link PA-1:	Inflow=1.48 cfs 6,655 cf Primary=1.48 cfs 6,655 cf
Link PA-2:	Inflow=2.08 cfs 6,990 cf Primary=2.08 cfs 6,990 cf
Link PA-2.1:	Inflow=0.34 cfs 1,134 cf Primary=0.34 cfs 1,134 cf
Link PA-3:	Inflow=3.27 cfs 11,318 cf Primary=3.27 cfs 11,318 cf

Total Runoff Area = 152,082 sf Runoff Volume = 24,963 cf Average Runoff Depth = 1.97" 72.74% Pervious = 110,618 sf 27.26% Impervious = 41,464 sf

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SubcatchmentPRE-1.0:	Runoff Area=61,649 sf 17.89% Impervious Runoff Depth>2.02" Flow Length=218' Tc=8.6 min CN=45 Runoff=2.61 cfs 10,370 cf
SubcatchmentPRE-2.0:	Runoff Area=24,290 sf 39.91% Impervious Runoff Depth>3.97" Flow Length=266' Tc=7.3 min CN=62 Runoff=2.44 cfs 8,029 cf
SubcatchmentPRE-2.1:	Runoff Area=7,081 sf 22.82% Impervious Runoff Depth>2.80" Flow Length=213' Tc=5.0 min CN=52 Runoff=0.51 cfs 1,655 cf
SubcatchmentPRE-3.0:	Runoff Area=59,062 sf 32.39% Impervious Runoff Depth>3.26" Flow Length=237' Tc=7.3 min CN=56 Runoff=4.78 cfs 16,063 cf
Link PA-1:	Inflow=2.61 cfs 10,370 cf Primary=2.61 cfs 10,370 cf
Link PA-2:	Inflow=2.94 cfs 9,684 cf Primary=2.94 cfs 9,684 cf
Link PA-2.1:	Inflow=0.51 cfs 1,655 cf Primary=0.51 cfs 1,655 cf
Link PA-3:	Inflow=4.78 cfs 16,063 cf Primary=4.78 cfs 16,063 cf

Total Runoff Area = 152,082 sf Runoff Volume = 36,117 cf Average Runoff Depth = 2.85" 72.74% Pervious = 110,618 sf 27.26% Impervious = 41,464 sf

## 2.2 Pre-Development Watershed Plan



# Section 3 Post-Development Conditions

The post-development condition was analyzed by using the same points of analysis (PA-1, PA-2, PA-2.1 & PA-3.) In the post-development conditions, the total watersheds increased with six (6) total watershed areas. Stormwater runoff from these sub-catchment areas flow via sheet flow to Lafayette Road - US-Route 1, the conservation lands, Sagamore Creek or through the subsurface drainage systems prior to discharging into the proposed surface stormwater systems before ultimately discharging off site.

The point of analysis and its sub-catchment areas are depicted on the plan entitled "Post-Development Watershed Plan," Sheet C-802. The point of analysis and it's contributing watershed areas are described below:

#### Point of Analysis (PA-1)

Point of analysis 1 (PA-1) includes one (1) Post-Development Watershed Area (POST 1.0). The POST 1.0 area has significantly decreased and is only comprised of a small strip of land to the south of the proposed pavement section. The area is composed of grass and wooded areas.

#### Point of Analysis (PA-2)

Point of analysis 2 (PA-2) includes two (2) Post-Development Watershed Areas, both depicted as POST 2.0 on the plans. The first POST 2.0 area is abutting Lafayette Road - US-Route 1 and comprised of a small strip of land. This area is mainly composed of grass and wooded area with a small section of pavement.

The second POST 2.0 area is comprised of an area of land located centrally on site. This area is composed of grassed area along with a roof section from the existing church building on site.

#### Point of Analysis (PA-2.1)

Point of analysis 2.1 (PA-2.1) includes one (1) Post-Development Watershed Area (POST 2.1). POST 2.1 is mainly composed of impervious and grass area.

As stated in Section 2, this subcatchment area includes an existing catch basin within the DOT Drainage easement. In order to decrease flows entering this point of analysis, the area around the catch basin will be converted to an Infiltration Basin and the existing catch basin will be removed and an outlet control structure will be constructed in its place.

#### Point of Analysis (PA-3)

Point of analysis 3 (PA-3) includes two (2) Post-Development Watershed Areas (POST 3.0 & POST 3.1). POST 3.0 is primarily grass and woods area with small sections of existing pavement and roof from the existing Church building. The majority of this subcatchment area will remain undisturbed with no additional impervious surfaces being added. Runoff from this watershed sheet flows stormwater directly into Sagamore Creek and ultimately into the Piscataqua River.

POST 3.1 is the last and largest subcatchment on site and is composed of both the proposed buildings and a section of the existing church building. In addition to the proposed buildings, the remainder of the area is comprised of impervious pavement, concrete, and grassed area. All stormwater will sheet flow into the closed drainage system where it will be discharged into the Bioretention ISR located within the subcatchment, on the Northeastern corner of the development before ultimately discharging into Sagamore Creek, defined as PA-3.

## **3.1 Post-Development Calculations**



#### Area Listing (selected nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
69,136	39	>75% Grass cover, Good, HSG A (POST-1.0, POST-2.0, POST-2.1, POST-3.0, POST-3.1)
9,321	96	Gravel surface, HSG A (POST-3.1)
41,579	98	Paved parking, HSG A (POST-2.0, POST-2.1, POST-3.0, POST-3.1)
22,249	98	Unconnected roofs, HSG A (POST-2.0, POST-3.0, POST-3.1)
9,797	30	Woods, Good, HSG A (POST-1.0, POST-3.0)
152,082	67	TOTAL AREA

#### Soil Listing (selected nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
152,082	HSG A	POST-1.0, POST-2.0, POST-2.1, POST-3.0, POST-3.1
0	HSG B	
0	HSG C	
0	HSG D	
0	Other	
152,082		TOTAL AREA

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SubcatchmentPOST-1.0:	Runoff Area=2,180 sf 0.00% Impervious Runoff Depth=0.00" Flow Length=211' Slope=0.0140 '/' Tc=9.3 min CN=32 Runoff=0.00 cfs 0 cf
SubcatchmentPOST-2.0:	Runoff Area=11,987 sf 25.27% Impervious Runoff Depth>0.19" Flow Length=84' Tc=5.0 min UI Adjusted CN=48 Runoff=0.01 cfs 190 cf
SubcatchmentPOST-2.1:	Runoff Area=11,781 sf 53.68% Impervious Runoff Depth>1.19" Flow Length=327' Tc=5.0 min CN=71 Runoff=0.36 cfs 1,170 cf
SubcatchmentPOST-3.0:	Runoff Area=27,648 sf 26.07% Impervious Runoff Depth>0.22" Flow Length=230' Tc=5.0 min UI Adjusted CN=49 Runoff=0.05 cfs 501 cf
SubcatchmentPOST-3.1:	Runoff Area=98,486 sf 47.99% Impervious Runoff Depth>1.31" Flow Length=580' Tc=9.7 min CN=73 Runoff=2.92 cfs 10,778 cf
Pond 2P: Infiltration Basin	Peak Elev=22.67' Storage=903 cf Inflow=0.36 cfs 1,170 cf Outflow=0.01 cfs 294 cf
Pond 3P: RG 2.0	Peak Elev=34.56' Storage=5,840 cf Inflow=2.92 cfs 10,778 cf Outflow=0.39 cfs 5,085 cf
Link PA-1:	Inflow=0.00 cfs 0 cf Primary=0.00 cfs 0 cf
Link PA-2:	Inflow=0.02 cfs 484 cf Primary=0.02 cfs 484 cf
Link PA-2.1:	Inflow=0.01 cfs 294 cf Primary=0.01 cfs 294 cf
Link PA-3:	Inflow=0.41 cfs 5,586 cf Primary=0.41 cfs 5,586 cf

#### Total Runoff Area = 152,082 sf Runoff Volume = 12,639 cf Average Runoff Depth = 1.00" 58.03% Pervious = 88,254 sf 41.97% Impervious = 63,828 sf

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SubcatchmentPOST-1.0:	Runoff Area=2,180 sf 0.00% Impervious Runoff Depth>0.08" Flow Length=211' Slope=0.0140 '/' Tc=9.3 min CN=32 Runoff=0.00 cfs 15 cf
SubcatchmentPOST-2.0:	Runoff Area=11,987 sf 25.27% Impervious Runoff Depth>0.83" Flow Length=84' Tc=5.0 min UI Adjusted CN=48 Runoff=0.18 cfs 833 cf
SubcatchmentPOST-2.1:	Runoff Area=11,781 sf 53.68% Impervious Runoff Depth>2.59" Flow Length=327' Tc=5.0 min CN=71 Runoff=0.82 cfs 2,546 cf
SubcatchmentPOST-3.0:	Runoff Area=27,648 sf 26.07% Impervious Runoff Depth>0.90" Flow Length=230' Tc=5.0 min UI Adjusted CN=49 Runoff=0.48 cfs 2,066 cf
SubcatchmentPOST-3.1:	Runoff Area=98,486 sf 47.99% Impervious Runoff Depth>2.77" Flow Length=580' Tc=9.7 min CN=73 Runoff=6.38 cfs 22,745 cf
Pond 2P: Infiltration Basin	Peak Elev=22.86' Storage=1,204 cf Inflow=0.82 cfs 2,546 cf Outflow=0.13 cfs 1,643 cf
Pond 3P: RG 2.0	Peak Elev=34.62' Storage=6,023 cf Inflow=6.38 cfs 22,745 cf Outflow=7.87 cfs 16,924 cf
Link PA-1:	Inflow=0.00 cfs 15 cf Primary=0.00 cfs 15 cf
Link PA-2:	Inflow=0.21 cfs 2,476 cf Primary=0.21 cfs 2,476 cf
Link PA-2.1:	Inflow=0.13 cfs 1,643 cf Primary=0.13 cfs 1,643 cf
Link PA-3:	Inflow=8.22 cfs 18,990 cf Primary=8.22 cfs 18,990 cf

Total Runoff Area = 152,082 sf Runoff Volume = 28,205 cf Average Runoff Depth = 2.23" 58.03% Pervious = 88,254 sf 41.97% Impervious = 63,828 sf

#### Summary for Subcatchment POST-1.0:

Runoff = 0.00 cfs @ 15.32 hrs, Volume= 15 cf, Depth> 0.08" Routed to Link PA-1 :

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Yr Rainfall=5.62"

A	rea (sf)	CN	Description		
	0	98	Unconnecte	ed roofs, H	SG A
	0	98	Paved park	ing, HSG A	N Contraction of the second
	1,764	30	Woods, Go	od, HSG A	
	416	39	>75% Gras	s cover, Go	bod, HSG A
	2,180	32	Weighted A	verage	
	2,180		100.00% P	ervious Are	a
Тс	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
6.1	50	0.0140	0.14		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.68"
3.2	161	0.0140	0.83		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
9.3	211	Total			

#### Summary for Subcatchment POST-2.0:

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.18 cfs @ 12.11 hrs, Volume= 833 cf, Depth> 0.83" Routed to Link PA-2 :

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Yr Rainfall=5.62"

Area (sf)	CN	Adj	Description
2,461	98		Unconnected roofs, HSG A
568	98		Paved parking, HSG A
0	30		Woods, Good, HSG A
8,958	39		>75% Grass cover, Good, HSG A
11,987	54	48	Weighted Average, UI Adjusted
8,958			74.73% Pervious Area
3,029			25.27% Impervious Area
2,461			81.25% Unconnected

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.8	31	0.0050	0.67		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.68"
0.7	53	0.0300	1.21		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
1.5	84	Total, I	ncreased t	o minimum	Tc = 5.0 min
0.7	53 84	0.0300 Total, I	1.21 ncreased t	o minimum	Shallow Concentrated Flow,       Short Grass Pasture       Kv= 7.0 fps       Tc = 5.0 min

#### Summary for Subcatchment POST-2.1:

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.82 cfs @ 12.08 hrs, Volume= 2,546 cf, Depth> 2.59" Routed to Pond 2P : Infiltration Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Yr Rainfall=5.62"

A	rea (sf)	CN	Description		
	0	98	Unconnecte	ed roofs, HS	SG A
	6,324	98	Paved park	ing, HSG A	N Contraction of the second
	0	30	Woods, Go	od, HSG A	
	5,457	39	>75% Gras	s cover, Go	bod, HSG A
	11,781	71	Weighted A	verage	
	5,457		46.32% Pe	rvious Area	
	6,324		53.68% Imp	pervious Are	ea
Тс	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	) (ft/sec)	(cfs)	
0.9	100	0.0360	) 1.87		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.68"
0.9	209	0.0360	) 3.85		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
0.0	18	0.0250	) 8.48	6.66	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.011
1.8	327	Total,	Increased t	o minimum	Tc = 5.0 min

### Summary for Subcatchment POST-3.0:

[49] Hint: Tc<2dt may require smaller dt

Runoff = 0.48 cfs @ 12.11 hrs, Volume= 2,066 cf, Depth> 0.90" Routed to Link PA-3 :

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Yr Rainfall=5.62"

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Type III 24-hr 10-Yr Rainfall=5.62" Printed 5/20/2024 Page 3 2

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A	rea (sf)	CN /	Adj Desc	cription	
	2,345	98	Unco	onnected ro	oofs, HSG A
	4,862	98	Pave	ed parking,	HSG A
	8,033	30	Woo	ds, Good, I	HSG A
	12,408	39	>75%	% Grass co	ver, Good, HSG A
	27,648	52	49 Weig	hted Avera	age, UI Adjusted
	20,441		73.9	3% Perviou	is Area
	7,207		26.0	7% Impervi	ous Area
	2,345		32.5	4% Unconr	nected
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.6	21	0.0050	0.62		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.68"
1.6	209	0.0960	2.17		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
2.2	230	Total, I	ncreased t	o minimum	Tc = 5.0 min

#### Summary for Subcatchment POST-3.1:

[47] Hint: Peak is 214% of capacity of segment #3

6.38 cfs @ 12.14 hrs, Volume= 22,745 cf, Depth> 2.77" Runoff = Routed to Pond 3P : RG 2.0

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Yr Rainfall=5.62"

A	rea (sf)	CN	Description					
	17,443	98	Unconnected roofs. HSG A					
	29,825	98	Paved park	ing, HSG A	N N N N N N N N N N N N N N N N N N N			
	9,321	96	Gravel surf	ace, HSG A	A line line line line line line line line			
	41,897	39	>75% Gras	s cover, Go	bod, HSG A			
	98,486	73	Weighted A	verage				
	51,218		52.01% Pe	rvious Area				
	47,268		47.99% Im	pervious Ar	ea			
	17,443		36.90% Un	connected				
Tc	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	·			
5.2	50	0.0200	0.16		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.68"			
2.9	170	0.0200	0.99		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
1.6	360	0.0050	) 3.79	2.98	Pipe Channel,			
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
					n= 0.011			
9.7	580	Total						

#### Summary for Pond 2P: Infiltration Basin

Inflow Ar Inflow Outflow Primary Route	rea = = 0 = 0 = 0 ed to Link P/	11,781 sf, 53 ).82 cfs @ 12. ).13 cfs @ 12. ).13 cfs @ 12. A-2.1 :	3.68% Impervious, .08 hrs, Volume= .61 hrs, Volume= .61 hrs, Volume=	Inflow Depth > 2.5 2,546 cf 1,643 cf, A 1,643 cf	9" for 10-Yr event tten= 84%, Lag= 31.7 min
Routing Peak Ele Flood Ele	by Dyn-Stor ev= 22.86' @ ev= 25.00'	-Ind method, T ) 12.61 hrs St Surf.Area= 2,6	ime Span= 0.00-2 urf.Area= 1,609 sf 68 sf Storage= 5	4.00 hrs, dt= 0.05 hrs Storage= 1,204 cf 5,775 cf	S
Plug-Flo Center-o	w detention f-Mass det.	time= 211.4 mi time= 105.7 m	in calculated for 1 in ( 943.4 - 837.7	,640 cf (64% of inflow )	/)
Volume	Invert	Avail.Stora	age Storage Des	scription	
#1	22.00'	5,775	o cf Custom Sta	ige Data (Prismatic)	Listed below (Recalc)
Elevatio (fee	n Sı t)	urf.Area (sq-ft) (	Inc.Store cubic-feet) (	Cum.Store (cubic-feet)	
22.0	0	1,182	0	0	
25.0	0	2,668	5,775	5,775	
Device	Routing	Invert	Outlet Devices		
#1	Primary	19.37'	<b>15.0" Round Cu</b> Inlet / Outlet Inver n= 0.012 Concret	<b>Ivert</b> L= 27.0' Ke= ( t= 19.37' / 18.85' S= te pipe, finished, Flo	0.500 = 0.0193 '/'     Cc= 0.900 w Area= 1.23 sf
#2	Device 1	22.60'	4.0" Vert. Orifice	/Grate C= 0.600 L	imited to weir flow at low heads
#3	Device 1	23.50'	4.0" W x 4.0" H V Limited to weir flo	/ert. Orifice/Grate X w at low heads	<b>104.00</b> C= 0.600
Primary 1=Cu 2= 3=	OutFlow M lvert (Pass Orifice/Gra Orifice/Gra	lax=0.13 cfs @ es 0.13 cfs of 1 <b>te</b> (Orifice Con <b>te</b> ( Controls 0	2 12.61 hrs HW=2 0.01 cfs potential trols 0.13 cfs @ 1 .00 cfs)	2.86' TW=0.00' (Dy flow) .75 fps)	ynamic Tailwater)
			Summary for I	Pond 3P: RG 2.0	
[90] War	ning: Qout>	Qin may requir	e smaller dt or Fir	er Routing	
Inflow Ar Inflow Outflow	rea = = 6 = 7	98,486 sf, 47 3.38 cfs @ 12. 7.87 cfs @ 12.	7.99% Impervious, .14 hrs, Volume= .20 hrs, Volume=	Inflow Depth > 2.7 22,745 cf 16,924 cf, A	7" for 10-Yr event tten= 0%, Lag= 3.5 min

 =
 7.87 cfs @
 12.20 hrs, Volume=
 16,924 cf, Atten= 0%, Lag= 3.5 min

 =
 7.87 cfs @
 12.20 hrs, Volume=
 16,924 cf

Routed to Link PA-3 :

Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 34.62' @ 12.20 hrs Surf.Area= 3,120 sf Storage= 6,023 cf Flood Elev= 35.25' Surf.Area= 3,344 sf Storage= 7,263 cf

Plug-Flow detention time= 135.7 min calculated for 16,889 cf (74% of inflow)

Volume	Inve	ert Avai	I.Storage	Storage Descri	ption	
#1	29.5	50'	7,263 cf	Custom Stage	Data (Prismatic	Listed below (Recalc)
Elevatio (fee 29.5 31.0 33.0 35.0	on 50 00 00 00	Surf.Area (sq-ft) 2,177 2,177 2,177 3,344	Voids (%) 0.0 40.0 10.0 100.0	Inc.Store (cubic-feet) 0 1,306 435 5,521	Cum.Store (cubic-feet) 0 1,306 1,742 7,263	
Device	Routing	In	vert Ou	tlet Devices		
#1	Primary	31	.00' <b>15.</b> Inle n=	<b>0" Round Culve</b> et / Outlet Invert= 3 0.012 Concrete p	rt L= 30.0' Ke= 31.00' / 30.50' S bipe. finished. Flo	0.500 = 0.0167 '/' Cc= 0.900 ow Area= 1.23 sf
#2	Device 1	30	.00' <b>1.2</b>	" Vert. Orifice/Gr	rate C= 0.600 L	imited to weir flow at low heads
#3	Device 2	33	.00' <b>10.</b>	000 in/hr Exfiltra	tion over Surfac	e area above 33.00'
#4	Device 1	34	.55' <b>4.0</b> Lim	<b>" x 4.0" Horiz. O</b> ited to weir flow a	ea = 2,177 st rifice/Grate X 10 at low heads	<b>4.00</b> C= 0.600

Center-of-Mass det. time= 47.1 min (883.7 - 836.6)

Primary OutFlow Max=7.77 cfs @ 12.20 hrs HW=34.62' TW=0.00' (Dynamic Tailwater)

-1=Culvert (Passes 7.77 cfs of 10.22 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.07 cfs @ 9.16 fps) -3=Exfiltration (Passes 0.07 cfs of 0.22 cfs potential flow)

-4=Orifice/Grate (Weir Controls 7.69 cfs @ 0.84 fps)

#### Summary for Link PA-1:

Inflow .	Area	=	2,180 sf,	0.00% Ir	mpervious,	Inflow Depth >	0.08"	for 10	0-Yr event
Inflow		=	0.00 cfs @	15.32 hrs,	Volume=	15 c	f		
Primar	У	=	0.00 cfs @	15.32 hrs,	Volume=	15 c	f, Atter	n= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

#### Summary for Link PA-2:

Inflow /	Area	ı =	23,768 sf,	, 39.35% Ir	npervious,	Inflow Depth >	1.25"	for 10	0-Yr event
Inflow		=	0.21 cfs @	12.42 hrs,	Volume=	2,476 c	f		
Primar	У	=	0.21 cfs @	12.42 hrs,	Volume=	2,476 c	f, Atte	n= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

#### Summary for Link PA-2.1:

11,781 sf, 53.68% Impervious, Inflow Depth > 1.67" for 10-Yr event Inflow Area = 0.13 cfs @ 12.61 hrs, Volume= 1,643 cf Inflow = 0.13 cfs @ 12.61 hrs, Volume= Primary = 1,643 cf, Atten= 0%, Lag= 0.0 min Routed to Link PA-2 :

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

### Summary for Link PA-3:

Inflow A	rea =	126,134 sf, 43.19% Impervious,	Inflow Depth > 1.81"	for 10-Yr event
Inflow	=	8.22 cfs @ 12.20 hrs, Volume=	18,990 cf	
Primary	- =	8.22 cfs @ 12.20 hrs, Volume=	18,990 cf, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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SubcatchmentPOST-1.0:	Runoff Area=2,180 sf 0.00% Impervious Runoff Depth>0.34" Flow Length=211' Slope=0.0140 '/' Tc=9.3 min CN=32 Runoff=0.00 cfs 62 cf
SubcatchmentPOST-2.0:	Runoff Area=11,987 sf 25.27% Impervious Runoff Depth>1.56" Flow Length=84' Tc=5.0 min UI Adjusted CN=48 Runoff=0.43 cfs 1,556 cf
SubcatchmentPOST-2.1:	Runoff Area=11,781 sf 53.68% Impervious Runoff Depth>3.83" Flow Length=327' Tc=5.0 min CN=71 Runoff=1.22 cfs 3,761 cf
SubcatchmentPOST-3.0:	Runoff Area=27,648 sf 26.07% Impervious Runoff Depth>1.65" Flow Length=230' Tc=5.0 min UI Adjusted CN=49 Runoff=1.07 cfs 3,795 cf
SubcatchmentPOST-3.1:	Runoff Area=98,486 sf 47.99% Impervious Runoff Depth>4.04" Flow Length=580' Tc=9.7 min CN=73 Runoff=9.33 cfs 33,165 cf
Pond 2P: Infiltration Basin	Peak Elev=23.14' Storage=1,677 cf Inflow=1.22 cfs 3,761 cf Outflow=0.26 cfs 2,840 cf
Pond 3P: RG 2.0	Peak Elev=34.63' Storage=6,059 cf Inflow=9.33 cfs 33,165 cf Outflow=9.97 cfs 27,341 cf
Link PA-1:	Inflow=0.00 cfs 62 cf Primary=0.00 cfs 62 cf
Link PA-2:	Inflow=0.56 cfs 4,396 cf Primary=0.56 cfs 4,396 cf
Link PA-2.1:	Inflow=0.26 cfs 2,840 cf Primary=0.26 cfs 2,840 cf
Link PA-3:	Inflow=10.84 cfs 31,136 cf Primary=10.84 cfs 31,136 cf

Total Runoff Area = 152,082 sf Runoff Volume = 42,339 cf Average Runoff Depth = 3.34" 58.03% Pervious = 88,254 sf 41.97% Impervious = 63,828 sf

P5118-001_POST	Тур
Prepared by Tighe & Bond Consulting	
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SubcatchmentPOST-1.0:	Runoff Area=2,180 sf 0.00% Impervious Runoff Depth>0.71" Flow Length=211' Slope=0.0140 '/' Tc=9.3 min CN=32 Runoff=0.02 cfs 130 cf
SubcatchmentPOST-2.0:	Runoff Area=11,987 sf 25.27% Impervious Runoff Depth>2.35" Flow Length=84' Tc=5.0 min UI Adjusted CN=48 Runoff=0.70 cfs 2,350 cf
SubcatchmentPOST-2.1:	Runoff Area=11,781 sf 53.68% Impervious Runoff Depth>5.04" Flow Length=327' Tc=5.0 min CN=71 Runoff=1.60 cfs 4,947 cf
SubcatchmentPOST-3.0:	Runoff Area=27,648 sf 26.07% Impervious Runoff Depth>2.46" Flow Length=230' Tc=5.0 min UI Adjusted CN=49 Runoff=1.71 cfs 5,678 cf
SubcatchmentPOST-3.1:	Runoff Area=98,486 sf 47.99% Impervious Runoff Depth>5.27" Flow Length=580' Tc=9.7 min CN=73 Runoff=12.15 cfs 43,286 cf
Pond 2P: Infiltration Basin	Peak Elev=23.44' Storage=2,209 cf Inflow=1.60 cfs 4,947 cf Outflow=0.34 cfs 4,013 cf
Pond 3P: RG 2.0	Peak Elev=34.79' Storage=6,557 cf Inflow=12.15 cfs 43,286 cf Outflow=10.50 cfs 37,459 cf
Link PA-1:	Inflow=0.02 cfs 130 cf Primary=0.02 cfs 130 cf
Link PA-2:	Inflow=0.94 cfs 6,362 cf Primary=0.94 cfs 6,362 cf
Link PA-2.1:	Inflow=0.34 cfs 4,013 cf Primary=0.34 cfs 4,013 cf
Link PA-3:	Inflow=12.15 cfs 43,137 cf Primary=12.15 cfs 43,137 cf

Total Runoff Area = 152,082 sf Runoff Volume = 56,391 cf Average Runoff Depth = 4.45" 58.03% Pervious = 88,254 sf 41.97% Impervious = 63,828 sf

## 3.2 Post-Development Watershed Plan



iaved: 5/20/2024

12.15

10.84

# Section 4 **Peak Rate Comparison**

The following table summarizes and compares the pre- and post-development peak runoff rates from the 2-year, 10-year, 25-year and 50-year storm events at the point of analysis.

#### **Comparison of Pre- and Post-Development Flows (CFS)** 2-Year 10-Year 25-Year 50-Year Storm Storm Storm Storm **Pre-Development Watershed** 0.02 0.51 2.61 PA-1 1.48 PA-2 0.36 1.24 2.08 2.94 PA-2.1 0.51 0.02 0.17 0.34 PA-3 0.38 1.81 3.27 4.78 **Post-Development Watershed** PA-1 0.00 0.00 0.00 0.02 PA-2 0.02 0.21 0.56 0.94 PA-2.1 0.01 0.13 0.26 0.34

The Peak Runoff Control Requirements of Env-Wg 1507.06 are not required to be met for point of analysis 3 (PA-3) per NHDES Alteration of Terrain regulation Env-Wg 1507.06(d).

0.41

8.22

Table 4.1

PA-3

# Section 5 Mitigation Description

The stormwater management system has been designed to provide stormwater treatment as required by the City of Portsmouth Site Review Regulations and NHDES AoT Regulations (Env-Wq 1500).

## **5.1 Pre-Treatment Methods for Protecting Water Quality**

Pre-treatment for the stormwater filtration systems consists of off-line deep sump catch basins.

## 5.2 Treatment Methods for Protecting Water Quality.

The runoff from proposed impervious areas will be treated using a Bioretention ISR and an Infiltration Basin. These BMPs are sized to treat the Water Quality Flow of their respective subcatchment areas. The systems are outfitted with an outlet control structure to bypass the peak flows away from treatment. The BMP worksheet for this treatment practice has been included in Section 6 of this report.

The proposed stormwater management system is required to remove 80% of the annual Total Suspended Soils (TSS) loads and 50% of the annual Total Nitrogen (TN) loads per the City of Portsmouth's Site Plan regulations, Section 7.6.2.1.a.i. As shown in table 5.1 the pollutant removal efficiencies for the proposed treatment system exceeds the City of Portsmouth's removal requirements.

Table 5.1 – Pollutant Removal Efficiencies								
ВМР	Total Suspended Solids	Total Nitrogen	Total Phosphorus					
Bioretention ISR <sup>1</sup>	90%	65%	65%					

Table 5.2 – Pollutant Removal Efficiencies								
BMP Total Suspended Total Nitrogen Total P								
Infiltration Basin <sup>1</sup>	90%	60%	65%					

1. Pollutant removal calculations for Bioretention ISR and Infiltration Basin with deep sump catchbasin pretreatment are shown in Table 5.3 & 5.4.

Table 5.3 – Pollutant Removal Calculations								
Bioretention ISR								
BMP	TSS Removal Rate	Starting TSS Load	TSS Removed	Remaining TSS Load				
Deep Sump Catchbasin w/Hood <sup>1</sup>	0.15	1.00	0.15	0.85				
Bioretention ISR <sup>2</sup>	0.90	0.85	0.77	0.08				
	Total S	uspended Soli	ds Removed:	92%				
	TN Removal Rate	Starting TN Load	TN Removed	Remaining TN Load				
Deep Sump Catchbasin w/Hood <sup>1</sup>	0.05	1.00	0.05	0.95				
Bioretention ISR <sup>2</sup>	0.65	0.95	0.62	0.33				
		Total Nitrog	en Removed:	67%				
	TP Removal Rate	Starting TP Load	TP Removed	Remaining TP Load				
Deep Sump Catchbasin w/Hood <sup>1</sup>	0.05	1.00	0.05	0.95				
Bioretention ISR <sup>2</sup>	0.65	0.95	0.62	0.33				
	Total Phosphorus Removed: 67%							

Table 5.4 – Pollutant Removal Calculations								
Infiltration Basin								
BMP	TSS Removal Rate	Starting TSS Load	TSS Removed	Remaining TSS Load				
Deep Sump Catchbasin w/Hood <sup>1</sup>	0.15	1.00	0.15	0.85				
Infiltration Basin <sup>3</sup>	0.90	0.85	0.77	0.08				
	Total Su	uspended Soli	ds Removed:	92%				
	TN Removal Rate	Starting TN Load	TN Removed	Remaining TN Load				
Deep Sump Catchbasin w/Hood <sup>1</sup>	0.05	1.00	0.05	0.95				
Infiltration Basin <sup>3</sup>	0.60	0.95	0.57	0.38				
		Total Nitrog	en Removed:	62%				
	TP Removal Rate	Starting TP Load	TP Removed	Remaining TP Load				
Deep Sump Catchbasin w/Hood <sup>1</sup>	0.05	1.00	0.05	0.95				
Infiltration Basin <sup>3</sup>	0.65	0.95	0.62	0.33				
	Total Phosphorus Removed: 67%							

1. Pollutant removal efficiencies from NH Stormwater Manual Volume 2, Appendix B.

2. Pollutant removal efficiencies from NH Stormwater Manual Volume 2, Appendix B.

3. Pollutant removal efficiencies from NH Stormwater Manual Volume 2, Appendix B.

# Section 6 BMP Worksheet


## BIORETENTION SYSTEM WITH INTERNAL STORAGE RESERVOIR (UNH Stormwater Center Specification)

Type/Node Name:	Rain Garden ISR									
	Enter the node name in the drainage analysis if applicable.									
2.26 ac	A = Area draining to the practice									
1.08 ac	A <sub>I</sub> = Impervious area draining to the practice									
0.48 decimal	I = Percent impervious area draining to the practice, in decimal form									
0.48 unitless	Rv = Runoff coefficient = 0.05 + (0.9 x l)									
1.09 ac-in	WQV= 1" x Rv x A									
3,939 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")									
394 cf	10% x WQV (check calc for sediment forebay)									
985 cf	25% x WQV (check calc for water stored in saturated zone)									
Offline Deep Sump	Method of Pretreatment									
N/A cf	If pretrt is sed forebay: V <sub>SED</sub> (sediment forebay volume)	<u>&gt;</u> 10%WQV								
4,075 cf	Volume below lowest orifice <sup>1</sup>	<u>&gt;</u> 100%WQV								
1,306 cf	Water stored in voids of saturated zone	<u>&gt;</u> 26%WQV								
0.09 cfs	2Q <sub>avg</sub> = 2* WQV / 24 hrs * (1hr / 3600 sec) <sup>2</sup>									
34.55 ft	E <sub>WQV</sub> = Elevation of WQV (attach stage-storage table)									
0.07 cfs	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table)	< 2Q <sub>WQV</sub>								
31.26 hours	$T_{ED}$ = Drawdown time of extended detention = 2WQV/Q <sub>WQV</sub>	<u>&gt;</u> 24-hrs								
18.00 in	Depth of Filter Media	<u>&gt;</u> 18"								
3.00 :1	Pond side slopes	<u>&gt;</u> 3:1								
	What mechanism is proposed to prevent the outlet structure from clo	ogging (applicable for								
Trash Rack	orifices/weirs with a dimension of <6")?									
34.79 ft	Peak elevation of the 50-year storm event ( $E_{50}$ )									
35.25 ft	Berm elevation of the pond									
YES	$E_{50} \leq$ the berm elevation?	← yes								

1. Volume stored above the wetland soil and below the high flow by-pass.

#### **Designer's Notes:**



### INFILTRATION PRACTICE CRITERIA (Env-Wq 1508.06)

#### Type/Node Name: Infiltration Basin #1

Enter the type of infiltration practice (e.g., basin, trench) and the node name in the drainage analysis, if applicable.

	Have you reviewed Env-Wq 1508.06(a) to ensure that infiltration is allowed?	← yes
0.27 ac	A = Area draining to the practice	-
0.15 ac	A <sub>I</sub> = Impervious area draining to the practice	
0.56 decimal	I = Percent impervious area draining to the practice, in decimal form	
0.55 unitless	Rv = Runoff coefficient = 0.05 + (0.9 x l)	
0.15 ac-in	WQV= 1" x Rv x A	
539 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
135 cf	25% x WQV (check calc for sediment forebay volume)	
Deep Sump CB	Method of pretreatment? (not required for clean or roof runoff)	
N/A cf	V <sub>SED</sub> = Sediment forebay volume, if used for pretreatment	> 25%WQV
2,525 cf	V = Volume <sup>1</sup> (attach a stage-storage table)	> WQV
1,182 sf	A <sub>SA</sub> = Surface area of the bottom of the pond	_
iph	Ksat <sub>DESIGN</sub> = Design infiltration rate <sup>2</sup>	
- hours	$I_{DRAIN} = Drain time = V / (A_{SA} * I_{DESIGN})$	<u>&lt;</u> 72-hrs
22.00 feet	E <sub>BTM</sub> = Elevation of the bottom of the basin	
feet	$E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test p	oit)
feet	$E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test	: pit)
22.00 feet	D <sub>SHWT</sub> = Separation from SHWT	<u>&gt;</u> * <sup>3</sup>
22.0 feet	D <sub>ROCK</sub> = Separation from bedrock	<u>&gt;</u> * <sup>3</sup>
ft	D <sub>amend</sub> = Depth of amended soil, if applicable due high infiltation rate	> 24"
ft	$D_T$ = Depth of trench, if trench proposed	4 - 10 ft
N/A Yes/No	If a trench or underground system is proposed, has observation well been provid	ed? <b>←yes</b>
N/A	If a trench is proposed, does materialmeet Env-Wq 1508.06(k)(2) requirements. <sup>4</sup>	← yes
Yes Yes/No	If a basin is proposed, Is the perimeter curvilinear, and basin floor flat?	← yes
3.0 :1	If a basin is proposed, pond side slopes.	<u>&gt;</u> 3:1
22.86 ft	Peak elevation of the 10-year storm event (infiltration can be used in analysis)	
23.44 ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
25.00 ft	Elevation of the top of the practice (if a basin, this is the elevation of the berm)	
YES	10 peak elevation ≤ Elevation of the top of the trench? <sup>5</sup>	← yes
YES	If a basin is proposed, 50-year peak elevation $\leq$ Elevation of berm?	← yes

1. Volume below the lowest invert of the outlet structure and excludes forebay volume

2. Ksat<sub>DESIGN</sub> includes a factor of safety. See Env-Wq 1504.14 for requirements for determining the infiltr. rate

3. 1' separation if treatment not required; 4' for treatment in GPAs & WSIPAs; & 3' in all other areas.

4. Clean, washed well graded diameter of 1.5 to 3 inches above the in-situ soil.

5. If 50-year peak elevation exceeds top of trench, the overflow must be routed in HydroCAD as secondary discharge.

#### **Designer's Notes:**

#### Elevation Surface Storage Elevation Surface Storage (cubic-feet) (sq-ft) (cubic-feet) (feet) (sq-ft) (feet) 22.00 1,182 24.60 2,470 4,747 0 22.05 1,207 60 24.65 2,495 4,872 22.10 1,232 2,519 4,997 121 24.70 22.15 1,256 183 24.75 2,544 5,123 22.20 1,281 246 24.80 2,569 5,251 22.25 1,306 2,594 311 24.85 5,380 22.30 1,331 377 24.90 2,618 5,511 22.35 1,355 444 24.95 2,643 5,642 22.40 1,380 512 25.00 2,668 5,775 22.45 1,405 582 22.50 1,430 653 1,454 22.55 725 22.60 1,479 798 22.65 1,504 873 1,529 949 22.70 22.75 1,554 1,026 22.80 1,578 1,104 22.85 1,603 1,184 22.90 1,264 1,628 22.95 1,653 1,346 23.00 1,677 1,430 23.05 1,702 1,514 23.10 1,727 1,600 23.15 1,752 1,687 23.20 1,776 1,775 23.25 1,801 1,864 23.30 1,826 1,955 23.35 1,851 2,047 23.40 1,875 2,140 23.45 1,900 2,235 23.50 1,925 2,330 1,950 23.55 2,427 23.60 1,975 2,525 23.65 1,999 2,625 23.70 2,024 2,725 2,049 2,827 23.75 2,930 23.80 2,074 STORAGE BELOW LOWEST 23.85 2,098 3.034 23.90 3,140 2,123 **INVERT OF OUTLET** 23.95 3,247 2,148 CONTROL STRUCTURE 24.00 3,355 2,173 24.05 3,464 2,197 24.10 2,222 3,574 24.15 2.247 3.686 24.20 2,272 3,799 24.25 2,297 3,913 24.30 2,321 4,029 24.35 2.346 4.145 24.40 2,371 4.263 24.45 4,383 2,396 24.50 2,420 4,503 24.55 2,445 4,625

#### Stage-Area-Storage for Pond 2P: Infiltration Basin

# **Tighe&Bond**

**APPENDIX A** 



United States Department of Agriculture

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants Custom Soil Resource Report for Rockingham County, New Hampshire



# Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

#### Custom Soil Resource Report Soil Map



	MAP L	EGEND		MAP INFORMATION					
Area of Int	erest (AOI)	3	Spoil Area	The soil surveys that comprise your AOI were mapped at					
	Area of Interest (AOI)	۵	Stony Spot	1:24,000.					
Soils		0	Very Stony Spot	Warning: Soil Man may not be valid at this scale					
	Soil Map Unit Polygons	w.	Wet Spot	Warning. Soli wap may not be valid at this scale.					
~	Soil Map Unit Lines	8	Other	Enlargement of maps beyond the scale of mapping can cause					
	Soil Map Unit Points	-	Special Line Features	misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of					
Special	Point Features	Water Fea	tures	contrasting soils that could have been shown at a more detailed					
అ	Blowout		Streams and Canals	scale.					
$\boxtimes$	Borrow Pit	Transport	ation	Please rely on the bar scale on each man sheet for man					
×	Clay Spot	+++	Rails	measurements.					
$\diamond$	Closed Depression	~	Interstate Highways	Course of Many Matural Decourses Concernation Coming					
X	Gravel Pit	~	US Routes	Web Soil Survey URL:					
0 0 0	Gravelly Spot	~	Major Roads	Coordinate System: Web Mercator (EPSG:3857)					
0	Landfill		Local Roads	Maps from the Web Soil Survey are based on the Web Mercator					
A	Lava Flow	Backgrou	nd	projection, which preserves direction and shape but distorts					
عله	Marsh or swamp	Backgrou	Aerial Photography	distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more					
*	Mine or Quarry			accurate calculations of distance or area are required.					
6	Miscellaneous Water			This product is generated from the USDA-NRCS certified data as					
õ	Perennial Water			of the version date(s) listed below.					
Š	Rock Outcrop								
*	Saline Spot			Soil Survey Area: Rockingnam County, New Hampsnire Survey Area Data: Version 26, Aug 22, 2023					
T	Sandy Spot								
°°0	Sandy Opot			Soil map units are labeled (as space allows) for map scales 1:50 000 or larger					
-	Severely Eroded Spot								
0	Sinknole			Date(s) aerial images were photographed: Jun 19, 2020—Sep					
≫	Slide or Slip			20, 2020					
ø	Sodic Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.					

	-		
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
26A	Windsor loamy sand, 0 to 3 percent slopes	4.5	45.0%
26C	Windsor loamy sand, 8 to 15 percent slopes	2.8	28.2%
510B	Hoosic gravelly fine sandy loam, 3 to 8 percent slopes	0.0	0.0%
597	Westbrook mucky peat, 0 to 2 percent slopes, very frequently flooded	0.0	0.3%
699	Urban land	2.6	26.5%
Totals for Area of Interest		10.0	100.0%

# Map Unit Legend

## **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## **Rockingham County, New Hampshire**

#### 26A—Windsor loamy sand, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2svkg Elevation: 0 to 990 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Farmland of local importance

#### **Map Unit Composition**

Windsor, loamy sand, and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### Description of Windsor, Loamy Sand

#### Setting

Landform: Dunes, deltas, outwash terraces, outwash plains Landform position (three-dimensional): Tread, riser Down-slope shape: Convex, linear Across-slope shape: Convex, linear Parent material: Loose sandy glaciofluvial deposits derived from granite and/or loose sandy glaciofluvial deposits derived from schist and/or loose sandy glaciofluvial deposits derived from gneiss

#### **Typical profile**

O - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loamy sand

Bw - 3 to 25 inches: loamy sand

C - 25 to 65 inches: sand

#### Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 3.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: A Ecological site: F144AY022MA - Dry Outwash Hydric soil rating: No

#### **Minor Components**

#### Deerfield, loamy sand

Percent of map unit: 10 percent Landform: Outwash plains, terraces, deltas Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread, talf Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### Hinckley, loamy sand

Percent of map unit: 5 percent Landform: Outwash plains, eskers, kames, deltas Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Crest, head slope, nose slope, side slope, rise Down-slope shape: Convex Across-slope shape: Linear, convex Hydric soil rating: No

#### 26C—Windsor loamy sand, 8 to 15 percent slopes

#### Map Unit Setting

National map unit symbol: 2svkq Elevation: 0 to 1,260 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Windsor and similar soils:* 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Windsor**

#### Setting

Landform: — error in exists on — Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, riser Down-slope shape: Convex

Across-slope shape: Linear, convex

*Parent material:* Loose sandy glaciofluvial deposits derived from granite and/or loose sandy glaciofluvial deposits derived from schist and/or loose sandy glaciofluvial deposits derived from gneiss

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

*Ap* - 1 to 11 inches: loamy sand *Bw* - 11 to 31 inches: loamy sand *C* - 31 to 65 inches: sand

#### **Properties and qualities**

Slope: 8 to 15 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 4.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: A Ecological site: F144AY022MA - Dry Outwash Hydric soil rating: No

#### **Minor Components**

#### Hinckley

Percent of map unit: 10 percent Landform: Outwash plains, eskers, kames, deltas Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Crest, head slope, nose slope, side slope, rise Down-slope shape: Convex Across-slope shape: Linear, convex Hydric soil rating: No

#### Deerfield

Percent of map unit: 5 percent Landform: Outwash plains, terraces, deltas Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread, talf Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### 510B—Hoosic gravelly fine sandy loam, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 9cp4 Elevation: 100 to 1,100 feet Mean annual precipitation: 30 to 50 inches *Mean annual air temperature:* 45 to 50 degrees F *Frost-free period:* 135 to 190 days *Farmland classification:* Farmland of statewide importance

#### Map Unit Composition

*Hoosic and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Hoosic**

#### Setting

Parent material: Outwash

#### **Typical profile**

*H1 - 0 to 8 inches:* gravelly fine sandy loam *H2 - 8 to 15 inches:* very gravelly fine sandy loam *H3 - 15 to 60 inches:* very gravelly coarse sand

#### **Properties and qualities**

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (2.00 to 20.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Very low (about 2.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s Hydrologic Soil Group: A Ecological site: F144AY022MA - Dry Outwash Hydric soil rating: No

#### **Minor Components**

#### Not named

*Percent of map unit:* 10 percent *Hydric soil rating:* No

# 597—Westbrook mucky peat, 0 to 2 percent slopes, very frequently flooded

#### Map Unit Setting

National map unit symbol: 2tyqf Elevation: 0 to 10 feet Mean annual precipitation: 36 to 71 inches *Mean annual air temperature:* 39 to 55 degrees F *Frost-free period:* 140 to 250 days *Farmland classification:* Not prime farmland

#### Map Unit Composition

*Westbrook and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### Description of Westbrook

#### Setting

Landform: Tidal marshes Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear Parent material: Partly-decomposed herbaceous organic material over loamy mineral material

#### **Typical profile**

Oe - 0 to 19 inches: mucky peat Cg - 19 to 59 inches: silt loam

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00 to 14.17 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: Very frequent
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Maximum salinity: Nonsaline to strongly saline (0.7 to 111.6 mmhos/cm)
Sodium adsorption ratio, maximum: 33.0
Available water supply, 0 to 60 inches: High (about 9.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8w Hydrologic Soil Group: B/D Ecological site: R144AY002CT - Tidal Salt High Marsh mesic very frequently flooded, R144AY001CT - Tidal Salt Low Marsh mesic very frequently flooded Hydric soil rating: Yes

#### Minor Components

#### lpswich

Percent of map unit: 5 percent Landform: Tidal marshes Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear Ecological site: R144AY002CT - Tidal Salt High Marsh mesic very frequently flooded, R144AY001CT - Tidal Salt Low Marsh mesic very frequently flooded Hydric soil rating: Yes

#### Pawcatuck

Percent of map unit: 5 percent Landform: Tidal marshes Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear Ecological site: R144AY002CT - Tidal Salt High Marsh mesic very frequently flooded, R144AY001CT - Tidal Salt Low Marsh mesic very frequently flooded Hydric soil rating: Yes

#### 699—Urban land

#### **Map Unit Composition**

Urban land: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Minor Components**

#### Not named

Percent of map unit: 15 percent Hydric soil rating: No

# Soil Information for All Uses

## **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

## **Soil Qualities and Features**

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

## Hydrologic Soil Group

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.





## Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
26A	Windsor loamy sand, 0 to 3 percent slopes	A	4.5	45.0%
26C	Windsor loamy sand, 8 to 15 percent slopes	A	2.8	28.2%
510B	Hoosic gravelly fine sandy loam, 3 to 8 percent slopes	A	0.0	0.0%
597	Westbrook mucky peat, 0 to 2 percent slopes, very frequently flooded	B/D	0.0	0.3%
699	Urban land		2.6	26.5%
Totals for Area of Intere	est	10.0	100.0%	

## Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

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# **Tighe&Bond**

**APPENDIX B** 

# **Extreme Precipitation Tables**

## Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Metadata for Point									
Smoothing	Yes								
State									
Location									
Latitude	43.052 degrees North								
Longitude	70.768 degrees West								
Elevation	0 feet								
Date/Time	Tue Oct 10 2023 16:27:23 GMT-0400 (Eastern Daylight Time)								

## **Extreme Precipitation Estimates**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.50	0.65	0.82	1.04	1yr	0.70	0.98	1.21	1.57	2.04	2.67	2.93	1yr	2.36	2.82	3.23	3.96	4.57	1yr
2yr	0.32	0.50	0.62	0.82	1.02	1.30	2yr	0.88	1.18	1.52	1.94	2.50	3.22	3.58	2yr	2.85	3.45	3.95	4.70	5.35	2yr
5yr	0.37	0.58	0.73	0.98	1.25	1.61	5yr	1.08	1.47	1.89	2.44	3.15	4.08	4.60	5yr	3.61	4.42	5.06	5.96	6.73	5yr
10yr	0.41	0.65	0.82	1.12	1.45	1.89	10yr	1.25	1.73	2.24	2.90	3.76	4.89	5.55	10yr	4.33	5.34	6.11	7.14	8.01	10yr
25yr	0.48	0.76	0.97	1.34	1.78	2.34	25yr	1.53	2.15	2.78	3.64	4.76	6.20	7.13	25yr	5.49	6.86	7.85	9.07	10.10	25yr
50yr	0.54	0.86	1.10	1.54	2.08	2.76	50yr	1.79	2.53	3.30	4.34	5.68	7.42	8.62	50yr	6.57	8.29	9.48	10.87	12.03	50yr
100yr	0.60	0.97	1.25	1.78	2.42	3.27	100yr	2.09	2.99	3.92	5.18	6.80	8.90	10.43	100yr	7.87	10.03	11.46	13.04	14.35	100yr
200yr	0.68	1.10	1.43	2.05	2.83	3.85	200yr	2.45	3.53	4.63	6.15	8.12	10.66	12.61	200yr	9.44	12.13	13.85	15.64	17.11	200yr
500yr	0.80	1.32	1.72	2.49	3.49	4.78	500yr	3.01	4.39	5.79	7.74	10.27	13.55	16.22	500yr	11.99	15.60	17.81	19.91	21.61	500yr

## **Lower Confidence Limits**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.23	0.36	0.44	0.59	0.72	0.88	1yr	0.63	0.87	0.92	1.33	1.68	2.25	2.53	1yr	1.99	2.43	2.88	3.18	3.91	1yr
2yr	0.32	0.49	0.60	0.81	1.00	1.19	2yr	0.86	1.16	1.37	1.82	2.34	3.07	3.47	2yr	2.72	3.34	3.84	4.57	5.10	2yr
5yr	0.35	0.54	0.67	0.92	1.17	1.40	5yr	1.01	1.37	1.61	2.12	2.73	3.81	4.22	5yr	3.37	4.06	4.74	5.57	6.28	5yr
10yr	0.39	0.59	0.74	1.03	1.33	1.60	10yr	1.15	1.57	1.81	2.39	3.06	4.40	4.90	10yr	3.89	4.71	5.49	6.46	7.24	10yr
25yr	0.44	0.67	0.83	1.19	1.57	1.90	25yr	1.35	1.86	2.10	2.75	3.53	4.75	5.95	25yr	4.20	5.72	6.72	7.87	8.75	25yr
50yr	0.48	0.74	0.92	1.32	1.77	2.17	50yr	1.53	2.12	2.35	3.07	3.93	5.37	6.88	50yr	4.75	6.61	7.83	9.14	10.11	50yr
100yr	0.54	0.81	1.02	1.47	2.02	2.47	100yr	1.74	2.42	2.63	3.41	4.35	6.04	7.95	100yr	5.35	7.65	9.12	10.64	11.68	100yr
200yr	0.60	0.90	1.14	1.64	2.29	2.82	200yr	1.98	2.76	2.94	3.77	4.79	6.78	9.19	200yr	6.00	8.84	10.63	12.40	13.51	200yr
500yr	0.69	1.03	1.32	1.92	2.73	3.37	500yr	2.36	3.30	3.42	4.30	5.45	7.90	11.13	500yr	7.00	10.70	13.00	15.20	16.37	500yr

Coastal and Great Bay Region Precipitation Increase									
	24-hr Storm Event (in.)	24-hr Storm Event + 15% (in.)							
1 Year	2.67	3.07							
2 Year	3.22	3.70							
10 Year	4.89	5.62							
25 Year	6.20	7.13							
50 Year	7.42	8.53							

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Proposed Mixed Use Development 1035 Lafayette Rd Portsmouth, NH

# Long-Term Operation & Maintenance Plan

100% Recyclable 🏠

**Portsmouth Housing Authority** 

May 20, 2024



# Section 1 Long-Term Operation & Maintenance Plan

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### **Section 2 Invasive Species**

### Section 3 Annual Updates and Log Requirements

# Section 1 Long-Term Operation & Maintenance Plan

It is the intent of this Operation and Maintenance Plan to identify the areas of this site that need special attention and consideration, as well as implement a plan to assure routine maintenance. By identifying the areas of concern as well as implementing a frequent and routine maintenance schedule the site will maintain a high-quality stormwater runoff.

# 1.1 Contact/Responsible Party

Portsmouth Housing Authority 245 Middle Street Portsmouth, NH 03801

(Note: The contact information for the Contact/Responsible Party shall be kept current. If ownership changes, the Operation and Maintenance Plan must be transferred to the new party.)

# **1.2 Maintenance Items**

Maintenance of the following items shall be recorded:

- Litter/Debris Removal
- Landscaping
- Catchbasin Cleaning
- Pavement Sweeping
- Bioretention ISR Maintenance
- Sediment Basin Maintenance
- Infiltration Basin

The following maintenance items and schedule represent the minimum action required. Periodic site inspections shall be conducted, and all measures must be maintained in effective operating condition. The following items shall be observed during site inspection and maintenance:

- Inspect vegetated areas, particularly slopes and embankments for areas of erosion. Replant and restore as necessary
- Inspect catch basins for sediment buildup
- Inspect site for trash and debris

# **1.3 Overall Site Operation & Maintenance Schedule**

Maintenance Item	Frequency of Maintenance
Litter/Debris Removal	Weekly
Pavement Sweeping - Sweep impervious areas to remove sand and litter.	Annually
Landscaping - Landscaped islands to be maintained and mulched.	Maintained as required and mulched each Spring
Catch Basin (CB) Cleaning - CB to be cleaned of solids and oils.	Annually
Bioretention ISR	Two (2) times annually and following any rainfall event exceeding 2.5 inches in a 24-hour period
Infiltration Basin	Two (2) times annually and following any rainfall event exceeding 2.5 inches in a 24-hour period
Stone Berm Level Spreader	Annually

#### **1.3.1** Disposal Requirements

Disposal of debris, trash, sediment and other waste material should be done at suitable disposal/recycling sites and in compliance with all applicable local, state and federal waste regulations.

# **1.4 Bioretention System Requirements**

Underground Detention System Inspection/Maintenance Requirements					
Inspection/ Maintenance	Frequency	Action			
Pretreatment measure	Two (2) times annually	<ul> <li>Removal of accumulated sediment</li> <li>No less than once annually</li> </ul>			
Drawdown Time	Once annually	<ul> <li>Removal of accumulated sediments or reconstruction of filter media if system does not drain within 72-hours following a rain event</li> </ul>			
Vegetation	Once annually	<ul> <li>Vegetation maintained in healthy condition</li> <li>Pruning</li> <li>Replacement of dead or diseased vegetation</li> <li>Removal of invasive species</li> </ul>			

# **1.5 Infiltration Basin Requirements**

Infiltration Basin Inspection/Maintenance Requirements					
Inspection/	Frequency	Action			
Maintenance					
Monitor to ensure that Basins function effectively after storms	Two (2) times annually and after any rainfall event exceeding 2.5" in a 24-hr period	<ul> <li>Trash and debris to be removed</li> <li>Any required maintenance shall be addressed</li> </ul>			
Inspect Vegetation	Annually	<ul> <li>Inspect the condition of all Basin vegetation</li> <li>Prune back overgrowth</li> <li>Replace dead vegetation</li> <li>Remove any invasive species</li> </ul>			
Inspect Drawdown Time - The system shall drawdown within 48- hours following a rainfall event.	Annually	- Assess the condition of the facility to determine measures required to restore the filtration function, including but not limited to removal of accumulated sediments or reconstruction of the filter.			

# **1.6 Stone Berm Level Spreader**

Stone Berm Level Spreader Inspection/Maintenance Requirements					
Inspection/ Frequency Action Maintenance					
Visual Inspection Annually		<ul> <li>Visually inspect for damage and deterioration</li> <li>Repair damages immediately</li> </ul>			

# 1.7 Snow & Ice Management for Standard Asphalt and Walkways

Snow storage areas shall be located such that no direct untreated discharges are possible to receiving waters from the storage site (snow storage areas have been shown on the Site Plan). The property manager will be responsible for timely snow removal from all private sidewalks, driveways, and parking areas. Any snow accumulation beyond a height of 3' in the snow storage areas will be hauled off-site and legally disposed of. Salt storage areas shall be covered or located such that no direct untreated discharges are possible to receiving waters from the storage site. Salt and sand shall be used to the minimum extent practical (refer to the attached for de-icing application rate guideline from the New Hampshire Stormwater Management Manual, Volume 2,).

#### **Deicing Application Rate Guidelines**

24' of pavement (typcial two-lane road)

These rates are not fixed values, but rather the middle of a range to be selected and adjusted by an agency according to its local conditions and experience.

		Pounds per two-lane mile				
Pavement Temp. (°F) and Trend (↑↓)	Weather Condition	Maintenance Actions	Salt Prewetted / Pretreated with Salt Brine	Salt Prewetted / Pretreated with Other Blends	Dry Salt*	Winter Sand (abrasives)
>30° ↑	Snow	Plow, treat intersections only	80	70	100*	Not recommended
	Freezing Rain	Apply Chemical	80 - 160	70 - 140	100 - 200*	Not recommended
30%	Snow	Plow and apply chemical	80 - 160	70 - 140	100 - 200*	Not recommended
50 V	Freezing Rain	Apply Chemical	150 - 200	130 - 180	180 - 240*	Not recommended
25° 20° A	Snow	Plow and apply chemical	120 - 160	100 - 140	150 - 200*	Not recommended
23 - 30	Freezing Rain	Apply Chemical	150 - 200	130 - 180	180 - 240*	Not recommended
	Snow	Plow and apply chemical	120 - 160	100 - 140	150 - 200*	Not recommended
25 - 50 🗸	Freezing Rain	Apply Chemical	160 - 240	140 - 210	200 - 300*	400
20°-25° ↑	Snow or Freezing Rain	Plow and apply chemical	160 - 240	140 - 210	200 - 300*	400
20% - 25% - 1	Snow	Plow and apply chemical	200 - 280	175 - 250	250 - 350*	Not recommended
20-23 ¥	Freezing Rain	Apply Chemical	240 - 320	210 - 280	300 - 400*	400
15°-20° T	Snow	Plow and apply chemical	200 - 280	175 - 250	250 - 350*	Not recommended
10 10 1	Freezing Rain	Apply Chemical	240 - 320	210 - 280	300 - 400*	400
15°-20° ↓	Snow or Freezing Rain Plow and apply chemical	Plow and apply chemical	240 - 320	210 - 280	300 - 400*	500 for freezing rain
0°-15° ↑↓	Snow	Plow, treat with blends, sand hazardous areas	Not recommended	300 - 400	Not recommended	500 - 750 spot treatment as needed
< 0°	Snow	Plow, treat with blends, sand hazardous areas	Not recommended	400 - 600**	Not recommended	500 - 750 spot treatment as needed

\* Dry salt is not recommended. It is likely to blow off the road before it melts ice.

\*\* A blend of 6 - 8 gal/ton MgCl<sub>2</sub> or CaCl<sub>2</sub> added to NaCl can melt ice as low as -10°.

	А	nti-icing Route Data	a Form		
Truck Station:					
Date:					
Air Temperature	Pavement Temperature	Relative Humidity	Dew Point	Sky	
Reason for applying:	1				
Route:					
Chemical:					
Application Time:					
Application Amount:					
Observation (first day	):				
Observation (after eve	ent):				
Observation (before n	next application):				
Name:					

# Section 2 Invasive Species

With respect to a particular ecosystem, any species, including its seeds, eggs, spores, or other biological material capable of propagating that species, that is not native to that ecosystem is classified as an invasive species. Refer to the following fact sheet prepared by the University of New Hampshire Cooperative Extension entitled Methods for Disposing Non-Native Invasive Plants for recommended methods to dispose of invasive plant species.

# UNIVERSITY of NEW HAMPSHIRE Methods for Disposing COOPERATIVE EXTENSION Non-Native Invasive Plants

Prepared by the Invasives Species Outreach Group, volunteers interested in helping people control invasive plants. Assistance provided by the Piscataquog Land Conservancy and the NH Invasives Species Committee. Edited by Karen Bennett, Extension Forestry Professor and Specialist.



Tatarian honeysuckleLonicera tataricaUSDA-NRCS PLANTS Database / Britton, N.L., andA. Brown. 1913. An illustrated flora of the northernUnited States, Canada and the British Possessions.Vol. 3: 282.

Non-native invasive plants crowd out natives in natural and managed landscapes. They cost taxpayers billions of dollars each year from lost agricultural and forest crops, decreased biodiversity, impacts to natural resources and the environment, and the cost to control and eradicate them.

Invasive plants grow well even in less than desirable conditions such as sandy soils along roadsides, shaded wooded areas, and in wetlands. In ideal conditions, they grow and spread even faster. There are many ways to remove these nonnative invasives, but once removed, care is needed to dispose the removed plant material so the plants don't grow where disposed.

Knowing how a particular plant reproduces indicates its method of spread and helps determine

the appropriate disposal method. Most are spread by seed and are dispersed by wind, water, animals, or people. Some reproduce by vegetative means from pieces of stems or roots forming new plants. Others spread through both seed and vegetative means.

Because movement and disposal of viable plant parts is restricted (see NH Regulations), viable invasive parts can't be brought to most transfer stations in the state. Check with your transfer station to see if there is an approved, designated area for invasives disposal. This fact sheet gives recommendations for rendering plant parts nonviable.

Control of invasives is beyond the scope of this fact sheet. For information about control visit <u>www.nhinvasives.org</u> or contact your UNH Cooperative Extension office.

#### **New Hampshire Regulations**

Prohibited invasive species shall only be disposed of in a manner that renders them nonliving and nonviable. (Agr. 3802.04)

No person shall collect, transport, import, export, move, buy, sell, distribute, propagate or transplant any living and viable portion of any plant species, which includes all of their cultivars and varieties, listed in Table 3800.1 of the New Hampshire prohibited invasive species list. (Agr 3802.01)

#### How and When to Dispose of Invasives?

To prevent seed from spreading remove invasive plants before seeds are set (produced). Some plants continue to grow, flower and set seed even after pulling or cutting. Seeds can remain viable in the ground for many years. If the plant has flowers or seeds, place the flowers and seeds in a heavy plastic bag "head first" at the weeding site and transport to the disposal site. The following are general descriptions of disposal methods. See the chart for recommendations by species.

**Burning:** Large woody branches and trunks can be used as firewood or burned in piles. For outside burning, a written fire permit from the local forest fire warden is required unless the ground is covered in snow. Brush larger than 5 inches in diameter can't be burned. Invasive plants with easily airborne seeds like black swallow-wort with mature seed pods (indicated by their brown color) shouldn't be burned as the seeds may disperse by the hot air created by the fire.

**Bagging (solarization):** Use this technique with softertissue plants. Use heavy black or clear plastic bags (contractor grade), making sure that no parts of the plants poke through. Allow the bags to sit in the sun for several weeks and on dark pavement for the best effect.

Tarping and Drying: Pile material on a sheet of plastic



Japanese knotweed Polygonum cuspidatum USDA-NRCS PLANTS Database / Britton, N.L., and A. Brown. 1913. An illustrated flora of the northern United States, Canada and the British Possessions. Vol. 1: 676.

and cover with a tarp, fastening the tarp to the ground and monitoring it for escapes. Let the material dry for several weeks, or until it is clearly nonviable.

Chipping: Use this method for woody plants that don't reproduce vegetatively.

**Burying:** This is risky, but can be done with watchful diligence. Lay thick plastic in a deep pit before placing the cut up plant material in the hole. Place the material away from the edge of the plastic before covering it with more heavy plastic. Eliminate as much air as possible and toss in soil to weight down the material in the pit. Note that the top of the buried material should be at least three feet underground. Japanese knotweed should be at least 5 feet underground!

**Drowning:** Fill a large barrel with water and place soft-tissue plants in the water. Check after a few weeks and look for rotted plant material (roots, stems, leaves, flowers). Well-rotted plant material may be composted. A word of caution- seeds may still be viable after using this method. Do this before seeds are set. This method isn't used often. Be prepared for an awful stink!

**Composting:** Invasive plants can take root in compost. Don't compost any invasives unless you know there is no viable (living) plant material left. Use one of the above techniques (bagging, tarping, drying, chipping, or drowning) to render the plants nonviable before composting. Closely examine the plant before composting and avoid composting seeds.

Be diligent looking for seedlings for years in areas where removal and disposal took place.

# **Suggested Disposal Methods for Non-Native Invasive Plants**

This table provides information concerning the disposal of removed invasive plant material. If the infestation is treated with herbicide and left in place, these guidelines don't apply. Don't bring invasives to a local transfer station, unless there is a designated area for their disposal, or they have been rendered non-viable. This listing includes wetland and upland plants from the New Hampshire Prohibited Invasive Species List. The disposal of aquatic plants isn't addressed.

Woody Plants	Method of Reproducing	Methods of Disposal
Norway maple (Acer platanoides) European barberry (Berberis vulgaris) Japanese barberry (Berberis thunbergii) autumn olive (Elaeagnus umbellata) burning bush (Euonymus alatus)	Fruit and Seeds	<ul> <li>Prior to fruit/seed ripening</li> <li>Seedlings and small plants <ul> <li>Pull or cut and leave on site with roots exposed. No special care needed.</li> </ul> </li> <li>Larger plants <ul> <li>Use as firewood.</li> <li>Make a brush pile.</li> <li>Chip.</li> <li>Burn.</li> </ul> </li> </ul>
Morrow's honeysuckle (Lonicera morrowii) Tatarian honeysuckle (Lonicera tatarica) showy bush honeysuckle (Lonicera x bella) common buckthorn (Rhamnus cathartica) glossy buckthorn (Frangula alnus)		<ul> <li>After fruit/seed is ripe</li> <li>Don't remove from site.</li> <li>Burn.</li> <li>Make a covered brush pile.</li> <li>Chip once all fruit has dropped from branches.</li> <li>Leave resulting chips on site and monitor.</li> </ul>
oriental bittersweet (Celastrus orbiculatus) multiflora rose (Rosa multiflora)	Fruits, Seeds, Plant Fragments	<ul> <li>Prior to fruit/seed ripening</li> <li>Seedlings and small plants</li> <li>Pull or cut and leave on site with roots exposed. No special care needed.</li> <li>Larger plants</li> <li>Make a brush pile.</li> <li>Burn.</li> </ul>
	<b>V</b>	<ul> <li>After fruit/seed is ripe Don't remove from site.</li> <li>Burn.</li> <li>Make a covered brush pile.</li> <li>Chip – only after material has fully dried (1 year) and all fruit has dropped from branches. Leave resulting chips on site and monitor.</li> </ul>

Non-Woody Plants	Method of Reproducing	Methods of Disposal
<pre>garlic mustard (Alliaria petiolata) spotted knapweed (Centaurea maculosa) • Sap of related knapweed can cause skin irritation and tumors. Wear gloves when handling. black swallow-wort (Cynanchum nigrum) • May cause skin rash. Wear gloves and long sleeves when handling. pale swallow-wort (Cynanchum rossicum) giant hogweed (Heracleum mantegazzianum) • Can cause major skin rash. Wear gloves and long sleeves when handling. dame's rocket (Hesperis matronalis) perennial pepperweed (Lepidium latifolium) purple loosestrife (Lythrum salicaria) Japanese stilt grass (Microstegium vimineum) mile-a-minute weed (Polygonum perfoliatum)</pre>	Fruits and Seeds	<ul> <li>Prior to flowering Depends on scale of infestation Small infestation <ul> <li>Pull or cut plant and leave on site with roots exposed.</li> </ul> </li> <li>Large infestation <ul> <li>Pull or cut plant and pile. (You can pile onto or cover with plastic sheeting).</li> <li>Monitor. Remove any re-sprouting material.</li> </ul> </li> <li>During and following flowering <ul> <li>Do nothing until the following year or remove flowering heads and bag and let rot.</li> </ul> </li> <li>Small infestation <ul> <li>Pull or cut plant and leave on site with roots exposed.</li> </ul> </li> <li>Large infestation <ul> <li>Pull or cut plant and pile remaining material. (You can pile onto plastic or cover with plastic sheeting).</li> <li>Monitor. Remove any re-sprouting material. (You can pile onto plastic or cover with plastic sheeting).</li> <li>Monitor. Remove any re-sprouting material.</li> </ul> </li> </ul>
common reed ( <i>Phragmites australis</i> ) Japanese knotweed ( <i>Polygonum cuspidatum</i> ) Bohemian knotweed ( <i>Polygonum x bohemicum</i> )	Fruits, Seeds, Plant Fragments Primary means of spread in these species is by plant parts. Although all care should be given to preventing the dispersal of seed during control activities, the presence of seed doesn't materially influence disposal activities.	<ul> <li>Small infestation <ul> <li>Bag all plant material and let rot.</li> <li>Never pile and use resulting material as compost.</li> <li>Burn.</li> </ul> </li> <li>Large infestation <ul> <li>Remove material to unsuitable habitat (dry, hot and sunny or dry and shaded location) and scatter or pile.</li> <li>Monitor and remove any sprouting material.</li> <li>Pile, let dry, and burn.</li> </ul> </li> </ul>

January 2010

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# Managing Invasive Plants Methods of Control by Christopher Mattrick

# They're out there. The problem of invasive plants is as close as your own backyard.

Maybe a favorite dogwood tree is struggling in the clutches of an Oriental bittersweet vine. Clawlike canes of multiflora rose are scratching at the side of your house. That handsome burning bush you planted few years ago has become a whole clump in practically no time ... but what happened to the azalea that used to grow right next to it?

If you think controlling or managing invasive plants on your property is a daunting task, you're not alone. Though this topic is getting lots of attention from federal, state, and local government agencies, as well as the media, the basic question for most homeowners is simply, "How do I get rid of the invasive plants in my own landscape?" Fortunately, the best place to begin to tackle this complex issue is in our own backyards and on local conservation lands. We hope the information provided here will help you take back your yard. We won't kid you—there's some work involved, but the payoff in beauty, wildlife habitat, and peace of mind makes it all worthwhile.

# PLAN OF ATTACK

Three broad categories cover most invasive plant control: mechanical, chemical, and biological. Mechanical control means physically removing plants from the environment



Spraying chemicals to control invasive plants.

through cutting or pulling. Chemical control uses herbicides to kill plants and inhibit regrowth. Techniques and chemicals used will vary depending on the species. Biological controls use plant diseases or insect predators, typically from the targeted species' home range. Several techniques may be effective in controlling a single species, but there is usually one preferred method—the one that is most resource efficient with minimal impact on non-target species and the environment.

# MECHANICAL CONTROL METHODS

Mechanical treatments are usually the first ones to look at when evaluating an invasive plant removal project. These procedures do not require special licensing or introduce chemicals into the environment. They do require permits in some situations, such as wetland zones. [See sidebar on page 23.] Mechanical removal is highly labor intensive and creates a significant amount of site disturbance, which can lead to rapid reinvasion if not handled properly.

#### Pulling and digging

Many herbaceous plants and some woody species (up to about one inch in diameter), if present in limited quantities, can be pulled out or dug up. It's important to remove as much of the root system as possible; even a small portion can restart the infestation. Pull plants by hand or use a digging fork, as shovels can shear off portions of the root

system, allowing for regrowth. To remove larger woody stems (up to about three inches in diameter), use a Weed Wrench<sup>™</sup>, Root Jack, or Root Talon. These tools, available from several manufacturers, are designed to remove the aboveground portion of the plant as well as the entire root system. It's easiest to undertake this type of control in the spring or early summer when soils are moist and plants come out more easily.



Using tools to remove woody stems.





Volunteers hand pulling invasive plants.

#### Suffocation

Try suffocating small seedlings and herbaceous plants. Place double or triple layers of thick UV-stabilized plastic sheeting, either clear or black (personally I like clear), over the infestation and secure the plastic with stakes or weights. Make sure the plastic extends at least five feet past the edge of infestation on all sides. Leave the plastic in place for at least two years. This technique will kill everything beneath the plastic—invasive and non-invasive plants alike. Once the plastic is removed, sow a cover crop such as annual rye to prevent new invasions.

#### Cutting or mowing

This technique is best suited for locations you can visit and treat often. To be effective, you will need to mow or cut infested areas three or four times a year for up to five years. The goal is to interrupt the plant's ability to photosynthesize by removing as much leafy material as possible. Cut the plants at ground level and remove all resulting debris from the site. With this treatment, the infestation may actually appear to get worse at first, so you will need to be as persistent as the invasive plants themselves. Each time you cut the plants back, the root system gets slightly larger, but must also rely on its energy reserves to push up new growth. Eventually, you will exhaust these reserves and the plants will die. This may take many years, so you have to remain committed to this process once you start; otherwise the treatment can backfire, making the problem worse.

## CHEMICAL CONTROL METHODS

Herbicides are among the most effective and resource-efficient tools to treat invasive species. Most of the commonly known invasive plants can be treated using only two herbicides—glyphosate (the active ingredient in Roundup™ and Rodeo<sup>TM</sup>) and triclopyr (the active ingredient in Brush-B-Gone<sup>™</sup> and Garlon<sup>™</sup>). Glyphosate is non-selective, meaning it kills everything it contacts. Triclopyr is selective and does not injure monocots (grasses, orchids, lilies, etc.). Please read labels and follow directions precisely for both environmental and personal safety. These are relatively benign herbicides, but improperly used they can still cause both short- and long-term health and environmental problems. Special aquatic formulations are required when working in wetland zones. You are required to have a stateissued pesticide applicator license when applying these chemicals on land you do not own. To learn more about the pesticide regulations in your state, visit or call your state's pesticide control division, usually part of the state's Department of Agriculture. In wetland areas, additional permits are usually required by the Wetlands Protection Act. [See sidebar on page 23.]

#### Foliar applications

When problems are on a small scale, this type of treatment is usually applied with a backpack sprayer or even a small handheld spray bottle. It is an excellent way to treat large monocultures of herbaceous plants, or to spot-treat individual plants that are difficult to remove mechanically, such as goutweed, swallowwort, or purple loosestrife. It is also an effective treatment for some woody species, such as Japanese barberry, multiflora rose, Japanese honeysuckle, and Oriental bittersweet that grow in dense masses or large numbers over many acres. The herbicide mixture should contain no more than five percent of the active ingredient, but it is important to follow the instructions on the product label. This treatment is most effective when the plants are actively growing, ideally when they are flowering or beginning to form fruit. It has been shown that plants are often more susceptible to this type of treatment if the existing stems are cut off and the regrowth is treated. This is especially true for Japanese knotweed. The target plants should be thoroughly wetted with the herbicide on a day when there is no rain in the forecast for the next 24 to 48 hours.

#### Cut stem treatments

There are several different types of cut stem treatments, but here we will review only the one most commonly used. All treatments of this type require a higher concentration of the active ingredient than is used in foliar applications. A 25 to 35 percent solution of the active ingredient should be used for cut stem treatments, but read and follow all label instructions. In most cases, the appropriate herbicide is glyphosate, except for Oriental bittersweet, on which triclopyr should be used. This treatment can be used on all woody stems, as well as phragmites and Japanese knotweed.

For woody stems, treatments are most effective when applied in the late summer and autumn—between late August and November. Stems should be cut close to the ground, but not so close that you will lose track of them. Apply herbicide directly to the cut surface as soon as possible after cutting. Delaying the application will reduce the effectiveness of the treatment. The herbicide can be applied with a sponge, paintbrush, or spray bottle.



For phragmites and Japanese knotweed, treatment is the same, but the timing and equipment are different. Plants should be treated anytime from mid-July through September, but the hottest, most humid days of the summer are best

Cut stem treatment tools.

for this method. Cut the stems halfway between two leaf nodes at a comfortable height. Inject (or squirt) herbicide into the exposed hollow stem. All stems in an infestation should be treated. A wash bottle is the most effective application tool, but you can also use an eyedropper, spray bottle, or one of the recently developed high-tech injection systems.

It is helpful to mix a dye in with the herbicide solution. The dye will stain the treated surface and mark the areas that have been treated, preventing unnecessary reapplication. You can buy a specially formulated herbicide dye, or use food coloring or laundry dye.

There is not enough space in this article to describe all the possible ways to control invasive plants. You can find other treatments, along with more details on the above-described methods, and species-specific recommendations on The Nature Conservancy Web site (tncweeds.ucdavis.edu). An upcoming posting on the Invasive Plant Atlas of New England (www.ipane.org) and the New England Wild Flower Society (www.newfs.org) Web sites will also provide further details.



Hollow stem injection tools.

#### Biological controls-still on the horizon

Biological controls are moving into the forefront of control methodology, but currently the only widely available and applied biocontrol relates to purple loosestrife. More information on purple loosestrife and other biological control projects can be found at www.invasiveplants.net.

### DISPOSAL OF INVASIVE PLANTS

Proper disposal of removed invasive plant material is critical to the control process. Leftover plant material can cause new infestations or reinfest the existing project area. There are many appropriate ways to dispose of invasive plant debris. I've listed them here in order of preference.

- **1. Burn it**—Make a brush pile and burn the material following local safety regulations and restrictions, or haul it to your town's landfill and place it in their burn pile.
- **2. Pile it**—Make a pile of the woody debris. This technique will provide shelter for wildlife as well.
- **3.** Compost it—Place all your herbaceous invasive plant debris in a pile and process as compost. Watch the pile closely for resprouts and remove as necessary. Do not use the resulting compost in your garden. The pile is for invasive plants only.



Injecting herbicide into the hollow stem of phragmites.

**4. Dry it/cook it**—Place woody debris out on your driveway or any asphalt surface and let it dry out for a month. Place herbaceous material in a doubled-up black trash bag and let it cook in the sun for one month. At the end of the month, the material should be non-viable and you can dump it or dispose of it with the trash. The method assumes there is no viable seed mixed in with the removed material.

Care should be taken in the disposal of all invasive plants, but several species need extra attention. These are the ones that have the ability to sprout vigorously from plant fragments and should ideally be burned or dried prior to disposal: Oriental bittersweet, multiflora rose, Japanese honeysuckle, phragmites, and Japanese knotweed. Christopher Mattrick is the former Senior Conservation Programs Manager for New England Wild Flower Society, where he managed conservation volunteer and invasive and rare plant management programs. Today, Chris and his family work and play in the White Mountains of New Hampshire, where he is the Forest Botanist and Invasive Species Coordinator for the White Mountain National Forest.



# **Controlling Invasive Plants in Wetlands**

Special concerns; special precautions

Control of invasive plants in or around wetlands or bodies of water requires a unique set of considerations. Removal projects in wetland zones can be legal and effective if handled appropriately. In many cases, herbicides may be the least disruptive tools with which to remove invasive plants. You will need a state-issued pesticide license to apply herbicide on someone else's property, but all projects in wetland or aquatic systems fall under the jurisdiction of the Wetlands Protection Act and therefore require a permit. *Yes, even hand-pulling that colony of glossy buckthorn plants from your own swampland requires a permit.* Getting a permit for legal removal is fairly painless if you plan your project carefully.

1. Investigate and understand the required permits and learn how to obtain them. The entity charged with the enforcement of the Wetlands Protection Act varies from state to state. For more information in your state, contact:

ME: Department of Environmental Protection www.state.me.us/dep/blwq/docstand/nrpapage.htm

**NH:** Department of Environmental Services www.des.state.nh.us/wetlands/

VT: Department of Environmental Conservation www.anr.state.vt.us/dec/waterq/permits/htm/ pm\_cud.htm

MA: Consult your local town conservation commission

**RI:** Department of Environmental Management www.dem.ri.gov/programs/benviron/water/ permits/fresh/index.htm

CT: Consult your local town Inland Wetland and Conservation Commission

- 2. Consult an individual or organization with experience in this area. Firsthand experience in conducting projects in wetland zones and navigating the permitting process is priceless. Most states have wetland scientist societies whose members are experienced in working in wetlands and navigating the regulations affecting them. A simple Web search will reveal the contact point for these societies. Additionally, most environmental consulting firms and some nonprofit organizations have skills in this area.
- **3.** Develop a well-written and thorough project plan. You are more likely to be successful in obtaining a permit for your project if you submit a project plan along with your permit application. The plan should include the reasons for the project, your objectives in completing the project, how you plan to reach those objectives, and how you will monitor the outcome.
- **4.** Ensure that the herbicides you plan to use are approved for aquatic use. Experts consider most herbicides harmful to water quality or aquatic organisms, but rate some formulations as safe for aquatic use. Do the research and select an approved herbicide, and then closely follow the instructions on the label.
- **5.** If you are unsure—research, study, and most of all, ask for help. Follow the rules. The damage caused to aquatic systems by the use of an inappropriate herbicide or the misapplication of an appropriate herbicide not only damages the environment, but also may reduce public support for safe, well-planned projects.

# Section 3 Annual Updates and Log Requirements

The Owner and/or Contact/Responsible Party shall review this Operation and Maintenance Plan once per year for its effectiveness and adjust the plan and deed as necessary.

A log of all preventative and corrective measures for the stormwater system shall be kept on-site and be made available upon request by any public entity with administrative, health environmental or safety authority over the site including NHDES.

Copies of the Stormwater Maintenance report shall be submitted to the City of Portsmouth on an annual basis.

Stormwater Management Report							
Proposed Mixed-U	se Development	1035 Lafaye	1035 Lafayette Road – Tax Map 246 Lot 1				
BMP Description	Date of Inspection	Inspector	BMP Installed and Operating Properly?	Cleaning / Corrective Action Needed	Date of Cleaning / Repair	Performed By	
Deep Sump CB's			□Yes □No				
Bioretention ISR			□Yes □No				
Infiltration Basin			□Yes □No				
Stone Berm Level Spreader			□Yes □No				

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www.tighebond.com







P5118-001 May 20, 2024

Mr. Peter Britz, Director of Planning & Sustainability City of Portsmouth Planning & Sustainability Department 1 Junkins Avenue Portsmouth, New Hampshire 03801

#### Re: Trip Generation Memorandum 1035 Lafayette Road Development Portsmouth, New Hampshire

Dear Peter:

Tighe & Bond has prepared a trip generation memorandum to outline the anticipated study area of the Traffic Impact Assessment (TIA) for the proposed mixed-use development located at 1035 Lafayette Road (US Route 1) in Portsmouth, NH. The site is bounded by Lafayette Road (US Route 1) to the west and by Sagamore Creek and Headlands Park to the north, east, and south. With the project, the Portsmouth Housing Authority proposes to construct residential units and office space, and repurpose a portion of the existing building at 1035 Lafayette Road. as part of the project, while a portion of the existing church will be renovated to remain. The project consists of a proposed seven-unit transitional housing area, and a separate three- to four-story apartment building consisting of 44 units. The existing daycare, with a current enrollment of 40 students, is currently housed in the basement of the existing church and will remain as part of the project but has the potential to expand enrollment up to 71 students. On-site parking will be provided by surface parking lots on site. Two existing site access driveways to Lafayette Road will remain, with the northern full-access driveway forming an existing signalized intersection with Lafayette Road opposite Mirona Road, and the southern driveway located approximately 400 feet south of Mirona Road. Lafayette Road is median divided at the southern driveway, prohibiting left turns entering or exiting the site from this driveway. The project will include site, access drive, stormwater management, utilities, lighting, and landscaping improvements. The trip generation estimate for the proposed development presented herein will serve as the basis for the traffic impact assessment.

## Study Area

Based on a preliminary review of expected trip generation and distribution for the surrounding area, the following intersections have been identified to be included in the study area:

- US Route 1 (Lafayette Road) at North Site Driveway/Minora Road (signalized)
- US Route 1 (Lafayette Road) at South Site Driveway (unsignalized)

Turning movement count (TMC) data were collected during the weekday morning (7:00-9:00 AM) and weekday afternoon (3:00-6:00 PM) peak periods on Thursday April 18, 2024 and Saturday midday peak period (11:00 AM-1:00 PM) on Saturday April 20, 2024 at the study intersections. An automatic traffic recorder (ATR) count was collected on US Route 1 (Lafayette Road) in the vicinity of the site driveways to collect directional traffic volume flows and vehicular travel speeds. Summarized and adjusted volumes will be presented in a future full Traffic Impact Study (TIS) supporting the project.



# **Trip Generation**

Trips expected to be generated by the proposed development were estimated using the Institute of Transportation Engineers (ITE) Trip Generation, 11<sup>th</sup> Edition, 2021. Multifamily Housing (Low-Rise) (LUC-220) was used to estimate vehicle trips for the proposed 44-unit three- to four-story apartment building and seven units of transitional housing. General Office Building (LUC-710) was used to estimate the office trips based on the proposed 6,900 SF building. Small Office Building (LUC-712) was considered given the size of the office component, but LUC 710 was utilized to represent a conservative estimate. The trip generation estimate for the proposed daycare was developed based on a rate established using the April 2024 turning movement counts.

Since the proposed daycare will replace the existing daycare, a credit was applied to account for the existing daycare trips and are subtracted from the proposed site trips to determine the total proposed net trips. ITE LUC 565 (Day Care Center) was considered to estimate both existing and proposed daycare trips. The existing turning movement counts were found to be lower than the ITE data in the morning peak period and higher in the afternoon peak period. The April 2024 turning movement counts were used as the basis for the proposed day care trip generation estimate to present a conservative estimate in the afternoon peak period and to align with the existing daycare operations. Credit for the existing daycare was only applied to the weekday morning and afternoon peak hour trips as the daycare is closed on the weekend. The existing church trips are negligible since the church is only in session on Sunday, outside of the analysis time periods.

Based on the ITE data and after applying the existing daycare trip credit, the proposed development is estimated to generate 77 trips (38 entering, 39 exiting) during the weekday morning peak hour, 92 trips (42 entering, 50 exiting) during the weekday afternoon peak hour, and 21 trips (10 entering, 11 exiting) during the Saturday midday peak hour. Table 1 provides a detailed summary of the trip generation.

# **Trip Distribution**

The distribution of the proposed traffic entering and exiting the site expected to be generated by the mixed-use development was reviewed based on U.S. Census journey-to-work data for people residing in Portsmouth for the residential uses and based on existing travel patterns and anticipated travel patterns for the office and daycare uses. The following arrival/departure distributions are anticipated for the residential uses:

- 30% to/ from the North to Portsmouth Center via US Route 1
- 25% to/ from the South via US Route 1 (Lafayette Road)
- 20% to/ from the West to US Route 4 (Spaulding Turnpike) via US Route 1 Bypass
- 15% to/ from the South to I-95 South via Route 33
- 5% to/ from the West via Route 33
- 5% to/ from the North to I-95 North via US Route 1 Bypass

Based on the residential regional distribution, it is estimated that 55% will access the site to/ from the north via US Route 1, 25% will access the site to/ from the south via US Route 1, and 20% will access the site to/ from the west via Mirona Road.

The following arrival/ departure distribution is anticipated for the office and daycare uses:

• 40% to/ from the North to Portsmouth Center via US Route 1

- 25% to/ from the South via US Route 1 (Lafayette Road)
- 20% to/ from the West to US Route 4 (Spaulding Turnpike) via US Route 1 Bypass
- 5% to/ from the South to I-95 South via Route 33
- 5% to/ from the West via Route 33
- 5% to/ from the North to I-95 North via US Route 1 Bypass

Based on the office/ daycare regional distribution, it is estimated that 65% will access the site to/ from the north via US Route 1, 25% will access the site to/ from the south via US Route 1, and 10% will access the site to/ from the west via Mirona Road.

Figure 1 presents the anticipated regional site traffic distributions of the traffic through the study area roadways. Distribution percentages for the office and daycare uses may be updated in development of the TIA based on collected traffic volume data.

# Conclusion

The proposed mixed-use development includes 51 residential units, a daycare with enrollment of up to 71 students, and 6,900 SF of office space. Based on the estimated trip generation and trip distribution, the TIA will analyze traffic operations at two intersections during the weekday morning, weekday afternoon, and Saturday midday peak periods.

Sincerely,

#### TIGHE & BOND, INC.

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Greg Lucas, PE, PTOE, RSP1 Senior Project Manager

Copy: Mark Lentz, Portsmouth Housing Authority

Enclosures: Study Area Map (Figure 1) Site-Generated Traffic Summary (Table 1) Conceptual Site Layout Plan

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#### TABLE 1 Site-Generated Traffic Summary

Existing Daycare - 40 Stu Peak Hour Period	dents Enter	Fyit	Total
Weekday Morning	18	10	28
Weekday Afternoon	15	25	40
Satruday Midday	NO DATA	NO DATA	NO DATA
Weekday	NO DATA	NO DATA	NO DATA
Saturday	NO DATA	NO DATA	NO DATA
Proposed - 51 Units Apar	tment		LUC 220
Weekday Morning	g	30	<b>10ta</b>
Weekday Afternoon	27	15	42
Saturday Midday	11	10	42
	11	10	21
Weekday	201	201	402
Saturday	116	116	232
Proposed Daycare - 71 St Peak Hour Period	udents Enter	Fxit	Total
Weekday Morning	32	18	50
Weekday Afternoon	27	44	71
Saturday Midday	NO DATA	NO DATA	NO DATA
Weekday	NO DATA	NO DATA	NO DATA
Saturday	NO DATA	NO DATA	NO DATA
Proposed - 6,900 SF Offic	e Building		LUC 710
Peak Hour Period	Enter	Exit	Total
Weekday Morning	15	2	17
Weekday Afternoon	3	15	18
Saturday Midday	NO DATA	NO DATA	NO DATA
Weekday	57	56	113
Saturday	NO DATA	NO DATA	NO DATA
Proposed Total Trips Peak Hour Period	Enter	Exit	Total
Weekday Morning	56	49	105
Weekday Afternoon	57	75	132
Saturday Midday	11	10	21
Weekday	258	258	516
Saturday	116	116	232

Net Vehicular Trips (Proposed minus Existing Daycare Trips)

Peak Hour Period	Enter	Exit	Total
Weekday Morning	38	39	77
Weekday Afternoon	42	50	92
Saturday Midday	11	10	21
Weekday	258	258	516
Saturday	116	116	232

Source: Institute of Transportation Engineers, Trip Generation, 11th Edition, 2021 Land Use - 220 [Multifamily Housing (Low-Rise)] 221 [Residential - Multifamily House (Mid-Rise)] 710 [General Office Building]



ZONING DISTRICT: GATEWAY CORRIDOR (G2) PROPOSED USE: MIXED USE MULTIFAMILY PROPOSED LOT SIZE: ±3.491 ACRES (±152.082 SE) BUILDING PLACEMENT & LOT STANDARDS BUILDING STANDARDS: MINIMUM LOT DEPTH: MINIMUM STREET FRONTAGE: 55 FRONT YARD SETBACK: LAFAYETTE ROAD SETBACK: MINIMUM SIDE BUILDING SETBACK: 26 MINIMUM OPEN SPACE COVERAGE: 27 FRONT U JUE BUILDING SETBACK: 27 MINIMUM OPEN SPACE COVERAGE: 27 REQUIRED 100 FT 50 FT ± 110 FT<sup>(1</sup> ± 25 FT ± 68 FT ±72% 48%<sup>(1)</sup> 70-90 FT 15 FT 20 FT 20% 75% FRONT LOT LINE BUILDOUT: BUILDING DESIGN STANDARDS: MAXIMUM BUILDING HEIGHT: 4 STORIES 50 FT 24 FT MINIMUM STREET FACING FACADE HEIGHT: MAXIMUM FINISHED FLOOR SURFACE OF GROUND FLOOR ABOVE SIDEWALK GRADE: MAXIMUM BUILDING FOOTPRINT: MAXIMUM FACADE MODULATION LENGTH: MINIMUM STREET FACING FACADE GLAZING: 36 IN 20,000 SF 50 FT 20% GROUND FLOOR DEVELOPMENT SITE STANDARDS:<sup>(3)</sup> MINIMUM DEVELOPMENT SITE AREA: 20,000 SF 100 FT 100 FT MINIMUM STEE WIDTH: MINIMUM SITE DEPTH: MINIMUM PERIMETER BUFFER FROM RESIDENTIAL, MIXED RESIDENTIAL, OR CD4-L1 DISTRICTS: MAXIMUM DEVELOPMENT BLOCK DIMENSIONS: 75 FT N/A MAXIMUM DEVELOPMENT BLOCK DI BLOCK LENGTH: ERIMETER: MAXIMUM BUILDING COVERAGE: MINIMUM OPEN SPACE COVERAGE: FRONT LOT LINE BUILDOUT: 800 FT 200 FT 70% 20% 75% N/A N/A 14 ±72 48%<sup>(1)</sup> DENSITY THRESHOLDS AND BONUSES: DWELLING UNITS PER ACRE: 16 UNITS 36 UNITS DWELLING UNITS PER BUILDING:

ARKING CALCULATIONS:					
ARKING SPACE REQUIREMENTS: ZONING REQUIRED PARKING SPACES					
1 PER 350 SF GFA x 6,900	= 20 SPACES				
1.0 SPACES PER UNIT (500 1.3 SPACES PER UNIT (500 1.3 SPACES PER UNIT ( >7 +1 VISITOR PER 5 UNITS X	= 11 SPACES = 52 SPACES = 11 SPACES				
0.5 PER STUDENT x 71 STU PLACE OF WORSHIP:	IDENTS	= 36 SPACES			
1 PER PERSON MAX CAPAC TOTAL REQUIRED PARKING	ITY (40 PERSON)	= 10 SPACES = 140 SPACES			
TOTAL REQUIRED PER SHARED PARKI	= 103 SPACES				
REQUIRED PARKING SPACES ON A PUE ZONING REQUIREMENTS x 80%	BLIC TRANSIT <sup>(5)</sup>	= 83 SPACES			
ROVIDED PARKING SPACES TOTAL PROVIDED SPACES:		= 84 SPACES			
CCESSIBLE PARKING SPACES:	REQUIRED 4	PROPOSED 6			
IMENSIONAL REQUIREMENTS: STANDARD 90° PARKING STALL :	0.F.FT	0.5.57			
LENGTH	8.5 FT 19 FT MIN	8.5 FT 19 FT			
90° (2-WAY TRAFFIC)	24 FT	24 FT			
4) - SHARED PARKING ANALYSIS ALLOWED THROUGH A CONDITIONAL USE PERMIT					





# **City of Portsmouth, New Hampshire**

# Site Plan Application Checklist

This site plan application checklist is a tool designed to assist the applicant in the planning process and for preparing the application for Planning Board review. The checklist is required to be completed and uploaded to the Site Plan application in the City's online permitting system. A preapplication conference with a member of the planning department is strongly encouraged as additional project information may be required depending on the size and scope. The applicant is cautioned that this checklist is only a guide and is not intended to be a complete list of all site plan review requirements. Please refer to the Site Plan review regulations for full details.

Applicant Responsibilities (Section 2.5.2): Applicable fees are due upon application submittal along with required attachments. The application shall be complete as submitted and provide adequate information for evaluation of the proposed site development. Waiver requests must be submitted in writing with appropriate justification.

Name of Applicant: \_\_\_\_\_ Portsmouth Housing Authority \_\_\_\_ Date Submitted: May 20, 2024

Application # (in City's online permitting): LU 23-

Site Address: 1035 Lafayette Rd

\_\_\_\_\_\_Map: <u>\_\_\_\_46</u>\_\_\_\_\_Lot 1

	Application Requirements				
Ŋ	Required Items for Submittal	Item Location (e.g. Page or Plan Sheet/Note #)	Waiver Requested		
Ŋ	Complete <u>application</u> form submitted via the City's web-based permitting program (2.5.2.1 <b>(2.5.2.3A)</b>	Enclosed	N/A		
A	All application documents, plans, supporting documentation and other materials uploaded to the application form in viewpoint in digital Portable Document Format (PDF). One hard copy of all plans and materials shall be submitted to the Planning Department by the published deadline. (2.5.2.8)	Enclosed	N/A		

	Site Plan Review Application Required Information			
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested	
	Statement that lists and describes "green" building components and systems. (2.5.3.1B)			
Ø	Existing and proposed gross floor area and dimensions of all buildings and statement of uses and floor area for each floor. (2.5.3.1C)	Site Plan Sheet C-102	N/A	
Ŋ	Tax map and lot number, and current zoning of all parcels under Site Plan Review. (2.5.3.1D)	Site Plan Sheet C-102	N/A	

	Site Plan Review Application Required Info	ormation	
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
Ŋ	Owner's name, address, telephone number, and signature. Name, address, and telephone number of applicant if different from owner. <b>(2.5.3.1E)</b>	Enclosed Cover Sheet	N/A
Ø	Names and addresses (including Tax Map and Lot number and zoning districts) of all direct abutting property owners (including properties located across abutting streets) and holders of existing conservation, preservation or agricultural preservation restrictions affecting the subject property. (2.5.3.1F)	Existing Conditions Plan Sheets	N/A
Ŋ	Names, addresses and telephone numbers of all professionals involved in the site plan design. (2.5.3.1G)	Cover Sheet	N/A
Ŋ	List of reference plans. (2.5.3.1H)	General Notes Sheet G-100 & Existing Conditions Plan Sheets	N/A
Þ	List of names and contact information of all public or private utilities servicing the site. (2.5.3.1)	General Notes Sheet G-100	N/A

	Site Plan Specifications			
Ø	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested	
Ø	Full size plans shall not be larger than 22 inches by 34 inches with match lines as required, unless approved by the Planning Director (2.5.4.1A)	Required on all plan sheets	N/A	
Ø	Scale: Not less than 1 inch = 60 feet and a graphic bar scale shall be included on all plans. (2.5.4.1B)	Required on all plan sheets	N/A	
Ŋ	GIS data should be referenced to the coordinate system New Hampshire State Plane, NAD83 (1996), with units in feet. (2.5.4.1C)	Existing Conditions Plan Sheets	N/A	
Ø	Plans shall be drawn to scale and stamped by a NH licensed civil engineer. (2.5.4.1D)	Required on all plan sheets	N/A	
Ø	Wetlands shall be delineated by a NH certified wetlands scientist and so stamped. (2.5.4.1E)	Existing Conditions Plan Sheet	N/A	
Ø	Title (name of development project), north point, scale, legend. (2.5.4.2A)	Required on all plan sheets	N/A	
Ø	Date plans first submitted, date and explanation of revisions. (2.5.4.2B)	Required on all plan sheets	N/A	
Ø	Individual plan sheet title that clearly describes the information that is displayed. (2.5.4.2C)	Required on all plan sheets	N/A	
Ø	Source and date of data displayed on the plan. (2.5.4.2D)	Required on all plan sheets	N/A	

Site Plan Application Checklist/December 2020

	Site Plan Specifications – Required Exhibits and Data		
Ŋ	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
	<ol> <li>Existing Conditions: (2.5.4.3A)         <ul> <li>Surveyed plan of site showing existing natural and built features;</li> <li>Existing building footprints and gross floor area;</li> <li>Existing parking areas and number of parking spaces provided;</li> <li>Zoning district boundaries;</li> <li>Existing, required, and proposed dimensional zoning requirements including building and open space coverage, yards and/or setbacks, and dwelling units per acre;</li> <li>Existing impervious and disturbed areas;</li> <li>Limits and type of existing vegetation;</li> <li>Wetland delineation, wetland function and value assessment (including vernal pools);</li> <li>SFHA, 100-year flood elevation line and BFE data, as required.</li> </ul> </li> </ol>	Existing Conditions Plan Sheets	
Ø	<ul> <li>2. Buildings and Structures: (2.5.4.3B)</li> <li>Plan view: Use, size, dimensions, footings, overhangs, 1st fl. elevation;</li> <li>Elevations: Height, massing, placement, materials, lighting, façade treatments;</li> <li>Total Floor Area;</li> <li>Number of Usable Floors;</li> <li>Gross floor area by floor and use.</li> </ul>	Architectural Plan Sheets	
Ø	<ul> <li>3. Access and Circulation: (2.5.4.3C) <ul> <li>Location/width of access ways within site;</li> <li>Location of curbing, right of ways, edge of pavement and sidewalks;</li> <li>Location, type, size and design of traffic signing (pavement markings);</li> <li>Names/layout of existing abutting streets;</li> <li>Driveway curb cuts for abutting prop. and public roads;</li> <li>If subdivision; Names of all roads, right of way lines and easements noted;</li> <li>AASHTO truck turning templates, description of minimum vehicle allowed being a WB-50 (unless otherwise approved by TAC).</li> </ul> </li> </ul>	Site Plan Sheet C-102	
	<ul> <li>4. Parking and Loading: (2.5.4.3D)</li> <li>Location of off street parking/loading areas, landscaped areas/buffers;</li> <li>Parking Calculations (# required and the # provided).</li> </ul>	Site Plan Sheet C-102	
Ø	<ul> <li>5. Water Infrastructure: (2.5.4.3E)</li> <li>Size, type and location of water mains, shut-offs, hydrants &amp; Engineering data;</li> <li>Location of wells and monitoring wells (include protective radii).</li> </ul>	Utilities Plan Sheet C-104	
Ø	<ul> <li>6. Sewer Infrastructure: (2.5.4.3F)</li> <li>Size, type and location of sanitary sewage facilities &amp; Engineering data, including any onsite temporary facilities during construction period.</li> </ul>	Utilities Plan Sheet C-104	

Site Plan Application Checklist/December 2020

$\mathbf{\nabla}$	7. Utilitie	es: (2.5.4.3G)	Litilities Plan Sheet	
	<ul> <li>The s</li> </ul>	ize, type and location of all above & below ground utilities;	C-104	
	<ul> <li>Size t</li> </ul>	ype and location of generator pads, transformers and other		
	fixtur	es.		
⊻	8. Solid \	Waste Facilities: (2.5.4.3H)		
	• The s	ize, type and location of solid waste facilities.	Site Plan Sheet C-102	
$\mathbf{\nabla}$	9. Storm	water Management: (2.5.4.3I)		
	<ul> <li>The log</li> </ul>	ocation, elevation and layout of all storm-water drainage.		
	The lo	ocation of onsite snow storage areas and/or proposed off-	Grading and Drainage	
	site sr	now removal provisions.	Plan Sheet C-103	
	Locati	ion of proposed temporary and permanent material storage		
	locati	ons and distance from wetlands, water bodies, and		
	storm	water structures.		
$\mathbf{N}$	10. Outdo	or Lighting: (2.5.4.3J)		
	• Type a	and placement of all lighting (exterior of building, parking lot	Photometrics Plan	
	and a	ny other areas of the site) and photometric plan.		
	<b>11.</b> Indica	te where dark sky friendly lighting measures have	Photometrics Plan	
	been i	mplemented. (10.1)		
	12. Lands	caping: (2.5.4.3K)	Landasana Dian Chast	
	• ide wł	nich is to be retained:	Landscape Plan Sheet	
	• Lo	cation of any irrigation system and water source.		
$\mathbf{\nabla}$	13. Conto	urs and Elevation: (2.5.4.3L)	Grading and Drainage	
	• Ex	isting/Proposed contours (2 foot minimum) and finished	Plan Sheet C-103	
	gra	ade elevations.		
$\Box$	14. Open	Space: (2.5.4.3M)	Site Plan Sheet	
	• Ty	pe, extent and location of all existing/proposed open space.	C-102	
V	15. All eas	sements, deed restrictions and non-public rights of	Existing Conditions Plan	
	ways.	(2.5.4.3N)	Sheets	
$\mathbf{\nabla}$	16. Chara	cter/Civic District (All following information shall be		
	includ	ed): (2.5.4.3P)		
	• Ap	pplicable Building Height (10.5A21.20 & 10.5A43.30);	Site Plan Sheet	
	• Ap	pplicable Special Requirements (10.5A21.30);	G-102	
	■ Pri	oposed pulluling joining type (10.5A45); oposed community space (10.5A46)		
	• Pi	oposea communicy space (10.3A40).		
R	17. Special	Flood Hazard Areas (2.5.4.3Q)		
	• Tł	ne proposed development is consistent with the need to		
	m	inimize flood damage;		
	• Al	I public utilities and facilities are located and construction to	N/A	
	m	inimize or eliminate flood damage; dequate drainage is provided so as to reduce exposure to		
	• Ad	bood hazards.		

	Other Required Information			
Ŋ	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested	
Ŋ	Traffic Impact Study or Trip Generation Report, as required. (3.2.1-2)	Enclosed		
Q	Indicate where Low Impact Development Design practices have been incorporated. (7.1)	Grading and Drainage Plan Sheet C-103		
Ø	Indicate whether the proposed development is located in a wellhead protection or aquifer protection area. Such determination shall be approved by the Director of the Dept. of Public Works. <b>(7.3.1)</b>	N/A		
Ŋ	Stormwater Management and Erosion Control Plan. (7.4)	Enclosed		
$\mathbf{\nabla}$	Inspection and Maintenance Plan (7.6.5)	Enclosed		

	Final Site Plan Approval Required Information			
Ŋ	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested	
Ø	All local approvals, permits, easements and licenses required, including but not limited to: • Waivers; • Driveway permits; • Special exceptions; • Variances granted; • Easements; • Licenses. (2.5.3.2A)	Cover Sheet		
	<ul> <li>Exhibits, data, reports or studies that may have been required as part of the approval process, including but not limited to: <ul> <li>Calculations relating to stormwater runoff;</li> <li>Information on composition and quantity of water demand and wastewater generated;</li> <li>Information on air, water or land pollutants to be discharged, including standards, quantity, treatment and/or controls;</li> <li>Estimates of traffic generation and counts pre- and post-construction;</li> <li>Estimates of noise generation;</li> <li>A Stormwater Management and Erosion Control Plan;</li> <li>Endangered species and archaeological / historical studies;</li> <li>Wetland and water body (coastal and inland) delineations;</li> <li>Environmental impact studies.</li> </ul> </li> </ul>	Enclosed		
Ŋ	A document from each of the required private utility service providers indicating approval of the proposed site plan and indicating an ability to provide all required private utilities to the site. (2.5.3.2D)	The applicant is currently working with Eversource to get a will serve letter.		

Site Plan Application Checklist/December 2020

Ŋ	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
Ø	A list of any required state and federal permit applications required for the project and the status of same. (2.5.3.2E)	Cover Sheet	
Ø	A note shall be provided on the Site Plan stating: "All conditions on this Plan shall remain in effect in perpetuity pursuant to the requirements of the Site Plan Review Regulations." (2.5.4.2E)	Site Plan Sheet C-102	N/A
	For site plans that involve land designated as "Special Flood Hazard Areas" (SFHA) by the National Flood Insurance Program (NFIP) confirmation that all necessary permits have been received from those governmental agencies from which approval is required by Federal or State law, including Section 404 of the Federal Water Pollution Control Act Amendments of 1972, 33 U.S.C. 1334. (2.5.4.2F)	N/A	
	<ul> <li>Plan sheets submitted for recording shall include the following notes: <ul> <li>a. "This Site Plan shall be recorded in the Rockingham County Registry of Deeds."</li> <li>b. "All improvements shown on this Site Plan shall be constructed and maintained in accordance with the Plan by the property owner and all future property owners. No changes shall be made to this Site Plan without the express approval of the Portsmouth Planning Director."</li> </ul> </li> <li>(2.13.3)</li> </ul>	Site Plan Sheet C-102	N/A
		5/20/2024	

City of Portsmouth Planning Department

# Site Plan Review Application Fee

Project:	1035 Lafayette Rd		Map/Lot: Map 246 Lo	:1
Applicant:	Portsmouth Housing Authors	ority		
All developme	ent			
Base fee \$600	)		[	\$600.00
Plus \$5.00 pei	r \$1,000 of site costs Site costs	\$1,000,000	+[	\$5,000.00
Plus \$10.00 p	<i>er 1,000 S.F. of site develop</i> Site development area	ment area 142,460 S	5.F. <b>+</b> [	\$1,424.60
			Fee	\$7,024.60
Maximum fee	e: \$20,000.00			
Fee received	by:		Date:	

Note: Initial application fee may be based on the applicant's estimates of site costs and site development area. Following site plan approval, the application fee will be recalculated based on the approved site plan and site engineer's corresponding site cost estimate as approved by the Department of Public Works, and any additional fee shall be paid prior to the issuance of a building permit.


L0700-026C May 20, 2024

Mr. Peter Britz, Director of Planning & Sustainability City of Portsmouth Planning & Sustainability Department 1 Junkins Avenue Portsmouth NH, 03801

#### Re: Lonza Biologics – Proposed PV Solar Carports Amended Site Plan Review Application LU-23-108

Dear Peter:

On behalf of Lonza Biologics, Inc. (Lonza), we are pleased to submit one (1) set of hard copies and one electronic file (.pdf) of the following information to support a request to the Planning Board for a recommendation for approval to the Pease Development Authority (PDA) for Amended Site Plan Review for a proposed industrial development located at 5 Technology Way, (Formerly 70 Corporate Drive) on Pease International Tradeport:

- PDA Application for Site Review, dated May 20, 2024;
- Site Plan Set, last revised May 20, 2024;
- Drainage Memo, dated May 20, 2024;
- Glare Study Results, dated February 22, 2024;

#### **PROJECT SUMMARY**

#### Background

The existing project was granted Site Plan approval on January 17, 2019, and amended by administrative approvals on September 27, 2019, January 27, 2023, and Amended Site Plan Approval on November 16, 2023.

#### **Existing Condition**

The project is located on the portion of Lonza's 46-acre parcel refered to as the Iron Parcel. The following summarizes the work currently approved through the November 16, 2023 Amended Site Plan Approval:

- Daylighting of Hodgson Brook on the Iron Parcel
- Removal of the existing Hodgson Brook culvert
- Construction of the sidewalk and landscaping along Corporate Drive
- Completion of Soils Management Plan
- Construction of Building #1
- Construction of the Central Utility Building
- Construction site improvements for Building #1 such as drive aisles, fire lanes, utilities, lighting, sidewalks and stormwater management.
- Construction of a temporary 150-space surface parking lot, sidewalks and stormwater management.

#### Amended Site Plan

The requested Site Plan amendment includes the construction of Photovoltaic Cell (PV) Solar canopies over the previously approved temporary surface parking lot. The addition of these Solar Canopies is being requested to support Lonza Biologics green infrastructure and sustainability initiatives. The addition of these Solar canopies will not result in any dimensional changes to the previously approved parking lot. There is a slight increase in impervious surfaces (~672 SF) which will not cause any adverse impact to the previously approved Phase 2 Drainage design as outlined in the Drainage Memorandum.

The proposed PV Solar system will require additional electrical infrastructure and modifications to the photometric lighting design as depicted in the enclosed Site Plan Set. The proposed system will not be connected to the larger electrical grid network but has been designed to supplement and reduce the proposed project's electrical demand.

We respectfully request to be placed on the Technical Advisory Committee (TAC) meeting agenda for June 4, 2024. If you have any questions or need any additional information, please contact Neil Hansen by phone at (603) 294-9213 or by email at <a href="mailto:nahansen@tighebond.com">nahansen@tighebond.com</a>.

Sincerely,

#### TIGHE & BOND, INC.

Neil A. Hansen, PE Project Manager

Copy: Lonza Biologics (via email) Pease Development Authority

Patrick M. Crimmins, PE Vice President

 $\label{eq:linear} J:\LD700 Lonza Biologics Expansion was 1576F\026_Project Albacore\Report_Evaluations\Applications\PDA\Solar\PDA Submission\L0700-026C_TAC Cover Letter.docx$ 

#### Pease Development Authority 55 International Drive, Portsmouth, NH 03801, (603) 433-6088



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#### Application for Site Review

For PDA Use Only			
Date Submitted:	Municipal Review:	Fee:	
Application Complete:	Date Forwarded:	Paid:	Check #:

#### Applicant Information

Applicant: Lonza Biologics, Inc.	Agent: Tighe & Bond, Inc.
Address: 101 International Drive	Address: 177 Corporate Drive
Portsmouth, NH 03801	Portsmouth, NH 03801
Business Phone: 603-570-3625	Business Phone: 603-433-8818
Mobile Phone:	Mobile Phone:
Fax:	Fax:

#### Site Information

Portsmouth Tax Map: 305	Lot #: 006	<sup>Zone:</sup> Airport, Business, Commercial
Site Address / Location : 101 International Drive, Portsmouth, NH 03801		
Site Address / Location :		Area of On-site Wetlands: 4,087 SF

#### **Activity Information**

Change of Use:	Yes [ ]	No [X]	Existing Use: Office/Research/Manufacturing
			Proposed Use: Office/Research/Manufacturing
Description of Proje	ect:		
The requeste	ed Site P	'lan ame	ndment includes the construction of Photovoltaic Cell (PV)
Solar canopie	es over t	the previ	ously approved temporary surface parking lot.
	-		
All above inform	nation shal	ll be showr	on a site plan submitted with this application. Provide 3 full size hard copies and one
PDF copy of all app	plication m	aterials as	well as one half-size set of drawings to PDA. Applicant shall supply additional copies as
may be requir	red by appl	licable mui	nicipality. Refer to Chapter 400 of PDA land Use Controls for additional information.

#### Certification

I hereby certify under the penalties of perjury that the foregoing inform are true and complete to the best of my knowledge. I hereby apply for a any conditions established by the Review Committee(s) and PD	nation and accompanying plans, documents, and supporting data Site Review and acknowledge I will comply with all regulations and A Board in the development and construction of this project.
Signature of Applicant	20 Mc V 24 Date
Michael Feeney Printed Name	

N:\Engineer\ ApplicationforSiteReview.xlsx

# **IRON PARCEL DEVELOPMENT - SOLAR 5 TECHNOLOGY WAY** (FORMERLY 70 CORPORATE DRIVE)

# PORTSMOUTH, NEW HAMPSHIRE PROJECT NO: L-0700-26 MAY 20, 2024

LIST OF DRAWINGS				
SHEET NO.	SHEET TITLE	LAST REVISED		
	COVER SHEET	5/20/2024		
C-161	PHASE 2 DEMOLITION PLAN	5/20/2024		
C-164	PHASE 2 OVERALL SITE PLAN	5/20/2024		
C-165	PHASE 2 SITE PLAN	5/20/2024		
C-168	PHASE 2 GRADING, DRAINAGE & EROSION CONTROL PLAN	5/20/2024		
C-171	PHASE 2 UTILITIES PLAN	5/20/2024		
C-174	PHASE 2 LANDSCAPE PLAN	5/20/2024		
C-177	PHASE 2 PHOTOMETRIC LIGHTING PLAN	5/20/2024		
C-501	EROSION CONTROL NOTES & DETAILS SHEET	5/20/2024		
C-503	DETAILS SHEET	5/20/2024		
8-046-3	SOLAR CANOPY DETAILS	5/20/2024		



LESSOR:

CLIENT:

CIVIL ENGINEER:

SURVEYOR:

WETLAND SCIENTIST: GOVE ENVIRONMENTAL SERVICES, INC. 8 CONTINENTAL DRIVE, UNIT H EXETER, NEW HAMPSHIRE 03833

LOCATION MAP SCALE: 1" = 2,000'

LIST OF PERMITS			
LOCAL	STATUS	DATE	
SITE PLAN REVIEW PERMIT	APPROVED	1/17/2019	
AMENDED SITE PLAN REVIEW PERMIT	APPROVED	11/16/2023	
AMENDED SITE PLAN REVIEW PERMIT - SOLAR			
STATE			
NHDES - ALTERATION OF TERRAIN PERMIT	ISSUED: AOT-1498	10/02/2018	
NHDES - WETLANDS PERMIT	ISSUED: #2018-01731	12/21/2018	
FEDERAL			
EPA - NPDES CGP (SWPPP)	ACTIVE: NHR1001SK	7/7/2023	





PEASE DEVELOPMENT AUTHORITY **55 INTERNATIONAL DRIVE** PORTSMOUTH, NEW HAMPSHIRE 03801

LONZA BIOLOGICS 101 INTERNATIONAL DRIVE PORTSMOUTH, NH 03801

## Tighe&Bond

177 CORPORATE DRIVE PORTSMOUTH, NEW HAMPSHIRE 03801

DOUCET SURVEY, INC. 102 KENT PLACE NEWMARKET, NEW HAMPSHIRE 03857

# **ISSUED FOR AMENDED SITE REVIEW COMPLETE SET 11 SHEETS**



- REQUIRED TO COMPLETE THE WORK.
- APPROPRIATE UTILITY COMPANY.
- ADDITIONAL COST TO THE OWNER.
- THE PERMIT APPROVALS.
- THE AUTHORITIES HAVING JURISDICTION.
- SPECIFIED IN NOTE #25.

- LIMITS OF PAVEMENT REMOVAL PRIOR TO BID. BUILDING SLABS, FOUNDATION, TREES AND LANDSCAPING.
- DEVELOPMENT AUTHORITY.
- STATE, AND LOCAL LAWS AND REGULATIONS.
- ACCUMULATED TO 1/3 THE DESIGN DEPTH OF THE BARRIER
- DEMOLITION ACTIVITIES.
- CONSTRUCTION SITE.
- ALLOW 7 CALENDAR DAYS FOR PROCESSING.
- PEASE DEVELOPMENT AUTHORITY.
- PRIOR TO CONSTRUCTION.

#### **DEMOLITION NOTES:** Tighe&Bond 1. THE LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE NOT GUARANTEED BY THE OWNER OR THE ENGINEER. IT IS THE CONTRACTOR'S RESPONSIBILITY TO LOCATE ALL UTILITIES, ANTICIPATE CONFLICTS, REPAIR EXISTING UTILITIES AND RELOCATE EXISTING UTILITIES THE CONTRACTOR SHALL VERIFY LOCATION OF ALL EXISTING UTILITIES. CALL DIG SAFE AT LEAST 72 HOURS PRIOR TO THE COMMENCEMENT OF ANY DEMOLITION/CONSTRUCTION ACTIVITIES. ALL MATERIALS SCHEDULED TO BE REMOVED SHALL BECOME THE PROPERTY OF THE CONTRACTOR UNLESS OTHERWISE SPECIFIED. THE CONTRACTOR SHALL DISPOSE OF ALL MATERIALS OFF-SITE IN ACCORDANCE WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS, ORDINANCES AND CODES EXCEPT AS SPECIFIED IN 4. COORDINATE REMOVAL, RELOCATION, DISPOSAL OR SALVAGE OF UTILITIES WITH THE OWNER AND 5. ANY EXISTING WORK OR PROPERTY DAMAGED OR DISRUPTED BY CONSTRUCTION/ DEMOLITION ACTIVITIES SHALL BE REPLACED OR REPAIRED TO MATCH ORIGINAL EXISTING CONDITIONS BY THE CONTRACTOR AT NO 6. SAW CUT AND REMOVE PAVEMENT ONE (1) FOOT OFF PROPOSED EDGE OF PAVEMENT OR EXISTING CURB LINE IN ALL AREAS WHERE PAVEMENT TO BE REMOVED ABUTS EXISTING PAVEMENT OR CONCRETE TO 7. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FAMILIARIZE THEMSELVES WITH THE CONDITIONS OF ALL OF 8. THE CONTRACTOR SHALL OBTAIN AND PAY FOR ADDITIONAL PERMITS, NOTICES AND FEES NECESSARY TO COMPLETE THE WORK AND ARRANGE FOR AND PAY FOR NECESSARY INSPECTIONS AND APPROVALS FROM 9. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL DEMOLITION AND OFF-SITE DISPOSAL OF MATERIALS NEW HA REQUIRED TO COMPLETE THE WORK, EXCEPT FOR WORK NOTED TO BE COMPLETED BY OTHERS AND AS PATRICK CRIMMINS 10. UTILITIES SHALL BE TERMINATED AT THE MAIN LINE PER UTILITY COMPANY AND THE CITY OF PORTSMOUTH STANDARDS. THE CONTRACTOR SHALL REMOVE ALL ABANDONED UTILITIES LOCATED WITHIN THE LIMITS No. 12378 CERSE TIN STOWAL . 11. CONTRACTOR SHALL VERIFY ORIGIN OF ALL DRAINS AND UTILITIES PRIOR TO REMOVAL/TERMINATION TO DETERMINE IF DRAINS OR UTILITY IS ACTIVE, AND SERVICES ANY ON OR OFF-SITE STRUCTURE TO REMAIN. 5/20/24//////// THE CONTRACTOR SHALL NOTIFY ENGINEER IMMEDIATELY OF ANY SUCH UTILITY FOUND AND SHALL MAINTAIN THESE UTILITIES UNTIL PERMANENT SOLUTION IS IN PLACE. 12. PAVEMENT REMOVAL LIMITS ARE SHOWN FOR CONTRACTOR'S CONVENIENCE. ADDITIONAL PAVEMENT REMOVAL MAY BE REQUIRED DEPENDING ON THE CONTRACTOR'S OPERATION. CONTRACTOR TO VERIFY FULL E NEW H 13. THE CONTRACTOR SHALL REMOVE AND DISPOSE OF ALL EXISTING STRUCTURES, CONCRETE PADS, UTILITIES NEIL AND PAVEMENT WITHIN THE WORK LIMITS SHOWN UNLESS SPECIFICALLY IDENTIFIED TO REMAIN. ITEMS TO Α. HANSEN BE REMOVED INCLUDE BUT ARE NOT LIMITED TO: CONCRETE, PAVEMENT, CURBS, LIGHTING, MANHOLES, No. 15227 CATCH BASINS, UNDER GROUND PIPING, POLES, STAIRS, SIGNS, FENCES, RAMPS, WALLS, BOLLARDS, 14. COORDINATE ALL WORK WITHIN THE PUBLIC RIGHT OF WAYS WITH THE CITY OF PORTSMOUTH AND PEASE 05/20/2024 15. REMOVE TREES AND BRUSH AS REQUIRED FOR COMPLETION OF WORK. CONTRACTOR SHALL GRUB AND REMOVE ALL STUMPS WITHIN LIMITS OF WORK AND DISPOSE OF OFF SITE IN ACCORDANCE WITH FEDERAL, 16. CONTRACTOR SHALL PROTECT ALL PROPERTY MONUMENTATION THROUGHOUT DEMOLITION AND CONSTRUCTION OPERATIONS. SHOULD ANY MONUMENTATION BE DISTURBED BY BY THE CONTRACTOR, THE CONTRACTOR SHALL EMPLOY A NEW HAMPSHIRE LICENSED SURVEYOR TO REPLACE DISTURBED MONUMENTS 17. PROVIDE INLET PROTECTION BARRIERS AT ALL CATCH BASINS/CURB INLETS WITHIN CONSTRUCTION LIMITS AS WELL AS CATCH BASINS/CURB INLETS THAT MAY RECEIVE RUNOFF FROM CONSTRUCTION ACTIVITIES. INLET PROTECTION BARRIERS SHALL BE MAINTAINED FOR THE DURATION OF THE PROJECT. INLET PROTECTION BARRIERS SHALL BE "HIGH FLOW SILT SACK" BY ACF ENVIRONMENTAL OR EQUAL. INSPECT SCALE IN FEET BARRIERS WEEKLY AND AFTER EACH RAIN EVENT OF 0.25 INCHES OR GREATER. CONTRACTOR SHALL COMPLETE A MAINTENANCE INSPECTION REPORT AFTER EACH INSPECTION. SEDIMENT DEPOSITS SHALL BE REMOVED AFTER EACH STORM EVENT OR MORE OFTEN IF THE FABRIC BECOMES CLOGGED OR SEDIMENT HAS GRAPHIC SCALE 18. THE CONTRACTOR SHALL PHASE DEMOLITION AND CONSTRUCTION AS REQUIRED TO PROVIDE CONTINUOUS SERVICE TO EXISTING BUSINESSES THROUGHOUT THE CONSTRUCTION PERIOD. EXISTING BUSINESS SERVICES INCLUDE, BUT ARE NOT LIMITED TO ELECTRICAL, COMMUNICATION, FIRE PROTECTION, DOMESTIC Proposed WATER AND SEWER SERVICES. TEMPORARY SERVICES, IF REQUIRED, SHALL COMPLY WITH ALL FEDERAL STATE, LOCAL AND UTILITY COMPANY STANDARDS. CONTRACTOR SHALL PROVIDE DETAILED CONSTRUCTION Industrial SCHEDULE TO OWNER PRIOR TO ANY DEMOLITION/CONSTRUCTION ACTIVITIES. 19. EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO THE START OF ANY CLEARING OR Development 20. THE CONTRACTOR SHALL PAY ALL COSTS NECESSARY FOR TEMPORARY PARTITIONING, BARRICADING, FENCING, SECURITY AND SAFETY DEVICES REQUIRED FOR THE MAINTENANCE OF A CLEAN AND SAFE 21. SAW CUT AND REMOVE PAVEMENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL UTILITIES TO BE REMOVED AND PROPOSED UTILITIES LOCATED IN EXISTING PAVEMENT AREAS TO REMAIN. Lonza Biologics 22. THE CONTRACTOR SHALL ACQUIRE A PDA DIG PERMIT BEFORE ANY EARTH DISTURBANCE CAN TAKE PLACE 23. ALL MONITORING WELLS WITHIN LIMIT OF WORK SHALL BE PROTECTED DURING CONSTRUCTION. IF ANY MONITORING WELL NEEDS TO BE REMOVED OR ADJUSTED THIS WORK SHALL BE COORDINATED WITH THE 24. CONTRACTOR SHALL COORDINATE WITH THE PROJECT SURVEYOR FOR BENCHMARK AND CONTROL POINTS 25. ALL EXCESS SOIL RESULTING FROM THE CONSTRUCTION SHALL REMAIN ON SITE. COORDINATE WITH OWNER AND PEASE DEVELOPMENT AUTHORITY ON FINAL LOCATION OF EXCESS MATERIALS. Portsmouth, 26. BEFORE ANY DEWATERING IS PERFORMED, COORDINATION BETWEEN THE OWNER, CONTRACTOR, PDA, NHDES AND THE AIR FORCE IS REQUIRED TO DETERMINE PROPER PROCEDURES AND PERMITTING REQUIRED New Hampshire AT A MINIMUM A NHDES TEMPORARY DISCHARGE PERMIT IS REQUIRED. Q 5/20/2024 Solar - Amended Approval 4/2/2024 Ph2 IFC Addendum #1 Р 12/15/2023 Ph2 Issued for Constructio 0 N 11/9/2023 Revised P.B. Submission M 9/27/2023 P.B. Submission 9/1/2022 Issued for Construction K 5/27/2022 Issued for Bid MARK DATE DESCRIPTION PROJECT NO: L-0700-013 DATE: 04/03/2018 FILE: L-0700-026-C-DSGN.dwg DRAWN BY CJK CHECKED: NAH APPROVED: PMC PHASE 2 DEMOLITION PLAN MATCH LINE SHEET 1 AS SHOWN SCALE: MATCH LINE SHEET 2 C-161



<u>SITE DATA</u>			PARKING REC
LOCATION: TAX MAP 305, LOTS 1 & 2	TAX MAP 305, LOT	6	
70 & 80 CORPORATE DRIVE	101 INTERNATIONA	L DRIVE	REQUIRED PARI
PORTSMOUTH, NH	PORTSMOUTH, NH		2 SPACES
			990 EXIST
ZONING DISTRICT: AIRPORT, BUSINESS	& COMMERCIAL (ABC)		<u>180 ANTIC</u>
			TOTAL RE
DIMENSIONAL REQUIREMENTS:			
	REQUIRED		PARKING PROV
	5 AC	$\frac{PROVIDED}{43.4 \pm AC}$	EXISTING
MINIMUM COT ARLA.		43.41 AC	PROPOSEL
MINIMUM STREET FRONTAGE.	200 FT	1,030 FT	TOTAL:
MINIMUM FRONT YARD SETBACK.	70 FT	70 FT	
SIDE SETBACK	30 FT	30 FT	
REAR SETBACK	50 FT	51 FT	
	5511	5111	



## LEGEND

MATCH LINE PROPOSED PROPERTY LINE PROPOSED SETBACK LINE PROPOSED LIMIT OF WORK PROPOSED GRANITE CURB

PROPOSED PAVEMENT SECTION

PROPOSED GRAVEL SECTION

PROPOSED CONCRETE

CONSTRUCT BUILDING TYPICAL COORDINATE PROPOSED CURB RADIUS VERTICAL GRANITE CURB SLOPED GRANITE CURB RIGHT OF WAY DOUBLE SOLID YELLOW LINE SINGLE SOLID WHITE LINE

EXISTING) — CONST TIP DOWN RAMP — CONST

BEGIN VGC (MEET/MATCH

AND STOP BAR - CONST TIP DOWN RAMP - BEGIN VGC (MEET/MATCH EXISTING)

R1-1 "STOP SIGN"

MATCH LINE SHEET 1 MATCH LINE SHEET 2



E SHEET 2



Z₽

GRADING AND DRAINAGE NOT	ES:	<b>Tighe&amp;Bond</b>
AREAS 95%		
95%		
5 90% ON SHALL BE OF THE MAXIMUM DRY D CONTROLLED IN ACCORDANCE WI DE IN ACCORDANCE WITH ASTM D-1!	Z DENSITY AT THE OPTIMUM MOISTURE TH ASTM D-1557, METHOD C FIELD 556 OR ASTM-2922.	
SHALL BE HIGH DENSITY POLYETHYLI THERWISE SPECIFIED.	ENE (HANCOR HI-Q, ADS N-12 OR	
HBASINS, CURB BOXES, ETC. WITHI A FINISH PAVEMENT SURFACE AND EAS INCLUDE BUILDING ENTRANCES DING.	N LIMITS OF WORK TO FINISH GRADE. LAWN AREAS FREE OF LOW SPOTS ANE 5, EXITS, RAMPS AND LOADING DOCK	)
GHLY CLEAN ALL CATCHBASINS AND ATELY UPON COMPLETION OF CONST JCTION SHALL CONFORM WITH APPL	DRAIN LINES, WITHIN THE LIMIT OF RUCTION. ICABLE FEDERAL, STATE AND LOCAL	
O BE PAVED OR OTHERWISE TREATE	D SHALL RECEIVE 6" LOAM, SEED	NINININI OF NEW HAMPS
TION SHALL BE IN ACCORDANCE WI	TH THE NHDOT STANDARD	
AYS AND BRIDGES, LATEST EDITION. SHALL BE EQUIPPED WITH OIL/GAS BUILT PLANS IN DIGITAL FORMAT (.C COMPLETION OF THE PROJECT. AS-E IRE LICENSED LAND SURVEYOR.	SEPARATOR HOODS AND 4' SUMPS. WG AND .PDF FILES) ON DISK TO THE SUILTS SHALL BE PREPARED AND	5/20/24
O THE CITY OF PORTSMOUTH DEPAR	TMENT OF PUBLIC WORKS, STANDARD	NEIL NEIL
OF ROAD AND BRIDGE CONSTRUCTION	ON", CURRENT EDITION.	A. HANSEN No. 15227
PDA, GROUNDWATER DISCHARGE F N OF BUILDING 1 AND THE CENTRAL RAINAGE SYSTEM. IF TREATMENT O D DURING THE BUILDING PERMITTING LTRATION SYSTEM WILL BE NEEDED	THE PROPOSED FOUNDATION UTILITY BUILDING WILL BE F THE GROUNDWATER DISCHARGE IS G PROCESS AND RE-INFILTRATION IS	CENSED ING
EROSION CONTROL NOTES: ARRIERS AS SHOWN AS FIRST ORDE	R OF WORK.	
ROL NOTES ON DETAIL SHEETS. AROUND ALL EXISTING AND PROPOS THE DURATION OF THE PROJECT UN	ED CATCHBASIN INLETS WITHIN THE TIL PAVEMENT HAS BEEN INSTALLED.	
JCTION ENTRANCES. ND SILT FENCES DAILY AND AFTER I DTECTION AS NECESSARY TO MAXIM /3 THE FILTER HEIGHT.	SCALE IN FEET	
O BE PAVED OR OTHERWISE TREATE	D SHALL RECEIVE 6" LOAM, SEED,	GRAPHIC SCALE
DISTURBANCE COMMENCING ON TH CANT SHALL INSTALL ALL EROSION A JIRED BY STATE AND LOCAL PERMITS DNSIBLE TO CONTROL DUST AND WI T CONTROL MEASURES SHALL INCLU SUBJECT TO ARID CONDITIONS. OVE AND PROPERLY DISPOSE OF ALL DF CONSTRUCTION AND FINAL STABA PIPING SHALL BE THOROUGHLY CLEA IAS BEEN PAVED.	E SUBJECT PROPERTY, INCLUDING AND SILTATION MITIGATION AND S AND APPROVALS. ND EROSION THROUGHOUT THE DE, BUT NOT LIMITED TO, SPRINKLING TEMPORARY EROSION CONTROL ALIZATION. ANED TO REMOVE ALL SEDIMENT AND	Proposed Industrial Development
SHALL BE SURROUNDED BY SILT FEN DL SEEDING. STOCKPILE AREAS TO E TLAND. OVIDED AROUND STOCKPILES OVER	ICE AND SHALL BE STABILIZED BY BE LOCATED AS FAR AS POSSIBLE FROM 10 FT.	Lonza Biologics
EQUIRED TO WASH OUT (IF NECESS PLACED. NO OTHER WASH OUT WILL	ARY) SHOOTS ONLY WITHIN AREAS BE ALLOWED.	
<u>L</u>	EGEND	Portsmouth
	MATCH LINE	New Hampshire
<b>_</b>	PROPOSED PROPERTY LINE PROPOSED CONTOUR LINE	
	PROPOSED DRAIN LINE (TYP) PROPOSED SILT SOCK	
0	INLET PROTECTION SILT SACK	
	PROPOSED CATCHBASIN PROPOSED DOUBLE GRATE	Q 5/20/2024 Solar - Amended Approval
<b>()</b>	CATCHBASIN PROPOSED DRAIN MANHOLE	P         4/2/2024         Ph2 IFC Addendum #1
CONST	CONSTRUCT	O12/15/2023Ph2 Issued for ConstructionN11/9/2023Revised P.B. Submission
BLDG	BUILDING	M 9/27/2023 P.B. Submission
COORD	COORDINATE	L9/1/2022Issued for ConstructionK5/27/2022Issued for Bid
RD VIF	ROOF DRAIN VERIFY IN FIFLD	MARK DATE DESCRIPTION
TC	TOP OF CURB	PROJECT NO:         L-0700-013           DATE:         04/03/2018
BC	BOTTOM OF CURB	FILE: L-0700-026-C-DSGN.dwg DRAWN BY: C1K
		CHECKED: NAH
		PHASE 2 GRADING, DRAINAGE & EROSION
ET 1		CONTROL PLAN
ET 2		SCALE: AS SHOWN
		C-108



P

NOT GUARANTEED BY THE OV ALL UTILITIES, ANTICIPATE REQUIRED TO COMPLETE THE 2. COORDINATE ALL UTILITY WO

- NATURAL GAS UNITI WATER - CITY OF POR SEWER - CITY OF POR ELECTRIC - EVERSOUR COMMUNICATIONS -
- 3. SEE EXISTING CONDITIONS 4. SEE GRADING, DRAINAGE & E
- MEASURES. 5. ALL WATER MAIN INSTALLATI 6. ALL WATER MAIN INSTALLATI
- PRIOR TO ACTIVATING THE S WITH THE CITY OF PORTSMO 7. ALL SEWER PIPE SHALL BE FI
- STATED.
- 8. ALL WORK WITHIN PORTSMO PEASE DEVELOPMENT AUTHO 9. CONTRACTOR SHALL MAINTA
- CONSTRUCTION.
- 10. CONNECTIONS TO EXISTING STANDARDS.
- 11. EXISTING UTILITIES TO BE R PORTSMOUTH DEPARTMENT SERVICES.
- 12. ALL ELECTRICAL MATERIAL W EDITION, AND ALL APPLICABL
- 13. THE EXACT LOCATION OF NEV BUILDING DRAWINGS AND TH
- 14. ADJUST ALL MANHOLES, CAT
- 15. ALL UNDERGROUND CONDUI
- 16. THE CONTRACTOR SHALL OB ALL INSPECTIONS, AND SUBN COMPLETION OF THIS PROJEC
- 17. THE CONTRACTOR SHALL PRO PLATES, AND OTHER MISCELL
- RENDER INSTALLATION OF U 18. CONTRACTOR SHALL PROVID
- SERVICES. 19. A 10-FOOT MINIMUM EDGE T WATER AND SANITARY SEWE
- SHALL BE PROVIDED AT ALL
- 20. THE CONTRACTOR SHALL COI CONTRACTOR SHALL HAVE TH
- 21. CONTRACTOR TO SUBMIT AS-
- OWNER AND ENGINEER UPON CERTIFIED BY A NEW HAMPSH
- 22. SAWCUT AND REMOVE PAVE UTILITIES LOCATED IN EXIST
- 23. HYDRANTS, GATE VALVES, FI
- PORTSMOUTH AND THE PEAS 24. COORDINATE TESTING OF SE
- 25. ALL SEWER PIPE WITH LESS
- AREAS SHALL BE INSULATED.
- 26. CONTRACTOR SHALL COORDI
- CONSTRUCTION, MANHOLE C
- **RELOCATION, AND TRANSFOR**
- 27. CONTRACTOR SHALL PHASE CONSTRUCTION, AS TO MAIN
- COORDINATE TEMPORARY SE
- 28. SITE LIGHTING SPECIFICATIO
- SIGN ILLUMINATION SHALL
- 29. CONTRACTOR SHALL CONSTR
- AND CONNECT THESE TO SEF
- 30. EXISTING SEWER MAIN AND UNDERWOOD ENGINEERS, DA PROPOSED ON-SITE SEWER
- CONSTRUCTION. THE CONT
- PORTSMOUTH, AND VERIFY A 31. LOCATION SHOWN IS APPROX
- BY UNITIL. WORK IN CORPOR
- RECONSTRUCTION OF CORPO 32. LOCATION AND TYPE SHOWN
- ASSOCIATED INFRASTRUCTU NEED TO BE COMPLETED IN
- COORDINATE WITH CITY OF F
- 33. FINAL LOCATION OF ALL WAT PORTSMOUTH DPW PRIOR TO
- 34. FINAL LOCATION OF FIRE HYD COORDINATED WITH THE BUI
- PRIOR TO CONSTRUCTION. 35. THE APPLICANT SHALL HAVE APPROVED BY THE CITY'S CO FAMILIAR AND CONVERSANT INDICATES IT IS NECESSARY PROJECT, THOSE COSTS SHA COORDINATE WITH THE SUPE 36. CONTRACTOR SHALL PERFOR CONSTRUCTION AND SHALL
- 37. CONTRACTOR SHALL DISPOS AND LOCAL REGULATIONS SH 38. COORDINATE LIGHTING CON 39. ABANDON EXISTING SEWERS INSTALLED, TESTED, AND AC
- ABANDONED BY PLACING CO SECTION 02280. 40. CONTRACTOR SHALL COORDI
- QUANTITY WITH COMMUNICA
  - MATCH LINE SHEE
    - MATCH LINE SHEE

UTILITY NOTES: G UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE WNER OR ENGINEER. IT IS THE CONTRACTOR'S RESPONSIBILITY TO LOCATE CONFLICTS, REPAIR EXISTING UTILITIES, AND RELOCATE EXISTING UTILITIES E WORK AT NO ADDITIONAL COST TO THE OWNER. ORK WITH APPROPRIATE UTILITY COMPANY.	<b>Tighe&amp;Bond</b>
L TSMOUTH DPW RTSMOUTH DPW RCE	
PLAN FOR BENCHMARK INFORMATION. EROSION CONTROL PLAN FOR PROPOSED GRADING AND EROSION CONTROL	
IONS SHALL BE CLASS 52, CEMENT LINED DUCTILE IRON PIPE. IONS SHALL BE PRESSURE TESTED AND CHLORINATED AFTER CONSTRUCTION SYSTEM. CONTRACTOR SHALL COORDINATE CHLORINATION AND TESTING OUTH WATER DEPARTMENT. IBERGLASS REINFORCED POLYMER MORTAR (FRP) PIPE UNLESS OTHERWISE	
OUTH ROWS SHALL BE COORDINATED WITH CITY OF PORTSMOUTH AND THE	
IRITY. IN UTILITY SERVICES TO ABUTTING PROPERTIES THROUGHOUT	
WATER MAIN SHALL BE CONSTRUCTED TO CITY OF PORTSMOUTH	PATRICK
EMOVED SHALL BE CAPPED AT THE MAIN AND MEET THE CITY OF OF PUBLIC WORKS STANDARDS FOR CAPPING OF WATER AND SEWER	CRIMMINS PROPERTY OF A CENTRE
VORKMANSHIP SHALL CONFORM TO THE NATIONAL ELECTRIC CODE, LATEST LE STATE AND LOCAL CODES. W UTILITY SERVICES AND CONNECTIONS SHALL BE COORDINATED WITH THE HE UTILITY COMPANIES.	5/20/24/////////////////////////////////
CH BASINS, CURB BOXES, ETC. WITHIN LIMITS OF WORK TO FINISH GRADE. TS SHALL HAVE NYLON PULL ROPES TO FACILITATE PULLING CABLES. TAIN, PAY FOR, AND COMPLY WITH ALL REQUIRED PERMITS, ARRANGE FOR MIT COPIES OF ACCEPTANCE CERTIFICATES TO THE OWNER PRIOR TO THE CT.	NEW HAMAN
OVIDE AND INSTALL ALL MANHOLES, BOXES, FITTINGS, CONNECTORS, COVER LANEOUS ITEMS NOT NECESSARILY DETAILED ON THESE DRAWINGS TO TILITIES COMPLETE AND OPERATIONAL. DE EXCAVATION, BEDDING, BACKFILL AND COMPACTION FOR NATURAL GAS	No. 15227
O EDGE HORIZONTAL SEPARATION SHALL BE PROVIDED BETWEEN ALL R LINES. AN 18-INCH MINIMUM OUTSIDE TO OUTSIDE VERTICAL SEPARATION WATER/SANITARY SEWER CROSSINGS. NTACT "DIG-SAFE" 72 HOURS PRIOR TO COMMENCING CONSTRUCTION. THE HE "DIG-SAFE" NUMBER ON SITE AT ALL TIMES. B-BUILT PLANS IN DIGITAL FORMAT (.DWG AND .PDF FILES) ON DISK TO THE	
N COMPLETION OF THE PROJECT. AS-BUILTS SHALL BE PREPARED AND HIRE LICENSED LAND SURVEYOR. MENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL PROPOSED FING PAVEMENT AREAS TO REMAIN. ITTINGS, ETC. SHALL MEET THE REQUIREMENTS OF THE CITY OF SE DEVELOPMENT AUTHORITY.	SCALE IN FEET 0 40' 80'
EWER CONSTRUCTION WITH THE CITY OF PORTSMOUTH. THAN 6' OF COVER IN PAVED AREAS OR LESS THAN 4' OF COVER IN UNPAVED	GRAFIIC SCALL
 INATE ALL ELECTRIC WORK INCLUDING BUT NOT LIMITED TO: CONDUIT CONSTRUCTION, UTILITY POLE CONSTRUCTION, OVERHEAD WIRE RMER CONSTRUCTION WITH POWER COMPANY. UTILITY CONSTRUCTION, PARTICULARLY WATER MAIN AND GAS MAIN ↓TAIN CONTINUOUS SERVICE TO ABUTTING PROPERTIES. CONTRACTOR SHALL ERVICES TO ABUTTERS WITH THE UTILITY COMPANY AND AFFECTED ABUTTER. ONS, CONDUIT LAYOUT AND CIRCUITRY FOR PROPOSED SITE LIGHTING AND BE PROVIDED BY THE PROJECT ELECTRICAL ENGINEER.	Proposed Industrial Development
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<ul> <li></li> <li>INATE ALL ELECTRIC WORK INCLUDING BUT NOT LIMITED TO: CONDUIT INATE ALL ELECTRIC WORK INCLUDING BUT NOT LIMITED TO: CONDUIT CONSTRUCTION, UTILITY POLE CONSTRUCTION, OVERHEAD WIRE RMER CONSTRUCTION WITH POWER COMPANY.</li> <li>UTILITY CONSTRUCTION, PARTICULARLY WATER MAIN AND GAS MAIN VTAIN CONTINUOUS SERVICE TO ABUTTING PROPERTIES. CONTRACTOR SHALL RVICES TO ABUTTERS WITH THE UTILITY COMPANY AND AFFECTED ABUTTER.</li> <li>DNS, CONDUIT LAYOUT AND CIRCUITRY FOR PROPOSED SITE LIGHTING AND BE PROVIDED BY THE PROJECT ELECTRICAL ENGINEER.</li> <li>RUCT ALL UTILITIES AND DRAINS TO WITHIN 10' OF THE FOUNDATION WALLS RVICE STUBS FROM THE BUILDING.</li> <li>STRUCTURES IN GOOSE BAY DRIVE ARE BASED ON A PROPOSED DESIGN BY ATED JULY 28, 2017, AND WAS CONSTRUCTED IN SUMMER 2018. THE DESIGN ELEVATIONS ARE BASED ON THE UNDERWOOD PLAN DURING RACTOR SHALL COORDINATE SEWER CONSTRUCTION WITH THE CITY OF VLL INVERTS PRIOR TO CONSTRUCTION.</li> <li>XIMATE ONLY. FINAL DESIGN OF NATURAL GAS SERVICE TO BE COMPLETED RATE DRIVE MAY NEED TO BE COMPLETED IN CONJUNCTION WITH FUTURE DRATE DRIVE. COORDINATE WITH CITY OF PORTSMOUTH AND UNITIL.</li> <li>VIS APPROXIMATE ONLY. FINAL DESIGN OF ELECTRIC SERVICE AND VIRE TO BE COMPLETED BY EVERSOURCE. WORK IN CORPORATE DRIVE MAY CONJUNCTION WITH FUTURE RECONSTRUCTION OF CORPORATE DRIVE MAY CONJUNCTION WITH FUTURE RECONSTRUCTION OF CORPORATE DRIVE.</li> <li>PORTSMOUTH AND EVERSOURCE.</li> <li>VER METER AND VALVES SHALL BE COORDINATED WITH THE CITY OF</li> <li>CONSTRUCTION.</li> <li>DRANTS, FIRE DEPARTMENT CONNECTIONS AND DRY STAND PIPES WILL BE ILDING DRAWINGS AND APPROVED BY THE PORTSMOUTH FIRE DEPARTMENT</li> </ul>	Proposed Jadustrial DevelopmentLonza BiologicsPortsmouth, New Hampshire
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		PLANT SCHEDULE		
CODE	BOTANICAL NAME	COMMON NAME	SIZE	REMARKS
TREES		·		
UA	ULMUS AMERICANA 'PRINCETON'	PRINCETON AMERICAN ELM	$2\frac{1}{2}$ - 3" CALIPER	B & B
QP	QUERCUS PULUSTRIS	PIN OAK	$2\frac{1}{2}$ - 3" CALIPER	B & B
GT	GLEIDITSIA TRIACANTHOS `SKYLINE'	SKYLINE HONEYLOCUST	$2\frac{1}{2}$ - 3" CALIPER	B & B
AR	ACER RUBRUM 'REDPOINTE'	REDPOINTE RED MAPLE	$2\frac{1}{2}$ - 3" CALIPER	B & B
AC	AESCULUS CARNEA ' FORT MCNAIR'	FORT MCNAIR HORSECHESTNUT	$2\frac{1}{2}$ - 3" CALIPER	B & B
PC	PYRUS CHANTICLEER	CHANTICLEER PEAR	2 - $2\frac{1}{2}$ " CALIPER	B & B
AG	AMELANCHIER GRANDIFLORA 'AUTUMN BRILLIANCE'	AUTUMN BRILLIANCE SERVICEBERRY	2 - $2\frac{1}{2}$ " CALIPER	B & B (SINGLE STEM)
BN	BETULA NIGRA `HERITAGE'	HERITAGE RIVER BIRCH	12 - 14' HT.	B & B (MULTISTEM)
PG	PICEA GLAUCA	WHITE SPRUCE	8 - 10' HT.	B & B
PP	PICEA PUNGENS	COLORADO SPRUCE	8 - 10' HT.	B & B
PA	PICEA ABIES	NORWAY SPRUCE	8 - 10' HT.	B & B
SHRUBS	5	•	•	•
VC	VIBURNUM CASSINOIDES	WITHEROD VIBURNUM	2 <u>1</u> - 3' HT.	B & B
RE	RHODODENDRON 'ENGLISH ROSEUM'	ENGLISH ROSEUM RHODODENDRON	2 <u>1</u> - 3' HT.	B & B
CA	CLETHERA ALNIFOLIA	SUMMERSWEET CLETHERA	7 GALLON	CONTAINER
HQ	HYDRANGEA QUERCIFOLIA 'SNOW QUEEN'	SNOW QUEEN OAKLEAF HYDRANGEA	2 <u>1</u> - 3' HT.	B & B
GROUNI	DCOVERS & PERENNIALS	•		•
DL	HEMEROCALLIS 'STELLA DORO'	STELLA DORO DAYLILY	2 GALLON	CONTAINER
HR	HOSTA 'ROYAL STANDARD'	ROYAL STANDARD HOSTA	2 GALLON	CONTAINER
AS	ASTILBE 'VISIONS IN PINK'	VISIONS IN PINK ASTILBE	2 GALLON	CONTAINER
CAL	CALAMAGROSTIS 'KARL FOERSTER'	KARL FOERSTER FEATHER REED GRASS	3 GALLON	CONTAINER



May 17, 2024 3:51 PM By May 17, 2024 Plotted By:

1. SEED MIX "A" SHALL CONTAIN THE FOLLOWING SEED REQUIREMENTS AND BE APPLIED AT A RATE OF 40LB/AC % BY WEIGHT

	70 DI WLIGIII
EL II" TALL FESCUE	70%
MER" PERENNIAL RYEGRASS	20%
ON" KENTUCKEY BLUEGRASS	10%

CONSERVATION/WILDLIFE MIX OR APPROVED EQUAL

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9	<b>SCHEDU</b>	LE	



C-174



: Save Date: May 17, 2024 3:51 PM By: NAHANSEN Date: Friday, May 17, 2024 Plotted By: Neil A. Hansen

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GENERAL PROJECT INFORMATION         PROJECT LESSOR:       PEASE DEVELOPMENT AUTHORITY         FE INTERNATIONAL DRIVE	<ol> <li>ALL AREAS SHALL BE STABILIZED WITHIN 45 DA</li> <li>WHEN CONSTRUCTION ACTIVITY PERMANENTLY</li> </ol>
PROJECT OWNER/ APPLICANT: LONZA BIOLOGICS 101 INTERNATIONAL DRIVE	WITHIN SEVEN (7) DAYS OR PRIOR TO A RAIN E CEASES PERMANENTLY IN AN THESE AREAS, SIL BARRIERS AND ANY EARTH/DIKES SHALL BE REI
PORTSMOUTH, NH 03801 PROJECT ADDRESS: 70 & 80 CORPORATE DRIVE	<ul> <li>6. DURING CONSTRUCTION, RUNOFF WILL BE DIVE</li> <li>DIKES PIPING OR STABILIZED CHANNELS WHEE</li> </ul>
PROJECT LATITUDE:43°-04'-59.0"NPROJECT LONGITUDE:71°-48'-09.7"W	WILL BE FILTERED THROUGH SILT FENCES, MUL SOCKS. ALL STORM DRAIN BASIN INLETS SHALL
<b>PROJECT DESCRIPTION</b> THE PROJECT CONSISTS OF THE EXPANSION OF LONZA BIOLOGICS, WHICH INCLUDES THE CONSTRUCTION OF 4 PROPOSED BUILDINGS, 1 PARKING GARAGE, AND ASSOCIATED SITE IMPROVEMENTS.	AND TRASH RACKS. THE SITE SHALL BE STABIL <b>DUST CONTROL:</b> 1. THE CONTRACTOR SHALL BE RESPONSIBLE TO ( CONSTRUCTION PERIOD.
DISTURBED AREA THE TOTAL AREA TO BE DISTURBED IS APPROXIMATELY 21.3 ACRES.	<ol> <li>DUST CONTROL METHODS SHALL INCLUDE, BUT EXPOSED AREAS, COVERING LOADED DUMP TRU MULCHING.</li> <li>DUST CONTROL MEASURES SHALL BE UTILIZED.</li> </ol>
SOIL CHARACTERISTICS BASED ON THE HIGH INTENSITY SOIL SURVEY PREPARED BY GOVE ENVIRONMENTAL SERVICES, INC. IN DECEMBER 2015, THE SITE SOILS VARY FROM WELL DRAINED TO VERY POORLY DRAINED	S. DOST CONTROL MEASURES SHALL BE UTILIZED DUST FROM THE SITE TO ABUTTING AREAS.
AND PRIMARILY CONSIST OF SOMEWHAT POORLY DRAINED SOILS.	<ol> <li>LOCATE STOCKPILES A MINIMUM OF 50 FEET AW CULVERTS.</li> <li>ALL STOCKPILES SHOULD BE SURROUNDED WIT</li> </ol>
CONSTRUCTION SEQUENCE OF MAJOR ACTIVITIES:	<ol> <li>MEASURES PRIOR TO THE ONSET OF PRECIPITA</li> <li>PERIMETER BARRIERS SHOULD BE MAINTAINED TO ACCOMMODATE THE DELIVERY AND REMOVA</li> </ol>
<ul> <li>CUT AND CLEAR TREES.</li> <li>CONSTRUCT TEMPORARY AND PERMANENT SEDIMENT, EROSION AND DETENTION CONTROL FACILITIES. EROSION, SEDIMENT AND DETENTION MEASURES SHALL BE INSTALLED PRIOR TO ANY EARTH MOVING OPERATIONS THAT WILL INFLUENCE STORMWATER RUNOFF SUCH AS:</li> </ul>	<ul> <li>4. PROTECT ALL STOCKPILES FROM STORMWATER</li> <li>CONTROL MEASURES SUCH AS BERMS, SILT SOU</li> <li>PREVENT MIGRATION OF MATERIAL BEYOND THE</li> </ul>
<ul> <li>NEW CONSTRUCTION</li> <li>CONTROL OF DUST</li> <li>NEARNESS OF CONSTRUCTION SITE TO RECEIVING WATERS</li> <li>CONSTRUCTION DURING LATE WINTER AND EARLY SPRING</li> </ul>	OFF SITE VEHICLE TRACKING: 1. THE CONTRACTOR SHALL CONSTRUCT STABILIZ ANY EXCAVATION ACTIVITIES.
<ol> <li>ALL PERMANENT DITCHES, SWALES, DETENTION, RETENTION AND SEDIMENTATION BASINS TO BE STABILIZED USING THE VEGETATIVE AND NON-STRUCTURAL BMPS PRIOR TO DIRECTING RUNOFF TO THEM.</li> <li>CLEAR AND DISPOSE OF DEBRIS</li> </ol>	VEGETATION: 1. TEMPORARY GRASS COVER: A. SEEDBED PREPARATION: ADDIX FERTILIZED AT THE PATE OF 600 PC
<ul> <li>CONSTRUCT TEMPORARY CULVERTS AND DIVERSION CHANNELS AS REQUIRED.</li> <li>GRADE AND GRAVEL ROADWAYS AND PARKING AREAS - ALL ROADS AND PARKING AREA SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.</li> </ul>	LIMESTONE (EQUIVALENT TO 50 PERCENT RATE OF THREE (3) TONS PER ACRE; B. SEEDING:
<ol> <li>BEGIN PERMANENT AND TEMPORARY SEEDING AND MULCHING. ALL CUT AND FILL SLOPES SHALL BE SEEDED AND MULCHED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.</li> <li>DAILY, OR AS REQUIRED, CONSTRUCT TEMPORARY BERMS, DRAINS, DITCHES, PERIMETER EROSION CONTROL MEASURES, SEDIMENT TRAPS, ETC., MULCH AND SEED AS REQUIRED.</li> <li>SEDIMENT TRAPS AND/OR BASINS SHALL BE USED AS NECESSARY TO CONTAIN RUNOFF UNTIL SOILS ARE STABILIZED.</li> </ol>	<ul> <li>a. UTILIZE ANNUAL RYE GRASS AT A RATE OF</li> <li>b. WHERE THE SOIL HAS BEEN COMPACTED E</li> <li>SOIL TO A DEPTH OF TWO (2) INCHES BEF</li> <li>c. APPLY SEED UNIFORMLY BY HAND, CYCLOF</li> <li>INCLUDING SEED AND FERTILIZER). HYDR</li> <li>BE LEFT ON SOIL SURFACE, SEEDING BATE</li> </ul>
<ol> <li>FINISH PAVING ALL ROADWAYS AND PARKING LOTS.</li> <li>INSPECT AND MAINTAIN ALL EROSION AND SEDIMENT CONTROL MEASURES.</li> <li>COMPLETE PERMANENT SEEDING AND LANDSCAPING.</li> <li>REMOVE TRAPPED SEDIMENTS FROM COLLECTOR DEVICES AS APPROPRIATE AND THEN DEMOVE TEMPODARY EROSION CONTROL MEASURES.</li> </ol>	HYDROSEEDING; C. MAINTENANCE: a. TEMPORARY SEEDING SHALL BE PERIODIC THE SOIL SURFACE SHOULD BE COVERED
<b>SPECIAL CONSTRUCTION NOTES:</b> 1. THE CONSTRUCTION SEQUENCE MUST LIMIT THE DURATION AND AREA OF DISTURBANCE. 2. THE PROJECT IS TO BE MANAGED IN A MANNER THAT MEETS THE REQUIREMENTS AND	TEMPORARY MEASURES USED IN THE INTE DAMS, ETC.). 2. VEGETATIVE PRACTICE:
INTENT OF RSA 430:53 AND CHAPTER AGR 3800 RELATIVE TO INVASIVE SPECIES.	<ul> <li>a. LIMESTONE SHALL BE THOROUGHLY INCOM</li> <li>OF THREE (3) TONS PER ACRE IN ORDER T</li> <li>b. FERTILIZER SHALL BE SPREAD ON THE TOP</li> </ul>
<ol> <li>ALL EROSION CONTROL MEASURES AND PRACTICES SHALL CONFORM TO THE "NEW HAMPSHIRE STORMWATER MANUAL VOLUME 3: EROSION AND SEDIMENT CONTROLS DURING CONSTRUCTION" PREPARED BY THE NHDES.</li> <li>PRIOR TO ANY WORK OR SOIL DISTURBANCE, CONTRACTOR SHALL SUBMIT SHOP</li> </ol>	SURFACE. FERTILIZER APPLICATION RATE 10-20-20 FERTILIZER; c. SOIL CONDITIONERS AND FERTILIZER SHA RATES AND SHALL BE THOROUGHLY WORK
DRAWINGS FOR EROSION CONTROL MEASURES AS REQUIRED IN THE PROJECT MANUAL. 3. CONTRACTOR SHALL INSTALL TEMPORARY EROSION CONTROL BARRIERS, INCLUDING HAY BALES, SILT FENCES, MULCH BERMS, SILT SACKS AND SILT SOCKS AS SHOWN IN THESE DRAWINGS AS THE FIRST ORDER OF WORK.	UNTIL THE SURFACE IS FINELY PULVERIZE COMPACTED TO AN EVEN SURFACE CONFO GRADES WITH APPROVED ROLLERS WEIGH POUNDS PER INCH OF WIDTH:
<ul> <li>SILT SACK INLET PROTECTION SHALL BE INSTALLED IN ALL EXISTING AND PROPOSED CATCH BASIN INLETS WITHIN THE WORK LIMITS AND BE MAINTAINED FOR THE DURATION OF THE PROJECT.</li> <li>PERIMETER CONTROLS INCLUDING SULT FENCES, MULCH BERM, SULT SOCK, AND/OR HAY</li> </ul>	d. SEED SHALL BE SOWN AT THE RATE SHOW CALM, DRY DAY, PREFERABLY BY MACHINI WORKMEN. IMMEDIATELY BEFORE SEEDIN
BALE BARRIERS SHALL BE MAINTAINED FOR THE DURATION OF THE PROJECT UNTIL NON-PAVED AREAS HAVE BEEN STABILIZED. 5. THE CONTRACTOR SHALL REMOVE AND PROPERLY DISPOSE OF ALL TEMPORARY EROSION	ANGLES TO THE ORIGINAL DIRECTION. IT A DEPTH NOT OVER 1/4 INCH AND ROLLEE OVER 100 POUNDS PER LINEAR FOOT OF V
CONTROL DEVICES UPON COMPLETION OF CONSTRUCTION. ALL DISTURBED AREAS NOT OTHERWISE BEING TREATED SHALL RECEIVE 6" LOAM, SEED AND FERTILIZER. INSPECT ALL INLET PROTECTION AND PERIMETER CONTROLS WEEKLY AND AFTER FACH RAIN	<ul> <li>e. HAY MULCH SHALL BE APPLIED IMMEDIATE</li> <li>f. THE SURFACE SHALL BE WATERED AND KE</li> <li>WITHOUT WASHING AWAY THE SOIL, UNT</li> </ul>
STORM OF 0.25 INCH OR GREATER. REPAIR/MODIFY PROTECTION AS NECESSARY TO MAXIMIZE EFFICIENCY OF FILTER. REPLACE ALL FILTERS WHEN SEDIMENT IS 1/3 THE FILTER HEIGHT.	AREAS WHICH ARE NOT SATISFACTORILY AND ALL NOXIOUS WEEDS REMOVED; g. THE CONTRACTOR SHALL PROTECT AND M ACCEPTED;
AN AREA SHALL BE CONSIDERED STABLE WHEN ONE OF THE FOLLOWING HAS OCCUPPED.	h. A GRASS SEED MIXTURE CONTAINING THE BE APPLIED AT A RATE OF 40 LB/AC OR AP SEED MIX A
<ul> <li>A. BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED;</li> <li>B. A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED;</li> <li>C. A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH AS STONE OR RIPRAP HAS BEEN INSTALLED:</li> </ul>	REDEL II TALL FESCUE "PALMER" PERENNIAL RYEGRASS "BARON" KENTUCKEY BLUEGRASS IN NO CASE SHALL THE WEED CONTENT E
<ul> <li>D. EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.;</li> <li>E. IN AREAS TO BE PAVED, "STABLE" MEANS THAT BASE COURSE GRAVELS MEETING THE REQUIREMENTS OF NHDOT STANDARD FOR ROAD AND BRIDGE CONSTRUCTION, 2016, ITEM 204 2 HAVE BEEN INSTALLED.</li> </ul>	SEED SHALL COMPLY WITH STATE AND FEI NO LATER THAN SEPTEMBER 15. IN NO CA 3. DORMANT SEEDING (SEPTEMBER 15 TO FIRST S A. FOLLOW PERMANENT MEASURES SLOPE, LIME
<ol> <li>WINTER STABILIZATION PRACTICES:</li> <li>A. ALL PROPOSED VEGETATED AREAS THAT DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15,</li> </ol>	REQUIREMENTS. APPLY SEED MIXTURE AT TW INDICATED FOR PERMANENT MEASURES. CONCRETE WASHOUT AREA:
SHALL BE STABILIZED BY SEEDING AND INSTALLING EROSION CONTROL BLANKETS ON SLOPES GREATER THAN 3:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER	<ol> <li>THE CONCRETE DELIVERY TRUCKS SHALL, WHEN AT THEIR OWN PLANT OR DISPATCH FACILITY;</li> <li>IF IT IS NECESSARY, SITE CONTRACTOR SHALL DESIGN FACILITIES TO HANDLE ANTICIDATED WAY</li> </ol>
<ul> <li>ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT EVENTS;</li> <li>B. ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15.</li> </ul>	<ol> <li>CONTRACTOR SHALL LOCATE WASHOUT AREAS DRAINS, SWALES AND SURFACE WATERS OR DE</li> <li>INSPECT WASHOUT FACILITIES DAILY TO DETEC MATERIALS NEED TO BE REMOVED</li> </ol>
<ul> <li>SHALL BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS;</li> <li>C. AFTER NOVEMBER 15, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3</li> </ul>	ALLOWABLE NON-STORMWATER DISCHARGES:         1.       THE FOLLOWING ARE THE ONLY NON-STORMWATER DISCHARGES ARE PROHIBIT
INCHES OF CRUSHED GRAVEL PER NHDOT ITEM 304.3, OR IF CONSTRUCTION IS TO CONTINUE THROUGH THE WINTER SEASON BE CLEARED OF ANY ACCUMULATED SNOW AFTER EACH STORM EVENT; STABILIZATION SHALL BE INITIATED ON ALL LOAM STOCKED AS AND DISTURBED ABOAC	<ul> <li>A. FIRE-FIGHTING ACTIVITIES;</li> <li>B. FIRE HYDRANT FLUSHING;</li> <li>C. WATERS USED TO WASH VEHICLES WHERE D</li> </ul>
WHERE CONSTRUCTION ACTIVITY SHALL NOT OCCUR FOR MORE THAN TWENTY-ONE (21) CALENDAR DAYS BY THE FOURTEENTH (14TH) DAY AFTER CONSTRUCTION ACTIVITY HAS PERMANENTLY OR TEMPORARILY CEASED IN THAT AREA STABILIZATION MEASURES TO BE	<ul> <li>D. WATER USED TO CONTROL DUST;</li> <li>E. POTABLE WATER INCLUDING UNCONTAMINAT</li> <li>F. ROUTINE EXTERNAL BUILDING WASH DOWN</li> </ul>
. LIN WITCH FOR TELL OF WITCH GENOLD IN THAT AREA DIADILIZATION PLADURED TO DE	G. PAVEMENT WASH WATERS WHERE DETERGEN

5 DAYS OF INITIAL DISTURBANCE. ITLY OR TEMPORARILY CEASES WITHIN 100 FEET ED WETLANDS, THE AREA SHALL BE STABILIZED IN EVENT. ONCE CONSTRUCTION ACTIVITY SILT FENCES, MULCH BERMS, HAY BALE REMOVED ONCE PERMANENT MEASURES ARE

DIVERTED AROUND THE SITE WITH EARTH HERE POSSIBLE. SHEET RUNOFF FROM THE SITE MULCH BERMS, HAY BALE BARRIERS, OR SILT HALL BE PROVIDED WITH FLARED END SECTIONS BILIZED FOR THE WINTER BY NOVEMBER 15.

TO CONTROL DUST THROUGHOUT THE

BUT BE NOT LIMITED TO SPRINKLING WATER ON TRUCKS LEAVING THE SITE, AND TEMPORARY

ZED SO AS TO PREVENT THE MIGRATION OF

FAWAY FROM CATCH BASINS, SWALES, AND

WITH TEMPORARY EROSION CONTROL

PITATION. NED AT ALL TIMES, AND ADJUSTED AS NEEDED IOVAL OF MATERIALS FROM THE STOCKPILE. THE SPECTED AT THE END OF EACH WORKING DAY. FER RUN-OFF USING TEMPORARY EROSION SOCK, OR OTHER APPROVED PRACTICE TO THE IMMEDIATE CONFINES OF THE STOCKPILES.

BILIZED CONSTRUCTION ENTRANCE(S) PRIOR TO

0 POUNDS PER ACRE OF 10-10-10. APPLY ENT CALCIUM PLUS MAGNESIUM OXIDE) AT A

E OF 40 LBS/ACRE; ED BY CONSTRUCTION OPERATIONS, LOOSEN BEFORE APPLYING FERTILIZER, LIME AND SEED; CLONE SEEDER, OR HYDROSEEDER (SLURRY YDROSEEDINGS, WHICH INCLUDE MULCH, MAY RATES MUST BE INCREASED 10% WHEN

DDICALLY INSPECTED. AT A MINIMUM, 95% OF RED BY VEGETATION. IF ANY EVIDENCE OF ARENT, REPAIRS SHALL BE MADE AND OTHER INTERIM (MULCH, FILTER BARRIERS, CHECK

NGS:

NCORPORATED INTO THE LOAM LAYER AT A RATE ER TO PROVIDE A PH VALUE OF 5.5 TO 6.5; TOP LAYER OF LOAM AND WORKED INTO THE ATE SHALL BE 800 POUNDS PER ACRE OF

SHALL BE APPLIED AT THE RECOMMENDED ORKED INTO THE LOAM. LOAM SHALL BE RAKED RIZED, SMOOTH AND EVEN, AND THEN NFORMING TO THE REQUIRED LINES AND EIGHING BETWEEN 4-1/2 POUNDS AND 5-1/2

HOWN BELOW. SOWING SHALL BE DONE ON A HINE, BUT IF BY HAND, ONLY BY EXPERIENCED EDING, THE SOIL SHALL BE LIGHTLY RAKED. ONE NE DIRECTION AND THE OTHER HALF AT RIGHT I. IT SHALL BE LIGHTLY RAKED INTO THE SOIL TO LLED WITH A HAND ROLLER WEIGHING NOT OF WIDTH;

IATELY AFTER SEEDING AS INDICATED ABOVE; ID KEPT MOIST WITH A FINE SPRAY AS REQUIRED, UNTIL THE GRASS IS WELL ESTABLISHED. ANY RILY COVERED WITH GRASS SHALL BE RESEEDED,

ND MAINTAIN THE SEEDED AREAS UNTIL

THE FOLLOWING SEED REQUIREMENTS SHALL R APPROVED EUQAL:

- APPLICATION RATE
- 70% 20%
- 10%

IT EXCEED ONE (1) PERCENT BY WEIGHT. ALL FEDERAL SEED LAWS. SEEDING SHALL BE DONE CASE SHALL SEEDING TAKE PLACE OVER SNOW. ST SNOWFALL):

LIME, FERTILIZER AND GRADING TWICE THE INDICATED RATE. APPLY MULCH AS

HENEVER POSSIBLE, USE WASHOUT FACILITIES

ALL DESIGNATE SPECIFIC WASHOUT AREAS AND ED WASHOUT WATER; EAS AT LEAST 150 FEET AWAY FROM STORM

R DELINEATED WETLANDS; TECT LEAKS OR TEARS AND TO IDENTIFY WHEN

1WATER DISCHARGES ALLOWED. ALL OTHER IBITED ON SITE:

RE DETERGENTS ARE NOT USED;

- INATED WATER LINE FLUSHING;
- WN WHERE DETERGENTS ARE NOT USED;
- GENTS ARE NOT USED;
- COMPRESSOR CONDENSATION; PRING WATER;
- CH ARE UNCONTAMINATED;

#### WASTE DISPOSAL: WASTE MATERIAL

- A. ALL WASTE MATERIALS SHALL BE COLLECTED AND STORED IN SECURELY LIDDED RECEPTACLES. ALL TRASH AND CONSTRUCTION DEBRIS FROM THE SITE SHALL BE DEPOSITED IN A DUMPSTER;
- B. NO CONSTRUCTION WASTE MATERIALS SHALL BE BURIED ON SITE;
- C. ALL PERSONNEL SHALL BE INSTRUCTED REGARDING THE CORRECT PROCEDURE FOR WASTE DISPOSAL BY THE SUPERINTENDENT. HAZARDOUS WASTE:
- A. ALL HAZARDOUS WASTE MATERIALS SHALL BE DISPOSED OF IN THE MANNER SPECIFIED BY LOCAL OR STATE REGULATION OR BY THE MANUFACTURER; B. SITE PERSONNEL SHALL BE INSTRUCTED IN THESE PRACTICES BY THE SUPERINTENDENT
- 3. SANITARY WASTE: A. ALL SANITARY WASTE SHALL BE COLLECTED FROM THE PORTABLE UNITS A MINIMUM OF ONCE PER WEEK BY A LICENSED SANITARY WASTE MANAGEMENT CONTRACTOR.

#### SPILL PREVENTION

- CONTRACTOR SHALL BE FAMILIAR WITH SPILL PREVENTION MEASURES REQUIRED BY LOCAL, STATE AND FEDERAL AGENCIES. AT A MINIMUM, CONTRACTOR SHALL FOLLOW THE BEST MANAGEMENT SPILL PREVENTION PRACTICES OUTLINED BELOW.
- 2. THE FOLLOWING ARE THE MATERIAL MANAGEMENT PRACTICES THAT SHALL BE USED TO REDUCE THE RISK OF SPILLS OR OTHER ACCIDENTAL EXPOSURE OF MATERIALS AND SUBSTANCES DURING CONSTRUCTION TO STORMWATER RUNOFF:
- A. GOOD HOUSEKEEPING THE FOLLOWING GOOD HOUSEKEEPING PRACTICE SHALL BE FOLLOWED ON SITE DURING CONSTRUCTION: a. ONLY SUFFICIENT AMOUNTS OF PRODUCTS TO DO THE JOB SHALL BE STORED ON
- SITE b. ALL MATERIALS STORED ON SITE SHALL BE STORED IN A NEAT, ORDERLY MANNER IN
- THEIR PROPER (ORIGINAL IF POSSIBLE) CONTAINERS AND, IF POSSIBLE, UNDER A ROOF OR OTHER ENCLOSURE; c. MANUFACTURER'S RECOMMENDATIONS FOR PROPER USE AND DISPOSAL SHALL BE
- FOLLOWED; d. THE SITE SUPERINTENDENT SHALL INSPECT DAILY TO ENSURE PROPER USE AND
- DISPOSAL OF MATERIALS; e. SUBSTANCES SHALL NOT BE MIXED WITH ONE ANOTHER UNLESS RECOMMENDED BY
- THE MANUFACTURER; f. WHENEVER POSSIBLE ALL OF A PRODUCT SHALL BE USED UP BEFORE DISPOSING OF THE CONTAINER.
- HAZARDOUS PRODUCTS THE FOLLOWING PRACTICES SHALL BE USED TO REDUCE THE RISKS ASSOCIATED WITH HAZARDOUS MATERIALS: g. PRODUCTS SHALL BE KEPT IN THEIR ORIGINAL CONTAINERS UNLESS THEY ARE NOT
- RESEALABLE; h. ORIGINAL LABELS AND MATERIAL SAFETY DATA SHALL BE RETAINED FOR IMPORTANT
- PRODUCT INFORMATION; i. SURPLUS PRODUCT THAT MUST BE DISPOSED OF SHALL BE DISCARDED ACCORDING
- TO THE MANUFACTURER'S RECOMMENDED METHODS OF DISPOSAL C. PRODUCT SPECIFIC PRACTICES - THE FOLLOWING PRODUCT SPECIFIC PRACTICES SHALL BE FOLLOWED ON SITE:
- a. PETROLEUM PRODUCTS:
- ALL ON SITE VEHICLES SHALL BE MONITORED FOR LEAKS AND RECEIVE REGULAR PREVENTIVE MAINTENANCE TO REDUCE LEAKAGE;
- PETROLEUM PRODUCTS SHALL BE STORED IN TIGHTLY SEALED CONTAINERS WHICH ARE CLEARLY LABELED. ANY ASPHALT BASED SUBSTANCES USED ON SITE SHALL BE APPLIED ACCORDING TO THE MANUFACTURER'S RECOMMENDATIONS. b. FERTILIZERS:
- FERTILIZERS USED SHALL BE APPLIED ONLY IN THE MINIMUM AMOUNTS DIRECTED BY THE SPECIFICATIONS;
- ONCE APPLIED FERTILIZER SHALL BE WORKED INTO THE SOIL TO LIMIT EXPOSURE TO STORMWATER; • STORAGE SHALL BE IN A COVERED SHED OR ENCLOSED TRAILERS. THE CONTENTS
- OF ANY PARTIALLY USED BAGS OF FERTILIZER SHALL BE TRANSFERRED TO A SEALABLE PLASTIC BIN TO AVOID SPILLS. c. PAINTS:
- ALL CONTAINERS SHALL BE TIGHTLY SEALED AND STORED WHEN NOT REQUIRED
- FOR USE; EXCESS PAINT SHALL NOT BE DISCHARGED TO THE STORM SEWER SYSTEM;
- EXCESS PAINT SHALL BE DISPOSED OF PROPERLY ACCORDING TO MANUFACTURER'S INSTRUCTIONS OR STATE AND LOCAL REGULATIONS.
- D. SPILL CONTROL PRACTICES IN ADDITION TO GOOD HOUSEKEEPING AND MATERIAL MANAGEMENT PRACTICES DISCUSSED IN THE PREVIOUS SECTION, THE FOLLOWING PRACTICES SHALL BE FOLLOWED FOR SPILL PREVENTION AND CLEANUP:
- a. MANUFACTURER'S RECOMMENDED METHODS FOR SPILL CLEANUP SHALL BE CLEARLY POSTED AND SITE PERSONNEL SHALL BE MADE AWARE OF THE PROCEDURES AND THE LOCATION OF THE INFORMATION AND CLEANUP SUPPLIES;
- b. MATERIALS AND EQUIPMENT NECESSARY FOR SPILL CLEANUP SHALL BE KEPT IN THE MATERIAL STORAGE AREA ON SITE. EQUIPMENT AND MATERIALS SHALL INCLUDE BUT NOT BE LIMITED TO BROOMS, DUSTPANS, MOPS, RAGS, GLOVES, GOGGLES, KITTY LITTER, SAND, SAWDUST AND PLASTIC OR METAL TRASH CONTAINERS SPECIFICALLY FOR THIS PURPOSE;
- c. ALL SPILLS SHALL BE CLEANED UP IMMEDIATELY AFTER DISCOVERY; d. THE SPILL AREA SHALL BE KEPT WELL VENTILATED AND PERSONNEL SHALL WEAR
- APPROPRIATE PROTECTIVE CLOTHING TO PREVENT INJURY FROM CONTACT WITH A HAZARDOUS SUBSTANCE;
- e. SPILLS OF TOXIC OR HAZARDOUS MATERIAL SHALL BE REPORTED TO THE APPROPRIATE LOCAL, STATE OR FEDERAL AGENCIES AS REQUIRED;
- f. THE SITE SUPERINTENDENT RESPONSIBLE FOR DAY-TO-DAY SITE OPERATIONS SHALL BE THE SPILL PREVENTION AND CLEANUP COORDINATOR.
- E. VEHICLE FUELING AND MAINTENANCE PRACTICE: a. CONTRACTOR SHALL MAKE AN EFFORT TO PERFORM EQUIPTMENT/VEHICAL FUELING
- AND MAINTENANCE AT AN OFF-SITE FACILITY; b. CONTRACTOR SHALL PROVIDE AN ON-SITE FUELING AND MAINTENANCE AREA THAT IS CLEAN AND DRY;
- c. IF POSSIBLE THE CONTRACTOR SHALL KEEP AREA COVERED;
- d. CONTRACTOR SHALL KEEP A SPILL KIT AT THE FUELING AND MAINTENANCE AREA;
- e. CONTRACTOR SHALL REGULARLY INSPECT VEHICLES FOR LEAKS AND DAMAGE; f. CONTRACTOR SHALL USE DRIP PANS, DRIP CLOTHS, OR ABSORBENT PADS WHEN
- REPLACING SPENT FLUID.

#### **EROSION CONTROL OBSERVATIONS AND MAINTENANCE PRACTICES**

THIS PROJECT EXCEEDS ONE (1) ACRE OF DISTURBANCE AND THUS REQUIRES A SWPPP. THE SWPPP SHALL BE PREPARED BY THE CONTRACTOR. THE CONTRACTOR SHALL BE FAMILIAR WITH THE SWPPP AND KEEP AN UPDATED COPY OF THE SWPPP ONSITE AT ALL TIMES.

- THE FOLLOWING REPRESENTS THE GENERAL OBSERVATION AND REPORTING PRACTICES THAT SHALL BE FOLLOWED AS PART OF THIS PROJECT: OBSERVATIONS OF THE PROJECT FOR COMPLIANCE WITH THE SWPPP SHALL BE MADE BY
- THE CONTRACTOR AT LEAST ONCE A WEEK OR WITHIN 24 HOURS OF A STORM 0.25 INCHES OR GREATER;
- 2. AN OBSERVATION REPORT SHALL BE MADE AFTER EACH OBSERVATION AND DISTRIBUTED TO THE ENGINEER, THE OWNER, AND THE CONTRACTOR;
- 3. A REPRESENTATIVE OF THE SITE CONTRACTOR, SHALL BE RESPONSIBLE FOR MAINTENANCE AND REPAIR ACTIVITIES;
- 4. IF A REPAIR IS NECESSARY, IT SHALL BE INITIATED WITHIN 24 HOURS OF REPORT.

FLOW -----

ACRE OF DRAINAGE AREA.

-	 	 	 	-

NOTES:

SILT SOCK
(12" TYPICAL)
WORK AREA

<u>NO</u> 1. 2.	<u>TES:</u> SILT SOCK SHA INSTALL SILT S

	K MA
V	<i>e</i> 1
	$\overline{\mathcal{D}}$

CATCH BASIN GRATE-(DIMENSIONS VARY)

![](_page_335_Figure_101.jpeg)

![](_page_336_Figure_0.jpeg)

![](_page_337_Figure_0.jpeg)

![](_page_337_Figure_3.jpeg)

#### **Drainage Memorandum**

To:Pease Development Authority (PDA)FROM:Neil A. Hansen, PE<br/>Patrick M. Crimmins, PECOPY:Lonza BiologicsDATE:May 20, 2024

## **1.0 Project Description**

The proposed work includes the addition of Solar Canopies over the previously approved 150space surface parking lot associated with Phase 2 of the Iron Parcel Development project. These Solar Canopies are planned to be removed along with the 150-space parking lot before the execution of the Master Plan, therefore there will be no changes to the Master Plan Drainage Design.

The Phase 2 drainage analysis has been updated and revised to include the 4'x4' concrete footings and 8'x22' concrete equipment pad. The proposed change includes the addition of approximately 672 SF of impervious surfaces. Although the addition of this area is very minimal in perspective to the whole watershed area (1,376,888 SF), we have prepared this technical memo to confirm that the previously approved Phase 2 drainage design and gravel wetlands are sized appropriately to accommodate this slight increase in impervious area.

## 2.0 Drainage Analysis

The previously approved Phase 2 Drainage Calculation has been updated to analyze the slight increase in impervious area and can be found in Attachment A. Subcatchment 1.0 has been updated to convert 304 SF of the previously grass surface to impervious surface. This additional 304 SF is approximately 0.09% of the total impervious area (314,795 SF) for this watershed.

Subcatchment 1.1 has been updated to convert 368 SF of the previously grass surface to impervious surface. This addition of 368 SF is approximately 0.7% of the total impervious area (48,674 SF) for this watershed.

![](_page_338_Picture_10.jpeg)

![](_page_338_Picture_11.jpeg)

#### 2.1 Peak Rate Comparisons

The following table summarizes and compares the Phase-2 2023 Approved, proposed Phase-2 2024 Amendment, and Master Plan pre- and post-development peak runoff rates for the 2-year, 10-year, 25-year and 50-year storm events at each point of analysis. These points of analysis remain unchanged from the previously prepared and approved drainage analysis.

Table 2.1 – Peak Flow Rate Comparison							
Point of Analysis	Phase	Pre 1-Year Storm (cfs)	Pre/ <b>Post</b> 2-Year Storm (cfs)	Pre/ <b>Post</b> 10-Year Storm (cfs)	Pre/ <b>Post</b> 25-Year Storm (cfs)	Pre/ <b>Post</b> 50-Year Storm (cfs)	
	Phase 2 (2023 Approval)	16.58	24.86/ <b>9.25</b>	52.70/ <b>31.22</b>	76.06/ <b>56.26</b>	98.56/ <b>74.09</b>	
PA1	Phase 2 (2024 Amendment)	16.58	24.86/ <b>9.25</b>	52.70/ <b>31.22</b>	76.06/ <b>56.26</b>	98.56/ <b>74.09</b>	
	Master	16.58	24.86/ <b>9.41</b>	52.70/ <b>39.92</b>	76.06/ <b>66.14</b>	98.56/ <b>83.35</b>	
	Phase 2 (2023 Approval)	3.38	4.41/ <b>3.10</b>	7.49/ <b>5.36</b>	9.90/ <b>7.12</b>	12.13/ <b>8.76</b>	
PA2	Phase 2 (2024 Amendment)	3.38	4.41/ <b>3.10</b>	7.49/ <b>5.36</b>	9.90/ <b>7.12</b>	12.13/ <b>8.76</b>	
	Master	3.38	4.41/3.72	7.49/ <b>5.94</b>	9.90/ <b>7.66</b>	12.13/9.25	

#### 2.2 Stormwater Treatment

Runoff from the newly created impervious surfaces will be directed to either of the previously approved Gravel Wetland 1 (POND 1.0) or Gravel Wetland 2 (POND 1.1). The following sections outline the treatment capacities of both gravel wetlands.

#### Gravel Wetland 1

Gravel Wetland 1 has a design capacity to treat 333,950 SF of impervious area for its 462,599 SF watershed area. The proposed change is to add 304 SF of impervious surface to the previously approved 314,491 SF of impervious surface for an amended total of 314,795 SF of impervious surface. This 314,795 SF is well within the gravel wetland design capacity of 333,950 SF of impervious surface.

#### Gravel Wetland 2

Gravel Wetland 2 has a design capacity to treat 142,418 SF of impervious area for its 242,496 SF watershed area. The proposed change is to add 368 SF of impervious surface to the previously approved 48,306 SF of impervious surface for an amended total of 48,674 SF of impervious surface. This 48,674 SF is well within the gravel wetland design capacity of 142,418 SF of impervious surface.

## 3.0 Conclusion

The proposed amendment will result in no change to the previously approved postdevelopment peak runoff rates for Phase 2 and does not affect the Master Plan Drainage design. The net increase in impervious areas resulting from the proposed work will be directed to either Gravel Wetland 1 or Gravel Wetland 2 which both have the capacity to treat the slight increase in impervious surfaces. Phase 2 (2023 Approval) Post-Development Calculations

![](_page_344_Picture_0.jpeg)

![](_page_346_Figure_0.jpeg)

## L-0700-26 POST P2 Prepared by Tighe & Bond HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC

#### Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
2.312	61	>75% Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3,
		POST 1.4)
13.558	74	>75% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3,
		POST 1.4, POST 2.0)
1.467	80	>75% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4)
0.514	58	Meadow, non-grazed, HSG B (POST 1.3)
1.662	71	Meadow, non-grazed, HSG C (POST 1.3)
0.639	98	Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3)
6.959	98	Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4,
		POST 2.0)
0.137	98	Paved parking, HSG D (POST 1.0, POST 1.3)
0.120	98	Roofs, HSG B (POST 1.0)
3.526	98	Roofs, HSG C (POST 1.0, POST 2.0)
0.714	98	Roofs, HSG D (POST 1.0)
31.609	82	TOTAL AREA

#### Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
3.586	HSG B	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4
25.705	HSG C	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0
2.318	HSG D	POST 1.0, POST 1.3, POST 1.4
0.000	Other	
31.609		TOTAL AREA

L-0700-26 POST P2 Type III 24-hr 2 Year Rainfall=3.68" Prepared by Tighe & Bond Printed 7/13/2023 HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC Page 4 Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>2.61" Flow Length=933' Tc=11.4 min CN=90 Runoff=25.38 cfs 2.201 af Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>1.63" SubcatchmentPOST 1.1: WATERSHED Flow Length=464' Tc=8.3 min CN=78 Runoff=6.25 cfs 0.492 af Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>2.34" SubcatchmentPOST 1.2: WATERSHED Flow Length=1,191' Tc=6.4 min CN=87 Runoff=6.94 cfs 0.511 af Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>1.62" SubcatchmentPOST 1.3: WATERSHED Flow Length=1,525' Tc=45.9 min CN=78 Runoff=5.96 cfs 0.929 af SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>1.36" Flow Length=585' Tc=13.5 min CN=74 Runoff=8.76 cfs 0.822 af SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>2.34" Flow Length=758' Tc=5.0 min CN=87 Runoff=3.10 cfs 0.221 af Avg. Flow Depth=0.63' Max Vel=2.08 fps Inflow=6.94 cfs 0.511 af Reach REACH 1.0: RESTORED n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=4.97 cfs 0.507 af Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=46.02' Storage=67,987 cf Inflow=25.38 cfs 2.201 af Primary=0.96 cfs 0.874 af Secondary=0.00 cfs 0.000 af Outflow=0.96 cfs 0.874 af Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=52.38' Storage=21,415 cf Inflow=6.25 cfs 0.492 af Outflow=0.00 cfs 0.000 af Peak Elev=50.38' Inflow=6.94 cfs 0.511 af Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=6.94 cfs 0.511 af Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' Storage=8,981 cf Inflow=9.25 cfs 3.060 af Primary=9.25 cfs 2.856 af Secondary=0.00 cfs 0.000 af Outflow=9.25 cfs 2.856 af Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=44.62' Storage=21,007 cf Inflow=8.76 cfs 0.822 af Primary=0.51 cfs 0.751 af Secondary=0.00 cfs 0.000 af Outflow=0.51 cfs 0.751 af Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af Link PA1: POINT OF ANALYSIS Inflow=9.25 cfs 2.856 af Primary=9.25 cfs 2.856 af Inflow=3.10 cfs 0.221 af Link PA2: POINT OF ANALYSIS Primary=3.10 cfs 0.221 af

> Total Runoff Area = 31.609 ac Runoff Volume = 5.176 af Average Runoff Depth = 1.96" 61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

L-0700-26 POST P2 Type III 24-hr 10 Year Rainfall=5.58" Prepared by Tighe & Bond Printed 7/13/2023 HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC Page 5 Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>4.43" Flow Length=933' Tc=11.4 min CN=90 Runoff=42.01 cfs 3.732 af Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>3.21" SubcatchmentPOST 1.1: WATERSHED Flow Length=464' Tc=8.3 min CN=78 Runoff=12.40 cfs 0.966 af Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>4.11" SubcatchmentPOST 1.2: WATERSHED Flow Length=1,191' Tc=6.4 min CN=87 Runoff=11.94 cfs 0.897 af Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>3.18" SubcatchmentPOST 1.3: WATERSHED Flow Length=1,525' Tc=45.9 min CN=78 Runoff=11.87 cfs 1.826 af SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>2.83" Flow Length=585' Tc=13.5 min CN=74 Runoff=18.77 cfs 1.708 af SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>4.11" Flow Length=758' Tc=5.0 min CN=87 Runoff=5.36 cfs 0.388 af **Reach REACH 1.0: RESTORED** Avg. Flow Depth=0.82' Max Vel=2.20 fps Inflow=11.94 cfs 0.897 af n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=6.12 cfs 0.891 af Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=46.78' Storage=83,438 cf Inflow=42.01 cfs 3.732 af Primary=9.22 cfs 2.105 af Secondary=5.86 cfs 0.170 af Outflow=15.08 cfs 2.275 af Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=54.11' Storage=42,049 cf Inflow=12.40 cfs 0.966 af Outflow=0.00 cfs 0.000 af Peak Elev=50.72' Inflow=11.94 cfs 0.897 af Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=11.94 cfs 0.897 af Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.77' Storage=13,560 cf Inflow=31.34 cfs 5.942 af Primary=31.22 cfs 5.655 af Secondary=0.00 cfs 0.000 af Outflow=31.22 cfs 5.655 af Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=45.79' Storage=50,580 cf Inflow=18.77 cfs 1.708 af Primary=0.68 cfs 0.950 af Secondary=0.00 cfs 0.000 af Outflow=0.68 cfs 0.950 af Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af Link PA1: POINT OF ANALYSIS Inflow=31.22 cfs 5.655 af Primary=31.22 cfs 5.655 af Inflow=5.36 cfs 0.388 af Link PA2: POINT OF ANALYSIS Primary=5.36 cfs 0.388 af

> Total Runoff Area = 31.609 ac Runoff Volume = 9.517 af Average Runoff Depth = 3.61" 61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

#### Summary for Subcatchment POST 1.0: WATERSHED 1.0

Runoff = 42.01 cfs @ 12.16 hrs, Volume= 3.732 af, Depth> 4.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

5,235       98       Roofs, HSG B         29,148       61       >75% Grass cover, Good, HSG B         18,966       98       Paved parking, HSG B         143,455       98       Roofs, HSG C         82,022       74       >75% Grass cover, Good, HSG C         110,236       98       Paved parking, HSG C         31,119       98       Roofs, HSG D         14,671       80       >75% Grass cover, Good, HSG D         5,480       98       Paved parking, HSG D	
29,148       61       >75% Grass cover, Good, HSG B         18,966       98       Paved parking, HSG B         143,455       98       Roofs, HSG C         82,022       74       >75% Grass cover, Good, HSG C         110,236       98       Paved parking, HSG C         31,119       98       Roofs, HSG D         14,671       80       >75% Grass cover, Good, HSG D         5,480       98       Paved parking, HSG D	
18,966       98       Paved parking, HSG B         143,455       98       Roofs, HSG C         82,022       74       >75% Grass cover, Good, HSG C         110,236       98       Paved parking, HSG C         31,119       98       Roofs, HSG D         14,671       80       >75% Grass cover, Good, HSG D         5,480       98       Paved parking, HSG D	
143,455       98       Roofs, HSG C         82,022       74       >75% Grass cover, Good, HSG C         110,236       98       Paved parking, HSG C         31,119       98       Roofs, HSG D         14,671       80       >75% Grass cover, Good, HSG D         5,480       98       Paved parking, HSG D	
82,022 74 >75% Grass cover, Good, HSG C 110,236 98 Paved parking, HSG C 31,119 98 Roofs, HSG D 14,671 80 >75% Grass cover, Good, HSG D 5 480 98 Paved parking, HSG D	
110,236 98 Paved parking, HSG C 31,119 98 Roofs, HSG D 14,671 80 >75% Grass cover, Good, HSG D 5 480 98 Paved parking HSG D	
31,119 98 Roofs, HSG D 14,671 80 >75% Grass cover, Good, HSG D 5 480 98 Paved parking HSG D	
14,671 80 >75% Grass cover, Good, HSG D 5 480 98 Paved parking HSG D	
5 480 98 Paved parking HSG D	
440,332 90 Weighted Average	
125,841 28.58% Pervious Area	
314,491 71.42% Impervious Area	
To Longth Clans Malasity Consolity Description	
IC Length Slope velocity Capacity Description	
7.7 70 0.0150 0.15 Sheet Flow,	
Grass: Short n= 0.150 P2= 3.68"	
0.2 32 0.0200 2.87 Shallow Concentrated Flow,	
Paved KV= 20.3 tps	
U.I 19 U.U200 2.12 Shallow Concentrated Flow,	
Glassed Waterway KV- 15.0 lps	
0.0 102 0.0000 5.21 2.52 Fipe Channel, 12.0" Bound Area 0.9 of Borim 2.1	r- 0.25'
n=0.013 Corrugated DE smooth interio	1-0.20 vr
0.4 84 0.0050 3.21 2.52 <b>Pine Channel</b>	И
12 0" Round Area = 0.8 sf Perim = 3.1'	r= 0.25'
n = 0.013	1-0.25
0.5 113 0.0050 3.72 4.57 <b>Pine Channel</b>	
15.0" Round Area= 1.2 sf Perim= 3.9	r= 0.31'
n= 0.013	1 0.01
1 2 299 0 0050 4 20 7 43 <b>Pipe Channel</b>	
18.0" Round Area= 1.8 sf Perim= 4.7'	r= 0.38'
n= 0.013	
0.4 94 0.0050 4.20 7.43 <b>Pipe Channel</b> .	
18.0" Round Area= 1.8 sf Perim= 4.7'	r= 0.38'
n= 0.013	
0.1 46 0.0240 11.16 35.05 <b>Pipe Channel.</b>	
24.0" Round Area= 3.1 sf Perim= 6.3'	r= 0.50'
n= 0.013	
0.0 5 0.0800 7.16 0.98 Pipe Channel,	
5.0" Round Area= 0.1 sf Perim= 1.3' r	= 0.10'
n= 0.013	
0.0 9 0.0110 9.90 69.95 Pipe Channel,	

11.4

36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'

933 Total

#### Summary for Subcatchment POST 1.1: WATERSHED 1.1

n= 0.013

Runoff = 12.40 cfs @ 12.12 hrs, Volume= 0.966 af, Depth> 3.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN	Description				
	36,403	61	>75% Grass cover, Good, HSG B				
	3,210	98	Paved park	ing, HSG B	3		
	72,719	74	>75% Ġras	s cover, Go	bod, HSG C		
	45,096	98	Paved park	ing, HSG C			
1	57,428	78	Weighted A	verage			
1	09,122		69.32% Pe	rvious Area			
	48,306		30.68% Imp	pervious Ar	ea		
Тс	Length	Slope	e Velocity	Capacity	Description		
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)			
5.8	100	0.0625	5 0.29		Sheet Flow,		
					Grass: Short n= 0.150 P2= 3.68"		
2.2	312	0.0220	) 2.39		Shallow Concentrated Flow,		
					Unpaved Kv= 16.1 fps		
0.3	33	0.0150	) 1.84		Shallow Concentrated Flow,		
					Grassed Waterway Kv= 15.0 fps		
0.0	19	0.3300	) 8.62		Shallow Concentrated Flow,		
					Grassed Waterway Kv= 15.0 fps		
8.3	464	Total					

#### Summary for Subcatchment POST 1.2: WATERSHED 1.2

Runoff = 11.94 cfs @ 12.09 hrs, Volume= 0.897 af, Depth> 4.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
9,848	61	>75% Grass cover, Good, HSG B
4,784	98	Paved parking, HSG B
37,701	74	>75% Grass cover, Good, HSG C
61,646	98	Paved parking, HSG C
113,979	87	Weighted Average
47,549		41.72% Pervious Area
66,430		58.28% Impervious Area

Type III 24-hr 10 Year Rainfall=5.58" Printed 7/13/2023

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.5	100	0.0100	1.12	(/	Sheet Flow.
					Smooth surfaces $n = 0.011$ P2= 3.68"
1.0	153	0.0150	2.49		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
1.6	343	0.0050	3.47	2.73	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.012 Concrete pipe, finished
0.1	13	0.0050	3.72	4.57	Pipe Channel,
					15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
					n= 0.013 Corrugated PE, smooth interior
1.8	453	0.0050	4.20	7.43	Pipe Channel,
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
					n= 0.013 Corrugated PE, smooth interior
0.4	129	0.0050	5.91	29.00	Pipe Channel,
					30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63'
					n= 0.013 Corrugated PE, smooth interior
~ 4	4 4 0 4	<b>T</b> ( )			

6.4 1,191 Total

#### Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 11.87 cfs @ 12.63 hrs, Volume= 1.826 af, Depth> 3.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Α	rea (sf)	CN	Description		
	1,830	61	>75% Gras	s cover, Go	bod, HSG B
	22,404	58	Meadow, n	on-grazed,	HSG B
	896	98	Paved park	ing, HSG B	8
1	31,991	74	>75% Gras	s cover, Go	bod, HSG C
	68,446	98	Paved park	ing, HSG C	
	72,396	71	Meadow, n	on-grazed,	HSG C
	1,638	80	>75% Gras	s cover, Go	ood, HSG D
	499	98	Paved park	ing, HSG D	)
3	00,100	78	Weighted A	verage	
2	30,259		76.73% Pe	rvious Area	
	69,841		23.27% Imp	pervious Ar	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.9	100	0.0130	0.15		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.68"
1.1	52	0.0130	0.80		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.1	27	0.2720	7.82		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
33.8	1,346	0.0090	0.66		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
45.9	1,525	Total			

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#### Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff = 18.77 cfs @ 12.19 hrs, Volume= 1.708 af, Depth> 2.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN I	Description		
	23,477	61 3	>75% Gras	s cover, Go	bod, HSG B
2	43,330	74 :	>75% Gras	s cover, Go	bod, HSG C
	1,334	98 I	Paved park	ing, HSG C	
	47,586	80 ;	>75% Gras	s cover, Go	bod, HSG D
	0	96 (	Gravel surfa	ace, HSG [	
3	15,727	74	Neighted A	verage	
3	14,393	ę	99.58% Pe	rvious Area	l de la constante d
	1,334	(	0.42% Impe	ervious Are	а
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.4	100	0.0245	0.20		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.68"
5.1	465	0.0103	1.52		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
0.0	20	0.3300	8.62		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
13.5	585	Total			

#### Summary for Subcatchment POST 2.0: WATERSHED 2.0

[49] Hint: Tc<2dt may require smaller dt

Runoff = 5.36 cfs @ 12.07 hrs, Volume= 0.388 af, Depth> 4.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
10,145	98	Roofs, HSG C
22,815	74	>75% Grass cover, Good, HSG C
16,376	98	Paved parking, HSG C
49,336	87	Weighted Average
22,815		46.24% Pervious Area
26,521		53.76% Impervious Area

Type III 24-hr 10 Year Rainfall=5.58" Printed 7/13/2023

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Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
1.2	100	0.0164	1.36		Sheet Flow,
0.3	48	0.0164	2.60		Smooth surfaces n= 0.011 P2= 3.68" <b>Shallow Concentrated Flow,</b> Paved Ky= 20.3 fps
0.3	130	0.0140	7.03	12.43	<b>Pipe Channel,</b> 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
0.5	70	0.0250	2.37		Shallow Concentrated Flow, Grassed Waterway, Ky= 15.0 fps
1.3	410	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013

3.6 758 Total, Increased to minimum Tc = 5.0 min

#### Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

Inflow A	rea =	6.231 ac, 4	2.27% Impervious,	Inflow Depth > 1.	73" for 10 Y	ear event
Inflow	=	11.94 cfs @	12.09 hrs, Volume	= 0.897 af		
Outflow	=	6.12 cfs @	12.86 hrs, Volume	= 0.891 af,	Atten= 49%,	Lag= 45.9 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Max. Velocity= 2.20 fps, Min. Travel Time= 9.9 min Avg. Velocity = 0.85 fps, Avg. Travel Time= 25.6 min

Peak Storage= 6,846 cf @ 12.27 hrs Average Depth at Peak Storage= 0.82' Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs

Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals) Constant n= 0.040 Winding stream, pools & shoals Inlet Invert= 48.00', Outlet Invert= 36.00'

![](_page_355_Figure_11.jpeg)

6.75

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	Offset	Elevat	ion Ch	an.Depth		
_	(feet)	(fe	et)	(feet)		
	0.00	12	.00	0.00		
	18.00	6	.00	6.00		
	30.25	6	.00	6.00		
	31.75	5	.25	6.75		
	34.25	5	.25	6.75		
	35.75	6	.00	6.00		
	48.00	6	.00	6.00		
	66.00	12	.00	0.00		
	Depth En	d Area	Perim	. 9	Storage	Discharge
_	(feet)	(sq-ft)	(feet	) (cub	oic-feet)	(cfs)
	0.00	0.0	2.5	5	0	0.00
	0.75	3.0	30.4	ł	3.927	2.28

68.3

#### Summary for Pond POND 1.0: GRAVEL WETLAND 1

2,720.29

[95] Warning: Outlet Device #4 rise exceeded

291.0

Inflow Area =	10.109 ac, 71.42	2% Impervious, In	flow Depth > 4.43"	for 10 Year event
Inflow =	42.01 cfs @ 12.	16 hrs, Volume=	3.732 af	
Outflow =	15.08 cfs @ 12.	50 hrs, Volume=	2.275 af, Atter	n= 64%, Lag= 20.8 min
Primary =	9.22 cfs @ 12.	50 hrs, Volume=	2.105 af	-
Secondary =	5.86 cfs @ 12.	50 hrs, Volume=	0.170 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 46.78' @ 12.50 hrs Surf.Area= 21,240 sf Storage= 83,438 cf Flood Elev= 48.00' Surf.Area= 23,557 sf Storage= 110,845 cf

380,919

Plug-Flow detention time= 226.3 min calculated for 2.275 af (61% of inflow) Center-of-Mass det. time= 125.2 min (916.2 - 791.0)

Volume	Invert	Avai	I.Storage	Storage Descrip	otion	
#1	39.05'	1	10,845 cf	Custom Stage	Data (Prismatio	<b>)L</b> isted below (Recalc)
Elevation (feet)	Surf (	Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
39.05		9,855	0.0	0	0	
41.35		9,855	30.0	6,800	6,800	
42.00		9,855	45.0	2,883	9,683	
43.00	1	1,943	100.0	10,899	20,582	
44.00	1	4,202	100.0	13,073	33,654	
45.00	1	6,891	100.0	15,547	49,201	
46.00	1	9,752	100.0	18,322	67,522	
47.00	2	1,668	100.0	20,710	88,232	
48.00	2	3,557	100.0	22,613	110,845	

Type III 24-hr 10 Year Rainfall=5.58" Printed 7/13/2023 LLC Page 12

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Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	18.0" Round Culvert
	-		L= 30.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 41.35' / 41.20' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	41.35'	3.5" Vert. Orifice/Grate C= 0.600
#3	Device 1	45.00'	3.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	46.00'	4.0' long x 0.50' rise Sharp-Crested Rectangular Weir
			2 End Contraction(s) 0.5' Crest Height
#5	Device 1	47.00'	4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600
			Limited to weir flow at low heads
#6	Secondary	46.50'	15.0' long x 15.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

**Primary OutFlow** Max=9.22 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater)

**2=Orifice/Grate** (Orifice Controls 0.74 cfs @ 11.06 fps)

-3=Orifice/Grate (Orifice Controls 0.30 cfs @ 6.19 fps)

-4=Sharp-Crested Rectangular Weir (Orifice Controls 8.17 cfs @ 4.19 fps)

Secondary OutFlow Max=5.85 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater) **GeBroad-Crested Rectangular Weir** (Weir Controls 5.85 cfs @ 1.41 fps)

#### Summary for Pond POND 1.1: GRAVEL WETLAND 2

Inflow Are	ea =	3.614 ac, 3	0.68% Impervious,	Inflow Depth > 3.	.21" for 10	0 Year event
Inflow	=	12.40 cfs @	12.12 hrs, Volume	= 0.966 af		
Outflow	=	0.00 cfs @	0.00 hrs, Volume	= 0.000 af,	, Atten= 10	0%, Lag= 0.0 min
Primary	=	0.00 cfs @	0.00 hrs, Volume	= 0.000 af		-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 54.11' @ 24.00 hrs Surf.Area= 14,115 sf Storage= 42,049 cf Flood Elev= 57.00' Surf.Area= 21,643 sf Storage= 94,743 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	47.55'	117,304 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevatio	on	Surf.Area	Void	s Inc.Store	Cum.Store				
(feet)		(sq-ft)	(%	) (cubic-feet)	(cubic-feet)				
47.55		6.269	0.0	) 0	0				
49 8	35	6,269	30 (	4 326	4 326				
50.5	50	6,269	45.0	1.834	6,159				
51.0	00	7,199	100.0	3.367	9.526				
52.0	00	9,187	100.0	8,193	17,719				
53.0	00	11.345	100.0	10.266	27.985				
54.0	00	13,814	100.0	) 12,580	40,565				
55.0	00	16,645	100.0	15,230	55,794				
56.0	00	19,805	100.0	18,225	74,019				
58.0	00	23,480	100.0	) 43,285	117,304				
	_								
Device	Routing	In	vert	Outlet Devices					
#1	Primary	49	.85'	24.0" Round Culv	ert				
				L= 12.0' CPP, squ	are edge headwal	l, Ke= 0.500			
				Inlet / Outlet Invert=	: 49.85 <sup>°</sup> / 49.45' S	S= 0.0333 '/' Cc= 0.900			
				n= 0.013 Corrugate	ed PE, smooth inte	erior, Flow Area= 3.14 sf			
#2	Device 1	I 49	.85'	2.0" Vert. Orifice/Grate C= 0.600					
#3	Device 1	I 53	5.50'	4.0' long x 2.00' ris	Rectangular Weir				
				2 End Contraction(s)					
#4 Device 1 56.50' 4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600				<b>6.00</b> C= 0.600					
				Limited to weir flow	at low heads				

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=47.55' TW=55.07' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

**2=Orifice/Grate** (Controls 0.00 cfs)

-3=Sharp-Crested Rectangular Weir(Controls 0.00 cfs)

-4=Orifice/Grate (Controls 0.00 cfs)

#### Summary for Pond POND 1.2: PDMH203

Inflow Area	a =	6.231 ac, 4	2.27% Impe	ervious,	Inflow Depth >	1.73	5" for 10	Year event	
Inflow	=	11.94 cfs @	12.09 hrs,	Volume	= 0.897	' af			
Outflow	=	11.94 cfs @	12.09 hrs,	Volume	= 0.897	′af, A	Atten= 0%,	Lag= 0.0 mi	n
Primary	=	11.94 cfs @	12.09 hrs,	Volume	= 0.897	' af		-	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 50.72' @ 12.09 hrs Flood Elev= 57.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.35'	<b>48.0" Round Culvert</b> L= 269.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 49.35' / 48.00' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 12.57 sf

Primary OutFlow Max=11.76 cfs @ 12.09 hrs HW=50.71' TW=48.76' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 11.76 cfs @ 3.13 fps)

#### Summary for Pond POND 1.3: OUTLET CULVERTS

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=12) [62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.58' @ 23.95 hrs

Inflow Area	=	30.477 ac, 3	7.69% Imp	ervious, l	nflow Dep	pth >	2.34"	for 10	Year event
Inflow :	=	31.34 cfs @	12.51 hrs,	Volume=	: 5	5.942 a	af		
Outflow :	=	31.22 cfs @	12.53 hrs,	Volume=	: 5	5.655 a	af, At	ten= 0%,	Lag= 1.3 min
Primary :	=	31.22 cfs @	12.53 hrs,	Volume=	: 5	5.655 a	af		
Secondary :	=	0.00 cfs @	0.00 hrs,	Volume=	: (	0.000 a	af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 38.77' @ 12.53 hrs Surf.Area= 8,870 sf Storage= 13,560 cf Flood Elev= 43.50' Surf.Area= 95,977 sf Storage= 236,017 cf

Plug-Flow detention time= 56.2 min calculated for 5.642 af (95% of inflow) Center-of-Mass det. time= 29.8 min ( 900.3 - 870.4 )

Volume	Invert	Avail.Stor	age Storage	Description	
#1	35.00'	236,01	7 cf Custom	Stage Data (Pris	matic)Listed below (Recalc)
Elevation	Su	rf.Area	Inc.Store	Cum.Store	
(feet)		(sq-ft)	(cubic-feet)	(cubic-feet)	
35.00		960	0	0	
36.00		1,428	1,194	1,194	
38.00		5,418	6,846	8,040	
40.00		14,354	19,772	27,812	
42.00		66,884	81,238	109,050	
43.00		92,707	79,796	188,846	
43.50		95,977	47,171	236,017	
Device F	Routing	Invert	Outlet Devices	5	
#1 F #2 S	Primary Secondary	35.60' 43.00'	<b>42.0" W x 29.</b> L= 68.0' CMF Inlet / Outlet In n= 0.025 Corr <b>143.1 deg x 1</b> Cv= 2.47 (C=	0" H, R=21.5"/66. P, square edge he nvert= 35.60' / 35.3 rugated metal, Flo 8.0' long x 0.50' r 3.09)	<b>1" Pipe Arch CMP_Arch_1/2 42x29 X 3.00</b> adwall, Ke= 0.500 30' S= 0.0044 '/' Cc= 0.900 bw Area= 6.72 sf rise Sharp-Crested Vee/Trap Weir

**Primary OutFlow** Max=31.11 cfs @ 12.53 hrs HW=38.77' TW=38.65' (Dynamic Tailwater) **1=CMP\_Arch\_1/2 42x29** (Outlet Controls 31.11 cfs @ 1.55 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=35.04' TW=38.65' (Dynamic Tailwater) 2=Sharp-Crested Vee/Trap Weir( Controls 0.00 cfs)
## Summary for Pond POND 1.4: SEDIMENT BASIN 1.0

Inflow Area	=	7.248 ac,	0.42% Impe	ervious,	Inflow	Depth >	2.8	3" for	<sup>·</sup> 10 Y	ear eve	ent	
Inflow =	=	18.77 cfs @	12.19 hrs,	Volume	=	1.708	af					
Outflow =	=	0.68 cfs @	17.24 hrs,	Volume	=	0.950	af,	Atten=	96%,	Lag= 3	303.1	min
Primary =	=	0.68 cfs @	17.24 hrs,	Volume	=	0.950	af					
Secondary =	=	0.00 cfs @	0.00 hrs,	Volume	=	0.000	af					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Starting Elev= 44.15' Surf.Area= 18,132 sf Storage= 11,702 cf Peak Elev= 45.79' @ 17.24 hrs Surf.Area= 29,244 sf Storage= 50,580 cf (38,878 cf above start) Flood Elev= 48.50' Surf.Area= 38,802 sf Storage= 127,441 cf (115,739 cf above start)

Plug-Flow detention time= 356.9 min calculated for 0.681 af (40% of inflow) Center-of-Mass det. time= 9.2 min ( 846.8 - 837.5 )

Volume	Invert	Avail.Sto	rage Storage	Description				
#1	43.00'	127,44	41 cf Custom	Stage Data (Prisn	natic)Listed below (Recalc)			
Elevatio (fee	on Si et)	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
43.0	00	1,000	0	0				
44.0	00	17,117	9,059	9,059				
46.0	00	30,657	47,774	56,833				
47.0	00	35,879	33,268	90,101				
48.0	00	38,802	37,341	127,441				
Device	Routing	Invert	Outlet Device	S				
#1	Primary	42.75'	<b>12.0" Round</b> Inlet / Outlet I n= 0.013, Flo	l <b>Culvert</b> L= 66.0' nvert= 42.75' / 42.4 w Area= 0.79 sf	Ke= 0.500 0' S= 0.0053 '/' Cc= 0.900			
#2	Device 1	43.00'	4.0" Vert. Ori	fice/Grate C= 0.6	00			
#3	Device 1	46.80'	10.0" x 17.5"	Horiz. Orifice/Gra	<b>te</b> C= 0.600			
			Limited to we	ir flow at low heads				
#4	Secondary	47.40'	Custom Wei	r/Orifice, Cv= 2.62	(C= 3.28)			
			Head (feet) 0 Width (feet) 8	0.00 1.10 3.00 14.60				
Primary <sup>●</sup> _1=Cu	Primary OutFlow Max=0.68 cfs @ 17.24 hrs HW=45.79' TW=38.65' (Dynamic Tailwater)							

-2=Orifice/Grate (Orifice Controls 0.68 cfs @ 7.80 fps)

**3=Orifice/Grate** (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=44.15' TW=35.04' (Dynamic Tailwater) -4=Custom Weir/Orifice (Controls 0.00 cfs)

## Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.1 by 7.52' @ 0.00 hrs (23.95 cfs 41.618 af)

Inflow A	rea =	3.614 ac, 3	0.68% Impervious, Infl	ow Depth = $0.00"$	for 10 Year event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Primary	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Y	ear	25 P	oint manual	elevation	table,	To=	0.00 hrs,	dt= 1.00 hrs,	feet =		
	55.0	)7	55.07	55.07	55	.07	55.07	55.07	55.07	55.07	55.07
	55.0	)7	55.07	55.07	55	.07	55.07	55.07	55.07	55.07	55.07
	55.0	)7	55.07	55.07	55	.07	55.07	55.07	55.07		

# Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.3 by 3.61' @ 0.00 hrs (92.51 cfs 60.023 af)

Inflow .	Area =	30.477 ac,	37.69% Impervious,	Inflow Depth > 2	.23" for 10 Y	ear event
Inflow	=	31.22 cfs @	12.53 hrs, Volume	e= 5.655 af		
Primar	y =	31.22 cfs @	12.53 hrs, Volume	e= 5.655 af	, Atten= 0%, L	.ag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 2 Point manual elevation table, To= 0.00 hrs, dt= 24.00 hrs, feet = 38.65 38.65

### Summary for Link PA2: POINT OF ANALYSIS

Inflow Are	a =	1.133 ac, 🗄	53.76% Impe	ervious,	Inflow Depth	1 > 4. <sup>°</sup>	11" for 10	Year event
Inflow	=	5.36 cfs @	12.07 hrs,	Volume	= 0.3	388 af		
Primary	=	5.36 cfs @	12.07 hrs,	Volume	= 0.3	388 af,	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

L-0700-26 POST P2 Type III 24-hr 25 Year Rainfall=7.07" Prepared by Tighe & Bond Printed 7/13/2023 HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC Page 17 Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>5.88" Flow Length=933' Tc=11.4 min CN=90 Runoff=54.93 cfs 4.956 af Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>4.53" SubcatchmentPOST 1.1: WATERSHED Flow Length=464' Tc=8.3 min CN=78 Runoff=17.44 cfs 1.365 af Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>5.54" SubcatchmentPOST 1.2: WATERSHED Flow Length=1,191' Tc=6.4 min CN=87 Runoff=15.85 cfs 1.209 af Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>4.50" SubcatchmentPOST 1.3: WATERSHED Flow Length=1,525' Tc=45.9 min CN=78 Runoff=16.75 cfs 2.583 af SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>4.09" Flow Length=585' Tc=13.5 min CN=74 Runoff=27.23 cfs 2.472 af SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>5.54" Flow Length=758' Tc=5.0 min CN=87 Runoff=7.12 cfs 0.523 af **Reach REACH 1.0: RESTORED** Avg. Flow Depth=0.87' Max Vel=2.22 fps Inflow=15.85 cfs 1.209 af n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=8.65 cfs 1.202 af Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=47.10' Storage=90,424 cf Inflow=54.93 cfs 4.956 af Primary=19.03 cfs 2.766 af Secondary=18.86 cfs 0.671 af Outflow=37.88 cfs 3.437 af Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=55.22' Storage=59,446 cf Inflow=17.44 cfs 1.365 af Outflow=0.00 cfs 0.000 af Peak Elev=50.94' Inflow=15.85 cfs 1.209 af Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=15.85 cfs 1.209 af Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.17' Storage=17,433 cf Inflow=57.33 cfs 8.292 af Primary=56.26 cfs 7.985 af Secondary=0.00 cfs 0.000 af Outflow=56.26 cfs 7.985 af Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=46.65' Storage=77,792 cf Inflow=27.23 cfs 2.472 af Primary=0.78 cfs 1.070 af Secondary=0.00 cfs 0.000 af Outflow=0.78 cfs 1.070 af Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af Link PA1: POINT OF ANALYSIS Inflow=56.26 cfs 7.985 af Primary=56.26 cfs 7.985 af Inflow=7.12 cfs 0.523 af Link PA2: POINT OF ANALYSIS Primary=7.12 cfs 0.523 af

> Total Runoff Area = 31.609 ac Runoff Volume = 13.108 af Average Runoff Depth = 4.98" 61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

L-0700-26 POST P2 Type III 24-hr 50 Year Rainfall=8.46" Prepared by Tighe & Bond Printed 7/13/2023 HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC Page 18 Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>7.25" Flow Length=933' Tc=11.4 min CN=90 Runoff=66.89 cfs 6.105 af Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>5.81" SubcatchmentPOST 1.1: WATERSHED Flow Length=464' Tc=8.3 min CN=78 Runoff=22.21 cfs 1.750 af Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>6.89" SubcatchmentPOST 1.2: WATERSHED Flow Length=1,191' Tc=6.4 min CN=87 Runoff=19.47 cfs 1.503 af Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>5.77" SubcatchmentPOST 1.3: WATERSHED Flow Length=1,525' Tc=45.9 min CN=78 Runoff=21.37 cfs 3.312 af SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>5.33" Flow Length=585' Tc=13.5 min CN=74 Runoff=35.32 cfs 3.218 af SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>6.89" Flow Length=758' Tc=5.0 min CN=87 Runoff=8.76 cfs 0.651 af Reach REACH 1.0: RESTORED Avg. Flow Depth=0.92' Max Vel=2.24 fps Inflow=19.47 cfs 1.503 af n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=11.76 cfs 1.495 af Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=47.39' Storage=96,897 cf Inflow=66.89 cfs 6.105 af Primary=19.58 cfs 3.347 af Secondary=33.37 cfs 1.209 af Outflow=52.94 cfs 4.556 af Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=56.11' Storage=76,209 cf Inflow=22.21 cfs 1.750 af Outflow=0.00 cfs 0.000 af Peak Elev=51.13' Inflow=19.47 cfs 1.503 af Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=19.47 cfs 1.503 af Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.58' Storage=22,150 cf Inflow=76.91 cfs 10.982 af Primary=74.09 cfs 10.655 af Secondary=0.00 cfs 0.000 af Outflow=74.09 cfs 10.655 af Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=47.02' Storage=90,878 cf Inflow=35.32 cfs 3.218 af Primary=2.39 cfs 1.619 af Secondary=0.00 cfs 0.000 af Outflow=2.39 cfs 1.619 af Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af Link PA1: POINT OF ANALYSIS Inflow=74.09 cfs 10.655 af Primary=74.09 cfs 10.655 af Inflow=8.76 cfs 0.651 af Link PA2: POINT OF ANALYSIS Primary=8.76 cfs 0.651 af

> Total Runoff Area = 31.609 ac Runoff Volume = 16.539 af Average Runoff Depth = 6.28" 61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

Phase 2 (2024 Amended) Post-Development Calculations





# Area Listing (all nodes)

	Area	CN	Description
(	acres)		(subcatchment-numbers)
	2.312	61	>75% Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3,
			POST 1.4)
	13.542	74	>75% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3,
			POST 1.4, POST 2.0)
	1.467	80	>75% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4)
	0.514	58	Meadow, non-grazed, HSG B (POST 1.3)
	1.662	71	Meadow, non-grazed, HSG C (POST 1.3)
	0.639	98	Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3)
	6.974	98	Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4,
			POST 2.0)
	0.137	98	Paved parking, HSG D (POST 1.0, POST 1.3)
	0.120	98	Roofs, HSG B (POST 1.0)
	3.526	98	Roofs, HSG C (POST 1.0, POST 2.0)
	0.714	98	Roofs, HSG D (POST 1.0)
:	31.609	82	TOTAL AREA

# Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
3.586	HSG B	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4
25.705	HSG C	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0
2.318	HSG D	POST 1.0, POST 1.3, POST 1.4
0.000	Other	
31.609		TOTAL AREA

L-0700-26 POST P2 Prepared by Tighe & Bond Consulting HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solutions	Type III 24-hr2 Year Rainfall=3.68"Printed 3/1/2024LLCPage 4
Time span=0.00-24.00 hrs, dt=0.05 hrs	, 481 points
Runoff by SCS TR-20 method, UH=SCS,	Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routin	Ig by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf	71.49% Impervious Runoff Depth>2.61"
Flow Length=933' Tc=11.4	min CN=90 Runoff=25.38 cfs 2.201 af
SubcatchmentPOST 1.1: WATERSHED Runoff Area=157,428 sf	30.92% Impervious Runoff Depth>1.63"
Flow Length=464' Tc=8.	3 min CN=78 Runoff=6.25 cfs 0.492 af
SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 sf	58.28% Impervious Runoff Depth>2.34"
Flow Length=1,191' Tc=6.	4 min CN=87 Runoff=6.94 cfs 0.511 af
SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 sf	23.27% Impervious Runoff Depth>1.62"
Flow Length=1,525' Tc=45.	9 min CN=78 Runoff=5.96 cfs 0.929 af
SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 st	f  0.42% Impervious  Runoff Depth>1.36"
Flow Length=585' Tc=13.	5 min  CN=74  Runoff=8.76 cfs  0.822 af
SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,336 sf	53.76% Impervious Runoff Depth>2.34"
Flow Length=758' Tc=5.	0 min CN=87 Runoff=3.10 cfs 0.221 af
Reach REACH 1.0: RESTORED         Avg. Flow Depth=0.63'         M           n=0.040         L=1,309.0'         S=0.0092 '/'         Capacity	ax Vel=2.08 fps Inflow=6.94 cfs 0.511 af =2,720.29 cfs Outflow=4.97 cfs 0.507 af
Pond POND 1.0: GRAVEL WETLAND1         Peak Elev=46.02' Stor           Primary=0.96 cfs         0.874 af         Secondary=0.00	age=67,987 cf Inflow=25.38 cfs 2.201 af ) cfs 0.000 af Outflow=0.96 cfs 0.874 af
Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=52.38' Sto	orage=21,415 cf Inflow=6.25 cfs 0.492 af Outflow=0.00 cfs 0.000 af
Pond POND 1.2: PDMH203	eak Elev=50.38' Inflow=6.94 cfs 0.511 af
48.0" Round Culvert n=0.013 L=269.0	' S=0.0050 '/' Outflow=6.94 cfs 0.511 af
Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' S	torage=8,981 cf Inflow=9.25 cfs 3.060 af
Primary=9.25 cfs 2.856 af Secondary=0.00	) cfs 0.000 af Outflow=9.25 cfs 2.856 af
Pond POND 1.4: SEDIMENT BASIN 1.0Peak Elev=44.62' StoPrimary=0.51 cfs0.751 afSecondary=0.00	orage=21,007 cf Inflow=8.76 cfs 0.822 af 0 cfs 0.000 af Outflow=0.51 cfs 0.751 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Link PA1: POINT OF ANALYSIS	Inflow=9.25 cfs 2.856 af Primary=9.25 cfs 2.856 af
Link PA2: POINT OF ANALYSIS	Inflow=3.10 cfs 0.221 af Primary=3.10 cfs 0.221 af

Total Runoff Area = 31.609 acRunoff Volume = 5.176 afAverage Runoff Depth = 1.96"61.68% Pervious = 19.497 ac38.32% Impervious = 12.112 ac

L-0700-26 POST P2 Prepared by Tighe & Bond Consulting HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solution	Type III 24-hr	10 Year Rainfall=5.58" Printed 3/1/2024 Page 5
Time span=0.00-24.00 hrs, dt=0.05 Runoff by SCS TR-20 method, UH=S0 Reach routing by Dyn-Stor-Ind method - Pond ro	hrs, 481 points CS, Weighted-CN uting by Dyn-Stor-I	Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 Flow Length=933' Tc=1	sf 71.49% Impervi 1.4 min CN=90 R	ous Runoff Depth>4.43" Runoff=42.01 cfs 3.732 af
SubcatchmentPOST 1.1: WATERSHED Runoff Area=157,428 Flow Length=464' Tc=	sf 30.92% Impervi 8.3 min CN=78 R	ous Runoff Depth>3.21" Runoff=12.40 cfs 0.966 af
SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 Flow Length=1,191' Tc=	sf 58.28% Impervi 6.4 min CN=87 R	ous Runoff Depth>4.11" Runoff=11.94 cfs 0.897 af
SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 Flow Length=1,525' Tc=4	sf 23.27% Impervi 5.9 min CN=78 R	ous Runoff Depth>3.18" Runoff=11.87 cfs 1.826 af
SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,72 Flow Length=585' Tc=1	7 sf 0.42% Impervi 3.5 min CN=74 R	ous Runoff Depth>2.83" Runoff=18.77 cfs 1.708 af
SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,336 Flow Length=758' To	sf 53.76% Impervi =5.0 min CN=87	ous Runoff Depth>4.11" Runoff=5.36 cfs 0.388 af
Reach REACH 1.0: RESTORED         Avg. Flow Depth=0.82'           n=0.040         L=1,309.0'         S=0.0092 '/'         Capa	Max Vel=2.20 fps l city=2,720.29 cfs C	Inflow=11.94 cfs 0.897 af Dutflow=6.12 cfs 0.891 af
Pond POND 1.0: GRAVEL WETLAND1Peak Elev=46.78' SPrimary=9.22 cfs2.105 afSecondary=5	Storage=83,438 cf   l 86 cfs  0.170 af   Oเ	Inflow=42.01 cfs  3.732 af utflow=15.08 cfs  2.275 af
Pond POND 1.1: GRAVEL WETLAND2       Peak Elev=54.11'	Storage=42,049 cf(	Inflow=12.40 cfs 0.966 af Outflow=0.00 cfs 0.000 af
Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=269	Peak Elev=50.72' 9.0' S=0.0050 '/' Ou	Inflow=11.94 cfs 0.897 af utflow=11.94 cfs 0.897 af
Pond POND 1.3: OUTLET CULVERTSPeak Elev=38.77'Primary=31.22 cfs5.655 afSecondary=0	Storage=13,560 cf ป 00 cfs 0.000 af Oเ	Inflow=31.34 cfs 5.942 af utflow=31.22 cfs 5.655 af
Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=45.79' S Primary=0.68 cfs 0.950 af Secondary=	Storage=50,580 cf I 0.00 cfs 0.000 af C	Inflow=18.77 cfs 1.708 af Dutflow=0.68 cfs 0.950 af
Link LINK 1.0: PDMH203 TAILWATER	F	Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Link PA1: POINT OF ANALYSIS	Pr	Inflow=31.22 cfs 5.655 af rimary=31.22 cfs 5.655 af
Link PA2: POINT OF ANALYSIS	F	Inflow=5.36 cfs 0.388 af Primary=5.36 cfs 0.388 af

Total Runoff Area = 31.609 ac Runoff Volume = 9.517 af Average Runoff Depth = 3.61" 61.68% Pervious = 19.497 ac 38.32% Impervious = 12.112 ac

## Summary for Subcatchment POST 1.0: WATERSHED 1.0

- [47] Hint: Peak is 1668% of capacity of segment #4
- [47] Hint: Peak is 1668% of capacity of segment #5
- [47] Hint: Peak is 920% of capacity of segment #6
- [47] Hint: Peak is 566% of capacity of segment #7
- [47] Hint: Peak is 566% of capacity of segment #8
- [47] Hint: Peak is 120% of capacity of segment #9 [47] Hint: Peak is 4305% of capacity of segment #10
- Runoff = 42.01 cfs @ 12.16 hrs, Volume= 3.732 af, Depth> 4.43" Routed to Pond POND 1.0 : GRAVEL WETLAND 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
5,235	98	Roofs, HSG B
29,148	61	>75% Grass cover, Good, HSG B
18,966	98	Paved parking, HSG B
143,455	98	Roofs, HSG C
81,718	74	>75% Grass cover, Good, HSG C
110,540	98	Paved parking, HSG C
31,119	98	Roofs, HSG D
14,671	80	>75% Grass cover, Good, HSG D
5,480	98	Paved parking, HSG D
440,332	90	Weighted Average
125,537		28.51% Pervious Area
314,795		71.49% Impervious Area

## L-0700-26 POST P2

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Tc Length Slope Velocity Capacity Description

(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
7.7	70	0.0150	0.15		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.68"
0.2	32	0.0200	2.87		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
0.1	19	0.0200	2.12		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
0.8	162	0.0050	3.21	2.52	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013 Corrugated PE, smooth interior
0.4	84	0.0050	3.21	2.52	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013
0.5	113	0.0050	3.72	4.57	Pipe Channel,
					15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
					n= 0.013
1.2	299	0.0050	4.20	7.43	Pipe Channel,
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
				- 10	n= 0.013
0.4	94	0.0050	4.20	7.43	Pipe Channel,
					18.0" Round Area= 1.8 st Perim= 4.7' r= 0.38'
	10	0 00 40			n= 0.013
0.1	46	0.0240	11.16	35.05	Pipe Channel,
					24.0" Round Area= 3.1 st Perim= 6.3' r= 0.50'
	-	0.0000	7.40	0.00	n= 0.013
0.0	5	0.0800	7.16	0.98	Pipe Channel,

 0.0
 5
 0.0800
 7.16
 0.98
 Pipe Channel,

 5.0"
 Round Area= 0.1 sf Perim= 1.3' r= 0.10'

 n= 0.013

 0.0
 9
 0.0110
 9.90
 69.95
 Pipe Channel,

 36.0"
 Round Area= 7.1 sf Perim= 9.4' r= 0.75'

 n= 0.013

11.4 933 Total

### Summary for Subcatchment POST 1.1: WATERSHED 1.1

Runoff = 12.40 cfs @ 12.12 hrs, Volume= 0.966 af, Depth> 3.21" Routed to Pond POND 1.1 : GRAVEL WETLAND 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description				
36,403	61	>75% Grass cover, Good, HSG B				
3,210	98	Paved parking, HSG B				
72,351	74	>75% Grass cover, Good, HSG C				
45,464	98	Paved parking, HSG C				
157,428	78	Weighted Average				
108,754		69.08% Pervious Area				
48,674		30.92% Impervious Area				

Type III 24-hr 10 Year Rainfall=5.58" Printed 3/1/2024

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### L-0700-26 POST P2 Prepared by Tighe & Bond Consulting

Type III 24-hr 10 Year Rainfall=5.58" Printed 3/1/2024 HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solutions LLC Page 8

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.8	100	0.0625	0.29		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.68"
2.2	312	0.0220	2.39		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
0.3	33	0.0150	1.84		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
0.0	19	0.3300	8.62		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps

8.3 464 Total

## Summary for Subcatchment POST 1.2: WATERSHED 1.2

- [47] Hint: Peak is 437% of capacity of segment #3
- [47] Hint: Peak is 261% of capacity of segment #4
- [47] Hint: Peak is 161% of capacity of segment #5

Runoff	=	11.94 cfs @	12.09 hrs,	Volume=
Routed	d to	Pond POND 1.2 :	PDMH203	

0.897 af, Depth> 4.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN D	CN Description						
	9,848	61 >	61 >75% Grass cover, Good, HSG B						
	4,784	98 P	aved park	ing, HSG B					
	37,701	74 >	75% Gras	s cover, Go	ood, HSG C				
	61,646	98 P	aved park	ing, HSG C					
1	13,979	87 V	Veighted A	verage					
	47,549	4	1.72% Per	vious Area					
	66,430	5	8.28% Imp	pervious Ar	ea				
Та	Longth	Clana	Valacity	Consoitu	Description				
(min)	(feet)				Description				
1	100		(1/300)	(015)	Shoot Flow				
1.5	100	0.0100	1.12		Smooth surfaces n= 0.011 P2= 3.68"				
10	153	0 0150	2 4 9		Shallow Concentrated Flow				
1.0	100	0.0100	2.40		Paved $Kv = 20.3 \text{ fps}$				
1.6	343	0.0050	3.47	2.73	Pipe Channel.				
			••••		12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
					n= 0.012 Concrete pipe, finished				
0.1	13	0.0050	3.72	4.57	Pipe Channel,				
					15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'				
					n= 0.013 Corrugated PE, smooth interior				
1.8	453	0.0050	4.20	7.43	Pipe Channel,				
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'				
					n= 0.013 Corrugated PE, smooth interior				
0.4	129	0.0050	5.91	29.00	Pipe Channel,				
					30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63'				
					n= 0.013 Corrugated PE, smooth interior				

6.4 1,191 Total

### Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 11.87 cfs @ 12.63 hrs, Volume= 1.826 af, Depth> 3.18" Routed to Pond POND 1.3 : OUTLET CULVERTS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Ar	ea (sf)	CN [	Description		
	1,830	61 >	>75% Gras	s cover, Go	bod, HSG B
2	22,404	58 N	Meadow, no	on-grazed,	HSG B
	896	98 F	Paved park	ing, HSG E	3
13	31,991	74 >	>75% Gras	s cover, Go	bod, HSG C
6	58,446	98 F	Paved park	ing, HSG C	
7	72,396	71 N	Aeadow, no	on-grazed,	HSG C
	1,638	80 >	>75% Gras	s cover, Go	bod, HSG D
	499	98 F	Paved park	ing, HSG E	)
30	00,100	78 \	Veighted A	verage	
23	30,259	7	76.73% Pei	rvious Area	
6	59,841	2	23.27% Imp	pervious Ar	ea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.9	100	0.0130	0.15		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.68"
1.1	52	0.0130	0.80		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.1	27	0.2720	7.82		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
33.8	1,346	0.0090	0.66		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
45.9	1,525	Total			

### Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff = 18.77 cfs @ 12.19 hrs, Volume= 1.708 af, Depth> 2.83" Routed to Pond POND 1.4 : SEDIMENT BASIN 1.0

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

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Type III 24-hr 10 Year Rainfall=5.58" Printed 3/1/2024 HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solutions LLC Page 10

Δ.	roa (cf)		<b>Noncorintian</b>						
A									
	23,477	61 >	·75% Gras	s cover, Go	bod, HSG B				
2	43,330	74 >	·75% Gras	s cover, Go	bod, HSG C				
	1,334	98 F	aved park	ing, HSG C					
	47.586	80 >	·75% Ġras	s cover. Go	bod, HSG D				
	0	96 C	Gravel surfa	ace, HSG D	)				
3	15.727	74 V	Veiahted A	verade					
3	14 393	ç	9 58% Pe	vious Area					
U	1 334	Ċ	42% Impe	rvious Are	a				
	1,004	C C	.4270 mpc		ü				
Тс	l enath	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Decomption				
	100	0.0245	0.20	(010)	Shoot Flow				
8.4	100	0.0245	0.20		Sneet Flow,				
					Grass: Short n= 0.150 P2= 3.68"				
5.1	465	0.0103	1.52		Shallow Concentrated Flow,				
					Grassed Waterway Kv= 15.0 fps				
0.0	20	0.3300	8.62		Shallow Concentrated Flow,				
					Grassed Waterway Kv= 15.0 fps				
13.5	585	Total							

## Summary for Subcatchment POST 2.0: WATERSHED 2.0

[49] Hint: Tc<2dt may require smaller dt

5.36 cfs @ 12.07 hrs, Volume= Runoff = Routed to Link PA2 : POINT OF ANALYSIS

0.388 af, Depth> 4.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

_	A	rea (sf)	CN D	escription			
_		10,145 98 Roofs, HSG C					
		22,815	74 >	75% Gras	s cover, Go	ood, HSG C	
		16,376	98 F	aved park	ing, HSG C		
_		49,336	87 V	Veighted A	verage		
		22,815	4	6.24% Per	vious Area		
		26,521	5	3.76% Imp	pervious Are	ea	
		,		•			
	Тс	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	'	
_	1.2	100	0.0164	1.36		Sheet Flow,	
						Smooth surfaces n= 0.011 P2= 3.68"	
	0.3	48	0.0164	2.60		Shallow Concentrated Flow,	
						Paved Kv= 20.3 fps	
	0.3	130	0.0140	7.03	12.43	Pipe Channel,	
						18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'	
						n= 0.013	
	0.5	70	0.0250	2.37		Shallow Concentrated Flow,	
						Grassed Waterway Kv= 15.0 fps	
	1.3	410	0.0050	5.09	16.00	Pipe Channel,	
						24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'	

#### n= 0.013

3.6 758 Total, Increased to minimum Tc = 5.0 min

### Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

Inflow Area = 6.231 ac, 42.41% Impervious, Inflow Depth > 1.73" for 10 Year event Inflow = 11.94 cfs @ 12.09 hrs, Volume= 0.897 af Outflow = 6.12 cfs @ 12.86 hrs, Volume= 0.891 af, Atten= 49%, Lag= 45.9 min Routed to Pond POND 1.3 : OUTLET CULVERTS

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Max. Velocity= 2.20 fps, Min. Travel Time= 9.9 min Avg. Velocity = 0.85 fps, Avg. Travel Time= 25.6 min

Peak Storage= 6,846 cf @ 12.27 hrs Average Depth at Peak Storage= 0.82', Surface Width= 30.44' Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs

Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals) Constant n= 0.040 Winding stream, pools & shoals Inlet Invert= 48.00', Outlet Invert= 36.00'

±

	Of	fset	Eleva	ation	Cha	n.De	oth		
	(fe	eet)	(1	feet)		(fe	et)		
	C	0.00	1	2.00		0.	00		
	18	3.00		6.00		6.	00		
	30	).25		6.00		6.	00		
	31	.75		5.25		6.	75		
	34	1.25		5.25		6.	75		
	35	5.75		6.00		6.	00		
	48	3.00		6.00		6.	00		
	66	6.00	1	2.00		0.	00		
C	Depth	En	d Area	Pe	erim.	W	idth		Stc
	(feet)		(sq-ft)	(1	eet)	(f	eet)	(cub	oic-
	0.00		0.0		2.5		0.0		

Depth	End Area	Perim.	Width	Storage	Discharge
(feet)	(sq-ft)	(feet)	(feet)	(cubic-feet)	(cfs)
0.00	0.0	2.5	0.0	0	0.00
0.75	3.0	30.4	30.0	3,927	2.28
6.75	291.0	68.3	66.0	380,919	2,720.29

## Summary for Pond POND 1.0: GRAVEL WETLAND 1

[95] Warning: Outlet Device #4 rise exceeded

Inflow Are	a =	10.109 ac, 7	1.49% Impervious,	Inflow Depth > 4.4	13" for 10 Year event
Inflow	=	42.01 cfs @	12.16 hrs, Volume	= 3.732 af	
Outflow	=	15.08 cfs @	12.50 hrs, Volume	= 2.275 af,	Atten= 64%, Lag= 20.8 min
Primary	=	9.22 cfs @	12.50 hrs, Volume	= 2.105 af	-
Routed	l to Po	ond POND 1.3 :	OUTLET CULVERT	S	
Secondary	y =	5.86 cfs @	12.50 hrs, Volume	= 0.170 af	
Routed	to Po	ond POND 1.3 :	OUTLET CULVERT	S	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 46.78' @ 12.50 hrs Surf.Area= 21,240 sf Storage= 83,438 cf Flood Elev= 48.00' Surf.Area= 23,557 sf Storage= 110,845 cf

Plug-Flow detention time= 226.3 min calculated for 2.275 af (61% of inflow) Center-of-Mass det. time= 125.2 min (916.2 - 791.0)

Volume	Invert	Avai	il.Storage	Storage Descript	tion	
#1	39.05'	1	10,845 cf	Custom Stage I	Data (Prismatic)Li	sted below (Recalc)
Elevatio	on S	urf.Area	Voids	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
39.0	)5	9,855	0.0	0	0	
41.3	35	9,855	30.0	6,800	6,800	
42.0	00	9,855	45.0	2,883	9,683	
43.0	00	11,943	100.0	10,899	20,582	
44.(	00	14,202	100.0	13,073	33,654	
45.0	)0	16,891	100.0	15,547	49,201	
46.0	00	19,752	100.0	18,322	67,522	
47.0	00	21,668	100.0	20,710	88,232	
48.0	00	23,557	100.0	22,613	110,845	
Device	Routing	In	vert Ou	tlet Devices		
#1	Primary	41	.35' 18.	0" Round Culver	t	
			L=	30.0' CPP, square	e edge headwall, k	Ke= 0.500
			Inle	et / Outlet Invert= 4	1.35'/41.20' S= (	0.0050 '/' Cc= 0.900
			n=	0.013 Corrugated	PE, smooth interio	r,  Flow Area= 1.77 sf
#2	Device 1	41	.35' <b>3.5</b>	" Vert. Orifice/Gra	te C= 0.600 Lim	nited to weir flow at low heads
#3	Device 1	45	5.00' <b>3.0</b>	" Vert. Orifice/Gra	te C= 0.600 Lim	nited to weir flow at low heads
#4	Device 1	46	5.00' <b>4.0</b>	' long x 0.50' rise	Sharp-Crested Re	ectangular Weir
			2 E	nd Contraction(s)	0.5' Crest Height	
#5	Device 1	47	'.00' <b>4.0</b>	" x 4.0" Horiz. Ori	fice/Grate X 106.0	<b>0</b> C= 0.600
#6	Secondary	46		nieu io wen now al	IOW HEAUS	tod Bootongular Wair
#0	Secondary	40	ס.טט <b>וס.</b> שמ	o 10119 x 13.0 DF	0 60 0 80 1 00	
				au (1601) 0.20 0.40	270 270 264 2	63 2 64 2 64 2 63
			00	51. (LIIYIISII) 2.00	2.10 2.10 2.04 2	.00 2.04 2.04 2.00

**Primary OutFlow** Max=9.22 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater)

**2=Orifice/Grate** (Orifice Controls 0.74 cfs @ 11.06 fps)

-3=Orifice/Grate (Orifice Controls 0.30 cfs @ 6.19 fps)

-4=Sharp-Crested Rectangular Weir (Orifice Controls 8.17 cfs @ 4.19 fps)

-5=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=5.85 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater) -6=Broad-Crested Rectangular Weir (Weir Controls 5.85 cfs @ 1.41 fps)

## Summary for Pond POND 1.1: GRAVEL WETLAND 2

Inflow Are	ea =	3.614 ac, 3	0.92% Impervious, I	Inflow Depth > 3.21" for 10 Year event
Inflow	=	12.40 cfs @	12.12 hrs, Volume=	= 0.966 af
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	= 0.000 af, Atten= 100%, Lag= 0.0 min
Primary	=	0.00 cfs @	0.00 hrs, Volume=	= 0.000 af
Routed	d to Lir	nk LINK 1.0 : PE	MH203 TAILWATEF	२

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 54.11' @ 24.00 hrs Surf.Area= 14,115 sf Storage= 42,049 cf Flood Elev= 57.00' Surf.Area= 21,643 sf Storage= 94,743 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

Volume	Inve	ert Avai	il.Storag	ge Storage Descri	ption			
#1	47.5	5' 1	17,304	cf Custom Stage	e Data (Prismatic)Lis	ted below (Recalc)		
Elevatio	on	Surf.Area	Voids	Inc.Store	Cum.Store			
(100	56	(SQ-II) 6 260	( /0 )					
47.0		6,209	20.0	1 3 2 6	1 3 2 6			
49.0 50.4	50	6 269	45 O	4,320	4,320			
51 (		7 199	100.0	3 367	9 526			
52 (	0	9 187	100.0	8 193	17 719			
53.0	00	11.345	100.0	10,266	27,985			
54.0	00	13.814	100.0	12.580	40.565			
55.0	00	16,645	100.0	15,230	55,794			
56.0	00	19,805	100.0	18,225	74,019			
58.0	00	23,480	100.0	43,285	117,304			
Device	Routing	In	vert C	Dutlet Devices				
#1	Primarv	49	).85' <b>2</b>	4.0" Round Culve	ert			
	,		L	= 12.0' CPP, squa	are edge headwall, K	ke= 0.500		
			h	nlet / Outlet Invert=	49.85' / 49.45' S= 0	.0333 '/' Cc= 0.900		
			n	n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf				
#2	Device 1	49	9.85' <b>2.0" Vert. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads					
#3	Device 1	53	3.50' <b>4</b>	l.0' long x 2.00' ris	e Sharp-Crested Re	ctangular Weir		
			2	2 End Contraction(s	)			
#4	Device 1	56	56.50' 4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600					

Limited to weir flow at low heads

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=47.55' TW=55.07' (Dynamic Tailwater)

-2=Orifice/Grate (Controls 0.00 cfs)

-3=Sharp-Crested Rectangular Weir(Controls 0.00 cfs)

-4=Orifice/Grate (Controls 0.00 cfs)

## Summary for Pond POND 1.2: PDMH203

 Inflow Area =
 6.231 ac, 42.41% Impervious, Inflow Depth >
 1.73" for 10 Year event

 Inflow =
 11.94 cfs @
 12.09 hrs, Volume=
 0.897 af

 Outflow =
 11.94 cfs @
 12.09 hrs, Volume=
 0.897 af, Atten= 0%, Lag= 0.0 min

 Primary =
 11.94 cfs @
 12.09 hrs, Volume=
 0.897 af, Atten= 0%, Lag= 0.0 min

 Primary =
 11.94 cfs @
 12.09 hrs, Volume=
 0.897 af

 Routed to Reach REACH 1.0 : RESTORED HODGSON BROOK
 0.807 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 50.72' @ 12.09 hrs Flood Elev= 57.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.35'	<b>48.0" Round Culvert</b> L= 269.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 49.35' / 48.00' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 12.57 sf

Primary OutFlow Max=11.76 cfs @ 12.09 hrs HW=50.71' TW=48.76' (Dynamic Tailwater) -1=Culvert (Inlet Controls 11.76 cfs @ 3.13 fps)

### Summary for Pond POND 1.3: OUTLET CULVERTS

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=12) [62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.58' @ 23.95 hrs

Inflow Area	ı =	30.477 ac,	37.74% Imp	ervious,	Inflow	Depth >	2.3	4" for	10`	Yeare	event
Inflow	=	31.34 cfs @	12.51 hrs,	Volume	=	5.942	af				
Outflow	=	31.22 cfs @	12.53 hrs,	Volume	=	5.655	af,	Atten= (	)%,	Lag=	1.3 min
Primary	=	31.22 cfs @	12.53 hrs,	Volume	=	5.655	af				
Routed	to Link	PA1 : POIN	T OF ANALY	′SIS							
Secondary	=	0.00 cfs @	0.00 hrs,	Volume	=	0.000	af				
Routed	to Link	PA1 : POIN	T OF ANALY	′SIS							

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 38.77' @ 12.53 hrs Surf.Area= 8,870 sf Storage= 13,560 cf Flood Elev= 43.50' Surf.Area= 95,977 sf Storage= 236,017 cf

Plug-Flow detention time= 56.2 min calculated for 5.642 af (95% of inflow) Center-of-Mass det. time= 29.8 min ( 900.3 - 870.4 )

Prepare	ed by Tighe	& Bond Cor	sulting		Printed 3/1/2024
HydroCA	DR 10.20-4	o s/n 01453 ©	2023 HydroCAD	Software Solution	ns LLC Page 15
Volume	Inver	t Avail.Sto	rage Storage	Description	
#1	35.00	' 236,0	17 cf Custom	i Stage Data (Pr	ismatic)Listed below (Recalc)
Elevatio (fee	on S et)	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
35.0	00	960	0	0	
36.0 38.0	00	1,428 5,418	6,846	1,194 8,040	
40.0 42 (	00 00	14,354 66 884	19,772 81 238	27,812 109.050	
43.0	00	92,707	79,796	188,846	
43.5	50	95,977	47,171	236,017	
Device	Routing	Invert	Outlet Device	S	
#1	Primary	35.60'	<b>42.0" W x 29</b> L= 68.0' CM Inlet / Outlet I n= 0.025 Cor	<b>.0" H, R=21.5"/6</b> P, square edge h nvert= 35.60' / 3 rugated metal, 1	6.1" Pipe Arch CMP_Arch_1/2 42x29 X 3.00 neadwall, Ke= 0.500 5.30' S= 0.0044 '/' Cc= 0.900 Flow Area= 6.72 sf
#2	Secondary	/ 43.00'	<b>143.1 deg x</b> 1 Cv= 2.47 (C=	1 <b>8.0' long x 0.50</b> 3.09)	' rise Sharp-Crested Vee/Trap Weir

Type III 24-hr 10 Year Rainfall=5.58"

**Primary OutFlow** Max=31.11 cfs @ 12.53 hrs HW=38.77' TW=38.65' (Dynamic Tailwater) **1=CMP\_Arch\_1/2 42x29** (Outlet Controls 31.11 cfs @ 1.55 fps)

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Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=35.04' TW=38.65' (Dynamic Tailwater) 2=Sharp-Crested Vee/Trap Weir( Controls 0.00 cfs)

## Summary for Pond POND 1.4: SEDIMENT BASIN 1.0

Inflow Are	a =	7.248 ac,	0.42% Impervious,	Inflow Depth > 2.83" for 10 Year event
Inflow	=	18.77 cfs @	12.19 hrs, Volume	= 1.708 af
Outflow	=	0.68 cfs @	17.24 hrs, Volume	= 0.950 af, Atten= 96%, Lag= 303.1 min
Primary	=	0.68 cfs @	17.24 hrs, Volume	= 0.950 af
Routed	l to Pon	nd POND 1.3 :	OUTLET CULVERT	ſS
Secondary	y =	0.00 cfs @	0.00 hrs, Volume	= 0.000 af
Routed	l to Pon	nd POND 1.3 :	OUTLET CULVERT	ſS

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Starting Elev= 44.15' Surf.Area= 18,132 sf Storage= 11,702 cf Peak Elev= 45.79' @ 17.24 hrs Surf.Area= 29,244 sf Storage= 50,580 cf (38,878 cf above start) Flood Elev= 48.50' Surf.Area= 38,802 sf Storage= 127,441 cf (115,739 cf above start)

Plug-Flow detention time= 356.2 min calculated for 0.680 af (40% of inflow) Center-of-Mass det. time= 9.2 min ( 846.8 - 837.5 )

Volume	Invert	Avail.Storage	Storage Description
#1	43.00'	127,441 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

### L-0700-26 POST P2 Prepared by Tighe & Bond Consulting

Elevatio	on	Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
43.0	00	1,000	0	0	
44.(	00	17,117	9,059	9,059	
46.0	00	30,657	47,774	56,833	
47.0	00	35,879	33,268	90,101	
48.0	00	38,802	37,341	127,441	
Device	Routing	Invert	Outlet Device	S	
#1	Primary	42.75'	12.0" Round	Culvert L= 66.	0' Ke= 0.500
	•		Inlet / Outlet I	nvert= 42.75' / 42	2.40' S= 0.0053 '/' Cc= 0.900
			n= 0.013, Flo	w Area= 0.79 sf	
#2	Device 1	43.00'	4.0" Vert. Ori	fice/Grate C=	0.600 Limited to weir flow at low head
#3	Device 1	46.80'	10.0" x 17.5"	Horiz. Orifice/G	Grate C= 0.600
			Limited to wei	r flow at low hea	ds
#4	Seconda	rv 47.40'	Custom Weir	/Orifice. Cv= 2.	62 (C= 3.28)

Head (feet) 0.00 1.10 Width (feet) 8.00 14.60

Primary OutFlow Max=0.68 cfs @ 17.24 hrs HW=45.79' TW=38.65' (Dynamic Tailwater)

-1=Culvert (Passes 0.68 cfs of 5.16 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.68 cfs @ 7.80 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=44.15' TW=35.04' (Dynamic Tailwater) **4=Custom Weir/Orifice** (Controls 0.00 cfs)

### Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.1 by 7.52' @ 0.00 hrs (23.95 cfs 41.618 af) 3.614 ac, 30.92% Impervious, Inflow Depth = 0.00" for 10 Year event Inflow Area = Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Primary 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min = Routed to Pond POND 1.2 : PDMH203 Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 25	Point manual	elevation	table, To=	0.00 hrs,	dt= 1.00 hrs,	feet =		
55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07
55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07
55.07	55.07	55.07	55.07	55.07	55.07	55.07		

## Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.3 by 3.61' @ 0.00 hrs (92.51 cfs 60.023 af)

Inflow .	Area	a =	30.477 ac,	37.74% Imp	ervious,	Inflow	Depth >	2.2	23" for 10	) Year e	vent
Inflow		=	31.22 cfs @	) 12.53 hrs,	Volume	=	5.655	af			
Primar	y	=	31.22 cfs @	) 12.53 hrs,	Volume	=	5.655	af,	Atten= 0%	, Lag= (	0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 2 Point manual elevation table, To= 0.00 hrs, dt= 24.00 hrs, feet = 38.65 38.65

### Summary for Link PA2: POINT OF ANALYSIS

 Inflow Area =
 1.133 ac, 53.76% Impervious, Inflow Depth > 4.11" for 10 Year event

 Inflow =
 5.36 cfs @ 12.07 hrs, Volume=
 0.388 af

 Primary =
 5.36 cfs @ 12.07 hrs, Volume=
 0.388 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

L-0700-26 POST P2 Prepared by Tighe & Bond Consulting		Type III 24-h	r 25 Year Raint Printed	<i>all=7.07"</i> 3/1/2024
HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAL	D Software Solu	itions LLC		Page 18
Time span=0.00-24. Runoff by SCS TR-20 Reach routing by Dyn-Stor-Ind me	00 hrs, dt=0.05 method, UH=S thod - Pond r	5 hrs, 481 points SCS, Weighted-CN routing by Dyn-Sto	l r-Ind method	
SubcatchmentPOST 1.0: WATERSHED Run	off Area=440,33	32 sf 71.49% Impe	rvious Runoff Der	oth>5.88"
Flow Le	ength=933' Tc=	=11.4 min CN=90	Runoff=54.93 cfs	4.956 af
SubcatchmentPOST 1.1: WATERSHED Run	off Area=157,42	28 sf 30.92% Impe	rvious Runoff Der	oth>4.53"
Flow I	₋ength=464' To	c=8.3 min CN=78	Runoff=17.44 cfs	1.365 af
SubcatchmentPOST 1.2: WATERSHED Run	off Area=113,97	79 sf 58.28% Impe	rvious Runoff Der	oth>5.54"
Flow Le	ngth=1,191' To	c=6.4 min CN=87	Runoff=15.85 cfs	1.209 af
SubcatchmentPOST 1.3: WATERSHED Run	off Area=300,10	00 sf 23.27% Impe	rvious Runoff Dep	oth>4.50"
Flow Len	gth=1,525' Tc=	=45.9 min CN=78	Runoff=16.75 cfs	2.583 af
SubcatchmentPOST 1.4: WATERSHED1.4 Ru	noff Area=315,7	727 sf 0.42% Impe	rvious Runoff Dep	oth>4.09"
Flow Le	ength=585' Tc=	=13.5 min CN=74	Runoff=27.23 cfs	2.472 af
SubcatchmentPOST 2.0: WATERSHED2.0 Ru	noff Area=49,33	36 sf 53.76% Impe	rvious Runoff Dep	oth>5.54"
Flow	Length=758'	Tc=5.0 min CN=87	′ Runoff=7.12 cfs	0.523 af
Reach REACH 1.0: RESTORED         Avg. Fl           n=0.040         L=1,309.0'         St	ow Depth=0.87'	′ Max Vel=2.22 fps	Inflow=15.85 cfs	1.209 af
	=0.0092 '/' Cap	bacity=2,720.29 cfs	Outflow=8.65 cfs	1.202 af
Pond POND 1.0: GRAVEL WETLAND 1 Pe	ak Elev=47.10'	Storage=90,424 cf	Inflow=54.93 cfs	4.956 af
Primary=19.03 cfs 2.766 at	f Secondary=1	8.86 cfs  0.671 af	Outflow=37.88 cfs	3.437 af
Pond POND 1.1: GRAVEL WETLAND 2	ak Elev=55.22'	Storage=59,446 cf	Inflow=17.44 cfs Outflow=0.00 cfs	1.365 af 0.000 af
Pond POND 1.2: PDMH203	t n=0.013 L=26	Peak Elev=50.94	Inflow=15.85 cfs	1.209 af
48.0" Round Culver		69.0' S=0.0050 '/'	Outflow=15.85 cfs	1.209 af
Pond POND 1.3: OUTLET CULVERTS Perimary=56.26 cfs 7.985	eak Elev=39.17'	Storage=17,433 cf	Inflow=57.33 cfs	8.292 af
	af Secondary=	0.00 cfs 0.000 af	Outflow=56.26 cfs	7.985 af
Pond POND 1.4: SEDIMENT BASIN 1.0 Per	eak Elev=46.65'	Storage=77,792 cf	Inflow=27.23 cfs	2.472 af
Primary=0.78 cfs 1.070	) af Secondary	=0.00 cfs 0.000 af	Outflow=0.78 cfs	1.070 af
Link LINK 1.0: PDMH203 TAILWATER			Inflow=0.00 cfs Primary=0.00 cfs	0.000 af 0.000 af
Link PA1: POINT OF ANALYSIS			Inflow=56.26 cfs Primary=56.26 cfs	7.985 af 7.985 af
Link PA2: POINT OF ANALYSIS			Inflow=7.12 cfs Primary=7.12 cfs	0.523 af 0.523 af

Total Runoff Area = 31.609 acRunoff Volume = 13.108 afAverage Runoff Depth = 4.98"61.68% Pervious = 19.497 ac38.32% Impervious = 12.112 ac

L-0700-26 POST P2 Prepared by Tighe & Bond Consulting	Type III 24-h	r 50 Year Rainfall=8.46" Printed 3/1/2024
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Time span=0.00-24.00 hrs, d Runoff by SCS TR-20 method, Reach routing by Dyn-Stor-Ind method - F	t=0.05 hrs, 481 points UH=SCS, Weighted-CN rond routing by Dyn-Sto	N r-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=4	140,332 sf 71.49% Impe	rvious Runoff Depth>7.25"
Flow Length=933	3' Tc=11.4 min CN=90	Runoff=66.89 cfs 6.105 af
SubcatchmentPOST 1.1: WATERSHED Runoff Area=	157,428 sf 30.92% Impe	rvious Runoff Depth>5.81"
Flow Length=46	54' Tc=8.3 min CN=78	Runoff=22.21 cfs 1.750 af
SubcatchmentPOST 1.2: WATERSHED Runoff Area=	113,979 sf 58.28% Impe	rvious Runoff Depth>6.89"
Flow Length=1,19	91' Tc=6.4 min CN=87	Runoff=19.47 cfs 1.503 af
SubcatchmentPOST 1.3: WATERSHED Runoff Area=3	800,100 sf 23.27% Impe	rvious Runoff Depth>5.77"
Flow Length=1,525	5' Tc=45.9 min CN=78	Runoff=21.37 cfs 3.312 af
SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area	=315,727 sf 0.42% Impe	rvious Runoff Depth>5.33"
Flow Length=585	5' Tc=13.5 min CN=74	Runoff=35.32 cfs 3.218 af
SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area	=49,336 sf 53.76% Impe	rvious Runoff Depth>6.89"
Flow Length=7	758' Tc=5.0 min CN=87	′ Runoff=8.76 cfs 0.651 af
Reach REACH 1.0: RESTORED         Avg. Flow Depth           n=0.040         L=1,309.0'         S=0.0092 '/'	=0.92' Max Vel=2.24 fps Capacity=2,720.29 cfs	Inflow=19.47 cfs 1.503 af Outflow=11.76 cfs 1.495 af
Pond POND 1.0: GRAVEL WETLAND 1         Peak Elev=4           Primary=19.58 cfs         3.347 af         Second	17.39' Storage=96,897 cf ary=33.37 cfs  1.209 af	<sup>5</sup> Inflow=66.89 cfs 6.105 af Outflow=52.94 cfs 4.556 af
Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=	56.11' Storage=76,209 cf	Inflow=22.21 cfs 1.750 af Outflow=0.00 cfs 0.000 af
Pond POND 1.2: PDMH203	Peak Elev=51.13	' Inflow=19.47 cfs 1.503 af
48.0" Round Culvert n=0.013	L=269.0' S=0.0050 '/'	Outflow=19.47 cfs 1.503 af
Pond POND 1.3: OUTLET CULVERTS Peak Elev=39	9.58' Storage=22,150 cf	Inflow=76.91 cfs 10.982 af
Primary=74.09 cfs 10.655 af Second	ary=0.00 cfs  0.000 af  C	0utflow=74.09 cfs 10.655 af
Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=4	17.02' Storage=90,878 cf	Inflow=35.32 cfs 3.218 af
Primary=2.39 cfs 1.619 af Seco	ndary=0.00 cfs 0.000 af	Outflow=2.39 cfs 1.619 af
Link LINK 1.0: PDMH203 TAILWATER		Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Link PA1: POINT OF ANALYSIS	F	Inflow=74.09 cfs 10.655 af Primary=74.09 cfs 10.655 af
Link PA2: POINT OF ANALYSIS		Inflow=8.76 cfs 0.651 af Primary=8.76 cfs 0.651 af

Total Runoff Area = 31.609 acRunoff Volume = 16.539 afAverage Runoff Depth = 6.28"61.68% Pervious = 19.497 ac38.32% Impervious = 12.112 ac

**Master Post-Development Calculations** 





# Area Listing (all nodes)

A	Area	CN	Description
(ac	res)		(subcatchment-numbers)
1.	.776	61	>75% Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3,
			POST 1.4)
6.	.801	74	>75% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3,
			POST 1.4, POST 2.0)
0.	.436	80	>75% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4)
0.	.323	58	Meadow, non-grazed, HSG B (POST 1.3)
3.	.143	71	Meadow, non-grazed, HSG C (POST 1.3)
0.	.799	98	Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4)
7.	.546	98	Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4,
			POST 2.0)
0.	.146	98	Paved parking, HSG D (POST 1.0, POST 1.3, POST 1.4)
0.	.688	98	Roofs, HSG B (POST 1.0, POST 1.1, POST 1.4)
8.	.166	98	Roofs, HSG C (POST 1.0, POST 1.1, POST 1.4, POST 2.0)
1.	.737	98	Roofs, HSG D (POST 1.0, POST 1.4)
0.	.049	76	Woods/grass comb., Fair, HSG C (POST 1.3)
31	.609	87	TOTAL AREA

# Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
3.586	HSG B	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4
25.705	HSG C	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0
2.318	HSG D	POST 1.0, POST 1.3, POST 1.4
0.000	Other	
31.609		TOTAL AREA

L-0700-26 POST	Type III 24-hr 2 Year Rainfall=3.68"
Prepared by Tighe & Bond	Printed 6/6/2023
HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions	LLC Page 4
Time span=0.00-24.00 hrs, dt=0.05 hrs,	, 481 points
Runoff by SCS TR-20 method, UH=SCS,	Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing	g by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=462,599 sf	72.19% Impervious Runoff Depth>2.71"
Flow Length=933' Tc=11.4	min CN=91 Runoff=27.46 cfs 2.396 af
SubcatchmentPOST 1.1: WATERSHED Runoff Area=242,496 sf	58.73% Impervious Runoff Depth>2.25"
Flow Length=750' Tc=10.3	min CN=86 Runoff=12.60 cfs 1.046 af
SubcatchmentPOST 1.2: WATERSHED Runoff Area=101,204 sf	62.15% Impervious Runoff Depth>2.43"
Flow Length=1,191' Tc=6.	4 min CN=88 Runoff=6.37 cfs 0.471 af
SubcatchmentPOST 1.3: WATERSHED Runoff Area=306,549 sf	22.64% Impervious Runoff Depth>1.55"
Flow Length=1,525' Tc=45.9	9 min CN=77 Runoff=5.81 cfs 0.908 af
SubcatchmentPOST 1.4: WATERSHED Runoff Area=214,764 sf	85.05% Impervious Runoff Depth>3.01"
Flow Length=717' Tc=7.5	min CN=94 Runoff=15.51 cfs 1.236 af
SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,290 sf	80.99% Impervious Runoff Depth>2.91"
Flow Length=758' Tc=5.	0 min CN=93 Runoff=3.72 cfs 0.274 af
Reach REACH 1.0: RESTORED         Avg. Flow Depth=0.60'         Ma           n=0.040         L=1,309.0'         S=0.0092 '/'         Capacity:	ax Vel=2.03 fps Inflow=6.37 cfs 0.617 af =2,720.29 cfs Outflow=4.54 cfs 0.608 af
Pond POND 1.0: GRAVEL WETLAND1Peak Elev=46.16' StoraPrimary=1.57 cfs1.041 afSecondary=0.00	age=70,734 cf Inflow=27.46 cfs 2.396 af cfs 0.000 af Outflow=1.57 cfs 1.041 af
Pond POND 1.1: GRAVEL WETLAND2       Peak Elev=53.90'       Storage	age=39,230 cf Inflow=12.60 cfs 1.046 af Outflow=0.40 cfs 0.146 af
Pond POND 1.2: PDMH203 Per 48.0" Round Culvert n=0.013 L=269.0	eak Elev=50.33' Inflow=6.37 cfs 0.617 af ' S=0.0050 '/' Outflow=6.37 cfs 0.617 af
Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' St	orage=8,984 cf Inflow=9.25 cfs 3.255 af
Primary=9.41 cfs 3.050 af Secondary=0.00	cfs 0.000 af Outflow=9.41 cfs 3.050 af
Pond POND 1.4: RAINGARDEN1.0Peak Elev=47.27' StoraPrimary=1.31 cfs0.699 afSecondary=0.00	age=34,235 cf Inflow=15.51 cfs 1.236 af cfs 0.000 af Outflow=1.31 cfs 0.699 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=0.40 cfs 0.146 af Primary=0.40 cfs 0.146 af
Link PA1: POINT OF ANALYSIS	Inflow=9.41 cfs 3.050 af Primary=9.41 cfs 3.050 af
Link PA2: POINT OF ANALYSIS	Inflow=3.72 cfs 0.274 af Primary=3.72 cfs 0.274 af

Total Runoff Area = 31.609 acRunoff Volume = 6.331 afAverage Runoff Depth = 2.40"39.63% Pervious = 12.527 ac60.37% Impervious = 19.083 ac
L-0700-26 POST	Type III 24-hr 10 Year Rainfall	l=5.58"
HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solution:	s LLC	0/2023 Page 5
Time span=0.00-24.00 hrs, dt=0.05 hr Runoff by SCS TR-20 method, UH=SCS Reach routing by Dyn-Stor-Ind method - Pond routi	s, 481 points , Weighted-CN ng by Dyn-Stor-Ind method	
SubcatchmentPOST 1.0: WATERSHED Runoff Area=462,599 sf Flow Length=933' Tc=11.	<sup>:</sup> 72.19% Impervious Runoff Depth 4 min CN=91 Runoff=44.88 cfs 4.	>4.54" 017 af
SubcatchmentPOST 1.1: WATERSHED Runoff Area=242,496 sf Flow Length=750' Tc=10.	<sup>5</sup> 58.73% Impervious Runoff Depth 3 min CN=86 Runoff=22.02 cfs 1.	>4.01" 858 af
SubcatchmentPOST 1.2: WATERSHED Runoff Area=101,204 sf Flow Length=1,191' Tc=6.	62.15% Impervious Runoff Depth 4 min CN=88 Runoff=10.81 cfs 0.	>4.22" 817 af
SubcatchmentPOST 1.3: WATERSHED Runoff Area=306,549 sf Flow Length=1,525' Tc=45.	22.64% Impervious Runoff Depth 9 min CN=77 Runoff=11.76 cfs 1.	>3.09" 810 af
SubcatchmentPOST 1.4: WATERSHED Runoff Area=214,764 sf Flow Length=717' Tc=7.	85.05% Impervious Runoff Depth 5 min CN=94 Runoff=24.45 cfs 2.	>4.88" 004 af
SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,290 sf Flow Length=758' Tc=5	<sup>:</sup> 80.99% Impervious Runoff Depth 5.0 min CN=93 Runoff=5.94 cfs 0.	>4.77" 449 af
Reach REACH 1.0: RESTORED         Avg. Flow Depth=0.81'         Mag. No.040           n=0.040         L=1,309.0'         S=0.0092 '/'         Capacit	ax Vel=2.20 fps Inflow=10.81 cfs 1. y=2,720.29 cfs Outflow=6.07 cfs 1.	.367 af 355 af
Pond POND 1.0: GRAVEL WETLAND1Peak Elev=46.94' StoPrimary=7.09 cfs2.106 afSecondary=11.63	orage=86,832 cf Inflow=44.88 cfs 4. 3 cfs 0.435 af Outflow=18.72 cfs 2.	.017 af 541 af
Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=55.08' Sto	orage=57,197 cf Inflow=22.02 cfs 1. Outflow=1.76 cfs 0.	.858 af .550 af
Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=269.0	eak Elev=50.65' Inflow=10.81 cfs 1. ' S=0.0050 '/' Outflow=10.81 cfs 1.	.367 af .367 af
Pond POND 1.3: OUTLET CULVERTSPeak Elev=38.86'StorePrimary=39.92 cfs6.819 afSecondary=0.00	orage=14,364 cf Inflow=40.12 cfs 7. ) cfs 0.000 af Outflow=39.92 cfs 6.	.107 af 819 af
Pond POND 1.4: RAINGARDEN1.0Peak Elev=48.07' StoPrimary=6.60 cfs1.401 afSecondary=0.0	orage=45,635 cf Inflow=24.45 cfs 2. 00 cfs 0.000 af Outflow=6.60 cfs 1.	.004 af 401 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=1.76 cfs 0 Primary=1.76 cfs 0	.550 af .550 af
Link PA1: POINT OF ANALYSIS	Inflow=39.92 cfs 6 Primary=39.92 cfs 6	.819 af .819 af
Link PA2: POINT OF ANALYSIS	Inflow=5.94 cfs 0 Primary=5.94 cfs 0	.449 af .449 af

Total Runoff Area = 31.609 acRunoff Volume = 10.955 afAverage Runoff Depth = 4.16"39.63% Pervious = 12.527 ac60.37% Impervious = 19.083 ac

### Summary for Subcatchment POST 1.0: WATERSHED 1.0

Runoff = 44.88 cfs @ 12.15 hrs, Volume= 4.017 af, Depth> 4.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN D	escription						
	5,235	98 R	oofs, HSC	βB					
	22,410	61 >	61 >75% Grass cover, Good, HSG B						
	19,146	98 P	aved park	ing, HSG B					
1	57,967	98 R	oofs, HSC	δČ					
	90,117	74 >	75% Gras	s cover, Go	ood, HSG C				
1	14,873	98 P	aved park	ing, HSG C					
	31,357	98 R	oofs, HSG	6 D					
	16,138	80 >	75% Gras	s cover, Go	ood, HSG D				
	5,356	98 P	aved park	ing, HSG D					
4	62,599	91 V	/eighted A	verage					
1	28,665	2	7.81% Per	vious Area					
3	33,934	7	2.19% Imp	pervious Ar	ea				
Та	Longth	Clana	Valacity	Consoitu	Description				
IC (min)	(foot)			Capacity	Description				
				(015)					
1.1	70	0.0150	0.15		Sheet Flow,				
0.0	20	0 0 0 0 0 0	0.07		Grass: Short n= 0.150 PZ= 3.08				
0.2	32	0.0200	2.07		Shallow Concentrated Flow,				
0.1	10	0 0 0 0 0 0	0 10		Paveu RV-20.5 lps Shallow Concentrated Flow				
0.1	19	0.0200	2.12		Grassed Waterway, Ky= 15.0 fpc				
0.8	162	0 0050	3 21	2 52	Dina Channel				
0.0	102	0.0000	0.21	2.02	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
					n=0.013 Corrugated PE smooth interior				
04	84	0 0050	3 21	2 52	Pine Channel				
0.4	04	0.0000	0.21	2.02	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
					n=0.013				
0.5	113	0.0050	3.72	4.57	Pipe Channel.				
			•=		15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'				
					n= 0.013				
1.2	299	0.0050	4.20	7.43	Pipe Channel.				
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'				
					n= 0.013				
0.4	94	0.0050	4.20	7.43	Pipe Channel,				
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'				
					n= 0.013				
0.1	46	0.0240	11.16	35.05	Pipe Channel,				
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'				
					n= 0.013				
0.0	5	0.0800	7.16	0.98	Pipe Channel,				
					5.0" Round Area= 0.1 sf Perim= 1.3' r= 0.10'				
					n= 0.013				
0.0	9	0.0110	9.90	69.95	Pipe Channel,				

36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'

11.4 933 Total

#### Summary for Subcatchment POST 1.1: WATERSHED 1.1

n= 0.013

Runoff = 22.02 cfs @ 12.14 hrs, Volume= 1.858 af, Depth> 4.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN I	Description					
	13,692	98 I	Roofs, HSG B					
	32,710	61 >	>75% Gras	s cover, Go	ood, HSG B			
	2,729	98 I	Paved park	ing, HSG B				
	88,019	98 I	Roofs, HSC	G C				
	67,375	74 >	>75% Gras	s cover, Go	ood, HSG C			
	37,971	98 I	Paved park	ing, HSG C				
2	42,496	86 \	Neighted A	verage				
1	00,085	4	11.27% Pei	rvious Area				
1	42,411	Ę	58.73% Imp	pervious Are	ea			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
7.1	100	0.0380	0.24		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.68"			
1.2	163	0.0245	2.35		Shallow Concentrated Flow,			
					Grassed Waterway Kv= 15.0 fps			
1.5	283	0.0050	3.21	2.52	Pipe Channel,			
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
					n= 0.013			
0.1	81	0.0240	9.21	16.27	Pipe Channel,			
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'			
					n= 0.013			
0.4	123	0.0050	5.09	16.00	Pipe Channel,			
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'			
					n= 0.013			
10.3	750	Total						

#### Summary for Subcatchment POST 1.2: WATERSHED 1.2

Runoff = 10.81 cfs @ 12.09 hrs, Volume= 0.817 af, Depth> 4.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58" L-0700-26 POST

 Type III 24-hr
 10 Year Rainfall=5.58"

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_	A	rea (sf)	CN D	escription							
		6,874	61 >	61 >75% Grass cover, Good, HSG B							
		4,785	98 P	aved park	ing, HSG B						
		31,436	74 >	75% Gras	s cover, Go	ood, HSG C					
_		58,109	<u>98</u> P	aved park	ing, HSG C	,					
	1	01,204	88 V	Veighted A	verage						
		38,310	3	7.85% Per	vious Area						
		62,894	6	2.15% Imp	pervious Ar	ea					
	-		<u></u>		<b>•</b> ••						
		Length	Slope	Velocity	Capacity	Description					
_	(min)		(11/11)	(ft/sec)	(CIS)						
	1.5	100	0.0100	1.12		Sheet Flow,					
	10	152	0.0150	2 40		Shallow Concentrated Flow					
	1.0	100	0.0150	2.49		Payed Ky= 20.3 fps					
	16	343	0 0050	3 4 7	2 73	Pine Channel					
	1.0	040	0.0000	0.47	2.70	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'					
						n= 0.012 Concrete pipe, finished					
	0.1	13	0.0050	3.72	4.57	Pipe Channel.					
				•		15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'					
						n= 0.013 Corrugated PE, smooth interior					
	1.8	453	0.0050	4.20	7.43	Pipe Channel,					
						18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'					
						n= 0.013 Corrugated PE, smooth interior					
	0.4	129	0.0050	5.91	29.00	Pipe Channel,					
						30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63'					
_						n= 0.013 Corrugated PE, smooth interior					
	~ 1	4 4 0 4	<b>T</b> ( )								

6.4 1,191 Total

### Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 11.76 cfs @ 12.63 hrs, Volume= 1.810 af, Depth> 3.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
11,450	61	>75% Grass cover, Good, HSG B
14,068	58	Meadow, non-grazed, HSG B
908	98	Paved parking, HSG B
70,956	74	>75% Grass cover, Good, HSG C
136,905	71	Meadow, non-grazed, HSG C
2,120	76	Woods/grass comb., Fair, HSG C
68,005	98	Paved parking, HSG C
1,638	80	>75% Grass cover, Good, HSG D
499	98	Paved parking, HSG D
306,549	77	Weighted Average
237,137		77.36% Pervious Area
69,412		22.64% Impervious Area

#### L-0700-26 POST Prepared by Tighe & Bond

 Type III 24-hr
 10 Year Rainfall=5.58"

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	•		0		-	_		-	-

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.9	100	0.0130	0.15		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.68"
1.1	52	0.0130	0.80		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.1	27	0.2720	7.82		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
33.8	1,346	0.0090	0.66		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps

45.9 1,525 Total

### Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff = 24.45 cfs @ 12.10 hrs, Volume= 2.004 af, Depth> 4.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN	Description		
	11,051	98	Roofs, HSC	ЭB	
	3,902	61	>75% Gras	s cover, Go	ood, HSG B
	7,241	98	Paved park	ing, HSG B	
	86,748	98	Roofs, HSC	ΞČ	
	26,995	74	>75% Gras	s cover, Go	ood, HSG C
	32,822	98	Paved park	ing, HSG C	
	44,300	98	Roofs, HSC	GD	
	1,206	80	>75% Gras	s cover, Go	ood, HSG D
	499	98	Paved park	ing, HSG D	
2	14,764	94	Weighted A	verage	
	32,103		14.95% Pe	rvious Area	
1	82,661		85.05% Imp	pervious Are	ea
Тс	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
4.9	40	0.0150	0.14		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.68"
0.3	53	0.0200	2.87		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
0.3	65	0.0050	3.21	2.52	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013 Corrugated PE, smooth interior
0.4	115	0.0100	) 4.54	3.56	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013
0.7	140	0.0050	) 3.21	2.52	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013
0.9	275	0.0070	) 4.97	8.79	Pipe Channel,
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
					n= 0.013

L-0700	-26 POS	ST			Type III 24-hr 10 Year Rainfall=5.58'
Prepare	d by Tig	he & Bor	nd		Printed 6/6/2023
HydroCA	<u>D® 10.00</u>	-20 s/n 03	436 © 201	17 HydroCA	D Software Solutions LLC Page 10
0.0	29	0.0550	13.94	24.63	<b>Pipe Channel,</b> 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
7.5	717	Total			
		Summ	ary for S	Subcatch	ment POST 2.0: WATERSHED 2.0
[49] Hint	: Tc<2dt	may requi	ire smaller	r dt	
Runoff	=	5.94 cfs	s@ 12.0	7 hrs, Volu	me= 0.449 af, Depth> 4.77"
Runoff b Type III :	y SCS TF 24-hr 10	R-20 meth Year Rai	nod, UH=S nfall=5.58'	SCS, Weigh "	ted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Α	rea (sf)	CN D	escription		
	22,995	98 R	oofs, HSO	ЭC	
	9,368 16,927	74 > 98 P	75% Gras aved park	s cover, Go ing, HSG C	ood, HSG C
	49,290 9,368 39,922	93 W 19 80	/eighted A 9.01% Per 0.99% Imp	verage rvious Area pervious Are	ea
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.2	100	0.0164	1.36		Sheet Flow,
0.3	48	0.0164	2.60		Smooth surfaces n= 0.011 P2= 3.68" <b>Shallow Concentrated Flow,</b> Paved Ky= 20.3 fps
0.3	130	0.0140	7.03	12.43	<b>Pipe Channel,</b> 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
0.5	70	0.0250	2.37		Shallow Concentrated Flow, Grassed Waterway Ky= 15.0 fps
1.3	410	0.0050	5.09	16.00	<b>Pipe Channel,</b> 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
3.6	758	Total, Ir	ncreased t	o minimum	Tc = 5.0 min

# Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

Inflow Are	ea =	7.890 ac, 5	9.73% Impervious,	Inflow Depth >	2.08"	for 10 Y	ear event	
Inflow	=	10.81 cfs @	12.09 hrs, Volume	e 1.367	af			
Outflow	=	6.07 cfs @	12.81 hrs, Volume	e 1.355	af, Atte	n= 44%,	Lag= 42.9 m	in

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Max. Velocity= 2.20 fps, Min. Travel Time= 9.9 min Avg. Velocity = 1.04 fps, Avg. Travel Time= 21.0 min

#### L-0700-26 POST Type III 24-hr 10 Year Rainfall=5.58" Printed 6/6/2023 Prepared by Tighe & Bond HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC

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Peak Storage= 6,364 cf @ 12.27 hrs Average Depth at Peak Storage= 0.81' Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs

Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals) Constant n= 0.040 Winding stream, pools & shoals Inlet Invert= 48.00', Outlet Invert= 36.00'

‡

6.75

	Offset	Elevat	ion	Cha	n.Depth		
	(feet)	(fe	et)		(feet)		
	0.00	12	.00		0.00		
	18.00	6	.00		6.00		
	30.25	6	.00		6.00		
	31.75	5	.25		6.75		
	34.25	5	.25		6.75		
	35.75	6	.00		6.00		
	48.00	6	.00		6.00		
	66.00	12	.00		0.00		
De	pth En	ld Area	Pe	rim.		Storage	Discharge
(fe	et)	(sq-ft)	(f	eet)	(cut	bic-feet)	(cfs)
0	.00	0.0		2.5		0	0.00
0	.75	3.0	3	30.4		3,927	2.28

68.3

#### Summary for Pond POND 1.0: GRAVEL WETLAND 1

2.720.29

[95] Warning: Outlet Device #4 rise exceeded

291.0

Inflow Area =	10.620 ac, 72.19% Impervious	s, Inflow Depth > 4.54" for 10 Year event
Inflow =	44.88 cfs @ 12.15 hrs, Volum	ne= 4.017 af
Outflow =	18.72 cfs @ 12.45 hrs, Volum	ne= 2.541 af, Atten= 58%, Lag= 18.0 min
Primary =	7.09 cfs @ 12.45 hrs, Volum	ne= 2.106 af
Secondary =	11.63 cfs @ 12.45 hrs, Volum	ne= 0.435 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 46.94' @ 12.45 hrs Surf.Area= 21,544 sf Storage= 86,832 cf Flood Elev= 48.00' Surf.Area= 23,557 sf Storage= 110,845 cf

380.919

Plug-Flow detention time= 216.6 min calculated for 2.536 af (63% of inflow) Center-of-Mass det. time= 118.8 min (906.1 - 787.3)

#### L-0700-26 POST

Prepared by Tighe & Bond

 Type III 24-hr
 10 Year Rainfall=5.58"

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Volume	Inver	t Ava	il.Stora	ge Storage Descri	ption						
#1	39.05	' 1	10,845	cf Custom Stage	Data (Prismatic)	isted below (Recalc)					
Elevatio (fee	on S et)	urf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)						
39.0	)5	9.855	0.0	0	0						
41.3	35	9,855	30.0	6,800	6,800						
42.0	00	9,855	45.0	2,883	9,683						
43.0	00	11,943	100.0	10,899	20,582						
44.(	00	14,202 100		13,073	33,654						
45.0	00	16,891	100.0	15,547	49,201						
46.0	00	19,752	100.0	18,322	67,522						
47.0	00	21,668	100.0	20,710	88,232						
48.0	00	23,557	100.0	22,613	110,845						
Device	Routing	In	vert (	Dutlet Devices							
#1	Primary	41	.35' 1	8.0" Round Culve	ert						
	-		L	.= 30.0' CPP, squa	are edge headwall,	Ke= 0.500					
			1	nlet / Outlet Invert=	41.35'/41.20' S=	: 0.0050 '/' Cc= 0.900					
			r	n= 0.013 Corrugate	d PE, smooth interi	ior, Flow Area= 1.77 sf					
#2	Device 1	41	.35' 3	3.5" Vert. Orifice/G	rate C= 0.600						
#3	Device 1	45	5.00' 3	3.0" Vert. Orifice/G	rate C= 0.600						
#4	Device 1	46	5.00' <b>3</b>	3.0' long x 0.50' ris	e Sharp-Crested F	Rectangular Weir					
			2	2 End Contraction(s)	) 4.0' Crest Height	t					
#5	Device 1	47	'.00' <b>4</b>	.0" x 4.0" Horiz. O	rifice/Grate X 106	<b>.00</b> C= 0.600					
			L	imited to weir flow a	at low heads						
#6	Secondary	y 46	6.50' <b>1</b>	5.0' long x 15.0' b	readth Broad-Cre	sted Rectangular Weir					
			F	lead (feet) $0.20$ 0.	40 0.60 0.80 1.00	) 1.20 1.40 1.60					
			C	Coef. (English) 2.68	3 2.70 2.70 2.64	2.63 2.64 2.64 2.63					
Primary 1=Cu -1=Cu -3= -3= -5=	Primary OutFlow Max=7.09 cfs @ 12.45 hrs HW=46.93' TW=38.85' (Dynamic Tailwater) 1=Culvert (Passes 7.09 cfs of 18.71 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.75 cfs @ 11.23 fps) 3=Orifice/Grate (Orifice Controls 0.32 cfs @ 6.48 fps) 4=Sharp-Crested Rectangular Weir(Orifice Controls 6.02 cfs @ 4.15 fps) 5=Orifice/Grate (Controls 0.00 cfs)										
Second	ary OutFlo	w May=1	1 50 cf	= 0.12.45  hrs  HW=	-16 93' TW=38 85'	(Dynamic Tailwater)					

Secondary OutFlow Max=11.59 cfs @ 12.45 hrs HW=46.93' TW=38.85' (Dynamic Tailwater) G=Broad-Crested Rectangular Weir (Weir Controls 11.59 cfs @ 1.78 fps)

# Summary for Pond POND 1.1: GRAVEL WETLAND 2

Inflow Are	ea =	5.567 ac, 5	8.73% Impervious,	Inflow Depth > 4	1.01" for	10 Year event
Inflow	=	22.02 cfs @	12.14 hrs, Volume	= 1.858 at	f	
Outflow	=	1.76 cfs @	13.65 hrs, Volume	= 0.550 at	f, Atten= 9	2%, Lag= 90.5 min
Primary	=	1.76 cfs @	13.65 hrs, Volume	= 0.550 at	f	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 55.08' @ 13.65 hrs Surf.Area= 16,909 sf Storage= 57,197 cf Flood Elev= 57.00' Surf.Area= 21,643 sf Storage= 94,743 cf

# L-0700-26 POST

 Type III 24-hr
 10 Year Rainfall=5.58"

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Plug-Flow detention time= 357.2 min calculated for 0.550 af (30% of inflow) Center-of-Mass det. time= 218.3 min (1,021.7 - 803.4)

Volume	Inver	t Avail.	Storage	Storage Descrip	ion	
#1	47.55	' 11	7,304 cf	Custom Stage	Data (Prismatic)Listed below (F	Recalc)
Elevatio (feet	n S t)	urf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
47.5	5	6.269	0.0	0	0	
49.8	5	6,269	30.0	4,326	4,326	
50.5	0	6,269	45.0	1,834	6,159	
51.0	0	7,199	100.0	3,367	9,526	
52.0	0	9,187	100.0	8,193	17,719	
53.0	0	11,345	100.0	10,266	27,985	
54.0	0	13,814	100.0	12,580	40,565	
55.0	0	16,645	100.0	15,230	55,794	
56.0	0	19,805	100.0	18,225	74,019	
58.0	0	23,480	100.0	43,285	117,304	
Device	Routing	Inv	ert Out	let Devices		
#1	Primary	49.	85' <b>24.(</b>	)" Round Culver		
	5		L= '	12.0' CPP, squar	e edge headwall, Ke= 0.500	
			Inle	t / Outlet Invert= 4	9.85 <sup>'</sup> / 49.45'   S= 0.0333 '/'   Co	c= 0.900
			n= (	0.013 Corrugated	PE, smooth interior, Flow Area	i= 3.14 sf
#2	Device 1	49.	85' <b>2.0'</b>	Vert. Orifice/Gra	<b>te</b> C= 0.600	
#3	Device 1	53.	50' <b>4.0'</b>	long x 2.00' rise	Sharp-Crested Rectangular W	Veir
			2 E	nd Contraction(s)		
#4	Device 1	56.	50' <b>4.0'</b>	' x 4.0" Horiz. Ori	fice/Grate X 106.00 C= 0.600	
			Lim	ited to weir flow at	low heads	
Primary 1=Cu 1-2=	OutFlow M Ivert (Inlet Orifice/Gra	Max=1.76 ( Controls 1 ate (Passe	cfs @ 13. .76 cfs @ s < 0.01	65 hrs HW=55.08 0.56 fps) cfs potential flow)	' TW=55.07' (Dynamic Tailwa	ater)
-3=	Sharp-Cre	sted Rect	angular	Weir(Passes < 3.3	3 cfs potential flow)	
<u>     4</u> =	Orifice/Gra	ate (Contr	OIS U.UU	CIS)		
		5	Summa	ry for Pond PO	ND 1.2: PDMH203	
Inflow Ar	ea =	7.890 ac.	59.73%	Impervious. Inflov	/ Depth > 2.08" for 10 Year	event
Inflow	= 10	0.81 cfs @	12.09	nrs, Volume=	1.367 af	
Outflow	= 1	0.81 cfs @	12.09	nrs, Volume=	1.367 af, Atten= 0%, Lao	= 0.0 min
Primary	= 1	0.81 cfs @	12.09	nrs, Volume=	1.367 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 50.65' @ 12.09 hrs Flood Elev= 57.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.35'	<b>48.0" Round Culvert</b> L= 269.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 49.35' / 48.00' S= 0.0050 '/' Cc= 0.900

n= 0.013 Corrugated PE, smooth interior, Flow Area= 12.57 sf

Primary OutFlow Max=10.64 cfs @ 12.09 hrs HW=50.64' TW=48.75' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 10.64 cfs @ 3.05 fps)

#### Summary for Pond POND 1.3: OUTLET CULVERTS

[62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.50' @ 23.95 hrs

Inflow Area	=	30.478 ac, 5	9.60% Imp	ervious,	Inflow D	epth >	2.80	)" for 1	0 Year	event
Inflow	=	40.12 cfs @	12.47 hrs,	Volume	=	7.107	af			
Outflow	=	39.92 cfs @	12.50 hrs,	Volume	=	6.819	af, A	Atten= 0%	5, Lag=	: 1.8 min
Primary	=	39.92 cfs @	12.50 hrs,	Volume	=	6.819	af		-	
Secondary	=	0.00 cfs @	0.00 hrs,	Volume	=	0.000	af			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 38.86' @ 12.50 hrs Surf.Area= 9,266 sf Storage= 14,364 cf Flood Elev= 43.50' Surf.Area= 95,977 sf Storage= 236,017 cf

Plug-Flow detention time= 32.3 min calculated for 6.819 af (96% of inflow) Center-of-Mass det. time= 11.6 min (905.1 - 893.5)

Invert	Avail.Sto	rage Storage	Description	
35.00'	236,02	17 cf Custom	Stage Data (Pri	ismatic)Listed below (Recalc)
Su	urf.Area	Inc.Store	Cum.Store	
	(sq-ft)	(cubic-feet)	(cubic-feet)	
	960	0	0	
	1,428	1,194	1,194	
	5,418	6,846	8,040	
	14,354	19,772	27,812	
	66,884	81,238	109,050	
	92,707	79,796	188,846	
	95,977	47,171	236,017	
outing	Invert	Outlet Device	S	
rimary econdary	35.60' 43.00'	<b>42.0" W x 29</b> L= 68.0' CM Inlet / Outlet I n= 0.025 Cor <b>143.1 deg x 1</b> Cv= 2.47 (C=	.0" H, R=21.5"/6 P, square edge h nvert= 35.60' / 35 rugated metal, F I8.0' long x 0.50 3.09)	6.1" Pipe Arch CMP_Arch_1/2 42x29 X 3.00 eadwall, Ke= 0.500 5.30' S= 0.0044 '/' Cc= 0.900 Flow Area= 6.72 sf ' rise Sharp-Crested Vee/Trap Weir
	<u>outing</u> rimary	Invert         Avail.Stor           35.00'         236,01           Surf.Area (sq-ft)         960           1,428         5,418           14,354         66,884           92,707         95,977           outing         Invert           rimary         35.60'           econdary         43.00'	$\begin{tabular}{ c c c c c c } \hline Invert & Avail.Storage & Storage \\ \hline 35.00' & 236,017 cf & Custom \\ \hline Surf.Area & Inc.Store \\ (sq-ft) & (cubic-feet) \\ \hline 960 & 0 \\ 1,428 & 1,194 \\ 5,418 & 6,846 \\ 14,354 & 19,772 \\ 66,884 & 81,238 \\ 92,707 & 79,796 \\ 95,977 & 47,171 \\ \hline outing & Invert & Outlet Device \\ rimary & 35.60' & 42.0" W x 29 \\ L= 68.0' & CM \\ Inlet / Outlet I \\ n= 0.025 & Cor \\ econdary & 43.00' & 143.1 & deg x 1 \\ Cv= 2.47 & (C= 0, 10, 10, 10, 10, 10, 10, 10, 10, 10, $	Invert         Avail.Storage         Storage Description $35.00'$ $236,017$ cf         Custom Stage Data (Pridicipal Constraints)           Surf.Area         Inc.Store         Cum.Store $(sq-ft)$ (cubic-feet)         (cubic-feet) $960$ 0         0 $1,428$ $1,194$ $1,194$ $5,418$ $6,846$ $8,040$ $14,354$ $19,772$ $27,812$ $66,884$ $81,238$ $109,050$ $92,707$ $79,796$ $188,846$ $95,977$ $47,171$ $236,017$ outing         Invert         Outlet Devices           rimary $35.60'$ $42.0"$ W x $29.0"$ H, $R=21.5"/6$ L= $68.0'$ CMP, square edge h         Inlet / Outlet Invert= $35.60'$ / $38$ $n= 0.025$ Corrugated metal, F $n= 0.025$ Corrugated metal, F $n= 0.025$ Corrugated metal, F $2.47$ (C= $3.09$ )

**Primary OutFlow** Max=39.88 cfs @ 12.50 hrs HW=38.86' TW=38.65' (Dynamic Tailwater) **1=CMP\_Arch\_1/2 42x29** (Outlet Controls 39.88 cfs @ 1.98 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=35.00' TW=38.65' (Dynamic Tailwater) 2=Sharp-Crested Vee/Trap Weir( Controls 0.00 cfs)

#### Summary for Pond POND 1.4: RAINGARDEN 1.0

Inflow Area	=	4.930 ac, 8	35.05% Imp	ervious,	Inflow Depth >	4.88"	for 10 Y	ear event
Inflow =	=	24.45 cfs @	12.10 hrs,	Volume=	= 2.004	af		
Outflow =	=	6.60 cfs @	12.48 hrs,	Volume=	= 1.401	af, Atte	en= 73%,	Lag= 22.2 min
Primary =	=	6.60 cfs @	12.48 hrs,	Volume=	= 1.401	af		
Secondary =	-	0.00 cfs @	0.00 hrs,	Volume=	= 0.000	af		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 48.07' @ 12.48 hrs Surf.Area= 14,774 sf Storage= 45,635 cf Flood Elev= 50.00' Surf.Area= 17,790 sf Storage= 77,050 cf

Plug-Flow detention time= 233.7 min calculated for 1.398 af (70% of inflow) Center-of-Mass det. time= 143.1 min (914.3 - 771.2)

Volume	Invert	Avail.	Storage	Storage Descript	ion				
#1	42.17'	7	7,050 cf	Custom Stage D	<b>)ata (Prismatic)</b> List	ed below (Recalc)			
Elevatio	on Su	urf.Area	Voids	Inc.Store	Cum.Store				
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)				
42.1	7	10,418	0.0	0	0				
43.5	50	10,418	40.0	5,542	5,542				
45.0	00	10,418	10.0	1,563	7,105				
46.0	00	11,745	100.0	11,082	18,187				
48.0	00	14,664	100.0	26,409	44,596				
50.0	00	17,790	100.0	32,454	77,050				
Device	Routing	Inv	ert Outl	et Devices					
#1	Primary	42.4	42' <b>12.0</b>	" Round Culvert					
	ŗ		L= 4 Inlet n= 0	8.0' CPP, project / Outlet Invert= 42 .013 Corrugated I	ting, no headwall,  k 2.42' / 42.20'   S= 0. PE, smooth interior.	€ 0.900 0046 '/' Cc= 0.900 Flow Area= 0.79 sf			
#2	Device 1	42.4	42' <b>6.0"</b>	Vert. Orifice/Gra	<b>te</b> C= 0.600				
#3	Device 2	45.0	00' <b>10.0</b>	00 in/hr Exfiltrati	on over Surface a	rea above 45.00'			
ща	Davis 1	47.			a = 10,418  st	600			
#4	Device I	47.	15 1 <b>3.2</b>	X 13.2 HORIZ. U	vrifice/Grate C= 0.	600			
#5 Secondary		49.3	Limi 35' <b>7.0'</b> Hea 2.50 Coe 2.64	ited to weir flow at low heads <b>long x 8.9' breadth Broad-Crested Rectangular Weir</b> ad (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 0 3.00 3.50 4.00 4.50 5.00 5.50 ef. (English) 2.46 2.55 2.70 2.69 2.68 2.68 2.67 2.64 2.64 4 2.65 2.64 2.65 2.65 2.66 2.67 2.69					

Primary OutFlow Max=6.59 cfs @ 12.48 hrs HW=48.07' TW=38.86' (Dynamic Tailwater) -1=Culvert (Passes 6.59 cfs of 6.77 cfs potential flow)

-2=Orifice/Grate (Passes 1.01 cfs of 2.20 cfs potential flow) -3=Exfiltration (Exfiltration Controls 1.01 cfs)

-4=Orifice/Grate (Orifice Controls 5.58 cfs @ 4.62 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=42.17' TW=35.00' (Dynamic Tailwater) **5=Broad-Crested Rectangular Weir**(Controls 0.00 cfs)

### Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.1 by 7.52' @ 0.00 hrs (23.95 cfs 25.099 af)

Inflow /	Area	=	5.567 ac, 5	58.73% Imp	ervious,	Inflow Depth >	1.1	9" for 10	Year eve	nt
Inflow	:	=	1.76 cfs @	13.65 hrs,	Volume	= 0.550	af			
Primar	y :	=	1.76 cfs @	13.65 hrs,	Volume	= 0.550	af,	Atten= 0%,	Lag= 0.0	) min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Y	/ear	25	Point manual	elevation	table,	To=	0.00 hrs,	dt= 1.00 hrs,	feet =		
	55.	07	55.07	55.07	55.	07	55.07	55.07	55.07	55.07	55.07
	55.	07	55.07	55.07	55.	07	55.07	55.07	55.07	55.07	55.07
	55.	07	55.07	55.07	55.	07	55.07	55.07	55.07		

# Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.3 by 3.65' @ 0.00 hrs (92.51 cfs 86.028 af)

Inflow /	Area =	30.478 ac, s	59.60% Impervi	ious, Inflow	Depth > $2.6$	69" for 10	Year event
Inflow	=	39.92 cfs @	12.50 hrs, Vo	olume=	6.819 af		
Primar	y =	39.92 cfs @	12.50 hrs, Vo	olume=	6.819 af,	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 2 Point manual elevation table, To= 0.00 hrs, dt= 24.00 hrs, feet = 38.65 38.65

#### Summary for Link PA2: POINT OF ANALYSIS

Inflow Are	a =	1.132 ac, 8	30.99% Impe	ervious,	Inflow De	pth > 4	.77" for <i>"</i>	10 Year event
Inflow	=	5.94 cfs @	12.07 hrs,	Volume	=	0.449 af		
Primary	=	5.94 cfs @	12.07 hrs,	Volume	=	0.449 af	, Atten= 0°	%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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Time span=0.00-24.00 hrs, Runoff by SCS TR-20 method Reach routing by Dyn-Stor-Ind method	dt=0.05 hrs, 481 points d, UH=SCS, Weighted-CN Pond routing by Dyn-Stor-Inc	d method
SubcatchmentPOST 1.0: WATERSHED Runoff Area	=462,599 sf   72.19% Imperviou	is Runoff Depth>6.00"
Flow Length=9	933'   Tc=11.4 min   CN=91   Rur	noff=58.40 cfs 5.309 af
SubcatchmentPOST 1.1: WATERSHED Runoff Area	=242,496 sf 58.73% Imperviou	is Runoff Depth>5.43"
Flow Length=7	/50' Tc=10.3 min CN=86 Rur	hoff=29.42 cfs 2.517 af
SubcatchmentPOST 1.2: WATERSHED Runoff Area	=101,204 sf 62.15% Imperviou	is Runoff Depth>5.66"
Flow Length=1	,191' Tc=6.4 min CN=88 Rur	hoff=14.27 cfs 1.095 af
SubcatchmentPOST 1.3: WATERSHED Runoff Area	=306,549 sf 22.64% Imperviou	is Runoff Depth>4.39"
Flow Length=1,5	25' Tc=45.9 min CN=77 Rur	noff=16.72 cfs 2.574 af
SubcatchmentPOST 1.4: WATERSHED Runoff Area	=214,764 sf 85.05% Imperviou	is Runoff Depth>6.35"
Flow Length=	717' Tc=7.5 min CN=94 Rur	hoff=31.40 cfs 2.610 af
SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Are	ea=49,290 sf  80.99% Imperviou	is Runoff Depth>6.24"
Flow Length	=758'  Tc=5.0 min  CN=93  Ru	unoff=7.66 cfs 0.588 af
Reach REACH 1.0: RESTORED         Avg. Flow Dep           n=0.040         L=1,309.0'         S=0.0092	th=0.86' Max Vel=2.20 fps Inf 2 '/' Capacity=2,720.29 cfs Out	low=14.27 cfs 2.076 af tflow=7.67 cfs 2.061 af
Pond POND 1.0: GRAVEL WETLAND1 Peak Elev	r=47.21' Storage=92,932 cf Infl	low=58.40 cfs 5.309 af
Primary=19.23 cfs 2.787 af Seco	ndary=24.16 cfs 0.988 af Outfl	low=43.41 cfs 3.776 af
Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev	r=55.71' Storage=68,356 cf Infl Ou	low=29.42 cfs 2.517 af tflow=4.20 cfs 0.981 af
Pond POND 1.2: PDMH203	Peak Elev=50.86' Inf	flow=14.27 cfs  2.076 af
48.0" Round Culvert n=0.0	13 L=269.0' S=0.0050 '/' Outfl	low=14.27 cfs  2.076 af
Pond POND 1.3: OUTLET CULVERTS Peak Elev=	39.33' Storage=19,198 cf Inflo	ow=67.56 cfs 10.378 af
Primary=66.14 cfs 10.071 af Seco	ndary=0.00 cfs 0.000 af Outflo	ow=66.14 cfs 10.071 af
Pond POND 1.4: RAINGARDEN1.0 Peak Elev	r=48.89' Storage=58,248 cf Infl	low=31.40 cfs 2.610 af
Primary=7.29 cfs 1.966 af Se	condary=0.00 cfs 0.000 af Out	tflow=7.29 cfs 1.966 af
Link LINK 1.0: PDMH203 TAILWATER	Ir Priı	nflow=4.20 cfs  0.981 af mary=4.20 cfs  0.981 af
Link PA1: POINT OF ANALYSIS	Inflo Prima	ow=66.14 cfs 10.071 af ary=66.14 cfs 10.071 af
Link PA2: POINT OF ANALYSIS	lr Prii	nflow=7.66 cfs  0.588 af mary=7.66 cfs  0.588 af

Total Runoff Area = 31.609 acRunoff Volume = 14.693 afAverage Runoff Depth = 5.58"39.63% Pervious = 12.527 ac60.37% Impervious = 19.083 ac

L-0700-26 POST	Туре	III 24-hr 50 Y	ear Rainfall=8.46"
Prepared by Tighe & Bond			Printed 6/6/2023
HydroCAD® 10.00-20 s/n 03436 © 2017 Hydro	drocad Software Solutions LLC		Page 18
Time span=0.	00-24.00 hrs, dt=0.05 hrs, 481	points	ethod
Runoff by SCS	FR-20 method, UH=SCS, Weig	ghted-CN	
Reach routing by Dyn-Stor-I	nd method - Pond routing by	Dyn-Stor-Ind me	
SubcatchmentPOST 1.0: WATERSHED	Runoff Area=462,599 sf 72.1	9% Impervious I	Runoff Depth>7.37"
	Flow Length=933' Tc=11.4 min	CN=91 Runoff=	=70.91 cfs  6.521 af
SubcatchmentPOST 1.1: WATERSHED	Runoff Area=242,496 sf 58.7	3% Impervious I	Runoff Depth>6.77"
	Flow Length=750' Tc=10.3 min	CN=86 Runoff=	=36.28 cfs  3.140 af
SubcatchmentPOST 1.2: WATERSHED	Runoff Area=101,204 sf 62.1	5% Impervious I	Runoff Depth>7.01"
	Flow Length=1,191' Tc=6.4 min	CN=88 Runoff	=17.48 cfs  1.358 af
SubcatchmentPOST 1.3: WATERSHED	Runoff Area=306,549 sf 22.6	4% Impervious  F	Runoff Depth>5.65"
	ow Length=1,525' Tc=45.9 min	CN=77  Runoff=	=21.42 cfs  3.313 af
SubcatchmentPOST 1.4: WATERSHED	Runoff Area=214,764 sf 85.0	5% Impervious I	Runoff Depth>7.73"
	Flow Length=717' Tc=7.5 min	CN=94 Runoff=	=37.84 cfs  3.177 af
SubcatchmentPOST 2.0: WATERSHED	<b>2.0</b> Runoff Area=49,290 sf 80.9	9% Impervious I	Runoff Depth>7.62"
	Flow Length=758' Tc=5.0 mir	ı CN=93 Runof	f=9.25 cfs  0.718 af
Reach REACH 1.0: RESTORED n=0.040 L=1,309.	Avg. Flow Depth=0.90' Max Vel	=2.19 fps Inflow=	=17.48 cfs  2.679 af
	0' S=0.0092 '/' Capacity=2,720	).29 cfs Outflow=	=10.33 cfs  2.662 af
Pond POND 1.0: GRAVEL WETLAND1	Peak Elev=47.48' Storage=	98,793 cf Inflow	=70.91 cfs  6.521 af
Primary=19.73 cfs 3	3.345 af Secondary=38.14 cfs 1	.616 af Outflow=	=57.87 cfs  4.961 af
Pond POND 1.1: GRAVEL WETLAND 2	Peak Elev=56.45' Storage=	83,107 cf Inflow Outflov	=36.28 cfs  3.140 af w=6.58 cfs  1.321 af
Pond POND 1.2: PDMH203	Peak Ele	ev=51.03' Inflow	=17.48 cfs  2.679 af
48.0" Round	Culvert n=0.013 L=269.0' S=0.	0050 '/' Outflow	=17.48 cfs  2.679 af
Pond POND 1.3: OUTLET CULVERTS	Peak Elev=39.77' Storage=2	4,643 cf Inflow=8	87.04 cfs  13.437 af
Primary=83.35 cfs 13	.109 af Secondary=0.00 cfs 0.0	000 af Outflow=8	33.35 cfs  13.109 af
Pond POND 1.4: RAINGARDEN1.0	Peak Elev=49.56' Storage=	69,290 cf Inflow	=37.84 cfs  3.177 af
Primary=7.69 cfs	2.462 af Secondary=1.60 cfs	0.039 af Outflow	v=9.29 cfs  2.500 af
Link LINK 1.0: PDMH203 TAILWATER		Inflov Primar	w=6.58 cfs 1.321 af y=6.58 cfs 1.321 af
Link PA1: POINT OF ANALYSIS		Inflow= Primary=	83.35 cfs  13.109 af 83.35 cfs  13.109 af
Link PA2: POINT OF ANALYSIS		Inflov Primar	w=9.25 cfs 0.718 af y=9.25 cfs 0.718 af

Total Runoff Area = 31.609 acRunoff Volume = 18.227 afAverage Runoff Depth = 6.92"39.63% Pervious = 12.527 ac60.37% Impervious = 19.083 ac



Proposed Solar Project

Portsmouth International Airport

# Portsmouth, NH Glare Study Results

Photovoltaic (Solar) Project in Portsmouth, Rockingham County, NH

# February 22, 2024

Prepared for:

IPS - Integrated Project Services, LLC 721 Arbor Way, Suite 100 Blue Bell, PA 19422 Prepared by:

Elizabeth C. Myers, PMP Certified Glare Analyst

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### Appendix



# Conclusion

Collier's Engineering & Design (CED) performed an analysis on the array areas of the proposed rooftop and carport solar project site in Portsmouth, Rockingham County, NH.

# Through extensive cross-checking, it was found that at a 5-degree resting angle or above for the rooftop system panels, there is no predicted glare throughout the entire project area. Small amounts of green glare predicted from the carports onto a route directly next to the proposed project are easily mitigated.

The study area is presented in the graphic below. Red Markers represent Observation Points, Turquoise Lines are the roads in and around the proposed project area, and Brown Lines represent the existing foliage in the area and/or the proposed landscaping lines. The Brown Lines around the rooftop systems represent the parapets that run the entire perimeter of the buildings.



A closer view of the immediate project area:





The triangulation of the proposed project in relation to Portsmouth International Airport is provided below. Because of the proximity to the airport and the Air Traffic Control Tower, the client specifically requested a full study to be certain that no glare of any kind would affect the Tower.



To establish a <u>worst-case scenario</u> baseline, a 15-degree angle for the proposed rooftop system facing 214 degrees (azimuth) was programmed on the rooftops of two buildings. For the proposed carports, four array areas were programmed facing 124 degrees (azimuth) and one carport was programmed facing 214 degrees (azimuth). The project was modeled <u>without</u> local foliage lines and other large buildings between the proposed project and the ATCT in the area programmed.



The Air Traffic Control Tower was modeled at a dual height of 130 feet and 120 feet to cover broader possibilities of the proposed project's sightline to anyone in the tower structure.



With the above settings, the modelling predicts ZERO minutes of YELLOW glare over the course of an entire year and ~4,474 minutes of GREEN glare over the course of an entire year. The glare results include ~1,863 minutes of GREEN glare on the Air Traffic Control Tower at Portsmouth International Airport from Carports 1, 3 and 4. **No glare whatsoever is predicted from the rooftop systems onto the ATCT or onto any other point in the study.** 

At the proposed working settings of a 5-degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

At the proposed working settings of a 10-degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

At the proposed working settings of a 13-degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

At the proposed working settings of a 15-degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.



A review of the Federal Aviation Administration's (FAA) New York area Visual Flight Rules (VFR) charts shows no restricted airspace in or around the proposed project area.



A review of Military Training Route (MTR) charts was performed utilizing an additional online resource and the proposed project falls entirely **OUTSIDE** of known training route areas.





The above conclusion is arrived at by utilizing the worst-case scenario results provided by the *ForgeSolar* software, and then manually layering back into each modeling scenario all real-world factors in the area of the proposed site location.

Full technical reporting output by the *ForgeSolar* program is included in the Appendix of this report.

Sincerely,

Colliers Engineering & Design, Inc. (DBA Maser Consulting)

Elizabeth Claire Myers, PMP Project Manager, Electrical Engineering Certified Glare Analyst through Sims Industries

cc: Lee Hill, PE, Colliers Engineering & Design (via email)

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# Resources

**Federal Aviation Administration – Publicly Available Visual Flight Rules (VFR) Charts** <u>https://www.faa.gov/air\_traffic/flight\_info/aeronav/digital\_products/vfr/</u>

• Utilized to obtain FAA-approved VFR charts of the project area for inclusion and consideration in this study.

**U.S. Military Training Routes (MTRs) and buffers -** May 4, 2018 (Last modified Oct 6, 2021) Uploaded by South Atlantic Blueprint <u>https://salcc.databasin.org/datasets/4c81852be18444b997f8f860ee568c54/</u>

• Utilized to obtain detail and graphic of US-wide Military Training Routes and location specific data for this study.

Ho, C. K., Ghanbari, C. M., and Diver, R. B., 2011, **Methodology to Assess Potential Glint and Glare Hazards From Concentrating Solar Power Plants: Analytical Models and Experimental Validation**, *ASME J. Sol. Energy Eng.*, *133*.

Solar Glare Hazard Analysis Tool (SGHAT) Technical Reference Manual



# Details of Glare Study Methodology

(Source Information: https://forgesolar.com/help/#intro)

Collier's Engineering & Design (CED) offers staff specifically trained on glare analyses utilizing *ForgeSolar*, a web-based interactive software that provides a quantified assessment of (1) when and where glare is predicted to occur throughout the year for a prescribed solar installation, and (2) potential effects on the human eye at locations where glare is predicted to occur. *ForgeSolar* is based on the Solar Glare Hazard Analysis Tool ("SGHAT") licensed from Sandia National Laboratories.

These tools meet the FAA standards for glare analysis.

Determination of glare occurrence requires knowledge of the following: sun position, observer location, and the tilt, orientation, location, extent, and optical properties of the modules in the solar array. Vector algebra is then used to determine if glare is likely to be visible from the prescribed observation points.

If glare is predicted, the software calculates the retinal irradiance and subtended angle (size/distance) of the glare source to predict potential ocular hazards ranging from temporary afterimage to more severe possible retinal damage. These results are presented in a simple, easy-tointerpret plot that specifies when glare is predicted to occur throughout the year, with color codes indicating the potential ocular hazard.



### **Background Information**

Glint is typically defined as a momentary flash of bright light, often caused by a reflection off a moving source. A typical example of glint is a momentary solar reflection from a moving car, or "catching" something bright out of the corner of your eye.

Glare is defined as a continuous source of bright light. Glare is generally associated with stationary objects, which, due to the slow relative movement of the sun, reflect sunlight for a longer duration.

The difference between glint and glare is duration. Industry-standard glare analysis tools evaluate the occurrence of glare on a minute-by-minute basis; accordingly, they generally refer to solar hazards as 'glare.'

The ocular impact of solar glare is quantified into three categories (Ho, 2011):

- 1. Green Unproblematic shine. Low potential to cause after-image. This type of glare can be compared to noticing something shiny in the distance.
- 2. Yellow Potential to cause temporary afterimage (flash blindness). This type of glare is much like sunrise and sunset glare for drivers who struggle to find the perfect angle for car visors so they can continue to operate their vehicle safely while traveling through areas of such glare.
  - Standard levels of yellow glare can, for the most part, be handled with relative ease utilizing slatted fencing or localfoliage landscape mitigation measures.
  - b. Only extremely high levels of this type of glare (in the area of the chart to the right labeled as "direct viewing of the sun" which is uncommon to find with PV installations) would be considered an insurmountable hurdle to a PV installation of any size.
  - c. High levels/intensities and long durations are different factors.





- 3. Red Potential to cause retinal burn (permanent eye damage). PV modules do not focus reflected sunlight and therefore retinal burn (RED glare) is typically not possible.
  - d. This is the ONLY type of glare that would be considered an insurmountable hurdle to a PV installation of any size.

These categories assume a typical blink response in the observer.



# Note that retinal burn is typically not possible for PV glare since PV modules do not focus reflected sunlight. They are, in fact, designed to absorb as much sunlight as possible.

To further put glare into perspective, the following is presented.

YELLOW glare such as in the graphic to the right could only be seen when standing directly next to project panels at the perfect angle when the sun is in a perfect place—indeed the point of a photographer standing directly by these panels and waiting for the perfect moment to capture this image. It is also possible that the panels in the picture shown do not have an anti-reflective coating.



Solar panel showing solar glare

GREEN glare, as illustrated directly to the right, is the more common occurrence with solar projects—a noticeable shiny area (in the northwest area) as compared to panels where the sun is not quite in perfect alignment yet.

Even so, the effect of this noticeable shine to certain areas of the project area is still seen from a relatively close up vantage point and at the optimal height this image was captured, possibly by a drone. A similarly sized project in the



distance, closer to the horizon of the photo would be unlikely to show even the levels of green glare that the system in the foreground reflects.



#### **Executive Summary**

The purpose of the glare study requested by IPS – Integrated Project Service, LLC (IPS) and their client is to closely examine a proposed solar project in Portsmouth, Rockingham County, NH and to provide feedback regarding areas that may warrant closer examination in order to mitigate possible problematic predicted glare to the businesses, residences, and roads surrounding the project area.

Information was provided by IPS and their client in order to complete this study. The project's rooftop PV systems were programmed to a 15-degree tilt axis facing 214 degrees at a height of 88 feet for the smaller structure and 93.83 feet for the larger building. The parapets for these buildings were programmed at heights of 93.21 feet and 99.3 feet respectively.

Four of the projects five carport systems were programmed with two top heights (20.17 feet and 22.48 feet) and a lower edge of 14 feet, facing 124 degrees southeast. A final carport was programmed with a 20.17 foot high edge, a 14 foot lower edge and facing 214 degrees.

It was further assumed that the panels used throughout the proposed project are constructed of Smooth Glass with an Anti-Reflective coating.

Seven (7) Observation Points were placed at different points around the site and programmed to an average height of 5 and a half (5.5) feet to model someone standing in these spots, and to a height of 15 to 20 feet to model a 5.5-foot person standing on the second floor of a home/business with 8-foot ceilings and a 1.5-foot plenum space.





The building directly southwest of the proposed project is industrial in nature, and an examination of the portion that will be facing the project shows that it is industrial in nature with very few windows. One OP was programmed here at a height of 40 feet.







Two Observation Points representing the Air Traffic Control Tower at Portsmouth International Airport were programmed to heights of 130 feet and 120 feet.

Six (6) Route Receptors were programmed for two-way traffic to heights of 4.5 feet and 8.5 feet, effectively representing the eyeline of an average person sitting on/in any vehicle from a bike to a motorcycle, a standard car or SUV, through to the approximated seated height in the cab of an 18-wheeler truck.



While it is impossible to study every possible point and/or angle surrounding a photovoltaic (solar) project, Collier's Engineering & Design (CED) has modeled the project and surrounding areas as best as possible with the most likely points of concern.

PV modules do not focus reflected sunlight and therefore retinal burn is typically not possible. They are, in fact, designed to absorb as much sunlight as possible. Modern photovoltaic panels actually cause less glare than standard home window glass; and research has shown that they reflect less light than snow, white concrete and energy-efficient white rooftops.

The YELLOW glare we are looking to identified with this study is much like sunrise and sunset glare for drivers who struggle to find the perfect angle for car visors so they can continue to operate their vehicle safely while traveling through areas of such glare. In general, photovoltaic panel systems of any size produce some glare predominately during early sunrise and sunset throughout the Spring



through Fall months—although glare is possible throughout each day as well as throughout the entire year.

*ForgeSolar* now allows the programming of obstructions. It was utilized in this study to model in existing treelines, local warehouses and other buildings and the parapets of the proposed new buildsings for this project with estimated heights. Local foliage lines were modeled at a conservative height of 17 to 30 feet in height. Local warehouses were modeled conservatively at 20 to 30 feet high.



After examining each point and then factoring in additionally recommended foliage, distance, and elevation changes, points where predicted glare is blocked by natural obstructions were removed from the listing of points to be examined more closely. Finally, if any glare continues to be predicted in any area, this analyst will address the areas that present the <u>most</u> possibility for likely glare.

#### ASSUMPTIONS

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.\*
- Glare analyses do not account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographic obstructions.
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Glare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.



## **Results of this Study**

#### WORST CASE SCENARIO without Local Foliage - RESULTS at 15 Degree Resting Angle

To establish a worst-case scenario baseline, the project was modeled <u>without</u> any local foliage lines or building obstructions between the proposed project and the Air Traffic Control Tower at the Portsmouth International Airport. The modelling predicts ZERO minutes of YELLOW glare over the course of an entire year and ~4,474 minutes of GREEN glare over the course of an entire year. The glare results include ~1,855 minutes of GREEN glare on the Air Traffic Control Tower at Portsmouth International Airport from Carports 1, 3 and 4. No glare whatsoever is predicted from the rooftop systems onto the ATCT or onto any other point in the study.

#### **RESULTS at 5 Degree Angle**

At the proposed working settings of a 5-degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

#### **RESULTS at 10 Degree Resting Angle**

At the proposed working settings of a 10-degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

#### **RESULTS at 13 Degree Resting Angle**

At the proposed working settings of a 13-degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

#### **RESULTS at 15 Degree Resting Angle**

At the proposed working settings of a 15-degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.



#### **AREAS OF GLARE**

In ALL results, the areas of glare from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.



A final run scenario with a small planting of trees at the area marked in green in the "Positions Along Path Receiving Glare" shows that a screen of 9 feet at initial planting will completely mitigate any glare shown.

PV Name	Tilt	Orientation	"Green" Glare
	deg	deg	min
CRPRT1	0.0	124.0	0
CRPRT2	0.0	124.0	0
CRPRT3	0.0	124.0	0
CRPRT4	0.0	124.0	0
CRPRT5	0.0	214.0	0
LGBLDG	10.0	214.0	0
SMBLDG	10.0	214.0	0

#### Summary of Results No glare predicted!





### Summary of FAA-Level Flight Path Screening Results

Portsmouth International Airport sits under 1 mile away from the project on the western side. All obstructions were kept in place for the FAA screening and the project was modeled at the 10 degree rooftop PV system tilt.

#### FEDERAL AVIATION ADMINISTRATION (FAA) SCREENS

An FAA-level glare analysis was performed and a report specific to this request can be found in Appendix A of this report. The Air Traffic Control Tower at Portsmouth International Airport is modeled for this study at its height of 130 feet. Additionally, a second point was modeled at 120 feet to be certain of the glare study results.

#### Per the FAA's most recent 2021 policy regarding solar around airports, this project PASSES.

#### Project: ALBACORE, Portsmouth, NH

Site configuration: Albacore\_10DegreeTilt\_124Carports\_ATCT\_FAAReport

Created 22 Feb, 2024 Updated 22 Feb, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg DNI peaks at 1,000.0 W/m<sup>2</sup> Site ID 112738.19298

Ocular transmission coefficient 0.5 Pupil diameter 0.002 m Eye focal length 0.017 m Sun subtended angle 9.3 mrad PV analysis methodology V2



# **Glare Policy Adherence**

The following table estimates the policy adherence of this glare analysis according to the 2021 U.S. Federal Aviation Administration Policy:

#### Review of Solar Energy System Projects on Federally-Obligated Airports

This policy may require the following criteria be met for solar energy systems on airport property:

- · No glare of any kind for Air Traffic Control Tower(s) ("ATCT") at cab height.
- · Default analysis and observer characteristics, including 1-minute time step.

ForgeSolar is not affiliated with the U.S. FAA and does not represent or speak officially for the U.S. FAA. ForgeSolar cannot approve or deny projects - results are informational only. Contact the relevant airport and FAA district office for information on policy and requirements.

COMPONENT	STATUS	DESCRIPTION		
Analysis parameters	PASS	Analysis time interval and eye characteristics used are acceptable		
ATCT(s)	PASS	Receptor(s) marked as ATCT do not receive glare		

The complete updated FAA Policy can be read at: https://www.federalregister.gov/d/2021-09862

*NOTE:* ForgeSolar does not represent or speak officially for the FAA and cannot approve or deny projects. *Results are informational only.* 



# On May 26, 2021, the Federal Aviation Administration updated their policies regarding the installation of solar on and/or near regulated airports/airstrips.

While this policy of the Federal Aviation Administeration does not apply to solar energy systems on airports that do not have an Air Traffic Control Tower (ATCT), airports that are not federally-obligated, or solar energy systems not located on airport property—it does provide a high benchmark to meet to ensure that proposed solar installations do not create glare that poses any sort of safety hazard for pilots.

The brief of this FAA policy update states:

"The Federal Aviation Administration (FAA) published a final policy aimed at ensuring that airport solar projects don't create hazardous glare. The policy requires airports to measure the visual impact of such projects on pilots and air traffic control personnel.

The policy applies to proposed solar energy systems at federally obligated airports with control towers. Federally obligated airports are public airports that have accepted federal assistance either in the form of grants of property conveyances

As more airports invests in this technology for environmental and economic benefits, the FAA wants to make sure that the reflection from the systems' glass surfaces do not create a glare that poses a safety hazard for pilots and air traffic controllers.

Under the final policy, airports are no longer required to submit the results of an ocular analysis to FAA. Instead, the airport must file a Notice of Proposed Construction or Alteration Form 7460-1 that includes a statement that the project will not cause any visual impact. The airport submits the form to the FAA for review and approval.

The FAA relies on the airport to confirm via the form that it has sufficiently analyzed the potential for glint and glare and determined there is no potential for ocular impact to the airport traffic control tower cab. If any impacts are discovered after construction, the airport must mitigate the impact at its expense. The airport may also face compliance action for failure to address visual impacts that create aviation safety hazards. As such, the agency encourages an airport to conduct sufficient analysis before installing a solar energy system.

The FAA is also withdrawing the recommended tool for measuring the ocular impact of potential glint and glare effects on pilots and air traffic controllers."

#### Additionally:

"Initially, FAA believed that solar energy systems could introduce a novel glint and glare effect to pilots on final approach. FAA has subsequently concluded that in most cases, the glint and glare from solar energy systems to pilots on final approach is similar to glint and glare pilots routinely experience from water bodies, glass-façade buildings, parking lots, and similar features. However, FAA has continued to receive reports of potential glint and glare from on-airport solar energy systems on personnel working in ATCT cabs. Therefore, FAA has determined the scope of agency policy should be focused on the impact of on-airport solar energy systems to federally-obligated towered airports, specifically the airport's ATCT cab."



# Appendix

# Appendix A | Detailed Glare Study Result Reports

The following pages are the full reporting results delivered directly from *ForgeSolar*.



# FORGESOLAR GLARE ANALYSIS

#### Project: ALBACORE, Portsmouth, NH

Site configuration: Albacore\_10DegreeTilt\_124Carports\_ATCT\_FAAReport

#### Client: Lonza

Created 22 Feb, 2024 Updated 22 Feb, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg DNI peaks at 1,000.0 W/m<sup>2</sup> Site ID 112738.19298

Ocular transmission coefficient 0.5 Pupil diameter 0.002 m Eye focal length 0.017 m Sun subtended angle 9.3 mrad PV analysis methodology V2



# **Glare Policy Adherence**

The following table estimates the policy adherence of this glare analysis according to the 2021 U.S. Federal Aviation Administration Policy:

#### Review of Solar Energy System Projects on Federally-Obligated Airports

This policy may require the following criteria be met for solar energy systems on airport property:

- No glare of any kind for Air Traffic Control Tower(s) ("ATCT") at cab height.
- Default analysis and observer characteristics, including 1-minute time step.

ForgeSolar is not affiliated with the U.S. FAA and does not represent or speak officially for the U.S. FAA. ForgeSolar cannot approve or deny projects - results are informational only. Contact the relevant airport and FAA district office for information on policy and requirements.

COMPONENT	STATUS	DESCRIPTION
Analysis parameters	PASS	Analysis time interval and eye characteristics used are acceptable
ATCT(s)	PASS	Receptor(s) marked as ATCT do not receive glare

The referenced policy can be read at https://www.federalregister.gov/d/2021-09862



# **Component Data**

This report includes results for PV arrays and Observation Point ("OP") receptors marked as ATCTs. Components that are not pertinent to the policy, such as routes, flight paths, and vertical surfaces, are excluded.

# **PV Arrays**

Name: CRPRT1 Axis tracking: Fixed (no rotation) Tilt: 0.0° Orientation: 124.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.085650	-70.803723	57.92	20.17	78.09
2	43.085595	-70.803619	57.81	14.00	71.81
3	43.085032	-70.804187	64.54	14.00	78.54
4	43.085084	-70.804291	66.68	20.17	86.85

Name: CRPRT2 Axis tracking: Fixed (no rotation) Tilt: 0.0° Orientation: 124.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.085519	-70.803626	57.88	22.48	80.36
2	43.085431	-70.803461	56.75	14.00	70.75
3	43.084981	-70.803912	58.98	14.00	72.98
4	43.085070	-70.804083	59.73	22.48	82.20


Name: CRPRT3 Axis tracking: Fixed (no rotation) Tilt: 0.0° Orientation: 124.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.085400	-70.803418	56.90	22.48	79.38
2	43.085325	-70.803271	56.23	14.00	70.23
3	43.084876	-70.803716	58.56	14.00	72.56
4	43.084953	-70.803866	59.01	22.48	81.49

### Name: CRPRT4

Axis tracking: Fixed (no rotation) Tilt: 0.0° Orientation: 124.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52



Name: CRPRT5 Axis tracking: Fixed (no rotation) Tilt: 0.0° Orientation: 214.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Name: LGBLDG Axis tracking: Fixed (no rotation)

Tilt: 10.0° Orientation: 214.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52



Name: SMBLDG Axis tracking: Fixed (no rotation) Tilt: 10.0° Orientation: 214.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.084480	-70.803051	56.19	88.00	144.19
2	43.084450	-70.803081	56.31	88.00	144.31
3	43.084506	-70.803193	56.74	88.00	144.74
4	43.084466	-70.803232	56.81	88.00	144.81
5	43.084412	-70.803118	56.55	88.00	144.55
6	43.084252	-70.803275	58.91	88.00	146.91
7	43.084414	-70.803594	61.58	88.00	149.58
8	43.084643	-70.803375	58.79	88.00	146.79

## **Observation Point ATCT Receptors**

Name	ID	Latitude (°)	Longitude (°)	Elevation (ft)	Height (ft)
1-ATCT	1	43.084384	-70.818882	89.93	130.00
6-ATCT	6	43.084349	-70.818856	89.97	120.00

Map image of 1-ATCT



Map image of 6-ATCT





## **Obstruction Components**

Name: BLDG1 Top height: 12.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.084600	-70.810084	76.71
2	43.084703	-70.809846	77.63
3	43.084534	-70.809702	77.38
4	43.084428	-70.809944	77.34
5	43.084600	-70.810084	76.71

Name: BLDG2 Top height: 20.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.084955	-70.806346	99.52
2	43.085031	-70.806408	98.08
3	43.084866	-70.806801	99.55
4	43.084555	-70.806565	99.98
5	43.084608	-70.806439	99.85
6	43.084444	-70.806325	99.64
7	43.084592	-70.806011	99.08
8	43.084965	-70.806346	99.43



Name: HighEdge1 Top height: 22.0 ft		Google e Geot dray t	Tater Technologies, U.S., Geologies Survey, USDAFPAC/GEO
Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50







Name: HighEdge4 Top height: 20.2 ft

Name: PRPT1 Top height: 93.2 ft



1     43.085307     -70.803260     56.28       2     43.084860     -70.803684     58.42	Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
2 43.084860 -70.803684 58.42	1	43.085307	-70.803260	56.28
	2	43.084860	-70.803684	58.42

Gogle is GeoLurary, Maxai Technologies, U.S. Geological Survey, USDA/FPAC/GEO

Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96



Name: PRPT2 Top height: 99.3 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

Name: TREELINE Top height: 35.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97



Name: Trees Top height: 30.0 ft		Google :: Geoladray, 1	Maxar Technologies, U.S. Geological Survey, USDAFPAC/GEO
Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees Top height: 17.0 ft		Coogle - Geolegy	Axar Technologes, U.S. Geological Survey, USDA/FRAC/EEO
Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085036	-70.807176	92.20
2	43.084131	-70.806567	95.41



Name: Trees1 Top height: 40.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

Name: Trees2 Top height: 60.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.084443	-70.818109	84.34
2	43.084602	-70.818167	84.74
3	43.084354	-70.818474	88.75



Name: Trees3<br/>Top height: 100.0 ftImage: State of the s





Name: Trees5 Top height: 45.0 ft



Latitude (*)	Longitude (°)	Ground elevation (ft)
43.084411	-70.807233	89.30
43.084554	-70.807316	89.33
43.084677	-70.807358	89.54
43.084730	-70.807552	87.97
	43.084411 43.084554 43.084677 43.084730	43.084411       -70.807233         43.084554       -70.807316         43.084677       -70.807358         43.084730       -70.807552

Name: Trees6 Top height: 20.0 ft		Google = Geollarary, I	Maxar Technologies, U.S. Geological Survey, USDA/FPAC/GEO
Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085286	-70.814633	80.07
2	43.083793	-70.813418	79.96



Name: Trees7 Top height: 30.0 ft		Google e Geol brany f	Aaxat Technologies, U.S. Geological Survey, USDA EPAC/GEO
Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Top height: 30.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26



Name: WRHSE2 Top height: 30.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.084916	-70.813107	81.43
2	43.084740	-70.813499	81.62
3	43.084705	-70.813466	81.64
4	43.084630	-70.813662	81.71
5	43.084174	-70.813292	81.76
6	43.084399	-70.812785	81.68
7	43.084501	-70.812860	81.70
8	43.084540	-70.812758	81.66
9	43.084916	-70.813107	81.43



PV Array	Tilt	Orient	Annual Gr	een Glare	Annual Yel	low Glare	Energy
	٥	0	min	hr	min	hr	kWh
CRPRT1	0.0	124.0	0	0.0	0	0.0	-
CRPRT2	0.0	124.0	0	0.0	0	0.0	-
CRPRT3	0.0	124.0	0	0.0	0	0.0	-
CRPRT4	0.0	124.0	0	0.0	0	0.0	-
CRPRT5	0.0	214.0	0	0.0	0	0.0	-
LGBLDG	10.0	214.0	0	0.0	0	0.0	-
SMBLDG	10.0	214.0	0	0.0	0	0.0	-

## Summary of Results No glare predicted

Total annual glare received by each receptor; may include duplicate times of glare from multiple reflective surfaces.

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0.0	0	0.0

## **PV: CRPRT1**

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0.0	0	0.0

## **CRPRT1** and **1-ATCT**

**CRPRT1** and 6-ATCT

Receptor type: ATCT Observation Point **No glare found** 

Receptor type: ATCT Observation Point **No glare found** 

## **PV: CRPRT2**

Receptor	Annual Green Glare		Annual Yellow Glare		
	min	hr	min	hr	
1-ATCT	0	0.0	0	0.0	
6-ATCT	0	0.0	0	0.0	



## **CRPRT2** and **1-ATCT**

Receptor type: ATCT Observation Point **No glare found** 

## **CRPRT2** and 6-ATCT

Receptor type: ATCT Observation Point **No glare found** 

## **PV: CRPRT3**

Receptor	Annual Green Glare		Annual Yellow Glare		
	min	hr	min	hr	
1-ATCT	0	0.0	0	0.0	
6-ATCT	0	0.0	0	0.0	

### **CRPRT3 and 1-ATCT**

### **CRPRT3 and 6-ATCT**

Receptor type: ATCT Observation Point **No glare found** 

Receptor type: ATCT Observation Point No glare found

## **PV: CRPRT4**

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0.0	0	0.0

## **CRPRT4 and 1-ATCT**

Receptor type: ATCT Observation Point **No glare found** 

### **CRPRT4 and 6-ATCT**

Receptor type: ATCT Observation Point **No glare found** 

## **PV: CRPRT5**

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0.0	0	0.0

## **CRPRT5** and **1-ATCT**

Receptor type: ATCT Observation Point **No glare found** 

**CRPRT5** and 6-ATCT

Receptor type: ATCT Observation Point **No glare found** 



## **PV: LGBLDG**

Receptor	Annual Green Glare		Annual Yellow Glare		
	min	hr	min	hr	
1-ATCT	0	0.0	0	0.0	
6-ATCT	0	0.0	0	0.0	

## LGBLDG and 1-ATCT

LGBLDG and 6-ATCT

Receptor type: ATCT Observation Point **No glare found** 

Receptor type: ATCT Observation Point **No glare found** 

## **PV: SMBLDG**

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0.0	0	0.0

## **SMBLDG and 1-ATCT**

Receptor type: ATCT Observation Point **No glare found** 

## **SMBLDG and 6-ATCT**

Receptor type: ATCT Observation Point **No glare found** 



## Assumptions

"Green" glare is glare with low potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. "Yellow" glare is glare with potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.

The algorithm does not rigorously represent the detailed geometry of a system; detailed features such as gaps between modules, variable height of the PV array, and support structures may impact actual glare results. However, we have validated our models against several systems, including a PV array causing glare to the air-traffic control tower at Manchester-Boston Regional Airport and several sites in Albuquerque, and the tool accurately predicted the occurrence and intensity of glare at different times and days of the year. Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare. This primarily

affects V1 analyses of path receptors.

Random number computations are utilized by various steps of the annual hazard analysis algorithm. Predicted minutes of glare can vary between runs as a result. This limitation primarily affects analyses of Observation Point receptors, including ATCTs. Note that the SGHAT/ ForgeSolar methodology has always relied on an analytical, qualitative approach to accurately determine the overall hazard (i.e. green vs. yellow) of expected glare on an annual basis.

The analysis does not automatically consider obstacles (either man-made or natural) between the observation points and the prescribed solar installation that may obstruct observed glare, such as trees, hills, buildings, etc.

The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)

The variable direct normal irradiance (DNI) feature (if selected) scales the user-prescribed peak DNI using a typical clear-day irradiance profile. This profile has a lower DNI in the mornings and evenings and a maximum at solar noon. The scaling uses a clear-day irradiance profile based on a normalized time relative to sunrise, solar noon, and sunset, which are prescribed by a sun-position algorithm and the latitude and longitude obtained from Google maps. The actual DNI on any given day can be affected by cloud cover, atmospheric attenuation, and other environmental factors.

The ocular hazard predicted by the tool depends on a number of environmental, optical, and human factors, which can be uncertain. We provide input fields and typical ranges of values for these factors so that the user can vary these parameters to see if they have an impact on the results. The speed of SGHAT allows expedited sensitivity and parametric analyses.

The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.

Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid based on aggregated research data. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.

Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.

Refer to the Help page at www.forgesolar.com/help/ for assumptions and limitations not listed here.

Default glare analysis parameters and observer eye characteristics (for reference only):

- · Analysis time interval: 1 minute
- Ocular transmission coefficient: 0.5
- Pupil diameter: 0.002 meters
- · Eye focal length: 0.017 meters
- · Sun subtended angle: 9.3 milliradians

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# ALBACORE, Portsmouth, NH Albacore\_10DegreeTilt\_124Carports\_ATCT\_FAAReport

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112738.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



#### Misc. Analysis Settings

DNI: varies (1,000.0 W/m<sup>2</sup> peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

## Summary of Results No glare predicted!

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	0	0	-
CRPRT4	0.0	124.0	0	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	10.0	214.0	0	0	-
SMBLDG	10.0	214.0	0	0	-

### PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085400	-70.803418	56.90	22.48	79.38
2	43.085325	-70.803271	56.23	14.00	70.23
3	43.084876	-70.803716	58.56	14.00	72.56
4	43.084953	-70.803866	59.01	22.48	81.49

#### Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

#### Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
	8	43.084643	-70.803375	58.79	88.00	146.79

## **Discrete Observation Receptors**

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97

## 1-ATCT map image



## 6-ATCT map image



## **Obstruction Components**

#### Name: BLDG1 Upper edge height: 12.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084600	-70.810084	76.71
2	43.084703	-70.809846	77.63
3	43.084534	-70.809702	77.38
4	43.084428	-70.809944	77.34
5	43.084600	-70.810084	76.71

Name: BLDG2 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084955	-70.806346	99.52
2	43.085031	-70.806408	98.08
3	43.084866	-70.806801	99.55
4	43.084555	-70.806565	99.98
5	43.084608	-70.806439	99.85
6	43.084444	-70.806325	99.64
7	43.084592	-70.806011	99.08
8	43.084965	-70.806346	99.43

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085593	-70.803598	57.75
2	43.085019	-70.804161	63.07

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

Name: TREELINE Upper edge height: 35.0 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.085164	-70.808848	82.83
43.085454	-70.807942	81.22
43.085373	-70.807765	82.86
43.085040	-70.807564	86.97
	Latitude deg 43.085164 43.085454 43.085373 43.085040	Latitude         Longitude           deg         deg           43.085164         -70.808848           43.085454         -70.807942           43.085373         -70.807765           43.085040         -70.807564

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085036	-70.807176	92.20
2	43.084131	-70.806567	95.41

Name: Trees1 Upper edge height: 40.0 ft



Vertex	Latitude Longitude		Ground elevation	
	deg	deg	ft	
1	43.085261	-70.816979	84.00	
2	43.084955	-70.816877	84.48	
3	43.084477	-70.817247	78.24	

Name: Trees2 Upper edge height: 60.0 ft



Vertex	Latitude	Longitude	Ground elevation	
	deg	deg	ft	
1	43.084443	-70.818109	84.34	
2	43.084602	-70.818167	84.74	
3	43.084354	-70.818474	88.75	

Name: Trees3 Upper edge height: 100.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084287	-70.810576	72.89
2	43.084550	-70.810195	75.28

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation	
	deg	deg	ft	
1	43.085286	-70.814633	80.07	
2	43.083793	-70.813418	79.96	

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Latitude	Longitude	Ground elevation	
deg	deg	ft	
43.085129	-70.813496	81.26	
43.085227	-70.813254	81.50	
43.085137	-70.813085	81.35	
43.084986	-70.813064	81.23	
43.084886	-70.813292	81.62	
43.085129	-70.813496	81.26	
	Latitude deg 43.085129 43.085227 43.085137 43.084986 43.084886 43.085129	Latitude         Longitude           deg         deg           43.085129         -70.813496           43.085227         -70.813254           43.085137         -70.813085           43.084986         -70.813064           43.084886         -70.813292           43.085129         -70.813496	

Name: WRHSE2 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation	
	deg	deg	ft	
1	43.084916	-70.813107	81.43	
2	43.084740	-70.813499	81.62	
3	43.084705	-70.813466	81.64	
4	43.084630	-70.813662	81.71	
5	43.084174	-70.813292	81.76	
6	43.084399	-70.812785	81.68	
7	43.084501	-70.812860	81.70	
8	43.084540	-70.812758	81.66	
9	43.084916	-70.813107	81.43	

## Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	0	0	-	-
CRPRT4	0.0	124.0	0	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	10.0	214.0	0	0	-	-
SMBLDG	10.0	214.0	0	0	-	-

## PV & Receptor Analysis Results

Results for each PV array and receptor

## **CRPRT1** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

## **CRPRT2** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

## **CRPRT3** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

## **CRPRT4** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

## **CRPRT5** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

### SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi
  obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous
  modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
  PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, nc discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.



# ALBACORE, Portsmouth, NH ALBCR\_15Tilt\_124Carports\_NOObstrctns\_2ATCT\_AddOP

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112714.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



#### Misc. Analysis Settings

DNI: varies (1,000.0 W/m<sup>2</sup> peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

## Summary of Results Glare with low potential for temporary after-image predicted

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	1,543	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	1,314	0	-
CRPRT4	0.0	124.0	1,617	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	15.0	214.0	0	0	-
SMBLDG	15.0	214.0	0	0	-

### PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085400	-70.803418	56.90	22.48	79.38
2	43.085325	-70.803271	56.23	14.00	70.23
3	43.084876	-70.803716	58.56	14.00	72.56
4	43.084953	-70.803866	59.01	22.48	81.49

#### Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

#### Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 15.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 15.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
	8	43.084643	-70.803375	58.79	88.00	146.79

## Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67
#### Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation	
	deg	deg	ft	ft	ft	
1	43.082313	-70.799503	41.53	4.50	46.03	
2	43.082995	-70.798326	37.86	4.50	42.36	

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

## **Discrete Observation Receptors**

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation	
	deg	deg	ft	ft	ft	
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93	
OP 2	43.082455	-70.800057	42.02	20.00	62.02	
OP 3	43.082529	-70.799934	41.99	30.00	71.99	
OP 4	43.083085	-70.799471	39.01	6.00	45.01	
OP 5	43.083191	-70.799294	38.75	15.00	53.75	
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97	
OP 7	43.083312	-70.803940	70.10	40.00	110.10	

#### 1-ATCT map image



#### 6-ATCT map image



## **Obstruction Components**

#### Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation			
	deg	deg	ft			
1	43.085534	-70.803609	57.89			
2	43.085267	-70.803116	55.50			

Name: HighEdge2 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085593	-70.803598	57.75
2	43.085019	-70.804161	63.07

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation		
	deg	deg	ft		
1	43.085424	-70.803445	56.71		
2	43.084960	-70.803895	59.16		

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation		
	deg	deg	ft		
1	43.084674	-70.803390	58.96		
2	43.084478	-70.802983	56.11		
3	43.084211	-70.803240	59.29		
4	43.084415	-70.803648	62.46		
5	43.084674	-70.803390	58.96		

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

# Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	1,543	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	1,314	0	-	-
CRPRT4	0.0	124.0	1,617	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	15.0	214.0	0	0	-	-
SMBLDG	15.0	214.0	0	0	-	-

#### Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

PV	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
crprt1 (green)	0	0	105	292	0	0	0	81	319	0	0	0
crprt1 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt3 (green)	0	88	142	137	0	0	0	1	281	86	0	0
crprt3 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt4 (green)	0	139	219	103	0	0	0	0	273	187	0	0
crprt4 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0

## PV & Receptor Analysis Results

Results for each PV array and receptor

## **CRPRT1** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	783	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	760	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

## **CRPRT1: 1-ATCT**

- PV array is expected to produce the following glare for this receptor:
  783 minutes of "green" glare with low potential to cause temporary after-image.
  0 minutes of "yellow" glare with potential to cause temporary after-image.







### CRPRT1: OP 2

No glare found

#### CRPRT1: OP 3

No glare found

#### CRPRT1: OP 4

No glare found

#### CRPRT1: OP 5

No glare found

### **CRPRT1: 6-ATCT**

- PV array is expected to produce the following glare for this receptor: 760 minutes of "green" glare with low potential to cause temporary after-image.
  - 0 minutes of "yellow" glare with potential to cause temporary after-image.







### CRPRT1: OP 7

No glare found

#### **CRPRT1: Route 1**

No glare found

#### CRPRT1: Route 2

No glare found

#### **CRPRT1: Route 3**

No glare found

#### **CRPRT1: Route 4**

No glare found

## **CRPRT1: Route 5**

No glare found

## **CRPRT1: Route 6**

No glare found



Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

# **CRPRT3** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	548	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	530	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	78	0
Route: Route 4	158	0
Route: Route 5	0	0
Route: Route 6	0	0

### **CRPRT3: 1-ATCT**

- PV array is expected to produce the following glare for this receptor:
  548 minutes of "green" glare with low potential to cause temporary after-image.
  0 minutes of "yellow" glare with potential to cause temporary after-image.







### CRPRT3: OP 2

No glare found

### CRPRT3: OP 3

No glare found

#### CRPRT3: OP 4

No glare found

#### CRPRT3: OP 5

No glare found

### **CRPRT3: 6-ATCT**

- PV array is expected to produce the following glare for this receptor:
  530 minutes of "green" glare with low potential to cause temporary after-image.
  0 minutes of "yellow" glare with potential to cause temporary after-image.







#### CRPRT3: OP 7

No glare found

#### **CRPRT3: Route 1**

No glare found

#### CRPRT3: Route 2

No glare found

#### **CRPRT3: Route 3**

PV array is expected to produce the following glare for this receptor: • 78 minutes of "green" glare with low potential to cause temporary after-image.

- 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### **CRPRT3: Route 4**

PV array is expected to produce the following glare for this receptor:

- 158 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### **CRPRT3: Route 5**

No glare found

#### **CRPRT3: Route 6**

No glare found

#### **CRPRT4** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	532	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	514	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	314	0
Route: Route 4	257	0
Route: Route 5	0	0
Route: Route 6	0	0

### **CRPRT4: 1-ATCT**

- PV array is expected to produce the following glare for this receptor: 532 minutes of "green" glare with low potential to cause temporary after-image.
  - 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### CRPRT4: OP 2

No glare found

#### CRPRT4: OP 3

No glare found

#### CRPRT4: OP 4

No glare found

#### CRPRT4: OP 5

No glare found

#### **CRPRT4: 6-ATCT**

PV array is expected to produce the following glare for this receptor:

- 514 minutes of "green" glare with low potential to cause temporary after-image.
  0 minutes of "yellow" glare with potential to cause temporary after-image.







#### CRPRT4: OP 7

No glare found

#### **CRPRT4: Route 1**

No glare found

### CRPRT4: Route 2

No glare found

### CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 314 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 257 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







### CRPRT4: Route 5

No glare found

#### CRPRT4: Route 6

No glare found

## **CRPRT5** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

# LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

### SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

#### No glare found

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
  PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no discrete, spectrum.
- · Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.



# ALBACORE, Portsmouth, NH ALBCR\_10Tilt\_124Carports\_Obstrctns\_2ATCT\_AddOP

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112715.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



#### Misc. Analysis Settings

DNI: varies (1,000.0 W/m<sup>2</sup> peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

## Summary of Results No glare predicted!

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	0	0	-
CRPRT4	0.0	124.0	0	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	10.0	214.0	0	0	-
SMBLDG	10.0	214.0	0	0	-

#### PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085400	-70.803418	56.90	22.48	79.38
2	43.085325	-70.803271	56.23	14.00	70.23
3	43.084876	-70.803716	58.56	14.00	72.56
4	43.084953	-70.803866	59.01	22.48	81.49

#### Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

#### Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg	Ventex	deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
	8	43.084643	-70.803375	58.79	88.00	146.79

## Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

#### Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation	
	deg	deg	ft	ft	ft	
1	43.082313	-70.799503	41.53	4.50	46.03	
2	43.082995	-70.798326	37.86	4.50	42.36	

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

## **Discrete Observation Receptors**

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083343	-70.803962	70.10	40.00	110.10

#### 1-ATCT map image



#### 6-ATCT map image



## **Obstruction Components**

Name: BLDG2 Upper edge height: 20.0 ft	Vertex	Latitude	Longitude	Ground elevation
		deg	deg	ft
	1	43.084955	-70.806346	99.52
	2	43.085031	-70.806408	98.08
	3	43.084866	-70.806801	99.55
	4	43.084555	-70.806565	99.98
	5	43.084608	-70.806439	99.85
	6	43.084444	-70.806325	99.64
	7	43.084592	-70.806011	99.08
	8	43.084965	-70.806346	99.43
Google & GeoListary, Maxer Technologies, U.S. Geological Survey, USEAFPAC CED				

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.085593	-70.803598	57.75
43.085019	-70.804161	63.07
	Latitude deg 43.085593 43.085019	Latitude         Longitude           deg         deg           43.085593         -70.803598           43.085019         -70.804161

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PLANTING Upper edge height: 9.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085446	-70.804721	64.24
2	43.084717	-70.804268	69.47
3	43.084592	-70.804158	69.46

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

Name: TREELINE Upper edge height: 35.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085036	-70.807176	92.20
2	43.084131	-70.806567	95.41

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees1 Upper edge height: 40.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084443	-70.818109	84.34
2	43.084602	-70.818167	84.74
3	43.084354	-70.818474	88.75

Name: Trees3 Upper edge height: 100.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084287	-70.810576	72.89
2	43.084550	-70.810195	75.28

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation	
	deg	deg	ft	
1	43.085286	-70.814633	80.07	
2	43.083793	-70.813418	79.96	

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Latitude	Longitude	Ground elevation	
deg	deg	ft	
43.085129	-70.813496	81.26	
43.085227	-70.813254	81.50	
43.085137	-70.813085	81.35	
43.084986	-70.813064	81.23	
43.084886	-70.813292	81.62	
43.085129	-70.813496	81.26	
	Latitude deg 43.085129 43.085227 43.085137 43.084986 43.084886 43.085129	Latitude         Longitude           deg         deg           43.085129         -70.813496           43.085227         -70.813254           43.085137         -70.813085           43.084986         -70.813064           43.084886         -70.813292           43.085129         -70.813496	

Name: WRHSE2 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation	
	deg	deg	ft	
1	43.084916	-70.813107	81.43	
2	43.084740	-70.813499	81.62	
3	43.084705	-70.813466	81.64	
4	43.084630	-70.813662	81.71	
5	43.084174	-70.813292	81.76	
6	43.084399	-70.812785	81.68	
7	43.084501	-70.812860	81.70	
8	43.084540	-70.812758	81.66	
9	43.084916	-70.813107	81.43	

# Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	0	0	-	-
CRPRT4	0.0	124.0	0	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	10.0	214.0	0	0	-	-
SMBLDG	10.0	214.0	0	0	-	-

# PV & Receptor Analysis Results

Results for each PV array and receptor

**CRPRT1** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

**CRPRT2** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

# **CRPRT3** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

CRPRT4 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

# **CRPRT5** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

## SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
  Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated. The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. . Actual values and results may vary.

- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous • modeling methods. Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
- PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no • discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.



# ALBACORE, Portsmouth, NH ALBCR\_5Tilt\_124Carports\_Obstrctns\_2ATCT\_NoPlant

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112718.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



#### Misc. Analysis Settings

DNI: varies (1,000.0 W/m<sup>2</sup> peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

## Summary of Results Glare with low potential for temporary after-image predicted

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	236	0	-
CRPRT4	0.0	124.0	566	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	5.0	214.0	0	0	-
SMBLDG	5.0	214.0	0	0	-

#### PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085400	-70.803418	56.90	22.48	79.38
2	43.085325	-70.803271	56.23	14.00	70.23
3	43.084876	-70.803716	58.56	14.00	72.56
4	43.084953	-70.803866	59.01	22.48	81.49

#### Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

#### Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating

Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 5.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation	
	deg	deg	ft	ft	ft	
1	43.084344	-70.802133	51.60	93.83	145.44	
2	43.084054	-70.801543	49.18	93.83	143.01	
3	43.083901	-70.801690	49.39	93.83	143.22	
4	43.083859	-70.801609	49.20	93.83	143.03	
5	43.083897	-70.801574	49.27	93.83	143.10	
6	43.083839	-70.801453	47.35	93.83	141.18	
7	43.083345	-70.801919	51.93	93.83	145.76	
8	43.083906	-70.803019	59.40	93.83	153.23	
9	43.084395	-70.802537	54.24	93.83	148.07	
10	43.084315	-70.802368	51.53	93.83	145.36	
11	43.084337	-70.802347	51.04	93.83	144.87	
12	43.084303	-70.802278	52.48	93.83	146.31	
13	43.084336	-70.802245	52.51	93.83	146.34	
14	43.084297	-70.802171	51.69	93.83	145.52	
Name: SMBLDG						
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Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation)						
Orientation: 214.0 deg		deg	deg	π	n	n
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
COMPACT IN ANALYSING STATES	8	43.084643	-70.803375	58.79	88.00	146.79

# Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

#### Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation	
	deg	deg	ft	ft	ft	
1	43.082313	-70.799503	41.53	4.50	46.03	
2	43.082995	-70.798326	37.86	4.50	42.36	

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

# **Discrete Observation Receptors**

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083343	-70.803962	70.10	40.00	110.10

#### 1-ATCT map image



#### 6-ATCT map image



# **Obstruction Components**

Name: BLDG2 Upper edge height: 20.0 ft	Vertex	Latitude	Longitude	Ground elevation
		deg	deg	ft
	1	43.084955	-70.806346	99.52
	2	43.085031	-70.806408	98.08
	3	43.084866	-70.806801	99.55
	4	43.084555	-70.806565	99.98
	5	43.084608	-70.806439	99.85
	6	43.084444	-70.806325	99.64
	7	43.084592	-70.806011	99.08
	8	43.084965	-70.806346	99.43
Google & GeoListary, Maxer Technologies, U.S. Geological Survey, USEAFPAC CED				

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.085593	-70.803598	57.75
43.085019	-70.804161	63.07
	Latitude deg 43.085593 43.085019	Latitude         Longitude           deg         deg           43.085593         -70.803598           43.085019         -70.804161

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

Name: TREELINE Upper edge height: 35.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085036	-70.807176	92.20
2	43.084131	-70.806567	95.41

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees1 Upper edge height: 40.0 ft



deg deg ft	Vertex	Latitude	Longitude	Ground elevation
4 42.005064 70.046070 04.00		deg	deg	ft
1 43.085261 -70.816979 84.00	1	43.085261	-70.816979	84.00
2 43.084955 -70.816877 84.48	2	43.084955	-70.816877	84.48
3 43.084477 -70.817247 78.24	3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084443	-70.818109	84.34
2	43.084602	-70.818167	84.74
3	43.084354	-70.818474	88.75

Name: Trees3 Upper edge height: 100.0 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.084287	-70.810576	72.89
43.084550	-70.810195	75.28
	Latitude deg 43.084287 43.084550	Latitude         Longitude           deg         deg           43.084287         -70.810576           43.084550         -70.810195

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085286	-70.814633	80.07
2	43.083793	-70.813418	79.96

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation		
	deg	deg	ft		
1	43.085129	-70.813496	81.26		
2	43.085227	-70.813254	81.50		
3	43.085137	-70.813085	81.35		
4	43.084986	-70.813064	81.23		
5	43.084886	-70.813292	81.62		
6	43.085129	-70.813496	81.26		

#### Name: WRHSE2 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation	
	deg	deg	ft	
1	43.084916	-70.813107	81.43	
2	43.084740	-70.813499	81.62	
3	43.084705	-70.813466	81.64	
4	43.084630	-70.813662	81.71	
5	43.084174	-70.813292	81.76	
6	43.084399	-70.812785	81.68	
7	43.084501	-70.812860	81.70	
8	43.084540	-70.812758	81.66	
9	43.084916	-70.813107	81.43	

# Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	236	0	-	-
CRPRT4	0.0	124.0	566	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	5.0	214.0	0	0	-	-
SMBLDG	5.0	214.0	0	0	-	-

## Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

PV	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
crprt3 (green)	0	87	0	0	0	0	0	0	0	85	0	0
crprt3 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt4 (green)	0	139	48	0	0	0	0	0	0	186	0	0
crprt4 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0

# PV & Receptor Analysis Results

Results for each PV array and receptor

# **CRPRT1** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

# **CRPRT2** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

# **CRPRT3** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	79	0
Route: Route 4	157	0
Route: Route 5	0	0
Route: Route 6	0	0

### **CRPRT3: 1-ATCT**

No glare found

# CRPRT3: OP 2

No glare found

# CRPRT3: OP 3

No glare found

### CRPRT3: OP 4

No glare found

### CRPRT3: OP 5

No glare found

### CRPRT3: 6-ATCT

No glare found

# CRPRT3: OP 7

No glare found

# CRPRT3: Route 1

No glare found

### CRPRT3: Route 2

No glare found

## **CRPRT3: Route 3**

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image. 0 minutes of "yellow" glare with potential to cause temporary after-image. •







## CRPRT3: Route 4

- PV array is expected to produce the following glare for this receptor: 157 minutes of "green" glare with low potential to cause temporary after-image.
  - 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### **CRPRT3: Route 5**

No glare found

### CRPRT3: Route 6

No glare found

# **CRPRT4** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	311	0
Route: Route 4	255	0
Route: Route 5	0	0
Route: Route 6	0	0

# CRPRT4: 1-ATCT

No glare found

# CRPRT4: OP 2

No glare found

# CRPRT4: OP 3

No glare found

# CRPRT4: OP 4

No glare found

# CRPRT4: OP 5

No glare found

# CRPRT4: 6-ATCT

No glare found

### CRPRT4: OP 7

No glare found

## CRPRT4: Route 1

No glare found

# CRPRT4: Route 2

No glare found

## CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







### **CRPRT4: Route 4**

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







# CRPRT4: Route 5

No glare found

### CRPRT4: Route 6

No glare found

# **CRPRT5** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

# LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

# SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

#### No glare found

# Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
  PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no discrete, spectrum.
- · Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.



# ALBACORE, Portsmouth, NH ALBCR\_10Tilt\_124Carports\_Obstrctns\_2ATCT\_NoPlant

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112717.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



#### Misc. Analysis Settings

DNI: varies (1,000.0 W/m<sup>2</sup> peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

# Summary of Results Glare with low potential for temporary after-image predicted

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	236	0	-
CRPRT4	0.0	124.0	566	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	10.0	214.0	0	0	-
SMBLDG	10.0	214.0	0	0	-

### PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085400	-70.803418	56.90	22.48	79.38
2	43.085325	-70.803271	56.23	14.00	70.23
3	43.084876	-70.803716	58.56	14.00	72.56
4	43.084953	-70.803866	59.01	22.48	81.49

#### Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

#### Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg	Ventex	deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
	8	43.084643	-70.803375	58.79	88.00	146.79

# Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

#### Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation	
	deg	deg	ft	ft	ft	
1	43.082313	-70.799503	41.53	4.50	46.03	
2	43.082995	-70.798326	37.86	4.50	42.36	

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

# **Discrete Observation Receptors**

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083343	-70.803962	70.10	40.00	110.10

#### 1-ATCT map image



#### 6-ATCT map image



# **Obstruction Components**

Name: BLDG2 Upper edge height: 20.0 ft	Vertex	Latitude	Longitude	Ground elevation
		deg	deg	ft
	1	43.084955	-70.806346	99.52
	2	43.085031	-70.806408	98.08
	3	43.084866	-70.806801	99.55
	4	43.084555	-70.806565	99.98
	5	43.084608	-70.806439	99.85
	6	43.084444	-70.806325	99.64
	7	43.084592	-70.806011	99.08
	8	43.084965	-70.806346	99.43
Google & GeoListary, Maxer Technologies, U.S. Geological Survey, USEAFPAC CED				

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.085593	-70.803598	57.75
43.085019	-70.804161	63.07
	Latitude deg 43.085593 43.085019	Latitude         Longitude           deg         deg           43.085593         -70.803598           43.085019         -70.804161

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

Name: TREELINE Upper edge height: 35.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62
2	43.084095	-70.811240	67.62

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085036	-70.807176	92.20
2	43.084131	-70.806567	95.41

Name: Trees1 Upper edge height: 40.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084443	-70.818109	84.34
2	43.084602	-70.818167	84.74
3	43.084354	-70.818474	88.75

Name: Trees3 Upper edge height: 100.0 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.084287	-70.810576	72.89
43.084550	-70.810195	75.28
	Latitude deg 43.084287 43.084550	Latitude         Longitude           deg         deg           43.084287         -70.810576           43.084550         -70.810195

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation		
	deg	deg	ft		
1	43.085286	-70.814633	80.07		
2	43.083793	-70.813418	79.96		

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26

#### Name: WRHSE2 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084916	-70.813107	81.43
2	43.084740	-70.813499	81.62
3	43.084705	-70.813466	81.64
4	43.084630	-70.813662	81.71
5	43.084174	-70.813292	81.76
6	43.084399	-70.812785	81.68
7	43.084501	-70.812860	81.70
8	43.084540	-70.812758	81.66
9	43.084916	-70.813107	81.43

# Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	236	0	-	-
CRPRT4	0.0	124.0	566	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	10.0	214.0	0	0	-	-
SMBLDG	10.0	214.0	0	0	-	-

### Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

PV	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
crprt3 (green)	0	87	0	0	0	0	0	0	0	85	0	0
crprt3 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt4 (green)	0	139	48	0	0	0	0	0	0	186	0	0
crprt4 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0

# PV & Receptor Analysis Results

Results for each PV array and receptor

# **CRPRT1** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

# **CRPRT2** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

# **CRPRT3** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	79	0
Route: Route 4	157	0
Route: Route 5	0	0
Route: Route 6	0	0

### **CRPRT3: 1-ATCT**

No glare found

# CRPRT3: OP 2

No glare found

# CRPRT3: OP 3

No glare found

### CRPRT3: OP 4

No glare found

### CRPRT3: OP 5

No glare found

### CRPRT3: 6-ATCT

No glare found

# CRPRT3: OP 7

No glare found

# CRPRT3: Route 1

No glare found

### CRPRT3: Route 2

No glare found

## **CRPRT3: Route 3**

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image. 0 minutes of "yellow" glare with potential to cause temporary after-image. •







## CRPRT3: Route 4

- PV array is expected to produce the following glare for this receptor: 157 minutes of "green" glare with low potential to cause temporary after-image.
  - 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### **CRPRT3: Route 5**

No glare found

### CRPRT3: Route 6

No glare found

# **CRPRT4** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	311	0
Route: Route 4	255	0
Route: Route 5	0	0
Route: Route 6	0	0

# CRPRT4: 1-ATCT

No glare found

# CRPRT4: OP 2

No glare found

# CRPRT4: OP 3

No glare found

# CRPRT4: OP 4

No glare found

# CRPRT4: OP 5

No glare found

# CRPRT4: 6-ATCT

No glare found

### CRPRT4: OP 7

No glare found

## CRPRT4: Route 1

No glare found

# CRPRT4: Route 2

No glare found

## CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







### **CRPRT4: Route 4**

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







# CRPRT4: Route 5

No glare found

### CRPRT4: Route 6

No glare found

# **CRPRT5** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

# LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

# SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

#### No glare found

# Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
  PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no discrete, spectrum.
- · Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.


# ALBACORE, Portsmouth, NH ALBCR\_13Tilt\_124Carports\_Obstrctns\_2ATCT\_NoPlant

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112727.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



#### Misc. Analysis Settings

DNI: varies (1,000.0 W/m<sup>2</sup> peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

## Summary of Results Glare with low potential for temporary after-image predicted

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	236	0	-
CRPRT4	0.0	124.0	566	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	13.0	214.0	0	0	-
SMBLDG	13.0	214.0	0	0	-

### PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085400	-70.803418	56.90	22.48	79.38
2	43.085325	-70.803271	56.23	14.00	70.23
3	43.084876	-70.803716	58.56	14.00	72.56
4	43.084953	-70.803866	59.01	22.48	81.49

#### Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

#### Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 13.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 13.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
A CALL AND A CALL	7	43.084414	-70.803594	61.58	88.00	149.58
	8	43.084643	-70.803375	58.79	88.00	146.79

## Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

#### Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation	
	deg	deg	ft	ft	ft	
1	43.082313	-70.799503	41.53	4.50	46.03	
2	43.082995	-70.798326	37.86	4.50	42.36	

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

## **Discrete Observation Receptors**

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083343	-70.803962	70.10	40.00	110.10

#### 1-ATCT map image



#### 6-ATCT map image



## **Obstruction Components**

Name: BLDG2 Upper edge height: 20.0 ft	Vertex	Latitude	Longitude	Ground elevation
		deg	deg	ft
	1	43.084955	-70.806346	99.52
	2	43.085031	-70.806408	98.08
	3	43.084866	-70.806801	99.55
	4	43.084555	-70.806565	99.98
	5	43.084608	-70.806439	99.85
	6	43.084444	-70.806325	99.64
	7	43.084592	-70.806011	99.08
	8	43.084965	-70.806346	99.43
Google & GeoListary, Maxer Technologies, U.S. Geological Survey, USEAFPAC CED				

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.085593	-70.803598	57.75
43.085019	-70.804161	63.07
	Latitude deg 43.085593 43.085019	Latitude         Longitude           deg         deg           43.085593         -70.803598           43.085019         -70.804161

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

Name: TREELINE Upper edge height: 35.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085036	-70.807176	92.20
2	43.084131	-70.806567	95.41

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees1 Upper edge height: 40.0 ft



deg deg ft	Vertex	Latitude	Longitude	Ground elevation
4 42.005064 70.046070 04.00		deg	deg	ft
1 43.085261 -70.816979 84.00	1	43.085261	-70.816979	84.00
2 43.084955 -70.816877 84.48	2	43.084955	-70.816877	84.48
3 43.084477 -70.817247 78.24	3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Vertex	Latitude	Longitude	Ground elevation		
	deg	deg	ft		
1	43.084443	-70.818109	84.34		
2	43.084602	-70.818167	84.74		
3	43.084354	-70.818474	88.75		

Name: Trees3 Upper edge height: 100.0 ft



Latitude	Longitude	Ground elevation		
deg	deg	ft		
43.084287	-70.810576	72.89		
43.084550	-70.810195	75.28		
	Latitude deg 43.084287 43.084550	Latitude         Longitude           deg         deg           43.084287         -70.810576           43.084550         -70.810195		

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation		
	deg	deg	ft		
1	43.085286	-70.814633	80.07		
2	43.083793	-70.813418	79.96		

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26

#### Name: WRHSE2 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084916	-70.813107	81.43
2	43.084740	-70.813499	81.62
3	43.084705	-70.813466	81.64
4	43.084630	-70.813662	81.71
5	43.084174	-70.813292	81.76
6	43.084399	-70.812785	81.68
7	43.084501	-70.812860	81.70
8	43.084540	-70.812758	81.66
9	43.084916	-70.813107	81.43

# Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	236	0	-	-
CRPRT4	0.0	124.0	566	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	13.0	214.0	0	0	-	-
SMBLDG	13.0	214.0	0	0	-	-

### Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

PV	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
crprt3 (green)	0	87	0	0	0	0	0	0	0	85	0	0
crprt3 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt4 (green)	0	139	48	0	0	0	0	0	0	186	0	0
crprt4 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0

# PV & Receptor Analysis Results

Results for each PV array and receptor

## **CRPRT1** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

## **CRPRT2** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

## **CRPRT3** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	79	0
Route: Route 4	157	0
Route: Route 5	0	0
Route: Route 6	0	0

### **CRPRT3: 1-ATCT**

No glare found

## CRPRT3: OP 2

No glare found

## CRPRT3: OP 3

No glare found

#### CRPRT3: OP 4

No glare found

### CRPRT3: OP 5

No glare found

### CRPRT3: 6-ATCT

No glare found

## CRPRT3: OP 7

No glare found

## CRPRT3: Route 1

No glare found

#### CRPRT3: Route 2

No glare found

## **CRPRT3: Route 3**

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image. 0 minutes of "yellow" glare with potential to cause temporary after-image. •







## CRPRT3: Route 4

- PV array is expected to produce the following glare for this receptor: 157 minutes of "green" glare with low potential to cause temporary after-image.
  - 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### **CRPRT3: Route 5**

No glare found

#### **CRPRT3: Route 6**

No glare found

## **CRPRT4** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	311	0
Route: Route 4	255	0
Route: Route 5	0	0
Route: Route 6	0	0

## CRPRT4: 1-ATCT

No glare found

## CRPRT4: OP 2

No glare found

## CRPRT4: OP 3

No glare found

## CRPRT4: OP 4

No glare found

## CRPRT4: OP 5

No glare found

## CRPRT4: 6-ATCT

No glare found

### CRPRT4: OP 7

No glare found

## CRPRT4: Route 1

No glare found

## CRPRT4: Route 2

No glare found

## CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### **CRPRT4: Route 4**

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







## CRPRT4: Route 5

No glare found

### CRPRT4: Route 6

No glare found

## **CRPRT5** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

# LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

## SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

#### No glare found

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
  PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no discrete, spectrum.
- · Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.



# ALBACORE, Portsmouth, NH ALBCR\_15Tilt\_124Carports\_Obstrctns\_2ATCT\_NoPlant

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112723.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



#### Misc. Analysis Settings

DNI: varies (1,000.0 W/m<sup>2</sup> peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

## Summary of Results Glare with low potential for temporary after-image predicted

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	236	0	-
CRPRT4	0.0	124.0	566	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	15.0	214.0	0	0	-
SMBLDG	15.0	214.0	0	0	-

### PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085400	-70.803418	56.90	22.48	79.38
2	43.085325	-70.803271	56.23	14.00	70.23
3	43.084876	-70.803716	58.56	14.00	72.56
4	43.084953	-70.803866	59.01	22.48	81.49

#### Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

#### Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 15.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 15.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
	8	43.084643	-70.803375	58.79	88.00	146.79

## Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

#### Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation	
	deg	deg	ft	ft	ft	
1	43.082313	-70.799503	41.53	4.50	46.03	
2	43.082995	-70.798326	37.86	4.50	42.36	

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

## **Discrete Observation Receptors**

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083343	-70.803962	70.10	40.00	110.10

#### 1-ATCT map image



#### 6-ATCT map image



## **Obstruction Components**

Name: BLDG2 Upper edge height: 20.0 ft	Vertex	Latitude	Longitude	Ground elevation
		deg	deg	ft
	1	43.084955	-70.806346	99.52
	2	43.085031	-70.806408	98.08
	3	43.084866	-70.806801	99.55
	4	43.084555	-70.806565	99.98
	5	43.084608	-70.806439	99.85
	6	43.084444	-70.806325	99.64
	7	43.084592	-70.806011	99.08
	8	43.084965	-70.806346	99.43
Google & GeoListary, Maxer Technologies, U.S. Geological Survey, USEAFPAC CED				

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.085593	-70.803598	57.75
43.085019	-70.804161	63.07
	Latitude deg 43.085593 43.085019	Latitude         Longitude           deg         deg           43.085593         -70.803598           43.085019         -70.804161

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

Name: TREELINE Upper edge height: 35.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62
2	43.084095	-70.811240	67.62

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085036	-70.807176	92.20
2	43.084131	-70.806567	95.41

Name: Trees1 Upper edge height: 40.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084443	-70.818109	84.34
2	43.084602	-70.818167	84.74
3	43.084354	-70.818474	88.75

Name: Trees3 Upper edge height: 100.0 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.084287	-70.810576	72.89
43.084550	-70.810195	75.28
	Latitude deg 43.084287 43.084550	Latitude         Longitude           deg         deg           43.084287         -70.810576           43.084550         -70.810195

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085286	-70.814633	80.07
2	43.083793	-70.813418	79.96

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26

#### Name: WRHSE2 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation		
	deg	deg	ft		
1	43.084916	-70.813107	81.43		
2	43.084740	-70.813499	81.62		
3	43.084705	-70.813466	81.64		
4	43.084630	-70.813662	81.71		
5	43.084174	-70.813292	81.76		
6	43.084399	-70.812785	81.68		
7	43.084501	-70.812860	81.70		
8	43.084540	-70.812758	81.66		
9	43.084916	-70.813107	81.43		

# Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	236	0	-	-
CRPRT4	0.0	124.0	566	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	15.0	214.0	0	0	-	-
SMBLDG	15.0	214.0	0	0	-	-

### Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

PV	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
crprt3 (green)	0	87	0	0	0	0	0	0	0	85	0	0
crprt3 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt4 (green)	0	139	48	0	0	0	0	0	0	186	0	0
crprt4 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0

# PV & Receptor Analysis Results

Results for each PV array and receptor

## **CRPRT1** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

## **CRPRT2** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

## **CRPRT3** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	79	0
Route: Route 4	157	0
Route: Route 5	0	0
Route: Route 6	0	0

### **CRPRT3: 1-ATCT**

No glare found

## CRPRT3: OP 2

No glare found

## CRPRT3: OP 3

No glare found

#### CRPRT3: OP 4

No glare found

### CRPRT3: OP 5

No glare found

### CRPRT3: 6-ATCT

No glare found

## CRPRT3: OP 7

No glare found

## CRPRT3: Route 1

No glare found

#### CRPRT3: Route 2

No glare found

## **CRPRT3: Route 3**

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image. 0 minutes of "yellow" glare with potential to cause temporary after-image. •







## CRPRT3: Route 4

- PV array is expected to produce the following glare for this receptor: 157 minutes of "green" glare with low potential to cause temporary after-image.
  - 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### **CRPRT3: Route 5**

No glare found

#### CRPRT3: Route 6

No glare found

## **CRPRT4** low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	311	0
Route: Route 4	255	0
Route: Route 5	0	0
Route: Route 6	0	0
## CRPRT4: 1-ATCT

No glare found

## CRPRT4: OP 2

No glare found

## CRPRT4: OP 3

No glare found

## CRPRT4: OP 4

No glare found

#### CRPRT4: OP 5

No glare found

### CRPRT4: 6-ATCT

No glare found

#### CRPRT4: OP 7

No glare found

#### CRPRT4: Route 1

No glare found

#### CRPRT4: Route 2

No glare found

#### CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### **CRPRT4: Route 4**

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







#### CRPRT4: Route 5

No glare found

#### CRPRT4: Route 6

No glare found

## **CRPRT5** no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

# LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

#### SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

#### No glare found

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
  PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no discrete, spectrum.
- · Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.



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