# PLANNING BOARD <br> PORTSMOUTH, NEW HAMPSHIRE 

# EILEEN DONDERO FOLEY COUNCIL CHAMBERS <br> CITY HALL, MUNICIPAL COMPLEX, 1 JUNKINS AVENUE 

7:00 PM Public Hearings begin
July 18, 2024

## AGENDA

## REGULAR MEETING 7:00pm

## I. APPROVAL OF MINUTES

A. Approval of the June 20, 2024 meeting minutes.

## II. PUBLIC HEARINGS - NEW BUSINESS

The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
A. REQUEST TO POSTPONE The request of Perkins Kwoka Joint Revocable Trust (Owner), for property located at 224 Broad Street, Unit 3 is requesting a Wetland Conditional Use Permit from Section 10.1017.50 for the replacement and expansion of an existing 192 s.f. sunroom and the demolition of a 286 s.f. rear deck, with new construction proposed for an addition of 384 s.f. to the existing sunroom, a new 367.5 s.f. rear deck and regrading of a portion of the site for the installation of a retaining wall and underdrain for stormwater control. The applicant is proposing to remove 491 s.f. of existing pavers and asphalt to be replaced with 401 s.f. of new pavers. This proposal includes the removal of the existing lawn to be replaced with a micro-clover seed mix, a planting plan, and a stone drip edge. Said property is located on Assessor Map 131 Lot 13-3 and lies within the General Residence A (GRA) District. REQUEST TO POSTPONE (LU-23-179)
B. The request of Lonza Biologics (Owner), for property located at 5 Technology Way (Formerly 70 Corporate Drive) requesting Amended Site Plan approval for the addition of Phase Photovoltaic Cell (PV) Solar canopies over the previously approved temporary surface parking lot with associated utility infrastructure improvements. Said property is located on Assessor Map 305 Lot 6 and lies within the Airport Business (ABC) District. (LU-23-108)
C. The request of The City of Portsmouth (Owner), for property located at 50 Andrew Jarvis Drive requesting a Wetland Conditional Use Permit from Section 10.1017.50 of the Ordinance for the conversion of an existing practice field into a baseball and softball practice field which includes adding an 800 s.f. batting cage, a 40' wide backstop with posts driven into the ground, and the removal of approximately 800 s.f. of existing grass for replacement with an infield mix of clay, sand and silt. All of this work will occur within the 100 ' wetland buffer. Said property is located on Assessor Map 229 Lot 3 and lies within the Municipal (M) District. (LU-24-50)
D. The request of The City of Portsmouth (Owner), for property located at $\mathbf{0}$ Maplewood Avenue requesting an after the fact Wetland Conditional Use Permit from Section 10.1017 .50 of the Ordinance due to the emergency authorization issued by NHDES on May 16, 2024 for repair of the stone wall alongside the North Cemetery. This application is for the restoration and repair of the wall in-kind which includes installation of new stone, installing non-woven geotextile along the eroded bank, importing structural backfill, and loam and seeding the disturbed areas once finished. Said property is located on Assessor Map 124 Lot 2 and lies within the Municipal (M) District. (LU-24-102)
E. The request of Rosania RR \& KL Revocable Trust (Owner), for property located at 32 Boss Avenue requesting a Conditional Use Permit in accordance with Section 10.440, Use 19.22 for a Home Occupation 2. Said property is located on Assessor Map 153 Lot 5 and lies within the Single Residence B (SRB) District. (LU-24-117)
F. The request of Mark E. and Janet Greenwood (Owners), for property located at 480 Dennett Street requesting a Conditional Use Permit from Section 10.814 for a Detached Accessory Dwelling Unit (DADU) for the demolition of the existing garage and construction of a new DADU Said property is located on Assessor Map 160 Lot 26 and lies within the General Residence A (GRA) District. (LU-24-120)
G. The request of Portsmouth West End Development LLC (Owner), for property located at $\mathbf{1 2 5}$ Brewery Lane requesting a Conditional Use Permit in accordance with Section 10.440, Use 19.50 for an outdoor dining and drinking area as an accessory use. Said property is located on Assessor Map 154 Lot 2 and lies within the Character District 4-W (CD-4W) District. (LU-24-108)

## III. PRELIMINARY CONCEPTUAL CONSULTATION

A. The request of Frances E. Mouflouze Revocable Trust of 2015 (Owner), for property located at 550 Sagamore Avenue requesting preliminary Conceptual Consultation for a subdivision of one lot into three conforming lots with associated site improvements. Said property is located on Assessor Map 222 Lot 11 and lies within the Single Residence B (SRB) District. (LUPD-24-5)
B. 361 Hanover Steam Factory, LLC (Owner), for property located at 361 Hanover Street, requesting Preliminary Conceptual Consultation for the construction of three residential buildings along Hanover Street and add a fourth story with a penthouse to the existing 361 Hanover Street (Portsmouth Steam Factory) building for a total of 48 dwelling units including 3 workforce housing units and 69 parking spaces and associated community space. Said property is located on Assessor Map 138 Lot 63 and lies within the Character District 5 (CD5) Downtown Overlay and North End Overlay Districts. (LUPD-24-3)

## IV. OTHER BUSINESS

A. Chairman updates and discussion items
B. Planning Board Rules and Procedures
C. Board discussion of Regulatory Amendments, Master Plan Scope \& other matters

## V. ADJOURNMENT

*Members of the public also have the option to join this meeting over Zoom, a unique meeting ID and password will be provided once you register. To register, click on the link below or copy and paste this into your web browser:
https://us06web.zoom.us/webinar/register/WN AXjPB9HpRnaVn9EtKcrc2w


City of Portsmouth
Planning Department
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Portsmouth, NH
(603)610-7216

## Memorandum

To: Planning Board
From: Peter Stith, AICP
Planning Manager
Date: July 18, 2024
Re: Recommendations for the July 18, 2024 Planning Board Meeting

## I. APPROVAL OF MINUTES

A. Approval of the June 20, 2024 meeting minutes.

## Planning Department Recommendation

1) Board members should determine if the draft minutes include all relevant details for the decision-making process that occurred at the June 20, 2024 meeting and vote to approve meeting minutes with edits if needed.

## II. PUBLIC HEARINGS - NEW BUSINESS

The Board's action in these matters has been deemed to be quasi-judicial in nature.
If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
A. The request of Perkins Kwoka Joint Revocable Trust (Owner), for property located at $\mathbf{2 2 4}$ Broad Street, Unit $\mathbf{3}$ is requesting a Wetland Conditional Use Permit from Section 10.1017.50 for the replacement and expansion of an existing 192 s.f. sunroom and the demolition of a 286 s.f. rear deck, with new construction proposed for an addition of 384 s.f. to the existing sunroom, a new 367.5 s.f. rear deck and regrading of a portion of the site for the installation of a retaining wall and underdrain for stormwater control. The applicant is proposing to remove 491 s.f. of existing pavers and asphalt to be replaced with 401 s.f. of new pavers. This proposal includes the removal of the existing lawn to be replaced with a micro-clover seed mix, a planting plan, and a stone drip edge. Said property is located on Assessor Map 131Lot 13-3 and lies within the General Residence A (GRA) District. (LU-23-179)

## Background

This application is requesting a Wetland Conditional Use Permit for the replacement and expansion of an existing 192 s.f. sunroom and the demolition of a 286 s.f. rear deck, with new construction proposed for an addition of 384 s.f. to the existing sunroom, a new 367.5 s.f. rear deck and regrading of a portion of the site for the installation of a retaining wall and underdrain for stormwater control. Additionally, the applicant is proposing to remove 491 s.f. of existing pavers and asphalt to be replaced with 401 s.f. of new pavers. This proposal includes the removal of the existing lawn to be replaced with a microclover seed mix, an extensive planting plan, and a stone drip edge surrounding the new sunroom and deck.


Staff Analysis - Wetland CUP
According to Article 10 Section 10.1017.50 the applicant must satisfy the following conditions for approval of this utility project.

## 1. The land is reasonably suited to the use activity or alteration.

The existing site has a steep slope which has been directing stormwater into and around the existing home, instead of towards the adjacent wetland. The proposed stormwater controls will involve some regrading of the lawn and the redirection of stormwater away from the home and through an underdrain to outlet underneath the expanded deck. This proposed deck will have $3 / 4$ " spaced decking and will have crushed stone underneath for infiltration.
2. There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use, activity or alteration.
The majority of this property is within the 100 ft . buffer. The existing home is within the buffer and experiencing impacts of stormwater and ponding on the property. The applicant is proposing to address these issues with new stormwater controls and the addition of plantings, while working to reduce the impervious surface where possible.
3. There will be no adverse impact on the wetland functional values of the site
or surrounding properties.
The applicant is proposing to redirect stormwater directly through an underdrain and into a crushed stone area to slow infiltration. This should improve the flooding conditions for the home while directing the flow closer to the wetland with an option for infiltration into the soil.
4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals.
The applicant is proposing to maintain all existing trees and vegetation. In addition, the applicant will be improving the vegetation on site by planting a native micro-clover lawn in addition to planting beds and multiple trees and shrubs.

## 5. The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this section.

While the applicant is proposing an expansion of the home within the buffer, the expansion is occurring in the direction opposite of the wetland and will be compensated with a reduction in existing impervious. There are plans for overall improvements to the buffer including landscaping and reseeding the lawn with a micro-clover seed mix.
6. Any area within the vegetated buffer strip will be returned to a natural state to the extent feasible.

The applicant is proposing to stay completely outside of the $25^{\prime}$ vegetated buffer.

## Project Review, Decisions, and Recommendations

The applicant was before the Conservation Commission. See below for details.

## Conservation Commission

The applicant was before the Conservation Commission at its regularly scheduled meeting of Wednesday, April 10, 2024 and the Commission voted unanimously to recommend approval as presented.

## Planning Department Recommendation <br> Wetland Conditional Use Permit

1) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact as presented.
(Alt.) Vote to find that the Conditional Use Permit Application meets the requirements
set forth in Section 10.1017 .50 of the Ordinance and adopt the findings of fact as amended.
2.) Vote to grant the Conditional Use Permit as presented.

## III. PUBLIC HEARINGS - NEW BUSINESS

The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
B. The request of (Owner), for property located at 5 Technology Way (Formerly 70 Corporate Drive) requesting Amended Site Plan approval for the addition of Phase Photovoltaic Cell (PV) Solar canopies over the previously approved temporary surface parking lot with associated utility infrastructure improvements. Said property is located on Assessor Map 305 Lot 6 and lies within the Airport Business (ABC) District. (LU-23-108)

## Background

This application is seeking Amended Site Plan approval to add Solar canopies over the proposed surface parking lot area. The addition of the solar canopies will require electrical modifications and will result in no impact to the drainage design for the project.


## Project Review, Discussion, and Recommendations

The project was before the Technical Advisory Committee in June. See below for
details.
Technical Advisory Committee
The applicant was before TAC for at their regularly scheduled meeting of Tuesday, June 4, 2024 meeting. TAC voted to recommend that the Planning Board recommend approval to the Pease Development Authority as presented.

The amendments to RSA 676:3 with regards to adopting findings of fact for a project apply to local planning boards making decisions based on the municipality's regulations. Pease falls exclusively under RSA 12-G and the Pease Land Use Controls, therefore the requirement to vote on and adopt findings of fact do not apply for this application.

## Planning Department Recommendation

Site Plan Approval

1) Vote to recommend Amended Site Plan Approval to the PDA Board.

## III. PUBLIC HEARINGS - NEW BUSINESS

The Board's action in these matters has been deemed to be quasi-judicial in nature.
If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
C. The request of The City of Portsmouth (Owner), for property located at $\mathbf{5 0}$ Andrew Jarvis Drive requesting a Wetland Conditional Use Permit from Section 10.1017.50 of the Ordinance for the conversion of an existing practice field into a baseball and softball practice field which includes adding an 800 s.f. batting cage, a $40^{\prime}$ wide backstop with posts driven into the ground, and the removal of approximately 800 s.f. of existing grass for replacement with an infield mix of clay, sand and silt. All of this work will occur within the 100' wetland buffer. Said property is located on Assessor Map 229 Lot 3 and lies within the Municipal (M) District. (LU-24-50)

## Project Background

This application is for the conversion of an existing practice field into a more formalized baseball and softball practice field at the high school. The proposal includes the addition of an 800 s.f. batting cage, and a $40^{\prime}$ wide backstop with posts driven into the ground, and the removal of approximately 800 s.f. of existing grass for replacement with an infield mix of clay, sand and silt. All of this work will occur within the 100 ' wetland buffer, with additional grass removal and infield mix placement outside the 100 buffer.


Staff Analysis - Wetland CUP
According to Article 10 Section 10.1017 .50 the applicant must satisfy the following conditions for approval of this utility project.

## 1. The land is reasonably suited to the use activity or alteration.

This area is already heavily used as a recreation area for high school students and other recreation leagues. The addition of baseball/softball equipment will allow for more teams to utilize the space.
2. There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use, activity or alteration.
While there is an alternative location in this area that would create minimal disturbance and be outside the buffer, it would create a safety hazard due to its proximity to buildings and parking areas. The chosen location within the buffer is already used as a recreational field and it does not receive any harmful maintenance such as fertilizer or chemical use, only occasional mowing. The conversion to a baseball/softball field will not change how the buffer has been used historically.

## 3. There will be no adverse impact on the wetland functional values of the site or surrounding properties.

The infield mix proposed for the new field will be a permeable mix that should not have a noticeable impact on infiltration within this buffer area. The adjacent
wetland is well forested and should not see an impact from this field conversion.
4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals.
The only vegetation proposed to be removed is a portion of existing grass lawn. This will be replaced with a permeable sand/silt/clay infield mix.
5. The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this section.
The proposal minimizes impacts to the buffer by proposing a permeable infield mix and minimal permanent equipment. On-site alternatives would require greater disturbance to areas that are not already used as recreational fields.
6. Any area within the vegetated buffer strip will be returned to a natural state to the extent feasible.
No work is proposed within the $25^{\prime}$ vegetated buffer.

## Project Review, Decisions, and Recommendations

The applicant was before the Conservation Commission. See below for details.

## Conservation Commission

The applicant was before the Commission at its regularly scheduled meeting of Wednesday, June 12, 2024 and the Commission voted unanimously to recommend approval with the following conditions:

1. The updated Planning Board submission shall include the new batting cage location, the location of the new no-mow area, and the locations for wetland boundary placards.
2. In accordance with Section 10.1018.40 of the Zoning Ordinance, applicant shall permanently install wetland boundary markers, which may be purchased through the City of Portsmouth Planning \& Sustainability Department. Markers are to be placed along the 25' vegetative buffer at 50-foot intervals and must be installed prior to the start of any construction.

The Conservation Commission recommended conditions have been satisfied or added to the staff recommendation.

## Planning Department Recommendation <br> Wetland Conditional Use Permit

1) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017 .50 of the Ordinance and adopt the findings of fact as presented.
(Alt.) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact as amended.
2.) Vote to grant the Conditional Use Permit with the following conditions:
2.1) In accordance with Section 10.1018 .40 of the Zoning Ordinance, applicant shall install permanent wetland boundary markers where applicable. In addition to the wetland boundary markers, an educational sign describing the project shall be installed near the restoration area and fencing should be utilized to keep disturbances such as dogs and geese from the area.

## III. PUBLIC HEARINGS - NEW BUSINESS

The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
D. The request of The City of Portsmouth (Owner), for property located at $\mathbf{0}$ Maplewood Avenue requesting an after the fact Wetland Conditional Use Permit from Section 10.1017.50 of the Ordinance due to the emergency authorization issued by NHDES on May 16, 2024 for repair of the stone wall alongside the North Cemetery. This application is for the restoration and repair of the wall in-kind which includes installation of new stone, installing non-woven geotextile along the eroded bank, importing structural backfill, and loam and seeding the disturbed areas once finished. Said property is located on Assessor Map 124 Lot 2 and lies within the Municipal (M) District. (LU-24-102)

## Project Background

The is an after the fact wetland conditional use permit due to the emergency authorization for this work. The stone wall alongside the North Cemetery is in danger of collapse due to significant erosion along the bank and this application is for the restoration and repair of the wall in-kind which includes installation of new stone, installing non-woven geotextile along the eroded bank, importing structural backfill, and loam and seeding the disturbed areas once finished. Recent inspections of this site concluded that any future storm events or heavy rains could cause significant damage and irreversible harm to the stability of this wall and the contents behind it. Due to this, the City of Portsmouth Department of Public Works has obtained an emergency authorization to perform this work from NHDES and is now seeking a wetland conditional use permit.


Staff Analysis - Wetland CUP
According to Article 10 Section 10.1017 .50 the applicant must satisfy the following conditions for approval of this utility project.

## 1. The land is reasonably suited to the use activity or alteration.

This work is an in-kind repair job. The damaged wall is structurally integral to keeping the cemetery border and fill contained.
2. There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use, activity or alteration.
There is no alternative location to rebuild this wall in. The safety of the tomb and burials behind the wall is reliant on the structure of this wall and it must be fortified in order to prevent further erosion, or worse, collapse.

## 3. There will be no adverse impact on the wetland functional values of the site or surrounding properties.

The applicant used professional services to access the area and wall from the adjacent property, so as not to disturb the hallowed ground. This may have impacts on the pathway of any necessary construction vehicles. The applicant shall restore any disturbed soils with native wetland buffer conservation seed mix and monitor for establishment.

## 4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals.

The natural vegetated state was disturbed in order to get construction equipment onto the site. This area should be stabilized with erosion controls, along with the wall, and should be reseeded at the end of construction with a native wetland buffer conservation seed mix.

## 5. The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this section.

The alternatives to not repairing this wall would be allowing it, and the fill, and historic infrastructure to erode and/or slide into the North Mill Pond. The repair of this wall was an emergency repair.
6. Any area within the vegetated buffer strip will be returned to a natural state to the extent feasible.
All areas disturbed within the $25^{\prime}$ vegetated buffer shall be reseeded at the end of construction with a native wetland buffer conservation seed mix.

## Project Review, Decisions, and Recommendations

The applicant was before the Conservation Commission. See below for details.

## Conservation Commission

The applicant was before the Conservation Commission at its regularly scheduled meeting of Wednesday, June 12, 2024 and the Commission unanimously voted to recommend approval with the following conditions:

1. Applicant shall monitor the success of reseeded areas to ensure stabilization. If stabilization is not successful within 30 days of seeding, the area will need to be reseeded.
2. Native wetland buffer shrub plantings shall be installed within the temporary accessway area in the Fall of 2024. This should be included in updated plan set for the Planning Board submission.

## Planning Department Recommendation

## Wetland Conditional Use Permit

1) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017 .50 of the Ordinance and adopt the findings of fact as presented.
(Alt.) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact as amended.
2.) Vote to grant the Conditional Use Permit with the following conditions:
2.1) Applicant shall monitor the success of reseeded areas to ensure stabilization. If stabilization is not successful within 30 days of seeding, the area will need to be reseeded.
2.2) A planting plan of the temporary accessway area shall be submitted to the Planning \& Sustainability Department for review and approval.

## III. PUBLIC HEARINGS - NEW BUSINESS

The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
E. The request of Rosania RR \& KL Revocable Trust (Owner), for property located at 32 Boss Avenue requesting a Conditional Use Permit in accordance with Section 10.440, Use 19.22 for a Home Occupation 2. Said property is located on Assessor Map 153 Lot 5 and lies within the Single Residence B (SRB) District. (LU-24-117)

## Project Background

On June 17, 2024, the City Council adopted zoning amendments for home occupations. The amendments provide for client or general public visitation for a home occupation 1 and 2 , which were previously not permitted. A home occupation 1 can have up to 2 clients at one time and is permitted in all zoning districts. A home occupation 2 can have up to 6 clients at one time and requires a Conditional Use Permit (CUP) in residential districts. The definitions are below for your reference. Both types of home occupations must comply with the requirements in main definition below:

## Home occupation

An office or other use customarily conducted as an accessory use to a dwelling, complying with all the following standards:
(a) Conducted entirely within a dwelling or an existing accessory building, and with no change to the character of the dwelling or accessory building;
(b) Maximum floor area of 300 square feet;
(c) No outdoor storage of materials or products;
(d) Outdoor parking of no more than one vehicle related to the home occupation;
(e) No deliveries by vehicles with more than two axles.

## Home occupation 1

A home occupation with no nonresident employees; no sign related to the business; no more than 2 client, vendor or general public visitations at one time; and no deliveries other than by regular postal service and no more than one package delivery service truck (e.g., FedEx, UPS, etc.) per day.

## Home occupation 2

A home occupation with not more than one nonresident employee and not more than 6 client, vendor or general public visitations at one time.


## Project Review, Decisions, and Recommendations

The applicant is requesting a CUP for a home occupation 2 in an existing studio that is less than the 300 square foot maximum floor area for the use. While the applicant shows ample parking in the existing driveway, only one space can be designated for the home occupation use.

Per Section 10.860 Hours of Operation, a home occupation 2 is limited to the hours of 8 am -5 pm unless different hours are established under a special exception or conditional use permit. The applicant is requesting the ability to have up to 2 classes per week from $6-9 \mathrm{pm}$ and one day on the weekend.

## Planning Department Recommendation

## Home Occupation 2 Conditional Use Permit

1) Vote to find that the Conditional Use Permit application meets the criteria set forth in Section 10.243.20 and to adopt the findings of fact as presented.
(Alt.) Vote to find that the Conditional Use Permit application meets the criteria set forth in Section 10.243.20 and to adopt the findings of fact as amended and read into the record.
2) Vote to approve the conditional use permit with the following condition:
2.1) The home occupation may have up to 2 additional classes per week between the hours of $6-9 \mathrm{pm}$ and one day on the weekend between the hours of $8 \mathrm{am}-5 \mathrm{pm}$.

## III. PUBLIC HEARINGS - NEW BUSINESS

The Board's action in these matters has been deemed to be quasi-judicial in nature.
If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
F. The P The request of Mark E. and Janet Greenwood (Owners), for property located at 480 Dennett Street requesting a Conditional Use Permit from Section 10.814 for a Detached Accessory Dwelling Unit (DADU) for the demolition of the existing garage and construction of a new DADU Said property is located on Assessor Map 160 Lot 26 and lies within the General Residence A (GRA) District. (LU-24-120)

## Project Background

The applicant is proposing to demolish the existing nonconforming garage and construct a new Detached Accessory Dwelling Unit (DADU) that will conform to the dimensional requirements in the GRA. The proposed DADU will be 750 sq . ft . and comply with all other dimensional and design requirements for a DADU.


## Planning Department Recommendation

## Detached Accessory Dwelling Unit Conditional Use Permit

1) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.814.62 of the Ordinance and adopt the findings of fact as presented.
(Alt.) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.814.62 of the Ordinance and adopt the findings of fact as amended.
2) Vote to grant the Conditional Use Permit with the following conditions:
2.1) Documentation of the conditional use permit approval shall be recorded at the Rockingham County Registry of Deeds, together with an affidavit that either the principal dwelling unit or the accessory dwelling unit will be occupied by the owner of the dwelling as the owner's principal place of residence, as required by Section 10.814.22.
2.2) A certificate of use issued by the Planning Department is required to verify compliance with the standards of this Section, including the owner occupancy and principal residency requirements. Said certificate shall be issued by the Planning Department upon issuance of a certificate of occupancy by the Inspection Department. A certificate of use shall not be issued prior to recording of documentation as required by this Ordinance.
2.3) The certificate of use shall be renewed annually upon submission of such documentation as the Planning Department may require to verify continued compliance with the standards of this Section. Failure to comply with this requirement shall be deemed a violation of the ordinance and may be enforced as provided in Article 2.

## III. PUBLIC HEARINGS - NEW BUSINESS

The Board's action in these matters has been deemed to be quasi-judicial in nature.
If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
G. The request of Portsmouth West End Development LLC (Owner), for property located at 125 Brewery Lane requesting a Conditional Use Permit in accordance with Section 10.440, Use 19.50 for an outdoor dining and drinking area as an accessory use. Said property is located on Assessor Map 154 Lot 2 and lies within the Character District 4-W (CD-4W) District. (LU-24108)

## Background

The property is located in the CD4-W district, where an outdoor dining and drinking area requires a conditional use permit as an accessory use to a principal use. The applicant is proposing to add picnic tables and bistro tables and chairs to an area at the back of the building which faces the existing parking lot. The proposal includes expanding the gravel area to accommodate the tables and chairs.


## Planning Department Recommendation

## Outdoor Dining Conditional Use Permit

1) Vote to find that the Conditional Use Permit application meets the criteria set forth in Section 10.243.20 and to adopt the findings of fact as presented.
(Alt.) Vote to find that the Conditional Use Permit application meets the criteria set forth in Section 10.243.20 and to adopt the findings of fact as amended and read into the record.
2) Vote to approve the conditional use permit as presented.

## IV. PRELIMINARY CONCEPTUAL CONSULTATION AND DESIGN REVIEW

A. The request of Frances E. Mouflouze Revocable Trust of 2015 (Owner), for property located at 550 Sagamore Avenue requesting preliminary Conceptual Consultation for a subdivision of one lot into three conforming lots with associated site improvements. Said property is located on Assessor Map 222 Lot 11 and lies within the Single Residence B (SRB) District. (LUPD-24-5)

The applicant has provided a set of preliminary plans for discussion with the Board. As authorized by NH RSA 676:4,II, the Site Plan Regulations require preliminary conceptual consultation for certain proposals, including (1) the construction of $30,000 \mathrm{sq}$. ft. or more gross floor area, (2) the creation of 20 or more dwelling units, or (3) the construction of more than one principal structure on a lot. Preliminary conceptual consultation precedes review by the Technical Advisory Committee. Preliminary consultation is not required for this application, however the applicant wanted to get feedback from the Board prior to submitting a formal TAC application for site plan and subdivision approval.

Preliminary conceptual consultation is described in the state statute as follows: [Preliminary conceptual consultation] ... shall be directed at review of the basic concept of the proposal and suggestions which might be of assistance in resolving problems with meeting requirements during final consideration. Such consultation shall not bind either the applicant or the board and statements made by planning board members shall not be the basis for disqualifying said members or invalidating any action taken. The board and the applicant may discuss proposals in conceptual form only and in general terms such as desirability of types of development and proposals under the master plan.

The preliminary conceptual consultation phase provides the Planning Board with an opportunity to review the outlines of a proposed project before it gets to detailed design (and before the applicant refines the plan as a result of review by the Technical Advisory Committee and public comment at TAC hearings). In order to maximize the value of this phase, Board members are encouraged to engage in dialogue with the proponent to offer suggestions and to raise any concerns so that they may be addressed in a formal application. Preliminary conceptual consultation does not involve a public hearing, and no vote is taken by the Board on the proposal at this stage. Unlike Design Review, completion of Preliminary Conceptual Consultation does not vest the project to the current zoning.
B. 361 Hanover Steam Factory, LLC (Owner), for property located at 361 Hanover Street, requesting Preliminary Conceptual Consultation for the construction of a new building along Hanover Street with a 20 -foot tunnel entrance from Hanover Street to a central courtyard between the new building and the existing 361 Hanover Street (Portsmouth Steam Factory) building. The courtyard will provide access to the indoor parking areas at both the existing and the new building. The upper floors of the new Hanover Street building will contain 12 residential dwelling units and the Portsmouth Steam Factory Building would contain 24 dwelling units; for a total of 36 dwelling units. There would be 72 offstreet parking spaces in the aggregate. (LUPD-24-3)

The applicant has provided a set of preliminary plans for discussion with the Board. As authorized by NH RSA 676:4,II, the Site Plan Regulations require preliminary conceptual consultation for certain proposals, including (1) the construction of $30,000 \mathrm{sq}$. ft. or more gross floor area, (2) the creation of 20 or more dwelling units, or (3) the construction of more than one principal structure on a lot. Preliminary conceptual consultation precedes review by the Technical Advisory Committee.

Preliminary conceptual consultation is described in the state statute as follows: [Preliminary conceptual consultation] ... shall be directed at review of the basic concept of the proposal and suggestions which might be of assistance in resolving problems with meeting requirements during final consideration. Such consultation shall not bind either the applicant or the board and statements made by planning board members shall not be the basis for disqualifying said members or invalidating any action taken. The board and the applicant may discuss proposals in conceptual form only and in general terms such as desirability of types of development and proposals under the master plan.

The preliminary conceptual consultation phase provides the Planning Board with an opportunity to review the outlines of a proposed project before it gets to detailed design (and before the applicant refines the plan as a result of review by the Technical Advisory Committee and public comment at TAC hearings). In order to maximize the value of this phase, Board members are encouraged to engage in dialogue with the proponent to offer suggestions and to raise any concerns so that they may be addressed in a formal application. Preliminary conceptual consultation does not involve a public hearing, and no vote is taken by the Board on the proposal at this stage. Unlike Design Review, completion of Preliminary Conceptual Consultation does not vest the project to the current zoning.

This project was before the Board in April for Preliminary Conceptual Consultation and then Design Review in May in order to vest the zoning. The
applicant has made substantial changes to the project based on input from the public and the Planning Board and wanted to present the new plan to the Board prior to seeking variances for certain elements of the project.

## V. OTHER BUSINESS

A. Chairman's Updates and Discussion Items
B. Board Discussion of Regulatory Amendments and Other Matters

## VI. ADJOURNMENT

# PLANNING BOARD <br> PORTSMOUTH, NEW HAMPSHIRE 

# EILEEN DONDERO FOLEY COUNCIL CHAMBERS CITY HALL, MUNICIPAL COMPLEX, 1 JUNKINS AVENUE 

7:00 PM Public Hearings begin
June 20, 2024
MEMBERS PRESENT: Rick Chellman, Chairman; Greg Mahanna, Vice Chair; Karen Conard, City Manager; Joseph Almeida, Facilities Manager; Beth Moreau, City Councilor; James Hewitt; Paul Giuliano; Andrew Samonas; Anthony Coviello; and William Bowen, Alternate

## ALSO PRESENT: <br> Peter Stith, Planning Department Manager <br> MEMBERS ABSENT: None.

Chair Chellman called the meeting to order at 7:00 p.m. He stated that Mr. Coviello would arrive at the meeting later and that Alternate Mr. Bowen would take a voting seat until then.

## I. APPROVAL OF MINUTES

A. Approval of the May 16, 2024 meeting minutes.

Vice-Chair Mahanna moved to approve the May 16 minutes as amended, seconded by Councilor Moreau and with Mr. Hewitt abstaining. The motion passed unanimously.

## II. DETERMINATIONS OF COMPLETENESS

## SITE PLAN REVIEW

A. The request of Friends of Lafayette House in care of Melanie Merz (Owner), for property located at $\mathbf{4 1 3}$ Lafayette Road requesting Site Plan Review Approval to construct an attached caretaker's unit to the existing residential care facility with associated site improvements. Said property is located on Assessor Map 230 Lot 23A and lies within the Single Residence B (SRB) District.

Councilor Moreau moved that the Board determine that Item A is complete according to the Site Plan Review Regulations (contingent on the granting of any required waivers under Section IV of the agenda) and to accept the application for consideration. Vice-Chair Mahanna seconded. The motion passed unanimously.

## III. PUBLIC HEARINGS - NEW BUSINESS

A. The request of Edmund R. St. Pierre (Owner), for property located at $\mathbf{1 5}$ Mariette Drive requesting a Conditional Use Permit from Section 10.814 for a Detached Accessory Dwelling Unit. Said property is located on Assessor Map 292 Lot 167 and lies within the Single Residence B (SRB) District. (LU-24-57)

## SPEAKING TO THE PETITION

[Timestamp 4:30] The applicant Edmund St. Pierre was present. He reviewed the petition and described what the proposed detached Accessory Dwelling Unit (ADU) would look like.
[Timestamp 7:58] Vice-Chair Mahanna noted that the applicant said he wanted to downsize and asked if the applicant would live in it. Mr. St. Pierre said he designed the ADU for himself or his sister to live in. Councilor Moreau said the applicant said a second-floor full bathroom was proposed but that he mentioned a half bath on the first floor. Mr. St. Pierre said the first-floor full bathroom would go away with the renovation. Chair Chellman said the applicant proposed to renovate part of the first floor into the ADU but that one of the plans showed the entire first floor going into the ADU. Mr. St. Pierre said he originally designed a handicap accessible first floor but did not follow through with it because of the square footage.

Chair Chellman opened the public hearing.

## SPEAKING TO, FOR, OR AGAINST THE PETITION

No one spoke, and Chair Chellman closed the public hearing.

## DECISION OF THE BOARD

Councilor Moreau moved that the Board find that the Conditional Use Permit Application meets the requirements set forth in Section 10.814.62 of the Ordinance and adopt the findings of fact as presented. Ms. Conard seconded. The motion passed unanimously.

Councilor Moreau moved that the Board grant the Conditional Use Permit with the following conditions:
2.1) Documentation of the conditional use permit approval shall be recorded at the Rockingham County Registry of Deeds, together with an affidavit that either the principal dwelling unit or the accessory dwelling unit will be occupied by the owner of the dwelling as the owner's principal place of residence, as required by Section 10.814.22.
2.2) A certificate of use issued by the Planning Department is required to verify compliance with the standards of this Section, including the owner occupancy and principal residency requirements. Said certificate shall be issued by the Planning Department upon issuance of a certificate of occupancy by the Inspection Department. A certificate of use shall not be issued prior to recording of documentation as required by this Ordinance.
2.3) The certificate of use shall be renewed annually upon submission of such documentation as the Planning Department may require to verify continued compliance with the standards of this Section. Failure to comply with this requirement shall be deemed a violation of the ordinance and may be enforced as provided in Article 2.

Ms. Conard seconded. The motion passed unanimously.
B. The request of Richard M. and Francoise S. Kinney (Owners), for property located at $\mathbf{8 9}$ Cliff Road requesting an after the fact Wetland Conditional Use Permit from Section 10.1017.50 for violations within the City's 100 ' wetland buffer. A threeseason porch, deck and concrete landing pad were constructed without permits, of which 225 s.f. is within the buffer. Said property is located on Assessor Map 223 Lot 9 and lies within the Single Residence B (SRB) District. (LU-24-54)

## SPEAKING TO THE PETITION

[Timestamp 13:00] The applicant Richard Kinney was present to review the petition. He said a 3 -season porch, adjoining deck, and concrete landing pad were added that intruded 225 square feet into the wetland buffer. He said he worked with the Conservation Commission to mitigate the impact onto the buffer, which included putting in a drywell, adding gravel under the porch and deck, extending the downspout out from the north side of the house, and adding shrubs and a recessed planting area. He said a microclover lawn mix would replace the back yard's grass.

The Board had no questions, and Chair Chellman opened the public hearing.

## SPEAKING TO, FOR, OR AGAINST THE PETITION

No one spoke, and Chair Chellman closed the public hearing.

## DECISION OF THE BOARD

Mr. Giuliano moved that the Board find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact as presented. Mr. Almeida seconded. The motion passed unanimously.

Mr. Giuliano moved that the Board grant_the Conditional Use Permit with the following condition:
2.1) In accordance with Section 10.1018 .40 of the Zoning Ordinance, applicant shall install permanent wetland boundary markers where applicable. In addition to the wetland boundary markers, an educational sign describing the project shall be installed near the restoration area and fencing should be utilized to keep disturbances such as dogs and geese from the area.

Ms. Conard seconded. The motion passed unanimously.
C. The request of Wentworth Senior Living (Applicant), and MH Wentworth HM for CHRNC INV (Owner), for property located at 346 Pleasant Street is requesting a Wetland Conditional Use Permit from Section 10.1017.50 to replace an existing wooden fence along the back of the property which abuts the South Mill Pond. This replacement project will have approximately 200 s.f. of impact within the buffer, with 10 s.f. of permanent impact below ground with the posts and 500 linear feet of permanent impact from the fence. Said property is located on Assessor Map 109 Lot 10 and lies within the General Residence B (GRB) District. (LU-24-63)

## SPEAKING TO THE PETITION

[Timestamp 19:12] Madison Abbott representing Wentworth Senior Living was present to review the petition. She said they wanted to replace 510 linear feet of wooden fence, most of which occurred within the $100-\mathrm{ft}$ wetland buffer. She said the reason for going through the whole permit requirement and not just an exception was because they had about 50 linear feet within the 25 - ft vegetation buffer. She said they were past the point of repairing and explained how the installation method would be the least disruptive as possible.
[Timestamp 20:11] Councilor Moreau said it wasn't clear which fence would be installed. Ms. Abbott said they currently had a scalloped picketed fence that they wanted to replace with a vinyl one that would have the same look but be more durable. Chair Chellman asked if it was shiny. Ms. Abbott said it would be for a few years. She said one of the Conservation Commission's stipulations was that a regular maintenance plan be followed and that only pressurized washing with water be done. Vice-Chair Mahanna said it was an interesting choice by the applicant to oppose what the Historic District Commission (HDC) suggested. Ms. Abbott said the HDC approved the vinyl material but that the Conservation Commission suggested that other options be explored. She said an Azek material would have been a choice but it was four times the cost of the vinyl fence. Vice-Chair Mahanna said he would have preferred a non-shiny wooden fence, especially since Wentworth Senior Living was a public place. Ms. Abbott said they had about 90 feet of frontage on Pleasant Street, with a concrete wall that included a wooden fence above it. She said eventually they would replace the fence with another wood one. Mr. Almeida noted that the front of the building was painstakingly restored and maintained and there was a total rebuild of the fence in the front. Chair Chellman asked Ms. Abbott if she would accept a condition that the fence along Pleasant Street would remain wood. Ms. Abbott agreed.

Chair Chellman opened the public hearing.

## SPEAKING TO, FOR, OR AGAINST THE PETITION

No one spoke, and Chair Chellman closed the public hearing.

## DECISION OF THE BOARD

Councilor Moreau moved that the Board find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact as presented. Ms. Almeida seconded. The motion passed unanimously.

Councilor Moreau moved that the Board grant the Conditional Use Permit with the following conditions:
2.1) In accordance with Section 10.1018 .40 of the Zoning Ordinance, applicant shall install permanent wetland boundary markers where applicable. In addition to the wetland boundary markers, an educational sign describing the project shall be installed near the restoration area and fencing should be utilized to keep disturbances such as dogs and geese from the area.
2.2) Maintenance for the new fencing shall include power washing with water only.
2.3) Fencing along Pleasant Street if replaced, will remain the current material that exists.

Mr. Almeida seconded. The motion passed unanimously.
D. The request of Friends of Lafayette House in care of Melanie Merz (Owner), for property located at $\mathbf{4 1 3}$ Lafayette Road requesting Site Plan Review Approval to construct an attached caretaker's unit to the existing residential care facility with associated site improvements. Said property is located on Assessor Map 230 Lot 23A and lies within the Single Residence B (SRB) District. (LU-23-208)

## SPEAKING TO THE PETITION

[Timestamp 27:55] Project engineer Joe Coronati was present to review the petition on behalf of the applicant, along with Friends of Lafayette House Executive Director Renee Sullivan and board member Melanie Merz. Mr. Coronati said the Friends of Lafayette House took care of twelve developmentally disabled adults. He said the full-time caretaker lived on the property and worked five days a week and a part-time caretaker worked on the weekend and stayed with the full-time caretaker then. He said the expansion was needed to add a one-story addition to the building so that the full-time caretaker had his own apartment. He said there would be no change to the number of residents or anything external except to modify the walkway.
[Timestamp 30:42] Councilor Moreau asked how people went in and out of the building. Mr. Coronati showed where the main entrance was and said it would not change. Chair Chellman said the site plan showed two accesses and asked if the one farther away was the main entrance. Mr. Coronati said the addition would be on the end of the building that had the boiler and storage rooms and would not alter any of the doorways or access points into the building. He said there would be a new entrance to the caretaker's unit. Councilor Moreau said the entrance on the right looked like it went into a kitchen. Mr. Coronati said there was an entrance on the long wall and egress doors that were fenced in and secured for residents. Mr. Bowen said there was plenty of parking at random times and that he assumed that most of the residents didn't drive but would have visitors. He asked if the parking would change and Mr. Coronati said it would not. Mr. Giuliano said the waiver request, Article 10, Outdoor Lighting, indicated that the applicant was
proposing additional lighting, and he asked if the applicant meant to say that they were not proposing additional lighting. Mr. Coronati agreed. He said there might be one residential light over entrance door that would be controlled by the caretakers and that there was one outside light that wasn't in the best of shape that may end up being removed.

Chair Chellman opened the public hearing.

## SPEAKING TO, FOR, OR AGAINST THE PETITION

No one spoke, and Chair Chellman closed the public hearing.

## DECISION OF THE BOARD

Mr. Giuliano moved that the Board find that the Site Plan Application meets the requirements set forth in the Site Plan Regulations Section 2.9 Evaluation Criteria and adopt the findings of fact as presented. Vice-Chair Mahanna seconded. The motion passed unanimously.

Mr. Giuliano moved that the Board find that the requested waivers will not have the effect of nullifying the spirit and intent of the City's Master Plan or the Site Plan Review Regulations, and to waive the regulations as requested. Councilor Moreau seconded.

Councilor Moreau said it was a little addition that would not really change the function or how the place works, so she agreed that the waivers were acceptable.

Mr. Giuliano moved that the Board grant Site Plan approval with the following conditions:
Conditions to be satisfied subsequent to final approval of site plan but prior to the issuance of a building permit or the commencement of any site work or construction activity:
3.1) The site plan and any easement plans and deeds shall be recorded at the Registry of Deeds by the City or as deemed appropriate by the Planning Department.

Ms. Conard seconded. The motion passed unanimously.
E. 806 US Route 1 Bypass requesting Amended Site Plan Approval and a second 1Year extension to the Site Plan Approval originally granted on June 23, 2022. (LU-22-81)

## SPEAKING TO THE PETITION

[Timestamp 38:23] Project engineer Alex Ross was present on behalf of the applicant, with builder Dave Grzybowski. Mr. Ross said they were before the Board a month ago for the abutting site because of the off-site draining. He said it was the same as the present site, and he reviewed the existing conditions plan and the drainage. He said there were several design options reviewed by the City and the NHDOT and that A22 was approved, so now they had the proposed changes before the Board to get the amended plan set and extension approved.
[Timestamp 40:13] Mr. Giuliano said he had asked at the previous meeting what the property's use would be. Mr. Ross said property was currently City Tobacco and it was just a small building, so the owner wanted to move next door. He said the small building could be rented out or used for something else. Mr. Grzybowski said that after the move, the place would be empty but the applicant would come back before the Board for any change in use or if any business went in. Chair Chellman noted that an approved walk-in cooler would be added to the back of it to make the approved square footage.

Chair Chellman opened the public hearing.

## SPEAKING TO, FOR, OR AGAINST THE PETITION

No one spoke, and Chair Chellman closed the public hearing.

## DECISION OF THE BOARD

Councilor Moreau moved that the Board find that the Site Plan Application meets the requirements set forth in the Site Plan Regulations Section 2.9 Evaluation Criteria and adopt the findings of fact as presented. Ms. Conard seconded. The motion passed unanimously.

Councilor Moreau moved that the Board grant amended site plan approval and a second oneyear extension with the original conditions as approved on June 23, 2022 and the following conditions:

## Conditions to be satisfied subsequent to final approval of site plan but prior to the issuance of

 a certificate of occupancy and release of the surety:2.1) The Engineer of Record shall submit a written report (with photographs and engineer stamp) certifying that the stormwater infrastructure was constructed to the approved plans and specifications and will meet the design performance;
2.2) A stormwater inspection and maintenance report shall be completed annually and copies shall be submitted for review to the City's Stormwater Division/ Public Works Department.

Ms. Conard seconded. The motion passed unanimously.
F. The Planning Board will hold a public hearing on the following amendments to Chapter 10, Article 5A - Character-Based Zoning, Section 10.5A43.33 regarding Building and Story Heights of the ZONING ORDINANCE of the City of Portsmouth, pursuant to Section 10.150 of the Zoning Ordinance.
[Timestamp 44:10] Chair Chellman asked if the Board members had a chance to look at the amendments. Mr. Hewitt said he didn't have time and preferred postponing it to give the Board members more time to look at the amendments carefully. Chair Chellman said it was a modification to something that was done last August, so it wasn't brand new. He said there was a question about whether there was a requirement to have workforce housing as part of the
proponent's application to qualify for the additional height story of building. He said it was corrected and that he requested that the Board members look at the other sections because the community space definitions were not what they would think. He said it included things like plazas and pedestrian passageways and was much more than greenspace. Vice-Chair Mahanna said he didn't get a chance to read the email. Councilor Moreau said the question was whether it needed to be mixed use residential and nonresidential uses for the incentives to be taken advantage of. She said that was why the City Council was trying to clarify that section because it was not as clear as what the intention was.

Chair Chellman said the original text included the phrase 'and/or' and that it could be confusing. He said it was meant to be a possible mix of building types. He said he also thought the 50 percent requirement for community space was high and a big ask as well as a detriment to the incentive itself. He said the Board might want to discuss whether they would want to suggest to the Council to reduce it. Vice-Chair Mahanna said it could be scaled down. Chair Chellman said he was thinking of scaling it down to half. Mr. Bowen asked if it would apply to the Steam Factory, and Chair Chellman said it would not because the Incentive Overlay District did not apply. He said there would have to be a one-acre minimum as well. He noted that the McIntyre and Citizens Bank properties would qualify as well as a few other properties. Vice-Chair Mahanna suggested that the Board receive more information to inform them on what they were deciding on for the next time they considered it. Councilor Moreau said there was a lot of discussion about the 50 percent community space at the Land Use Committee meeting, and due to the density and size of the one acre or more lots, trying to get as much community space as possible was very important, so she would not be in favor of trying to change that at this time. Chair Chellman said the building types included houses, and there had been discussion that The Hill, for example, was a nonconforming situation that could not be built downtown under the existing zoning but that it could be theoretically built on the Citizens Bank property with houses, so it would qualify for that type of development on that site. He said he thought it would be more difficult to do with a 50 percent community space allocation. Ms. Conard asked if the City Council could act in the absence of the Planning Board acting. Chair Chellman said the zoning ordinance required the Planning Board to make a recommendation to the City Council. He said he would be okay with revisiting the community space issue in the future. He said the other sections were strategically more important, especially the goal for workforce housing.

Ms. Conard moved to recommend that the City Council take up the new section as amended as of that day to the Planning Board. Mr. Giuliano seconded.
[Timestamp 53:47] There was further discussion about whether the Board would have the authority to grant an extra layer of height or extra floor in exchange for 5 or 10 percent being controlled rent price and 50 percent being greenspace. Chair Chellman said it was community space, not greenspace, and said examples would include pedestrian passageways, wide pedestrian sidewalks, pedestrian arcades, pocket parks, playgrounds, public observation decks, and that there was a requirement to include a plaza or square of at least 5,000 sf per acre. Chair Chellman said none of those were greenspaces and were hardscaped community spaces. Mr. Bowen asked if there was no discretion on a proposal that would conform to those conditions. Chair Chellman said it would be a Conditional Use Permit, so there was discretion involved and
some back-and-forth. He said if an applicant met all the requirements, the Board was supposed to grant it. Mr. Bowen said the average person thought of community space as greenspace. ViceChair Mahanna said he supported the clarification but thought the Board should see the normal overlay that showed the properties to be affected. Chair Chellman said none of the applicable properties were changing in any way and that very few could qualify. Vice-Chair Mahanna said it was a burden for the developer to have 50 percent of an acre for community space. Mr. Almeida agreed and said he thought part of the purpose of the amendment was due to workforce housing and thought it would encourage and discourage workforce housing at the same time. Chair Chellman said the motion was to correct the mistake. He said he was inclined to vote it up but that the Board could come back to it because workforce housing was a big topic.

## Ms. Conard amended her motion as follows:

Ms. Conard moved that the Board vote to recommend to City Council to approve the zoning amendments as amended and to hold first reading and to convey the discussion the Board had about the 50\% community space requirement. Mr. Giuliano seconded.
[Timestamp 1:01:22] There was further discussion. Mr. Samonas said one of the ways to achieve better public and community space results were amenities that welcomed the public, as opposed to wider pedestrian sidewalks. He said the second community space objective was to break up the massing of some of the larger north end projects that tried to utilize the parcel and drive economic return but created congestion. He said the workforce housing objective set the threshold so high that the developer had to come before the Board to ask if they would end up at 50 percent, but at least it allowed them to discuss it before the Board. He noted that the amendment mentioned the term 'as further described'. He said the revisions helped the Board get a cohesive view of all the considerations, and if they had the figures and entire zoning ordinance in front of them, it helped to get the full big picture. Chair Chellman said it was not a change in any of that, however. He said if a second version of it happened, the first sentence about community space could be changed to say that "at least a smaller amount and up to 50 percent or whatever the range would be" to have a provision where the applicant is required to show both and have a discussion with the Board. It was further discussed. Mr. Hewitt said it may be a logical step but that he had to vote in opposition due to the nine hours' notice. Mr. Giuliano said Mr. Samonas brought up a good points about the large projects in the north end, and it was further discussed. Mr. Almeida said he would support the motion because the Board was correcting minor language changes, but in the future they would need more discussion. Councilor Moreau said she could bring up the 50 percent issue at the City Council meeting.

The motion passed 7-2, with Member Hewitt and Vice-Chair Mahanna voting against.
Note: At this point in the meeting, Mr. Coviello arrived and took his voting seat, and Mr. Bowen went back to alternate status.

## IV. CITY COUNCIL REFERRALS

A. Chapter 10, Article 5A - Character-Based Zoning (See item F. above)

See Item F above.

## V. OTHER BUSINESS

A. 325 Little Harbor Road requesting a 1-Year Extension to the Wetland Conditional Use Permit originally granted on July 20, 2023. (LU-23-81)

## DECISION OF THE BOARD

Councilor Moreau moved that the Board grant a one-year extension to the Planning Board Approval of the Conditional Use Permit to July 20, 2025. Mr. Almeida seconded. The motion passed unanimously.

## B. Chairman Updates and Discussion Items

[Timestamp 1:14:00] Chair Chellman said there was a desire to go through the Board's site plan and subdivision regulations that had not had attention for some time, and the Legal Department wanted to have a meeting with a Planning Board subcommittee. Mr. Coviello and Mr. Bowen volunteered. Chair Chellman said he would set it up.

## C. Board Discussion of Regulatory Amendments, Master Plan Scope \& Other Matters

[Timestamp 1:14:51] Chair Chellman said a draft of the Master Plan Scope would go out to the Board members for a proposed RFQ similar to what the City did with the Sherburne school.

Mr. Coviello said he and Mr. Bowen were at a housing conference where Assistant Mayor Joanna Kelley spoke and said that the City Council collected data on new housing and the number of students that came out of that new housing. He asked if that data was available to the Board. Councilor Moreau said it was the Parson Woods in the west end and that two students were designated for Little Harbour School. Mr. Coviello asked if it were possible to have data on calls for service from Police and Fire, and Ms. Conard said she would find out.

## VI. ADJOURNMENT

The meeting adjourned at 8:20 p.m.
Respectfully submitted,
Joann Breault
Planning Board Recording Secretary

L0700-026C
June 14, 2024
Mr. Rick Chellman, Chairman
City of Portsmouth Planning Board
1 Junkins Avenue
Portsmouth, New Hampshire 03801

## Re: Lonza Biologics - Proposed PV Solar Carports Amended Site Plan Review Application LU-23-108

Dear Chairman Chellman:
On behalf of Lonza Biologics, Inc. (Lonza), we are pleased to submit one (1) set of hard copies and one electronic file (.pdf) of the following information to support a request to the Planning Board for a recommendation for approval to the Pease Development Authority (PDA) for Amended Site Plan Review for proposed PV Solar Carports located at 5 Technology Way, (Formerly 70 Corporate Drive) on Pease International Tradeport:

- PDA Application for Site Review, dated May 20, 2024;
- Site Plan Set, last revised May 20, 2024;
- Drainage Memo, dated May 20, 2024;
- Glare Study Results, dated February 22, 2024;


## PROJECT SUMMARY

## Background

The existing project was granted Site Plan approval on January 17, 2019, and amended by administrative approvals on September 27, 2019, January 27, 2023, and Amended Site Plan Approval on November 16, 2023.

## Existing Condition

The project is located on the portion of Lonza's 46 -acre parcel refered to as the Iron Parcel. The following summarizes the work currently approved through the November 16, 2023 Amended Site Plan Approval:

- Daylighting of Hodgson Brook on the Iron Parcel
- Removal of the existing Hodgson Brook culvert
- Construction of the sidewalk and landscaping along Corporate Drive
- Completion of Soils Management Plan
- Construction of Building \#1
- Construction of the Central Utility Building
- Construction site improvements for Building \#1 such as drive aisles, fire lanes, utilities, lighting, sidewalks and stormwater management.
- Construction of a temporary 150 -space surface parking lot, sidewalks and stormwater management.


## Amended Site Plan

The requested Site Plan amendment includes the construction of Photovoltaic Cell (PV) Solar canopies over the previously approved temporary surface parking lot. The addition of these Solar Canopies is being requested to support Lonza Biologics green infrastructure and sustainability initiatives. The addition of these Solar canopies will not result in any dimensional changes to the previously approved parking lot. There is a slight increase in impervious surfaces ( $\sim 672$ SF) which will not cause any adverse impact to the previously approved Phase 2 Drainage design as outlined in the Drainage Memorandum.

The proposed PV Solar system will require additional electrical infrastructure and modifications to the photometric lighting design as depicted in the enclosed Site Plan Set. The proposed system is being designed to supplement and reduce the proposed project's overall electrical demand.

The project also received a recommendation for approval from the Technical Advisory Committee (TAC) at their June 4, 2024, meeting. We respectfully request to be placed on the Planning Board (PB) meeting agenda for July 18, 2024. If you have any questions or need any additional information, please contact Neil Hansen by phone at (603) 294-9213 or by email at nahansen@tighebond.com.

Sincerely,
TIGHE \& BOND, INC.


Neil A. Hansen, PE
Project Manager


Patrick M. Crimmins, PE Vice President

Copy: Lonza Biologics (via email)<br>Pease Development Authority

# Pease Development Authority 55 International Drive, Portsmouth, NH 03801, (603) 433-6088 <br> Application for Site Review 

| For PDA Use Only |  |  |  |
| :--- | :--- | :--- | :--- |
| Date Submitted: | Municipal Review: | Fee: |  |
| Application Complete: | Date Forwarded: | Paid: | Check \#: |

## Applicant Information

| Applicant: Lonza Biologics, Inc. | Agent: Tighe \& Bond, Inc. |
| :--- | :--- |
| Address:101 International Drive <br> Portsmouth, NH 03801 | Address: 177 Corporate Drive <br> Portsmouth, NH 03801 |
| Business Phone: 603-570-3625 | Business Phone: 603-433-8818 |
| Mobile Phone: | Mobile Phone: |
| Fax: | Fax: |

## Site Information

| Portsmouth Tax Map: 305 | Lot \#: 006 |
| :--- | :--- |
| Site Address / Location : 101 International Drive, Portsmouth, NH 03801 |  |
| Site Address / Location : | Area of On-site Wetlands: 4,087 SF |

## Activity Information

| Change of Use: Yes [ $]$ No [X] | Existing Use: Office/Research/Manufacturing |
| :--- | :--- |
| Description of Project: |  |
| The requested Site Plan amendment includes the Construction of Photovoltaic Cell (PV) |  |
| Solar canopies over the previously approved temporary surface parking lot. |  |
|  |  |
|  |  |

## Certification


$\mathrm{N}:$ :IEngineer ApplicationforSiteReview.xIsx

## IRON PARCEL DEVELOPMENT - SOLAR 5 TECHNOLOGY WAY

(FORMERLY 70 CORPORATE DRIVE)

## PORTSMOUTH, NEW HAMPSHIRE PROJECT NO: L-0700-26 <br> MAY 20, 2024




LOCATION MAP
SCALE: $1{ }^{10}=2,000^{\circ}$

LESSOR

CLIENT:

CIVIL ENGINEER:

SURVEYOR:

WETLAND SCIENTIST:









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## OSION CONTROL NOTES

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## CONCRETE WASHOUT AREA






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## EROSIO NOTTROL OSSERVATIONS AND MTATTENACCE PRACTTEES









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 $\frac{\text { STABILZED CONSTRUCTION ENTRANCE }}{\text { NO SCALE }}$

 $\frac{\text { SILT SOCK }}{\text { No SCALE }}$


##  

 $\frac{\text { INLET PROTECTION }}{\text { NOSCALE }}$Proposed
Industrial

Portsmouth, New Hampshire

| - | $31 / 2024$ | Amended Site Plan Review |
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| EROSION CONTROL NOTES \& DETAILS SHEET |  |  |
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|  |  | -501 |




## Drainage Memorandum

To: Pease Development Authority (PDA)<br>From: Neil A. Hansen, PE Patrick M. Crimmins, PE<br>Copy: Lonza Biologics<br>Date: May 20, 2024

### 1.0 Project Description

The proposed work includes the addition of Solar Canopies over the previously approved 150space surface parking lot associated with Phase 2 of the Iron Parcel Development project. These Solar Canopies are planned to be removed along with the 150 -space parking lot before the execution of the Master Plan, therefore there will be no changes to the Master Plan Drainage Design.

The Phase 2 drainage analysis has been updated and revised to include the $4^{\prime} \times 4^{\prime}$ concrete footings and $8{ }^{\prime} \times 22^{\prime}$ concrete equipment pad. The proposed change includes the addition of approximately 672 SF of impervious surfaces. Although the addition of this area is very minimal in perspective to the whole watershed area ( $1,376,888 \mathrm{SF}$ ), we have prepared this technical memo to confirm that the previously approved Phase 2 drainage design and gravel wetlands are sized appropriately to accommodate this slight increase in impervious area.

### 2.0 Drainage Analysis

The previously approved Phase 2 Drainage Calculation has been updated to analyze the slight increase in impervious area and can be found in Attachment A. Subcatchment 1.0 has been updated to convert 304 SF of the previously grass surface to impervious surface. This additional 304 SF is approximately $0.09 \%$ of the total impervious area (314,795 SF) for this watershed.

Subcatchment 1.1 has been updated to convert 368 SF of the previously grass surface to impervious surface. This addition of 368 SF is approximately $0.7 \%$ of the total impervious area ( $48,674 \mathrm{SF}$ ) for this watershed.


### 2.1 Peak Rate Comparisons

The following table summarizes and compares the Phase-2 2023 Approved, proposed Phase-2 2024 Amendment, and Master Plan pre- and post-development peak runoff rates for the 2-year, 10-year, 25-year and 50-year storm events at each point of analysis. These points of analysis remain unchanged from the previously prepared and approved drainage analysis.

Table 2.1 - Peak Flow Rate Comparison

| Point of Analysis | Phase | $\begin{gathered} \hline \text { Pre } \\ \text { 1-Year } \\ \text { Storm } \\ \text { (cfs) } \\ \hline \end{gathered}$ | ```Pre/Post 2-Year Storm (cfs)``` | Pre/Post 10-Year Storm (cfs) | Pre/Post <br> 25-Year <br> Storm <br> (cfs) | Pre/Post 50-Year Storm (cfs) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PA1 | Phase 2 (2023 Approval) | 16.58 | 24.86/9.25 | 52.70/31.22 | 76.06/56.26 | 98.56/74.09 |
|  | Phase 2 (2024 <br> Amendment) | 16.58 | 24.86/9.25 | 52.70/31.22 | 76.06/56.26 | 98.56/74.09 |
|  | Master | 16.58 | 24.86/9.41 | 52.70/39.92 | 76.06/66.14 | 98.56/83.35 |
| PA2 | Phase 2 (2023 Approval) | 3.38 | 4.41/3.10 | 7.49/5.36 | 9.90/7.12 | 12.13/8.76 |
|  | Phase 2 (2024 Amendment) | 3.38 | 4.41/3.10 | 7.49/5.36 | 9.90/7.12 | 12.13/8.76 |
|  | Master | 3.38 | 4.41/3.72 | 7.49/5.94 | 9.90/7.66 | 12.13/9.25 |

### 2.2 Stormwater Treatment

Runoff from the newly created impervious surfaces will be directed to either of the previously approved Gravel Wetland 1 (POND 1.0) or Gravel Wetland 2 (POND 1.1). The following sections outline the treatment capacities of both gravel wetlands.

## Gravel Wetland 1

Gravel Wetland 1 has a design capacity to treat 333,950 SF of impervious area for its 462,599 SF watershed area. The proposed change is to add 304 SF of impervious surface to the previously approved 314,491 SF of impervious surface for an amended total of 314,795 SF of impervious surface. This 314,795 SF is well within the gravel wetland design capacity of 333,950 SF of impervious surface.

## Gravel Wetland 2

Gravel Wetland 2 has a design capacity to treat 142,418 SF of impervious area for its 242,496 SF watershed area. The proposed change is to add 368 SF of impervious surface to the previously approved 48,306 SF of impervious surface for an amended total of 48,674 SF of impervious surface. This $48,674 \mathrm{SF}$ is well within the gravel wetland design capacity of 142,418 SF of impervious surface.

### 3.0 Conclusion

The proposed amendment will result in no change to the previously approved postdevelopment peak runoff rates for Phase 2 and does not affect the Master Plan Drainage design. The net increase in impervious areas resulting from the proposed work will be directed to either Gravel Wetland 1 or Gravel Wetland 2 which both have the capacity to treat the slight increase in impervious surfaces.

## Phase 2 (2023 Approval) Post-Development Calculations




## Area Listing (all nodes)

| $\begin{array}{r} \text { Area } \\ \text { (acres) } \\ \hline \end{array}$ | CN | Description (subcatchment-numbers) |
| :---: | :---: | :---: |
| 2.312 | 61 | $>75 \%$ Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4) |
| 13.558 | 74 | >75\% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0) |
| 1.467 | 80 | >75\% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4) |
| 0.514 | 58 | Meadow, non-grazed, HSG B (POST 1.3) |
| 1.662 | 71 | Meadow, non-grazed, HSG C (POST 1.3) |
| 0.639 | 98 | Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3) |
| 6.959 | 98 | Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0) |
| 0.137 | 98 | Paved parking, HSG D (POST 1.0, POST 1.3) |
| 0.120 | 98 | Roofs, HSG B (POST 1.0) |
| 3.526 | 98 | Roofs, HSG C (POST 1.0, POST 2.0) |
| 0.714 | 98 | Roofs, HSG D (POST 1.0) |
| 31.609 | 82 | TOTAL AREA |

## L-0700-26 POST P2

Prepared by Tighe \& Bond
Printed 7/13/2023
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Page 3

## Soil Listing (all nodes)

| Area <br> $($ acres $)$ | Soil <br> Group | Subcatchment <br> Numbers |
| ---: | :--- | :--- |
| 0.000 | HSG A |  |
| 3.586 | HSG B | POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4 |
| 25.705 | HSG C | POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0 |
| 2.318 | HSG D | POST 1.0, POST 1.3, POST 1.4 |
| 0.000 | Other |  |
| 31.609 |  | TOTAL AREA |

Time span $=0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}, 481$ points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED $\begin{gathered}\text { Runoff Area=440,332 sf } 71.42 \% \text { Impervious Runoff Depth }>2.61 \text { " } \\ \text { Flow Length }=933^{\prime} \quad \text { Tc }=11.4 \mathrm{~min} \quad \mathrm{CN}=90 \text { Runoff }=25.38 \mathrm{cfs} 2.201 \text { af }\end{gathered}$
SubcatchmentPOST 1.1: WATERSHED Runoff Area=157,428 sf $30.68 \%$ Impervious Runoff Depth $>1.63$ " Flow Length=464' $\mathrm{Tc}=8.3 \mathrm{~min} \quad \mathrm{CN}=78$ Runoff $=6.25 \mathrm{cfs} 0.492$ af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 sf $58.28 \%$ Impervious Runoff Depth $>2.34$ " Flow Length=1,191' Tc=6.4 min CN=87 Runoff=6.94 cfs 0.511 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 sf $23.27 \%$ Impervious Runoff Depth>1.62" Flow Length=1,525' Tc=45.9 min CN=78 Runoff=5.96 cfs 0.929 af

SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf $0.42 \%$ Impervious Runoff Depth $>1.36^{\prime \prime}$ Flow Length=585' Tc=13.5 min CN=74 Runoff=8.76 cfs 0.822 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area $=49,336 \mathrm{sf} 53.76 \%$ Impervious Runoff Depth $>2.34$ " Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \quad \mathrm{CN}=87$ Runoff $=3.10 \mathrm{cfs} 0.221$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.63' Max Vel=2.08 fps Inflow=6.94 cfs 0.511 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0$ ' $\mathrm{S}=0.0092$ '/' Capacity=2,720.29 cfs Oufflow=4.97 cfs 0.507 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=46.02' Storage=67,987 cf Inflow=25.38 cfs 2.201 af Primary $=0.96$ cfs 0.874 af Secondary $=0.00$ cfs 0.000 af Outflow= 0.96 cfs 0.874 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=52.38' Storage=21,415 cf Inflow=6.25 cfs 0.492 af Outflow=0.00 cfs 0.000 af

Pond POND 1.2: PDMH203
Peak Elev=50.38' Inflow=6.94 cfs 0.511 af 48.0" Round Culvert $n=0.013$ L=269.0' $\mathrm{S}=0.0050$ '//' Outflow=6.94 cfs 0.511 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' Storage=8,981 cf Inflow=9.25 cfs 3.060 af Primary $=9.25$ cfs 2.856 af Secondary $=0.00$ cfs 0.000 af Outflow= 9.25 cfs 2.856 af

Pond POND 1.4: SEDIMENTBASIN $1.0 \quad$ Peak Elev=44.62' Storage=21,007 cf Inflow=8.76 cfs 0.822 af Primary $=0.51$ cfs 0.751 af Secondary $=0.00$ cfs 0.000 af Outflow $=0.51$ cfs 0.751 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS

Inflow=0.00 cfs 0.000 af Primary $=0.00$ cfs 0.000 af

Inflow=9.25 cfs 2.856 af Primary $=9.25$ cfs 2.856 af

Inflow=3.10 cfs 0.221 af Primary $=3.10$ cfs 0.221 af

Total Runoff Area $=31.609$ ac Runoff Volume $=5.176$ af Average Runoff Depth = 1.96" 61.73\% Pervious = 19.513 ac $38.27 \%$ Impervious $=12.096$ ac

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf $71.42 \%$ Impervious Runoff Depth $>4.43$ " Flow Length=933' $\quad \mathrm{c}=11.4 \mathrm{~min} \quad \mathrm{CN}=90$ Runoff=42.01 cfs 3.732 af

SubcatchmentPOST 1.1: WATERSHED Runoff Area $=157,428$ sf $30.68 \%$ Impervious Runoff Depth $>3.21$ " Flow Length=464' Tc=8.3 min CN=78 Runoff=12.40 cfs 0.966 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 sf $58.28 \%$ Impervious Runoff Depth $>4.11$ " Flow Length=1,191' Tc=6.4 min CN=87 Runoff=11.94 cfs 0.897 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 sf 23.27\% Impervious Runoff Depth>3.18" Flow Length=1,525' Tc=45.9 min CN=78 Runoff=11.87 cfs 1.826 af

SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf $0.42 \%$ Impervious Runoff Depth $>2.83$ " Flow Length=585' Tc=13.5 min CN=74 Runoff=18.77 cfs 1.708 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,336 sf $53.76 \%$ Impervious Runoff Depth $>4.11^{\prime \prime}$ Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \quad \mathrm{CN}=87$ Runoff $=5.36 \mathrm{cfs} 0.388$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.82' Max Vel=2.20 fps Inflow=11.94 cfs 0.897 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0$ ' $\mathrm{S}=0.0092$ '/' Capacity=2,720.29 cfs Outflow=6.12 cfs 0.891 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=46.78' Storage=83,438 cf Inflow=42.01 cfs 3.732 af Primary=$=9.22$ cfs 2.105 af Secondary=5.86 cfs 0.170 af Outflow=15.08 cfs 2.275 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=54.11' Storage=42,049 cf Inflow=12.40 cfs 0.966 af Outflow= 0.00 cfs 0.000 af

Pond POND 1.2: PDMH203
Peak Elev=50.72' Inflow=11.94 cfs 0.897 af 48.0" Round Culvert $\mathrm{n}=0.013 \mathrm{~L}=269.0^{\prime} \mathrm{S}=0.0050$ '/' Outflow=11.94 cfs 0.897 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.77' Storage=13,560 cf Inflow=31.34 cfs 5.942 af Primary $=31.22$ cfs 5.655 af Secondary= 0.00 cfs 0.000 af Outflow=31.22 cfs 5.655 af

Pond POND 1.4: SEDIMENTBASIN 1.0 Peak Elev=45.79' Storage=50,580 cf Inflow=18.77 cfs 1.708 af Primary $=0.68$ cfs 0.950 af Secondary $=0.00$ cfs 0.000 af Outflow= 0.68 cfs 0.950 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS
Inflow=0.00 cfs 0.000 af Primary $=0.00$ cfs 0.000 af

Inflow=31.22 cfs 5.655 af Primary $=31.22$ cfs 5.655 af

Inflow=5.36 cfs 0.388 af Primary $=5.36$ cfs 0.388 af

Total Runoff Area $=31.609$ ac Runoff Volume $=9.517$ af Average Runoff Depth $=3.61$ " $61.73 \%$ Pervious $=19.513$ ac $38.27 \%$ Impervious $=12.096$ ac

## Summary for Subcatchment POST 1.0: WATERSHED 1.0

Runoff = 42.01 cfs @ 12.16 hrs, Volume= 3.732 af, Depth> 4.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

|  | Area (sf) | CN | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5,235 | 98 | Roofs, HSG B |  |  |
|  | 29,148 | 61 | >75\% Grass cover, Good, HSG B |  |  |
|  | 18,966 | 98 | Paved parking, HSG B |  |  |
|  | 143,455 | 98 | Roofs, HSG C |  |  |
|  | 82,022 | 74 > | >75\% Grass cover, Good, HSG C |  |  |
|  | 110,236 | 98 P | Paved parking, HSG C |  |  |
|  | 31,119 | 98 | Roofs, HSG D |  |  |
|  | 14,671 | 80 | >75\% Grass cover, Good, HSG D |  |  |
|  | 5,480 | 98 | Paved parking, HSG D |  |  |
| 440,332 |  | 90 |  |  |  |
|  | 125,841 |  | 28.58\% Pervious Area |  |  |
| 314,491 |  |  | 71.42\% Impervious Area |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | $\begin{array}{r} \text { c } \begin{array}{r} \text { Length } \\ \text { (feet) } \\ \hline \end{array}{ }^{2} \end{array}$ | Slope (ft/ft) | Velocity (ft/sec) | $\begin{array}{r} \text { Capacity } \\ \text { (cfs) } \\ \hline \end{array}$ | Description |
| 7.7 | 70 | 0.0150 | 0.15 |  | Sheet Flow, Grass: Short n=0.150 P2=3.68" |
| 0.2 | 232 | 0.0200 | - 2.87 |  | Shallow Concentrated Flow, |
|  |  |  |  |  | Paved Kv= 20.3 fps |
| 0.1 | 19 | 0.0200 | - 2.12 |  | Shallow Concentrated Flow, |
|  |  |  |  |  | Grassed Waterway Kv= 15.0 fps |
| 0.8 | 8162 | 0.0050 | - 3.21 | 2.52 | Pipe Channel, |
|  |  |  |  |  | 12.0" Round Area= 0.8 sf Perim=3.1' r= $0.25^{\prime}$ $\mathrm{n}=0.013$ Corrugated PE, smooth interior |
| 0.4 | 484 | 0.0050 | - 3.21 | 2.52 | Pipe Channel, |
|  |  |  |  |  | $\begin{aligned} & \text { 12.0" Round Area= } 0.8 \mathrm{sf} \text { Perim= } 3.1^{\prime} \mathrm{r}=0.25^{\prime} \\ & \mathrm{n}=0.013 \end{aligned}$ |
| 0.5 | 5113 | 0.0050 | - 3.72 | 4.57 | Pipe Channel, |
|  |  |  |  |  | 15.0" Round Area= 1.2 sf Perim=3.9' r= 0.31' $\mathrm{n}=0.013$ |
| 1.2 | 2299 | 0.0050 | - 4.20 | 7.43 | Pipe Channel, |
|  |  |  |  |  | $\begin{aligned} & \text { 18.0" Round Area= } 1.8 \text { sf Perim= } 4.7^{\prime} r=0.38^{\prime} \\ & n=0.013 \end{aligned}$ |
| 0.4 | 494 | 0.0050 | - 4.20 | 7.43 | Pipe Channel, |
|  |  |  |  |  | $\begin{aligned} & \text { 18.0" Round Area= } 1.8 \mathrm{sf} \text { Perim= } 4.7^{\prime} \mathrm{r}=0.38^{\prime} \\ & \mathrm{n}=0.013 \end{aligned}$ |
| 0.1 | 146 | 0.0240 | -11.16 | 35.05 | Pipe Channel, |
|  |  |  |  |  | $\begin{aligned} & \text { 24.0" Round Area= } 3.1 \text { sf Perim= } 6.3^{\prime} \mathrm{r}=0.50^{\prime} \\ & \mathrm{n}=0.013 \end{aligned}$ |
| 0.0 | 5 | 0.0800 | -7.16 | 0.98 | Pipe Channel, |
|  |  |  |  |  | 5.0" Round Area= 0.1 sf Perim= 1.3' r=0.10' |
|  |  |  |  |  | $n=0.013$ |
| 0.0 | 0 | 0.0110 | - 9.90 | 69.95 | Pipe Channel, |

36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
$\mathrm{n}=0.013$
11.4933 Total

## Summary for Subcatchment POST 1.1: WATERSHED 1.1

Runoff $=12.40$ cfs @ 12.12 hrs, Volume $=0.966$ af, Depth> 3.21"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

|  | ea (sf) | CN 61 | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 36,403 |  | >75\% Grass cover, Good, HSG B |  |  |
|  | 3,210 | 98 | Paved parking, HSG B |  |  |
|  | 72,719 | 74 | >75\% Grass cover, Good, HSG C |  |  |
|  | 45,096 | 98 | Paved parking, HSG C |  |  |
|  | 57,428 | 78 | Weighted Average 69.32\% Pervious Area 30.68\% Impervious Are |  |  |
|  | 09,122 |  |  |  |  |
|  | 48,306 |  |  |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
| 5.8 | 100 |  | 0.29 |  | Sheet Flow, Grass: Short $\mathrm{n}=0.150 \quad \mathrm{P} 2=3.68{ }^{\prime \prime}$ |
| 2.2 | 312 | 0.0220 | 2.39 |  | Shallow Concentrated Flow, Unpaved Kv= 16.1 fps |
| 0.3 | 33 | 0.0150 | 1.84 |  | Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps |
| 0.0 | 19 | 0.3300 | 8.62 |  | Shallow Concentrated Flow, Grassed Waterway Kv=15.0 fps |
| 8.3 | 464 | Total |  |  |  |

## Summary for Subcatchment POST 1.2: WATERSHED 1.2

Runoff $=11.94$ cfs @ 12.09 hrs, Volume $=\quad 0.897$ af, Depth> 4.11"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

| Area (sf) | CN | Description |
| ---: | ---: | :--- |
| 9,848 | 61 | $>75 \%$ Grass cover, Good, HSG B |
| 4,784 | 98 | Paved parking, HSG B |
| 37,701 | 74 | $>75 \%$ Grass cover, Good, HSG C |
| 61,646 | 98 | Paved parking, HSG C |
| 113,979 | 87 | Weighted Average |
| 47,549 |  | $41.72 \%$ Pervious Area |
| 66,430 |  | $58.28 \%$ Impervious Area |


| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \end{array}$ | Length (feet) | Slope <br> (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1.5 | 100 | 0.0100 | 1.12 |  | Sheet Flow, <br> Smooth surfaces $n=0.011 \quad \mathrm{P} 2=3.68$ " |
| 1.0 | 153 | 0.0150 | 2.49 |  | Shallow Concentrated Flow, Paved Kv= 20.3 fps |
| 1.6 | 343 | 0.0050 | 3.47 | 2.73 | Pipe Channel, <br> 12.0" Round Area= 0.8 sf Perim=3.1' $\mathrm{r}=0.25^{\prime}$ $\mathrm{n}=0.012$ Concrete pipe, finished |
| 0.1 | 13 | 0.0050 | 3.72 | 4.57 | Pipe Channel, <br> 15.0" Round Area= 1.2 sf Perim=3.9' $\mathrm{r}=0.31^{\prime}$ <br> $n=0.013$ Corrugated $P E$, smooth interior |
| 1.8 | 453 | 0.0050 | 4.20 | 7.43 | Pipe Channel, <br> 18.0" Round Area= 1.8 sf Perim=4.7' r=0.38' $\mathrm{n}=0.013$ Corrugated PE , smooth interior |
| 0.4 | 129 | 0.0050 | 5.91 | 29.00 | Pipe Channel, <br> 30.0" Round Area= 4.9 sf Perim= 7.9' r= $0.63^{\prime}$ <br> $\mathrm{n}=0.013$ Corrugated PE , smooth interior |

6.4 1,191 Total

## Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff $=11.87$ cfs @ 12.63 hrs, Volume= 1.826 af, Depth> 3.18"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"


## Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff = 18.77 cfs @ 12.19 hrs, Volume= 1.708 af, Depth> 2.83"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"


## Summary for Subcatchment POST 2.0: WATERSHED 2.0

[49] Hint: Tc<2dt may require smaller dt
Runoff $=5.36$ cfs @ 12.07 hrs, Volume= 0.388 af, Depth> 4.11"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

| Area (sf) | CN | Description |
| ---: | ---: | :--- |
| 10,145 | 98 | Roofs, HSG C |
| 22,815 | 74 | $>75 \%$ Grass cover, Good, HSG C |
| 16,376 | 98 | Paved parking, HSG C |
| 49,336 | 87 | Weighted Average |
| 22,815 |  | 46.24\% Pervious Area |
| 26,521 |  | $53.76 \%$ Impervious Area |


| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | $\begin{gathered} \text { Capacity } \\ \text { (cfs) } \end{gathered}$ | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1.2 | 100 | 0.0164 | 1.36 |  | Sheet Flow, <br> Smooth surfaces $\mathrm{n}=0.011 \quad \mathrm{P} 2=3.68$ " |
| 0.3 | 48 | 0.0164 | 2.60 |  | Shallow Concentrated Flow, Paved Kv=20.3 fps |
| 0.3 | 130 | 0.0140 | 7.03 | 12.43 | Pipe Channel, <br> 18.0" Round Area= 1.8 sf Perim= $4.7^{\prime} \mathrm{r}=0.38^{\prime}$ $\mathrm{n}=0.013$ |
| 0.5 | 70 | 0.0250 | 2.37 |  | Shallow Concentrated Flow, Grassed Waterway Kv=15.0 fps |
| 1.3 | 410 | 0.0050 | 5.09 | 16.00 | Pipe Channel, <br> 24.0" Round Area= 3.1 sf Perim=6.3' r= 0.50' $\mathrm{n}=0.013$ |

$3.6 \quad 758$ Total, Increased to minimum Tc $=5.0 \mathrm{~min}$

## Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

|  | $6.231 \mathrm{ac}, 42.27 \%$ Impervious, Inflow Depth > 1.73" for 10 Year event |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Inflow |  |  |  |  |
| Outflow | 6.12 cfs @ | 12.86 hrs , Volume= | 0.891 af, | = 49\%, Lag= 45.9 |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Max. Velocity $=2.20 \mathrm{fps}$, Min. Travel Time $=9.9 \mathrm{~min}$
Avg. Velocity $=0.85 \mathrm{fps}$, Avg. Travel Time $=25.6 \mathrm{~min}$
Peak Storage= 6,846 cf @ 12.27 hrs
Average Depth at Peak Storage= 0.82'
Bank-Full Depth=6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs
Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals)
Constant $\mathrm{n}=0.040$ Winding stream, pools \& shoals
Inlet Invert= 48.00', Outlet Invert= 36.00'


| Offset <br> (feet) | Elevation <br> (feet) | Chan. Depth <br> (feet) |
| ---: | ---: | ---: |
| 0.00 | 12.00 | 0.00 |
| 18.00 | 6.00 | 6.00 |
| 30.25 | 6.00 | 6.00 |
| 31.75 | 5.25 | 6.75 |
| 34.25 | 5.25 | 6.75 |
| 35.75 | 6.00 | 6.00 |
| 48.00 | 6.00 | 6.00 |
| 66.00 | 12.00 | 0.00 |


| Depth <br> (feet) | End Area <br> (sq-ft) | Perim. <br> (feet) | Storage <br> (cubic-feet) | Discharge <br> (cfs) |
| ---: | ---: | ---: | ---: | ---: |
| 0.00 | 0.0 | 2.5 | 0 | 0.00 |
| 0.75 | 3.0 | 30.4 | 3,927 | 2.28 |
| 6.75 | 291.0 | 68.3 | 380,919 | $2,720.29$ |

## Summary for Pond POND 1.0: GRAVEL WETLAND 1

[95] Warning: Outlet Device \#4 rise exceeded

| Inflow Area | 10.109 ac, $71.42 \%$ Impervious, Inflow Depth > 4.43" for 10 Year event |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Inflow | 42.01 cfs @ | 12.16 hrs , Volume= | 3.732 af |  |
| Outflow | 15.08 cfs @ | 12.50 hrs , Volume= | 2.275 af, | Atten= 64\%, Lag= 20.8 min |
| Primary | 9.22 cfs @ | 12.50 hrs , Volume= | 2.105 af |  |
| Secondary = | 5.86 cfs @ | 12.50 hrs , Volume= | 0.170 af |  |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 46.78' @ 12.50 hrs Surf.Area= 21,240 sf Storage= 83,438 cf Flood Elev= 48.00' Surf.Area= 23,557 sf Storage $=110,845$ cf

Plug-Flow detention time= 226.3 min calculated for 2.275 af ( $61 \%$ of inflow)
Center-of-Mass det. time= 125.2 min ( 916.2 - 791.0 )

| Volume | Invert | Avail.Storage | Storage Description |
| :---: | ---: | ---: | ---: |
| $\# 1$ | $39.05^{\prime}$ | 110,845 cf | Custom Stage Data (Prismatic)Listed below (Recalc) |


| Elevation <br> (feet) | Surf.Area <br> (sq-ft) | Voids <br> $(\%)$ | Inc.Store <br> (cubic-feet) | Cum.Store <br> (cubic-feet) |
| ---: | ---: | ---: | ---: | ---: |
| 39.05 | 9,855 | 0.0 | 0 | 0 |
| 41.35 | 9,855 | 30.0 | 6,800 | 6,800 |
| 42.00 | 9,855 | 45.0 | 2,883 | 9,683 |
| 43.00 | 1,943 | 100.0 | 10,899 | 20,582 |
| 44.00 | 14,202 | 100.0 | 13,073 | 33,654 |
| 45.00 | 16,891 | 100.0 | 15,547 | 49,201 |
| 46.00 | 19,752 | 100.0 | 18,322 | 67,522 |
| 47.00 | 21,668 | 100.0 | 20,710 | 88,232 |
| 48.00 | 23,557 | 100.0 | 22,613 | 110,845 |


| Device | Routing | Invert | Outlet Devices |
| :---: | :---: | :---: | :---: |
| \#1 | Primary | 41.35' | 18.0" Round Culvert |
|  |  |  | $\mathrm{L}=30.0^{\prime}$ CPP, square edge headwall, $\mathrm{Ke}=0.500$ |
|  |  |  | Inlet / Outlet Invert= 41.35' / 41.20' S=0.0050 '/' Cc= 0.900 |
|  |  |  | $\mathrm{n}=0.013$ Corrugated PE, smooth interior, Flow Area= 1.77 sf |
| \#2 | Device 1 | 41.35' | 3.5" Vert. Orifice/Grate $\mathrm{C}=0.600$ |
| \#3 | Device 1 | 45.00' | 3.0" Vert. Orifice/Grate $\mathrm{C}=0.600$ |
| \#4 | Device 1 | 46.00' | 4.0' long x 0.50 ' rise Sharp-Crested Rectangular Weir 2 End Contraction(s) 0.5 Crest Height |
| \#5 | Device 1 | 47.00' | 4.0" x 4.0" Horiz. Orifice/Grate X $106.00 \mathrm{C}=0.600$ |
|  |  |  | Limited to weir flow at low heads |
| \#6 | Secondary | 46.50' | 15.0' long x 15.0' breadth Broad-Crested Rectangular Weir |
|  |  |  | Head (feet) 0.200 .400 .600 .801 .001 .201 .401 .60 |
|  |  |  | Coef. (English) 2.682 .702 .702 .642 .632 .642 .642 .63 |

Primary OutFlow Max=9.22 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater)
-1=Culvert (Passes 9.22 cfs of 18.40 cfs potential flow)
-2=Orifice/Grate (Orifice Controls 0.74 cfs @ 11.06 fps)
-3=Orifice/Grate (Orifice Controls 0.30 cfs @ 6.19 fps)
4=Sharp-Crested Rectangular Weir(Orifice Controls 8.17 cfs @ 4.19 fps$)$
$-5=$ Orifice/Grate ( Controls 0.00 cfs )
Secondary OutFlow Max=5.85 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater)
${ }^{L_{6}}=$ Broad-Crested Rectangular Weir(Weir Controls 5.85 cfs @ 1.41 fps )

## Summary for Pond POND 1.1: GRAVEL WETLAND 2



Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev=54.11' @ 24.00 hrs Surf.Area= $14,115 \mathrm{sf}$ Storage $=42,049 \mathrm{cf}$
Flood Elev=57.00' Surf.Area=21,643 sf Storage= $94,743 \mathrm{cf}$
Plug-Flow detention time=(not calculated: initial storage exceeds outflow)
Center-of-Mass det. time= (not calculated: no outflow)

| Volume | Invert | Avail.Storage | Storage Description |
| :---: | ---: | ---: | ---: |
| $\# 1$ | $47.55^{\prime}$ | $117,304 \mathrm{cf}$ | Custom Stage Data (Prismatic)Listed below (Recalc) |


| Elevation <br> (feet) | Surf.Area <br> (sq-ft) | Voids <br> (\%) | Inc.Store <br> (cubic-feet) | Cum.Store <br> (cubic-feet) |
| ---: | ---: | ---: | ---: | ---: |
| 47.55 | 6,269 | 0.0 | 0 | 0 |
| 49.85 | 6,269 | 30.0 | 4,326 | 4,326 |
| 50.50 | 6,269 | 45.0 | 1,834 | 6,159 |
| 51.00 | 7,199 | 100.0 | 3,367 | 9,526 |
| 52.00 | 9,187 | 100.0 | 8,193 | 17,719 |
| 53.00 | 11,345 | 100.0 | 10,266 | 27,985 |
| 54.00 | 13,814 | 100.0 | 12,580 | 40,565 |
| 55.00 | 16,645 | 100.0 | 15,230 | 55,794 |
| 56.00 | 19,805 | 100.0 | 18,225 | 74,019 |
| 58.00 | 23,480 | 100.0 | 43,285 | 117,304 |


| Device | Routing | Invert | Outlet Devices |
| :---: | :---: | :---: | :---: |
| \#1 | Primary | 49.85' | 24.0" Round Culvert |
|  |  |  | $\mathrm{L}=12.0{ }^{\prime}$ CPP, square edge headwall, $\mathrm{Ke}=0.500$ |
|  |  |  | Inlet / Outlet Invert= 49.85' / 49.45' S=0.0333 '/' Cc= 0.900 |
|  |  |  | $\mathrm{n}=0.013$ Corrugated PE, smooth interior, Flow Area= 3.14 sf |
| \#2 | Device 1 | 49.85' | 2.0" Vert. Orifice/Grate $\mathrm{C}=0.600$ |
| \#3 | Device 1 | 53.50' | 4.0' long x 2.00 ' rise Sharp-Crested Rectangular Weir 2 End Contraction(s) |
| \#4 | Device 1 | 56.50' | 4.0 " 4.0 " Horiz. Orifice/Grate X $106.00 \mathrm{C}=0.600$ |
|  |  |  | Limited to weir flow at low heads |
| Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=47.55' TW=55.07' (Dynamic Tailwater) $L_{1=C u l v e r t}$ ( Controls 0.00 cfs ) |  |  |  |
| -2=Orifice/Grate ( Controls 0.00 cfs ) |  |  |  |
| - $\mathbf{4 = S h a r p - C r e s t e d ~ R e c t a n g u l a r ~ W e i r ~ ( ~ C o n t r o l s ~} 0.00 \mathrm{cfs}$ ) |  |  |  |
|  |  |  |  |  |  |

## Summary for Pond POND 1.2: PDMH203



Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 50.72' @ 12.09 hrs
Flood Elev= 57.00'

| Device | Routing | Invert | Outlet Devices |
| :---: | :--- | :--- | :--- |
| $\# 1$ | Primary | $49.35^{\prime}$ | $48.0^{\prime \prime}$ Round Culvert |
|  |  | L= 269.0' CPP, projecting, no headwall, Ke= $=0.900$ |  |
|  |  | Inlet / Outlet Invert= $49.35^{\prime} / 48.00^{\prime} \quad \mathrm{S}=0.0050 \mathrm{Cc}=0.900$ |  |
|  |  | $\mathrm{n}=0.013$ Corrugated PE, smooth interior, Flow Area= 12.57 sf |  |

Primary OutFlow Max=11.76 cfs @ 12.09 hrs HW=50.71' TW=48.76' (Dynamic Tailwater)
—1=Culvert (Inlet Controls 11.76 cfs @ 3.13 fps )

## Summary for Pond POND 1.3: OUTLET CULVERTS

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=12)
[62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.58' @ 23.95 hrs
Inflow Area $=30.477$ ac, $37.69 \%$ Impervious, Inflow Depth > 2.34" for 10 Year event
Inflow = 31.34 cfs @ 12.51 hrs, Volume= 5.942 af
Outflow = 31.22 cfs @ 12.53 hrs , Volume= 5.655 af , Atten= 0\%, Lag= 1.3 min
Primary $=31.22$ cfs @ 12.53 hrs , Volume $=\quad 5.655 \mathrm{af}$
Secondary $=\quad 0.00$ cfs @ 0.00 hrs , Volume= 0.000 af
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 38.77' @ 12.53 hrs Surf.Area= 8,870 sf Storage= 13,560 cf
Flood Elev=43.50' Surf.Area= 95,977 sf Storage $=236,017$ cf
Plug-Flow detention time $=56.2$ min calculated for 5.642 af ( $95 \%$ of inflow)
Center-of-Mass det. time $=29.8 \mathrm{~min}(900.3-870.4)$

| Volume | Invert | Avail.Storage | Storage Description |
| :---: | ---: | ---: | ---: |
| $\# 1$ | $35.00^{\prime}$ | 236,017 cf | Custom Stage Data (Prismatic)Listed below (Recalc) |


| Elevation <br> (feet) | Surf.Area <br> (sq-ft) | Inc.Store <br> (cubic-feet) | Cum.Store <br> (cubic-feet) |
| ---: | ---: | ---: | ---: |
| 35.00 | 960 | 0 | 0 |
| 36.00 | 1,428 | 1,194 | 1,194 |
| 38.00 | 5,418 | 6,846 | 8,040 |
| 40.00 | 14,354 | 19,772 | 27,812 |
| 42.00 | 66,884 | 81,238 | 109,050 |
| 43.00 | 92,707 | 79,796 | 188,846 |
| 43.50 | 95,977 | 47,171 | 236,017 |

Device Routing Invert Outlet Devices


Primary OutFlow Max=31.11 cfs @ 12.53 hrs HW=38.77' TW=38.65' (Dynamic Tailwater)
——=CMP_Arch_1/2 42x29 (Outlet Controls 31.11 cfs @ 1.55 fps )
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=35.04' TW=38.65' (Dynamic Tailwater)
L-2=Sharp-Crested Vee/Trap Weir ( Controls 0.00 cfs)

## Summary for Pond POND 1.4: SEDIMENT BASIN 1.0



Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Starting Elev=44.15' Surf.Area= 18,132 sf Storage= 11,702 cf
Peak Elev= 45.79' @ 17.24 hrs Surf.Area= 29,244 sf Storage $=50,580 \mathrm{cf}$ ( 38,878 cf above start)
Flood Elev=48.50' Surf.Area= 38,802 sf Storage $=127,441$ cf (115,739 cf above start)
Plug-Flow detention time $=356.9$ min calculated for 0.681 af ( $40 \%$ of inflow)
Center-of-Mass det. time $=9.2 \mathrm{~min}(846.8-837.5)$

| Volume | Invert | t Avail.Storage Storage Description |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| \#1 | 43.00 | ' 127,441 cf Cus |  | tage Data (Prismatic)Listed below | (Recalc) |
| Elevation (feet) | $\begin{array}{rr} n \\ t) & \begin{array}{r} \text { Surf.Area } \\ (\mathrm{sq}-\mathrm{ft}) \end{array} \\ \hline \end{array}$ |  | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |  |
| 43.00 |  | 1,000 | 0 | 0 |  |
| 44.00 |  | 17,117 | 9,059 | 9,059 |  |
| 46.00 |  | 30,657 | 47,774 | 56,833 |  |
| 47.00 |  | 35,879 | 33,268 | 90,101 |  |
| 48.00 |  | 38,802 | 37,341 | 127,441 |  |
| Device | Routing | Invert | Outlet Devices |  |  |
| \#1 | Primary | 42.75' | 12.0" Round Inlet / Outle $\mathrm{n}=0.013$, | ulvert $L=66.0^{\prime} \quad \mathrm{Ke}=0.500$ <br> ert= $42.75^{\prime} / 42.40^{\prime} \quad S=0.00531 /$ <br> Area $=0.79 \mathrm{sf}$ | $\mathrm{Cc}=0.900$ |
| \#2 | Device 1 | $43.00{ }^{\prime}$ | 4.0" Vert. | e/Grate C= 0.600 |  |
| \#3 | Device 1 | 46.80' | $10.0 " \times 17$ <br> Limited to | oriz. Orifice/Grate C= 0.600 fow at low heads |  |
| \#4 | Secondary | 47.40' | Custom W <br> Head (feet) <br> Width (feet) | $\begin{aligned} & \text { Orifice, } C v=2.62(C=3.28) \\ & 01.10 \\ & 0014.60 \end{aligned}$ |  |

Primary OutFlow Max=0.68 cfs @ 17.24 hrs HW=45.79' TW=38.65' (Dynamic Tailwater)
L1=Culvert (Passes 0.68 cfs of 5.16 cfs potential flow)
-2=Orifice/Grate (Orifice Controls 0.68 cfs @ 7.80 fps )
$\square_{3=O r i f i c e / G r a t e ~(~ C o n t r o l s ~} 0.00 \mathrm{cfs}$ )
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=44.15' TW=35.04' (Dynamic Tailwater)
$L_{4=C u s t o m ~ W e i r / O r i f i c e ~(~ C o n t r o l s ~} 0.00 \mathrm{cfs}$ )

## Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.
[80] Warning: Exceeded Pond POND 1.1 by 7.52 ' @ 0.00 hrs (23.95 cfs 41.618 af)

| Inflow Area $=$ | 3.614 ac, | $30.68 \%$ | Impervious, Inflow Depth $=0.00 "$ for 10 Year event |  |
| :--- | :--- | :--- | :--- | :--- |
| Inflow | $=$ | $0.00 \mathrm{cfs} @$ | 0.00 hrs, Volume | 0.000 af |
| Primary | $=$ | $0.00 \mathrm{cfs} @$ | 0.00 hrs, Volume $=$ | 0.000 af , Atten $=0 \%$, Lag $=0.0 \mathrm{~min}$ |

Primary outflow $=$ Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

| 10 Year 25 | Point manual elevation table, To= $0.00 \mathrm{hrs}, \mathrm{dt}=1.00 \mathrm{hrs}$, feet $=$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 |
| 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 |
| 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 |  |  |

## Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.
[80] Warning: Exceeded Pond POND 1.3 by 3.61 ' @ 0.00 hrs ( 92.51 cfs 60.023 af)


Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
10 Year 2 Point manual elevation table, To= $0.00 \mathrm{hrs}, \mathrm{dt}=24.00 \mathrm{hrs}$, feet $=$ $38.65 \quad 38.65$

## Summary for Link PA2: POINT OF ANALYSIS



Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf $71.42 \%$ Impervious Runoff Depth $>5.88$ " Flow Length=933' $\quad$ cc=11.4 min $C N=90$ Runoff=54.93 cfs 4.956 af

SubcatchmentPOST 1.1: WATERSHED Runoff Area $=157,428$ sf $30.68 \%$ Impervious Runoff Depth $>4.53$ " Flow Length=464' Tc=8.3 min CN=78 Runoff=17.44 cfs 1.365 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 sf $58.28 \%$ Impervious Runoff Depth $>5.54$ " Flow Length=1,191' Tc=6.4 min CN=87 Runoff=15.85 cfs 1.209 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 sf 23.27\% Impervious Runoff Depth>4.50" Flow Length=1,525' Tc=45.9 min CN=78 Runoff=16.75 cfs 2.583 af

SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf $0.42 \%$ Impervious Runoff Depth $>4.09$ " Flow Length=585' Tc=13.5 min CN=74 Runoff=27.23 cfs 2.472 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area $=49,336 \mathrm{sf} 53.76 \%$ Impervious Runoff Depth $>5.54$ " Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \quad \mathrm{CN}=87$ Runoff $=7.12 \mathrm{cfs} 0.523$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.87' Max Vel=2.22 fps Inflow=15.85 cfs 1.209 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0$ ' $\mathrm{S}=0.0092$ '/' Capacity=2,720.29 cfs Outflow=8.65 cfs 1.202 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=47.10' Storage=90,424 cf Inflow=54.93 cfs 4.956 af Primary $=19.03$ cfs 2.766 af Secondary= 18.86 cfs 0.671 af Outflow= 37.88 cfs 3.437 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=55.22' Storage=59,446 cf Inflow=17.44 cfs 1.365 af Outflow=0.00 cfs 0.000 af

Pond POND 1.2: PDMH203
Peak Elev=50.94' Inflow=15.85 cfs 1.209 af 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '//' Outflow=15.85 cfs 1.209 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.17' Storage=17,433 cf Inflow=57.33 cfs 8.292 af Primary $=56.26$ cfs 7.985 af Secondary $=0.00$ cfs 0.000 af Outflow=56.26 cfs 7.985 af

Pond POND 1.4: SEDIMENTBASIN 1.0 Peak Elev=46.65' Storage=77,792 cf Inflow=27.23 cfs 2.472 af Primary $=0.78$ cfs 1.070 af Secondary $=0.00$ cfs 0.000 af Outflow= 0.78 cfs 1.070 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS

Inflow=0.00 cfs 0.000 af Primary $=0.00$ cfs 0.000 af

Inflow=56.26 cfs 7.985 af Primary $=56.26$ cfs 7.985 af

Inflow=7.12 cfs 0.523 af Primary=7.12 cfs 0.523 af

Total Runoff Area $=31.609$ ac Runoff Volume $=13.108$ af Average Runoff Depth $=4.98$ " 61.73\% Pervious = 19.513 ac $38.27 \%$ Impervious $=12.096$ ac

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf $71.42 \%$ Impervious Runoff Depth>7.25" Flow Length=933' $\quad$ cc=11.4 min $C N=90$ Runoff=66.89 cfs 6.105 af

SubcatchmentPOST 1.1: WATERSHED Runoff Area=157,428 sf $30.68 \%$ Impervious Runoff Depth $>5.81$ " Flow Length=464' Tc=8.3 min CN=78 Runoff=22.21 cfs 1.750 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 sf $58.28 \%$ Impervious Runoff Depth $>6.89$ " Flow Length=1,191' Tc=6.4 min CN=87 Runoff=19.47 cfs 1.503 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 sf 23.27\% Impervious Runoff Depth>5.77" Flow Length=1,525' Tc=45.9 min CN=78 Runoff=21.37 cfs 3.312 af

SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf $0.42 \%$ Impervious Runoff Depth $>5.33^{\prime \prime}$ Flow Length=585' Tc=13.5 min CN=74 Runoff=35.32 cfs 3.218 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,336 sf $53.76 \%$ Impervious Runoff Depth>6.89" Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \mathrm{CN}=87$ Runoff $=8.76 \mathrm{cfs} 0.651$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.92' Max Vel=2.24 fps Inflow=19.47 cfs 1.503 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0$ ' $\mathrm{S}=0.0092$ '//' Capacity=2,720.29 cfs Outflow=11.76 cfs 1.495 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=47.39' Storage=96,897 cf Inflow=66.89 cfs 6.105 af Primary=19.58 cfs 3.347 af Secondary=33.37 cfs 1.209 af Outflow=52.94 cfs 4.556 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=56.11' Storage=76,209 cf Inflow=22.21 cfs 1.750 af Outflow=0.00 cfs 0.000 af

Pond POND 1.2: PDMH203
Peak Elev=51.13' Inflow=19.47 cfs 1.503 af 48.0" Round Culvert $\mathrm{n}=0.013 \mathrm{~L}=269.0^{\prime} \mathrm{S}=0.0050$ '//' Outflow=19.47 cfs 1.503 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.58' Storage=22,150 cf Inflow=76.91 cfs 10.982 af Primary $=74.09$ cfs 10.655 af Secondary $=0.00$ cfs 0.000 af Outflow= 74.09 cfs 10.655 af

Pond POND 1.4: SEDIMENTBASIN 1.0 Peak Elev=47.02' Storage=90,878 cf Inflow=35.32 cfs 3.218 af Primary $=2.39$ cfs 1.619 af Secondary= 0.00 cfs 0.000 af Outflow=2.39 cfs 1.619 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS
Inflow=0.00 cfs 0.000 af Primary $=0.00$ cfs 0.000 af

Inflow=74.09 cfs 10.655 af Primary $=74.09$ cfs 10.655 af

Inflow=8.76 cfs 0.651 af Primary $=8.76$ cfs 0.651 af

Phase 2 (2024 Amended) Post-Development Calculations



## L-0700-26 POST P2

Prepared by Tighe \& Bond Consulting
Printed 3/1/2024
HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solutions LLC

## Area Listing (all nodes)

| $\begin{array}{r} \text { Area } \\ \text { (acres) } \\ \hline \end{array}$ | CN | Description (subcatchment-numbers) |
| :---: | :---: | :---: |
| 2.312 | 61 | $>75 \%$ Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4) |
| 13.542 | 74 | >75\% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0) |
| 1.467 | 80 | >75\% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4) |
| 0.514 | 58 | Meadow, non-grazed, HSG B (POST 1.3) |
| 1.662 | 71 | Meadow, non-grazed, HSG C (POST 1.3) |
| 0.639 | 98 | Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3) |
| 6.974 | 98 | Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0) |
| 0.137 | 98 | Paved parking, HSG D (POST 1.0, POST 1.3) |
| 0.120 | 98 | Roofs, HSG B (POST 1.0) |
| 3.526 | 98 | Roofs, HSG C (POST 1.0, POST 2.0) |
| 0.714 | 98 | Roofs, HSG D (POST 1.0) |
| 31.609 | 82 | TOTAL AREA |

## L-0700-26 POST P2

Prepared by Tighe \& Bond Consulting
Printed 3/1/2024
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## Soil Listing (all nodes)

| Area <br> $($ acres $)$ | Soil <br> Group | Subcatchment <br> Numbers |
| ---: | :--- | :--- |
| 0.000 | HSG A |  |
| 3.586 | HSG B | POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4 |
| 25.705 | HSG C | POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0 |
| 2.318 | HSG D | POST 1.0, POST 1.3, POST 1.4 |
| 0.000 | Other |  |
| 31.609 |  | TOTAL AREA |

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED $\begin{gathered}\text { Runoff Area=440,332 sf } \\ \text { Flow Length }=933^{\prime} \quad \mathrm{Tc}=11.4 \mathrm{~min} \text { in } \mathrm{CN}=90 \text { Runoff }=25.38 \mathrm{cfs} 2.201 \text { af }\end{gathered}$
SubcatchmentPOST 1.1: WATERSHED Runoff Area $=157,428$ sf $30.92 \%$ Impervious Runoff Depth $>1.63$ " Flow Length=464' Tc=8.3 min CN=78 Runoff $=6.25$ cfs 0.492 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 sf $58.28 \%$ Impervious Runoff Depth $>2.34$ " Flow Length=1,191' Tc=6.4 min CN=87 Runoff=6.94 cfs 0.511 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 sf 23.27\% Impervious Runoff Depth>1.62" Flow Length=1,525' Tc=45.9 min CN=78 Runoff=5.96 cfs 0.929 af

SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf $0.42 \%$ Impervious Runoff Depth $>1.36$ " Flow Length=585' Tc=13.5 min CN=74 Runoff=8.76 cfs 0.822 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,336 sf $53.76 \%$ Impervious Runoff Depth $>2.34$ " Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \quad \mathrm{CN}=87$ Runoff $=3.10 \mathrm{cfs} 0.221$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.63' Max Vel=2.08 fps Inflow=6.94 cfs 0.511 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0^{\prime} \mathrm{S}=0.0092$ '/' Capacity=2,720.29 cfs Outflow=4.97 cfs 0.507 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=46.02' Storage=67,987 cf Inflow=25.38 cfs 2.201 af Primary $=0.96$ cfs 0.874 af Secondary $=0.00$ cfs 0.000 af Outflow=0.96 cfs 0.874 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=52.38' Storage=21,415 cf Inflow=6.25 cfs 0.492 af Outflow=0.00 cfs 0.000 af

Pond POND 1.2: PDMH203
Peak Elev=50.38' Inflow=6.94 cfs 0.511 af 48.0" Round Culvert $n=0.013$ L=269.0' $\mathrm{S}=0.0050$ '// Outflow=6.94 cfs 0.511 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' Storage=8,981 cf Inflow=9.25 cfs 3.060 af Primary $=9.25$ cfs 2.856 af Secondary $=0.00$ cfs 0.000 af Outflow $=9.25$ cfs 2.856 af

Pond POND 1.4: SEDIMENTBASIN $1.0 \quad$ Peak Elev=44.62' Storage=21,007 cf Inflow=8.76 cfs 0.822 af Primary $=0.51$ cfs 0.751 af Secondary $=0.00$ cfs 0.000 af Outflow= 0.51 cfs 0.751 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS

Inflow=0.00 cfs 0.000 af Primary $=0.00$ cfs 0.000 af

Inflow=9.25 cfs 2.856 af Primary $=9.25$ cfs 2.856 af

Inflow=3.10 cfs 0.221 af Primary $=3.10$ cfs 0.221 af

Total Runoff Area $=31.609$ ac Runoff Volume $=5.176$ af Average Runoff Depth $=1.96$ " 61.68\% Pervious = 19.497 ac $38.32 \%$ Impervious $=12.112$ ac

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf $71.49 \%$ Impervious Runoff Depth $>4.43$ " Flow Length=933' $\quad \mathrm{cc}=11.4 \mathrm{~min} \quad \mathrm{CN}=90$ Runoff $=42.01 \mathrm{cfs} 3.732$ af

SubcatchmentPOST 1.1: WATERSHED Runoff Area $=157,428$ sf $30.92 \%$ Impervious Runoff Depth $>3.21$ " Flow Length=464' Tc=8.3 min CN=78 Runoff=12.40 cfs 0.966 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 sf $58.28 \%$ Impervious Runoff Depth $>4.11$ " Flow Length=1,191' Tc=6.4 min CN=87 Runoff=11.94 cfs 0.897 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 sf 23.27\% Impervious Runoff Depth>3.18" Flow Length=1,525' Tc=45.9 min CN=78 Runoff=11.87 cfs 1.826 af

SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf $0.42 \%$ Impervious Runoff Depth $>2.83$ " Flow Length=585' Tc=13.5 min CN=74 Runoff=18.77 cfs 1.708 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,336 sf $53.76 \%$ Impervious Runoff Depth $>4.11^{\prime \prime}$ Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \quad \mathrm{CN}=87$ Runoff $=5.36 \mathrm{cfs} 0.388$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.82' Max Vel=2.20 fps Inflow=11.94 cfs 0.897 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0$ ' $\mathrm{S}=0.0092$ '/' Capacity=2,720.29 cfs Outflow=6.12 cfs 0.891 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=46.78' Storage=83,438 cf Inflow=42.01 cfs 3.732 af Primary=9.22 cfs 2.105 af Secondary=5.86 cfs 0.170 af Outflow=15.08 cfs 2.275 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=54.11' Storage=42,049 cf Inflow=12.40 cfs 0.966 af Outflow=0.00 cfs 0.000 af

Pond POND 1.2: PDMH203
Peak Elev=50.72' Inflow=11.94 cfs 0.897 af 48.0" Round Culvert $\mathrm{n}=0.013 \mathrm{~L}=269.0^{\prime} \mathrm{S}=0.0050$ '/' Outflow=11.94 cfs 0.897 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.77' Storage=13,560 cf Inflow=31.34 cfs 5.942 af Primary $=31.22$ cfs 5.655 af Secondary $=0.00$ cfs 0.000 af Outflow=31.22 cfs 5.655 af

Pond POND 1.4: SEDIMENTBASIN $1.0 \quad$ Peak Elev=45.79' Storage=50,580 cf Inflow=18.77 cfs 1.708 af Primary $=0.68$ cfs 0.950 af Secondary $=0.00$ cfs 0.000 af Outflow $=0.68$ cfs 0.950 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS

Inflow=0.00 cfs 0.000 af Primary $=0.00$ cfs 0.000 af

Inflow=31.22 cfs 5.655 af Primary $=31.22$ cfs 5.655 af

Inflow=5.36 cfs 0.388 af Primary $=5.36$ cfs 0.388 af

Total Runoff Area $=31.609$ ac Runoff Volume $=9.517$ af Average Runoff Depth $=3.61$ " 61.68\% Pervious = 19.497 ac $38.32 \%$ Impervious $=12.112$ ac

## Summary for Subcatchment POST 1.0: WATERSHED 1.0

[47] Hint: Peak is $1668 \%$ of capacity of segment \#4
[47] Hint: Peak is $1668 \%$ of capacity of segment \#5
[47] Hint: Peak is $920 \%$ of capacity of segment \#6
[47] Hint: Peak is $566 \%$ of capacity of segment \#7
[47] Hint: Peak is $566 \%$ of capacity of segment \#8
[47] Hint: Peak is $120 \%$ of capacity of segment \#9
[47] Hint: Peak is $4305 \%$ of capacity of segment \#10
Runoff $=\quad 42.01$ cfs @ 12.16 hrs, Volume=
3.732 af, Depth> 4.43"

Routed to Pond POND 1.0 : GRAVEL WETLAND 1
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

| Area (sf) | CN | Description |
| ---: | ---: | :--- |
| 5,235 | 98 | Roofs, HSG B |
| 29,148 | 61 | $>75 \%$ Grass cover, Good, HSG B |
| 18,966 | 98 | Paved parking, HSG B |
| 143,455 | 98 | Roofs, HSG C |
| 81,718 | 74 | $>75 \%$ Grass cover, Good, HSG C |
| 110,540 | 98 | Paved parking, HSG C |
| 31,119 | 98 | Roofs, HSG D |
| 14,671 | 80 | $>75 \%$ Grass cover, Good, HSG D |
| 5,480 | 98 | Paved parking, HSG D |
| 440,332 | 90 | Weighted Average |
| 125,537 |  | $28.51 \%$ Pervious Area |
| 314,795 |  | $71.49 \%$ Impervious Area |


| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope <br> (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 7.7 | 70 | 0.0150 | 0.15 |  | Sheet Flow, <br> Grass: Short $n=0.150 \quad$ P2 $=3.68 "$ |
| 0.2 | 32 | 0.0200 | 2.87 |  | Shallow Concentrated Flow, Paved Kv= 20.3 fps |
| 0.1 | 19 | 0.0200 | 2.12 |  | Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps |
| 0.8 | 162 | 0.0050 | 3.21 | 2.52 | Pipe Channel, <br> 12.0" Round Area= 0.8 sf Perim=3.1' r= $0.25^{\prime}$ $\mathrm{n}=0.013$ Corrugated PE , smooth interior |
| 0.4 | 84 | 0.0050 | 3.21 | 2.52 | Pipe Channel, <br> 12.0" Round Area= 0.8 sf Perim=3.1' r=0.25' $\mathrm{n}=0.013$ |
| 0.5 | 113 | 0.0050 | 3.72 | 4.57 | Pipe Channel, <br> 15.0" Round Area= 1.2 sf Perim=3.9'r= $0.31^{\prime}$ $\mathrm{n}=0.013$ |
| 1.2 | 299 | 0.0050 | 4.20 | 7.43 | Pipe Channel, <br> 18.0" Round Area= 1.8 sf Perim=4.7'r=0.38' $\mathrm{n}=0.013$ |
| 0.4 | 94 | 0.0050 | 4.20 | 7.43 | Pipe Channel, <br> 18.0" Round Area= 1.8 sf Perim=4.7'r=0.38' $\mathrm{n}=0.013$ |
| 0.1 | 46 | 0.0240 | 11.16 | 35.05 | Pipe Channel, <br> 24.0" Round Area= 3.1 sf Perim=6.3' r= $0.50^{\prime}$ $\mathrm{n}=0.013$ |
| 0.0 | 5 | 0.0800 | 7.16 | 0.98 | Pipe Channel, <br> 5.0" Round Area= 0.1 sf Perim=1.3' r=0.10' $\mathrm{n}=0.013$ |
| 0.0 | 9 | 0.0110 | 9.90 | 69.95 | Pipe Channel, <br> 36.0" Round Area= 7.1 sf Perim= 9.4' r= $0.75^{\prime}$ $\mathrm{n}=0.013$ |

11.4933 Total

## Summary for Subcatchment POST 1.1: WATERSHED 1.1

Runoff $=12.40$ cfs @ 12.12 hrs, Volume $=0.966$ af, Depth> 3.21"
Routed to Pond POND 1.1 : GRAVEL WETLAND 2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= $0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}$ Type III 24-hr 10 Year Rainfall=5.58"

| Area (sf) | CN | Description |
| ---: | ---: | :--- |
| 36,403 | 61 | $>75 \%$ Grass cover, Good, HSG B |
| 3,210 | 98 | Paved parking, HSG B |
| 72,351 | 74 | >75\% Grass cover, Good, HSG C |
| 45,464 | 98 | Paved parking, HSG C |
| 157,428 | 78 | Weighted Average |
| 108,754 |  | 69.08\% Pervious Area |
| 48,674 |  | $30.92 \%$ Impervious Area |


| Tc <br> $(\mathrm{min})$ | Length <br> $(\mathrm{feet})$ | Slope <br> $(\mathrm{ft} / \mathrm{ft})$ | Velocity <br> $(\mathrm{ft} / \mathrm{sec})$ | Capacity <br> $(\mathrm{cfs})$ |
| ---: | ---: | ---: | ---: | :--- |
| 5.8 | 100 | 0.0625 | 0.29 | Sheet Flow, <br> Grass: Short $\mathrm{n}=0.150 \quad$ P2= |
| 2.2 | 312 | 0.0220 | 2.39 | Shallow Concentrated Flow, <br> Unpaved Kv=16.1 fps |
| 0.3 | 33 | 0.0150 | 1.84 | Shallow Concentrated Flow, <br> Grassed Waterway Kv=15.0 fps <br> Shallow Concentrated Flow, <br> Grassed Waterway Kv= 15.0 fps |
| 0.0 | 19 | 0.3300 | 8.62 |  |

## Summary for Subcatchment POST 1.2: WATERSHED 1.2

[47] Hint: Peak is $437 \%$ of capacity of segment \#3
[47] Hint: Peak is $261 \%$ of capacity of segment \#4
[47] Hint: Peak is $161 \%$ of capacity of segment \#5
Runoff = 11.94 cfs @ 12.09 hrs, Volume= 0.897 af, Depth> 4.11"
Routed to Pond POND 1.2 : PDMH203
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

|  | a (sf) | CN D | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 9,848 |  | >75\% Grass cover, Good, HSG B |  |  |
|  | 4,784 | 98 P | Paved parking, HSG B |  |  |
|  | 7,701 | 74 > | >75\% Grass cover, Good, HSG C |  |  |
|  | 1,646 | 98 P | Paved parking, HSG C |  |  |
| 113,979 47,549 66,430 |  | 87 | Weighted Average 41.72\% Pervious Area 58.28\% Impervious Are |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) |  | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
| 1.5 | 100 |  | 0.0100 | 1.12 |  | Sheet Flow, <br> Smooth surfaces $n=0.011 \quad \mathrm{P} 2=3.68$ " |
| 1.0 | 153 | 0.0150 | 2.49 |  | Shallow Concentrated Flow, Paved Kv= 20.3 fps |
| 1.6 | 343 | 0.0050 | 3.47 | 2.73 | Pipe Channel, <br> 12.0" Round Area= 0.8 sf Perim=3.1' r= $0.25^{\prime}$ $\mathrm{n}=0.012$ Concrete pipe, finished |
| 0.1 | 13 | 0.0050 | 3.72 | 4.57 | Pipe Channel, 15.0" Round Area= 1.2 sf Perim=3.9'r=0.31' $\mathrm{n}=0.013$ Corrugated PE , smooth interior |
| 1.8 | 453 | 0.0050 | 4.20 | 7.43 | Pipe Channel, 18.0" Round Area= 1.8 sf Perim=4.7'r= $0.38^{\prime}$ $\mathrm{n}=0.013$ Corrugated PE , smooth interior |
| 0.4 | 129 | 0.0050 | 5.91 | 29.00 | Pipe Channel, <br> 30.0" Round Area= 4.9 sf Perim= 7.9'r= $0.63^{\prime}$ <br> $\mathrm{n}=0.013$ Corrugated PE , smooth interior |

### 6.4 1,191 Total

## Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 11.87 cfs @ 12.63 hrs, Volume= 1.826 af, Depth> 3.18"
Routed to Pond POND 1.3 : OUTLET CULVERTS
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"


## Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff $=18.77$ cfs @ 12.19 hrs, Volume= 1.708 af, Depth> 2.83"
Routed to Pond POND 1.4 : SEDIMENT BASIN 1.0
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"


## Summary for Subcatchment POST 2.0: WATERSHED 2.0

[49] Hint: Tc<2dt may require smaller dt
Runoff $=5.36$ cfs @ 12.07 hrs, Volume $=0.388$ af, Depth> 4.11"

Routed to Link PA2 : POINT OF ANALYSIS
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

$\frac{\mathrm{n}=0.013}{3.6} 758$ Total, Increased to minimum Tc $=5.0 \mathrm{~min}$

## Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)


Routed to Pond POND 1.3 : OUTLET CULVERTS
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Max. Velocity= $2.20 \mathrm{fps}, \mathrm{Min}$. Travel Time $=9.9 \mathrm{~min}$
Avg. Velocity $=0.85 \mathrm{fps}$, Avg. Travel Time $=25.6 \mathrm{~min}$
Peak Storage= 6,846 cf @ 12.27 hrs
Average Depth at Peak Storage= 0.82' , Surface Width= 30.44'
Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs
Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals)
Constant $\mathrm{n}=0.040$ Winding stream, pools \& shoals
Inlet Invert= 48.00', Outlet Invert= 36.00'


| Depth <br> (feet) | End Area <br> (sq-ft) | Perim. <br> (feet) | Width <br> (feet) | Storage <br> (cubic-feet) | Discharge <br> (cfs) |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 0.00 | 0.0 | 2.5 | 0.0 | 0 | 0.00 |
| 0.75 | 3.0 | 30.4 | 30.0 | 3,927 | 2.28 |
| 6.75 | 291.0 | 68.3 | 66.0 | 380,919 | $2,720.29$ |

## Summary for Pond POND 1.0: GRAVEL WETLAND 1

[95] Warning: Outlet Device \#4 rise exceeded


Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev=46.78' @ 12.50 hrs Surf.Area= 21,240 sf Storage= 83,438 cf
Flood Elev=48.00' Surf.Area= 23,557 sf Storage $=110,845$ cf
Plug-Flow detention time $=226.3 \mathrm{~min}$ calculated for 2.275 af ( $61 \%$ of inflow)
Center-of-Mass det. time= 125.2 min (916.2-791.0)

| Volume | Invert Avail.Storage |  | Storage Description |  |
| :---: | :---: | :---: | :---: | :---: |
| \#1 | $39.05{ }^{\prime}$ | 10,845 cf | Custom Stag | ta (Prismatic)_isted below (Recalc) |
| Elevation (feet) | Surf.Area $(\mathrm{sq}-\mathrm{ft})$ | Voids (\%) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
| 39.05 | 9,855 | 0.0 | 0 | 0 |
| 41.35 | 9,855 | 30.0 | 6,800 | 6,800 |
| 42.00 | 9,855 | 45.0 | 2,883 | 9,683 |
| 43.00 | 11,943 | 100.0 | 10,899 | 20,582 |
| 44.00 | 14,202 | 100.0 | 13,073 | 33,654 |
| 45.00 | 16,891 | 100.0 | 15,547 | 49,201 |
| 46.00 | 19,752 | 100.0 | 18,322 | 67,522 |
| 47.00 | 21,668 | 100.0 | 20,710 | 88,232 |
| 48.00 | 23,557 | 100.0 | 22,613 | 110,845 |


| Device | Routing | Invert | Outlet Devices |
| :---: | :---: | :---: | :---: |
| \#1 | Primary | 41.35' | 18.0" Round Culvert |
|  |  |  | $\mathrm{L}=30.0^{\prime} \mathrm{CPP}$, square edge headwall, $\mathrm{Ke}=0.500$ |
|  |  |  | Inlet / Outlet Invert= 41.35' / 41.20' S=0.0050 '/' Cc= 0.900 |
|  |  |  | $\mathrm{n}=0.013$ Corrugated PE, smooth interior, Flow Area= 1.77 sf |
| \#2 | Device 1 | 41.35' | 3.5" Vert. Orifice/Grate $\mathrm{C}=0.600$ Limited to weir flow at low heads |
| \#3 | Device 1 | 45.00' | 3.0" Vert. Orifice/Grate $\mathrm{C}=0.600$ Limited to weir flow at low heads |
| \#4 | Device 1 | 46.00' | 4.0' long x 0.50 ' rise Sharp-Crested Rectangular Weir 2 End Contraction(s) 0.5' Crest Height |
| \#5 | Device 1 | 47.00' | 4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600 |
|  |  |  | Limited to weir flow at low heads |
| \#6 | Secondary | 46.50' | 15.0' long x 15.0' breadth Broad-Crested Rectangular Weir |
|  |  |  | Head (feet) $0.20 \quad 0.400 .600 .801 .001 .201 .401 .60$ |
|  |  |  | Coef. (English) 2.682 .702 .702 .642 .632 .642 .642 .63 |

Primary OutFlow Max=9.22 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater)
-1=Culvert (Passes 9.22 cfs of 18.40 cfs potential flow)
-2=Orifice/Grate (Orifice Controls 0.74 cfs @ 11.06 fps)
-3=Orifice/Grate (Orifice Controls 0.30 cfs @ 6.19 fps )
-4=Sharp-Crested Rectangular Weir(Orifice Controls 8.17 cfs @ 4.19 fps )
$\square_{5=O \text { Oifice/Grate ( Controls } 0.00 \mathrm{cfs} \text { ) }}$
Secondary OutFlow Max=5.85 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater)


## Summary for Pond POND 1.1: GRAVEL WETLAND 2



| Elevation <br> (feet) | Surf.Area <br> (sq-ft) | Voids <br> $(\%)$ | Inc.Store <br> (cubic-feet) | Cum.Store <br> (cubic-feet) |
| ---: | ---: | ---: | ---: | ---: |
| 47.55 | 6,269 | 0.0 | 0 | 0 |
| 49.85 | 6,269 | 30.0 | 4,326 | 4,326 |
| 50.50 | 6,269 | 45.0 | 1,834 | 6,159 |
| 51.00 | 7,199 | 100.0 | 3,367 | 9,526 |
| 52.00 | 9,187 | 100.0 | 8,193 | 17,719 |
| 53.00 | 11,345 | 100.0 | 10,266 | 27,985 |
| 54.00 | 13,814 | 100.0 | 12,580 | 40,565 |
| 55.00 | 16,645 | 100.0 | 15,230 | 55,794 |
| 56.00 | 19,805 | 100.0 | 18,225 | 74,019 |
| 58.00 | 23,480 | 100.0 | 43,285 | 117,304 |


| Device | Routing | Invert | Outlet Devices |
| :---: | :---: | :---: | :---: |
| \#1 | Primary | 49.85' | 24.0" Round Culvert |
|  |  |  | $\mathrm{L}=12.0^{\prime} \mathrm{CPP}$, square edge headwall, $\mathrm{Ke}=0.500$ |
|  |  |  | Inlet / Outlet Invert= 49.85' / 49.45' S=0.0333 '/' Cc= 0.900 |
|  |  |  | $\mathrm{n}=0.013$ Corrugated PE, smooth interior, Flow Area= 3.14 sf |
| \#2 | Device 1 | 49.85' | 2.0" Vert. Orifice/Grate $\mathrm{C}=0.600$ Limited to weir flow at low heads |
| \#3 | Device 1 | 53.50' | 4.0' long x 2.00' rise Sharp-Crested Rectangular Weir |
|  |  |  | 2 End Contraction(s) |
| \#4 | Device 1 | 56.50' | 4.0 " x 4.0" Horiz. Orifice/Grate X $106.00 \mathrm{C}=0.600$ |

Limited to weir flow at low heads
Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=47.55' TW=55.07' (Dynamic Tailwater)
$L_{1}=$ Culvert ( Controls 0.00 cfs )
-2=Orifice/Grate (Controls 0.00 cfs )
-3=Sharp-Crested Rectangular Weir( Controls 0.00 cfs)
$\square_{4=O r i f i c e / G r a t e ~(~ C o n t r o l s ~} 0.00 \mathrm{cfs}$ )

## Summary for Pond POND 1.2: PDMH203



Routed to Reach REACH 1.0 : RESTORED HODGSON BROOK
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 50.72' @ 12.09 hrs
Flood Elev= 57.00'


## Summary for Pond POND 1.3: OUTLET CULVERTS

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=12)
[62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.58' @ 23.95 hrs


Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 38.77' @ 12.53 hrs Surf.Area= 8,870 sf Storage= $13,560 \mathrm{cf}$
Flood Elev=43.50' Surf.Area= 95,977 sf Storage= 236,017 cf
Plug-Flow detention time $=56.2$ min calculated for 5.642 af ( $95 \%$ of inflow)
Center-of-Mass det. time= 29.8 min (900.3-870.4)

| Volume | Invert Avai | rage Stora | escription |
| :---: | :---: | :---: | :---: |
| \#1 | 35.00' 236,017 cf | 17 cf Cu | Custom Stage Data (P |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
| 35.00 | 960 | 0 | 0 |
| 36.00 | 1,428 | 1,194 | 1,194 |
| 38.00 | 5,418 | 6,846 | 8,040 |
| 40.00 | 14,354 | 19,772 | 27,812 |
| 42.00 | 66,884 | 81,238 | 109,050 |
| 43.00 | 92,707 | 79,796 | 188,846 |
| 43.50 | 95,977 | 47,171 | 236,017 |


| Device | Routing | Invert | Outlet Devices |
| :---: | :---: | :---: | :---: |
| \#1 | Primary | 35.60' | 42.0" W x 29.0" H, R=21.5"/66.1" Pipe Arch CMP_Arch_1/2 42x29 X 3.00 $\mathrm{L}=68.0^{\prime} \quad \mathrm{CMP}$, square edge headwall, $\mathrm{Ke}=0.500$ <br> Inlet / Outlet Invert= 35.60' 35.30 ' S=0.0044 '// Cc= 0.900 $n=0.025$ Corrugated metal, Flow Area= 6.72 sf |
| \#2 | Secondary | 43.00' | 143.1 deg $\times 18 . \mathbf{0}^{\prime}$ long $\times \mathbf{0 . 5 0}$ ' rise Sharp-Crested Vee/Trap Weir $\mathrm{Cv}=2.47(\mathrm{C}=3.09)$ |

Primary OutFlow Max=31.11 cfs @ 12.53 hrs HW=38.77' TW=38.65' (Dynamic Tailwater)
—1=CMP_Arch_1/2 42x29 (Outlet Controls 31.11 cfs @ 1.55 fps )
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=35.04' TW=38.65' (Dynamic Tailwater)
-2=Sharp-Crested Vee/Trap Weir ( Controls 0.00 cfs)

## Summary for Pond POND 1.4: SEDIMENT BASIN 1.0

| Inflow Area = | $=7.248 \mathrm{ac}$, | 0.42\% Impervious, Inflow Depth > 2.83" for 10 Year event |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Inflow | 18.77 cfs @ | 12.19 hrs , Volume= | 1.708 af |  |
| Outflow | 0.68 cfs @ | 17.24 hrs , Volume= | 0.950 af, Atten= 96\%, Lag= 303.1 min |  |
| Primary | 0.68 cfs @ | 17.24 hrs , Volume= | 0.950 af |  |
| Routed to | Pond POND 1.3 : | : OUTLET CULVERTS |  |  |
| Secondary = | 0.00 cfs @ | 0.00 hrs , Volume= | 0.000 af |  |
| Routed to | Pond POND | TLET CULVERTS |  |  |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Starting Elev=44.15' Surf.Area=18,132 sf Storage= 11,702 cf
Peak Elev= 45.79' @ 17.24 hrs Surf.Area= 29,244 sf Storage $=50,580 \mathrm{cf}$ ( 38,878 cf above start)
Flood Elev=48.50' Surf.Area= 38,802 sf Storage $=127,441$ cf (115,739 cf above start)
Plug-Flow detention time $=356.2$ min calculated for 0.680 af ( $40 \%$ of inflow)
Center-of-Mass det. time $=9.2 \min (846.8-837.5)$

| Volume | Invert | Avail.Storage | Storage Description |
| :---: | ---: | ---: | ---: |
| $\# 1$ | 43.00 | $127,441 \mathrm{cf}$ | Custom Stage Data (Prismatic)Listed below (Recalc) |


| Elevation <br> (feet) | Surf.Area <br> (sq-ft) | Inc.Store <br> (cubic-feet) | Cum.Store <br> (cubic-feet) |
| ---: | ---: | ---: | ---: |
| 43.00 | 1,000 | 0 | 0 |
| 44.00 | 17,117 | 9,059 | 9,059 |
| 46.00 | 30,657 | 47,774 | 56,833 |
| 47.00 | 35,879 | 33,268 | 90,101 |
| 48.00 | 38,802 | 37,341 | 127,441 |


| Device | Routing | Invert | Outlet Devices |
| :---: | :---: | :---: | :---: |
| \#1 | Primary | 42.75' | 12.0" Round Culvert L=66.0' $\mathrm{Ke}=0.500$ |
|  |  |  | Inlet / Outlet Invert= 42.75' / 42.40' S=0.0053 '/' Cc= 0.900 |
|  |  |  | $\mathrm{n}=0.013$, Flow Area $=0.79 \mathrm{sf}$ |
| \#2 | Device 1 | 43.00' | 4.0" Vert. Orifice/Grate $\mathrm{C}=0.600$ Limited to weir flow at low heads |
| \#3 | Device 1 | 46.80' | 10.0" $\times 17.5$ " Horiz. Orifice/Grate $\mathrm{C}=0.600$ |
|  |  |  | Limited to weir flow at low heads |
| \#4 | Secondary | 47.40' | Custom Weir/Orifice, Cv= 2.62 ( $\mathrm{C}=3.28$ ) |
|  |  |  | Head (feet) 0.001 .10 |
|  |  |  | Width (feet) 8.0014 .60 |

Primary OutFlow Max=0.68 cfs @ 17.24 hrs HW=45.79' TW=38.65' (Dynamic Tailwater)
$\mathcal{L}_{1}=$ Culvert (Passes 0.68 cfs of 5.16 cfs potential flow)
-2=Orifice/Grate (Orifice Controls 0.68 cfs @ 7.80 fps )
-3=Orifice/Grate (Controls 0.00 cfs )
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=44.15' TW=35.04' (Dynamic Tailwater) 4=Custom Weir/Orifice ( Controls 0.00 cfs )

## Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.
[80] Warning: Exceeded Pond POND 1.1 by 7.52 @ 0.00 hrs ( 23.95 cfs 41.618 af)


Routed to Pond POND 1.2 : PDMH203
Primary outflow $=$ Inflow, Time Span $=0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}$
10 Year 25 Point manual elevation table, To= 0.00 hrs , dt= 1.00 hrs , feet $=$

| 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | $\begin{array}{lllllll}55.07 & 55.07 & 55.07 & 55.07 & 55.07 & 55.07 & 55.07\end{array}$

## Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.
[80] Warning: Exceeded Pond POND 1.3 by 3.61 ' @ 0.00 hrs ( 92.51 cfs 60.023 af)


Primary outflow $=$ Inflow, Time Span= $0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}$
10 Year 2 Point manual elevation table, To= 0.00 hrs , $\mathrm{dt}=24.00 \mathrm{hrs}$, feet $=$ $38.65 \quad 38.65$

## Summary for Link PA2: POINT OF ANALYSIS



Primary outflow $=$ Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Time span $=0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}, 481$ points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf $71.49 \%$ Impervious Runoff Depth $>5.88$ " Flow Length=933' $\quad$ cc=11.4 min $C N=90$ Runoff=54.93 cfs 4.956 af

SubcatchmentPOST 1.1: WATERSHED Runoff Area $=157,428$ sf $30.92 \%$ Impervious Runoff Depth $>4.53$ " Flow Length=464' Tc=8.3 min CN=78 Runoff=17.44 cfs 1.365 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 sf $58.28 \%$ Impervious Runoff Depth $>5.54$ " Flow Length=1,191' Tc=6.4 min CN=87 Runoff=15.85 cfs 1.209 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 sf 23.27\% Impervious Runoff Depth>4.50" Flow Length=1,525' Tc=45.9 min CN=78 Runoff=16.75 cfs 2.583 af

SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf $0.42 \%$ Impervious Runoff Depth $>4.09$ " Flow Length=585' Tc=13.5 min CN=74 Runoff=27.23 cfs 2.472 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,336 sf $53.76 \%$ Impervious Runoff Depth $>5.54$ " Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \quad \mathrm{CN}=87$ Runoff $=7.12 \mathrm{cfs} 0.523$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.87' Max Vel=2.22 fps Inflow=15.85 cfs 1.209 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0$ ' $\mathrm{S}=0.0092$ '/' Capacity=2,720.29 cfs Outflow=8.65 cfs 1.202 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=47.10' Storage=90,424 cf Inflow=54.93 cfs 4.956 af Primary $=19.03$ cfs 2.766 af Secondary= 18.86 cfs 0.671 af Outflow= 37.88 cfs 3.437 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=55.22' Storage=59,446 cf Inflow=17.44 cfs 1.365 af Outflow= 0.00 cfs 0.000 af

Pond POND 1.2: PDMH203
Peak Elev=50.94' Inflow=15.85 cfs 1.209 af 48.0" Round Culvert $\mathrm{n}=0.013 \mathrm{~L}=269.0^{\prime} \mathrm{S}=0.0050$ '//' Outflow=15.85 cfs 1.209 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.17' Storage=17,433 cf Inflow=57.33 cfs 8.292 af Primary $=56.26$ cfs 7.985 af Secondary $=0.00$ cfs 0.000 af Outflow=56.26 cfs 7.985 af

Pond POND 1.4: SEDIMENTBASIN 1.0 Peak Elev=46.65' Storage=77,792 cf Inflow=27.23 cfs 2.472 af Primary $=0.78$ cfs 1.070 af Secondary $=0.00$ cfs 0.000 af Outflow= 0.78 cfs 1.070 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS

Inflow=0.00 cfs 0.000 af Primary $=0.00$ cfs 0.000 af

Inflow=56.26 cfs 7.985 af Primary $=56.26$ cfs 7.985 af

Inflow=7.12 cfs 0.523 af Primary=7.12 cfs 0.523 af

Total Runoff Area $=31.609$ ac Runoff Volume $=13.108$ af Average Runoff Depth $=4.98$ " 61.68\% Pervious = 19.497 ac $38.32 \%$ Impervious $=12.112$ ac

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf $71.49 \%$ Impervious Runoff Depth $>7.25^{\prime \prime}$ Flow Length=933' $\quad$ cc=11.4 min $C N=90$ Runoff=66.89 cfs 6.105 af

SubcatchmentPOST 1.1: WATERSHED Runoff Area $=157,428$ sf $30.92 \%$ Impervious Runoff Depth $>5.81$ " Flow Length=464' Tc=8.3 min CN=78 Runoff=22.21 cfs 1.750 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 sf $58.28 \%$ Impervious Runoff Depth>6.89" Flow Length=1,191' Tc=6.4 $\mathrm{min} \mathrm{CN}=87$ Runoff=19.47 cfs 1.503 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 sf $23.27 \%$ Impervious Runoff Depth>5.77" Flow Length=1,525' Tc=45.9 min CN=78 Runoff=21.37 cfs 3.312 af

SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf $0.42 \%$ Impervious Runoff Depth $>5.33^{\prime \prime}$ Flow Length=585' Tc=13.5 min CN=74 Runoff=35.32 cfs 3.218 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,336 sf $53.76 \%$ Impervious Runoff Depth>6.89" Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \mathrm{CN}=87$ Runoff $=8.76 \mathrm{cfs} 0.651$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.92' Max Vel=2.24 fps Inflow=19.47 cfs 1.503 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0$ ' $\mathrm{S}=0.0092$ '/' Capacity=2,720.29 cfs Outflow=11.76 cfs 1.495 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=47.39' Storage=96,897 cf Inflow=66.89 cfs 6.105 af Primary=19.58 cfs 3.347 af Secondary=33.37 cfs 1.209 af Outflow=52.94 cfs 4.556 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=56.11' Storage=76,209 cf Inflow=22.21 cfs 1.750 af Outflow=0.00 cfs 0.000 af

Pond POND 1.2: PDMH203
Peak Elev=51.13' Inflow=19.47 cfs 1.503 af 48.0" Round Culvert n=0.013 L=269.0' $\mathrm{S}=0.0050$ '//' Outflow=19.47 cfs 1.503 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.58' Storage=22,150 cf Inflow=76.91 cfs 10.982 af Primary $=74.09$ cfs 10.655 af Secondary $=0.00$ cfs 0.000 af Outflow=74.09 cfs 10.655 af

Pond POND 1.4: SEDIMENTBASIN 1.0 Peak Elev=47.02' Storage=90,878 cf Inflow=35.32 cfs 3.218 af Primary $=2.39$ cfs 1.619 af Secondary= 0.00 cfs 0.000 af Outflow=2.39 cfs 1.619 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS
Inflow=0.00 cfs 0.000 af Primary $=0.00$ cfs 0.000 af

Inflow=74.09 cfs 10.655 af Primary $=74.09$ cfs 10.655 af

Inflow=8.76 cfs 0.651 af Primary $=8.76$ cfs 0.651 af

## Master Post-Development Calculations




## Area Listing (all nodes)

| Area <br> (acres) | CN | Description <br> (subcatchment-numbers) |
| ---: | :--- | :--- |
| 1.776 | 61 | >75\% Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3, <br> POST 1.4) |
| 6.801 | 74 | >75\% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, <br> POST 1.4, POST 2.0) |
| 0.436 | 80 | >75\% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4) <br> 0.323 |
| 38 | Meadow, non-grazed, HSG B (POST 1.3) |  |
| 0.143 | 71 | Meadow, non-grazed, HSG C (POST 1.3) |
| 0.799 | 98 | Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4) |
| 7.546 | 98 | Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, |
|  |  | POST 2.0) |
| 0.146 | 98 | Paved parking, HSG D (POST 1.0, POST 1.3, POST 1.4) |
| 0.688 | 98 | Roofs, HSG B (POST 1.0, POST 1.1, POST 1.4) |
| 8.166 | 98 | Roofs, HSG C (POST 1.0, POST 1.1, POST 1.4, POST 2.0) |
| 1.737 | 98 | Roofs, HSG D (POST 1.0, POST 1.4) |
| 0.049 | 76 | Woods/grass comb., Fair, HSG C (POST 1.3) |
| 31.609 | 87 | TOTAL AREA |

## L-0700-26 POST

Prepared by Tighe \& Bond
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## Soil Listing (all nodes)

| Area <br> $($ acres $)$ | Soil <br> Group | Subcatchment <br> Numbers |
| ---: | :--- | :--- |
| 0.000 | HSG A |  |
| 3.586 | HSG B | POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4 |
| 25.705 | HSG C | POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0 |
| 2.318 | HSG D | POST 1.0, POST 1.3, POST 1.4 |
| 0.000 | Other |  |
| 31.609 |  | TOTAL AREA |

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED $\begin{gathered}\text { Runoff Area=462,599 sf } \\ \text { Flow Length }=933 ' \quad \mathrm{Tc}=11.4 \mathrm{~min} \quad \mathrm{~m} \\ \mathrm{CN}=91\end{gathered}$
SubcatchmentPOST 1.1: WATERSHED Runoff Area=242,496 sf $58.73 \%$ Impervious Runoff Depth $>2.25$ " Flow Length=750' Tc=10.3 min CN=86 Runoff=12.60 cfs 1.046 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=101,204 sf $62.15 \%$ Impervious Runoff Depth $>2.43$ " Flow Length=1,191' Tc=6.4 min CN=88 Runoff=6.37 cfs 0.471 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=306,549 sf 22.64\% Impervious Runoff Depth>1.55" Flow Length=1,525' Tc=45.9 min CN=77 Runoff=5.81 cfs 0.908 af

SubcatchmentPOST 1.4: WATERSHED Runoff Area=214,764 sf 85.05\% Impervious Runoff Depth>3.01" Flow Length=717' Tc=7.5 min CN=94 Runoff=15.51 cfs 1.236 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,290 sf $80.99 \%$ Impervious Runoff Depth>2.91" Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \quad \mathrm{CN}=93$ Runoff $=3.72 \mathrm{cfs} 0.274$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.60' Max Vel=2.03 fps Inflow=6.37 cfs 0.617 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0^{\prime} \mathrm{S}=0.0092$ '/' Capacity=2,720.29 cfs Outflow=4.54 cfs 0.608 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=46.16' Storage=70,734 cf Inflow=27.46 cfs 2.396 af Primary $=1.57$ cfs 1.041 af Secondary= 0.00 cfs 0.000 af Outflow=1.57 cfs 1.041 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=53.90' Storage=39,230 cf Inflow=12.60 cfs 1.046 af Outflow= 0.40 cfs 0.146 af

Pond POND 1.2: PDMH203
Peak Elev=50.33' Inflow=6.37 cfs 0.617 af 48.0" Round Culvert $n=0.013$ L=269.0' $\mathrm{S}=0.0050$ '/' Oufflow=6.37 cfs 0.617 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' Storage=8,984 cf Inflow=9.25 cfs 3.255 af Primary $=9.41$ cfs 3.050 af Secondary $=0.00$ cfs 0.000 af Outflow=9.41 cfs 3.050 af

Pond POND 1.4: RAINGARDEN1.0 Peak Elev=47.27' Storage=34,235 cf Inflow=15.51 cfs 1.236 af Primary $=1.31$ cfs 0.699 af Secondary $=0.00$ cfs 0.000 af Outflow=1.31 cfs 0.699 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS

Inflow=0.40 cfs 0.146 af Primary $=0.40$ cfs 0.146 af

Inflow $=9.41$ cfs 3.050 af Primary $=9.41$ cfs 3.050 af

Inflow=3.72 cfs 0.274 af Primary $=3.72$ cfs 0.274 af

Total Runoff Area $=31.609$ ac Runoff Volume = 6.331 af Average Runoff Depth = 2.40" $39.63 \%$ Pervious $=12.527$ ac $60.37 \%$ Impervious $=19.083$ ac

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=462,599 sf $72.19 \%$ Impervious Runoff Depth $>4.54$ " Flow Length=933' Tc=11.4 min CN=91 Runoff=44.88 cfs 4.017 af

SubcatchmentPOST 1.1: WATERSHED Runoff Area=242,496 sf $58.73 \%$ Impervious Runoff Depth>4.01" Flow Length=750' Tc=10.3 min CN=86 Runoff=22.02 cfs 1.858 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=101,204 sf $62.15 \%$ Impervious Runoff Depth>4.22" Flow Length=1,191' Tc=6.4 $\mathrm{min} \mathrm{CN}=88$ Runoff=10.81 cfs 0.817 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=306,549 sf 22.64\% Impervious Runoff Depth>3.09" Flow Length=1,525' Tc=45.9 min CN=77 Runoff=11.76 cfs 1.810 af

SubcatchmentPOST 1.4: WATERSHED Runoff Area=214,764 sf 85.05\% Impervious Runoff Depth>4.88" Flow Length=717' Tc=7.5 min CN=94 Runoff=24.45 cfs 2.004 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,290 sf $80.99 \%$ Impervious Runoff Depth>4.77" Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \quad \mathrm{CN}=93$ Runoff $=5.94 \mathrm{cfs} 0.449$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.81' Max Vel=2.20 fps Inflow=10.81 cfs 1.367 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0$ ' $\mathrm{S}=0.0092$ '/' Capacity=2,720.29 cfs Outflow=6.07 cfs 1.355 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=46.94' Storage=86,832 cf Inflow=44.88 cfs 4.017 af Primary $=7.09$ cfs 2.106 af Secondary=11.63 cfs 0.435 af Outflow= 18.72 cfs 2.541 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=55.08' Storage=57,197 of Inflow=22.02 cfs 1.858 af Outflow=1.76 cfs 0.550 af

Pond POND 1.2: PDMH203
Peak Elev=50.65' Inflow=10.81 cfs 1.367 af 48.0" Round Culvert $\mathrm{n}=0.013 \mathrm{~L}=269.0^{\prime} \mathrm{S}=0.0050$ '/' Outflow=10.81 cfs 1.367 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.86' Storage=14,364 cf Inflow=40.12 cfs 7.107 af Primary $=39.92$ cfs 6.819 af Secondary $=0.00$ cfs 0.000 af Outflow=39.92 cfs 6.819 af

Pond POND 1.4: RAINGARDEN1.0 Peak Elev=48.07' Storage=45,635 cf Inflow=24.45 cfs 2.004 af Primary $=6.60$ cfs 1.401 af Secondary= 0.00 cfs 0.000 af Outflow=6.60 cfs 1.401 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS

Inflow=1.76 cfs 0.550 af Primary $=1.76$ cfs 0.550 af

Inflow=39.92 cfs 6.819 af Primary $=39.92$ cfs 6.819 af

Inflow=5.94 cfs 0.449 af Primary $=5.94$ cfs 0.449 af

Total Runoff Area $=31.609$ ac Runoff Volume $=10.955$ af Average Runoff Depth $=4.16$ " 39.63\% Pervious = 12.527 ac
$60.37 \%$ Impervious $=19.083$ ac

## Summary for Subcatchment POST 1.0: WATERSHED 1.0

Runoff = 44.88 cfs @ 12.15 hrs, Volume= 4.017 af, Depth> 4.54"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
$\mathrm{n}=0.013$
11.4933 Total

## Summary for Subcatchment POST 1.1: WATERSHED 1.1

Runoff $=\quad 22.02$ cfs @ 12.14 hrs, Volume $=1.858$ af, Depth> 4.01"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

|  | ea (sf) | CN | escription |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 13,692 | 98 R | Roofs, HSG B |  |  |
|  | 32,710 | $61>$ | >75\% Grass cover, Good, HSG B |  |  |
|  | 2,729 | 98 P | Paved parking, HSG B |  |  |
|  | 88,019 | 98 R | Roofs, HSG C |  |  |
|  | 67,375 | 74 > | >75\% Grass cover, Good, HSG C |  |  |
|  | 37,971 | 98 P | Paved parking, HSG C |  |  |
| 242,496 |  | 86 | Weighted Average |  |  |
|  | 00,085 |  | 41.27\% Pervious Area |  |  |
| 142,411 |  |  | 58.73\% Impervious Area |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \end{array}$ | Length (feet) | Slope <br> (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
| 7.1 | 100 | 0.0380 | 0.24 |  | Sheet Flow, <br> Grass: Short $n=0.150 \quad$ P2 $=3.68{ }^{\prime \prime}$ |
| 1.2 | 163 | 0.0245 | 2.35 |  | Shallow Concentrated Flow, |
|  |  |  |  |  | Grassed Waterway Kv= 15.0 fps |
| 1.5 | 283 | 0.0050 | 3.21 | 2.52 | Pipe Channel, |
|  |  |  |  |  | 12.0" Round Area= 0.8 sf Perim=3.1' r=0.25' |
| 0.1 | 81 | 0.0240 | 9.21 | 16.27 | Pipe Channel, |
|  |  |  |  |  | 18.0" Round Area= 1.8 sf Perim=4.7' r= $0.38^{\prime}$ $\mathrm{n}=0.013$ |
| 0.4 | 123 | 0.0050 | 5.09 | 16.00 | Pipe Channel, |
|  |  |  |  |  | 24.0" Round Area= 3.1 sf Perim=6.3' r=0.50' $\mathrm{n}=0.013$ |

$10.3 \quad 750$ Total

## Summary for Subcatchment POST 1.2: WATERSHED 1.2

Runoff $=10.81$ cfs @ 12.09 hrs, Volume= 0.817 af, Depth> 4.22"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

|  | ea (sf) | CN | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6,874 | 61 | >75\% Grass cover, Good, HSG B |  |  |
|  | 4,785 | 98 | Paved parking, HSG B |  |  |
|  | 31,436 | 74 | >75\% Grass cover, Good, HSG C |  |  |
|  | 58,109 | 98 | Paved parking, HSG C |  |  |
|  | 1,204 | 88 | Weighted Average 37.85\% Pervious Area 62.15\% Impervious Are |  |  |
|  | 38,310 |  |  |  |  |
|  | 62,894 |  |  |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
| 1.5 | 100 | $0.0100$ | 1.12 |  | Sheet Flow, Smooth surfaces $n=0.011 \quad \mathrm{P} 2=3.68$ " |
| 1.0 | 153 | 0.0150 | 2.49 |  | Shallow Concentrated Flow, Paved $\mathrm{Kv}=20.3 \mathrm{fps}$ |
| 1.6 | 343 | 0.0050 | 3.47 | 2.73 | Pipe Channel, <br> 12.0" Round Area= 0.8 sf Perim=3.1' r= $0.25^{\prime}$ $\mathrm{n}=0.012$ Concrete pipe, finished |
| 0.1 | 13 | 0.0050 | 3.72 | 4.57 | Pipe Channel, <br> 15.0" Round Area= 1.2 sf Perim=3.9' $\mathrm{r}=0.31^{\prime}$ <br> $\mathrm{n}=0.013$ Corrugated PE , smooth interior |
| 1.8 | 453 | 0.0050 | 4.20 | 7.43 | Pipe Channel, <br> 18.0" Round Area= 1.8 sf Perim=4.7'r=0.38' $\mathrm{n}=0.013$ Corrugated PE , smooth interior |
| 0.4 | 129 | 0.0050 | 5.91 | 29.00 | Pipe Channel, <br> 30.0" Round Area= 4.9 sf Perim=7.9' $\mathrm{r}=0.63^{\prime}$ <br> $\mathrm{n}=0.013$ Corrugated PE , smooth interior |

6.4 1,191 Total

## Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 11.76 cfs @ 12.63 hrs, Volume= 1.810 af, Depth> 3.09"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= $0.00-24.00 \mathrm{hrs}$, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall $=5.58{ }^{\prime \prime}$

| Area (sf) | CN | Description |
| ---: | ---: | :--- |
| 11,450 | 61 | $>75 \%$ Grass cover, Good, HSG B |
| 14,068 | 58 | Meadow, non-grazed, HSG B |
| 908 | 98 | Paved parking, HSG B |
| 70,956 | 74 | $>75 \%$ Grass cover, Good, HSG C |
| 136,905 | 71 | Meadow, non-grazed, HSG C |
| 2,120 | 76 | Woods/grass comb., Fair, HSG C |
| 68,005 | 98 | Paved parking, HSG C |
| 1,638 | 80 | $>75 \%$ Grass cover, Good, HSG D |
| 499 | 98 | Paved parking, HSG D |
| 306,549 | 77 | Weighted Average |
| 237,137 |  | 77.36\% Pervious Area |
| 69,412 |  | $22.64 \%$ Impervious Area |


| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope $(\mathrm{ft} / \mathrm{ft})$ | Velocity (ft/sec) | $\begin{array}{r} \text { Capacity } \\ \text { (cfs) } \end{array}$ | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10.9 | 100 | 0.0130 | 0.15 |  | Sheet Flow, <br> Grass: Short $n=0.150 \quad P 2=3.68 "$ |
| 1.1 | 52 | 0.0130 | 0.80 |  | Shallow Concentrated Flow, Short Grass Pasture Kv=7.0 fps |
| 0.1 | 27 | 0.2720 | 7.82 |  | Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps |
| 33.8 | 1,346 | 0.0090 | 0.66 |  | Shallow Concentrated Flow, Short Grass Pasture Kv=7.0 fps |

## Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff $=\quad 24.45$ cfs @ 12.10 hrs, Volume= 2.004 af, Depth> 4.88"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

|  | Area (sf) | CN | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 11,051 | 98 R | Roofs, HSG B |  |  |
|  | 3,902 | 61 > | >75\% Grass cover, Good, HSG B |  |  |
|  | 7,241 | 98 P | Paved parking, HSG B |  |  |
|  | 86,748 | 98 R | Roofs, HSG C |  |  |
|  | 26,995 | 74 > | >75\% Grass cover, Good, HSG C |  |  |
|  | 32,822 | 98 P | Paved parking, HSG C |  |  |
|  | 44,300 | 98 R | Roofs, HSG D |  |  |
|  | 1,206 | 80 > | >75\% Grass cover, Good, HSG D |  |  |
|  | 499 | 98 P | Paved parking, HSG D |  |  |
|  | $\begin{array}{r} \hline 214,764 \\ 32,103 \\ 182,661 \end{array}$ | $94$ | Weighted Average 14.95\% Pervious Area 85.05\% Impervious Area |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope $(\mathrm{ft} / \mathrm{ft})$ | Velocity (ft/sec) | $\begin{array}{r} \text { Capacity } \\ \text { (cfs) } \end{array}$ | Description |
| 4.9 | 40 | 0.0150 | 0.14 |  | Sheet Flow, <br> Grass: Short $n=0.150 \quad \mathrm{P} 2=3.68^{\prime \prime}$ |
| 0.3 | 53 | 0.0200 | - 2.87 |  | Shallow Concentrated Flow, Paved Kv= 20.3 fps |
| 0.3 | 65 | 0.0050 | - 3.21 | 2.52 | Pipe Channel, <br> 12.0" Round Area= 0.8 sf Perim=3.1' $\mathrm{r}=0.25^{\prime}$ $\mathrm{n}=0.013$ Corrugated PE , smooth interior |
| 0.4 | 115 | 0.0100 | - 4.54 | 3.56 | Pipe Channel, <br> 12.0" Round Area= 0.8 sf Perim=3.1' $\mathrm{r}=0.25^{\prime}$ $\mathrm{n}=0.013$ |
| 0.7 | 140 | 0.0050 | - 3.21 | 2.52 | Pipe Channel, <br> 12.0" Round Area= 0.8 sf Perim=3.1' $r=0.25^{\prime}$ $\mathrm{n}=0.013$ |
| 0.9 | 275 | 0.0070 | - 4.97 | 8.79 | Pipe Channel, <br> 18.0" Round Area= 1.8 sf Perim= 4.7 'r= 0.38 ' $\mathrm{n}=0.013$ |

0.0
$29 \quad 0.0550$
13.94
24.63 Pipe Channel,
18.0" Round Area= 1.8 sf Perim=4.7' r=0.38' $\mathrm{n}=0.013$
7.5

717 Total

## Summary for Subcatchment POST 2.0: WATERSHED 2.0

[49] Hint: Tc<2dt may require smaller dt
Runoff $=5.94$ cfs @ 12.07 hrs, Volume= 0.449 af, Depth> 4.77"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= $0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}$ Type III 24-hr 10 Year Rainfall=5.58"

|  | Area (sf) | CN | Roofs, HSG C |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 22,995 |  |  |  |  |
|  | 9,368 |  | Roofs, HSG C <br> >75\% Grass cover, Good, HSG C |  |  |
|  | 16,927 |  |  |  |  |
|  | 49,290 | 93 | Weighted Average 19.01\% Pervious Area 80.99\% Impervious Are |  |  |
|  | 9,368 |  |  |  |  |
|  | 39,922 |  |  |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | $\begin{array}{r} \text { Capacity } \\ \text { (cfs) } \end{array}$ | Description |
| 1.2 | 100 | 0.0164 | 1.36 |  | Sheet Flow, <br> Smooth surfaces $\mathrm{n}=0.011 \quad \mathrm{P} 2=3.68{ }^{\prime \prime}$ |
| 0.3 | 48 | 0.0164 | 2.60 |  | Shallow Concentrated Flow, Paved Kv= 20.3 fps |
| 0.3 | 130 | 0.0140 | 7.03 | 12.43 | Pipe Channel, <br> 18.0" Round Area= 1.8 sf Perim=4.7'r=0.38' $n=0.013$ |
| 0.5 | 70 | 0.0250 | 2.37 |  | Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps |
| 1.3 | 410 | 0.0050 | 5.09 | 16.00 | Pipe Channel, <br> $24.0^{\prime \prime}$ Round Area= 3.1 sf Perim=6.3' $r=0.50^{\prime}$ $\mathrm{n}=0.013$ |

3.6758 Total, Increased to minimum Tc $=5.0 \mathrm{~min}$

## Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)


Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Max. Velocity $=2.20 \mathrm{fps}$, Min. Travel Time $=9.9 \mathrm{~min}$
Avg. Velocity $=1.04 \mathrm{fps}$, Avg. Travel Time $=21.0 \mathrm{~min}$

Peak Storage= 6,364 cf @ 12.27 hrs
Average Depth at Peak Storage= 0.81'
Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs
Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals)
Constant $\mathrm{n}=0.040$ Winding stream, pools \& shoals
Inlet Invert= 48.00', Outlet Invert= 36.00'


| Offset <br> (feet) | Elevation <br> (feet) | Chan. Depth <br> (feet) |
| ---: | ---: | ---: |
| 0.00 | 12.00 | 0.00 |
| 18.00 | 6.00 | 6.00 |
| 30.25 | 6.00 | 6.00 |
| 31.75 | 5.25 | 6.75 |
| 34.25 | 5.25 | 6.75 |
| 35.75 | 6.00 | 6.00 |
| 48.00 | 6.00 | 6.00 |
| 66.00 | 12.00 | 0.00 |


| Depth <br> (feet) | End Area <br> (sq-ft) | Perim. <br> (feet) | Storage <br> (cubic-feet) | Discharge <br> (cfs) |
| ---: | ---: | ---: | ---: | ---: |
| 0.00 | 0.0 | 2.5 | 0 | 0.00 |
| 0.75 | 3.0 | 30.4 | 3,927 | 2.28 |
| 6.75 | 291.0 | 68.3 | 380,919 | $2,720.29$ |

## Summary for Pond POND 1.0: GRAVEL WETLAND 1

[95] Warning: Outlet Device \#4 rise exceeded

| Inflow Area = | 10.620 ac, $72.19 \%$ Impervious, Inflow Depth > 4.54" for 10 Year event |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Inflow | 44.88 cfs @ | 12.15 hrs , Volume= | 4.017 af |  |
| Outflow | 18.72 cfs @ | 12.45 hrs , Volume $=$ | 2.541 af, | Atten $=58 \%$, Lag $=18.0$ min |
| Primary | 7.09 cfs @ | 12.45 hrs , Volume= | 2.106 af |  |
| Secondary = | 11.63 cfs @ | 12.45 hrs , Volume $=$ | 0.435 af |  |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 46.94' @ 12.45 hrs Surf.Area= 21,544 sf Storage $=86,832$ cf Flood Elev=48.00' Surf.Area= 23,557 sf Storage $=110,845$ cf

Plug-Flow detention time= 216.6 min calculated for 2.536 af ( $63 \%$ of inflow)
Center-of-Mass det. time= 118.8 min ( 906.1-787.3)

| Volume | Invert | Avail.Storage |
| :---: | ---: | ---: | ---: | ---: | ---: | Storage Description

Primary OutFlow Max=7.09 cfs @ 12.45 hrs HW=46.93' TW=38.85' (Dynamic Tailwater)
L1=Culvert (Passes 7.09 cfs of 18.71 cfs potential flow)
-2=Orifice/Grate (Orifice Controls 0.75 cfs @ 11.23 fps)

- $\mathbf{3}=$ Orifice/Grate (Orifice Controls 0.32 cfs @ 6.48 fps )
-4=Sharp-Crested Rectangular Weir(Orifice Controls 6.02 cfs @ 4.15 fps)
$-5=$ Orifice/Grate (Controls 0.00 cfs )
Secondary OutFlow Max=11.59 cfs @ 12.45 hrs HW=46.93' TW=38.85' (Dynamic Tailwater) $\mathbf{C B H}_{\mathbf{6}}$ Broad-Crested Rectangular Weir(Weir Controls 11.59 cfs @ 1.78 fps )


## Summary for Pond POND 1.1: GRAVEL WETLAND 2



Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev=55.08' @ 13.65 hrs Surf.Area= 16,909 sf Storage= 57,197 cf
Flood Elev=57.00' Surf.Area= 21,643 sf Storage $=94,743 \mathrm{cf}$

Plug-Flow detention time= 357.2 min calculated for 0.550 af ( $30 \%$ of inflow)
Center-of-Mass det. time $=218.3 \mathrm{~min}(1,021.7-803.4$ )

| Volume | Invert | Avail.Storage | Storage Description |
| :---: | ---: | ---: | ---: |
| $\# 1$ | $47.55^{\prime}$ | $117,304 \mathrm{cf}$ | Custom Stage Data (Prismatic)Listed below (Recalc) |


| Elevation <br> (feet) | Surf.Area <br> (sq-ft) | Voids <br> $(\%)$ | Inc.Store <br> (cubic-feet) | Cum.Store <br> (cubic-feet) |
| ---: | ---: | ---: | ---: | ---: |
| 47.55 | 6,269 | 0.0 | 0 | 0 |
| 49.85 | 6,269 | 30.0 | 4,326 | 4,326 |
| 50.50 | 6,269 | 45.0 | 1,834 | 6,159 |
| 51.00 | 7,199 | 100.0 | 3,367 | 9,526 |
| 52.00 | 9,187 | 100.0 | 8,193 | 17,719 |
| 53.00 | 11,345 | 100.0 | 10,266 | 27,985 |
| 54.00 | 13,814 | 100.0 | 12,580 | 40,565 |
| 55.00 | 16,645 | 100.0 | 15,230 | 55,794 |
| 56.00 | 19,805 | 100.0 | 18,225 | 74,019 |
| 58.00 | 23,480 | 100.0 | 43,285 | 117,304 |


| Device | Routing | Invert | Outlet Devices |
| :---: | :---: | :---: | :---: |
| \#1 | Primary | 49.85' | 24.0" Round Culvert |
|  |  |  | $\mathrm{L}=12.0{ }^{\prime}$ CPP, square edge headwall, $\mathrm{Ke}=0.500$ |
|  |  |  | Inlet / Outlet Invert= 49.85' / 49.45' S=0.0333 '/' Cc= 0.900 |
|  |  |  | $\mathrm{n}=0.013$ Corrugated PE, smooth interior, Flow Area= 3.14 sf |
| \#2 | Device 1 | 49.85' | 2.0" Vert. Orifice/Grate C= 0.600 |
| \#3 | Device 1 | 53.50' | 4.0' long x 2.00 ' rise Sharp-Crested Rectangular Weir |
|  |  |  | 2 End Contraction(s) |
| \#4 | Device 1 | 56.50' | 4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600 |
|  |  |  | Limited to weir flow at low heads |

Primary OutFlow Max=1.76 cfs @ 13.65 hrs HW=55.08' TW=55.07' (Dynamic Tailwater)
$\left\llcorner_{1}=\right.$ Culvert (Inlet Controls 1.76 cfs @ 0.56 fps )
-2=Orifice/Grate (Passes < 0.01 cfs potential flow)

- $\mathbf{3}=$ Sharp-Crested Rectangular Weir(Passes $<3.33$ cfs potential flow)
-4=Orifice/Grate (Controls 0.00 cfs )


## Summary for Pond POND 1.2: PDMH203



Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 50.65' @ 12.09 hrs
Flood Elev= 57.00'
Device Routing Invert Outlet Devices
\#1 Primary 49.35' 48.0" Round Culvert
L=269.0' CPP, projecting, no headwall, $\mathrm{Ke}=0.900$
Inlet / Outlet Invert= 49.35' / 48.00' S=0.0050 '/' Cc= 0.900
$\mathrm{n}=0.013$ Corrugated PE, smooth interior, Flow Area= 12.57 sf
Primary OutFlow Max=10.64 cfs @ 12.09 hrs HW=50.64' TW=48.75' (Dynamic Tailwater)
-1=Culvert (Inlet Controls 10.64 cfs @ 3.05 fps )

## Summary for Pond POND 1.3: OUTLET CULVERTS

[62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.50' @ 23.95 hrs

| Inflow Area = | 30.478 ac, 59.60\% Impervious, Inflow Depth > 2.80" for 10 Year event |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Inflow | 40.12 cfs @ | 12.47 hrs , Volume= | 7.107 af |  |
| Outflow | 39.92 cfs @ | 12.50 hrs , Volume= | 6.819 af , | Atten= 0\%, Lag= 1.8 min |
| Primary | 39.92 cfs @ | 12.50 hrs , Volume= | 6.819 af |  |
| Secondary = | 0.00 cfs @ | 0.00 hrs , Volume= | 0.000 af |  |

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 38.86' @ 12.50 hrs Surf.Area= 9,266 sf Storage= 14,364 cf
Flood Elev=43.50' Surf.Area= 95,977 sf Storage $=236,017 \mathrm{cf}$
Plug-Flow detention time $=32.3 \mathrm{~min}$ calculated for 6.819 af ( $96 \%$ of inflow)
Center-of-Mass det. time= 11.6 min ( 905.1 - 893.5 )

| Volume | Invert | Avail.Storage | Storage Description |
| :---: | ---: | ---: | ---: |
| $\# 1$ | $35.00^{\prime}$ | 236,017 cf | Custom Stage Data (Prismatic)Listed below (Recalc) |


| Elevation <br> (feet) | Surf.Area <br> (sq-ft) | Inc.Store <br> (cubic-feet) | Cum.Store <br> (cubic-feet) |
| ---: | ---: | ---: | ---: |
| 35.00 | 960 | 0 | 0 |
| 36.00 | 1,428 | 1,194 | 1,194 |
| 38.00 | 5,418 | 6,846 | 8,040 |
| 40.00 | 14,354 | 19,772 | 27,812 |
| 42.00 | 66,884 | 81,238 | 109,050 |
| 43.00 | 92,707 | 79,796 | 188,846 |
| 43.50 | 95,977 | 47,171 | 236,017 |


| Device | Routing | Invert | Outlet Devices |
| :---: | :---: | :---: | :---: |
| \#1 | Primary | $35.60{ }^{\prime}$ | 42.0" W x 29.0" H, R=21.5"/66.1" Pipe Arch CMP_Arch_1/2 42x29 X 3.00 $\mathrm{L}=68.0^{\prime} \quad \mathrm{CMP}$, square edge headwall, $\mathrm{Ke}=0.500$ <br> Inlet / Outlet Invert= 35.60' 35.30 ' S=0.0044 '// Cc= 0.900 $n=0.025$ Corrugated metal, Flow Area= 6.72 sf |
| \#2 | Secondary | 43.00' | 143.1 deg x 18.0' long x 0.50' rise Sharp-Crested Vee/Trap Weir $\mathrm{Cv}=2.47(\mathrm{C}=3.09)$ |

Primary OutFlow Max=39.88 cfs @ 12.50 hrs HW=38.86' TW=38.65' (Dynamic Tailwater)
L-1=CMP_Arch_1/2 42x29 (Outlet Controls 39.88 cfs @ 1.98 fps )
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=35.00' TW=38.65' (Dynamic Tailwater)
$L_{2=S h a r p-C r e s t e d ~ V e e / T r a p ~ W e i r ~(~ C o n t r o l s ~} 0.00 \mathrm{cfs}$ )

## Summary for Pond POND 1.4: RAINGARDEN 1.0



Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev=48.07' @ 12.48 hrs Surf.Area= 14,774 sf Storage $=45,635$ cf
Flood Elev=50.00' Surf.Area= 17,790 sf Storage $=77,050 \mathrm{cf}$
Plug-Flow detention time $=233.7 \mathrm{~min}$ calculated for 1.398 af ( $70 \%$ of inflow)
Center-of-Mass det. time= 143.1 min ( 914.3-771.2)

| Volume | Invert Avail.Storage |  | Storage Description |  |
| :---: | :---: | :---: | :---: | :---: |
| \#1 | 42.17' | 77,050 cf | Custom Stag | ta (Prismatic |
| Elevation (feet) | Surf.Area $(\mathrm{sq}-\mathrm{ft})$ | Voids (\%) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
| 42.17 | 10,418 | 0.0 | 0 | 0 |
| 43.50 | 10,418 | 40.0 | 5,542 | 5,542 |
| 45.00 | 10,418 | 10.0 | 1,563 | 7,105 |
| 46.00 | 11,745 | 100.0 | 11,082 | 18,187 |
| 48.00 | 14,664 | 100.0 | 26,409 | 44,596 |
| 50.00 | 17,790 | 100.0 | 32,454 | 77,050 |


| Device | Routing | Invert | Outlet Devices |
| :---: | :---: | :---: | :---: |
| \#1 | Primary | 42.42' | 12.0" Round Culvert |
|  |  |  | $\mathrm{L}=48.0$ CPP, projecting, no headwall, $\mathrm{Ke}=0.900$ |
|  |  |  | Inlet / Outlet Invert= 42.42' / 42.20' S=0.0046 '/' Cc= 0.900 |
|  |  |  | $\mathrm{n}=0.013$ Corrugated PE, smooth interior, Flow Area= 0.79 sf |
| \#2 | Device 1 | 42.42' | 6.0" Vert. Orifice/Grate C= 0.600 |
| \#3 | Device 2 | 45.00' | $10.000 \mathrm{in} / \mathrm{hr}$ Exfiltration over Surface area above 45.00' |
|  |  |  | Excluded Surface area $=10,418 \mathrm{sf}$ |
| \#4 | Device 1 | 47.15' | 13.2" $\times 13.2$ " Horiz. Orifice/Grate $\mathrm{C}=0.600$ |
|  |  |  | Limited to weir flow at low heads |
| \#5 | Secondary | 49.35' | 7.0' long x 8.9' breadth Broad-Crested Rectangular Weir |
|  |  |  | Head (feet) 0.200 .400 .600 .801 .001 .201 .401 .601 .80 |
|  |  |  | 2.503 .003 .504 .004 .505 .005 .50 |
|  |  |  | Coef. (English) 2.462 .552 .702 .692 .682 .6812 .672 .642 .64 |
|  |  |  | 2.642 .652 .642 .652 .652 .662 .672 .69 |

Primary OutFlow Max=6.59 cfs @ 12.48 hrs HW=48.07' TW=38.86' (Dynamic Tailwater)
-1=Culvert (Passes 6.59 cfs of 6.77 cfs potential flow)
-2 $\mathbf{2}=\mathbf{O r i f i c e / G r a t e ~ ( P a s s e s ~} 1.01$ cfs of 2.20 cfs potential flow)
-3=Exfiltration (Exfiltration Controls 1.01 cfs)
-4=Orifice/Grate (Orifice Controls 5.58 cfs @ 4.62 fps )
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=42.17' TW=35.00' (Dynamic Tailwater) -5=Broad-Crested Rectangular Weir( Controls 0.00 cfs )

## Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.
[80] Warning: Exceeded Pond POND 1.1 by 7.52 @ 0.00 hrs (23.95 cfs 25.099 af)


Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

| 10 Year 25 | Point manual | elevation table, To= 0.00 hrs , $\mathrm{dt}=1.00 \mathrm{hrs}$, feet $=$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 |
| 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 |
| 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 | 55.07 |  |  |

## Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.
[80] Warning: Exceeded Pond POND 1.3 by 3.65 @ 0.00 hrs ( 92.51 cfs 86.028 af)


Primary outflow $=$ Inflow, Time Span $=0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}$
10 Year 2 Point manual elevation table, To= $0.00 \mathrm{hrs}, \mathrm{dt}=24.00 \mathrm{hrs}$, feet $=$ $38.65 \quad 38.65$

## Summary for Link PA2: POINT OF ANALYSIS



Primary outflow $=$ Inflow, Time Span $=0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}$

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=462,599 sf $72.19 \%$ Impervious Runoff Depth>6.00" Flow Length=933' Tc=11.4 min CN=91 Runoff=58.40 cfs 5.309 af

SubcatchmentPOST 1.1: WATERSHED Runoff Area=242,496 sf $58.73 \%$ Impervious Runoff Depth $>5.43$ " Flow Length=750' Tc=10.3 min CN=86 Runoff=29.42 cfs 2.517 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=101,204 sf 62.15\% Impervious Runoff Depth $>5.66$ " Flow Length=1,191' Tc=6.4 min CN=88 Runoff=14.27 cfs 1.095 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=306,549 sf 22.64\% Impervious Runoff Depth>4.39" Flow Length=1,525' Tc=45.9 min CN=77 Runoff=16.72 cfs 2.574 af

SubcatchmentPOST 1.4: WATERSHED Runoff Area=214,764 sf 85.05\% Impervious Runoff Depth>6.35" Flow Length=717' Tc=7.5 min CN=94 Runoff=31.40 cfs 2.610 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,290 sf $80.99 \%$ Impervious Runoff Depth>6.24" Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \quad \mathrm{CN}=93$ Runoff $=7.66 \mathrm{cfs} 0.588$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.86' Max Vel=2.20 fps Inflow=14.27 cfs 2.076 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0$ ' $\mathrm{S}=0.0092$ '/' Capacity=2,720.29 cfs Outflow=7.67 cfs 2.061 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=47.21' Storage=92,932 cf Inflow=58.40 cfs 5.309 af Primary=19.23 cfs 2.787 af Secondary=24.16 cfs 0.988 af Outflow=43.41 cfs 3.776 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=55.71' Storage=68,356 cf Inflow=29.42 cfs 2.517 af Outflow=4.20 cfs 0.981 af

Pond POND 1.2: PDMH203
Peak Elev=50.86' Inflow=14.27 cfs 2.076 af 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '//' Outflow=14.27 cfs 2.076 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.33' Storage=19,198 cf Inflow=67.56 cfs 10.378 af Primary $=66.14$ cfs 10.071 af Secondary $=0.00$ cfs 0.000 af Outflow= 66.14 cfs 10.071 af

Pond POND 1.4: RAINGARDEN1.0 Peak Elev=48.89' Storage=58,248 cf Inflow=31.40 cfs 2.610 af Primary=7.29 cfs 1.966 af Secondary= 0.00 cfs 0.000 af Outflow=7.29 cfs 1.966 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS
Inflow=4.20 cfs 0.981 af Primary $=4.20$ cfs 0.981 af

Inflow=66.14 cfs 10.071 af Primary=66.14 cfs 10.071 af

Inflow=7.66 cfs 0.588 af Primary=7.66 cfs 0.588 af

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method
SubcatchmentPOST 1.0: WATERSHED Runoff Area=462,599 sf $72.19 \%$ Impervious Runoff Depth>7.37" Flow Length=933' Tc=11.4 min CN=91 Runoff=70.91 cfs 6.521 af

SubcatchmentPOST 1.1: WATERSHED Runoff Area=242,496 sf $58.73 \%$ Impervious Runoff Depth>6.77" Flow Length=750' Tc=10.3 min CN=86 Runoff=36.28 cfs 3.140 af

SubcatchmentPOST 1.2: WATERSHED Runoff Area=101,204 sf $62.15 \%$ Impervious Runoff Depth>7.01" Flow Length=1,191' Tc=6.4 min CN=88 Runoff=17.48 cfs 1.358 af

SubcatchmentPOST 1.3: WATERSHED Runoff Area=306,549 sf 22.64\% Impervious Runoff Depth>5.65" Flow Length=1,525' Tc=45.9 min CN=77 Runoff=21.42 cfs 3.313 af

SubcatchmentPOST 1.4: WATERSHED Runoff Area=214,764 sf $85.05 \%$ Impervious Runoff Depth $>7.73$ " Flow Length=717' Tc=7.5 min CN=94 Runoff=37.84 cfs 3.177 af

SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,290 sf $80.99 \%$ Impervious Runoff Depth>7.62" Flow Length=758' $\mathrm{Tc}=5.0 \mathrm{~min} \quad \mathrm{CN}=93$ Runoff $=9.25 \mathrm{cfs} 0.718$ af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.90' Max Vel=2.19 fps Inflow=17.48 cfs 2.679 af $\mathrm{n}=0.040 \mathrm{~L}=1,309.0$ ' $\mathrm{S}=0.0092$ '//' Capacity=2,720.29 cfs Outflow=10.33 cfs 2.662 af

Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=47.48' Storage=98,793 cf Inflow=70.91 cfs 6.521 af Primary=19.73 cfs 3.345 af Secondary=38.14 cfs 1.616 af Outflow=57.87 cfs 4.961 af

Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=56.45' Storage=83,107 cf Inflow=36.28 cfs 3.140 af Outflow=6.58 cfs 1.321 af

Pond POND 1.2: PDMH203
Peak Elev=51.03' Inflow=17.48 cfs 2.679 af 48.0" Round Culvert $\mathrm{n}=0.013 \mathrm{~L}=269.0^{\prime} \mathrm{S}=0.0050$ '/' Outflow=17.48 cfs 2.679 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.77' Storage=24,643 cf Inflow=87.04 cfs 13.437 af Primary $=83.35$ cfs 13.109 af Secondary $=0.00$ cfs 0.000 af Outflow= 83.35 cfs 13.109 af

Pond POND 1.4: RAINGARDEN1.0 Peak Elev=49.56' Storage=69,290 cf Inflow=37.84 cfs 3.177 af Primary $=7.69$ cfs 2.462 af Secondary=1.60 cfs 0.039 af Outflow=9.29 cfs 2.500 af

## Link LINK 1.0: PDMH203 TAILWATER

## Link PA1: POINT OF ANALYSIS

Link PA2: POINT OF ANALYSIS
Inflow=6.58 cfs 1.321 af Primary $=6.58$ cfs 1.321 af

Inflow=83.35 cfs 13.109 af Primary $=83.35$ cfs 13.109 af

Inflow=9.25 cfs 0.718 af Primary $=9.25$ cfs 0.718 af

Total Runoff Area $=31.609$ ac Runoff Volume $=18.227$ af Average Runoff Depth $=6.92$ " $39.63 \%$ Pervious $=12.527$ ac $60.37 \%$ Impervious $=19.083$ ac


February 22, 2024
Prepared for:
Prepared by:

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## Conclusion

Collier's Engineering \& Design (CED) performed an analysis on the array areas of the proposed rooftop and carport solar project site in Portsmouth, Rockingham County, NH.

Through extensive cross-checking, it was found that at a 5-degree resting angle or above for the rooftop system panels, there is no predicted glare throughout the entire project area. Small amounts of green glare predicted from the carports onto a route directly next to the proposed project are easily mitigated.

The study area is presented in the graphic below. Red Markers represent Observation Points, Turquoise Lines are the roads in and around the proposed project area, and Brown Lines represent the existing foliage in the area and/or the proposed landscaping lines. The Brown Lines around the rooftop systems represent the parapets that run the entire perimeter of the buildings.


A closer view of the immediate project area:


The triangulation of the proposed project in relation to Portsmouth International Airport is provided below. Because of the proximity to the airport and the Air Traffic Control Tower, the client specifically requested a full study to be certain that no glare of any kind would affect the Tower.


To establish a worst-case scenario baseline, a 15-degree angle for the proposed rooftop system facing 214 degrees (azimuth) was programmed on the rooftops of two buildings. For the proposed carports, four array areas were programmed facing 124 degrees (azimuth) and one carport was programmed facing 214 degrees (azimuth). The project was modeled without local foliage lines and other large buildings between the proposed project and the ATCT in the area programmed.


The Air Traffic Control Tower was modeled at a dual height of 130 feet and 120 feet to cover broader possibilities of the proposed project's sightline to anyone in the tower structure.

With the above settings, the modelling predicts ZERO minutes of YELLOW glare over the course of an entire year and $\sim 4,474$ minutes of GREEN glare over the course of an entire year. The glare results include $\sim 1,863$ minutes of GREEN glare on the Air Traffic Control Tower at Portsmouth International Airport from Carports 1,3 and 4. No glare whatsoever is predicted from the rooftop systems onto the ATCT or onto any other point in the study.

At the proposed working settings of a 5 -degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and $\sim 802$ minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes $3(4.5$ feet) and $4(8.5$ feet) which run directly in front of the proposed project area.

At the proposed working settings of a 10-degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and $\sim 802$ minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 ( 4.5 feet) and 4 ( 8.5 feet) which run directly in front of the proposed project area.

At the proposed working settings of a 13-degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and $\sim 802$ minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes $3(4.5$ feet) and 4 ( 8.5 feet) which run directly in front of the proposed project area.

At the proposed working settings of a 15 -degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and $\sim 802$ minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 ( 4.5 feet) and 4 ( 8.5 feet) which run directly in front of the proposed project area.

A review of the Federal Aviation Administration's (FAA) New York area Visual Flight Rules (VFR) charts shows no restricted airspace in or around the proposed project area.


A review of Military Training Route (MTR) charts was performed utilizing an additional online resource and the proposed project falls entirely OUTSIDE of known training route areas.


The above conclusion is arrived at by utilizing the worst-case scenario results provided by the ForgeSolar software, and then manually layering back into each modeling scenario all real-world factors in the area of the proposed site location.

Full technical reporting output by the ForgeSolar program is included in the Appendix of this report.

## Sincerely,

Colliers Engineering \& Design, Inc.
(DBA Maser Consulting)

cc: Lee Hill, PE, Colliers Engineering \& Design (via email)

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## Resources

## Federal Aviation Administration - Publicly Available Visual Flight Rules (VFR) Charts https://www.faa.gov/air_traffic/flight_info/aeronav/digital_products/vfr/

- Utilized to obtain FAA-approved VFR charts of the project area for inclusion and consideration in this study.
U.S. Military Training Routes (MTRs) and buffers - May 4, 2018 (Last modified Oct 6, 2021)
Uploaded by South Atlantic Blueprint
https://salcc.databasin.org/datasets/4c81852be18444b997f8f860ee568c54/
- Utilized to obtain detail and graphic of US-wide Military Training Routes and location specific data for this study.

Ho, C. K., Ghanbari, C. M., and Diver, R. B., 2011, Methodology to Assess Potential Glint and Glare Hazards From Concentrating Solar Power Plants: Analytical Models and Experimental Validation, ASMEJ. Sol. Energy Eng., 133.

## Solar Glare Hazard Analysis Tool (SGHAT) Technical Reference Manual

## Details of Glare Study

## Methodology

## (Source Information: https://forgesolar.com/help/\#intro)

> Collier's Engineering \& Design (CED) offers staff specifically trained on glare analyses utilizing ForgeSolar, a web-based interactive software that provides a quantified assessment of (1) when and where glare is predicted to occur throughout the year for a prescribed solar installation, and (2) potential effects on the human eye at locations where glare is predicted to occur. ForgeSolar is based on the Solar Glare Hazard Analysis Tool ("SGHAT") licensed from Sandia National Laboratories.

These tools meet the FAA standards for glare analysis.
Determination of glare occurrence requires knowledge of the following: sun position, observer location, and the tilt, orientation, location, extent, and optical properties of the modules in the solar array. Vector algebra is then used to determine if glare is likely to be visible from the prescribed observation points.

If glare is predicted, the software calculates the retinal irradiance and subtended angle (size/distance) of the glare source to predict potential ocular hazards ranging from temporary afterimage to more severe possible retinal damage. These results are presented in a simple, easy-tointerpret plot that specifies when glare is predicted to occur throughout the year, with color codes indicating the potential ocular hazard.

## Background Information

Glint is typically defined as a momentary flash of bright light, often caused by a reflection off a moving source. A typical example of glint is a momentary solar reflection from a moving car, or "catching" something bright out of the corner of your eye.

Glare is defined as a continuous source of bright light. Glare is generally associated with stationary objects, which, due to the slow relative movement of the sun, reflect sunlight for a longer duration.

The difference between glint and glare is duration. Industry-standard glare analysis tools evaluate the occurrence of glare on a minute-by-minute basis; accordingly, they generally refer to solar hazards as 'glare.'

The ocular impact of solar glare is quantified into three categories (Ho, 2011):

1. Green - Unproblematic shine. Low potential to cause after-image. This type of glare can be compared to noticing something shiny in the distance.
2. Yellow - Potential to cause temporary afterimage (flash blindness). This type of glare is much like sunrise and sunset glare for drivers who struggle to find the perfect angle for car visors so they can continue to operate their vehicle safely while traveling through areas of such glare.
a. Standard levels of yellow glare can, for the most part, be handled with relative ease utilizing slatted fencing or localfoliage landscape mitigation measures.
b. Only extremely high levels of this type of glare (in the area of the chart to the right labeled as "direct viewing of the sun" which is uncommon to find with PV installations) would be considered an insurmountable hurdle to a PV installation of any size.


Figure 1 - From ForgeSolar website (sample glare hazard plot defining ocular impact as function of retinal irradiance and subtended source angle ( Ho, 2011))
c. High levels/intensities and long durations are different factors.
3. Red - Potential to cause retinal burn (permanent eye damage). PV modules do not focus reflected sunlight and therefore retinal burn (RED glare) is typically not possible.
d. This is the ONLY type of glare that would be considered an insurmountable hurdle to a PV installation of any size.

These categories assume a typical blink response in the observer.

## Note that retinal burn is typically not possible for PV glare since PV modules do not focus reflected sunlight. They are, in fact, designed to absorb as much sunlight as possible.

To further put glare into perspective, the following is presented.

YELLOW glare such as in the graphic to the right could only be seen when standing directly next to project panels at the perfect angle when the sun is in a perfect place—indeed the point of a photographer standing directly by these panels and waiting for the perfect moment to capture this image. It is also possible that the panels in the picture shown do not have an anti-reflective coating.


Solar panel showing solar glare

GREEN glare, as illustrated directly to the right, is the more common occurrence with solar projects-a noticeable shiny area (in the northwest area) as compared to panels where the sun is not quite in perfect alignment yet.

Even so, the effect of this noticeable shine to certain areas of the project area is still seen from a relatively close up vantage point and at the optimal height this image was captured, possibly by a drone. A
 similarly sized project in the distance, closer to the horizon of the photo would be unlikely to show even the levels of green glare that the system in the foreground reflects.

## Executive Summary

The purpose of the glare study requested by IPS - Integrated Project Service, LLC (IPS) and their client is to closely examine a proposed solar project in Portsmouth, Rockingham County, NH and to provide feedback regarding areas that may warrant closer examination in order to mitigate possible problematic predicted glare to the businesses, residences, and roads surrounding the project area.

Information was provided by IPS and their client in order to complete this study. The project's rooftop PV systems were programmed to a 15 -degree tilt axis facing 214 degrees at a height of 88 feet for the smaller structure and 93.83 feet for the larger building. The parapets for these buildings were programmed at heights of 93.21 feet and 99.3 feet respectively.

Four of the projects five carport systems were programmed with two top heights (20.17 feet and 22.48 feet) and a lower edge of 14 feet, facing 124 degrees southeast. A final carport was programmed with a 20.17 foot high edge, a 14 foot lower edge and facing 214 degrees.

It was further assumed that the panels used throughout the proposed project are constructed of Smooth Glass with an Anti-Reflective coating.

Seven (7) Observation Points were placed at different points around the site and programmed to an average height of 5 and a half (5.5) feet to model someone standing in these spots, and to a height of 15 to 20 feet to model a 5.5 -foot person standing on the second floor of a home/business with 8 foot ceilings and a 1.5-foot plenum space.


The building directly southwest of the proposed project is industrial in nature, and an examination of the portion that will be facing the project shows that it is industrial in nature with very few windows. One OP was programmed here at a height of 40 feet.


Two Observation Points representing the Air Traffic Control Tower at Portsmouth International Airport were programmed to heights of 130 feet and 120 feet.

Six (6) Route Receptors were programmed for two-way traffic to heights of 4.5 feet and 8.5 feet, effectively representing the eyeline of an average person sitting on/in any vehicle from a bike to a motorcycle, a standard car or SUV, through to the approximated seated height in the cab of an 18wheeler truck.


While it is impossible to study every possible point and/or angle surrounding a photovoltaic (solar) project, Collier's Engineering \& Design (CED) has modeled the project and surrounding areas as best as possible with the most likely points of concern.

PV modules do not focus reflected sunlight and therefore retinal burn is typically not possible. They are, in fact, designed to absorb as much sunlight as possible. Modern photovoltaic panels actually cause less glare than standard home window glass; and research has shown that they reflect less light than snow, white concrete and energy-efficient white rooftops.

The YELLOW glare we are looking to identified with this study is much like sunrise and sunset glare for drivers who struggle to find the perfect angle for car visors so they can continue to operate their vehicle safely while traveling through areas of such glare. In general, photovoltaic panel systems of any size produce some glare predominately during early sunrise and sunset throughout the Spring
through Fall months-although glare is possible throughout each day as well as throughout the entire year.

ForgeSolar now allows the programming of obstructions. It was utilized in this study to model in existing treelines, local warehouses and other buildings and the parapets of the proposed new buildsings for this project with estimated heights. Local foliage lines were modeled at a conservative height of 17 to 30 feet in height. Local warehouses were modeled conservatively at 20 to 30 feet high.


After examining each point and then factoring in additionally recommended foliage, distance, and elevation changes, points where predicted glare is blocked by natural obstructions were removed from the listing of points to be examined more closely. Finally, if any glare continues to be predicted in any area, this analyst will address the areas that present the most possibility for likely glare.

## ASSUMPTIONS

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.*
- Glare analyses do not account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographic obstructions.
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Glare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.


## Results of this Study

## WORST CASE SCENARIO without Local Foliage - RESULTS at 15 Degree Resting Angle

To establish a worst-case scenario baseline, the project was modeled without any local foliage lines or building obstructions between the proposed project and the Air Traffic Control Tower at the Portsmouth International Airport. The modelling predicts ZERO minutes of YELLOW glare over the course of an entire year and $\sim 4,474$ minutes of GREEN glare over the course of an entire year. The glare results include $\sim 1,855$ minutes of GREEN glare on the Air Traffic Control Tower at Portsmouth International Airport from Carports 1, 3 and 4. No glare whatsoever is predicted from the rooftop systems onto the ATCT or onto any other point in the study.

## RESULTS at 5 Degree Angle

At the proposed working settings of a 5 -degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and $\sim 802$ minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 ( 4.5 feet) and 4 ( 8.5 feet) which run directly in front of the proposed project area.

## RESULTS at 10 Degree Resting Angle

At the proposed working settings of a 10 -degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and $\sim 802$ minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 ( 4.5 feet) and 4 ( 8.5 feet) which run directly in front of the proposed project area.

## RESULTS at 13 Degree Resting Angle

At the proposed working settings of a 13-degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and $\sim 802$ minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 ( 4.5 feet) and 4 ( 8.5 feet) which run directly in front of the proposed project area.

## RESULTS at 15 Degree Resting Angle

At the proposed working settings of a 15-degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and $\sim 802$ minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 ( 4.5 feet) and 4 ( 8.5 feet) which run directly in front of the proposed project area.

## AREAS OF GLARE

In ALL results, the areas of glare from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.


A final run scenario with a small planting of trees at the area marked in green in the "Positions Along Path Receiving Glare" shows that a screen of 9 feet at initial planting will completely mitigate any glare shown.

Summary of Results No glare predicted!

| PV Name | Tilt | Orientation | "Green" Glare |
| :--- | :---: | :---: | :---: |
|  | deg | deg | min |
| CRPRT1 | 0.0 | 124.0 | 0 |
| CRPRT2 | 0.0 | 124.0 | 0 |
| CRPRT3 | 0.0 | 124.0 | 0 |
| CRPRT4 | 0.0 | 124.0 | 0 |
| CRPRT5 | 0.0 | 214.0 | 0 |
| LGBLDG | 10.0 | 214.0 | 0 |
| SMBLDG | 10.0 | 214.0 | 0 |



## Summary of FAA-Level Flight Path Screening Results

Portsmouth International Airport sits under 1 mile away from the project on the western side. All obstructions were kept in place for the FAA screening and the project was modeled at the 10 degree rooftop PV system tilt.

## FEDERAL AVIATION ADMINISTRATION (FAA) SCREENS

An FAA-level glare analysis was performed and a report specific to this request can be found in Appendix A of this report. The Air Traffic Control Tower at Portsmouth International Airport is modeled for this study at its height of 130 feet. Additionally, a second point was modeled at 120 feet to be certain of the glare study results.

Per the FAA's most recent 2021 policy regarding solar around airports, this project PASSES.

Project: ALBACORE, Portsmouth, NH<br>Site configuration: Albacore_10DegreeTilt_124Carports_ATCT_FAAReport

Created 22 Feb, 2024 Updated 22 Feb, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg DNI peaks at $1,000.0 \mathrm{~W} / \mathrm{m}^{2}$ Site ID 112738.19298

Ocular transmission coefficient 0.5
Pupil diameter 0.002 m Eye focal length 0.017 m Sun subtended angle 9.3 mrad PV analysis methodology V2

## Glare Policy Adherence

The following table estimates the policy adherence of this glare analysis according to the 2021 U.S. Federal Aviation Administration Policy: Review of Solar Energy System Projects on Federally-Obligated Airports

This policy may require the following criteria be met for solar energy systems on airport property:

- No glare of any kind for Air Traffic Control Tower(s) ("ATCT") at cab height.
- Default analysis and observer characteristics, including 1-minute time step.

ForgeSolar is not affiliated with the U.S. FAA and does not represent or speak officially for the U.S. FAA. ForgeSolar cannot approve or deny projects - results are informational only. Contact the relevant airport and FAA district office for information on policy and requirements.

| COMPONENT | STATUS | DESCRIPTION |
| :--- | :--- | :--- |
| Analysis parameters | PASS | Analysis time interval and eye characteristics used are acceptable |
| ATCT(s) | PASS | Receptor(s) marked as ATCT do not receive glare |

The complete updated FAA Policy can be read at: https://www.federalregister.gov/d/2021-09862
NOTE: ForgeSolar does not represent or speak officially for the FAA and cannot approve or deny projects. Results are informational only.

## On May 26, 2021, the Federal Aviation Administration updated their policies regarding the installation of solar on and/or near regulated airports/airstrips.

While this policy of the Federal Aviation Administeration does not apply to solar energy systems on airports that do not have an Air Traffic Control Tower (ATCT), airports that are not federally-obligated, or solar energy systems not located on airport property-it does provide a high benchmark to meet to ensure that proposed solar installations do not create glare that poses any sort of safety hazard for pilots.

The brief of this FAA policy update states:
"The Federal Aviation Administration (FAA) published a final policy aimed at ensuring that airport solar projects don't create hazardous glare. The policy requires airports to measure the visual impact of such projects on pilots and air traffic control personnel.

The policy applies to proposed solar energy systems at federally obligated airports with control towers. Federally obligated airports are public airports that have accepted federal assistance either in the form of grants of property conveyances

As more airports invests in this technology for environmental and economic benefits, the FAA wants to make sure that the reflection from the systems'glass surfaces do not create a glare that poses a safety hazard for pilots and air traffic controllers.

Under the final policy, airports are no longer required to submit the results of an ocular analysis to FAA. Instead, the airport must file a Notice of Proposed Construction or Alteration Form 7460-1 that includes a statement that the project will not cause any visual impact. The airport submits the form to the FAA for review and approval.

The FAA relies on the airport to confirm via the form that it has sufficiently analyzed the potential for glint and glare and determined there is no potential for ocular impact to the airport traffic control tower cab. If any impacts are discovered after construction, the airport must mitigate the impact at its expense. The airport may also face compliance action for failure to address visual impacts that create aviation safety hazards. As such, the agency encourages an airport to conduct sufficient analysis before installing a solar energy system.

The FAA is also withdrawing the recommended tool for measuring the ocular impact of potential glint and glare effects on pilots and air traffic controllers."

Additionally:
"Initially, FAA believed that solar energy systems could introduce a novel glint and glare effect to pilots on final approach. FAA has subsequently concluded that in most cases, the glint and glare from solar energy systems to pilots on final approach is similar to glint and glare pilots routinely experience from water bodies, glass-façade buildings, parking lots, and similar features. However, FAA has continued to receive reports of potential glint and glare from on-airport solar energy systems on personnel working in ATCT cabs. Therefore, FAA has determined the scope of agency policy should be focused on the impact of on-airport solar energy systems to federally-obligated towered airports, specifically the airport's ATCT cab."

## Appendix

## Appendix A | Detailed Glare Study Result Reports

The following pages are the full reporting results delivered directly from ForgeSolar.

## FORGESOLAR GLARE ANALYSIS

Project: ALBACORE, Portsmouth, NH
Site configuration: Albacore_10DegreeTilt_124Carports_ATCT_FAAReport

Client: Lonza

Created 22 Feb, 2024
Updated 22 Feb, 2024
Time-step 1 minute
Timezone offset UTC-5
Minimum sun altitude 0.0 deg
DNI peaks at $1,000.0 \mathrm{~W} / \mathrm{m}^{2}$
Site ID 112738.19298

Ocular transmission coefficient 0.5
Pupil diameter 0.002 m
Eye focal length 0.017 m
Sun subtended angle 9.3 mrad
PV analysis methodology V2


## Glare Policy Adherence

The following table estimates the policy adherence of this glare analysis according to the 2021 U.S. Federal Aviation Administration Policy: Review of Solar Energy System Projects on Federally-Obligated Airports

This policy may require the following criteria be met for solar energy systems on airport property:

- No glare of any kind for Air Traffic Control Tower(s) ("ATCT") at cab height.
- Default analysis and observer characteristics, including 1-minute time step.

ForgeSolar is not affiliated with the U.S. FAA and does not represent or speak officially for the U.S. FAA. ForgeSolar cannot approve or deny projects - results are informational only. Contact the relevant airport and FAA district office for information on policy and requirements.

| COMPONENT | STATUS | DESCRIPTION |
| :--- | :--- | :--- |
| Analysis parameters | PASS | Analysis time interval and eye characteristics used are acceptable |
| ATCT(s) | PASS | Receptor(s) marked as ATCT do not receive glare |

The referenced policy can be read at https://www.federalregister.gov/d/2021-09862

## Component Data

This report includes results for PV arrays and Observation Point ("OP") receptors marked as ATCTs. Components that are not pertinent to the policy, such as routes, flight paths, and vertical surfaces, are excluded.

## PV Arrays

Name: CRPRT1
Axis tracking: Fixed (no rotation)
Tilt: $0.0^{\circ}$
Orientation: $124.0^{\circ}$
Rated power: -
Panel material: Smooth glass with AR coating
Reflectivity: Vary with sun
Slope error: correlate with material


| Vertex | Latitude ( ${ }^{\circ}$ ) | Longitude ( ${ }^{\circ}$ ) | Ground elevation ( ft ) | Height above ground (ft) | Total elevation (ft) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1 | 43.085650 | -70.803723 | 57.92 | 20.17 | 78.09 |
| 2 | 43.085595 | -70.803619 | 57.81 | 14.00 | 71.81 |
| 3 | 43.085032 | -70.804187 | 64.54 | 14.00 | 78.54 |
| 4 | 43.085084 | -70.804291 | 66.68 | 20.17 | 86.85 |

Name: CRPRT2
Axis tracking: Fixed (no rotation)
Tilt: $0.0^{\circ}$
Orientation: $124.0^{\circ}$
Rated power: -
Panel material: Smooth glass with AR coating
Reflectivity: Vary with sun
Slope error: correlate with material


| Vertex | Latitude ( ${ }^{\circ}$ ) | Longitude ( ${ }^{\circ}$ ) | Ground elevation (ft) | Height above ground (ft) | Total elevation (ft) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1 | 43.085519 | -70.803626 | 57.88 | 22.48 | 80.36 |
| 2 | 43.085431 | -70.803461 | 56.75 | 14.00 | 70.75 |
| 3 | 43.084981 | -70.803912 | 58.98 | 14.00 | 72.98 |
| 4 | 43.085070 | -70.804083 | 59.73 | 22.48 | 82.20 |

Name: CRPRT3
Axis tracking: Fixed (no rotation)
Tilt: $0.0^{\circ}$
Orientation: $124.0^{\circ}$
Rated power: -
Panel material: Smooth glass with AR coating
Reflectivity: Vary with sun
Slope error: correlate with material


| Vertex | Latitude ( ${ }^{\circ}$ ) | Longitude ( ${ }^{\circ}$ ) | Ground elevation (ft) | Height above ground (ft) | Total elevation (ft) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1 | 43.085400 | -70.803418 | 56.90 | 22.48 | 79.38 |
| 2 | 43.085325 | -70.803271 | 56.23 | 14.00 | 70.23 |
| 3 | 43.084876 | -70.803716 | 58.56 | 14.00 | 72.56 |
| 4 | 43.084953 | -70.803866 | 59.01 | 22.48 | 81.49 |

Name: CRPRT4
Axis tracking: Fixed (no rotation)
Tilt: $0.0^{\circ}$
Orientation: $124.0^{\circ}$
Rated power: -
Panel material: Smooth glass with AR coating
Reflectivity: Vary with sun
Slope error: correlate with material


| Vertex | Latitude ( ${ }^{\circ}$ ) | Longitude ( ${ }^{\circ}$ ) | Ground elevation (ft) | Height above ground (ft) | Total elevation (ft) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1 | 43.085298 | -70.803223 | 56.02 | 20.17 | 76.19 |
| 2 | 43.085253 | -70.803139 | 56.21 | 14.00 | 70.21 |
| 3 | 43.084808 | -70.803572 | 58.45 | 14.00 | 72.45 |
| 4 | 43.084851 | -70.803658 | 58.35 | 20.17 | 78.52 |

Name: CRPRT5
Axis tracking: Fixed (no rotation)
Tilt: $0.0^{\circ}$
Orientation: $214.0^{\circ}$
Rated power: -
Panel material: Smooth glass with AR coating
Reflectivity: Vary with sun
Slope error: correlate with material


| Vertex | Latitude $\left({ }^{\circ}\right)$ | Longitude ( ${ }^{\circ}$ ) | Ground elevation (ft) | Height above ground (ft) | Total elevation (ft) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1 | 43.085549 | -70.803405 | 56.86 | 20.17 | 77.02 |
| 2 | 43.085404 | -70.803116 | 55.16 | 20.17 | 75.32 |
| 3 | 43.085334 | -70.803188 | 55.25 | 14.00 | 69.25 |
| 4 | 43.085478 | -70.803470 | 57.01 | 14.00 | 71.01 |

Name: LGBLDG
Axis tracking: Fixed (no rotation)
Tilt: $10.0^{\circ}$
Orientation: $214.0^{\circ}$
Rated power: -
Panel material: Smooth glass with AR coating
Reflectivity: Vary with sun
Slope error: correlate with material


| Vertex | Latitude ( ${ }^{\circ}$ ) | Longitude ( ${ }^{\circ}$ ) | Ground elevation (ft) | Height above ground (ft) | Total elevation (ft) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | 43.084344 | -70.802133 | 51.60 | 93.83 | 145.44 |
| 2 | 43.084054 | -70.801543 | 49.18 | 93.83 | 143.01 |
| 3 | 43.083901 | -70.801690 | 49.39 | 93.83 | 143.22 |
| 4 | 43.083859 | -70.801609 | 49.20 | 93.83 | 143.03 |
| 5 | 43.083897 | -70.801574 | 49.27 | 93.83 | 143.10 |
| 6 | 43.083839 | -70.801453 | 47.35 | 93.83 | 141.18 |
| 7 | 43.083345 | -70.801919 | 51.93 | 93.83 | 145.76 |
| 8 | 43.083906 | -70.803019 | 59.40 | 93.83 | 153.23 |
| 9 | 43.084395 | -70.802537 | 54.24 | 93.83 | 148.07 |
| 10 | 43.084315 | -70.802368 | 51.53 | 93.83 | 145.36 |
| 11 | 43.084337 | -70.802347 | 51.04 | 93.83 | 144.87 |
| 12 | 43.084303 | -70.802278 | 52.48 | 93.83 | 146.31 |
| 13 | 43.084336 | -70.802245 | 52.51 | 93.83 | 146.34 |
| 14 | 43.084297 | -70.802171 | 51.69 | 93.83 | 145.52 |

## Name: SMBLDG

Axis tracking: Fixed (no rotation)
Tilt: $10.0^{\circ}$
Orientation: $214.0^{\circ}$
Rated power: -
Panel material: Smooth glass with AR coating
Reflectivity: Vary with sun
Slope error: correlate with material


| Vertex | Latitude ( ${ }^{\circ}$ ) | Longitude ( ${ }^{\circ}$ ) | Ground elevation (ft) | Height above ground (ft) | Total elevation (ft) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1 | 43.084480 | -70.803051 | 56.19 | 88.00 | 144.19 |
| 2 | 43.084450 | -70.803081 | 56.31 | 88.00 | 144.31 |
| 3 | 43.084506 | -70.803193 | 56.74 | 88.00 | 144.74 |
| 4 | 43.084466 | -70.803232 | 56.81 | 88.00 | 144.81 |
| 5 | 43.084412 | -70.803118 | 56.55 | 88.00 | 144.55 |
| 6 | 43.084252 | -70.803275 | 58.91 | 88.00 | 146.91 |
| 7 | 43.084414 | -70.803594 | 61.58 | 88.00 | 149.58 |
| 8 | 43.084643 | -70.803375 | 58.79 | 88.00 | 146.79 |

## Observation Point ATCT Receptors

| Name | ID | Latitude ( ${ }^{\circ}$ ) | Longitude ( ${ }^{\circ}$ ) | Elevation (ft) | Height ( ft ) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 1-ATCT | 1 | 43.084384 | -70.818882 | 89.93 | 130.00 |
| 6-ATCT | 6 | 43.084349 | -70.818856 | 89.97 | 120.00 |

Map image of 1-ATCT


Map image of 6-ATCT


## Obstruction Components



Name: BLDG2
Top height: 20.0 ft


| Vertex | Latitude $\left({ }^{\circ}\right)$ | Longitude $\left({ }^{\circ}{ }^{\circ}\right)$ | Ground elevation (ft) |
| :--- | :---: | :---: | :---: |
| 1 | 43.084955 | -70.806346 | 99.52 |
| 2 | 43.085031 | -70.806408 | 98.08 |
| 3 | 43.084866 | -70.806801 | 99.55 |
| 4 | 43.084555 | -70.806565 | 99.98 |
| 5 | 43.084608 | -70.806439 | 99.85 |
| 6 | 43.084444 | -70.806325 | 99.64 |
| 7 | 43.084592 | -70.806011 | 99.08 |
| 8 | 43.084965 | -70.806346 | 99.43 |



Name: HighEdge2
Top height: 22.5 ft


| Vertex | Latitude $\left({ }^{\circ}\right)$ | Longitude $\left({ }^{\circ}\right)$ | Ground elevation (ft) |
| :--- | :---: | :---: | :---: |
| 1 | 43.085593 | -70.803598 | 57.75 |
| 2 | 43.085019 | -70.804161 | 63.07 |

Name: HighEdge3
Top height: 22.5 ft


| Vertex | Latitude $\left({ }^{\circ}\right)$ | Longitude $\left({ }^{\circ}\right)$ | Ground elevation (ft) |
| :--- | :---: | :---: | :---: |
| 1 | 43.085424 | -70.803445 | 56.71 |
| 2 | 43.084960 | -70.803895 | 59.16 |



| Name: PRPT1 <br> Top height: 93.2 ft |  | Googlefer |  |
| :---: | :---: | :---: | :---: |
| Vertex | Latitude ( ${ }^{\circ}$ ) | Longitude ( ${ }^{\circ}$ ) | Ground elevation (ft) |
| 1 | 43.084674 | -70.803390 | 58.96 |
| 2 | 43.084478 | -70.802983 | 56.11 |
| 3 | 43.084211 | -70.803240 | 59.29 |
| 4 | 43.084415 | -70.803648 | 62.46 |
| 5 | 43.084674 | -70.803390 | 58.96 |


| Name: PRPT2 <br> Top height: 99.3 ft |  |  |  |
| :---: | :---: | :---: | :---: |
| Vertex | Latitude ( ${ }^{\circ}$ ) | Longitude ( ${ }^{\circ}$ ) | Ground elevation (ft) |
| 1 | 43.084580 | -70.802457 | 53.31 |
| 2 | 43.083953 | -70.801212 | 46.09 |
| 3 | 43.083224 | -70.801856 | 52.36 |
| 4 | 43.083866 | -70.803165 | 61.10 |
| 5 | 43.084580 | -70.802457 | 53.31 |

Name: TREELINE
Top height: 35.0 ft


| Vertex | Latitude $\left({ }^{\circ}\right)$ | Longitude $\left({ }^{\circ}\right)$ | Ground elevation (ft) |
| :--- | :---: | :---: | :---: |
| 1 | 43.085164 | -70.808848 | 82.83 |
| 2 | 43.085454 | -70.807942 | 81.22 |
| 3 | 43.085373 | -70.807765 | 82.86 |
| 4 | 43.085040 | -70.807564 | 86.97 |



Name: Trees
Top height: 17.0 ft


| Vertex | Latitude $\left({ }^{\circ}\right)$ | Longitude $\left({ }^{\circ}\right)$ | Ground elevation (ft) |
| :--- | :---: | :---: | :---: |
| 1 | 43.085036 | -70.807176 | 92.20 |
| 2 | 43.084131 | -70.806567 | 95.41 |



| Name: Trees2 |
| :--- |
| Top height: 60.0 ft |
|  |
|  |
|  |



Name: Trees4
Top height: 30.0 ft


| Vertex | Latitude $\left({ }^{\circ}\right)$ | Longitude $\left({ }^{\circ}\right)$ | Ground elevation (ft) |
| :--- | :---: | :---: | :---: |
| 1 | 43.085793 | -70.815175 | 77.90 |
| 2 | 43.085354 | -70.814585 | 81.00 |
| 3 | 43.086098 | -70.812858 | 77.64 |



| Name: Trees6 |
| :--- |
| Top height: 20.0 ft |
| Latitude ( ${ }^{\circ}$ ) |
| 43.085286 |





## Glare Analysis Results

Summary of Results No glare predicted

| PV Array | Tilt | Orient | Annual Green Glare |  | Annual Yellow Glare | Energy |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\circ^{2}$ | $\circ$ | $\mathbf{m i n}$ | $\mathbf{h r}$ | $\mathbf{m i n}$ | $\mathbf{h r}$ | $\mathbf{k W h}$ |
| CRPRT1 | 0.0 | 124.0 | 0 | 0.0 | 0 | 0.0 | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0.0 | 0 | 0.0 | - |
| CRPRT3 | 0.0 | 124.0 | 0 | 0.0 | 0 | 0.0 | - |
| CRPRT4 | 0.0 | 124.0 | 0 | 0.0 | 0 | 0.0 | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0.0 | 0 | 0.0 | - |
| LGBLDG | 10.0 | 214.0 | 0 | 0.0 | 0 | 0.0 | - |
| SMBLDG | 10.0 | 214.0 | 0 | 0.0 | 0 | 0.0 | - |

Total annual glare received by each receptor; may include duplicate times of glare from multiple reflective surfaces.

| Receptor | Annual Green Glare |  | Annual Yellow Glare |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $\min$ | hr | $\min$ | hr |
| 1-ATCT | 0 | 0.0 | 0 | 0.0 |
| 6-ATCT | 0 | 0.0 | 0 | 0.0 |

## PV: CRPRT1

| Receptor | Annual Green Glare |  | Annual Yellow Glare |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $\min$ | hr | $\min$ | hr |
| 1-ATCT | 0 | 0.0 | 0 | 0.0 |
| 6-ATCT | 0 | 0.0 | 0 | 0.0 |

## CRPRT1 and 1-ATCT

Receptor type: ATCT Observation Point No glare found

## CRPRT1 and 6-ATCT

Receptor type: ATCT Observation Point
No glare found

## PV: CRPRT2

| Receptor | Annual Green Glare |  | Annual Yellow Glare |  |
| :--- | :---: | :---: | :---: | :---: |
|  | min | hr | $\min$ | hr |
| 1-ATCT | 0 | 0.0 | 0 | 0.0 |
| 6-ATCT | 0 | 0.0 | 0 | 0.0 |

## CRPRT2 and 1-ATCT

Receptor type: ATCT Observation Point
No glare found

## CRPRT2 and 6-ATCT

Receptor type: ATCT Observation Point
No glare found

## PV: CRPRT3

| Receptor | Annual Green Glare |  | Annual Yellow Glare |  |
| :--- | :---: | :---: | :---: | :---: |
|  | min | hr | $\min$ | hr |
| 1-ATCT | 0 | 0.0 | 0 | 0.0 |
| 6-ATCT | 0 | 0.0 | 0 | 0.0 |

## CRPRT3 and 1-ATCT

Receptor type: ATCT Observation Point No glare found

## CRPRT3 and 6-ATCT

Receptor type: ATCT Observation Point
No glare found

## PV: CRPRT4

| Receptor | Annual Green Glare |  | Annual Yellow Glare |
| :--- | :---: | :---: | :---: |
|  | $\min$ | hr | $\min$ |
| 1-ATCT | 0 | 0.0 | 0 |
| 6-ATCT | 0 | 0.0 | 0 |

## CRPRT4 and 1-ATCT

Receptor type: ATCT Observation Point No glare found

## CRPRT4 and 6-ATCT

Receptor type: ATCT Observation Point
No glare found

## PV: CRPRT5

| Receptor | Annual Green Glare |  | Annual Yellow Glare |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $\min$ | hr | $\min$ | hr |
| 1-ATCT | 0 | 0.0 | 0 | 0.0 |
| 6-ATCT | 0 | 0.0 | 0 | 0.0 |

## CRPRT5 and 1-ATCT

Receptor type: ATCT Observation Point No glare found

## CRPRT5 and 6-ATCT

Receptor type: ATCT Observation Point
No glare found

## PV: LGBLDG

| Receptor | Annual Green Glare |  | Annual Yellow Glare |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $\min$ | hr | $\min$ | hr |
| 1-ATCT | 0 | 0.0 | 0 | 0.0 |
| 6-ATCT | 0 | 0.0 | 0 | 0.0 |

## LGBLDG and 1-ATCT

Receptor type: ATCT Observation Point
No glare found

## LGBLDG and 6-ATCT

Receptor type: ATCT Observation Point
No glare found

## PV: SMBLDG

| Receptor | Annual Green Glare |  | Annual Yellow Glare |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $\min$ | hr | $\min$ | hr |
| 1-ATCT | 0 | 0.0 | 0 | 0.0 |
| 6-ATCT | 0 | 0.0 | 0 | 0.0 |

## SMBLDG and 1-ATCT

Receptor type: ATCT Observation Point
No glare found

## SMBLDG and 6-ATCT

Receptor type: ATCT Observation Point
No glare found

## Assumptions

"Green" glare is glare with low potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. "Yellow" glare is glare with potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
The algorithm does not rigorously represent the detailed geometry of a system; detailed features such as gaps between modules, variable height of the PV array, and support structures may impact actual glare results. However, we have validated our models against several systems, including a PV array causing glare to the air-traffic control tower at Manchester-Boston Regional Airport and several sites in Albuquerque, and the tool accurately predicted the occurrence and intensity of glare at different times and days of the year.
Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare. This primarily affects V1 analyses of path receptors.
Random number computations are utilized by various steps of the annual hazard analysis algorithm. Predicted minutes of glare can vary between runs as a result. This limitation primarily affects analyses of Observation Point receptors, including ATCTs. Note that the SGHAT/ ForgeSolar methodology has always relied on an analytical, qualitative approach to accurately determine the overall hazard (i.e. green vs. yellow) of expected glare on an annual basis.
The analysis does not automatically consider obstacles (either man-made or natural) between the observation points and the prescribed solar installation that may obstruct observed glare, such as trees, hills, buildings, etc.
The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
The variable direct normal irradiance (DNI) feature (if selected) scales the user-prescribed peak DNI using a typical clear-day irradiance profile. This profile has a lower DNI in the mornings and evenings and a maximum at solar noon. The scaling uses a clear-day irradiance profile based on a normalized time relative to sunrise, solar noon, and sunset, which are prescribed by a sun-position algorithm and the latitude and longitude obtained from Google maps. The actual DNI on any given day can be affected by cloud cover, atmospheric attenuation, and other environmental factors.
The ocular hazard predicted by the tool depends on a number of environmental, optical, and human factors, which can be uncertain. We provide input fields and typical ranges of values for these factors so that the user can vary these parameters to see if they have an impact on the results. The speed of SGHAT allows expedited sensitivity and parametric analyses.
The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid based on aggregated research data. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.
Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
Refer to the Help page at www.forgesolar.com/help/ for assumptions and limitations not listed here.

Default glare analysis parameters and observer eye characteristics (for reference only):

- Analysis time interval: 1 minute
- Ocular transmission coefficient: 0.5
- Pupil diameter: 0.002 meters
- Eye focal length: 0.017 meters
- Sun subtended angle: 9.3 milliradians


# ALBACORE, Portsmouth, NH Albacore_10DegreeTilt_124Carports_ATCT_FAAReport 

## Client: Lonza

Created Feb 22, 2024
Updated Feb 22, 2024
Time-step 1 minute
Timezone offset UTC-5
Minimum sun altitude 0.0 deg
Site ID 112738.19298
Project type Advanced
Project status: active
Category 1 MW to 5 MW


Misc. Analysis Settings

DNI: varies ( $1,000.0 \mathbf{W} / \mathrm{m}^{\wedge} \mathbf{2}$ peak)
Ocular transmission coefficient: 0.5
Pupil diameter: $\mathbf{0 . 0 0 2} \mathbf{~ m}$
Eye focal length: 0.017 m
Sun subtended angle: 9.3 mrad

PV Analysis Methodology: Version 2
Enhanced subtended angle calculation: On

Summary of Results No glare predicted!

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{d e g}$ | $\mathbf{d e g}$ | $\boldsymbol{m i n}$ | $\boldsymbol{m i n}$ | $\mathbf{k W h}$ |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT3 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT4 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - |
| LGBLDG | 10.0 | 214.0 | 0 | 0 | - |
| SMBLDG | 10.0 | 214.0 | 0 | 0 | - |

## Component Data

## PV Array(s)

Total PV footprint area: 3.1 acres

| Name: CRPRT1 <br> Footprint area: 0.20 acre | Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Axis tracking: Fixed (no rotation) Tilt: 0.0 deg <br> Orientation: 124.0 deg |  | deg | $\operatorname{deg}$ | ft | ft | ft |
| Rated power: - | 1 | 43.085650 | -70.803723 | 57.92 | 20.17 | 78.09 |
| Panel material: Smooth glass with AR coating | 2 | 43.085595 | -70.803619 | 57.81 | 14.00 | 71.81 |
| Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes | 3 | 43.085032 | -70.804187 | 64.54 | 14.00 | 78.54 |
| Slope error: 8.43 mrad | 4 | 43.085084 | -70.804291 | 66.68 | 20.17 | 86.85 |



Name: CRPRT2
Footprint area: 0.26 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085519 | -70.803626 | 57.88 | 22.48 | 80.36 |
| 2 | 43.085431 | -70.803461 | 56.75 | 14.00 | 70.75 |
| 3 | 43.084981 | -70.803912 | 58.98 | 14.00 | 72.98 |
| 4 | 43.085070 | -70.804083 | 59.73 | 22.48 | 82.20 |



Name: CRPRT3
Footprint area: 0.23 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 124.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes
Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085400 | -70.803418 | 56.90 | 22.48 | 79.38 |
| 2 | 43.085325 | -70.803271 | 56.23 | 14.00 | 70.23 |
| 3 | 43.084876 | -70.803716 | 58.56 | 14.00 | 72.56 |
| 4 | 43.084953 | -70.803866 | 59.01 | 22.48 | 81.49 |



Name: CRPRT4
Footprint area: 0.13 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085298 | -70.803223 | 56.02 | 20.17 | 76.19 |
| 2 | 43.085253 | -70.803139 | 56.21 | 14.00 | 70.21 |
| 3 | 43.084808 | -70.803572 | 58.45 | 14.00 | 72.45 |
| 4 | 43.084851 | -70.803658 | 58.35 | 20.17 | 78.52 |



Name: CRPRT5
Footprint area: 0.07 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085549 | -70.803405 | 56.86 | 20.17 | 77.02 |
| 2 | 43.085404 | -70.803116 | 55.16 | 20.17 | 75.32 |
| 3 | 43.085334 | -70.803188 | 55.25 | 14.00 | 69.25 |
| 4 | 43.085478 | -70.803470 | 57.01 | 14.00 | 71.01 |



Name: LGBLDG
Footprint area: 2.0 acres
Axis tracking: Fixed (no rotation)
Tilt: 10.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.084344 | -70.802133 | 51.60 | 93.83 | 145.44 |
| 2 | 43.084054 | -70.801543 | 49.18 | 93.83 | 143.01 |
| 3 | 43.083901 | -70.801690 | 49.39 | 93.83 | 143.22 |
| 4 | 43.083859 | -70.801609 | 49.20 | 93.83 | 143.03 |
| 5 | 43.083897 | -70.801574 | 49.27 | 93.83 | 143.10 |
| 6 | 43.083839 | -70.801453 | 47.35 | 93.83 | 141.18 |
| 7 | 43.083345 | -70.801919 | 51.93 | 93.83 | 145.76 |
| 8 | 43.083906 | -70.803019 | 59.40 | 93.83 | 153.23 |
| 10 | 43.084395 | -70.802537 | 54.24 | 93.83 | 148.07 |
| 11 | 43.084315 | -70.802368 | 51.53 | 93.83 | 145.36 |
| 12 | 43.084337 | -70.802347 | 51.04 | 93.83 | 144.87 |
| 13 | 43.084303 | -70.802278 | 52.48 | 93.83 | 146.31 |
| 14 | 43.084336 | -70.802245 | 52.51 | 93.83 | 146.34 |
|  |  |  | 51.69 |  | 145.52 |


| Name: SMBLDG <br> Footprint area: 0.22 acre <br> Axis tracking: Fixed (no rotation) <br> Tilt: 10.0 deg <br> Orientation: 214.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rated power: - | 1 | 43.084480 | -70.803051 | 56.19 | 88.00 | 144.19 |
| Panel material: Smooth glass with AR coating | 2 | 43.084450 | -70.803081 | 56.31 | 88.00 | 144.31 |
| Vary reflectivity with sun position? Yes | 3 | 43.084506 | -70.803193 | 56.74 | 88.00 | 144.74 |
| Slope error: 8.43 mrad | 4 | 43.084466 | -70.803232 | 56.81 | 88.00 | 144.81 |
|  | 5 | 43.084412 | -70.803118 | 56.55 | 88.00 | 144.55 |
|  | 6 | 43.084252 | -70.803275 | 58.91 | 88.00 | 146.91 |
|  | 7 | 43.084414 | -70.803594 | 61.58 | 88.00 | 149.58 |
|  | 8 | 43.084643 | -70.803375 | 58.79 | 88.00 | 146.79 |

## Discrete Observation Receptors

| Number | Latitude | Longitude | Ground elevation | Height above ground | Total Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | ft | ft | ft |
| 1-ATCT | 43.084384 | -70.818882 | 89.93 | 130.00 | 219.93 |
| OP 2 | 43.082455 | -70.800057 | 42.02 | 20.00 | 62.02 |
| OP 3 | 43.082529 | -70.799934 | 41.99 | 30.00 | 71.99 |
| OP 4 | 43.083085 | -70.799471 | 39.01 | 6.00 | 45.01 |
| OP 5 | 43.083191 | -70.799294 | 38.75 | 15.00 | 53.75 |
| 6-ATCT | 43.084349 | -70.818856 | 89.97 | 120.00 | 209.97 |

## 1-ATCT map image



## 6-ATCT map image



Obstruction Components


Name: BLDG2

| Vertex | Latitude | Longitude | Ground elevation |
| :--- | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ |
| 1 | 43.084955 | -70.806346 | 99.52 |
| 2 | 43.085031 | -70.806408 | 98.08 |
| 3 | 43.084866 | -70.806801 | 99.55 |
| 4 | 43.084555 | -70.806565 | 99.98 |
| 5 | 43.084608 | -70.806439 | 99.85 |
| 6 | 43.084444 | -70.806325 | 99.64 |
| 7 | 43.084592 | -70.806011 | 99.08 |
| 8 | 43.084965 | -70.806346 | 99.43 |


| Name: HighEdge1 <br> Upper edge height: 22.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.085534 | -70.803609 | 57.89 |
|  | 2 | 43.085267 | -70.803116 | 55.50 |
| Name: HighEdge2 <br> Upper edge height: 22.5 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
|  | 1 | 43.085593 | -70.803598 | 57.75 |
|  | 2 | 43.085019 | -70.804161 | 63.07 |


| Name: HighEdge3 <br> Upper edge height: 22.5 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.085424 | -70.803445 | 56.71 |
| d | 2 | 43.084960 | -70.803895 | 59.16 |
| Name: HighEdge4 <br> Upper edge height: 20.2 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| $12 \mathrm{mos}+1.06$ | 1 | 43.085307 | -70.803260 | 56.28 |
|  | 2 | 43.084860 | -70.803684 | 58.42 |
| Name: PRPT1 <br> Upper edge height: 93.2 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
|  | 1 | 43.084674 | -70.803390 | 58.96 |
|  | 2 | 43.084478 | -70.802983 | 56.11 |
|  | 3 | 43.084211 | -70.803240 | 59.29 |
|  | 4 | 43.084415 | -70.803648 | 62.46 |
|  | 5 | 43.084674 | -70.803390 | 58.96 |
| Name: PRPT2 <br> Upper edge height: 99.3 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
|  | 1 | 43.084580 | -70.802457 | 53.31 |
|  | 2 | 43.083953 | -70.801212 | 46.09 |
|  | 3 | 43.083224 | -70.801856 | 52.36 |
|  | 4 | 43.083866 | -70.803165 | 61.10 |
|  | 5 | 43.084580 | -70.802457 | 53.31 |


| Name: TREELINE <br> Upper edge height: 35.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.085164 | -70.808848 | 82.83 |
|  | 2 | 43.085454 | -70.807942 | 81.22 |
| - | 3 | 43.085373 | -70.807765 | 82.86 |
|  | 4 | 43.085040 | -70.807564 | 86.97 |
| Name: Trees <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.083891 | -70.811509 | 72.86 |
|  | 2 | 43.084095 | -70.811240 | 67.62 |
| Name: Trees <br> Upper edge height: 17.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085036 | -70.807176 | 92.20 |
|  | 2 | 43.084131 | -70.806567 | 95.41 |
| Name: Trees1 <br> Upper edge height: 40.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
|  | 1 | 43.085261 | -70.816979 | 84.00 |
|  | 2 | 43.084955 | -70.816877 | 84.48 |
|  | 3 | 43.084477 | -70.817247 | 78.24 |


| Name: Trees2 |
| :--- |
| Upper edge height: 60.0 ft |



## Summary of PV Glare Analysis

PV configuration and total predicted glare

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced | Data File |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | min | min | kWh |  |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT3 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT4 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - | - |
| LGBLDG | 10.0 | 214.0 | 0 | 0 | - | - |
| SMBLDG | 10.0 | 214.0 | 0 | 0 | - | - |

## PV \& Receptor Analysis Results

Results for each PV array and receptor
CRPRT1 no glare found

| Component | Green glare (min) |
| :--- | :---: | Yellow glare (min)

No glare found

CRPRT2 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: $6-$ ATCT | 0 | 0 |

CRPRT3 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |

No glare found

CRPRT4 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |

No glare found

CRPRT5 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |

[^0]LGBLDG no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |

No glare found

SMBLDG no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |

No glare found

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, nc discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.


# ALBACORE, Portsmouth, NH <br> ALBCR_15Tilt_124Carports_NOObstrctns_2ATCT_AddOP 

Client: Lonza
Created Feb 22, 2024
Updated Feb 22, 2024
Time-step 1 minute
Timezone offset UTC-5
Minimum sun altitude 0.0 deg
Site ID 112714.19298
Project type Advanced
Project status: active
Category 1 MW to 5 MW


Misc. Analysis Settings

PV Analysis Methodology: Version 2
Enhanced subtended angle calculation: On

Summary of Results Glare with low potential for temporary after-image predicted

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{d e g}$ | $\mathbf{d e g}$ | $\mathbf{m i n}$ | $\mathbf{m i n}$ | $\mathbf{k W h}$ |
| CRPRT1 | 0.0 | 124.0 | 1,543 | 0 | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT3 | 0.0 | 124.0 | 1,314 | 0 | - |
| CRPRT4 | 0.0 | 124.0 | 1,617 | 0 | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - |
| LGBLDG | 15.0 | 214.0 | 0 | 0 | - |
| SMBLDG | 15.0 | 214.0 | 0 | 0 | - |

## Component Data

## PV Array(s)

Total PV footprint area: 3.1 acres

| Name: CRPRT1 <br> Footprint area: 0.20 acre | Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Axis tracking: Fixed (no rotation) Tilt: 0.0 deg <br> Orientation: 124.0 deg |  | deg | $\operatorname{deg}$ | ft | ft | ft |
| Rated power: - | 1 | 43.085650 | -70.803723 | 57.92 | 20.17 | 78.09 |
| Panel material: Smooth glass with AR coating | 2 | 43.085595 | -70.803619 | 57.81 | 14.00 | 71.81 |
| Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes | 3 | 43.085032 | -70.804187 | 64.54 | 14.00 | 78.54 |
| Slope error: 8.43 mrad | 4 | 43.085084 | -70.804291 | 66.68 | 20.17 | 86.85 |



Name: CRPRT2
Footprint area: 0.26 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085519 | -70.803626 | 57.88 | 22.48 | 80.36 |
| 2 | 43.085431 | -70.803461 | 56.75 | 14.00 | 70.75 |
| 3 | 43.084981 | -70.803912 | 58.98 | 14.00 | 72.98 |
| 4 | 43.085070 | -70.804083 | 59.73 | 22.48 | 82.20 |



Name: CRPRT3
Footprint area: 0.23 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 124.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes
Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085400 | -70.803418 | 56.90 | 22.48 | 79.38 |
| 2 | 43.085325 | -70.803271 | 56.23 | 14.00 | 70.23 |
| 3 | 43.084876 | -70.803716 | 58.56 | 14.00 | 72.56 |
| 4 | 43.084953 | -70.803866 | 59.01 | 22.48 | 81.49 |



Name: CRPRT4
Footprint area: 0.13 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085298 | -70.803223 | 56.02 | 20.17 | 76.19 |
| 2 | 43.085253 | -70.803139 | 56.21 | 14.00 | 70.21 |
| 3 | 43.084808 | -70.803572 | 58.45 | 14.00 | 72.45 |
| 4 | 43.084851 | -70.803658 | 58.35 | 20.17 | 78.52 |



Name: CRPRT5
Footprint area: 0.07 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085549 | -70.803405 | 56.86 | 20.17 | 77.02 |
| 2 | 43.085404 | -70.803116 | 55.16 | 20.17 | 75.32 |
| 3 | 43.085334 | -70.803188 | 55.25 | 14.00 | 69.25 |
| 4 | 43.085478 | -70.803470 | 57.01 | 14.00 | 71.01 |



Name: LGBLDG
Footprint area: 2.0 acres
Axis tracking: Fixed (no rotation)
Tilt: 15.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.084344 | -70.802133 | 51.60 | 93.83 | 145.44 |
| 2 | 43.084054 | -70.801543 | 49.18 | 93.83 | 143.01 |
| 3 | 43.083901 | -70.801690 | 49.39 | 93.83 | 143.22 |
| 4 | 43.083859 | -70.801609 | 49.20 | 93.83 | 143.03 |
| 5 | 43.083897 | -70.801574 | 49.27 | 93.83 | 143.10 |
| 6 | 43.083839 | -70.801453 | 47.35 | 93.83 | 141.18 |
| 7 | 43.083345 | -70.801919 | 51.93 | 93.83 | 145.76 |
| 8 | 43.083906 | -70.803019 | 59.40 | 93.83 | 153.23 |
| 10 | 43.084395 | -70.802537 | 54.24 | 93.83 | 148.07 |
| 11 | 43.084315 | -70.802368 | 51.53 | 93.83 | 145.36 |
| 12 | 43.084337 | -70.802347 | 51.04 | 93.83 | 144.87 |
| 13 | 43.084303 | -70.802278 | 52.48 | 93.83 | 146.31 |
| 14 | 43.084336 | -70.802245 | 52.51 | 93.83 | 146.34 |
|  |  |  | 51.69 |  | 145.52 |


| Name: SMBLDG <br> Footprint area: 0.22 acre <br> Axis tracking: Fixed (no rotation) <br> Tilt: 15.0 deg <br> Orientation: 214.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rated power: - | 1 | 43.084480 | -70.803051 | 56.19 | 88.00 | 144.19 |
| Panel material: Smooth glass with AR coating | 2 | 43.084450 | -70.803081 | 56.31 | 88.00 | 144.31 |
| Vary reflectivity with sun position? Yes | 3 | 43.084506 | -70.803193 | 56.74 | 88.00 | 144.74 |
| Slope error: 8.43 mrad | 4 | 43.084466 | -70.803232 | 56.81 | 88.00 | 144.81 |
|  | 5 | 43.084412 | -70.803118 | 56.55 | 88.00 | 144.55 |
| - | 6 | 43.084252 | -70.803275 | 58.91 | 88.00 | 146.91 |
|  | 7 | 43.084414 | -70.803594 | 61.58 | 88.00 | 149.58 |
|  | 8 | 43.084643 | -70.803375 | 58.79 | 88.00 | 146.79 |

Route Receptor(s)

| Name: Route 1 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.082607 | -70.800659 | 43.16 | 4.50 | 47.66 |
|  | 2 | 43.082965 | -70.800254 | 39.75 | 4.50 | 44.25 |
|  | 3 | 43.084118 | -70.798835 | 40.69 | 4.50 | 45.19 |
| Name: Route 2 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.084096 | -70.798795 | 40.76 | 8.50 | 49.26 |
|  | 2 | 43.082949 | -70.800223 | 39.72 | 8.50 | 48.22 |
|  | 3 | 43.082597 | -70.800616 | 42.88 | 8.50 | 51.38 |
| Name: Route 3 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| \% | 1 | 43.085442 | -70.804811 | 63.97 | 4.50 | 68.47 |
|  | 2 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
| bxic | 3 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
|  | 4 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
| $8$ | 5 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
|  | 6 | 43.084394 | -70.804068 | 68.75 | 4.50 | 73.25 |
|  | 7 | 43.083881 | -70.803489 | 64.40 | 4.50 | 68.90 |
|  | 8 | 43.083614 | -70.803103 | 60.85 | 4.50 | 65.35 |
| Name: Route 4 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude deg | Longitude deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.083602 | -70.803135 | 60.76 | 8.50 | 69.26 |
|  | 2 | 43.083841 | -70.803542 | 64.38 | 8.50 | 72.88 |
|  | 3 | 43.084382 | -70.804111 | 68.76 | 8.50 | 77.26 |
|  | 4 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 5 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 6 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 7 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 8 | 43.085416 | -70.804830 | 64.17 | 8.50 | 72.67 |


| Name: Route 5 <br> Route type Two-way <br> View angle: 50.0 deg |
| :--- |

## Discrete Observation Receptors

| Number | Latitude | Longitude | Ground elevation | Height above ground | Total Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | ft | ft | ft |
| 1-ATCT | 43.084384 | -70.818882 | 89.93 | 130.00 | 219.93 |
| OP 2 | 43.082455 | -70.800057 | 42.02 | 20.00 | 62.02 |
| OP 3 | 43.082529 | -70.799934 | 41.99 | 30.00 | 71.99 |
| OP 4 | 43.083085 | -70.799471 | 39.01 | 6.00 | 45.01 |
| OP 5 | 43.083191 | -70.799294 | 38.75 | 15.00 | 53.75 |
| 6-ATCT | 43.084349 | -70.818856 | 89.97 | 120.00 | 209.97 |
| OP 7 | 43.083312 | -70.803940 | 70.10 | 40.00 | 110.10 |

## 1-ATCT map image



## 6-ATCT map image



Obstruction Components

| Name: HighEdge1 <br> Upper edge height: 22.0 ft | Vertex | Latitude | Longitude | Ground elevation |
| :---: | :---: | :---: | :---: | :---: |
|  |  | deg | deg | ft |
|  | 1 | 43.085534 | -70.803609 | 57.89 |
|  | 2 | 43.085267 | -70.803116 | 55.50 |




| Name: PRPT1 <br> Upper edge height: 93.2 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
| - | 1 | 43.084674 | -70.803390 | 58.96 |
|  | 2 | 43.084478 | -70.802983 | 56.11 |
|  | 3 | 43.084211 | -70.803240 | 59.29 |
|  | 4 | 43.084415 | -70.803648 | 62.46 |
|  | 5 | 43.084674 | -70.803390 | 58.96 |
| Name: PRPT2 <br> Upper edge height: 99.3 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
| 8 | 1 | 43.084580 | -70.802457 | 53.31 |
|  | 2 | 43.083953 | -70.801212 | 46.09 |
|  | 3 | 43.083224 | -70.801856 | 52.36 |
|  | 4 | 43.083866 | -70.803165 | 61.10 |
|  | 5 | 43.084580 | -70.802457 | 53.31 |

## Summary of PV Glare Analysis

PV configuration and total predicted glare

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced | Data File |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | min | min | kWh |  |
| CRPRT1 | 0.0 | 124.0 | 1,543 | 0 | - | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT3 | 0.0 | 124.0 | 1,314 | 0 | - | - |
| CRPRT4 | 0.0 | 124.0 | 1,617 | 0 | - | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - | - |
| LGBLDG | 15.0 | 214.0 | 0 | 0 | - | - |
| SMBLDG | 15.0 | 214.0 | 0 | 0 | - | - |

## Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

| PV | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| crprt1 (green) | 0 | 0 | 105 | 292 | 0 | 0 | 0 | 81 | 319 | 0 | 0 |  |
| crprt1 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| crprt3 (green) | 0 | 88 | 142 | 137 | 0 | 0 | 0 | 1 | 281 | 86 | 0 | 0 |
| crprt3 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| crprt4 (green) | 0 | 139 | 219 | 103 | 0 | 0 | 0 | 0 | 273 | 187 | 0 | 0 |
| crprt4 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## PV \& Receptor Analysis Results

Results for each PV array and receptor
CRPRT1 low potential for temporary after-image

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 783 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 760 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

PV array is expected to produce the following glare for this receptor:

- 783 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.




## CRPRT1: OP 2

No glare found

## CRPRT1: OP 3

No glare found

## CRPRT1: OP 4

No glare found

## CRPRT1: OP 5

No glare found

PV array is expected to produce the following glare for this receptor:

- 760 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


Sampled Annual Glare Reflections on PV Footprint


CRPRT1: OP 7
No glare found

## CRPRT1: Route 1

No glare found

## CRPRT1: Route 2

No glare found

## CRPRT1: Route 3

No glare found

## CRPRT1: Route 4

No glare found

## CRPRT1: Route 5

No glare found

## CRPRT1: Route 6

No glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

CRPRT3 low potential for temporary after-image

| Component | Green glare (min) |
| :--- | :---: |
| OP: 1-ATCT | 548 |
| OP: OP 2 | 0 |
| Yellow glare (min) |  |
| OP: OP 3 OP 4 | 0 |
| OP: OP 5 | 0 |
| OP: 6-ATCT | 0 |
| OP: OP 7 | 530 |
| Route: Route 1 | 0 |
| Route: Route 2 | 0 |
| Route: Route 3 | 0 |
| Route: Route 4 | 78 |
| Route: Route 5 | 158 |
| Route: Route 6 | 0 |

PV array is expected to produce the following glare for this receptor:

- 548 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.



CRPRT3: OP 2
No glare found

## CRPRT3: OP 3

No glare found

CRPRT3: OP 4
No glare found

CRPRT3: OP 5
No glare found

PV array is expected to produce the following glare for this receptor:

- 530 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


CRPRT3: OP 7
No glare found

## CRPRT3: Route 1

No glare found

## CRPRT3: Route 2

No glare found

## CRPRT3: Route 3

PV array is expected to produce the following glare for this receptor:

- 78 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


## CRPRT3: Route 4

PV array is expected to produce the following glare for this receptor:

- 158 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.








## CRPRT3: Route 5

No glare found

CRPRT3: Route 6
No glare found

CRPRT4 low potential for temporary after-image

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :---: | :---: |
| OP: 1-ATCT | 532 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 514 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 314 | 0 |
| Route: Route 4 | 257 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

## CRPRT4: 1-ATCT

PV array is expected to produce the following glare for this receptor:

- 532 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.



## CRPRT4: OP 2

No glare found

CRPRT4: OP 3
No glare found

## CRPRT4: OP 4

No glare found

## CRPRT4: OP 5

No glare found

## CRPRT4: 6-ATCT

PV array is expected to produce the following glare for this receptor:

- 514 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.



CRPRT4: OP 7
No glare found

## CRPRT4: Route 1

No glare found

## CRPRT4: Route 2

No glare found

## CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 314 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


## CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 257 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.








## CRPRT4: Route 5

No glare found

## CRPRT4: Route 6

No glare found

CRPRT5 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

LGBLDG no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |


| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, nc discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.


# ALBACORE, Portsmouth, NH ALBCR_10Tilt_124Carports_Obstrctns_2ATCT_AddOP 

Client: Lonza
Created Feb 22, 2024
Updated Feb 22, 2024
Time-step 1 minute
Timezone offset UTC-5
Minimum sun altitude 0.0 deg
Site ID 112715.19298
Project type Advanced
Project status: active
Category 1 MW to 5 MW


Misc. Analysis Settings

PV Analysis Methodology: Version 2
Enhanced subtended angle calculation: On

Summary of Results № glare predicted!

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\boldsymbol{m i n}$ | $\mathbf{m i n}$ | $\mathbf{k W h}$ |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT3 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT4 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - |
| LGBLDG | 10.0 | 214.0 | 0 | 0 | - |
| SMBLDG | 10.0 | 214.0 | 0 | 0 | - |

## Component Data

## PV Array(s)

Total PV footprint area: 3.1 acres

| Name: CRPRT1 <br> Footprint area: 0.20 acre | Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Axis tracking: Fixed (no rotation) Tilt: 0.0 deg <br> Orientation: 124.0 deg |  | deg | $\operatorname{deg}$ | ft | ft | ft |
| Rated power: - | 1 | 43.085650 | -70.803723 | 57.92 | 20.17 | 78.09 |
| Panel material: Smooth glass with AR coating | 2 | 43.085595 | -70.803619 | 57.81 | 14.00 | 71.81 |
| Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes | 3 | 43.085032 | -70.804187 | 64.54 | 14.00 | 78.54 |
| Slope error: 8.43 mrad | 4 | 43.085084 | -70.804291 | 66.68 | 20.17 | 86.85 |



Name: CRPRT2
Footprint area: 0.26 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085519 | -70.803626 | 57.88 | 22.48 | 80.36 |
| 2 | 43.085431 | -70.803461 | 56.75 | 14.00 | 70.75 |
| 3 | 43.084981 | -70.803912 | 58.98 | 14.00 | 72.98 |
| 4 | 43.085070 | -70.804083 | 59.73 | 22.48 | 82.20 |



Name: CRPRT3
Footprint area: 0.23 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 124.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes
Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085400 | -70.803418 | 56.90 | 22.48 | 79.38 |
| 2 | 43.085325 | -70.803271 | 56.23 | 14.00 | 70.23 |
| 3 | 43.084876 | -70.803716 | 58.56 | 14.00 | 72.56 |
| 4 | 43.084953 | -70.803866 | 59.01 | 22.48 | 81.49 |



Name: CRPRT4
Footprint area: 0.13 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085298 | -70.803223 | 56.02 | 20.17 | 76.19 |
| 2 | 43.085253 | -70.803139 | 56.21 | 14.00 | 70.21 |
| 3 | 43.084808 | -70.803572 | 58.45 | 14.00 | 72.45 |
| 4 | 43.084851 | -70.803658 | 58.35 | 20.17 | 78.52 |



Name: CRPRT5
Footprint area: 0.07 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085549 | -70.803405 | 56.86 | 20.17 | 77.02 |
| 2 | 43.085404 | -70.803116 | 55.16 | 20.17 | 75.32 |
| 3 | 43.085334 | -70.803188 | 55.25 | 14.00 | 69.25 |
| 4 | 43.085478 | -70.803470 | 57.01 | 14.00 | 71.01 |



Name: LGBLDG
Footprint area: 2.0 acres
Axis tracking: Fixed (no rotation)
Tilt: 10.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.084344 | -70.802133 | 51.60 | 93.83 | 145.44 |
| 2 | 43.084054 | -70.801543 | 49.18 | 93.83 | 143.01 |
| 3 | 43.083901 | -70.801690 | 49.39 | 93.83 | 143.22 |
| 4 | 43.083859 | -70.801609 | 49.20 | 93.83 | 143.03 |
| 5 | 43.083897 | -70.801574 | 49.27 | 93.83 | 143.10 |
| 6 | 43.083839 | -70.801453 | 47.35 | 93.83 | 141.18 |
| 7 | 43.083345 | -70.801919 | 51.93 | 93.83 | 145.76 |
| 8 | 43.083906 | -70.803019 | 59.40 | 93.83 | 153.23 |
| 10 | 43.084395 | -70.802537 | 54.24 | 93.83 | 148.07 |
| 11 | 43.084315 | -70.802368 | 51.53 | 93.83 | 145.36 |
| 12 | 43.084337 | -70.802347 | 51.04 | 93.83 | 144.87 |
| 13 | 43.084303 | -70.802278 | 52.48 | 93.83 | 146.31 |
| 14 | 43.084336 | -70.802245 | 52.51 | 93.83 | 146.34 |
|  |  |  | 51.69 |  | 145.52 |


| Name: SMBLDG <br> Footprint area: 0.22 acre <br> Axis tracking: Fixed (no rotation) <br> Tilt: 10.0 deg <br> Orientation: 214.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rated power: - | 1 | 43.084480 | -70.803051 | 56.19 | 88.00 | 144.19 |
| Panel material: Smooth glass with AR coating | 2 | 43.084450 | -70.803081 | 56.31 | 88.00 | 144.31 |
| Vary reflectivity with sun position? Yes | 3 | 43.084506 | -70.803193 | 56.74 | 88.00 | 144.74 |
| Slope error: 8.43 mrad | 4 | 43.084466 | -70.803232 | 56.81 | 88.00 | 144.81 |
|  | 5 | 43.084412 | -70.803118 | 56.55 | 88.00 | 144.55 |
| - | 6 | 43.084252 | -70.803275 | 58.91 | 88.00 | 146.91 |
|  | 7 | 43.084414 | -70.803594 | 61.58 | 88.00 | 149.58 |
|  | 8 | 43.084643 | -70.803375 | 58.79 | 88.00 | 146.79 |

Route Receptor(s)

| Name: Route 1 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.082607 | -70.800659 | 43.16 | 4.50 | 47.66 |
|  | 2 | 43.082965 | -70.800254 | 39.75 | 4.50 | 44.25 |
|  | 3 | 43.084118 | -70.798835 | 40.69 | 4.50 | 45.19 |
| Name: Route 2 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.084096 | -70.798795 | 40.76 | 8.50 | 49.26 |
|  | 2 | 43.082949 | -70.800223 | 39.72 | 8.50 | 48.22 |
|  | 3 | 43.082597 | -70.800616 | 42.88 | 8.50 | 51.38 |
| Name: Route 3 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| \% | 1 | 43.085442 | -70.804811 | 63.97 | 4.50 | 68.47 |
|  | 2 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
| bxic | 3 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
|  | 4 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
| $8$ | 5 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
|  | 6 | 43.084394 | -70.804068 | 68.75 | 4.50 | 73.25 |
|  | 7 | 43.083881 | -70.803489 | 64.40 | 4.50 | 68.90 |
|  | 8 | 43.083614 | -70.803103 | 60.85 | 4.50 | 65.35 |
| Name: Route 4 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude deg | Longitude deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.083602 | -70.803135 | 60.76 | 8.50 | 69.26 |
|  | 2 | 43.083841 | -70.803542 | 64.38 | 8.50 | 72.88 |
|  | 3 | 43.084382 | -70.804111 | 68.76 | 8.50 | 77.26 |
|  | 4 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 5 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 6 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 7 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 8 | 43.085416 | -70.804830 | 64.17 | 8.50 | 72.67 |


| Name: Route 5 <br> Route type Two-way <br> View angle: 50.0 deg |
| :--- |

## Discrete Observation Receptors

| Number | Latitude | Longitude | Ground elevation | Height above ground | Total Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | ft | ft | ft |
| 1-ATCT | 43.084384 | -70.818882 | 89.93 | 130.00 | 219.93 |
| OP 2 | 43.082455 | -70.800057 | 42.02 | 20.00 | 62.02 |
| OP 3 | 43.082529 | -70.799934 | 41.99 | 30.00 | 71.99 |
| OP 4 | 43.083085 | -70.799471 | 39.01 | 6.00 | 45.01 |
| OP 5 | 43.083191 | -70.799294 | 38.75 | 15.00 | 53.75 |
| 6-ATCT | 43.084349 | -70.818856 | 89.97 | 120.00 | 209.97 |
| OP 7 | 43.083343 | -70.803962 | 70.10 | 40.00 | 110.10 |

## 1-ATCT map image



6-ATCT map image


## Obstruction Components

| Name: BLDG2 <br> Upper edge height: 20.0 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.084955 | -70.806346 | 99.52 |
|  | 2 | 43.085031 | -70.806408 | 98.08 |
|  | 3 | 43.084866 | -70.806801 | 99.55 |
|  | 4 | 43.084555 | -70.806565 | 99.98 |
|  | 5 | 43.084608 | -70.806439 | 99.85 |
|  | 6 | 43.084444 | -70.806325 | 99.64 |
|  | 7 | 43.084592 | -70.806011 | 99.08 |
|  | 8 | 43.084965 | -70.806346 | 99.43 |



| Name: HighEdge4 <br> Upper edge height: 20.2 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
| 1 m | 1 | 43.085307 | -70.803260 | 56.28 |
| - $1 . \sim 2$ | 2 | 43.084860 | -70.803684 | 58.42 |
| Name: PLANTING <br> Upper edge height: 9.0 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
|  | 1 | 43.085446 | -70.804721 | 64.24 |
|  | 2 | 43.084717 | -70.804268 | 69.47 |
|  | 3 | 43.084592 | -70.804158 | 69.46 |
| Name: PRPT1 <br> Upper edge height: 93.2 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
|  | 1 | 43.084674 | -70.803390 | 58.96 |
|  | 2 | 43.084478 | -70.802983 | 56.11 |
|  | 3 | 43.084211 | -70.803240 | 59.29 |
|  | 4 | 43.084415 | -70.803648 | 62.46 |
|  | 5 | 43.084674 | -70.803390 | 58.96 |
| Name: PRPT2 <br> Upper edge height: 99.3 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
|  | 1 | 43.084580 | -70.802457 | 53.31 |
| (8) | 2 | 43.083953 | -70.801212 | 46.09 |
|  | 3 | 43.083224 | -70.801856 | 52.36 |
|  | 4 | 43.083866 | -70.803165 | 61.10 |
|  | 5 | 43.084580 | -70.802457 | 53.31 |


| Name: TREELINE <br> Upper edge height: 35.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.085164 | -70.808848 | 82.83 |
|  | 2 | 43.085454 | -70.807942 | 81.22 |
|  | 3 | 43.085373 | -70.807765 | 82.86 |
|  | 4 | 43.085040 | -70.807564 | 86.97 |
| Name: Trees <br> Upper edge height: 17.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085036 | -70.807176 | 92.20 |
|  | 2 | 43.084131 | -70.806567 | 95.41 |
| Name: Trees <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.083891 | -70.811509 | 72.86 |
|  | 2 | 43.084095 | -70.811240 | 67.62 |
| Name: Trees1 <br> Upper edge height: 40.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
| + | 1 | 43.085261 | -70.816979 | 84.00 |
|  | 2 | 43.084955 | -70.816877 | 84.48 |
|  | 3 | 43.084477 | -70.817247 | 78.24 |


| Name: Trees2 |
| :--- |
| Upper edge height: 60.0 ft |



## Summary of PV Glare Analysis

PV configuration and total predicted glare

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced | Data File |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | min | min | kWh |  |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT3 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT4 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - | - |
| LGBLDG | 10.0 | 214.0 | 0 | 0 | - | - |
| SMBLDG | 10.0 | 214.0 | 0 | 0 | - | - |

## PV \& Receptor Analysis Results

Results for each PV array and receptor
CRPRT1 no glare found

| Component | Green glare (min) |
| :--- | :---: |
| OP: 1-ATCT | 0 |
| Yellow glare (min) |  |
| OP: OP 2 | 0 |
| OP: OP 3 | 0 |
| OP: OP 4 | 0 |
| OP: OP 5 | 0 |
| OP: 6-ATCT | 0 |
| OP: OP 7 | 0 |
| Route: Route 1 | 0 |
| Route: Route 2 | 0 |
| Route: Route 3 | 0 |

No glare found

CRPRT2 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

CRPRT3 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

CRPRT4 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

CRPRT5 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

LGBLDG no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

SMBLDG no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, nc discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.


## ALBACORE, Portsmouth, NH

ALBCR_5Tilt_124Carports_Obstrctns_2ATCT_NoPlant
Client: Lonza
Created Feb 22, 2024
Updated Feb 22, 2024
Time-step 1 minute
Timezone offset UTC-5
Minimum sun altitude 0.0 deg
Site ID 112718.19298
Project type Advanced
Project status: active
Category 1 MW to 5 MW


Misc. Analysis Settings

PV Analysis Methodology: Version 2
Enhanced subtended angle calculation: On

Summary of Results Glare with low potential for temporary after-image predicted

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{d e g}$ | $\mathbf{d e g}$ | $\boldsymbol{m i n}$ | $\mathbf{m i n}$ | $\mathbf{k W h}$ |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT3 | 0.0 | 124.0 | 236 | 0 | - |
| CRPRT4 | 0.0 | 124.0 | 566 | 0 | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - |
| LGBLDG | 5.0 | 214.0 | 0 | 0 | - |
| SMBLDG | 5.0 | 214.0 | 0 | 0 | - |

## Component Data

## PV Array(s)

Total PV footprint area: 3.1 acres

| Name: CRPRT1 <br> Footprint area: 0.20 acre | Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Axis tracking: Fixed (no rotation) Tilt: 0.0 deg <br> Orientation: 124.0 deg |  | deg | $\operatorname{deg}$ | ft | ft | ft |
| Rated power: - | 1 | 43.085650 | -70.803723 | 57.92 | 20.17 | 78.09 |
| Panel material: Smooth glass with AR coating | 2 | 43.085595 | -70.803619 | 57.81 | 14.00 | 71.81 |
| Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes | 3 | 43.085032 | -70.804187 | 64.54 | 14.00 | 78.54 |
| Slope error: 8.43 mrad | 4 | 43.085084 | -70.804291 | 66.68 | 20.17 | 86.85 |



Name: CRPRT2
Footprint area: 0.26 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085519 | -70.803626 | 57.88 | 22.48 | 80.36 |
| 2 | 43.085431 | -70.803461 | 56.75 | 14.00 | 70.75 |
| 3 | 43.084981 | -70.803912 | 58.98 | 14.00 | 72.98 |
| 4 | 43.085070 | -70.804083 | 59.73 | 22.48 | 82.20 |



Name: CRPRT3
Footprint area: 0.23 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 124.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes
Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085400 | -70.803418 | 56.90 | 22.48 | 79.38 |
| 2 | 43.085325 | -70.803271 | 56.23 | 14.00 | 70.23 |
| 3 | 43.084876 | -70.803716 | 58.56 | 14.00 | 72.56 |
| 4 | 43.084953 | -70.803866 | 59.01 | 22.48 | 81.49 |



Name: CRPRT4
Footprint area: 0.13 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085298 | -70.803223 | 56.02 | 20.17 | 76.19 |
| 2 | 43.085253 | -70.803139 | 56.21 | 14.00 | 70.21 |
| 3 | 43.084808 | -70.803572 | 58.45 | 14.00 | 72.45 |
| 4 | 43.084851 | -70.803658 | 58.35 | 20.17 | 78.52 |



Name: CRPRT5
Footprint area: 0.07 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085549 | -70.803405 | 56.86 | 20.17 | 77.02 |
| 2 | 43.085404 | -70.803116 | 55.16 | 20.17 | 75.32 |
| 3 | 43.085334 | -70.803188 | 55.25 | 14.00 | 69.25 |
| 4 | 43.085478 | -70.803470 | 57.01 | 14.00 | 71.01 |



Name: LGBLDG
Footprint area: 2.0 acres
Axis tracking: Fixed (no rotation)
Tilt: 5.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.084344 | -70.802133 | 51.60 | 93.83 | 145.44 |
| 2 | 43.084054 | -70.801543 | 49.18 | 93.83 | 143.01 |
| 3 | 43.083901 | -70.801690 | 49.39 | 93.83 | 143.22 |
| 4 | 43.083859 | -70.801609 | 49.20 | 93.83 | 143.03 |
| 5 | 43.083897 | -70.801574 | 49.27 | 93.83 | 143.10 |
| 6 | 43.083839 | -70.801453 | 47.35 | 93.83 | 141.18 |
| 7 | 43.083345 | -70.801919 | 51.93 | 93.83 | 145.76 |
| 8 | 43.083906 | -70.803019 | 59.40 | 93.83 | 153.23 |
| 10 | 43.084395 | -70.802537 | 54.24 | 93.83 | 148.07 |
| 11 | 43.084315 | -70.802368 | 51.53 | 93.83 | 145.36 |
| 12 | 43.084337 | -70.802347 | 51.04 | 93.83 | 144.87 |
| 13 | 43.084303 | -70.802278 | 52.48 | 93.83 | 146.31 |
| 14 | 43.084336 | -70.802245 | 52.51 | 93.83 | 146.34 |
|  |  |  | 51.69 |  | 145.52 |


| Name: SMBLDG <br> Footprint area: 0.22 acre <br> Axis tracking: Fixed (no rotation) <br> Tilt: 5.0 deg <br> Orientation: 214.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rated power: - | 1 | 43.084480 | -70.803051 | 56.19 | 88.00 | 144.19 |
| Panel material: Smooth glass with AR coating | 2 | 43.084450 | -70.803081 | 56.31 | 88.00 | 144.31 |
| Vary reflectivity with sun position? Yes | 3 | 43.084506 | -70.803193 | 56.74 | 88.00 | 144.74 |
| Slope error: 8.43 mrad | 4 | 43.084466 | -70.803232 | 56.81 | 88.00 | 144.81 |
|  | 5 | 43.084412 | -70.803118 | 56.55 | 88.00 | 144.55 |
| - | 6 | 43.084252 | -70.803275 | 58.91 | 88.00 | 146.91 |
|  | 7 | 43.084414 | -70.803594 | 61.58 | 88.00 | 149.58 |
|  | 8 | 43.084643 | -70.803375 | 58.79 | 88.00 | 146.79 |

Route Receptor(s)

| Name: Route 1 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.082607 | -70.800659 | 43.16 | 4.50 | 47.66 |
|  | 2 | 43.082965 | -70.800254 | 39.75 | 4.50 | 44.25 |
|  | 3 | 43.084118 | -70.798835 | 40.69 | 4.50 | 45.19 |
| Name: Route 2 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.084096 | -70.798795 | 40.76 | 8.50 | 49.26 |
|  | 2 | 43.082949 | -70.800223 | 39.72 | 8.50 | 48.22 |
|  | 3 | 43.082597 | -70.800616 | 42.88 | 8.50 | 51.38 |
| Name: Route 3 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| \% | 1 | 43.085442 | -70.804811 | 63.97 | 4.50 | 68.47 |
|  | 2 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
| bxic | 3 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
|  | 4 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
| $8$ | 5 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
|  | 6 | 43.084394 | -70.804068 | 68.75 | 4.50 | 73.25 |
|  | 7 | 43.083881 | -70.803489 | 64.40 | 4.50 | 68.90 |
|  | 8 | 43.083614 | -70.803103 | 60.85 | 4.50 | 65.35 |
| Name: Route 4 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude deg | Longitude deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.083602 | -70.803135 | 60.76 | 8.50 | 69.26 |
|  | 2 | 43.083841 | -70.803542 | 64.38 | 8.50 | 72.88 |
|  | 3 | 43.084382 | -70.804111 | 68.76 | 8.50 | 77.26 |
|  | 4 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 5 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 6 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 7 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 8 | 43.085416 | -70.804830 | 64.17 | 8.50 | 72.67 |


| Name: Route 5 <br> Route type Two-way <br> View angle: 50.0 deg |
| :--- |

## Discrete Observation Receptors

| Number | Latitude | Longitude | Ground elevation | Height above ground | Total Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | ft | ft | ft |
| 1-ATCT | 43.084384 | -70.818882 | 89.93 | 130.00 | 219.93 |
| OP 2 | 43.082455 | -70.800057 | 42.02 | 20.00 | 62.02 |
| OP 3 | 43.082529 | -70.799934 | 41.99 | 30.00 | 71.99 |
| OP 4 | 43.083085 | -70.799471 | 39.01 | 6.00 | 45.01 |
| OP 5 | 43.083191 | -70.799294 | 38.75 | 15.00 | 53.75 |
| 6-ATCT | 43.084349 | -70.818856 | 89.97 | 120.00 | 209.97 |
| OP 7 | 43.083343 | -70.803962 | 70.10 | 40.00 | 110.10 |

## 1-ATCT map image



6-ATCT map image


## Obstruction Components

| Name: BLDG2 <br> Upper edge height: 20.0 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.084955 | -70.806346 | 99.52 |
|  | 2 | 43.085031 | -70.806408 | 98.08 |
|  | 3 | 43.084866 | -70.806801 | 99.55 |
|  | 4 | 43.084555 | -70.806565 | 99.98 |
|  | 5 | 43.084608 | -70.806439 | 99.85 |
|  | 6 | 43.084444 | -70.806325 | 99.64 |
|  | 7 | 43.084592 | -70.806011 | 99.08 |
|  | 8 | 43.084965 | -70.806346 | 99.43 |



| Name: HighEdge4 Upper edge height: 20.2 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.085307 | -70.803260 | 56.28 |
|  | 2 | 43.084860 | -70.803684 | 58.42 |
| Name: PRPT1 <br> Upper edge height: 93.2 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084674 | -70.803390 | 58.96 |
|  | 2 | 43.084478 | -70.802983 | 56.11 |
| - | 3 | 43.084211 | -70.803240 | 59.29 |
| - | 4 | 43.084415 | -70.803648 | 62.46 |
|  | 5 | 43.084674 | -70.803390 | 58.96 |
| Name: PRPT2 <br> Upper edge height: 99.3 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
| , , ¢-m yorir | 1 | 43.084580 | -70.802457 | 53.31 |
| - 2 - 1 | 2 | 43.083953 | -70.801212 | 46.09 |
|  | 3 | 43.083224 | -70.801856 | 52.36 |
|  | 4 | 43.083866 | -70.803165 | 61.10 |
| , $\times^{2}$ | 5 | 43.084580 | -70.802457 | 53.31 |
| Name: TREELINE <br> Upper edge height: 35.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085164 | -70.808848 | 82.83 |
|  | 2 | 43.085454 | -70.807942 | 81.22 |
|  | 3 | 43.085373 | -70.807765 | 82.86 |
|  | 4 | 43.085040 | -70.807564 | 86.97 |


| Name: Trees <br> Upper edge height: 17.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.085036 | -70.807176 | 92.20 |
|  | 2 | 43.084131 | -70.806567 | 95.41 |
| Name: Trees <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.083891 | -70.811509 | 72.86 |
|  | 2 | 43.084095 | -70.811240 | 67.62 |
| Name: Trees1 <br> Upper edge height: 40.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085261 | -70.816979 | 84.00 |
|  | 2 | 43.084955 | -70.816877 | 84.48 |
|  | 3 | 43.084477 | -70.817247 | 78.24 |
| Name: Trees2 <br> Upper edge height: 60.0 ft | Vertex | Latitude deg | Longitude deg | Ground elevation <br> ft |
|  | 1 | 43.084443 | -70.818109 | 84.34 |
|  | 2 | 43.084602 | -70.818167 | 84.74 |
|  | 3 | 43.084354 | -70.818474 | 88.75 |


| Name: Trees3 <br> Upper edge height: 100.0 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.084287 | -70.810576 | 72.89 |
|  | 2 | 43.084550 | -70.810195 | 75.28 |
| Name: Trees 4 <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085793 | -70.815175 | 77.90 |
|  | 2 | 43.085354 | -70.814585 | 81.00 |
|  | 3 | 43.086098 | -70.812858 | 77.64 |
| Name: Trees5 <br> Upper edge height: 45.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084411 | -70.807233 | 89.30 |
|  | 2 | 43.084554 | -70.807316 | 89.33 |
|  | 3 | 43.084677 | -70.807358 | 89.54 |
|  | 4 | 43.084730 | -70.807552 | 87.97 |
| Name: Trees6 <br> Upper edge height: 20.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085286 | -70.814633 | 80.07 |
|  | 2 | 43.083793 | -70.813418 | 79.96 |


| Name: Trees7 <br> Upper edge height: 30.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.083527 | -70.812571 | 74.50 |
|  | 2 | 43.083829 | -70.811932 | 72.49 |
| Name: WRHSE1 <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085129 | -70.813496 | 81.26 |
| Hasehy- | 2 | 43.085227 | -70.813254 | 81.50 |
|  | 3 | 43.085137 | -70.813085 | 81.35 |
| $13 \times$ | 4 | 43.084986 | -70.813064 | 81.23 |
|  | 5 | 43.084886 | -70.813292 | 81.62 |
|  | 6 | 43.085129 | -70.813496 | 81.26 |
| Name: WRHSE2Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084916 | -70.813107 | 81.43 |
|  | 2 | 43.084740 | -70.813499 | 81.62 |
|  | 3 | 43.084705 | -70.813466 | 81.64 |
|  | 4 | 43.084630 | -70.813662 | 81.71 |
|  | 5 | 43.084174 | -70.813292 | 81.76 |
|  | 6 | 43.084399 | -70.812785 | 81.68 |
|  | 7 | 43.084501 | -70.812860 | 81.70 |
|  | 8 | 43.084540 | -70.812758 | 81.66 |
|  | 9 | 43.084916 | -70.813107 | 81.43 |

## Summary of PV Glare Analysis

PV configuration and total predicted glare

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced | Data File |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | min | min | kWh |  |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT3 | 0.0 | 124.0 | 236 | 0 | - | - |
| CRPRT4 | 0.0 | 124.0 | 566 | 0 | - | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - | - |
| LGBLDG | 5.0 | 214.0 | 0 | 0 | - | - |
| SMBLDG | 5.0 | 214.0 | 0 | 0 | - | - |

## Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

| PV | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| crprt3 (green) | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 85 | 0 |  |
| crprt3 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| crprt4 (green) | 0 | 139 | 48 | 0 | 0 | 0 | 0 | 0 | 0 | 186 | 0 |  |
| crprt4 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## PV \& Receptor Analysis Results

Results for each PV array and receptor
CRPRT1 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

CRPRT2 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

CRPRT3 low potential for temporary after-image

| Component | Green glare (min) |
| :--- | :---: |
| OP: 1-ATCT | 0 |
| Yellow glare (min) |  |
| OP: OP 2 | 0 |
| OP: OP 3 | 0 |
| OP: OP 4 | 0 |
| OP: OP 5 | 0 |
| OP: 6-ATCT | 0 |
| OP: OP 7 | 0 |
| Route: Route 1 | 0 |
| Route: Route 2 | 0 |
| Route: Route 3 | 79 |
| Route: Route 4 | 157 |
| Route: Route 5 | 0 |
| Route: Route 6 | 0 |

## CRPRT3: 1-ATCT

No glare found

## CRPRT3: OP 2

No glare found

## CRPRT3: OP 3

No glare found

## CRPRT3: OP 4

No glare found

CRPRT3: OP 5
No glare found

## CRPRT3: 6-ATCT

No glare found

CRPRT3: OP 7
No glare found

## CRPRT3: Route 1

No glare found

## CRPRT3: Route 2

No glare found

## CRPRT3: Route 3

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.




## CRPRT3: Route 4

PV array is expected to produce the following glare for this receptor:

- 157 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


CRPRT3: Route 5
No glare found

## CRPRT3: Route 6

No glare found

CRPRT4 Iow potential for temporary after-image

| Component | Green glare (min) |
| :--- | :---: |
| OP: 1-ATCT | 0 |
| Yellow glare (min) |  |
| OP: OP 2 | 0 |
| OP: OP 3 | 0 |
| OP: OP 4 | 0 |
| OP: OP 5 | 0 |
| OP: 6-ATCT | 0 |
| OP: OP 7 | 0 |
| Route: Route 1 | 0 |
| Route: Route 2 | 0 |
| Route: Route 3 | 311 |

CRPRT4: 1-ATCT
No glare found

CRPRT4: OP 2
No glare found

CRPRT4: OP 3
No glare found

## CRPRT4: OP 4

No glare found

## CRPRT4: OP 5

No glare found

## CRPRT4: 6-ATCT

No glare found

## CRPRT4: OP 7

No glare found

## CRPRT4: Route 1

No glare found

CRPRT4: Route 2
No glare found

## CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


## CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.








## CRPRT4: Route 5

No glare found

## CRPRT4: Route 6

No glare found

CRPRT5 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

LGBLDG no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |


| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, nc discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.


# ALBACORE, Portsmouth, NH ALBCR_10Tilt_124Carports_Obstrctns_2ATCT_NoPlant 

Client: Lonza
Created Feb 22, 2024
Updated Feb 22, 2024
Time-step 1 minute
Timezone offset UTC-5
Minimum sun altitude 0.0 deg
Site ID 112717.19298
Project type Advanced
Project status: active
Category 1 MW to 5 MW


Misc. Analysis Settings

PV Analysis Methodology: Version 2
Enhanced subtended angle calculation: On

Summary of Results Glare with low potential for temporary after-image predicted

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{d e g}$ | $\mathbf{d e g}$ | $\mathbf{m i n}$ | $\mathbf{m i n}$ | $\mathbf{k W h}$ |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT3 | 0.0 | 124.0 | 236 | 0 | - |
| CRPRT4 | 0.0 | 124.0 | 566 | 0 | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - |
| LGBLDG | 10.0 | 214.0 | 0 | 0 | - |
| SMBLDG | 10.0 | 214.0 | 0 | 0 | - |

## Component Data

## PV Array(s)

Total PV footprint area: 3.1 acres

| Name: CRPRT1 <br> Footprint area: 0.20 acre | Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Axis tracking: Fixed (no rotation) Tilt: 0.0 deg <br> Orientation: 124.0 deg |  | deg | $\operatorname{deg}$ | ft | ft | ft |
| Rated power: - | 1 | 43.085650 | -70.803723 | 57.92 | 20.17 | 78.09 |
| Panel material: Smooth glass with AR coating | 2 | 43.085595 | -70.803619 | 57.81 | 14.00 | 71.81 |
| Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes | 3 | 43.085032 | -70.804187 | 64.54 | 14.00 | 78.54 |
| Slope error: 8.43 mrad | 4 | 43.085084 | -70.804291 | 66.68 | 20.17 | 86.85 |



Name: CRPRT2
Footprint area: 0.26 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085519 | -70.803626 | 57.88 | 22.48 | 80.36 |
| 2 | 43.085431 | -70.803461 | 56.75 | 14.00 | 70.75 |
| 3 | 43.084981 | -70.803912 | 58.98 | 14.00 | 72.98 |
| 4 | 43.085070 | -70.804083 | 59.73 | 22.48 | 82.20 |



Name: CRPRT3
Footprint area: 0.23 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 124.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes
Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085400 | -70.803418 | 56.90 | 22.48 | 79.38 |
| 2 | 43.085325 | -70.803271 | 56.23 | 14.00 | 70.23 |
| 3 | 43.084876 | -70.803716 | 58.56 | 14.00 | 72.56 |
| 4 | 43.084953 | -70.803866 | 59.01 | 22.48 | 81.49 |



Name: CRPRT4
Footprint area: 0.13 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085298 | -70.803223 | 56.02 | 20.17 | 76.19 |
| 2 | 43.085253 | -70.803139 | 56.21 | 14.00 | 70.21 |
| 3 | 43.084808 | -70.803572 | 58.45 | 14.00 | 72.45 |
| 4 | 43.084851 | -70.803658 | 58.35 | 20.17 | 78.52 |



Name: CRPRT5
Footprint area: 0.07 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085549 | -70.803405 | 56.86 | 20.17 | 77.02 |
| 2 | 43.085404 | -70.803116 | 55.16 | 20.17 | 75.32 |
| 3 | 43.085334 | -70.803188 | 55.25 | 14.00 | 69.25 |
| 4 | 43.085478 | -70.803470 | 57.01 | 14.00 | 71.01 |



Name: LGBLDG
Footprint area: 2.0 acres
Axis tracking: Fixed (no rotation)
Tilt: 10.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.084344 | -70.802133 | 51.60 | 93.83 | 145.44 |
| 2 | 43.084054 | -70.801543 | 49.18 | 93.83 | 143.01 |
| 3 | 43.083901 | -70.801690 | 49.39 | 93.83 | 143.22 |
| 4 | 43.083859 | -70.801609 | 49.20 | 93.83 | 143.03 |
| 5 | 43.083897 | -70.801574 | 49.27 | 93.83 | 143.10 |
| 6 | 43.083839 | -70.801453 | 47.35 | 93.83 | 141.18 |
| 7 | 43.083345 | -70.801919 | 51.93 | 93.83 | 145.76 |
| 8 | 43.083906 | -70.803019 | 59.40 | 93.83 | 153.23 |
| 10 | 43.084395 | -70.802537 | 54.24 | 93.83 | 148.07 |
| 11 | 43.084315 | -70.802368 | 51.53 | 93.83 | 145.36 |
| 12 | 43.084337 | -70.802347 | 51.04 | 93.83 | 144.87 |
| 13 | 43.084303 | -70.802278 | 52.48 | 93.83 | 146.31 |
| 14 | 43.084336 | -70.802245 | 52.51 | 93.83 | 146.34 |
|  |  |  | 51.69 |  | 145.52 |


| Name: SMBLDG <br> Footprint area: 0.22 acre <br> Axis tracking: Fixed (no rotation) <br> Tilt: 10.0 deg <br> Orientation: 214.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rated power: - | 1 | 43.084480 | -70.803051 | 56.19 | 88.00 | 144.19 |
| Panel material: Smooth glass with AR coating | 2 | 43.084450 | -70.803081 | 56.31 | 88.00 | 144.31 |
| Vary reflectivity with sun position? Yes | 3 | 43.084506 | -70.803193 | 56.74 | 88.00 | 144.74 |
| Slope error: 8.43 mrad | 4 | 43.084466 | -70.803232 | 56.81 | 88.00 | 144.81 |
|  | 5 | 43.084412 | -70.803118 | 56.55 | 88.00 | 144.55 |
| - | 6 | 43.084252 | -70.803275 | 58.91 | 88.00 | 146.91 |
|  | 7 | 43.084414 | -70.803594 | 61.58 | 88.00 | 149.58 |
|  | 8 | 43.084643 | -70.803375 | 58.79 | 88.00 | 146.79 |

Route Receptor(s)

| Name: Route 1 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.082607 | -70.800659 | 43.16 | 4.50 | 47.66 |
|  | 2 | 43.082965 | -70.800254 | 39.75 | 4.50 | 44.25 |
|  | 3 | 43.084118 | -70.798835 | 40.69 | 4.50 | 45.19 |
| Name: Route 2 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.084096 | -70.798795 | 40.76 | 8.50 | 49.26 |
|  | 2 | 43.082949 | -70.800223 | 39.72 | 8.50 | 48.22 |
|  | 3 | 43.082597 | -70.800616 | 42.88 | 8.50 | 51.38 |
| Name: Route 3 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| \% | 1 | 43.085442 | -70.804811 | 63.97 | 4.50 | 68.47 |
|  | 2 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
| bxic | 3 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
|  | 4 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
| $8$ | 5 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
|  | 6 | 43.084394 | -70.804068 | 68.75 | 4.50 | 73.25 |
|  | 7 | 43.083881 | -70.803489 | 64.40 | 4.50 | 68.90 |
|  | 8 | 43.083614 | -70.803103 | 60.85 | 4.50 | 65.35 |
| Name: Route 4 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude deg | Longitude deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.083602 | -70.803135 | 60.76 | 8.50 | 69.26 |
|  | 2 | 43.083841 | -70.803542 | 64.38 | 8.50 | 72.88 |
|  | 3 | 43.084382 | -70.804111 | 68.76 | 8.50 | 77.26 |
|  | 4 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 5 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 6 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 7 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 8 | 43.085416 | -70.804830 | 64.17 | 8.50 | 72.67 |


| Name: Route 5 <br> Route type Two-way <br> View angle: 50.0 deg |
| :--- |

## Discrete Observation Receptors

| Number | Latitude | Longitude | Ground elevation | Height above ground | Total Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | ft | ft | ft |
| 1-ATCT | 43.084384 | -70.818882 | 89.93 | 130.00 | 219.93 |
| OP 2 | 43.082455 | -70.800057 | 42.02 | 20.00 | 62.02 |
| OP 3 | 43.082529 | -70.799934 | 41.99 | 30.00 | 71.99 |
| OP 4 | 43.083085 | -70.799471 | 39.01 | 6.00 | 45.01 |
| OP 5 | 43.083191 | -70.799294 | 38.75 | 15.00 | 53.75 |
| 6-ATCT | 43.084349 | -70.818856 | 89.97 | 120.00 | 209.97 |
| OP 7 | 43.083343 | -70.803962 | 70.10 | 40.00 | 110.10 |

## 1-ATCT map image



6-ATCT map image


## Obstruction Components

| Name: BLDG2 <br> Upper edge height: 20.0 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.084955 | -70.806346 | 99.52 |
|  | 2 | 43.085031 | -70.806408 | 98.08 |
|  | 3 | 43.084866 | -70.806801 | 99.55 |
|  | 4 | 43.084555 | -70.806565 | 99.98 |
|  | 5 | 43.084608 | -70.806439 | 99.85 |
|  | 6 | 43.084444 | -70.806325 | 99.64 |
|  | 7 | 43.084592 | -70.806011 | 99.08 |
|  | 8 | 43.084965 | -70.806346 | 99.43 |



| Name: HighEdge4 Upper edge height: 20.2 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.085307 | -70.803260 | 56.28 |
|  | 2 | 43.084860 | -70.803684 | 58.42 |
| Name: PRPT1 <br> Upper edge height: 93.2 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084674 | -70.803390 | 58.96 |
|  | 2 | 43.084478 | -70.802983 | 56.11 |
| - | 3 | 43.084211 | -70.803240 | 59.29 |
| - | 4 | 43.084415 | -70.803648 | 62.46 |
|  | 5 | 43.084674 | -70.803390 | 58.96 |
| Name: PRPT2 <br> Upper edge height: 99.3 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
| , , ¢-m yorir | 1 | 43.084580 | -70.802457 | 53.31 |
| - 2 - 1 | 2 | 43.083953 | -70.801212 | 46.09 |
|  | 3 | 43.083224 | -70.801856 | 52.36 |
|  | 4 | 43.083866 | -70.803165 | 61.10 |
| , $\times^{2}$ | 5 | 43.084580 | -70.802457 | 53.31 |
| Name: TREELINE <br> Upper edge height: 35.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085164 | -70.808848 | 82.83 |
|  | 2 | 43.085454 | -70.807942 | 81.22 |
|  | 3 | 43.085373 | -70.807765 | 82.86 |
|  | 4 | 43.085040 | -70.807564 | 86.97 |


| Name: Trees <br> Upper edge height: 30.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.083891 | -70.811509 | 72.86 |
|  | 2 | 43.084095 | -70.811240 | 67.62 |
| Name: Trees <br> Upper edge height: 17.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085036 | -70.807176 | 92.20 |
|  | 2 | 43.084131 | -70.806567 | 95.41 |
| Upper edge height: 40.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085261 | -70.816979 | 84.00 |
|  | 2 | 43.084955 | -70.816877 | 84.48 |
|  | 3 | 43.084477 | -70.817247 | 78.24 |
| Name: Trees2 <br> Upper edge height: 60.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
|  | 1 | 43.084443 | -70.818109 | 84.34 |
|  | 2 | 43.084602 | -70.818167 | 84.74 |
|  | 3 | 43.084354 | -70.818474 | 88.75 |


| Name: Trees3 <br> Upper edge height: 100.0 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.084287 | -70.810576 | 72.89 |
|  | 2 | 43.084550 | -70.810195 | 75.28 |
| Name: Trees 4 <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085793 | -70.815175 | 77.90 |
|  | 2 | 43.085354 | -70.814585 | 81.00 |
|  | 3 | 43.086098 | -70.812858 | 77.64 |
| Name: Trees5 <br> Upper edge height: 45.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084411 | -70.807233 | 89.30 |
|  | 2 | 43.084554 | -70.807316 | 89.33 |
|  | 3 | 43.084677 | -70.807358 | 89.54 |
|  | 4 | 43.084730 | -70.807552 | 87.97 |
| Name: Trees6 <br> Upper edge height: 20.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085286 | -70.814633 | 80.07 |
|  | 2 | 43.083793 | -70.813418 | 79.96 |


| Name: Trees7 <br> Upper edge height: 30.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.083527 | -70.812571 | 74.50 |
|  | 2 | 43.083829 | -70.811932 | 72.49 |
| Name: WRHSE1 <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085129 | -70.813496 | 81.26 |
| Hasehy- | 2 | 43.085227 | -70.813254 | 81.50 |
|  | 3 | 43.085137 | -70.813085 | 81.35 |
| $13 \times$ | 4 | 43.084986 | -70.813064 | 81.23 |
|  | 5 | 43.084886 | -70.813292 | 81.62 |
|  | 6 | 43.085129 | -70.813496 | 81.26 |
| Name: WRHSE2Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084916 | -70.813107 | 81.43 |
|  | 2 | 43.084740 | -70.813499 | 81.62 |
|  | 3 | 43.084705 | -70.813466 | 81.64 |
|  | 4 | 43.084630 | -70.813662 | 81.71 |
|  | 5 | 43.084174 | -70.813292 | 81.76 |
|  | 6 | 43.084399 | -70.812785 | 81.68 |
|  | 7 | 43.084501 | -70.812860 | 81.70 |
|  | 8 | 43.084540 | -70.812758 | 81.66 |
|  | 9 | 43.084916 | -70.813107 | 81.43 |

## Summary of PV Glare Analysis

PV configuration and total predicted glare

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced | Data File |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | min | min | kWh |  |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT3 | 0.0 | 124.0 | 236 | 0 | - | - |
| CRPRT4 | 0.0 | 124.0 | 566 | 0 | - | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - | - |
| LGBLDG | 10.0 | 214.0 | 0 | 0 | - | - |
| SMBLDG | 10.0 | 214.0 | 0 | 0 | - | - |

## Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

| PV | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| crprt3 (green) | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 85 | 0 |  |
| crprt3 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| crprt4 (green) | 0 | 139 | 48 | 0 | 0 | 0 | 0 | 0 | 0 | 186 | 0 |  |
| crprt4 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## PV \& Receptor Analysis Results

Results for each PV array and receptor
CRPRT1 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

CRPRT2 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

CRPRT3 low potential for temporary after-image

| Component | Green glare (min) |
| :--- | :---: |
| OP: 1-ATCT | 0 |
| Yellow glare (min) |  |
| OP: OP 2 | 0 |
| OP: OP 3 | 0 |
| OP: OP 4 | 0 |
| OP: OP 5 | 0 |
| OP: 6-ATCT | 0 |
| OP: OP 7 | 0 |
| Route: Route 1 | 0 |
| Route: Route 2 | 0 |
| Route: Route 3 | 79 |
| Route: Route 4 | 157 |
| Route: Route 5 | 0 |
| Route: Route 6 | 0 |

## CRPRT3: 1-ATCT

No glare found

## CRPRT3: OP 2

No glare found

## CRPRT3: OP 3

No glare found

## CRPRT3: OP 4

No glare found

CRPRT3: OP 5
No glare found

## CRPRT3: 6-ATCT

No glare found

CRPRT3: OP 7
No glare found

## CRPRT3: Route 1

No glare found

## CRPRT3: Route 2

No glare found

## CRPRT3: Route 3

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.




## CRPRT3: Route 4

PV array is expected to produce the following glare for this receptor:

- 157 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


CRPRT3: Route 5
No glare found

## CRPRT3: Route 6

No glare found

CRPRT4 Iow potential for temporary after-image

| Component | Green glare (min) |
| :--- | :---: |
| OP: 1-ATCT | 0 |
| Yellow glare (min) |  |
| OP: OP 2 | 0 |
| OP: OP 3 | 0 |
| OP: OP 4 | 0 |
| OP: OP 5 | 0 |
| OP: 6-ATCT | 0 |
| OP: OP 7 | 0 |
| Route: Route 1 | 0 |
| Route: Route 2 | 0 |
| Route: Route 3 | 311 |

CRPRT4: 1-ATCT
No glare found

CRPRT4: OP 2
No glare found

CRPRT4: OP 3
No glare found

## CRPRT4: OP 4

No glare found

## CRPRT4: OP 5

No glare found

## CRPRT4: 6-ATCT

No glare found

## CRPRT4: OP 7

No glare found

## CRPRT4: Route 1

No glare found

CRPRT4: Route 2
No glare found

## CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


## CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.








## CRPRT4: Route 5

No glare found

## CRPRT4: Route 6

No glare found

CRPRT5 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

LGBLDG no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |


| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, nc discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.


# ALBACORE, Portsmouth, NH ALBCR_13Tilt_124Carports_Obstrctns_2ATCT_NoPlant 

Client: Lonza
Created Feb 22, 2024
Updated Feb 22, 2024
Time-step 1 minute
Timezone offset UTC-5
Minimum sun altitude 0.0 deg
Site ID 112727.19298
Project type Advanced
Project status: active
Category 1 MW to 5 MW


Misc. Analysis Settings

PV Analysis Methodology: Version 2
Enhanced subtended angle calculation: On

Summary of Results Glare with low potential for temporary after-image predicted

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{d e g}$ | $\mathbf{d e g}$ | $\mathbf{m i n}$ | $\mathbf{m i n}$ | $\mathbf{k W h}$ |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT3 | 0.0 | 124.0 | 236 | 0 | - |
| CRPRT4 | 0.0 | 124.0 | 566 | 0 | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - |
| LGBLDG | 13.0 | 214.0 | 0 | 0 | - |
| SMBLDG | 13.0 | 214.0 | 0 | 0 | - |

## Component Data

## PV Array(s)

Total PV footprint area: 3.1 acres

| Name: CRPRT1 <br> Footprint area: 0.20 acre | Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Axis tracking: Fixed (no rotation) Tilt: 0.0 deg <br> Orientation: 124.0 deg |  | deg | $\operatorname{deg}$ | ft | ft | ft |
| Rated power: - | 1 | 43.085650 | -70.803723 | 57.92 | 20.17 | 78.09 |
| Panel material: Smooth glass with AR coating | 2 | 43.085595 | -70.803619 | 57.81 | 14.00 | 71.81 |
| Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes | 3 | 43.085032 | -70.804187 | 64.54 | 14.00 | 78.54 |
| Slope error: 8.43 mrad | 4 | 43.085084 | -70.804291 | 66.68 | 20.17 | 86.85 |



Name: CRPRT2
Footprint area: 0.26 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085519 | -70.803626 | 57.88 | 22.48 | 80.36 |
| 2 | 43.085431 | -70.803461 | 56.75 | 14.00 | 70.75 |
| 3 | 43.084981 | -70.803912 | 58.98 | 14.00 | 72.98 |
| 4 | 43.085070 | -70.804083 | 59.73 | 22.48 | 82.20 |



Name: CRPRT3
Footprint area: 0.23 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 124.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes
Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085400 | -70.803418 | 56.90 | 22.48 | 79.38 |
| 2 | 43.085325 | -70.803271 | 56.23 | 14.00 | 70.23 |
| 3 | 43.084876 | -70.803716 | 58.56 | 14.00 | 72.56 |
| 4 | 43.084953 | -70.803866 | 59.01 | 22.48 | 81.49 |



Name: CRPRT4
Footprint area: 0.13 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085298 | -70.803223 | 56.02 | 20.17 | 76.19 |
| 2 | 43.085253 | -70.803139 | 56.21 | 14.00 | 70.21 |
| 3 | 43.084808 | -70.803572 | 58.45 | 14.00 | 72.45 |
| 4 | 43.084851 | -70.803658 | 58.35 | 20.17 | 78.52 |



Name: CRPRT5
Footprint area: 0.07 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085549 | -70.803405 | 56.86 | 20.17 | 77.02 |
| 2 | 43.085404 | -70.803116 | 55.16 | 20.17 | 75.32 |
| 3 | 43.085334 | -70.803188 | 55.25 | 14.00 | 69.25 |
| 4 | 43.085478 | -70.803470 | 57.01 | 14.00 | 71.01 |



Name: LGBLDG
Footprint area: 2.0 acres
Axis tracking: Fixed (no rotation)
Tilt: 13.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.084344 | -70.802133 | 51.60 | 93.83 | 145.44 |
| 2 | 43.084054 | -70.801543 | 49.18 | 93.83 | 143.01 |
| 3 | 43.083901 | -70.801690 | 49.39 | 93.83 | 143.22 |
| 4 | 43.083859 | -70.801609 | 49.20 | 93.83 | 143.03 |
| 5 | 43.083897 | -70.801574 | 49.27 | 93.83 | 143.10 |
| 6 | 43.083839 | -70.801453 | 47.35 | 93.83 | 141.18 |
| 7 | 43.083345 | -70.801919 | 51.93 | 93.83 | 145.76 |
| 8 | 43.083906 | -70.803019 | 59.40 | 93.83 | 153.23 |
| 10 | 43.084395 | -70.802537 | 54.24 | 93.83 | 148.07 |
| 11 | 43.084315 | -70.802368 | 51.53 | 93.83 | 145.36 |
| 12 | 43.084337 | -70.802347 | 51.04 | 93.83 | 144.87 |
| 13 | 43.084303 | -70.802278 | 52.48 | 93.83 | 146.31 |
| 14 | 43.084336 | -70.802245 | 52.51 | 93.83 | 146.34 |
|  |  |  | 51.69 |  | 145.52 |


| Name: SMBLDG <br> Footprint area: 0.22 acre <br> Axis tracking: Fixed (no rotation) <br> Tilt: 13.0 deg <br> Orientation: 214.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rated power: - | 1 | 43.084480 | -70.803051 | 56.19 | 88.00 | 144.19 |
| Panel material: Smooth glass with AR coating | 2 | 43.084450 | -70.803081 | 56.31 | 88.00 | 144.31 |
| Vary reflectivity with sun position? Yes | 3 | 43.084506 | -70.803193 | 56.74 | 88.00 | 144.74 |
| Slope error: 8.43 mrad | 4 | 43.084466 | -70.803232 | 56.81 | 88.00 | 144.81 |
|  | 5 | 43.084412 | -70.803118 | 56.55 | 88.00 | 144.55 |
| - | 6 | 43.084252 | -70.803275 | 58.91 | 88.00 | 146.91 |
|  | 7 | 43.084414 | -70.803594 | 61.58 | 88.00 | 149.58 |
|  | 8 | 43.084643 | -70.803375 | 58.79 | 88.00 | 146.79 |

Route Receptor(s)

| Name: Route 1 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.082607 | -70.800659 | 43.16 | 4.50 | 47.66 |
|  | 2 | 43.082965 | -70.800254 | 39.75 | 4.50 | 44.25 |
|  | 3 | 43.084118 | -70.798835 | 40.69 | 4.50 | 45.19 |
| Name: Route 2 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.084096 | -70.798795 | 40.76 | 8.50 | 49.26 |
|  | 2 | 43.082949 | -70.800223 | 39.72 | 8.50 | 48.22 |
|  | 3 | 43.082597 | -70.800616 | 42.88 | 8.50 | 51.38 |
| Name: Route 3 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| \% | 1 | 43.085442 | -70.804811 | 63.97 | 4.50 | 68.47 |
|  | 2 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
| bxic | 3 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
|  | 4 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
| $8$ | 5 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
|  | 6 | 43.084394 | -70.804068 | 68.75 | 4.50 | 73.25 |
|  | 7 | 43.083881 | -70.803489 | 64.40 | 4.50 | 68.90 |
|  | 8 | 43.083614 | -70.803103 | 60.85 | 4.50 | 65.35 |
| Name: Route 4 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude deg | Longitude deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.083602 | -70.803135 | 60.76 | 8.50 | 69.26 |
|  | 2 | 43.083841 | -70.803542 | 64.38 | 8.50 | 72.88 |
|  | 3 | 43.084382 | -70.804111 | 68.76 | 8.50 | 77.26 |
|  | 4 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 5 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 6 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 7 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 8 | 43.085416 | -70.804830 | 64.17 | 8.50 | 72.67 |


| Name: Route 5 <br> Route type Two-way <br> View angle: 50.0 deg |
| :--- |

## Discrete Observation Receptors

| Number | Latitude | Longitude | Ground elevation | Height above ground | Total Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | ft | ft | ft |
| 1-ATCT | 43.084384 | -70.818882 | 89.93 | 130.00 | 219.93 |
| OP 2 | 43.082455 | -70.800057 | 42.02 | 20.00 | 62.02 |
| OP 3 | 43.082529 | -70.799934 | 41.99 | 30.00 | 71.99 |
| OP 4 | 43.083085 | -70.799471 | 39.01 | 6.00 | 45.01 |
| OP 5 | 43.083191 | -70.799294 | 38.75 | 15.00 | 53.75 |
| 6-ATCT | 43.084349 | -70.818856 | 89.97 | 120.00 | 209.97 |
| OP 7 | 43.083343 | -70.803962 | 70.10 | 40.00 | 110.10 |

## 1-ATCT map image



6-ATCT map image


## Obstruction Components

| Name: BLDG2 <br> Upper edge height: 20.0 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.084955 | -70.806346 | 99.52 |
|  | 2 | 43.085031 | -70.806408 | 98.08 |
|  | 3 | 43.084866 | -70.806801 | 99.55 |
|  | 4 | 43.084555 | -70.806565 | 99.98 |
|  | 5 | 43.084608 | -70.806439 | 99.85 |
|  | 6 | 43.084444 | -70.806325 | 99.64 |
|  | 7 | 43.084592 | -70.806011 | 99.08 |
|  | 8 | 43.084965 | -70.806346 | 99.43 |



| Name: HighEdge4 Upper edge height: 20.2 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.085307 | -70.803260 | 56.28 |
|  | 2 | 43.084860 | -70.803684 | 58.42 |
| Name: PRPT1 <br> Upper edge height: 93.2 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084674 | -70.803390 | 58.96 |
|  | 2 | 43.084478 | -70.802983 | 56.11 |
| - | 3 | 43.084211 | -70.803240 | 59.29 |
| - | 4 | 43.084415 | -70.803648 | 62.46 |
|  | 5 | 43.084674 | -70.803390 | 58.96 |
| Name: PRPT2 <br> Upper edge height: 99.3 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
| , , ¢-m yorir | 1 | 43.084580 | -70.802457 | 53.31 |
| - 2 - 1 | 2 | 43.083953 | -70.801212 | 46.09 |
|  | 3 | 43.083224 | -70.801856 | 52.36 |
|  | 4 | 43.083866 | -70.803165 | 61.10 |
| , $\times^{2}$ | 5 | 43.084580 | -70.802457 | 53.31 |
| Name: TREELINE <br> Upper edge height: 35.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085164 | -70.808848 | 82.83 |
|  | 2 | 43.085454 | -70.807942 | 81.22 |
|  | 3 | 43.085373 | -70.807765 | 82.86 |
|  | 4 | 43.085040 | -70.807564 | 86.97 |


| Name: Trees <br> Upper edge height: 17.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.085036 | -70.807176 | 92.20 |
|  | 2 | 43.084131 | -70.806567 | 95.41 |
| Name: Trees <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.083891 | -70.811509 | 72.86 |
|  | 2 | 43.084095 | -70.811240 | 67.62 |
| Name: Trees1 <br> Upper edge height: 40.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085261 | -70.816979 | 84.00 |
|  | 2 | 43.084955 | -70.816877 | 84.48 |
|  | 3 | 43.084477 | -70.817247 | 78.24 |
| Name: Trees2 <br> Upper edge height: 60.0 ft | Vertex | Latitude deg | Longitude deg | Ground elevation <br> ft |
|  | 1 | 43.084443 | -70.818109 | 84.34 |
|  | 2 | 43.084602 | -70.818167 | 84.74 |
|  | 3 | 43.084354 | -70.818474 | 88.75 |


| Name: Trees3 <br> Upper edge height: 100.0 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.084287 | -70.810576 | 72.89 |
|  | 2 | 43.084550 | -70.810195 | 75.28 |
| Name: Trees 4 <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085793 | -70.815175 | 77.90 |
|  | 2 | 43.085354 | -70.814585 | 81.00 |
|  | 3 | 43.086098 | -70.812858 | 77.64 |
| Name: Trees5 <br> Upper edge height: 45.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084411 | -70.807233 | 89.30 |
|  | 2 | 43.084554 | -70.807316 | 89.33 |
|  | 3 | 43.084677 | -70.807358 | 89.54 |
|  | 4 | 43.084730 | -70.807552 | 87.97 |
| Name: Trees6 <br> Upper edge height: 20.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085286 | -70.814633 | 80.07 |
|  | 2 | 43.083793 | -70.813418 | 79.96 |


| Name: Trees7 <br> Upper edge height: 30.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.083527 | -70.812571 | 74.50 |
|  | 2 | 43.083829 | -70.811932 | 72.49 |
| Name: WRHSE1 <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085129 | -70.813496 | 81.26 |
| Hasehy- | 2 | 43.085227 | -70.813254 | 81.50 |
|  | 3 | 43.085137 | -70.813085 | 81.35 |
| $13 \times$ | 4 | 43.084986 | -70.813064 | 81.23 |
|  | 5 | 43.084886 | -70.813292 | 81.62 |
|  | 6 | 43.085129 | -70.813496 | 81.26 |
| Name: WRHSE2Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084916 | -70.813107 | 81.43 |
|  | 2 | 43.084740 | -70.813499 | 81.62 |
|  | 3 | 43.084705 | -70.813466 | 81.64 |
|  | 4 | 43.084630 | -70.813662 | 81.71 |
|  | 5 | 43.084174 | -70.813292 | 81.76 |
|  | 6 | 43.084399 | -70.812785 | 81.68 |
|  | 7 | 43.084501 | -70.812860 | 81.70 |
|  | 8 | 43.084540 | -70.812758 | 81.66 |
|  | 9 | 43.084916 | -70.813107 | 81.43 |

## Summary of PV Glare Analysis

PV configuration and total predicted glare

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced | Data File |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | min | min | kWh |  |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT3 | 0.0 | 124.0 | 236 | 0 | - | - |
| CRPRT4 | 0.0 | 124.0 | 566 | 0 | - | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - | - |
| LGBLDG | 13.0 | 214.0 | 0 | 0 | - | - |
| SMBLDG | 13.0 | 214.0 | 0 | 0 | - | - |

## Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

| PV | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| crprt3 (green) | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 85 | 0 |  |
| crprt3 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| crprt4 (green) | 0 | 139 | 48 | 0 | 0 | 0 | 0 | 0 | 0 | 186 | 0 |  |
| crprt4 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## PV \& Receptor Analysis Results

Results for each PV array and receptor
CRPRT1 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

CRPRT2 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

CRPRT3 low potential for temporary after-image

| Component | Green glare (min) |
| :--- | :---: |
| OP: 1-ATCT | 0 |
| Yellow glare (min) |  |
| OP: OP 2 | 0 |
| OP: OP 3 | 0 |
| OP: OP 4 | 0 |
| OP: OP 5 | 0 |
| OP: 6-ATCT | 0 |
| OP: OP 7 | 0 |
| Route: Route 1 | 0 |
| Route: Route 2 | 0 |
| Route: Route 3 | 79 |
| Route: Route 4 | 157 |
| Route: Route 5 | 0 |
| Route: Route 6 | 0 |

## CRPRT3: 1-ATCT

No glare found

## CRPRT3: OP 2

No glare found

## CRPRT3: OP 3

No glare found

## CRPRT3: OP 4

No glare found

CRPRT3: OP 5
No glare found

## CRPRT3: 6-ATCT

No glare found

CRPRT3: OP 7
No glare found

## CRPRT3: Route 1

No glare found

## CRPRT3: Route 2

No glare found

## CRPRT3: Route 3

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.




## CRPRT3: Route 4

PV array is expected to produce the following glare for this receptor:

- 157 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


CRPRT3: Route 5
No glare found

## CRPRT3: Route 6

No glare found

CRPRT4 Iow potential for temporary after-image

| Component | Green glare (min) |
| :--- | :---: |
| OP: 1-ATCT | 0 |
| Yellow glare (min) |  |
| OP: OP 2 | 0 |
| OP: OP 3 | 0 |
| OP: OP 4 | 0 |
| OP: OP 5 | 0 |
| OP: 6-ATCT | 0 |
| OP: OP 7 | 0 |
| Route: Route 1 | 0 |
| Route: Route 2 | 0 |
| Route: Route 3 | 311 |

CRPRT4: 1-ATCT
No glare found

CRPRT4: OP 2
No glare found

CRPRT4: OP 3
No glare found

## CRPRT4: OP 4

No glare found

## CRPRT4: OP 5

No glare found

## CRPRT4: 6-ATCT

No glare found

## CRPRT4: OP 7

No glare found

## CRPRT4: Route 1

No glare found

CRPRT4: Route 2
No glare found

## CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


## CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.








## CRPRT4: Route 5

No glare found

## CRPRT4: Route 6

No glare found

CRPRT5 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

LGBLDG no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |


| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, nc discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.


# ALBACORE, Portsmouth, NH ALBCR_15Tilt_124Carports_Obstrctns_2ATCT_NoPlant 

Client: Lonza
Created Feb 22, 2024
Updated Feb 22, 2024
Time-step 1 minute
Timezone offset UTC-5
Minimum sun altitude 0.0 deg
Site ID 112723.19298
Project type Advanced
Project status: active
Category 1 MW to 5 MW


Misc. Analysis Settings

PV Analysis Methodology: Version 2
Enhanced subtended angle calculation: On

Summary of Results Glare with low potential for temporary after-image predicted

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{d e g}$ | $\mathbf{d e g}$ | $\mathbf{m i n}$ | $\mathbf{m i n}$ | $\mathbf{k W h}$ |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - |
| CRPRT3 | 0.0 | 124.0 | 236 | 0 | - |
| CRPRT4 | 0.0 | 124.0 | 566 | 0 | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - |
| LGBLDG | 15.0 | 214.0 | 0 | 0 | - |
| SMBLDG | 15.0 | 214.0 | 0 | 0 | - |

## Component Data

## PV Array(s)

Total PV footprint area: 3.1 acres

| Name: CRPRT1 <br> Footprint area: 0.20 acre | Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Axis tracking: Fixed (no rotation) Tilt: 0.0 deg <br> Orientation: 124.0 deg |  | deg | $\operatorname{deg}$ | ft | ft | ft |
| Rated power: - | 1 | 43.085650 | -70.803723 | 57.92 | 20.17 | 78.09 |
| Panel material: Smooth glass with AR coating | 2 | 43.085595 | -70.803619 | 57.81 | 14.00 | 71.81 |
| Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes | 3 | 43.085032 | -70.804187 | 64.54 | 14.00 | 78.54 |
| Slope error: 8.43 mrad | 4 | 43.085084 | -70.804291 | 66.68 | 20.17 | 86.85 |



Name: CRPRT2
Footprint area: 0.26 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085519 | -70.803626 | 57.88 | 22.48 | 80.36 |
| 2 | 43.085431 | -70.803461 | 56.75 | 14.00 | 70.75 |
| 3 | 43.084981 | -70.803912 | 58.98 | 14.00 | 72.98 |
| 4 | 43.085070 | -70.804083 | 59.73 | 22.48 | 82.20 |



Name: CRPRT3
Footprint area: 0.23 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 124.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes
Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085400 | -70.803418 | 56.90 | 22.48 | 79.38 |
| 2 | 43.085325 | -70.803271 | 56.23 | 14.00 | 70.23 |
| 3 | 43.084876 | -70.803716 | 58.56 | 14.00 | 72.56 |
| 4 | 43.084953 | -70.803866 | 59.01 | 22.48 | 81.49 |



Name: CRPRT4
Footprint area: 0.13 acre

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085298 | -70.803223 | 56.02 | 20.17 | 76.19 |
| 2 | 43.085253 | -70.803139 | 56.21 | 14.00 | 70.21 |
| 3 | 43.084808 | -70.803572 | 58.45 | 14.00 | 72.45 |
| 4 | 43.084851 | -70.803658 | 58.35 | 20.17 | 78.52 |



Name: CRPRT5
Footprint area: 0.07 acre
Axis tracking: Fixed (no rotation)
Tilt: 0.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | $\mathbf{d e g}$ | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.085549 | -70.803405 | 56.86 | 20.17 | 77.02 |
| 2 | 43.085404 | -70.803116 | 55.16 | 20.17 | 75.32 |
| 3 | 43.085334 | -70.803188 | 55.25 | 14.00 | 69.25 |
| 4 | 43.085478 | -70.803470 | 57.01 | 14.00 | 71.01 |



Name: LGBLDG
Footprint area: 2.0 acres
Axis tracking: Fixed (no rotation)
Tilt: 15.0 deg
Orientation: 214.0 deg
Rated power: -
Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes
Correlate slope error with surface type? Yes Slope error: 8.43 mrad

| Vertex | Latitude | Longitude | Ground elevation | Height above ground | Total elevation |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | $\mathbf{f t}$ | $\mathbf{f t}$ | $\mathbf{f t}$ |
| 1 | 43.084344 | -70.802133 | 51.60 | 93.83 | 145.44 |
| 2 | 43.084054 | -70.801543 | 49.18 | 93.83 | 143.01 |
| 3 | 43.083901 | -70.801690 | 49.39 | 93.83 | 143.22 |
| 4 | 43.083859 | -70.801609 | 49.20 | 93.83 | 143.03 |
| 5 | 43.083897 | -70.801574 | 49.27 | 93.83 | 143.10 |
| 6 | 43.083839 | -70.801453 | 47.35 | 93.83 | 141.18 |
| 7 | 43.083345 | -70.801919 | 51.93 | 93.83 | 145.76 |
| 8 | 43.083906 | -70.803019 | 59.40 | 93.83 | 153.23 |
| 10 | 43.084395 | -70.802537 | 54.24 | 93.83 | 148.07 |
| 11 | 43.084315 | -70.802368 | 51.53 | 93.83 | 145.36 |
| 12 | 43.084337 | -70.802347 | 51.04 | 93.83 | 144.87 |
| 13 | 43.084303 | -70.802278 | 52.48 | 93.83 | 146.31 |
| 14 | 43.084336 | -70.802245 | 52.51 | 93.83 | 146.34 |
|  |  |  | 51.69 |  | 145.52 |


| Name: SMBLDG <br> Footprint area: 0.22 acre <br> Axis tracking: Fixed (no rotation) <br> Tilt: 15.0 deg <br> Orientation: 214.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rated power: - | 1 | 43.084480 | -70.803051 | 56.19 | 88.00 | 144.19 |
| Panel material: Smooth glass with AR coating | 2 | 43.084450 | -70.803081 | 56.31 | 88.00 | 144.31 |
| Vary reflectivity with sun position? Yes | 3 | 43.084506 | -70.803193 | 56.74 | 88.00 | 144.74 |
| Slope error: 8.43 mrad | 4 | 43.084466 | -70.803232 | 56.81 | 88.00 | 144.81 |
|  | 5 | 43.084412 | -70.803118 | 56.55 | 88.00 | 144.55 |
| - | 6 | 43.084252 | -70.803275 | 58.91 | 88.00 | 146.91 |
|  | 7 | 43.084414 | -70.803594 | 61.58 | 88.00 | 149.58 |
|  | 8 | 43.084643 | -70.803375 | 58.79 | 88.00 | 146.79 |

Route Receptor(s)

| Name: Route 1 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.082607 | -70.800659 | 43.16 | 4.50 | 47.66 |
|  | 2 | 43.082965 | -70.800254 | 39.75 | 4.50 | 44.25 |
|  | 3 | 43.084118 | -70.798835 | 40.69 | 4.50 | 45.19 |
| Name: Route 2 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.084096 | -70.798795 | 40.76 | 8.50 | 49.26 |
|  | 2 | 43.082949 | -70.800223 | 39.72 | 8.50 | 48.22 |
|  | 3 | 43.082597 | -70.800616 | 42.88 | 8.50 | 51.38 |
| Name: Route 3 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
| \% | 1 | 43.085442 | -70.804811 | 63.97 | 4.50 | 68.47 |
|  | 2 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
| bxic | 3 | 43.084962 | -70.804519 | 67.50 | 4.50 | 72.00 |
|  | 4 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
| $8$ | 5 | 43.084630 | -70.804302 | 69.07 | 4.50 | 73.57 |
|  | 6 | 43.084394 | -70.804068 | 68.75 | 4.50 | 73.25 |
|  | 7 | 43.083881 | -70.803489 | 64.40 | 4.50 | 68.90 |
|  | 8 | 43.083614 | -70.803103 | 60.85 | 4.50 | 65.35 |
| Name: Route 4 <br> Route type Two-way <br> View angle: 50.0 deg | Vertex | Latitude deg | Longitude deg | Ground elevation <br> ft | Height above ground <br> ft | Total elevation <br> ft |
|  | 1 | 43.083602 | -70.803135 | 60.76 | 8.50 | 69.26 |
|  | 2 | 43.083841 | -70.803542 | 64.38 | 8.50 | 72.88 |
|  | 3 | 43.084382 | -70.804111 | 68.76 | 8.50 | 77.26 |
|  | 4 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 5 | 43.084618 | -70.804339 | 69.09 | 8.50 | 77.59 |
|  | 6 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 7 | 43.084888 | -70.804519 | 67.86 | 8.50 | 76.36 |
|  | 8 | 43.085416 | -70.804830 | 64.17 | 8.50 | 72.67 |


| Name: Route 5 <br> Route type Two-way <br> View angle: 50.0 deg |
| :--- |

## Discrete Observation Receptors

| Number | Latitude | Longitude | Ground elevation | Height above ground | Total Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | ft | ft | ft |
| 1-ATCT | 43.084384 | -70.818882 | 89.93 | 130.00 | 219.93 |
| OP 2 | 43.082455 | -70.800057 | 42.02 | 20.00 | 62.02 |
| OP 3 | 43.082529 | -70.799934 | 41.99 | 30.00 | 71.99 |
| OP 4 | 43.083085 | -70.799471 | 39.01 | 6.00 | 45.01 |
| OP 5 | 43.083191 | -70.799294 | 38.75 | 15.00 | 53.75 |
| 6-ATCT | 43.084349 | -70.818856 | 89.97 | 120.00 | 209.97 |
| OP 7 | 43.083343 | -70.803962 | 70.10 | 40.00 | 110.10 |

## 1-ATCT map image



6-ATCT map image


## Obstruction Components

| Name: BLDG2 <br> Upper edge height: 20.0 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.084955 | -70.806346 | 99.52 |
|  | 2 | 43.085031 | -70.806408 | 98.08 |
|  | 3 | 43.084866 | -70.806801 | 99.55 |
|  | 4 | 43.084555 | -70.806565 | 99.98 |
|  | 5 | 43.084608 | -70.806439 | 99.85 |
|  | 6 | 43.084444 | -70.806325 | 99.64 |
|  | 7 | 43.084592 | -70.806011 | 99.08 |
|  | 8 | 43.084965 | -70.806346 | 99.43 |



| Name: HighEdge4 Upper edge height: 20.2 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.085307 | -70.803260 | 56.28 |
|  | 2 | 43.084860 | -70.803684 | 58.42 |
| Name: PRPT1 <br> Upper edge height: 93.2 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084674 | -70.803390 | 58.96 |
|  | 2 | 43.084478 | -70.802983 | 56.11 |
| - | 3 | 43.084211 | -70.803240 | 59.29 |
| - | 4 | 43.084415 | -70.803648 | 62.46 |
|  | 5 | 43.084674 | -70.803390 | 58.96 |
| Name: PRPT2 <br> Upper edge height: 99.3 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
| , , ¢-m yorir | 1 | 43.084580 | -70.802457 | 53.31 |
| - 2 - 1 | 2 | 43.083953 | -70.801212 | 46.09 |
|  | 3 | 43.083224 | -70.801856 | 52.36 |
|  | 4 | 43.083866 | -70.803165 | 61.10 |
| , $\times^{2}$ | 5 | 43.084580 | -70.802457 | 53.31 |
| Name: TREELINE <br> Upper edge height: 35.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085164 | -70.808848 | 82.83 |
|  | 2 | 43.085454 | -70.807942 | 81.22 |
|  | 3 | 43.085373 | -70.807765 | 82.86 |
|  | 4 | 43.085040 | -70.807564 | 86.97 |


| Name: Trees <br> Upper edge height: 30.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.083891 | -70.811509 | 72.86 |
|  | 2 | 43.084095 | -70.811240 | 67.62 |
| Name: Trees <br> Upper edge height: 17.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085036 | -70.807176 | 92.20 |
|  | 2 | 43.084131 | -70.806567 | 95.41 |
| Upper edge height: 40.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085261 | -70.816979 | 84.00 |
|  | 2 | 43.084955 | -70.816877 | 84.48 |
|  | 3 | 43.084477 | -70.817247 | 78.24 |
| Name: Trees2 <br> Upper edge height: 60.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
|  | 1 | 43.084443 | -70.818109 | 84.34 |
|  | 2 | 43.084602 | -70.818167 | 84.74 |
|  | 3 | 43.084354 | -70.818474 | 88.75 |


| Name: Trees3 <br> Upper edge height: 100.0 ft | Vertex | Latitude deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.084287 | -70.810576 | 72.89 |
|  | 2 | 43.084550 | -70.810195 | 75.28 |
| Name: Trees 4 <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085793 | -70.815175 | 77.90 |
|  | 2 | 43.085354 | -70.814585 | 81.00 |
|  | 3 | 43.086098 | -70.812858 | 77.64 |
| Name: Trees5 <br> Upper edge height: 45.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084411 | -70.807233 | 89.30 |
|  | 2 | 43.084554 | -70.807316 | 89.33 |
|  | 3 | 43.084677 | -70.807358 | 89.54 |
|  | 4 | 43.084730 | -70.807552 | 87.97 |
| Name: Trees6 <br> Upper edge height: 20.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085286 | -70.814633 | 80.07 |
|  | 2 | 43.083793 | -70.813418 | 79.96 |


| Name: Trees7 <br> Upper edge height: 30.0 ft | Vertex | Latitude <br> deg | Longitude <br> deg | Ground elevation <br> ft |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 43.083527 | -70.812571 | 74.50 |
|  | 2 | 43.083829 | -70.811932 | 72.49 |
| Name: WRHSE1 <br> Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.085129 | -70.813496 | 81.26 |
| Hasehy- | 2 | 43.085227 | -70.813254 | 81.50 |
|  | 3 | 43.085137 | -70.813085 | 81.35 |
| $13 \times$ | 4 | 43.084986 | -70.813064 | 81.23 |
|  | 5 | 43.084886 | -70.813292 | 81.62 |
|  | 6 | 43.085129 | -70.813496 | 81.26 |
| Name: WRHSE2Upper edge height: 30.0 ft | Vertex | Latitude | Longitude | Ground elevation |
|  |  | deg | deg | ft |
|  | 1 | 43.084916 | -70.813107 | 81.43 |
|  | 2 | 43.084740 | -70.813499 | 81.62 |
|  | 3 | 43.084705 | -70.813466 | 81.64 |
|  | 4 | 43.084630 | -70.813662 | 81.71 |
|  | 5 | 43.084174 | -70.813292 | 81.76 |
|  | 6 | 43.084399 | -70.812785 | 81.68 |
|  | 7 | 43.084501 | -70.812860 | 81.70 |
|  | 8 | 43.084540 | -70.812758 | 81.66 |
|  | 9 | 43.084916 | -70.813107 | 81.43 |

## Summary of PV Glare Analysis

PV configuration and total predicted glare

| PV Name | Tilt | Orientation | "Green" Glare | "Yellow" Glare | Energy Produced | Data File |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | deg | deg | min | min | kWh |  |
| CRPRT1 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT2 | 0.0 | 124.0 | 0 | 0 | - | - |
| CRPRT3 | 0.0 | 124.0 | 236 | 0 | - | - |
| CRPRT4 | 0.0 | 124.0 | 566 | 0 | - | - |
| CRPRT5 | 0.0 | 214.0 | 0 | 0 | - | - |
| LGBLDG | 15.0 | 214.0 | 0 | 0 | - | - |
| SMBLDG | 15.0 | 214.0 | 0 | 0 | - | - |

## Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

| PV | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| crprt3 (green) | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 85 | 0 |  |
| crprt3 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| crprt4 (green) | 0 | 139 | 48 | 0 | 0 | 0 | 0 | 0 | 0 | 186 | 0 |  |
| crprt4 (yellow) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## PV \& Receptor Analysis Results

Results for each PV array and receptor
CRPRT1 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

CRPRT2 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

CRPRT3 low potential for temporary after-image

| Component | Green glare (min) |
| :--- | :---: |
| OP: 1-ATCT | 0 |
| Yellow glare (min) |  |
| OP: OP 2 | 0 |
| OP: OP 3 | 0 |
| OP: OP 4 | 0 |
| OP: OP 5 | 0 |
| OP: 6-ATCT | 0 |
| OP: OP 7 | 0 |
| Route: Route 1 | 0 |
| Route: Route 2 | 0 |
| Route: Route 3 | 79 |
| Route: Route 4 | 157 |
| Route: Route 5 | 0 |
| Route: Route 6 | 0 |

## CRPRT3: 1-ATCT

No glare found

## CRPRT3: OP 2

No glare found

## CRPRT3: OP 3

No glare found

## CRPRT3: OP 4

No glare found

CRPRT3: OP 5
No glare found

## CRPRT3: 6-ATCT

No glare found

CRPRT3: OP 7
No glare found

## CRPRT3: Route 1

No glare found

## CRPRT3: Route 2

No glare found

## CRPRT3: Route 3

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.




## CRPRT3: Route 4

PV array is expected to produce the following glare for this receptor:

- 157 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


CRPRT3: Route 5
No glare found

## CRPRT3: Route 6

No glare found

CRPRT4 Iow potential for temporary after-image

| Component | Green glare (min) |
| :--- | :---: |
| OP: 1-ATCT | 0 |
| Yellow glare (min) |  |
| OP: OP 2 | 0 |
| OP: OP 3 | 0 |
| OP: OP 4 | 0 |
| OP: OP 5 | 0 |
| OP: 6-ATCT | 0 |
| OP: OP 7 | 0 |
| Route: Route 1 | 0 |
| Route: Route 2 | 0 |
| Route: Route 3 | 311 |

CRPRT4: 1-ATCT
No glare found

CRPRT4: OP 2
No glare found

CRPRT4: OP 3
No glare found

## CRPRT4: OP 4

No glare found

## CRPRT4: OP 5

No glare found

## CRPRT4: 6-ATCT

No glare found

## CRPRT4: OP 7

No glare found

## CRPRT4: Route 1

No glare found

CRPRT4: Route 2
No glare found

## CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.


## CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image
- 0 minutes of "yellow" glare with potential to cause temporary after-image.








## CRPRT4: Route 5

No glare found

## CRPRT4: Route 6

No glare found

CRPRT5 no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

No glare found

LGBLDG no glare found

| Component | Green glare (min) | Yellow glare (min) |
| :---: | :---: | :---: |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |


| Component | Green glare (min) | Yellow glare (min) |
| :--- | :--- | :--- |
| OP: 1-ATCT | 0 | 0 |
| OP: OP 2 | 0 | 0 |
| OP: OP 3 | 0 | 0 |
| OP: OP 4 | 0 | 0 |
| OP: OP 5 | 0 | 0 |
| OP: 6-ATCT | 0 | 0 |
| OP: OP 7 | 0 | 0 |
| Route: Route 1 | 0 | 0 |
| Route: Route 2 | 0 | 0 |
| Route: Route 3 | 0 | 0 |
| Route: Route 4 | 0 | 0 |
| Route: Route 5 | 0 | 0 |
| Route: Route 6 | 0 | 0 |

## Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, nc discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.


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# Findings of Fact | Wetland Conditional Use Permit City of Portsmouth Planning Board 

Date: July 18, 2024
Property Address: 50 Andrew Jarvis Dr.
Application \#: LU-24-50
Decision: $\square$ Approve $\square$ Deny $\square$ Approve with Conditions

## Findings of Fact:

Per RSA 676:3, I: The local land use board shall issue a final written decision which either approves or disapproves an application for a local permit and make a copy of the decision available to the applicant. The decision shall include specific written findings of fact that support the decision. Failure of the board to make specific written findings of fact supporting a disapproval shall be grounds for automatic reversal and remand by the superior court upon appeal, in accordance with the time periods set forth in RSA 677:5 or RSA 677:15, unless the court determines that there are other factors warranting the disapproval. If the application is not approved, the board shall provide the applicant with written reasons for the disapproval. If the application is approved with conditions, the board shall include in the written decision a detailed description of all conditions necessary to obtain final approval.

In order to grant Wetland Conditional Use permit approval the Planning Board shall find the application satisfies criteria set forth in the Section 10.1017.50 (Criteria for Approval) of the Zoning Ordinance.

|  | Zoning Ordinance <br> Sector 10.1017.50 <br> Criteria for Approval | Finding <br> (Meets <br> Criteria for <br> Approval) | Supporting Information |
| :---: | :--- | :---: | :--- |
| $\mathbf{1}$ | l. The land is reasonably <br> suited to the use activity <br> or alteration. | Meets <br> Does Not <br> Meet | This area is already heavily used as a recreation area for <br> high school students and other recreation leagues. The <br> addition of baseball/softball equipment will allow for <br> more teams to utilize the space. |
| $\mathbf{2}$ | 2. There is no alternative <br> location outside the <br> wetland buffer that is <br> feasible and reasonable <br> for the proposed use, <br> activity or alteration. | Meets <br> Does Not <br> Meet | While there is an alternative location in this area that <br> would create minimal disturbance and be outside the <br> buffer, it would create a safety hazard due to its <br> proximity to buildings and parking areas. The chosen <br> location within the buffer is already used as a <br> recreational field and it does not receive any harmful <br> maintenance such as fertilizer or chemical use, only <br> occasional mowing. The conversion to a <br> baseball/softball field will not change how the buffer <br> has been used historically. |


|  | Zoning Ordinance <br> Sector 10.1017.50 <br> Criteria for Approval | Finding <br> (Meets Criteria for Approval) | Supporting Information |
| :---: | :---: | :---: | :---: |
| 3 | 3. There will be no adverse impact on the wetland functional values of the site or surrounding properties. |  | The infield mix proposed for the new field will be a permeable mix that should not have a noticeable impact on infiltration within this buffer area. The adjacent wetland is well forested and should not see an impact from this field conversion. |
| 4 | 4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals. | Meets <br> Does Not Meet | The only vegetation proposed to be removed is a portion of existing grass lawn. This will be replaced with a permeable sand/silt/clay infield mix. |
| 5 | 5. The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this section. | Meets <br> Does Not Meet | The proposal minimizes impacts to the buffer by proposing a permeable infield mix and minimal permanent equipment. On-site alternatives would require greater disturbance to areas that are not already used as recreational fields. |
| 6 | 6. Any area within the vegetated buffer strip will be returned to a natural state to the extent feasible. | Meets <br> Does Not Meet | No work is proposed within the 25 ' vegetated buffer. |
| 7 | Other Board Findings: |  |  |

Portsmouth School Department - SAU 52
City Hall, 1 Junkins Ave. Suite 402
Portsmouth, NH 03801

Date: April 9, 2024
To: Wetland Conservation Committee
From: Ken Linchey, Director of Building's and Ground's
Re: Tennis Courts Walkthrough Questions

The Portsmouth High Schools Athletic Department is requesting permission to enhance the usage of one their practice fields. The softball and baseball teams are always juggling field usage between the high school fields, Granite Street softball field, Leary field, and Cough field. Making changes to this practice field will allow some relief to the scheduling and practice needs for all of Portsmouth School programs.

Project details:

- Remove 3" of sod \& loam to create a skinned infield diamond.
- Replaced skinned area with a native infield softball/baseball infield mix. The mixture is made up a clay, silt, and sand.
- Installation of a backstop that would minimize softballs from being hit into the wetland.
- Backstop installation would consist of driving posts into the ground vs using concrete.

In summary, we evaluated how can we accommodate all of our programs within the original field structure year-round. We believe that this is just a slight adjustment with how we layout our field usage within the existing field structure.

Sincerely'
Ken Linchey
Ken Linchey
Portsmouth School Department
Director of Building's \& Ground's
"THE PURPOSE OF THE PORTSMOUTH SCHOOLS IS TO EDUCATE ALL STUDENTS BY CHALLENGING THEM TO BECOME THINKING, RESPONSIBLE, CONTRIBUTING CITIZENS WHO CONTINUE TO LEARN THROUGHOUT THEIR LIVES,"

AN EQUAL OPPORTUNITY EMPLOYER - EQUAL EDUCATIONAL OPPORTUNITIES

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# Findings of Fact | Wetland Conditional Use Permit City of Portsmouth Planning Board 

Date: July 18, 2024
Property Address: 0 Maplewood Ave.
Application \#: LU-24-102
Decision: $\square$ Approve $\quad$ Deny $\square$ Approve with Conditions

## Findings of Fact:

Per RSA 676:3, I: The local land use board shall issue a final written decision which either approves or disapproves an application for a local permit and make a copy of the decision available to the applicant. The decision shall include specific written findings of fact that support the decision. Failure of the board to make specific written findings of fact supporting a disapproval shall be grounds for automatic reversal and remand by the superior court upon appeal, in accordance with the time periods set forth in RSA 677:5 or RSA 677:15, unless the court determines that there are other factors warranting the disapproval. If the application is not approved, the board shall provide the applicant with written reasons for the disapproval. If the application is approved with conditions, the board shall include in the written decision a detailed description of all conditions necessary to obtain final approval.

In order to grant Wetland Conditional Use permit approval the Planning Board shall find the application satisfies criteria set forth in the Section 10.1017.50 (Criteria for Approval) of the Zoning Ordinance.

|  | Zoning Ordinance <br> Sector 10.1017.50 <br> Criteria for Approval | Finding <br> (Meets <br> Criteria for <br> Approval) | Supporting Information |
| :---: | :--- | :---: | :--- |
| $\mathbf{1}$ | l. The land is reasonably <br> suited to the use activity <br> or alteration. | Meets <br> Does Not <br> Meet | This work is an in-kind repair job. The damaged wall is <br> structurally integral to keeping the cemetery border <br> and fill contained. |
| $\mathbf{2}$ | 2. There is no alternative <br> location outside the <br> wetland buffer that is <br> feasible and reasonable <br> for the proposed use, <br> activity or alteration. | Meets <br> Does Not <br> Meet | There is no alternative location to rebuild this wall in. <br> The safety of the tomb and burials behind the wall is <br> reliant on the structure of this wall and it must be <br> fortified in order to prevent further erosion, or worse, <br> collapse. |
| $\mathbf{3}$ | 3. There will be no <br> adverse impact on the <br> wetland functional <br> values of the site or <br> surrounding properties. | Dees Not <br> Meet | Meets <br> The applicant used professional services to access the <br> disturb the hallowed ground. This may have impacts on <br> the pathway of any necessary construction vehicles. <br> The applicant shall restore any disturbed soils with <br> native wetland buffer conservation seed mix and <br> monitor for establishment. |



# City of Portsmouth <br> Department of Public Works 

# MEMORANDUM 

TO: Samantha Collins, Conservation Commission Chair
CC: Peter Britz, Director of Planning and Sustainability
Kate Homet, Associate Environmental Planner
FROM: Christine Sproviero, Project Manager
DATE: June 7, 2024

SUBJECT: Union Cemetery Emergency Shore Wall Repair

The Union Cemetery shore wall has sustained damage and erosion over multiple years due to large storm and tidal events. On 4/26/24, it was observed that multiple sections of the wall have fallen into the tidal area below. The City immediately filed a wetlands emergency authorization request to the New Hampshire Department of Environmental Services (NHDES) to perform repairs on the 41 ' section of shore wall, as shown in the plans attached, before further degradation occurs. The City received authorization from NHDES on $5 / 16 / 24$ which is attached.
Once authorization was granted, the City engaged Riverside \& Pickering Marine Contractors to schedule the emergency repair "in kind" work which is scheduled to begin on 6/10/24.
Following the completion of the re-construction of the wall, the City will submit post work photos as required by the Emergency Authorization.

Kind Regards,
Christine Sproviero



Robert R. Scott, Commissioner

## EMERGENCY AUTHORIZATION VERIFICATION

FILE NUMBER:
OWNER:
SITE LOCATION:
AGENT/CONTRACTOR:
AUTHORIZATION DATE:
WATERBODY:

2024-01385
CITY OF PORTSMOUTH UNION CEMETERY MAPLEWOOD AVE, PORTSMOUTH TED
MAY 16, 2024
TIDAL BUFFER ZONE

This is to confirm that New Hampshire Department of Environmental Services (NHDES) Wetlands Bureau has given emergency authorization in accordance with NH Administrative Rule Env-Wt 315 to the owner/agent to conduct the following work in the NHDES Wetlands Bureau jurisdiction (under RSA 482-A):
DESCRIPTION: Emergency authorization for the in-kind repair to an existing retaining wall.
This authorization is subject to the following conditions:

1. The applicant/contractor shall file a follow up report describing the work performed under this authorization including pre-construction and post-construction photos to NHDES by June 24, 2024; the need for additional permitting will then be determined by NHDES (if no further impacts are needed).
2. Work shall be conducted in a manner so as to minimize turbidity and sedimentation to surface waters and wetlands.
3. Appropriate siltation, erosion controls, turbidity, and sedimentation controls shall be utilized.
4. Extreme precautions shall be taken within riparian areas to limit unnecessary removal of vegetation for access.
5. Construction equipment shall be inspected daily for leaking fuel, oil, and hydraulic fluid prior to working near surface waters or wetlands.
6. Faulty equipment shall be repaired prior to working near jurisdictional areas.
7. The contractor shall have appropriate oil spill kits on site and readily accessible at all times during construction and each operator shall be trained in its use.
8. This form shall be properly posted at the work site.
9. This authorization does not convey a property right, nor authorize any injury to property of others, nor invasion of rights of others.
THIS AUTHORIZATION EXPIRES ON June 17, 2024. All work must be completed by this date. This authorization has been given file number 2024-01385. Please use this number in all future correspondence.

Signed:


Eben M. Lewis
Southeast Region Supervisor
Land Resources Management, Water Division

www.des.nh.gov
29 Hazan Drive • PO Box 95 • Concord, NH 03302-0095
NHDES Main Line: (603) 271-3503 • Subsurface Fax: (603) 271-6683 • Wetlands Fax: (603) 271-6588

From:
Sent:
To:
Subject:

Christine R. Sproviero
Wednesday, May 22, 2024 9:05 AM
Duncan Mellor
Authorization for Civilworks New England

Good morning Duncan,
Please consider this as an authorization for Civilworks New England to act as an authorized agent for the City of Portsmouth in regard to the Union Cemetery Shore Wall Project.

Regards,
Christine R. Sproviero
Project Manager
City of Portsmouth
Public Works Department
680 Peverly Hill Road
Portsmouth, NH 03801
Office: (603) 766-1755
Mobile: (603) 380-4805
Email: crSproviero@cityofportsmouth.com

# CIVILWORKS NEW ENGLAND <br> 181 WATSON ROAD <br> P.O. BOX 1166 <br> DOVER, NH 03821-1166 <br> PHONE: 603.749.0443 

## MEMORANDUM

Date: June 25, 2024
To: Portsmouth Planning Board
Re: DES 2024-01385, City of Portsmouth, Union Cemetery wall repairs
From: Duncan Mellor, PE
Civilworks New England
The damaged stone wall at Union Cemetery in Portsmouth on the bank of North Mill Pond has been repaired in-kind with dry set stonework in the Tidal Buffer Zone. All work was performed in the dry and was above and inshore of the high tide line. The disturbed lawn area was seeded with the City wetland buffer seed mix. Concurrently the project was approved by the Portsmouth Conservation Commission (letter attached).

## Before Photograph:



Photo 1 Main span removal for localized member removal and observation

## After Photographs:



Photo 2 Repaired wall looking north 6-18-24


Photo 3 Disturbed area erosion controls and seeding 6-18-24

## CIVILWORKS NEW ENGLAND

181 WATSON ROAD
P.O. BOX 1166

DOVER, NH 03821-1166
PHONE: 603.749.0443


Photo 4 Disturbed area erosion control matting over City wetland buffer seed mix 6-18-24.

In accordance with the Portsmouth Conservation Commission WCUP approval conditions, dated June 17, 2024, this area will be reseeded if growth is not successful, and native wetland buffer shrubs will be planted along the temporary access area.


# CITY OF PORTSMOUTH 

Planning \& Sustainability
Department
1 Junking Avenue
Portsmouth, New
Hampshire 03801
(603) 610-7216

## CONSERVATION COMMISSION

June 17, 2024
City of Portsmouth
PO BOX 628
Portsmouth, NH 03802
RE: Wetland Conditional Use Permit for property located at 0 Maplewood Avenue

## Dear Owner:

The Conservation Commission, at its regularly scheduled meeting of Wednesday, June 12, 2024, considered your application for an after the fact Wetland Conditional Use Permit due to the emergency authorization for repair of the stone wall alongside the North Cemetery. This application is for the restoration and repair of the wall in-kind which includes installation of new stone, installing non-woven geotextile along the eroded bank, importing structural backfill, and loam and seeding the disturbed areas once finished. Said property is shown on Assessor Map 124, Lot 3 and lies within the Municipal (M). As a result of said consideration, the Commission voted to approve the Wetland Conditional Use Permit with the following stipulations.

1. Applicant shall monitor the success of reseeded areas to ensure stabilization. If stabilization is not successful within 30 days of seeding, the area will need to be reseeded.
2. Native wetland buffer shrub plantings shall be installed within the temporary accessway area in the Fall of 2024. This should be included in updated plan set for the Planning Board submission.

This matter will be placed on the agenda for the Planning Board meeting scheduled for Thursday, July 18, 2024. One (1) hard copy of any revised plans and/or exhibits as well as an updated electronic file (in a PDF format) must be filed in the Planning \& Sustainability Department and uploaded to the online permit system no later than Wednesday, June 26, 2024.

The minutes and audio recording of this meeting are available by contacting the Planning \& Sustainability Department.

Very truly yours,


Samantha Collins, Chair Conservation Commission
cc:

# Findings of Fact | Home Occupation 2 Conditional Use Permit City of Portsmouth Planning Board 

Date: July 18, 2024
Property Address: 32 Boss Ave.
Application \#: LU-24-117
Decision: $\square$ Approve $\square$ Deny $\square$ Approve with Conditions

## Findings of Fact:

Per RSA 676:3, I: The local land use board shall issue a final written decision which either approves or disapproves an application for a local permit and make a copy of the decision available to the applicant. The decision shall include specific written findings of fact that support the decision. Failure of the board to make specific written findings of fact supporting a disapproval shall be grounds for automatic reversal and remand by the superior court upon appeal, in accordance with the time periods set forth in RSA 677:5 or RSA 677:15, unless the court determines that there are other factors warranting the disapproval. If the application is not approved, the board shall provide the applicant with written reasons for the disapproval. If the application is approved with conditions, the board shall include in the written decision a detailed description of the all conditions necessary to obtain final approval.

## Home Occupation 2 Conditional Use Permit

10.242.10 The Planning Board may grant a conditional use permit if the application is found to be in compliance with the general criteria in Section 10.243 or, if applicable, the specific standards or criteria set forth in this Ordinance for the particular use or activity.

|  | Home Occupation 2 <br> Conditional Use Permit 10.243 <br> Requirements | Finding <br> (Meets <br> Criteria/Requirement) | Supporting Information |
| :---: | :--- | :---: | :--- |
| $\mathbf{1}$ | l0.243.21 The design of <br> proposed structures, their <br> height and scale in relation to <br> the site's surroundings, the <br> nature and intensity of the <br> proposed use or activity, and <br> the layout and design of the <br> site will be compatible with <br> adjacent and nearby <br> properties, buildings and uses, <br> will complement or enhance <br> the character of surrounding <br> development, and will <br> encourage the appropriate <br> and orderly development and <br> Use of land and buildings in the <br> surrounding area. | The home occupation will be in an <br> existing studio which is contained within <br> the existing dwelling. |  |
| $\mathbf{2}$ | lo.243.22 All necessary public <br> and private utility infrastructure <br> and services will be available <br> and adequate to serve the | Does Not Meet | Meets <br> and electricity usage from the existing <br> services that serve the dwelling. |


|  | Home Occupation 2 Conditional Use Permit 10.243 Requirements | Finding <br> (Meets <br> Criteria/Requirement) | Supporting Information |
| :---: | :---: | :---: | :---: |
|  | proposed use. |  |  |
| 3 | 10.243.23 The site and surrounding streets will have adequate vehicular and pedestrian infrastructure to serve the proposed use consistent with the City's Master Plan. | Meets <br> Does Not Meet | There are three different routes to access the location in addition to lighted sidewalks. The property has 155 feet of street frontage. The Master Plan supports expanding opportunities for home-based businesses. |
| 4 | 10.243.24 The proposed structures, uses, or activities will not have significant adverse impacts on abutting and surrounding properties on account of traffic, noise, odors, vibrations, dust, fumes, hours of operation, and exterior lighting and glare. | Meets Does Not Meet | The classes will be a few hours in length and will not have any significant adverse impact on abutting and surrounding properties on account of traffic, noise, odors, vibrations, dust, fumes, hours of operation and exterior lighting glare. |
| 5 | 10.243.25 The proposed structures and uses will not have significant adverse impacts on natural or scenic resources surrounding the site, including wetlands, floodplains, and significant wildlife habitat. | Meets Does Not Meet | The art studio is fully contained within the home and will not impact the wetlands, floodplains or wildlife habitats. |
| 6 | 10.243.26 The proposed use will not cause or contribute to a significant decline in property values of adjacent properties. | Meets <br> Does Not Meet | Granting a conditional use permit to allow small art classes will be an asset to the neighborhood and will not cause a decline in property values. |
| 6 | Other Board Findings: |  |  |
| 7 | Additional Conditions of Approval: |  |  |

Rick Chellman, Chair
City of Portsmouth Planning Board
1 Junkins Avenue
Portsmouth, NH 03801

## RE: Home Occupation 2 Request for 32 Boss Ave

Dear Mr. Chellman and members of the Planning Board:
I am requesting approval for a Home Occupation 2 Conditional Use Permit so I may provide small art classes (up to 6 students) in my home studio. Proposed number of classes will not exceed 1-2 classes per day and each class will generally be $\sim 2-3$ hours in length. Anticipated hours for art classes will fall between 8am-5pm M-F (as currently allowed by Home Occupation ordinance). To accommodate working adults/parents, I would like to request flexibility in offering classes in the evenings $\sim 6-9 p m 1-2$ days a week and one day on the weekend.

Based on current parking spot standards, 3 cars can fit at the base of our driveway in front of our garage, and if needed, 1 in the neck of our driveway (see photos marked Exhibit A). As part of this conditional use permit, I am requesting 2 additional parking spots on the street (1 is currently allowed by Home Occupation Ordinance) so I can best accommodate seniors and those with mobility challenges*. I have over 155 linear feet of open space on the street directly in front of our home (see property map) which can easily fit 7-8 cars. In addition, I will strongly encourage carpooling whenever possible and install a bike rack next to my studio entrance.

Sincerely,

## Karen Rosania

32 Boss Ave
Portsmouth, NH

[^1]

PRELIMINARY DRAWING NOT FOR CONSTRUCTION


Exhebit A


32 Boss Are
$=$ proposced parkeng 3-4 spoto in drerewacy
Qoss Are



Sufficient room for another car to pass

# Findings of Fact | Detached Accessory Dwelling Unit City of Portsmouth Planning Board 

Date: July 18. 2024
Property Address: 480 Dennett Street
Application \#: LU-24-120
Decision: $\square$ Approve $\square$ Deny $\square$ Approve with Conditions

## Findings of Fact:

Per RSA 676:3, I: The local land use board shall issue a final written decision which either approves or disapproves an application for a local permit and make a copy of the decision available to the applicant. The decision shall include specific written findings of fact that support the decision. Failure of the board to make specific written findings of fact supporting a disapproval shall be grounds for automatic reversal and remand by the superior court upon appeal, in accordance with the time periods set forth in RSA 677:5 or RSA 677:15, unless the court determines that there are other factors warranting the disapproval. If the application is not approved, the board shall provide the applicant with written reasons for the disapproval. If the application is approved with conditions, the board shall include in the written decision a detailed description of the all conditions necessary to obtain final approval.

Zoning Ordinance-10.814.60: Before granting a conditional use permit for a detached ADU, the Planning Board shall make the following findings:

|  | Section 10.814.62 | Finding (Meets Requirement/ Criteria) | Supporting Information |
| :---: | :---: | :---: | :---: |
| 1 | 10.814.621 The ADU complies with all applicable standards of this Section 10.814 or as may be modified by the conditional use permit. | Meets Does Not Meet | The DADU complies with the standards in Section 10.814 with no requested modifications. |
| 2 | 10.814.622 The exterior design of the ADU is architecturally consistent with or similar in appearance to the existing principal dwelling on a lot. | Meets <br> Does Not Meet | The design of the DADU is compatible with the existing principal dwelling. |
| 3 | 10.814.623 The site plan provides adequate and appropriate open space and landscaping for both the ADU and the principal dwelling unit and complies with the off-street parking requirements of 10.814.26. | Meets Does Not Meet | The site plan provides adequate open space and the parking on the lot will exceed the requirement for the DADU. |
| 4 | 10.814.624 The ADU will maintain a compatible relationship with the character of adjacent and neighborhood properties in terms of location, design, and off-street parking layout, and will not significantly reduce the privacy of adjacent properties. | Meets Does Not Meet | The new conforming location of the DADU will be compatible with the existing neighborhood and will not reduce the privacy of adjacent properties. The DADU will be located within the existing fenced yard in a conforming location. |
| 5 | Other Board Findings: |  |  |

Planning Department City of Portsmouth

Re: 480 Dennett St

The property at 480 Dennett St is owned by the applicant and spouse. The house is occupied by the owner and family of three generations.

There is no plan for any change of ownership.

The application is for a detached ADU. The ADU will be occupied by the property owner and spouse. The primary residence will continue to be occupied by the owner's daughter and children.

There will not be a business operated from the residence per city regulations.

The property is currently connected to city water and sewer. No additional connections to city services. All connections for ADU will be provided by the primary residence.

The proposed DADU will be a one bedroom, one bathroom self contained standalone structure with separate access. All zoning requirements for lot coverage and lot line setbacks will be satisfied for an accessory structure.

There will be 4 off road parking spaces provided. There is also city planned on street parking directly in front of the residence.


Left side of backyard.

Backyard from deck.



Left side of front yard.

Right side of front yard.



Address: 480 Dennett St. Portsmouth, NH
Zone: GRA
Proposal: D-ADU
Proposal area: 750 sq. ft.
Bedrooms: 1
Bathrooms: 1


Abutting Lot
17 Stark St.
~. 18 ac
FID: 834989
Mblu: 161-03

Abutting Lo 466 Dennett St
~. 07 ac
PD: 34970
Mblu: 160-25


24 Burkitt St 24 Burkitt St.
~. 09 ac FID: 34968
Mblu: 160-23

—..

$\cdots+$ (TO BE REMOVED)

Abutting Lot
500 Dennett St.
. 12 ac
FID: 34987
Mblu: 161-01

## FLOOR PLAN


(T)
(E1)

## ELEVATION 1 יن:"



## ELEVATION 2 a/k



## 



## ELEVATION 4 anc:-1:



# Findings of Fact | Outdoor Dining Conditional Use Permit City of Portsmouth Planning Board 

Date: July 18, 2024
Property Address: 125 Brewery Lane
Application \#: LU-24-108
Decision: $\square$ Approve $\square$ Deny $\square$ Approve with Conditions

## Findings of Fact:

Per RSA 676:3, I: The local land use board shall issue a final written decision which either approves or disapproves an application for a local permit and make a copy of the decision available to the applicant. The decision shall include specific written findings of fact that support the decision. Failure of the board to make specific written findings of fact supporting a disapproval shall be grounds for automatic reversal and remand by the superior court upon appeal, in accordance with the time periods set forth in RSA 677:5 or RSA 677:15, unless the court determines that there are other factors warranting the disapproval. If the application is not approved, the board shall provide the applicant with written reasons for the disapproval. If the application is approved with conditions, the board shall include in the written decision a detailed description of the all conditions necessary to obtain final approval.

## Outdoor Dining Conditional Use Permit

10.242.10 The Planning Board may grant a conditional use permit if the application is found to be in compliance with the general criteria in Section 10.243 or, if applicable, the specific standards or criteria set forth in this Ordinance for the particular use or activity.

|  | Outdoor Dining Conditional Use Permit 10.243 Requirements | Finding <br> (Meets Criteria/Requirement) | Supporting Information |
| :---: | :---: | :---: | :---: |
| 1 | 10.243.21 The design of proposed structures, their height and scale in relation to the site's surroundings, the nature and intensity of the proposed use or activity, and the layout and design of the site will be compatible with adjacent and nearby properties, buildings and uses, will complement or enhance the character of surrounding development, and will encourage the appropriate and orderly development and use of land and buildings in the surrounding area. | Meets <br> Does Not Meet | The proposed patio, located behind the building at 125 Brewery Lane, will consist of an approximately 470 square foot gravel patio. Seating will consist of picnic tables and bistro tables and seating. One table will be adjacent to the concrete space to allow for handicap access. Seating will consist of approximately 1-2 picnic tables and 1-3 bistro tables and chairs and/or an assortment of lawn chairs. |
| 2 | 10.243.22 All necessary public and private utility infrastructure and services will be available and adequate to serve the | Meets Does Not Meet | No alteration to public and/or private utility infrastructure is required as part of the proposed use. |


|  | Outdoor Dining Conditional Use Permit 10.243 Requirements | Finding <br> (Meets <br> Criteria/Requirement) | Supporting Information |
| :---: | :---: | :---: | :---: |
|  | proposed use. |  |  |
| 3 | 10.243.23 The site and surrounding streets will have adequate vehicular and pedestrian infrastructure to serve the proposed use consistent with the City's Master Plan. | Meets Does Not Meet | There will be no impact to vehicular or pedestrian infrastructure as part of the proposed use of the space. |
| 4 | 10.243.24 The proposed structures, uses, or activities will not have significant adverse impacts on abutting and surrounding properties on account of traffic, noise, odors, vibrations, dust, fumes, hours of operation, and exterior lighting and glare. | Meets Does Not Meet | Sufficient parking is available at the business address. Additional parking is located in nearby lots during business hours. No outdoor speakers or live music will be offered on the patio. Hours of operation are between 10am-8pm. |
| 5 | 10.243.25 The proposed structures and uses will not have significant adverse impacts on natural or scenic resources surrounding the site, including wetlands, floodplains, and significant wildlife habitat. | Meets Does Not Meet | No wetlands, floodplains, wildlife habitats, or other natural or scenic resources are present at the site of the proposed patio. |
| 6 | 10.243.26 The proposed use will not cause or contribute to a significant decline in property values of adjacent properties. | Meets Does Not Meet | The proposed patio will not cause or contribute to a significant decline in property value of the adjacent properties. |
| 6 | Other Board Findings: |  |  |
| 7 | Additional Conditions of Approval: |  |  |

# Conditional Use Permit Narrative 

For

TREELINE OUTFITTERS
125 Brewery Lane

* 10.243.21 The design of proposed structures, their height and scale in relation to the site's surroundings, the nature and intensity of the proposed use or activity, and the layout and design of the site will be compatible with adjacent and nearby properties, buildings and uses, will complement or enhance the character of surrounding development, and will encourage the appropriate and orderly development and use of land and buildings in the surrounding area.

The proposed patio, located behind the building at 125 Brewery Lane, will consist of an approximately 470 square foot gravel patio. Seating will consist of picnic tables and bistro tables and seating. One table will be adjacent to the concrete space to allow for handicap access. Seating will consist of approximately 1-2 picnic tables and 1-3 bistro tables and chairs and/or an assortment of lawn chairs.

* 10.243.22 All necessary public and private utility infrastructure and services will be available and adequate to serve the proposed use.

No alteration to public and/or private utility infrastructure is required as part of the proposed use.

* 10.243.23 The site and surrounding streets will have adequate vehicular and pedestrian infrastructure to serve the proposed use consistent with the City's Master Plan.

There will be no impact to vehicular or pedestrian infrastructure as part of the proposed use of the space.

* 10.243.24 The proposed structures, uses, or activities will not have significant adverse impacts on abutting and surrounding properties on account of traffic, noise, odors, vibrations, dust, fumes, hours of operation, and exterior lighting and glare.

Sufficient parking is available at the business address. Additional parking is located in nearby lots during business hours. No outdoor speakers or live music will be offered on the patio. Hours of operation are between 10am-8pm.

* 10.243.25 The proposed structures and uses will not have significant adverse impacts on natural or scenic resources surrounding the site, including wetlands, floodplains, and significant wildlife habitat.

No wetlands, floodplains, wildlife habitats, or other natural or scenic resources are present at the site of the proposed patio.

* 10.243.26 The proposed use will not cause or contribute to a significant decline in property values of adjacent properties.

The proposed patio will not cause or contribute to a significant decline in property value of the adjacent properties.

## Photo Log



Photo 1: Existing gravel patio with concrete walkway and landscaped areas.


Photo 2: Existing gravel patio and landscaped area. The proposed plan includes a) removing the arborvitae (center of the photo) and overgrown weeds; b) laying gravel over the area with grass and overgrown weeds; and c) leaving the mulched area, lilies, and maple tree.


Photo 3: Rear of the building at 125 Brewery Lane with existing gravel patio, landscaped area, and overgrown weeds. The proposed plan includes removing the arborvitae (left) and overgrown weeds (right) and laying gravel over the area with grass and overgrown weeds. The granite curb demarcating the current grass and gravel patio will be removed.

July 8, 2024

Rick Chellman, Chairman
City of Portsmouth Planning Board
City of Portsmouth Municipal Complex
1 Junkins Avenue
Portsmouth, New Hampshire 03801

## Re: Application for Preliminary/Conceptual Review <br> Assessor's Map 222, Lot 11 <br> 550 Sagamore Avenue <br> Altus Project No. 5591

Dear Mr. Chellman,

On behalf of Green and Company (Green), Altus Engineering, LLC (Altus) is pleased to submit an application for the Planning Board Conceptual/Preliminary Review. Green has an agreement to purchase the property located at 550 Sagamore Avenue from The Frances E. Mouflouze Revocable Trust of 2015. They are proposing to construct a new subdivision roadway to access three new residential house lots.

Enclosed is the Existing Conditions Survey Plan and the Conceptual Subdivision Plan for discussion at the July 19, 2024 Planning Board meeting.

There is a single residence on the 1.44 -acre parcel. The parcel lies within the Single Resident B Zoning District which has a minimum $15,000 \mathrm{SF}$ lot size requirement. By area, the parcel can support 4-homes. Multiple dwelling units on a lot is not permitted in the zone. The current Owner applied for variances on two occasions to allow 4 then 3 dwelling units on the parcel without subdivision with the concept to preserve and protect the majority of the forested area. The Board of Adjustment denied the variances in both scenarios leaving the only viable alternative to develop the parcel as a conventional subdivision.

The majority of the parcel is forested with some ledge outcrops. There is a small wetland system along the northerly boundary that is not a vernal pool and does not require any buffer protection. Enclosed is documentation from Joseph Noel, Wetlands Scientist, confirming the wetland status.

We are proposing to construct a private 40 -foot wide with a 20 -foot-wide paved surface roadway to access the lots. All of the lots will be accessed from the new private street. A homeowner's
association will maintain the roadway and stormwater management system. The lots will be serviced with municipal water and sewer.

On June $11^{\text {th }}$, we presented the proposal to the Technical Advisory Committee to obtain their feedback and input. They gave us guidance on the technical aspects of the design should we decide to proceed with permitting.

We look forward to getting input from the Board. Please feel free to call or email me directly should you have any questions or need any additional information in advance of the meeting.

Sincerely,

## ALTUS ENGINEERING, LLC



## Enclosures

eCopy: Michael Green<br>Jenna Green

wde/5591.00 7-8-24 cvr ltr.docx

## Letter of Authorization

I/We, Ted W Alex and Patricia Cameron trustees of The Frances E Mouflouze Revocable Trust of $2015 \mathrm{u} / \mathrm{d} / \mathrm{t}$ dated September 24, 2015, as owner of certain real property situated in Portsmouth, NH further described $1.48+/$-acres of land with single family home located at 550 Sagamore Avenue with $140^{\prime}$ of frontage on Sagamore Avenue, as shown in Tax Assessors Map 222 Lot 11 and further defined by legal description found at the Rockingham Countr Registry of Deeds Book 5660 Page 2227 dated October $7^{\text {th }}$, 2015. (hereinafter, "Property") do hereby authorize Green \& Company Building and Development Corp. and its Affiliates, Agents, Assigns and Engineers to act on my/our behalf and to appear before the zoning board of adjustment and/or the planning board of said city/town and/or any of its boards or commissions, in my/our behalf for the purpose of seeking any regulatory relief that may be requested by the person $1 /$ we have above authorized, including variances, special exceptions, dimensional waivers, site plan approval, lot line adjustment approval and subdivision approval, hereby ratifying any actions taken by him/her/them to obtain any such relief. 1/We authorize Green \& Company Building and Development Corp. and its Affiliates, Agents, Assigns and Engineers to act in my/our behalf in all matters concerning the development and approval process, without limitation, for the above stated property, to include any required signatures.

I/We shall cooperate fully with Green \& Company Building and Development Corp. and its Affiliates, Agents, Assigns and Engineers in seeking timely public approvals and for the completion of the sale contemplated herein. I/We agree to use my/our good faith efforts to provide any assistance $1 /$ we reasonably can to Green \& Company Building and Development Corp. and its Affiliates, Agents, Assigns and Engineers throughout the development process, including but not limited to signing permit applications as needed.


Witness


Witness


Owner:


5/29/2024
Date

5/29/2024
Date

# JOSEPH W. NOEL <br> P.O. BOX 174 <br> SOUTH BERWICK, MAINE 03908 

(207) 384-5587

CERTIFIED SOIL SCIENTIST $\quad * \quad$ WETLAND SCIENTIST $\quad$ _ LICENSED SITE EVALUATOR

June 15, 2024

Mr. Eric D. Weinrieb, P.E.
Altus Engineering
133 Court Street
Portsmouth, New Hampshire 03801
RE: Wetland Delineation, 550 Sagamore Avenue, Portsmouth, New Hampshire, JWN \#24-58
Dear Eric:
On May 10, 2024, an on-site was made to the above-referenced property (per your request). The purpose was to determine if there were any areas on the lot that would classify as a wetland. A residential home is situated near Sagamore Avenue with the eastern side of the lot being wooded with sporadic bedrock outcrops. One small isolated basin, centrally located on the northern property line did qualify as a welland. Six sequentially numbered pink and black striped flags (labelled EOW1 thru EOW6) were placed along the wetland-upland boundary.

To determine the wetland boundary, the methodologies in the U.S. Army Corps of Engineers document Corps of Engineers Wetlands Delineation Manual (1987) along with the required Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Northcentral and Northeast Region, (Version 2.0) were used. Wetlands were identified based on soils, vegetation, and hydrology. Except in special cases, all three factors (hydric soils, hydrophytic vegetation, and wetland hydrology) must be present for an area to classify as wetland.

The wetland area was not ponded with surface water on the day of the site visit. There was evidence of occasional surface water (i.e., water marks) along with blackened leaves and orientated pine needles on the soil surface. The lack of surface water eliminated this area, in my opinion, from being a potential vernal pool. There appears to be a limited watershed that contributes run-off to this basin. Also, there is some evidence that the abutting lot has added fill material that may have blocked the natural runoff from this basin to downslope areas. To be a viable vernal pool surface water needs to be present in the early spring and the hydroperiod needs to be long enough for the breeding amphibians to complete the early life cycle to a juvenile age. This spring there were a number of rain events that filled most vernal pools and this basin did not contain water on May 10, 2024.

This basin does classify as a wetland based on: the poorly drained soil conditions (i.e., hydric soils), evidence of soil saturation and occasional ponding (evidence of wetland hydrology), and
while vegetation was limited in the basin, a few red maples (Acer rubrum) were observed (i.e., hydrophytic vegetation).

I hope this letter is sufficient for your planning purposes. Please do not hesitate to call with any questions or concerns.

Sincerely,
Gornw. Mieil
Joseph W. Noel
NH Certified Soil Scientist \#017
NH Certified Wetland Scientist \#086




Bosen © Associates
ATTORNEYS AT LAW

John K. Bosen<br>Admitted in NH \& MA<br>Christopher P. Mulligan<br>Admitted in NH \& ME<br>Mr. Rick Chellman, Chair<br>City of Portsmouth Planning Board<br>Molly C. Ferrara<br>1 Junkins Avenue<br>Portsmouth, NH 03801<br>Austin Mikolaities<br>Admitted in NH<br>Re: Preliminary Conceptual Consultation / Design Review Completion 361 Hanover Street<br>Bernard W. Pelech<br>1949-2021<br>\section*{Dear Chairman Chellman:}

On behalf of 361 Hanover Steam Factory, LLC, we are pleased to submit one (1) set of hard copies and one electronic file of the following information to support a second request for a Preliminary Conceptual Consultation and a request to complete the Design Review process for the above referenced project:

- Design Review Plans, dated July 3, 2024

Since the initial Preliminary Conceptual Consultation, we have listened to the comments and concerns of this Board and the abutters and redesigned the site to include four (4) buildings in order to allow more light and air into property and give it an overall neighborhood look and feel. As a result, we believe a second Preliminary Conceptual Consultation is warranted. Also, as the completion of the Design Review process included a Public Hearing and site walk we hereby request that these plans be the subject of this process.

The Site Plan depicts Building A as an 18,082 S.F, 4 story building with a Penthouse. It will have 34 dwelling units and 3 workforce housing units. Building $B$ is a 3,116 S.F. two ( $21 / 2$ ) story building with 4 dwelling units, Building $C$ is a 2,280 two (2) story building with 2 dwelling units (Duplex) and Building D is a 4,320 S.F. three ( $31 / 2$ ) story building with 8 dwelling units. The project will also provide a total of 69 parking spaces.

The applicant respectfully requests to be placed on the July 18, 2024 Planning Board meeting agenda. If you have any questions or concerns, please do not hesitate to call or email me at jbosen@bosenandassociates.com.
cc: client


John Chagnon
Nicholas Cracknell

# PORTSMOUTH STEAM FACTORY PROJECT 

## PRELIMINARY CONCEPTUAL REVIEW - Alternative cup plan -



# 361 HANOVER STREET, PORTSMOUTH, NH HAMPSHIRE DEVELOPMENT CORPORATION 

July $\mathbf{1 8}^{\text {TH }} 2024$

To: Rick Chellman, Planning Board Chair
Re: Preliminary Conceptual Review - Building and Site Design Revisions for 361 Hanover St.

## Purpose

The purpose of this submission for Preliminary Conceptual Review is three-fold. First, we would like to present an alternative building and site plan from the so-called "as-of-right" plan that was recently approved for Design Review (see Figure 1).


Figure 1 - Proposed "As-of-Right Plan" showing a large Mixed-Use Building fronting on Hanover St.
As a response to your feedback, we developed an alternative building and site plan - "the CUP Plan" that we believe better addresses your comments, suggestions, and the many issues and concerns expressed by members of the public during the Preliminary Conceptual and Design Review meetings.


Figure 2 - Proposed "CUP Plan" showing three traditionally-designed buildings along Hanover St.

Secondly, we would like to receive input and feedback on our proposed CUP Plan in order to make any final design adjustments prior to filing a formal Site Plan Application. Finally, realizing that we will require zoning relief to implement the CUP Plan, we would like to request the Board consider informally supporting our alternative CUP plan prior to us filing a variance application in August.

## Site Plan Elements

As discussed during the Design Review phase of the project, the site planning issues of parking, loading, solid waste, deliveries, drainage, utilities, lighting, landscaping, off-site improvements, and the location of all mechanical equipment will all be formally addressed when a site plan is updated and reviewed by both the Technical Advisory Committee and the Planning Board. We would refer the Board to our submission packet and project narrative, dated April $4^{\text {th }}, 2002$, and on file with the Planning Department for any questions pertaining to those issues.

## Issues Raised during Design Review

As you recall, as part of the public hearing within the Design Review process, several core issues of concern were expressed from both Planning Board members, neighbors, and members of the general public. The core issues included the height, scale, volume, and massing of the proposed buildings. Additionally, there were also concerns about the prospect of ground-floor commercial uses and their potential impact on spill-over street parking, lighting, and noise. Other issues included emergency access concerns via the proposed tunnel, parking and loading areas, and whether the proposed buildings and zoning requirements were consistent with the North End Vision Plan. Other issues of concern related to pedestrian access to Foundry Place, improving on-site drainage, and consideration for a better building design to reflect the historic quality and character of the smaller historic structures within the surrounding neighborhood.

## Our Preliminary Response

As discussed during the Design Review process, we listened to Board and public feedback and have reevaluated the proposed building and site design and re-examined the density, dimensional, and the architectural character of the surrounding neighborhood. Additionally, we have revisited the existing zoning regulations and the goals and objectives of the North End Vision Plan in order to refine the design to better reflect the goals of both the Board and the surrounding neighborhood. In doing so, we reconsidered the five (5) following elements as follows: 1) the goals and objectives of the North End Vision Plan; 2) the existing neighborhood context (density and design); 3) the surrounding land use pattern (especially on the ground-floor); 4) the pedestrian circulation; and, 5) the building placement, volume, and design.

## 1. North End Vision Plan

As listed in Figure 3, the goals and objectives of the North End Vision Plan were focused on generating building and site designs that were both respectful and sensitive to the surrounding context. In particular, the buildings were intended to step up or down in transitional areas like the property at 361 Hanover Street. This stepping element is exactly why the North End Overlay District does not carry over to the parking lot portion of the property along Hanover Street. Additionally, the Vision Plan encourages ground-floor commercial uses to active the sidewalk and enhance the
pedestrian experience. Thus, the Downtown Overlay District (DOD) was extended into much of the North End. Streets were also encouraged to support multi-modal traffic with an emphasis of nonvehicular use of new streets and driveways. Finally, to achieve more vibrant, walkable streets and sidewalks, the zoning also includes incentives for public or civic spaces like shared streets, wide public sidewalks, or public park areas.

Despite the zoning for the North End allowing taller and larger buildings than the surrounding context and mandating ground-floor commercial uses, we developed an alternative plan - the "CUP Plan" - that we believe better reflects the goals and objectives of the North End Vision Plan. The CUP Plan seeks to step the buildings down from the taller buildings along Hill and Hanover Streets to the much shorter and smaller building types along Rock Street.

## PLAN PORTSMOUTH

## NORTH END PRELIMINARY VISION PLAN



Figure 3 - North End Vision Plan

## 2. Neighborhood Context

Project density can be defined in a number of ways including, but not limited to, the number of dwelling units, or the height, volume, footprint, or massing of the buildings. When looking at density as a function of the number of dwelling units, Figure 4 illustrates the transition from the highdensity developments and land use pattern within the character-district zoning along Foundry Place and Hill Street in the North End with the lower density traditional neighborhoods along Rock or Sudbury Street in the abutting Islington Creek Neighborhood.


Figure 4 - Existing Neighborhood Density (Estimated Units / Acre)
When looking at the existing and allowed densities in terms of building height, scale, and volume, the variation within the surrounding neighborhood is even more dramatic. For example, within the CD5, buildings are permitted to have footprints as large as $20,000 \mathrm{SF}$ and heights between 40-60' depending on overlay districts. In contrast, new buildings in the abutting CD4-L1 are restricted to much smaller footprints of 2,500 SF (about the size of the Pearl Street Church) and heights of 40-42' (again about the height of the Pearl Street Church). Interestingly, like the character-based zoning, the abutting General Residence C District allows for new buildings to be between 35-43' in height depending on whether parking is provided within the ground-floor of the building.

Perhaps the biggest difference between the GRC, CD4-L1, and the CD5 is the coverage and open space requirements as buildings in the CD5 are allowed to occupy $95 \%$ of the lot area and thus, do not require significant open space areas whereas the GRC and CD4-L1 require between $40 \%$ and $65 \%$ of the lot area to be remain undeveloped for parking or open space.

Coupled with the size of the footprints allowed in the CD5, the high coverage allowance promotes and encourage buildings that are significantly larger than those permitted in the abutting GRC District. Importantly, the allowable density (as reflected by the allowable footprints and building heights) transitions from a high density along Foundry Place and Hill Street (the CD5 district with large footprints and a 50-60' height limitation) to a moderate density along Hanover Street (the CD4-L1 district with smaller footprints and a $40^{\prime}$ height limitation) and to a much lower density along Tanner, Pearl, and Parker Streets (the GRC district with small footprints and a 35-43' height limitation) before increasing to a moderate density allows along Islington Street (the CD4-L2). Thus,
our evaluation of the surrounding context suggests that we consider reconfiguring the density and volume of the so-called "As-of-Right Plan" to substantially reduce the building height, volume, and footprints along Hanover Street.

## 3. Ground-Floor Commercial Uses

Although the Downtown Overlay District (DOD) includes the total land area of 361 Hanover Street it is important to acknowledge that there are no other properties fronting on Hanover Street included in the DOD. Within Downtown Portsmouth, DOD requires ground-floor commercial uses with the intention to activate the street edge and enhance the pedestrian experience.


Figure 5 - Existing Streetscape showing Residential Land Use Pattern on Hanover St.

Unfortunately, in this particular area along Hanover Street Figure 6 shows that only 293 Hanover Street is designed for and used as a commercial use. Moreover, except for the non-conforming Peral Street Church property, all other nearby properties on Hanover Street and the intersecting streets are all residential uses (see Figure 5).


Figure 6-Commercial Use at 293 Hanover Street
To the east, Bridge Street is essentially the edge of the downtown commercial district and Islington Street - a mixed-use commercial corridor linking the downtown to the West End - provides intermittent commercial uses that support the adjacent neighborhoods (see Figure 7).


Figure 7 - Commercial Use at 63 Islington Street

Thus, along with the question of the economic viability of this location, the concerns and compatibility issues with the surrounding residential neighborhood led us to continue to evaluate the more suitable ground-floor use of residential dwelling units; consistent with the existing neighborhood context.

## 4. Pedestrian Circulation

During the Design Review process suggestions were made to consider and provide for pedestrian connections between the proposed project and the public parking garage on Foundry Place. In review of the serious physical challenges of opening the City's existing retaining wall along Foundry Place to introduce a stairway to Foundry Place we evaluated other less-challenging options. In particular, we reviewed the approved site plans for the abutting 53 unit project at 89 Foundry Place. The approved plans show a $6-8$ ' wide public pedestrian accessway connecting the entrance of the public parking garage on Foundry Place with Hill Street (see Figure 8 below). The entrance to the public parking garage is less than 300 feet from the proposed multi-modal way that is proposed within the project. Thus, visitors and any spillover parking can utilize this pedestrian passageway to easily access the Foundry Place Public Parking Garage.


Figure 8 - Pedestrian Connector at 89 Foundry Place

## 5. Building Design

Some Board members and most members of the public suggested we reevaluate the proposed architectural style of the proposed building(s) along Hanover Street with a clear preference for buildings that are more consistent with the quality and historic character of the surrounding historic buildings. More specifically, suggestions were made for smaller building footprints, reduced height and volume, and the application of traditional building principles that would better reflect the historic architecture of the surrounding neighborhood.

## Alternative CUP Plan

## Overall Building and Site Design

The alternative CUP Plan seeks to address the core issues listed above by adhering to the goals and objectives of the North End Vision Plan. Moreover, it also seeks to redevelop the property by employing a context-sensitive approach that steps down and transitions from a high-density newer development along Foundry Place and Hill Street to a moderate density along Hanover Street and lower density along Rock and Sudbury Streets.


Figure 9 - Proposed "As-of-Right Plan" showing a large Mixed-Use Building fronting on Hanover St.
Figure 9 illustrates how the previously proposed $31 / 2$ story mansard building along Hanover Street occupies the full street frontage along Hanover Street and overpowers some of the smaller abutting buildings. In contrast, Figure 10 illustrates the alternative CUP Plan where the larger building has been broken into three separate buildings with reduced height and volume to better align with the lower density context of the western side of the site.

As we discussed within the Design Review process, the CUP Plan also proposes to increase the height of the Kearsarge Building along Foundry Place - in a historically sensitive manner - to reestablish the volume, height, and historic character of the building and support the transfer of development rights from Hanover Street to Foundry Place as intended in the North End Vision Plan and the Character-Based Zoning.


Figure 10 - Proposed Lower-Scale, Traditionally-Designed Buildings along Hanover Street

## Ground-Floor Residential Uses

Given the questions of economic viability and the potential for adverse impacts on the surrounding neighborhood (i.e. spillover parking, noise, and light pollution), the CUP Plan proposes a residential ground-floor use in all four buildings.

## Building Placement \& Open Space

As shown in Figure 11, there is parking available on-site to support up to 48 dwelling units within the four (4) proposed buildings.


Figure 11 - Alternative CUP Plan showing Proposed Buildings and Driveways and Open Space

## Building Design

As shown in Figures 12-15, all four buildings have been redesigned to be more consistent with the historic character of the surrounding neighborhood. Understanding this property is located outside the Historic District, we have intentionally redesigned these buildings to reference the historic elements in the surrounding context versus the more contemporary buildings being constructed along Foundry Place and Deer Street in the North End.


Figure 12 - Building A: 4½-Story "Apartment" Building (the Kearsarge Building)


Figure 13 - Building B: 3-Story "Rowhouse" Building


Figure 14 - Building C: 3-Story "Duplex" Building


Figure 15 - Building D: 3½-Story "Apartment" Building

## Community Space

As required under the CUP, at least $10 \%(3,853 \mathrm{SF}+/-)$ of the property would be deeded as Community Space. As shown on Figure 16, the proposed Community Space would be a 4,500 +/- SF Shared MultiModal Way connecting Rock Street to Hill Street. The shared street would include formal landscaping, lighting and street furniture.


Figure 16 - Proposed Community Space - Multi-Modal Way

## Workforce Housing

As required under the CUP, at least 10\% of the proposed dwelling units would be deed restricted as rental Workforce Housing Units and be rented to a household with an income of no more than $60 \%$ of the median family income for a 3-person household. Such units will be at least 600 SF in GFA and are proposed to be located within the $1^{\text {st }}$ and $2^{\text {nd }}$ floor of Building A (the only building located within the North End Incentive Overlay District).

## Zoning Relief

Table 1 shows how the proposed four (4) buildings align with the development standards for the CD5.

| ZONING DEVELOPMENT STANDARD - CUP PLAN |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CD5: CHARACTER DISTRICT 5, DOD: DOWNTOWN OVERLAY DISTRICT |  |  |  |  |  |  |
|  | REQUIRED | ExISting | PROPOSED - Building A | PROPOSED - Building B | PROPOSED - Building C | PROPOSED - Building D |
| Height | 2-3 stories 40' | 2 Stories/ 18' + /- | 4 stories w/ penthouse 52' | 3 stories / 36' | 3 stories / 36' | $31 / 2$ stories / 40' |
| Penthouses | may exceed bldg height by $2^{\prime}$ | N/A | Yes (75\% Habitable Space /8' Setback) | N/A | N/A | N/A |
| Roof appurtenance | may exceed bldg height by $10^{\prime}$ | <10' | <10' | No | No | <10' |
| Façade Types |  | N/A | N/A | N/A | N/A | N/A |
| Building Types | commercial, live-work, mixed use, flex space \& community. | Commerical | Apartment | Rowhouse | Duplex | Apartment |
| Front (principle) max | 5 | 99' | 99' | $0^{\prime}$ | $5{ }^{\prime}$ | $2^{\prime}$ |
| Front (secondary) max | 5 | $0^{\prime}$ | $\mathrm{O}^{\prime}$ | 2' | N/A | N/A |
| Side | NR | NR | NR | NR | NR | NR |
| Rear yard | 5' | $0^{\prime}$ | $0^{\prime}$ | >5' | >5' | >5' |
| Front lotline buildout | 80\% min | 100\% | 100\% | 80\% | 80\% | 80\% |
| Lot area (sf) | NR | N/A | N/A | N/A | N/A | N/A |
| LOT area per dwelling | NR | N/A | N/A | N/A | N/A | N/A |
| Building coverage, maximum | 95\% | 38\% | 47\% | 8\% | 6\% | 11.0\% |
| Maximum building footprint | 20,000 | 14,808 | 18,082 | 3,116 | 2,280 | 4,320 |
| Ground floor area per use, max | 15,000 | 14,808 | <15,000 | 3,116 | 2,280 | 4,320 |
| Open space, minimum | 5\% | <5\% | >5\% | >5\% | >5\% | >5\% |
| Permitted uses |  | Commercial | Residential | Residential | Residential | Residential |
| Block length, max (ft) | 225 | 205' | 205' | 82' | 40' | 72' |
| Façade modulation length, max $(\mathrm{ft})$ | 100 | 205 | 205 | 82' | $40^{\prime}$ | 72' |
| Entrance spacing, max (ft) | 50 | >50' | 50 | $20^{\prime}$ | $20^{\prime}$ | <50' |
| Floor height above sidewalk, max | $36^{\prime \prime}$ | $0^{\prime}$ | $0^{\prime}$ | $24^{\prime \prime}$ | $24^{\prime \prime}$ | $24^{\prime}$ |
| Ground story height, min | $12^{\prime}$ | 10' | $10^{\prime}$ | 12' | 12' | 12' |
| Second story height, min | $10^{\prime}$ | 10' | $10.5{ }^{\prime}$ | 10.5' | 10.5 | 10.5' |
| Glazing, shopfront, min | 70\% | N/A | N/A | N/A | N/A | N/A |
| Glazing, other | 20\%-50\% | >20\% | >20\% | >20\% | >20\% | >20\% |
| Roof types | flat, gable, hip, gambrel, mansard | Flat | Flat | Hip | Hip | Mansard |
| Community Space | >10\% or $3,852 \mathrm{SF}$ (1,926 SF as pervious) | N/A | 4,250 SF +/-( $12 \%$ ) | N/A | N/A | N/A |
| Wokforce Housing Units | If rental units $=10 \%$ of total units. $10 \%$ of $36=3.4$ Units $=3$ Units) | N/A | 3 Workforce Housing Units <br> Floor 1 = 1 Unit <br> Floor 2 = 2 Units | N/A | N/A | N/A |

Table 1 -Zoning Table showing Development Standards for each Building
As illustrated with the shaded boxes in Table 1, to support the CUP Plan, zoning relief from the Board of Adjustment (BOA) will be necessary. The following variances are required to permit and construct the plan:

1. To allow the ground-floor use of the buildings to be residential.
2. To allow for an "apartment", "rowhouse", and "duplex" building type in the CD5.
3. To allow the ground floor height of Building A (the Kearsarge Building) to be 10 ' versus 12 '.
4. To allow the penthouse level of Building A (the Kearsarge Building) to exceed $50 \%$ of the total floor area of the floor below and have a setback of 8 ' from the roof edge.

## Summary

After consideration of the many valuable comments, issues, concerns, and suggestions provided by the Board and members of the public within the Design Review process for the "As-of-Right Plan", we believe the proposed CUP Plan meets the goals and objectives of the North End Vision Plan and, subject to the granting of zoning relief from the Board of Adjustment, exceeds the findings and criteria needed for approval of a CUP.

In closing, we would respectfully request the Board consider an informal vote in support for the CUP Plan. Doing so would not only acknowledge our collective efforts to address the concerns raised during the Design Review process but also "right-size" this development and demonstrate our common goals to make this project a success for urban infill and redevelopment in downtown Portsmouth. Moreover, it would also be likely to have a positive effect on the BOA's review and provide them a deeper appreciation and understanding of how these design changes were collaboratively developed. In the end, we believe this CUP Plan better aligns with the Board's and the public's strong desire for a more balanced, respectful, and context-sensitive, redevelopment of this property; one that also includes Community Space and Workforce Housing.

## PROPOSED DEVELOPMENT

OWNER／APPLICANT 361 HANOVER STEAM 41 INDUSTRIAL DRIVE UNIT 20 EXETER，NH 03833
TEL．（603） $235-5475$

CIVIL ENGINEER／LAND SURVEYOR： AMBIT ENGINEERING，INC．
200 GRIFFIN ROAD 200 GRIFIN ROAD，UNIT 3
PORTSMOUTH N． TEL．（603）430－9282 ARCHITECT： SCOTT BROWN 29 WATER STREET，SUITE 209
NEWBURYPORT，MA 01950 NEWBURYPORT，MA－ 19950
TEL．（978） $465-3535$ PLANNING CONSULTANT： NICHOLAS CRACKNELL
TEL．（978）270－4789

LAND USE ATTORNEY： BOSEN \＆ASSOCIATES 266 MIDDLE STREET
PORTSMOUTH，N．H． 03801 PORESMOUTH．N．（603） $427-5500$


INDEX OF SHEETS


approved by the portsmouth planning board
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361 HANOVER STREET
PORTSMOUTH，NEW HAMPSHIRE DESIGN REVIEW PLANS

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CABLE： COMSASMMERCE WAY
PORTSMOUTH，N．H． 0380 Tel．（603） $679-5695$（ $\times 1037$ ）

UTILITY CONTACTS

## ELECTRIC：

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Tel．（ 603 ） 436 －7708，Ext． 555.5678
ATTN：MICAAEL BUSBY，P．E．（MANAGER）
 680 PEVERLY HILL ROAD
PORTSMOUHH，N．H． 0380


NATURAL GAS：
 Tell（603）294－5144
ATTN：DAVE BEAULEU
 COMMUNICATINSS：
FARPOINT COMMUN：
JOE CONSIONS
COMIC JOE CONSIDNE
157 GRENEND ROAD
GREENAND，A．H． 03840 GREENLAND，N．H－H 03840
Tel．（603） $427-5525$

DESIGN APPLICATION PLAN PROPOSED DEVELOPMENT 361 HANOVER STREET PORTSMOUTH，N．H．








[^0]:    No glare found

[^1]:    *Currently, we don't have a walkway extending from street to studio entrance - however, if granted a Conditional Use Permit, we will take necessary steps to have a porous brick walkway installed.

