PLANNING BOARD PORTSMOUTH, NEW HAMPSHIRE

EILEEN DONDERO FOLEY COUNCIL CHAMBERS CITY HALL, MUNICIPAL COMPLEX, 1 JUNKINS AVENUE

7:00 PM Public Hearings begin

July 18, 2024

<u>AGENDA</u>

REGULAR MEETING 7:00pm

I. APPROVAL OF MINUTES

A. Approval of the June 20, 2024 meeting minutes.

II. PUBLIC HEARINGS – NEW BUSINESS

The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.

- A. REQUEST TO POSTPONE The request of Perkins Kwoka Joint Revocable Trust (Owner), for property located at 224 Broad Street, Unit 3 is requesting a Wetland Conditional Use Permit from Section 10.1017.50 for the replacement and expansion of an existing 192 s.f. sunroom and the demolition of a 286 s.f. rear deck, with new construction proposed for an addition of 384 s.f. to the existing sunroom, a new 367.5 s.f. rear deck and regrading of a portion of the site for the installation of a retaining wall and underdrain for stormwater control. The applicant is proposing to remove 491 s.f. of existing pavers and asphalt to be replaced with 401 s.f. of new pavers. This proposal includes the removal of the existing lawn to be replaced with a micro-clover seed mix, a planting plan, and a stone drip edge. Said property is located on Assessor Map 131 Lot 13-3 and lies within the General Residence A (GRA) District. REQUEST TO POSTPONE (LU-23-179)
- **B.** The request of Lonza Biologics (Owner), for property located at 5 Technology Way (*Formerly 70 Corporate Drive*) requesting Amended Site Plan approval for the addition of Phase Photovoltaic Cell (PV) Solar canopies over the previously approved temporary surface parking lot with associated utility infrastructure improvements. Said property is located on Assessor Map 305 Lot 6 and lies within the Airport Business (ABC) District. (LU-23-108)

- C. The request of **The City of Portsmouth (Owner)**, for property located at **50 Andrew Jarvis Drive** requesting a Wetland Conditional Use Permit from Section 10.1017.50 of the Ordinance for the conversion of an existing practice field into a baseball and softball practice field which includes adding an 800 s.f. batting cage, a 40' wide backstop with posts driven into the ground, and the removal of approximately 800 s.f. of existing grass for replacement with an infield mix of clay, sand and silt. All of this work will occur within the 100' wetland buffer. Said property is located on Assessor Map 229 Lot 3 and lies within the Municipal (M) District. (LU-24-50)
- D. The request of The City of Portsmouth (Owner), for property located at 0 Maplewood Avenue requesting an after the fact Wetland Conditional Use Permit from Section 10.1017.50 of the Ordinance due to the emergency authorization issued by NHDES on May 16, 2024 for repair of the stone wall alongside the North Cemetery. This application is for the restoration and repair of the wall in-kind which includes installation of new stone, installing non-woven geotextile along the eroded bank, importing structural backfill, and loam and seeding the disturbed areas once finished. Said property is located on Assessor Map 124 Lot 2 and lies within the Municipal (M) District. (LU-24-102)
- E. The request of Rosania RR & KL Revocable Trust (Owner), for property located at 32 Boss Avenue requesting a Conditional Use Permit in accordance with Section 10.440, Use 19.22 for a Home Occupation 2. Said property is located on Assessor Map 153 Lot 5 and lies within the Single Residence B (SRB) District. (LU-24-117)
- F. The request of Mark E. and Janet Greenwood (Owners), for property located at 480 Dennett Street requesting a Conditional Use Permit from Section 10.814 for a Detached Accessory Dwelling Unit (DADU) for the demolition of the existing garage and construction of a new DADU Said property is located on Assessor Map 160 Lot 26 and lies within the General Residence A (GRA) District. (LU-24-120)
- G. The request of Portsmouth West End Development LLC (Owner), for property located at 125 Brewery Lane requesting a Conditional Use Permit in accordance with Section 10.440, Use 19.50 for an outdoor dining and drinking area as an accessory use. Said property is located on Assessor Map 154 Lot 2 and lies within the Character District 4-W (CD-4W) District. (LU-24-108)

III. PRELIMINARY CONCEPTUAL CONSULTATION

A. The request of Frances E. Mouflouze Revocable Trust of 2015 (Owner), for property located at 550 Sagamore Avenue requesting preliminary Conceptual Consultation for a subdivision of one lot into three conforming lots with associated site improvements. Said property is located on Assessor Map 222 Lot 11 and lies within the Single Residence B (SRB) District. (LUPD-24-5)

B. 361 Hanover Steam Factory, LLC (Owner), for property located at **361 Hanover Street**, requesting Preliminary Conceptual Consultation for the construction of three residential buildings along Hanover Street and add a fourth story with a penthouse to the existing 361 Hanover Street (Portsmouth Steam Factory) building for a total of 48 dwelling units including 3 workforce housing units and 69 parking spaces and associated community space. Said property is located on Assessor Map 138 Lot 63 and lies within the Character District 5 (CD5) Downtown Overlay and North End Overlay Districts. (LUPD-24-3)

IV. OTHER BUSINESS

- A. Chairman updates and discussion items
- B. Planning Board Rules and Procedures
- C. Board discussion of Regulatory Amendments, Master Plan Scope & other matters

V. ADJOURNMENT

*Members of the public also have the option to join this meeting over Zoom, a unique meeting ID and password will be provided once you register. To register, click on the link below or copy and paste this into your web browser:

https://us06web.zoom.us/webinar/register/WN AXjPB9HpRnaVn9EtKcrc2w



City of Portsmouth Planning Department 1 Junkins Ave, 3rd Floor Portsmouth, NH (603)610-7216

Memorandum

To: Planning Board

From: Peter Stith, AICP Planning Manager

Date: July 18, 2024

Re: Recommendations for the July 18, 2024 Planning Board Meeting

I. APPROVAL OF MINUTES

A. Approval of the June 20, 2024 meeting minutes.

Planning Department Recommendation

1) Board members should determine if the draft minutes include all relevant details for the decision-making process that occurred at the June 20, 2024 meeting and vote to approve meeting minutes with edits if needed.

The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.

A. The request of **Perkins Kwoka Joint Revocable Trust (Owner)**, for property located at **224 Broad Street, Unit 3** is requesting a Wetland Conditional Use Permit from Section 10.1017.50 for the replacement and expansion of an existing 192 s.f. sunroom and the demolition of a 286 s.f. rear deck, with new construction proposed for an addition of 384 s.f. to the existing sunroom, a new 367.5 s.f. rear deck and regrading of a portion of the site for the installation of a retaining wall and underdrain for stormwater control. The applicant is proposing to remove 491 s.f. of existing pavers and asphalt to be replaced with 401 s.f. of new pavers. This proposal includes the removal of the existing lawn to be replaced with a micro-clover seed mix, a planting plan, and a stone drip edge. Said property is located on Assessor Map 131Lot 13-3 and lies within the General Residence A (GRA) District. (LU-23-179)

Background

This application is requesting a Wetland Conditional Use Permit for the replacement and expansion of an existing 192 s.f. sunroom and the demolition of a 286 s.f. rear deck, with new construction proposed for an addition of 384 s.f. to the existing sunroom, a new 367.5 s.f. rear deck and regrading of a portion of the site for the installation of a retaining wall and underdrain for stormwater control. Additionally, the applicant is proposing to remove 491 s.f. of existing pavers and asphalt to be replaced with 401 s.f. of new pavers. This proposal includes the removal of the existing lawn to be replaced with a microclover seed mix, an extensive planting plan, and a stone drip edge surrounding the new sunroom and deck.



Staff Analysis – Wetland CUP

According to Article 10 Section 10.1017.50 the applicant must satisfy the following conditions for approval of this utility project.

1. The land is reasonably suited to the use activity or alteration.

The existing site has a steep slope which has been directing stormwater into and around the existing home, instead of towards the adjacent wetland. The proposed stormwater controls will involve some regrading of the lawn and the redirection of stormwater away from the home and through an underdrain to outlet underneath the expanded deck. This proposed deck will have $\frac{34}{7}$ spaced decking and will have crushed stone underneath for infiltration.

2. There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use, activity or alteration.

The majority of this property is within the 100 ft. buffer. The existing home is within the buffer and experiencing impacts of stormwater and ponding on the property. The applicant is proposing to address these issues with new stormwater controls and the addition of plantings, while working to reduce the impervious surface where possible.

3. There will be no adverse impact on the wetland functional values of the site

or surrounding properties.

The applicant is proposing to redirect stormwater directly through an underdrain and into a crushed stone area to slow infiltration. This should improve the flooding conditions for the home while directing the flow closer to the wetland with an option for infiltration into the soil.

4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals.

The applicant is proposing to maintain all existing trees and vegetation. In addition, the applicant will be improving the vegetation on site by planting a native micro-clover lawn in addition to planting beds and multiple trees and shrubs.

5. The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this section.

While the applicant is proposing an expansion of the home within the buffer, the expansion is occurring in the direction opposite of the wetland and will be compensated with a reduction in existing impervious. There are plans for overall improvements to the buffer including landscaping and reseeding the lawn with a micro-clover seed mix.

6. Any area within the vegetated buffer strip will be returned to a natural state to the extent feasible.

The applicant is proposing to stay completely outside of the 25' vegetated buffer.

Project Review, Decisions, and Recommendations

The applicant was before the Conservation Commission. See below for details.

Conservation Commission

The applicant was before the Conservation Commission at its regularly scheduled meeting of Wednesday, April 10, 2024 and the Commission voted unanimously to recommend approval as presented.

<u>Planning Department Recommendation</u> <u>Wetland Conditional Use Permit</u>

1) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact <u>as presented</u>.

(Alt.) Vote to find that the Conditional Use Permit Application meets the requirements

July 18, 2024 Planning Board Meeting

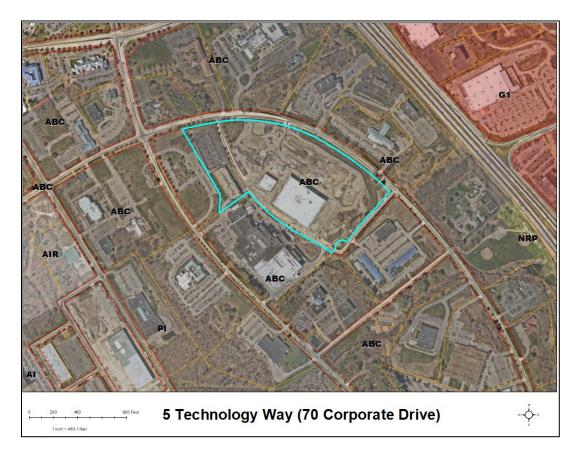
set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact <u>as</u> <u>amended</u>.

2.) Vote to grant the Conditional Use Permit as presented.

- The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
- B. The request of (Owner), for property located at 5 Technology Way (Formerly 70 Corporate Drive) requesting Amended Site Plan approval for the addition of Phase Photovoltaic Cell (PV) Solar canopies over the previously approved temporary surface parking lot with associated utility infrastructure improvements. Said property is located on Assessor Map 305 Lot 6 and lies within the Airport Business (ABC) District. (LU-23-108)

Background

This application is seeking Amended Site Plan approval to add Solar canopies over the proposed surface parking lot area. The addition of the solar canopies will require electrical modifications and will result in no impact to the drainage design for the project.



Project Review, Discussion, and Recommendations

The project was before the Technical Advisory Committee in June. See below for

details.

Technical Advisory Committee

The applicant was before TAC for at their regularly scheduled meeting of Tuesday, June 4, 2024 meeting. TAC voted to recommend that the Planning Board recommend approval to the Pease Development Authority as presented.

The amendments to RSA 676:3 with regards to adopting findings of fact for a project apply to local planning boards making decisions based on the municipality's regulations. Pease falls exclusively under RSA 12-G and the Pease Land Use Controls, therefore the requirement to vote on and adopt findings of fact do not apply for this application.

Planning Department Recommendation

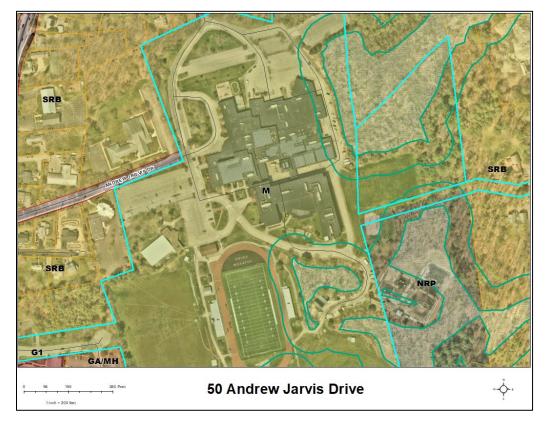
<u>Site Plan Approval</u>

1) Vote to recommend Amended Site Plan Approval to the PDA Board.

- The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
- C. The request of The City of Portsmouth (Owner), for property located at 50 Andrew Jarvis Drive requesting a Wetland Conditional Use Permit from Section 10.1017.50 of the Ordinance for the conversion of an existing practice field into a baseball and softball practice field which includes adding an 800 s.f. batting cage, a 40' wide backstop with posts driven into the ground, and the removal of approximately 800 s.f. of existing grass for replacement with an infield mix of clay, sand and silt. All of this work will occur within the 100' wetland buffer. Said property is located on Assessor Map 229 Lot 3 and lies within the Municipal (M) District. (LU-24-50)

Project Background

This application is for the conversion of an existing practice field into a more formalized baseball and softball practice field at the high school. The proposal includes the addition of an 800 s.f. batting cage, and a 40' wide backstop with posts driven into the ground, and the removal of approximately 800 s.f. of existing grass for replacement with an infield mix of clay, sand and silt. All of this work will occur within the 100' wetland buffer, with additional grass removal and infield mix placement outside the 100' buffer.



Staff Analysis – Wetland CUP

According to Article 10 Section 10.1017.50 the applicant must satisfy the following conditions for approval of this utility project.

1. The land is reasonably suited to the use activity or alteration.

This area is already heavily used as a recreation area for high school students and other recreation leagues. The addition of baseball/softball equipment will allow for more teams to utilize the space.

2. There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use, activity or alteration.

While there is an alternative location in this area that would create minimal disturbance and be outside the buffer, it would create a safety hazard due to its proximity to buildings and parking areas. The chosen location within the buffer is already used as a recreational field and it does not receive any harmful maintenance such as fertilizer or chemical use, only occasional mowing. The conversion to a baseball/softball field will not change how the buffer has been used historically.

3. There will be no adverse impact on the wetland functional values of the site or surrounding properties.

The infield mix proposed for the new field will be a permeable mix that should not have a noticeable impact on infiltration within this buffer area. The adjacent wetland is well forested and should not see an impact from this field conversion.

4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals.

The only vegetation proposed to be removed is a portion of existing grass lawn. This will be replaced with a permeable sand/silt/clay infield mix.

5. The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this section.

The proposal minimizes impacts to the buffer by proposing a permeable infield mix and minimal permanent equipment. On-site alternatives would require greater disturbance to areas that are not already used as recreational fields.

6. Any area within the vegetated buffer strip will be returned to a natural state to the extent feasible.

No work is proposed within the 25' vegetated buffer.

Project Review, Decisions, and Recommendations

The applicant was before the Conservation Commission. See below for details.

Conservation Commission

The applicant was before the Commission at its regularly scheduled meeting of Wednesday, June 12, 2024 and the Commission voted unanimously to recommend approval with the following conditions:

- 1. The updated Planning Board submission shall include the new batting cage location, the location of the new no-mow area, and the locations for wetland boundary placards.
- 2. In accordance with Section 10.1018.40 of the Zoning Ordinance, applicant shall permanently install wetland boundary markers, which may be purchased through the City of Portsmouth Planning & Sustainability Department. Markers are to be placed along the 25' vegetative buffer at 50-foot intervals and must be installed prior to the start of any construction.

The Conservation Commission recommended conditions have been satisfied or added to the staff recommendation.

<u>Planning Department Recommendation</u> <u>Wetland Conditional Use Permit</u>

1) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact <u>as presented</u>.

(Alt.) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact <u>as</u> <u>amended</u>.

2.) Vote to grant the Conditional Use Permit with the following conditions:

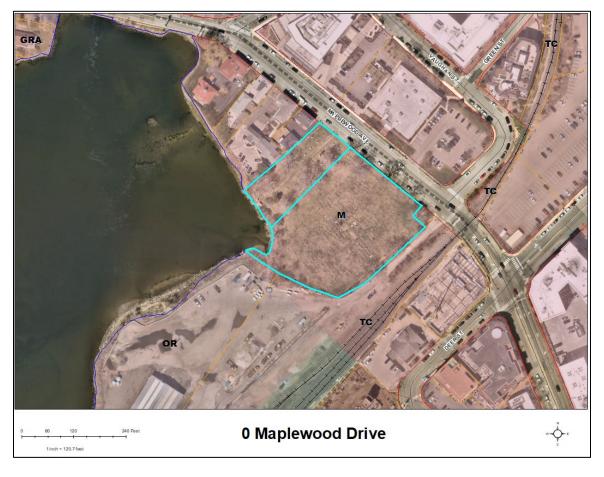
2.1) In accordance with Section 10.1018.40 of the Zoning Ordinance, applicant shall install permanent wetland boundary markers where applicable. In addition to the wetland boundary markers, an educational sign describing the project shall be installed near the restoration area and fencing should be utilized to keep disturbances such as dogs and geese from the area.

The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.

D. The request of The City of Portsmouth (Owner), for property located at 0 Maplewood Avenue requesting an after the fact Wetland Conditional Use Permit from Section 10.1017.50 of the Ordinance due to the emergency authorization issued by NHDES on May 16, 2024 for repair of the stone wall alongside the North Cemetery. This application is for the restoration and repair of the wall in-kind which includes installation of new stone, installing non-woven geotextile along the eroded bank, importing structural backfill, and loam and seeding the disturbed areas once finished. Said property is located on Assessor Map 124 Lot 2 and lies within the Municipal (M) District. (LU-24-102)

Project Background

The is an after the fact wetland conditional use permit due to the emergency authorization for this work. The stone wall alongside the North Cemetery is in danger of collapse due to significant erosion along the bank and this application is for the restoration and repair of the wall in-kind which includes installation of new stone, installing non-woven geotextile along the eroded bank, importing structural backfill, and loam and seeding the disturbed areas once finished. Recent inspections of this site concluded that any future storm events or heavy rains could cause significant damage and irreversible harm to the stability of this wall and the contents behind it. Due to this, the City of Portsmouth Department of Public Works has obtained an emergency authorization to perform this work from NHDES and is now seeking a wetland conditional use permit.



Staff Analysis – Wetland CUP

According to Article 10 Section 10.1017.50 the applicant must satisfy the following conditions for approval of this utility project.

1. The land is reasonably suited to the use activity or alteration.

This work is an in-kind repair job. The damaged wall is structurally integral to keeping the cemetery border and fill contained.

2. There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use, activity or alteration.

There is no alternative location to rebuild this wall in. The safety of the tomb and burials behind the wall is reliant on the structure of this wall and it must be fortified in order to prevent further erosion, or worse, collapse.

3. There will be no adverse impact on the wetland functional values of the site or surrounding properties.

The applicant used professional services to access the area and wall from the adjacent property, so as not to disturb the hallowed ground. This may have impacts on the pathway of any necessary construction vehicles. The applicant shall restore any disturbed soils with native wetland buffer conservation seed mix and monitor for establishment.

4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals.

The natural vegetated state was disturbed in order to get construction equipment onto the site. This area should be stabilized with erosion controls, along with the wall, and should be reseeded at the end of construction with a native wetland buffer conservation seed mix.

5. The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this section.

The alternatives to not repairing this wall would be allowing it, and the fill, and historic infrastructure to erode and/or slide into the North Mill Pond. The repair of this wall was an emergency repair.

6. Any area within the vegetated buffer strip will be returned to a natural state to the extent feasible.

All areas disturbed within the 25' vegetated buffer shall be reseeded at the end of construction with a native wetland buffer conservation seed mix.

Project Review, Decisions, and Recommendations

The applicant was before the Conservation Commission. See below for details.

Conservation Commission

The applicant was before the Conservation Commission at its regularly scheduled meeting of Wednesday, June 12, 2024 and the Commission unanimously voted to recommend approval with the following conditions:

- 1. Applicant shall monitor the success of reseeded areas to ensure stabilization. If stabilization is not successful within 30 days of seeding, the area will need to be reseeded.
- 2. Native wetland buffer shrub plantings shall be installed within the temporary accessway area in the Fall of 2024. This should be included in updated plan set for the Planning Board submission.

Planning Department Recommendation

Wetland Conditional Use Permit

1) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact <u>as presented</u>.

(Alt.) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact <u>as</u> <u>amended</u>.

- 2.) Vote to grant the Conditional Use Permit with the following conditions:
 - 2.1) Applicant shall monitor the success of reseeded areas to ensure stabilization. If stabilization is not successful within 30 days of seeding, the area will need to be reseeded.
 - 2.2) A planting plan of the temporary accessway area shall be submitted to the Planning & Sustainability Department for review and approval.

The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.

E. The request of Rosania RR & KL Revocable Trust (Owner), for property located at 32 Boss Avenue requesting a Conditional Use Permit in accordance with Section 10.440, Use 19.22 for a Home Occupation 2. Said property is located on Assessor Map 153 Lot 5 and lies within the Single Residence B (SRB) District. (LU-24-117)

Project Background

On June 17, 2024, the City Council adopted zoning amendments for home occupations. The amendments provide for client or general public visitation for a home occupation 1 and 2, which were previously not permitted. A home occupation 1 can have up to 2 clients at one time and is permitted in all zoning districts. A home occupation 2 can have up to 6 clients at one time and requires a Conditional Use Permit (CUP) in residential districts. The definitions are below for your reference. Both types of home occupations must comply with the requirements in main definition below:

Home occupation

An **office** or other **use** customarily conducted as an **accessory use** to a **dwelling**, complying with all the following standards:

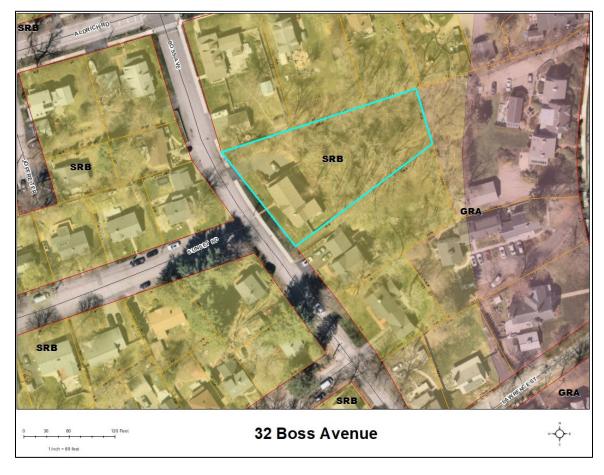
- (a) Conducted entirely within a dwelling or an existing accessory building, and with no change to the character of the dwelling or accessory building;
- (b) Maximum floor area of 300 square feet;
- (c) No outdoor storage of materials or products;
- (d) Outdoor parking of no more than one vehicle related to the home occupation;
- (e) No deliveries by vehicles with more than two axles.

Home occupation 1

A **home occupation** with no nonresident employees; no **sign** related to the business; no more than 2 client, vendor or general public visitations at one time; and no deliveries other than by regular postal service and no more than one package delivery service truck (e.g., FedEx, UPS, etc.) per day.

Home occupation 2

A **home occupation** with not more than one nonresident employee and not more than 6 client, vendor or general public visitations at one time.



Project Review, Decisions, and Recommendations

The applicant is requesting a CUP for a home occupation 2 in an existing studio that is less than the 300 square foot maximum floor area for the use. While the applicant shows ample parking in the existing driveway, only one space can be designated for the home occupation use.

Per Section 10.860 Hours of Operation, a home occupation 2 is limited to the hours of 8 am – 5 pm unless different hours are established under a special exception or conditional use permit. The applicant is requesting the ability to have up to 2 classes per week from 6 - 9 pm and one day on the weekend.

Planning Department Recommendation

Home Occupation 2 Conditional Use Permit

1) Vote to find that the Conditional Use Permit application meets the criteria set forth in Section 10.243.20 and to adopt the findings of fact <u>as presented.</u>

(Alt.) Vote to find that the Conditional Use Permit application meets the criteria set forth in Section 10.243.20 and to adopt the findings of fact <u>as amended and read into the record</u>.

2) Vote to approve the conditional use permit with the following condition:

2.1) The home occupation may have up to 2 additional classes per week between the hours of 6 - 9 pm and one day on the weekend between the hours of 8 am - 5 pm.

- The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
 - F. The P The request of Mark E. and Janet Greenwood (Owners), for property located at 480 Dennett Street requesting a Conditional Use Permit from Section 10.814 for a Detached Accessory Dwelling Unit (DADU) for the demolition of the existing garage and construction of a new DADU Said property is located on Assessor Map 160 Lot 26 and lies within the General Residence A (GRA) District. (LU-24-120)

Project Background

The applicant is proposing to demolish the existing nonconforming garage and construct a new Detached Accessory Dwelling Unit (DADU) that will conform to the dimensional requirements in the GRA. The proposed DADU will be 750 sq. ft. and comply with all other dimensional and design requirements for a DADU.



<u>Planning Department Recommendation</u> Detached Accessory Dwelling Unit Conditional Use Permit

1) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.814.62 of the Ordinance and adopt the findings of fact <u>as presented</u>.

(Alt.) Vote to find that the Conditional Use Permit Application meets the requirements set forth in Section 10.814.62 of the Ordinance and adopt the findings of fact <u>as</u> <u>amended</u>.

2) Vote to grant the Conditional Use Permit with the following conditions:

- 2.1) Documentation of the conditional use permit approval shall be recorded at the Rockingham County Registry of Deeds, together with an affidavit that either the principal dwelling unit or the accessory dwelling unit will be occupied by the owner of the dwelling as the owner's principal place of residence, as required by Section 10.814.22.
- 2.2) A certificate of use issued by the Planning Department is required to verify compliance with the standards of this Section, including the owner occupancy and principal residency requirements. Said certificate shall be issued by the Planning Department upon issuance of a certificate of occupancy by the Inspection Department. A certificate of use shall not be issued prior to recording of documentation as required by this Ordinance.
- 2.3) The certificate of use shall be renewed annually upon submission of such documentation as the Planning Department may require to verify continued compliance with the standards of this Section. Failure to comply with this requirement shall be deemed a violation of the ordinance and may be enforced as provided in Article 2.

- The Board's action in these matters has been deemed to be quasi-judicial in nature. If any person believes any member of the Board has a conflict of interest, that issue should be raised at this point or it will be deemed waived.
 - G. The request of Portsmouth West End Development LLC (Owner), for property located at 125 Brewery Lane requesting a Conditional Use Permit in accordance with Section 10.440, Use 19.50 for an outdoor dining and drinking area as an accessory use. Said property is located on Assessor Map 154 Lot 2 and lies within the Character District 4-W (CD-4W) District. (LU-24-108)

Background

The property is located in the CD4-W district, where an outdoor dining and drinking area requires a conditional use permit as an accessory use to a principal use. The applicant is proposing to add picnic tables and bistro tables and chairs to an area at the back of the building which faces the existing parking lot. The proposal includes expanding the gravel area to accommodate the tables and chairs.



Planning Department Recommendation

Outdoor Dining Conditional Use Permit

1) Vote to find that the Conditional Use Permit application meets the criteria set forth in Section 10.243.20 and to adopt the findings of fact <u>as presented.</u>

(Alt.) Vote to find that the Conditional Use Permit application meets the criteria set forth in Section 10.243.20 and to adopt the findings of fact <u>as amended and read into the record.</u>

2) Vote to approve the conditional use permit as presented.

IV. PRELIMINARY CONCEPTUAL CONSULTATION AND DESIGN REVIEW

A. The request of Frances E. Mouflouze Revocable Trust of 2015 (Owner), for property located at 550 Sagamore Avenue requesting preliminary Conceptual Consultation for a subdivision of one lot into three conforming lots with associated site improvements. Said property is located on Assessor Map 222 Lot 11 and lies within the Single Residence B (SRB) District. (LUPD-24-5)

The applicant has provided a set of preliminary plans for discussion with the Board. As authorized by NH <u>RSA 676:4,II</u>, the Site Plan Regulations require preliminary conceptual consultation for certain proposals, including (1) the construction of 30,000 sq. ft. or more gross floor area, (2) the creation of 20 or more dwelling units, or (3) the construction of more than one principal structure on a lot. Preliminary conceptual consultation precedes review by the Technical Advisory Committee. Preliminary consultation is not required for this application, however the applicant wanted to get feedback from the Board prior to submitting a formal TAC application for site plan and subdivision approval.

Preliminary conceptual consultation is described in the state statute as follows: [Preliminary conceptual consultation] ... shall be directed at review of the basic concept of the proposal and suggestions which might be of assistance in resolving problems with meeting requirements during final consideration. Such consultation shall not bind either the applicant or the board and statements made by planning board members shall not be the basis for disqualifying said members or invalidating any action taken. The board and the applicant may discuss proposals in conceptual form only and in general terms such as desirability of types of development and proposals under the master plan.

The preliminary conceptual consultation phase provides the Planning Board with an opportunity to review the outlines of a proposed project before it gets to detailed design (and before the applicant refines the plan as a result of review by the Technical Advisory Committee and public comment at TAC hearings). In order to maximize the value of this phase, Board members are encouraged to engage in dialogue with the proponent to offer suggestions and to raise any concerns so that they may be addressed in a formal application. Preliminary conceptual consultation does not involve a public hearing, and no vote is taken by the Board on the proposal at this stage. Unlike Design Review, completion of Preliminary Conceptual Consultation does not vest the project to the current zoning. B. 361 Hanover Steam Factory, LLC (Owner), for property located at 361 Hanover Street, requesting Preliminary Conceptual Consultation for the construction of a new building along Hanover Street with a 20-foot tunnel entrance from Hanover Street to a central courtyard between the new building and the existing 361 Hanover Street (Portsmouth Steam Factory) building. The courtyard will provide access to the indoor parking areas at both the existing and the new building. The upper floors of the new Hanover Street building will contain 12 residential dwelling units and the Portsmouth Steam Factory Building would contain 24 dwelling units; for a total of 36 dwelling units. There would be 72 off-street parking spaces in the aggregate. (LUPD-24-3)

The applicant has provided a set of preliminary plans for discussion with the Board. As authorized by NH <u>RSA 676:4,II</u>, the Site Plan Regulations require preliminary conceptual consultation for certain proposals, including (1) the construction of 30,000 sq. ft. or more gross floor area, (2) the creation of 20 or more dwelling units, or (3) the construction of more than one principal structure on a lot. Preliminary conceptual consultation precedes review by the Technical Advisory Committee.

Preliminary conceptual consultation is described in the state statute as follows: [Preliminary conceptual consultation] ... shall be directed at review of the basic concept of the proposal and suggestions which might be of assistance in resolving problems with meeting requirements during final consideration. Such consultation shall not bind either the applicant or the board and statements made by planning board members shall not be the basis for disqualifying said members or invalidating any action taken. The board and the applicant may discuss proposals in conceptual form only and in general terms such as desirability of types of development and proposals under the master plan.

The preliminary conceptual consultation phase provides the Planning Board with an opportunity to review the outlines of a proposed project before it gets to detailed design (and before the applicant refines the plan as a result of review by the Technical Advisory Committee and public comment at TAC hearings). In order to maximize the value of this phase, Board members are encouraged to engage in dialogue with the proponent to offer suggestions and to raise any concerns so that they may be addressed in a formal application. Preliminary conceptual consultation does not involve a public hearing, and no vote is taken by the Board on the proposal at this stage. Unlike Design Review, completion of Preliminary Conceptual Consultation does not vest the project to the current zoning.

This project was before the Board in April for Preliminary Conceptual Consultation and then Design Review in May in order to vest the zoning. The applicant has made substantial changes to the project based on input from the public and the Planning Board and wanted to present the new plan to the Board prior to seeking variances for certain elements of the project.

V. OTHER BUSINESS

- **A.** Chairman's Updates and Discussion Items
- **B.** Board Discussion of Regulatory Amendments and Other Matters

VI. ADJOURNMENT

PLANNING BOARD PORTSMOUTH, NEW HAMPSHIRE

EILEEN DONDERO FOLEY COUNCIL CHAMBERS CITY HALL, MUNICIPAL COMPLEX, 1 JUNKINS AVENUE

7:00 PM Public Hearings begin

June 20, 2024

MEMBERS PRESENT:	Rick Chellman, Chairman; Greg Mahanna, Vice Chair; Karen Conard, City Manager; Joseph Almeida, Facilities Manager; Beth Moreau, City Councilor; James Hewitt; Paul Giuliano; Andrew Samonas; Anthony Coviello; and William Bowen, Alternate
ALSO PRESENT:	Peter Stith, Planning Department Manager

MEMBERS ABSENT: None.

Chair Chellman called the meeting to order at 7:00 p.m. He stated that Mr. Coviello would arrive at the meeting later and that Alternate Mr. Bowen would take a voting seat until then.

I. APPROVAL OF MINUTES

A. Approval of the May 16, 2024 meeting minutes.

Vice-Chair Mahanna moved to approve the May 16 minutes as amended, seconded by Councilor Moreau and with Mr. Hewitt abstaining. The motion passed unanimously.

II. DETERMINATIONS OF COMPLETENESS

SITE PLAN REVIEW

A. The request of Friends of Lafayette House in care of Melanie Merz (Owner), for property located at 413 Lafayette Road requesting Site Plan Review Approval to construct an attached caretaker's unit to the existing residential care facility with associated site improvements. Said property is located on Assessor Map 230 Lot 23A and lies within the Single Residence B (SRB) District.

Councilor Moreau moved that the Board determine that Item A is complete according to the Site Plan Review Regulations (contingent on the granting of any required waivers under Section IV of the agenda) and to accept the application for consideration. Vice-Chair Mahanna seconded. The motion **passed** unanimously.

A. The request of Edmund R. St. Pierre (Owner), for property located at 15 Mariette Drive requesting a Conditional Use Permit from Section 10.814 for a Detached Accessory Dwelling Unit. Said property is located on Assessor Map 292 Lot 167 and lies within the Single Residence B (SRB) District. (LU-24-57)

SPEAKING TO THE PETITION

[Timestamp 4:30] The applicant Edmund St. Pierre was present. He reviewed the petition and described what the proposed detached Accessory Dwelling Unit (ADU) would look like.

[Timestamp 7:58] Vice-Chair Mahanna noted that the applicant said he wanted to downsize and asked if the applicant would live in it. Mr. St. Pierre said he designed the ADU for himself or his sister to live in. Councilor Moreau said the applicant said a second-floor full bathroom was proposed but that he mentioned a half bath on the first floor. Mr. St. Pierre said the first-floor full bathroom would go away with the renovation. Chair Chellman said the applicant proposed to renovate part of the first floor into the ADU but that one of the plans showed the entire first floor going into the ADU. Mr. St. Pierre said he originally designed a handicap accessible first floor but did not follow through with it because of the square footage.

Chair Chellman opened the public hearing.

SPEAKING TO, FOR, OR AGAINST THE PETITION

No one spoke, and Chair Chellman closed the public hearing.

DECISION OF THE BOARD

Councilor Moreau moved that the Board find that the Conditional Use Permit Application meets the requirements set forth in Section 10.814.62 of the Ordinance and adopt the findings of fact as presented. Ms. Conard seconded. The motion **passed** unanimously.

Councilor Moreau moved that the Board grant the Conditional Use Permit with the following conditions:

2.1) Documentation of the conditional use permit approval shall be recorded at the Rockingham County Registry of Deeds, together with an affidavit that either the principal dwelling unit or the accessory dwelling unit will be occupied by the owner of the dwelling as the owner's principal place of residence, as required by Section 10.814.22.

2.2) A certificate of use issued by the Planning Department is required to verify compliance with the standards of this Section, including the owner occupancy and principal residency requirements. Said certificate shall be issued by the Planning Department upon issuance of a certificate of occupancy by the Inspection Department. A certificate of use shall not be issued prior to recording of documentation as required by this Ordinance.

2.3) The certificate of use shall be renewed annually upon submission of such documentation as the Planning Department may require to verify continued compliance with the standards of this Section. Failure to comply with this requirement shall be deemed a violation of the ordinance and may be enforced as provided in Article 2.

Ms. Conard seconded. The motion **passed** unanimously.

B. The request of **Richard M.** and **Francoise S. Kinney (Owners)**, for property located at **89 Cliff Road** requesting an after the fact Wetland Conditional Use Permit from Section 10.1017.50 for violations within the City's 100' wetland buffer. A three-season porch, deck and concrete landing pad were constructed without permits, of which 225 s.f. is within the buffer. Said property is located on Assessor Map 223 Lot 9 and lies within the Single Residence B (SRB) District. (LU-24-54)

SPEAKING TO THE PETITION

[Timestamp 13:00] The applicant Richard Kinney was present to review the petition. He said a 3-season porch, adjoining deck, and concrete landing pad were added that intruded 225 square feet into the wetland buffer. He said he worked with the Conservation Commission to mitigate the impact onto the buffer, which included putting in a drywell, adding gravel under the porch and deck, extending the downspout out from the north side of the house, and adding shrubs and a recessed planting area. He said a microclover lawn mix would replace the back yard's grass.

The Board had no questions, and Chair Chellman opened the public hearing.

SPEAKING TO, FOR, OR AGAINST THE PETITION

No one spoke, and Chair Chellman closed the public hearing.

DECISION OF THE BOARD

Mr. Giuliano moved that the Board find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact <u>as presented</u>. *Mr.* Almeida seconded. The motion **passed** unanimously.

Mr. Giuliano moved that the Board grant_the Conditional Use Permit with the following condition:

2.1) In accordance with Section 10.1018.40 of the Zoning Ordinance, applicant shall install permanent wetland boundary markers where applicable. In addition to the wetland boundary markers, an educational sign describing the project shall be installed near the restoration area and fencing should be utilized to keep disturbances such as dogs and geese from the area.

Ms. Conard seconded. The motion **passed** unanimously.

C. The request of Wentworth Senior Living (Applicant), and MH Wentworth HM for CHRNC INV (Owner), for property located at 346 Pleasant Street is requesting a Wetland Conditional Use Permit from Section 10.1017.50 to replace an existing wooden fence along the back of the property which abuts the South Mill Pond. This replacement project will have approximately 200 s.f. of impact within the buffer, with 10 s.f. of permanent impact below ground with the posts and 500 linear feet of permanent impact from the fence. Said property is located on Assessor Map 109 Lot 10 and lies within the General Residence B (GRB) District. (LU-24-63)

SPEAKING TO THE PETITION

[Timestamp 19:12] Madison Abbott representing Wentworth Senior Living was present to review the petition. She said they wanted to replace 510 linear feet of wooden fence, most of which occurred within the 100-ft wetland buffer. She said the reason for going through the whole permit requirement and not just an exception was because they had about 50 linear feet within the 25-ft vegetation buffer. She said they were past the point of repairing and explained how the installation method would be the least disruptive as possible.

[Timestamp 20:11] Councilor Moreau said it wasn't clear which fence would be installed. Ms. Abbott said they currently had a scalloped picketed fence that they wanted to replace with a vinyl one that would have the same look but be more durable. Chair Chellman asked if it was shiny. Ms. Abbott said it would be for a few years. She said one of the Conservation Commission's stipulations was that a regular maintenance plan be followed and that only pressurized washing with water be done. Vice-Chair Mahanna said it was an interesting choice by the applicant to oppose what the Historic District Commission (HDC) suggested. Ms. Abbott said the HDC approved the vinyl material but that the Conservation Commission suggested that other options be explored. She said an Azek material would have been a choice but it was four times the cost of the vinyl fence. Vice-Chair Mahanna said he would have preferred a non-shiny wooden fence, especially since Wentworth Senior Living was a public place. Ms. Abbott said they had about 90 feet of frontage on Pleasant Street, with a concrete wall that included a wooden fence above it. She said eventually they would replace the fence with another wood one. Mr. Almeida noted that the front of the building was painstakingly restored and maintained and there was a total rebuild of the fence in the front. Chair Chellman asked Ms. Abbott if she would accept a condition that the fence along Pleasant Street would remain wood. Ms. Abbott agreed.

Chair Chellman opened the public hearing.

SPEAKING TO, FOR, OR AGAINST THE PETITION

No one spoke, and Chair Chellman closed the public hearing.

DECISION OF THE BOARD

Councilor Moreau moved that the Board find that the Conditional Use Permit Application meets the requirements set forth in Section 10.1017.50 of the Ordinance and adopt the findings of fact <u>as presented</u>. Ms. Almeida seconded. The motion **passed** unanimously.

Councilor Moreau moved that the Board grant the Conditional Use Permit with the following conditions:

2.1) In accordance with Section 10.1018.40 of the Zoning Ordinance, applicant shall install permanent wetland boundary markers where applicable. In addition to the wetland boundary markers, an educational sign describing the project shall be installed near the restoration area and fencing should be utilized to keep disturbances such as dogs and geese from the area.

2.2) Maintenance for the new fencing shall include power washing with water only.

2.3) Fencing along Pleasant Street if replaced, will remain the current material that exists.

Mr. Almeida seconded. The motion passed unanimously.

D. The request of **Friends of Lafayette House in care of Melanie Merz (Owner),** for property located at **413 Lafayette Road** requesting Site Plan Review Approval to construct an attached caretaker's unit to the existing residential care facility with associated site improvements. Said property is located on Assessor Map 230 Lot 23A and lies within the Single Residence B (SRB) District. (LU-23-208)

SPEAKING TO THE PETITION

[Timestamp 27:55] Project engineer Joe Coronati was present to review the petition on behalf of the applicant, along with Friends of Lafayette House Executive Director Renee Sullivan and board member Melanie Merz. Mr. Coronati said the Friends of Lafayette House took care of twelve developmentally disabled adults. He said the full-time caretaker lived on the property and worked five days a week and a part-time caretaker worked on the weekend and stayed with the full-time caretaker then. He said the expansion was needed to add a one-story addition to the building so that the full-time caretaker had his own apartment. He said there would be no change to the number of residents or anything external except to modify the walkway.

[Timestamp 30:42] Councilor Moreau asked how people went in and out of the building. Mr. Coronati showed where the main entrance was and said it would not change. Chair Chellman said the site plan showed two accesses and asked if the one farther away was the main entrance. Mr. Coronati said the addition would be on the end of the building that had the boiler and storage rooms and would not alter any of the doorways or access points into the building. He said there would be a new entrance to the caretaker's unit. Councilor Moreau said the entrance on the right looked like it went into a kitchen. Mr. Coronati said there was an entrance on the long wall and egress doors that were fenced in and secured for residents. Mr. Bowen said there was plenty of parking at random times and that he assumed that most of the residents didn't drive but would have visitors. He asked if the parking would change and Mr. Coronati said it would not. Mr. Giuliano said the waiver request, Article 10, Outdoor Lighting, indicated that the applicant was

proposing additional lighting, and he asked if the applicant meant to say that they were not proposing additional lighting. Mr. Coronati agreed. He said there might be one residential light over entrance door that would be controlled by the caretakers and that there was one outside light that wasn't in the best of shape that may end up being removed.

Chair Chellman opened the public hearing.

SPEAKING TO, FOR, OR AGAINST THE PETITION

No one spoke, and Chair Chellman closed the public hearing.

DECISION OF THE BOARD

Mr. Giuliano moved that the Board find that the Site Plan Application meets the requirements set forth in the Site Plan Regulations Section 2.9 Evaluation Criteria and adopt the findings of fact as presented. Vice-Chair Mahanna seconded. The motion **passed** unanimously.

Mr. Giuliano moved that the Board find that the requested waivers will not have the effect of nullifying the spirit and intent of the City's Master Plan or the Site Plan Review Regulations, and to waive the regulations as requested. Councilor Moreau seconded.

Councilor Moreau said it was a little addition that would not really change the function or how the place works, so she agreed that the waivers were acceptable.

Mr. Giuliano moved that the Board grant Site Plan approval with the following conditions:

<u>Conditions to be satisfied subsequent to final approval of site plan but prior to the issuance of</u> <u>a building permit or the commencement of any site work or construction activity:</u>

3.1) The site plan and any easement plans and deeds shall be recorded at the Registry of Deeds by the City or as deemed appropriate by the Planning Department.

Ms. Conard seconded. The motion passed unanimously.

E. 806 US Route 1 Bypass requesting Amended Site Plan Approval and a second 1-Year extension to the Site Plan Approval originally granted on June 23, 2022. (LU-22-81)

SPEAKING TO THE PETITION

[Timestamp 38:23] Project engineer Alex Ross was present on behalf of the applicant, with builder Dave Grzybowski. Mr. Ross said they were before the Board a month ago for the abutting site because of the off-site draining. He said it was the same as the present site, and he reviewed the existing conditions plan and the drainage. He said there were several design options reviewed by the City and the NHDOT and that A22 was approved, so now they had the proposed changes before the Board to get the amended plan set and extension approved.

[Timestamp 40:13] Mr. Giuliano said he had asked at the previous meeting what the property's use would be. Mr. Ross said property was currently City Tobacco and it was just a small building, so the owner wanted to move next door. He said the small building could be rented out or used for something else. Mr. Grzybowski said that after the move, the place would be empty but the applicant would come back before the Board for any change in use or if any business went in. Chair Chellman noted that an approved walk-in cooler would be added to the back of it to make the approved square footage.

Chair Chellman opened the public hearing.

SPEAKING TO, FOR, OR AGAINST THE PETITION

No one spoke, and Chair Chellman closed the public hearing.

DECISION OF THE BOARD

Councilor Moreau moved that the Board find that the Site Plan Application meets the requirements set forth in the Site Plan Regulations Section 2.9 Evaluation Criteria and adopt the findings of fact as presented. Ms. Conard seconded. The motion **passed** unanimously.

Councilor Moreau moved that the Board grant amended site plan approval and a second oneyear extension with the original conditions as approved on June 23, 2022 and the following conditions:

<u>Conditions to be satisfied subsequent to final approval of site plan but prior to the issuance of a certificate of occupancy and release of the surety:</u>

2.1) The Engineer of Record shall submit a written report (with photographs and engineer stamp) certifying that the stormwater infrastructure was constructed to the approved plans and specifications and will meet the design performance;

2.2) A stormwater inspection and maintenance report shall be completed annually and copies shall be submitted for review to the City's Stormwater Division/ Public Works Department.

Ms. Conard seconded. The motion passed unanimously.

F. The Planning Board will hold a public hearing on the following amendments to Chapter 10, Article 5A - Character-Based Zoning, Section 10.5A43.33 regarding Building and Story Heights of the ZONING ORDINANCE of the City of Portsmouth, pursuant to Section 10.150 of the Zoning Ordinance.

[Timestamp 44:10] Chair Chellman asked if the Board members had a chance to look at the amendments. Mr. Hewitt said he didn't have time and preferred postponing it to give the Board members more time to look at the amendments carefully. Chair Chellman said it was a modification to something that was done last August, so it wasn't brand new. He said there was a question about whether there was a requirement to have workforce housing as part of the

proponent's application to qualify for the additional height story of building. He said it was corrected and that he requested that the Board members look at the other sections because the community space definitions were not what they would think. He said it included things like plazas and pedestrian passageways and was much more than greenspace. Vice-Chair Mahanna said he didn't get a chance to read the email. Councilor Moreau said the question was whether it needed to be mixed use residential and nonresidential uses for the incentives to be taken advantage of. She said that was why the City Council was trying to clarify that section because it was not as clear as what the intention was.

Chair Chellman said the original text included the phrase 'and/or' and that it could be confusing. He said it was meant to be a possible mix of building types. He said he also thought the 50 percent requirement for community space was high and a big ask as well as a detriment to the incentive itself. He said the Board might want to discuss whether they would want to suggest to the Council to reduce it. Vice-Chair Mahanna said it could be scaled down. Chair Chellman said he was thinking of scaling it down to half. Mr. Bowen asked if it would apply to the Steam Factory, and Chair Chellman said it would not because the Incentive Overlay District did not apply. He said there would have to be a one-acre minimum as well. He noted that the McIntyre and Citizens Bank properties would qualify as well as a few other properties. Vice-Chair Mahanna suggested that the Board receive more information to inform them on what they were deciding on for the next time they considered it. Councilor Moreau said there was a lot of discussion about the 50 percent community space at the Land Use Committee meeting, and due to the density and size of the one acre or more lots, trying to get as much community space as possible was very important, so she would not be in favor of trying to change that at this time. Chair Chellman said the building types included houses, and there had been discussion that The Hill, for example, was a nonconforming situation that could not be built downtown under the existing zoning but that it could be theoretically built on the Citizens Bank property with houses, so it would qualify for that type of development on that site. He said he thought it would be more difficult to do with a 50 percent community space allocation. Ms. Conard asked if the City Council could act in the absence of the Planning Board acting. Chair Chellman said the zoning ordinance required the Planning Board to make a recommendation to the City Council. He said he would be okay with revisiting the community space issue in the future. He said the other sections were strategically more important, especially the goal for workforce housing.

Ms. Conard moved to recommend that the City Council take up the new section as amended as of that day to the Planning Board. Mr. Giuliano seconded.

[Timestamp 53:47] There was further discussion about whether the Board would have the authority to grant an extra layer of height or extra floor in exchange for 5 or 10 percent being controlled rent price and 50 percent being greenspace. Chair Chellman said it was community space, not greenspace, and said examples would include pedestrian passageways, wide pedestrian sidewalks, pedestrian arcades, pocket parks, playgrounds, public observation decks, and that there was a requirement to include a plaza or square of at least 5,000 sf per acre. Chair Chellman said none of those were greenspaces and were hardscaped community spaces. Mr. Bowen asked if there was no discretion on a proposal that would conform to those conditions. Chair Chellman said it would be a Conditional Use Permit, so there was discretion involved and

some back-and-forth. He said if an applicant met all the requirements, the Board was supposed to grant it. Mr. Bowen said the average person thought of community space as greenspace. Vice-Chair Mahanna said he supported the clarification but thought the Board should see the normal overlay that showed the properties to be affected. Chair Chellman said none of the applicable properties were changing in any way and that very few could qualify. Vice-Chair Mahanna said it was a burden for the developer to have 50 percent of an acre for community space. Mr. Almeida agreed and said he thought part of the purpose of the amendment was due to workforce housing and thought it would encourage and discourage workforce housing at the same time. Chair Chellman said the motion was to correct the mistake. He said he was inclined to vote it up but that the Board could come back to it because workforce housing was a big topic.

Ms. Conard amended her motion as follows:

Ms. Conard moved that the Board vote to recommend to City Council to approve the zoning amendments as amended and to hold first reading and to convey the discussion the Board had about the 50% community space requirement. Mr. Giuliano seconded.

[Timestamp 1:01:22] There was further discussion. Mr. Samonas said one of the ways to achieve better public and community space results were amenities that welcomed the public, as opposed to wider pedestrian sidewalks. He said the second community space objective was to break up the massing of some of the larger north end projects that tried to utilize the parcel and drive economic return but created congestion. He said the workforce housing objective set the threshold so high that the developer had to come before the Board to ask if they would end up at 50 percent, but at least it allowed them to discuss it before the Board. He noted that the amendment mentioned the term 'as further described'. He said the revisions helped the Board get a cohesive view of all the considerations, and if they had the figures and entire zoning ordinance in front of them, it helped to get the full big picture. Chair Chellman said it was not a change in any of that, however. He said if a second version of it happened, the first sentence about community space could be changed to say that "at least a smaller amount and up to 50 percent or whatever the range would be" to have a provision where the applicant is required to show both and have a discussion with the Board. It was further discussed. Mr. Hewitt said it may be a logical step but that he had to vote in opposition due to the nine hours' notice. Mr. Giuliano said Mr. Samonas brought up a good points about the large projects in the north end, and it was further discussed. Mr. Almeida said he would support the motion because the Board was correcting minor language changes, but in the future they would need more discussion. Councilor Moreau said she could bring up the 50 percent issue at the City Council meeting.

The motion passed 7-2, with Member Hewitt and Vice-Chair Mahanna voting against.

Note: At this point in the meeting, Mr. Coviello arrived and took his voting seat, and Mr. Bowen went back to alternate status.

IV. CITY COUNCIL REFERRALS

A. Chapter 10, Article 5A - Character-Based Zoning (See item F. above)

See Item F above.

V. OTHER BUSINESS

A. 325 Little Harbor Road requesting a 1-Year Extension to the Wetland Conditional Use Permit originally granted on July 20, 2023. (LU-23-81)

DECISION OF THE BOARD

Councilor Moreau moved that the Board grant a one-year extension to the Planning Board Approval of the Conditional Use Permit to July 20, 2025. Mr. Almeida seconded. The motion **passed** unanimously.

B. Chairman Updates and Discussion Items

[Timestamp 1:14:00] Chair Chellman said there was a desire to go through the Board's site plan and subdivision regulations that had not had attention for some time, and the Legal Department wanted to have a meeting with a Planning Board subcommittee. Mr. Coviello and Mr. Bowen volunteered. Chair Chellman said he would set it up.

C. Board Discussion of Regulatory Amendments, Master Plan Scope & Other Matters

[Timestamp 1:14:51] Chair Chellman said a draft of the Master Plan Scope would go out to the Board members for a proposed RFQ similar to what the City did with the Sherburne school.

Mr. Coviello said he and Mr. Bowen were at a housing conference where Assistant Mayor Joanna Kelley spoke and said that the City Council collected data on new housing and the number of students that came out of that new housing. He asked if that data was available to the Board. Councilor Moreau said it was the Parson Woods in the west end and that two students were designated for Little Harbour School. Mr. Coviello asked if it were possible to have data on calls for service from Police and Fire, and Ms. Conard said she would find out.

VI. ADJOURNMENT

The meeting adjourned at 8:20 p.m.

Respectfully submitted,

Joann Breault Planning Board Recording Secretary

Tighe&Bond

L0700-026C June 14, 2024

Mr. Rick Chellman, Chairman City of Portsmouth Planning Board 1 Junkins Avenue Portsmouth, New Hampshire 03801

Re: Lonza Biologics – Proposed PV Solar Carports Amended Site Plan Review Application LU-23-108

Dear Chairman Chellman:

On behalf of Lonza Biologics, Inc. (Lonza), we are pleased to submit one (1) set of hard copies and one electronic file (.pdf) of the following information to support a request to the Planning Board for a recommendation for approval to the Pease Development Authority (PDA) for Amended Site Plan Review for proposed PV Solar Carports located at 5 Technology Way, (Formerly 70 Corporate Drive) on Pease International Tradeport:

- PDA Application for Site Review, dated May 20, 2024;
- Site Plan Set, last revised May 20, 2024;
- Drainage Memo, dated May 20, 2024;
- Glare Study Results, dated February 22, 2024;

PROJECT SUMMARY

Background

The existing project was granted Site Plan approval on January 17, 2019, and amended by administrative approvals on September 27, 2019, January 27, 2023, and Amended Site Plan Approval on November 16, 2023.

Existing Condition

The project is located on the portion of Lonza's 46-acre parcel refered to as the Iron Parcel. The following summarizes the work currently approved through the November 16, 2023 Amended Site Plan Approval:

- Daylighting of Hodgson Brook on the Iron Parcel
- Removal of the existing Hodgson Brook culvert
- Construction of the sidewalk and landscaping along Corporate Drive
- Completion of Soils Management Plan
- Construction of Building #1
- Construction of the Central Utility Building
- Construction site improvements for Building #1 such as drive aisles, fire lanes, utilities, lighting, sidewalks and stormwater management.
- Construction of a temporary 150-space surface parking lot, sidewalks and stormwater management.

Amended Site Plan

The requested Site Plan amendment includes the construction of Photovoltaic Cell (PV) Solar canopies over the previously approved temporary surface parking lot. The addition of these Solar Canopies is being requested to support Lonza Biologics green infrastructure and sustainability initiatives. The addition of these Solar canopies will not result in any dimensional changes to the previously approved parking lot. There is a slight increase in impervious surfaces (~672 SF) which will not cause any adverse impact to the previously approved Phase 2 Drainage design as outlined in the Drainage Memorandum.

The proposed PV Solar system will require additional electrical infrastructure and modifications to the photometric lighting design as depicted in the enclosed Site Plan Set. The proposed system is being designed to supplement and reduce the proposed project's overall electrical demand.

The project also received a recommendation for approval from the Technical Advisory Committee (TAC) at their June 4, 2024, meeting. We respectfully request to be placed on the Planning Board (PB) meeting agenda for July 18, 2024. If you have any questions or need any additional information, please contact Neil Hansen by phone at (603) 294-9213 or by email at nahansen@tighebond.com.

Sincerely,

TIGHE & BOND, INC.

Neil A. Hansen, PE Project Manager

Patrick M. Crimmins, PE Vice President

Copy: Lonza Biologics (via email) Pease Development Authority

J:\L\L0700 Lonza Biologics Expansion was 1576F\026_Project Albacore\Report_Evaluations\Applications\City of Portsmouth\20240614_Solar PB Submission\L0700-026C_PB Cover Letter.docx

Pease Development Authority 55 International Drive, Portsmouth, NH 03801, (603) 433-6088



Application for Site Review

For PDA Use Only			
Date Submitted:	Municipal Review:	Fee:	
Application Complete:	Date Forwarded:	Paid:	Check #:

Applicant Information

Applicant: Lonza Biologics, Inc.	Agent: Tighe & Bond, Inc.
Address: 101 International Drive Portsmouth, NH 03801	Address: 177 Corporate Drive Portsmouth, NH 03801
Business Phone: 603-570-3625 Mobile Phone:	Business Phone: 603-433-8818 Mobile Phone:
Fax:	Fax:

Site Information

Portsmouth Tax Map: 305	Lot #: 006	Zone: Airport, Business, Commercial
Site Address / Location : 101 Interna	tional Drive, Portsm	outh, NH 03801
		Area of On-site Wetlands: 4,087 SF

Activity Information

Change of Use:	Yes []	No [X]	Existing Use: Office/Research/Manufacturing
			Description (Description / Manufacturing
			Proposed Use: Office/Research/Manufacturing
Description of Project			
The requeste	d Site P	lan amend	ment includes the construction of Photovoltaic Cell (PV)
Solar canopie	es over t	he previou	sly approved temporary surface parking lot.
	_		
All above inform	ation shal	l be shown on	a site plan submitted with this application. Provide 3 full size hard copies and one
			ell as one half-size set of drawings to PDA. Applicant shall supply additional copies as pality. Refer to Chapter 400 of PDA land Use Controls for additional information.

Certification

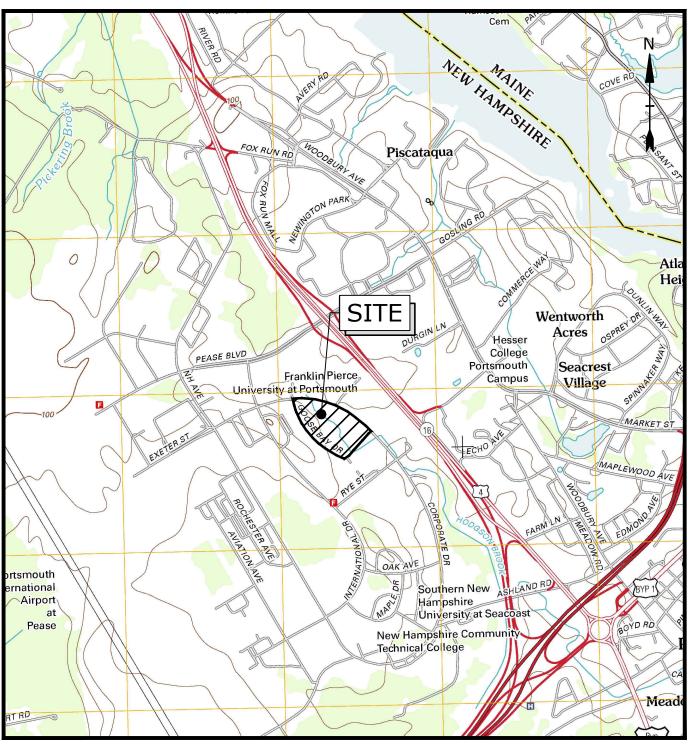
I hereby certify under the penalties of perjury that the foregoing inform are true and complete to the best of my knowledge. I hereby apply for S any conditions established by the Review Committee(s) and PDA	ite Review and acknowledge I will comply with all regulations and
alty	20 May 24
Signature of Applicant	' Date
MIChael Feeney Printed Name	

N:\Engineer\ ApplicationforSiteReview.xlsx

IRON PARCEL DEVELOPMENT - SOLAR 5 TECHNOLOGY WAY (FORMERLY 70 CORPORATE DRIVE)

PORTSMOUTH, NEW HAMPSHIRE PROJECT NO: L-0700-26 MAY 20, 2024

LIST OF DRAWINGS				
SHEET NO.	SHEET TITLE	LAST REVISED		
	COVER SHEET	5/20/2024		
C-161	PHASE 2 DEMOLITION PLAN	5/20/2024		
C-164	PHASE 2 OVERALL SITE PLAN	5/20/2024		
C-165	PHASE 2 SITE PLAN	5/20/2024		
C-168	PHASE 2 GRADING, DRAINAGE & EROSION CONTROL PLAN	5/20/2024		
C-171	PHASE 2 UTILITIES PLAN	5/20/2024		
C-174	PHASE 2 LANDSCAPE PLAN	5/20/2024		
C-177	PHASE 2 PHOTOMETRIC LIGHTING PLAN	5/20/2024		
C-501	EROSION CONTROL NOTES & DETAILS SHEET	5/20/2024		
C-503	DETAILS SHEET	5/20/2024		
8-046-3	SOLAR CANOPY DETAILS	5/20/2024		



LESSOR:

CLIENT:

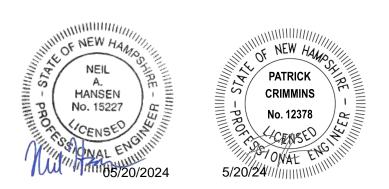
CIVIL ENGINEER:

SURVEYOR:

WETLAND SCIENTIST: GOVE ENVIRONMENTAL SERVICES, INC. 8 CONTINENTAL DRIVE, UNIT H EXETER, NEW HAMPSHIRE 03833

LOCATION MAP SCALE: 1" = 2,000'

LIST OF PERMITS			
LOCAL	STATUS	DATE	
SITE PLAN REVIEW PERMIT	APPROVED	1/17/2019	
AMENDED SITE PLAN REVIEW PERMIT	APPROVED	11/16/2023	
AMENDED SITE PLAN REVIEW PERMIT - SOLAR			
STATE			
NHDES - ALTERATION OF TERRAIN PERMIT	ISSUED: AOT-1498	10/02/2018	
NHDES - WETLANDS PERMIT	ISSUED: #2018-01731	12/21/2018	
FEDERAL			
EPA - NPDES CGP (SWPPP)	ACTIVE: NHR1001SK	7/7/2023	





PEASE DEVELOPMENT AUTHORITY **55 INTERNATIONAL DRIVE** PORTSMOUTH, NEW HAMPSHIRE 03801

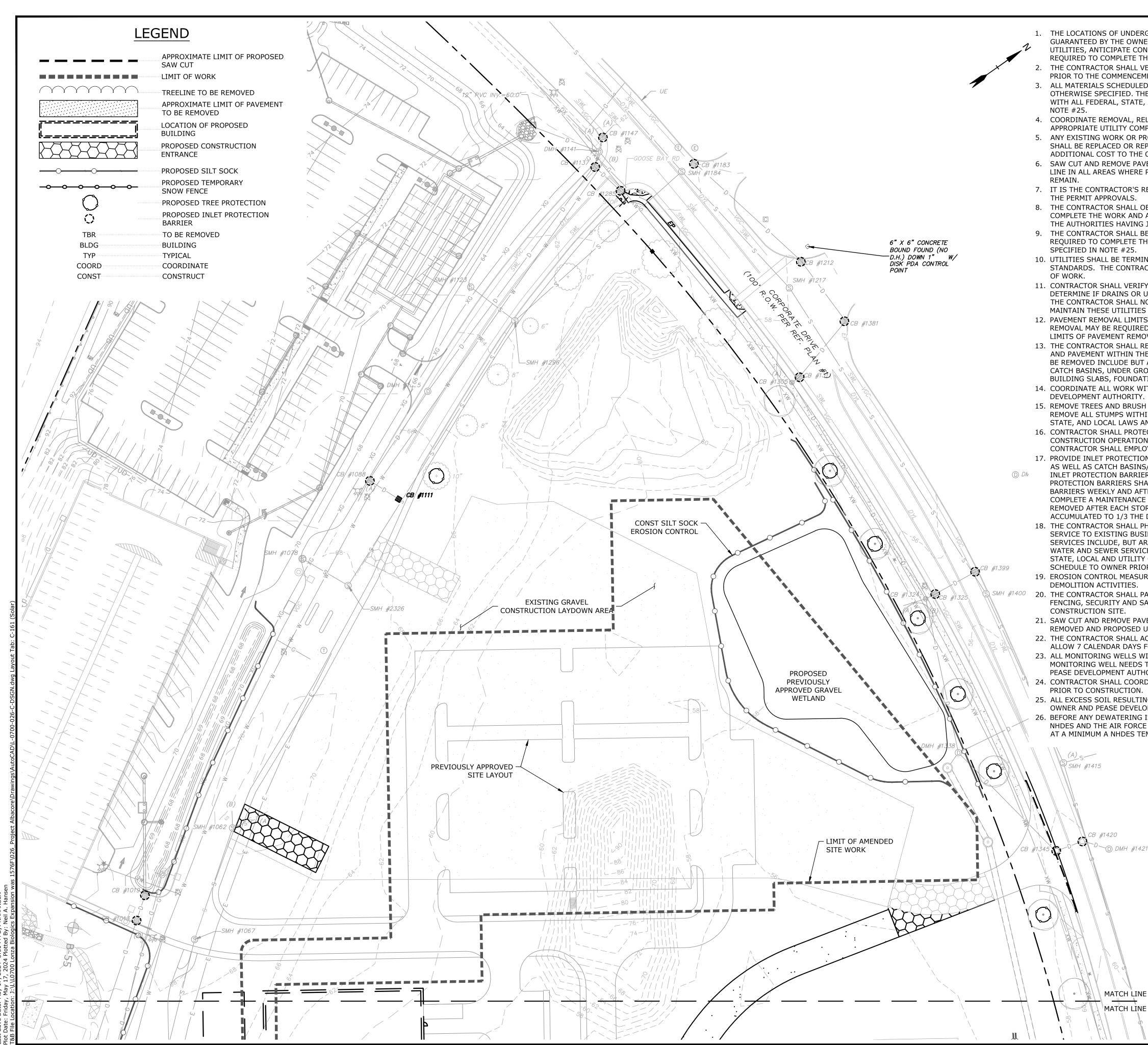
LONZA BIOLOGICS 101 INTERNATIONAL DRIVE PORTSMOUTH, NH 03801

Tighe&Bond

177 CORPORATE DRIVE PORTSMOUTH, NEW HAMPSHIRE 03801

DOUCET SURVEY, INC. 102 KENT PLACE NEWMARKET, NEW HAMPSHIRE 03857

ISSUED FOR AMENDED SITE REVIEW COMPLETE SET 11 SHEETS

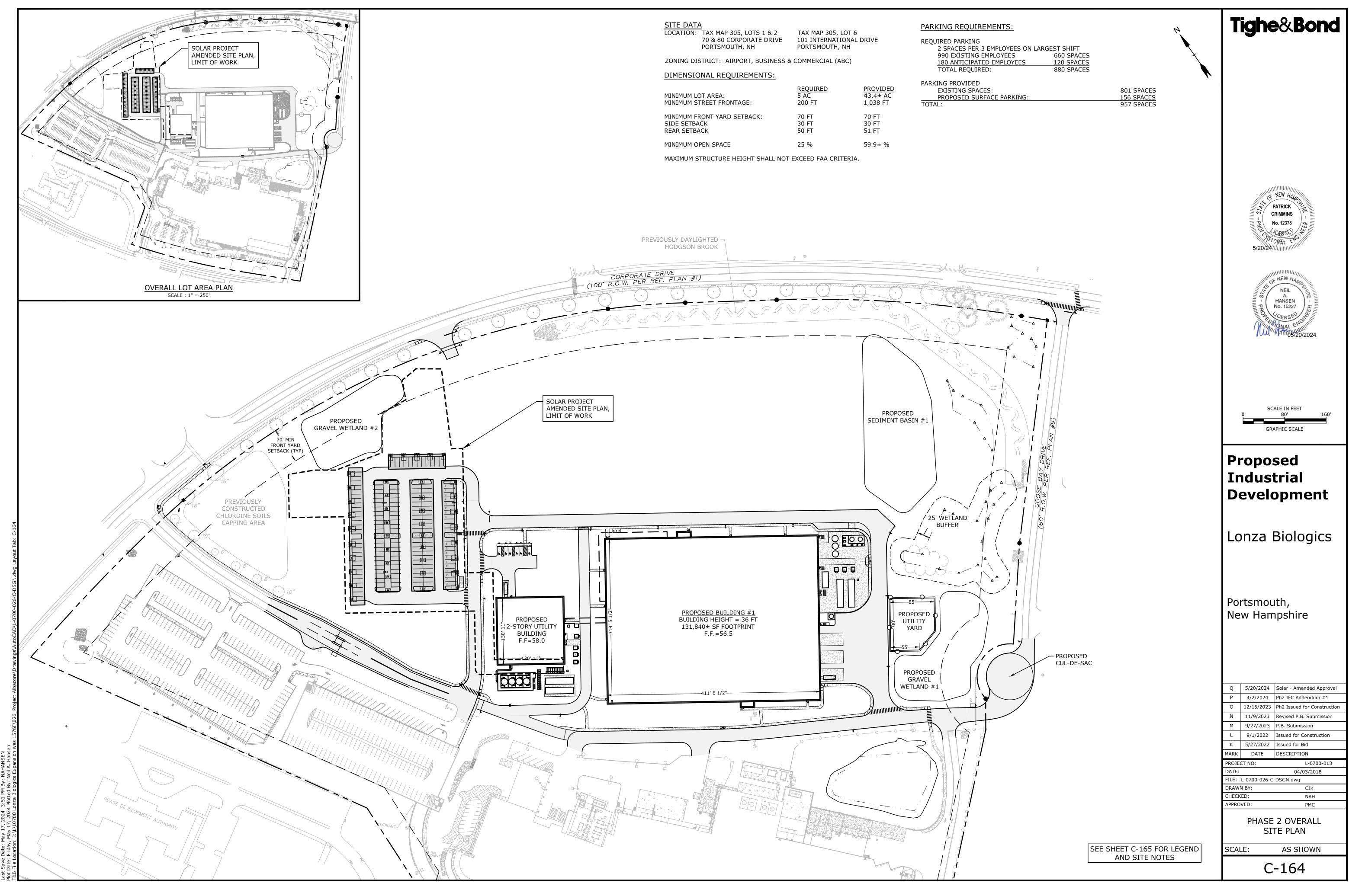


- REQUIRED TO COMPLETE THE WORK.
- APPROPRIATE UTILITY COMPANY.
- ADDITIONAL COST TO THE OWNER.
- THE PERMIT APPROVALS.
- THE AUTHORITIES HAVING JURISDICTION.
- SPECIFIED IN NOTE #25.

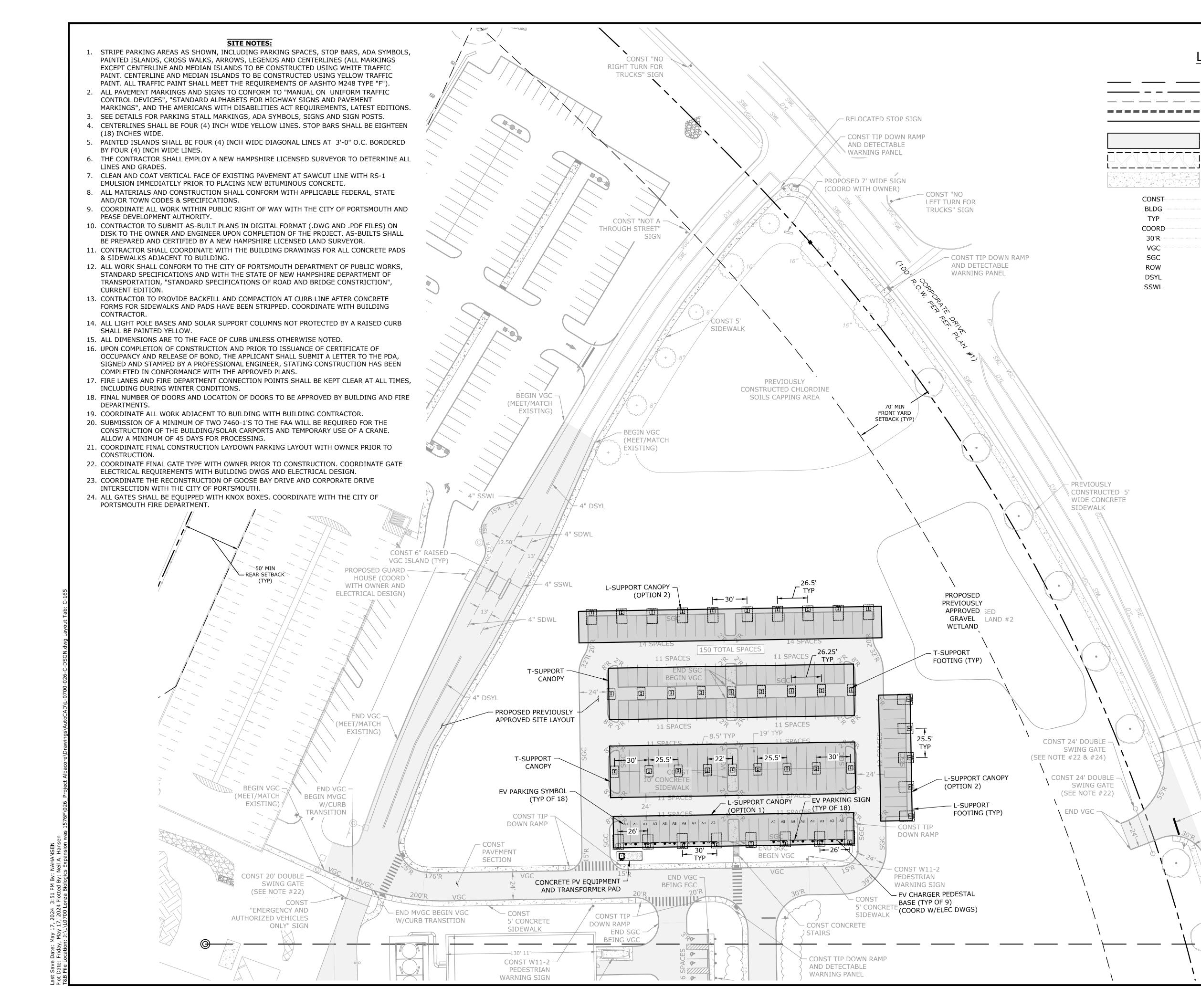
- LIMITS OF PAVEMENT REMOVAL PRIOR TO BID.
- BUILDING SLABS, FOUNDATION, TREES AND LANDSCAPING.
- DEVELOPMENT AUTHORITY.
- STATE, AND LOCAL LAWS AND REGULATIONS.

- ACCUMULATED TO 1/3 THE DESIGN DEPTH OF THE BARRIER.
- DEMOLITION ACTIVITIES.
- CONSTRUCTION SITE.
- ALLOW 7 CALENDAR DAYS FOR PROCESSING.
- PEASE DEVELOPMENT AUTHORITY.
- PRIOR TO CONSTRUCTION.

DEMOLITION NOTES: Tighe&Bond 1. THE LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE NOT GUARANTEED BY THE OWNER OR THE ENGINEER. IT IS THE CONTRACTOR'S RESPONSIBILITY TO LOCATE ALL UTILITIES, ANTICIPATE CONFLICTS, REPAIR EXISTING UTILITIES AND RELOCATE EXISTING UTILITIES THE CONTRACTOR SHALL VERIFY LOCATION OF ALL EXISTING UTILITIES. CALL DIG SAFE AT LEAST 72 HOURS PRIOR TO THE COMMENCEMENT OF ANY DEMOLITION/CONSTRUCTION ACTIVITIES. ALL MATERIALS SCHEDULED TO BE REMOVED SHALL BECOME THE PROPERTY OF THE CONTRACTOR UNLESS OTHERWISE SPECIFIED. THE CONTRACTOR SHALL DISPOSE OF ALL MATERIALS OFF-SITE IN ACCORDANCE WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS, ORDINANCES AND CODES EXCEPT AS SPECIFIED IN 4. COORDINATE REMOVAL, RELOCATION, DISPOSAL OR SALVAGE OF UTILITIES WITH THE OWNER AND 5. ANY EXISTING WORK OR PROPERTY DAMAGED OR DISRUPTED BY CONSTRUCTION/ DEMOLITION ACTIVITIES SHALL BE REPLACED OR REPAIRED TO MATCH ORIGINAL EXISTING CONDITIONS BY THE CONTRACTOR AT NO 6. SAW CUT AND REMOVE PAVEMENT ONE (1) FOOT OFF PROPOSED EDGE OF PAVEMENT OR EXISTING CURB LINE IN ALL AREAS WHERE PAVEMENT TO BE REMOVED ABUTS EXISTING PAVEMENT OR CONCRETE TO 7. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FAMILIARIZE THEMSELVES WITH THE CONDITIONS OF ALL OF 8. THE CONTRACTOR SHALL OBTAIN AND PAY FOR ADDITIONAL PERMITS, NOTICES AND FEES NECESSARY TO COMPLETE THE WORK AND ARRANGE FOR AND PAY FOR NECESSARY INSPECTIONS AND APPROVALS FROM 9. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL DEMOLITION AND OFF-SITE DISPOSAL OF MATERIALS NEW HA REQUIRED TO COMPLETE THE WORK, EXCEPT FOR WORK NOTED TO BE COMPLETED BY OTHERS AND AS PATRICK CRIMMINS 10. UTILITIES SHALL BE TERMINATED AT THE MAIN LINE PER UTILITY COMPANY AND THE CITY OF PORTSMOUTH STANDARDS. THE CONTRACTOR SHALL REMOVE ALL ABANDONED UTILITIES LOCATED WITHIN THE LIMITS No. 12378 CERSE TIN STOWAL . 11. CONTRACTOR SHALL VERIFY ORIGIN OF ALL DRAINS AND UTILITIES PRIOR TO REMOVAL/TERMINATION TO DETERMINE IF DRAINS OR UTILITY IS ACTIVE, AND SERVICES ANY ON OR OFF-SITE STRUCTURE TO REMAIN. 5/20/24//////// THE CONTRACTOR SHALL NOTIFY ENGINEER IMMEDIATELY OF ANY SUCH UTILITY FOUND AND SHALL MAINTAIN THESE UTILITIES UNTIL PERMANENT SOLUTION IS IN PLACE. 12. PAVEMENT REMOVAL LIMITS ARE SHOWN FOR CONTRACTOR'S CONVENIENCE. ADDITIONAL PAVEMENT REMOVAL MAY BE REQUIRED DEPENDING ON THE CONTRACTOR'S OPERATION. CONTRACTOR TO VERIFY FULL E NEW H 13. THE CONTRACTOR SHALL REMOVE AND DISPOSE OF ALL EXISTING STRUCTURES, CONCRETE PADS, UTILITIES NEIL AND PAVEMENT WITHIN THE WORK LIMITS SHOWN UNLESS SPECIFICALLY IDENTIFIED TO REMAIN. ITEMS TO Α. HANSEN BE REMOVED INCLUDE BUT ARE NOT LIMITED TO: CONCRETE, PAVEMENT, CURBS, LIGHTING, MANHOLES, No. 15227 CATCH BASINS, UNDER GROUND PIPING, POLES, STAIRS, SIGNS, FENCES, RAMPS, WALLS, BOLLARDS, 14. COORDINATE ALL WORK WITHIN THE PUBLIC RIGHT OF WAYS WITH THE CITY OF PORTSMOUTH AND PEASE 05/20/2024 15. REMOVE TREES AND BRUSH AS REQUIRED FOR COMPLETION OF WORK. CONTRACTOR SHALL GRUB AND REMOVE ALL STUMPS WITHIN LIMITS OF WORK AND DISPOSE OF OFF SITE IN ACCORDANCE WITH FEDERAL, 16. CONTRACTOR SHALL PROTECT ALL PROPERTY MONUMENTATION THROUGHOUT DEMOLITION AND CONSTRUCTION OPERATIONS. SHOULD ANY MONUMENTATION BE DISTURBED BY BY THE CONTRACTOR, THE CONTRACTOR SHALL EMPLOY A NEW HAMPSHIRE LICENSED SURVEYOR TO REPLACE DISTURBED MONUMENTS 17. PROVIDE INLET PROTECTION BARRIERS AT ALL CATCH BASINS/CURB INLETS WITHIN CONSTRUCTION LIMITS AS WELL AS CATCH BASINS/CURB INLETS THAT MAY RECEIVE RUNOFF FROM CONSTRUCTION ACTIVITIES. INLET PROTECTION BARRIERS SHALL BE MAINTAINED FOR THE DURATION OF THE PROJECT. INLET PROTECTION BARRIERS SHALL BE "HIGH FLOW SILT SACK" BY ACF ENVIRONMENTAL OR EQUAL. INSPECT SCALE IN FEET BARRIERS WEEKLY AND AFTER EACH RAIN EVENT OF 0.25 INCHES OR GREATER. CONTRACTOR SHALL COMPLETE A MAINTENANCE INSPECTION REPORT AFTER EACH INSPECTION. SEDIMENT DEPOSITS SHALL BE REMOVED AFTER EACH STORM EVENT OR MORE OFTEN IF THE FABRIC BECOMES CLOGGED OR SEDIMENT HAS GRAPHIC SCALE 18. THE CONTRACTOR SHALL PHASE DEMOLITION AND CONSTRUCTION AS REQUIRED TO PROVIDE CONTINUOUS SERVICE TO EXISTING BUSINESSES THROUGHOUT THE CONSTRUCTION PERIOD. EXISTING BUSINESS SERVICES INCLUDE, BUT ARE NOT LIMITED TO ELECTRICAL, COMMUNICATION, FIRE PROTECTION, DOMESTIC Proposed WATER AND SEWER SERVICES. TEMPORARY SERVICES, IF REQUIRED, SHALL COMPLY WITH ALL FEDERAL STATE, LOCAL AND UTILITY COMPANY STANDARDS. CONTRACTOR SHALL PROVIDE DETAILED CONSTRUCTION Industrial SCHEDULE TO OWNER PRIOR TO ANY DEMOLITION/CONSTRUCTION ACTIVITIES. 19. EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO THE START OF ANY CLEARING OR Development 20. THE CONTRACTOR SHALL PAY ALL COSTS NECESSARY FOR TEMPORARY PARTITIONING, BARRICADING, FENCING, SECURITY AND SAFETY DEVICES REQUIRED FOR THE MAINTENANCE OF A CLEAN AND SAFE 21. SAW CUT AND REMOVE PAVEMENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL UTILITIES TO BE REMOVED AND PROPOSED UTILITIES LOCATED IN EXISTING PAVEMENT AREAS TO REMAIN. Lonza Biologics 22. THE CONTRACTOR SHALL ACQUIRE A PDA DIG PERMIT BEFORE ANY EARTH DISTURBANCE CAN TAKE PLACE 23. ALL MONITORING WELLS WITHIN LIMIT OF WORK SHALL BE PROTECTED DURING CONSTRUCTION. IF ANY MONITORING WELL NEEDS TO BE REMOVED OR ADJUSTED THIS WORK SHALL BE COORDINATED WITH THE 24. CONTRACTOR SHALL COORDINATE WITH THE PROJECT SURVEYOR FOR BENCHMARK AND CONTROL POINTS 25. ALL EXCESS SOIL RESULTING FROM THE CONSTRUCTION SHALL REMAIN ON SITE. COORDINATE WITH OWNER AND PEASE DEVELOPMENT AUTHORITY ON FINAL LOCATION OF EXCESS MATERIALS. Portsmouth, 26. BEFORE ANY DEWATERING IS PERFORMED, COORDINATION BETWEEN THE OWNER, CONTRACTOR, PDA, NHDES AND THE AIR FORCE IS REQUIRED TO DETERMINE PROPER PROCEDURES AND PERMITTING REQUIRED New Hampshire AT A MINIMUM A NHDES TEMPORARY DISCHARGE PERMIT IS REQUIRED. Q 5/20/2024 Solar - Amended Approval 4/2/2024 Ph2 IFC Addendum #1 Р 12/15/2023 Ph2 Issued for Constructio 0 N 11/9/2023 Revised P.B. Submission M 9/27/2023 P.B. Submission 9/1/2022 Issued for Construction K 5/27/2022 Issued for Bid MARK DATE DESCRIPTION PROJECT NO: L-0700-013 DATE: 04/03/2018 FILE: L-0700-026-C-DSGN.dwg DRAWN BY CJK CHECKED: NAH APPROVED: PMC PHASE 2 DEMOLITION PLAN MATCH LINE SHEET 1 AS SHOWN SCALE: MATCH LINE SHEET 2 C-161



SITE DAT				PARKING REQ
LOCATION:	TAX MAP 305, LOTS 1 & 2 70 & 80 CORPORATE DRIVE PORTSMOUTH, NH	TAX MAP 305, LOT 6 101 INTERNATIONAL PORTSMOUTH, NH		REQUIRED PARK
ZONING DI	STRICT: AIRPORT, BUSINESS &	COMMERCIAL (ABC)		990 EXISTI <u>180 ANTICI</u>
DIMENSIC	DNAL REQUIREMENTS:			TOTAL REQ
MINIMUM L MINIMUM S	OT AREA: TREET FRONTAGE:	<u>REQUIRED</u> 5 AC 200 FT	PROVIDED 43.4± AC 1,038 FT	PARKING PROVIE EXISTING S <u>PROPOSED</u> TOTAL:
MINIMUM F SIDE SETBA REAR SETBA		70 FT 30 FT 50 FT	70 FT 30 FT 51 FT	



LEGEND

MATCH LINE PROPOSED PROPERTY LINE PROPOSED SETBACK LINE PROPOSED LIMIT OF WORK PROPOSED GRANITE CURB

PROPOSED PAVEMENT SECTION

PROPOSED GRAVEL SECTION

PROPOSED CONCRETE

CONSTRUCT BUILDING TYPICAL COORDINATE PROPOSED CURB RADIUS VERTICAL GRANITE CURB SLOPED GRANITE CURB RIGHT OF WAY DOUBLE SOLID YELLOW LINE SINGLE SOLID WHITE LINE

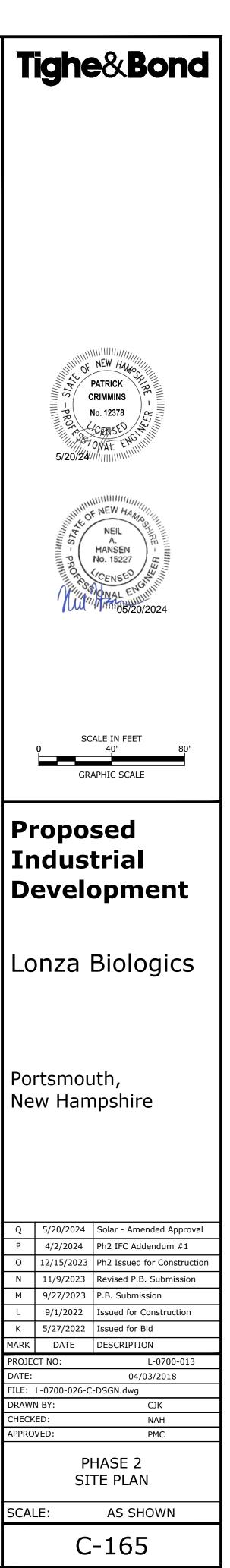
EXISTING) — CONST TIP DOWN RAMP — CONST

BEGIN VGC (MEET/MATCH

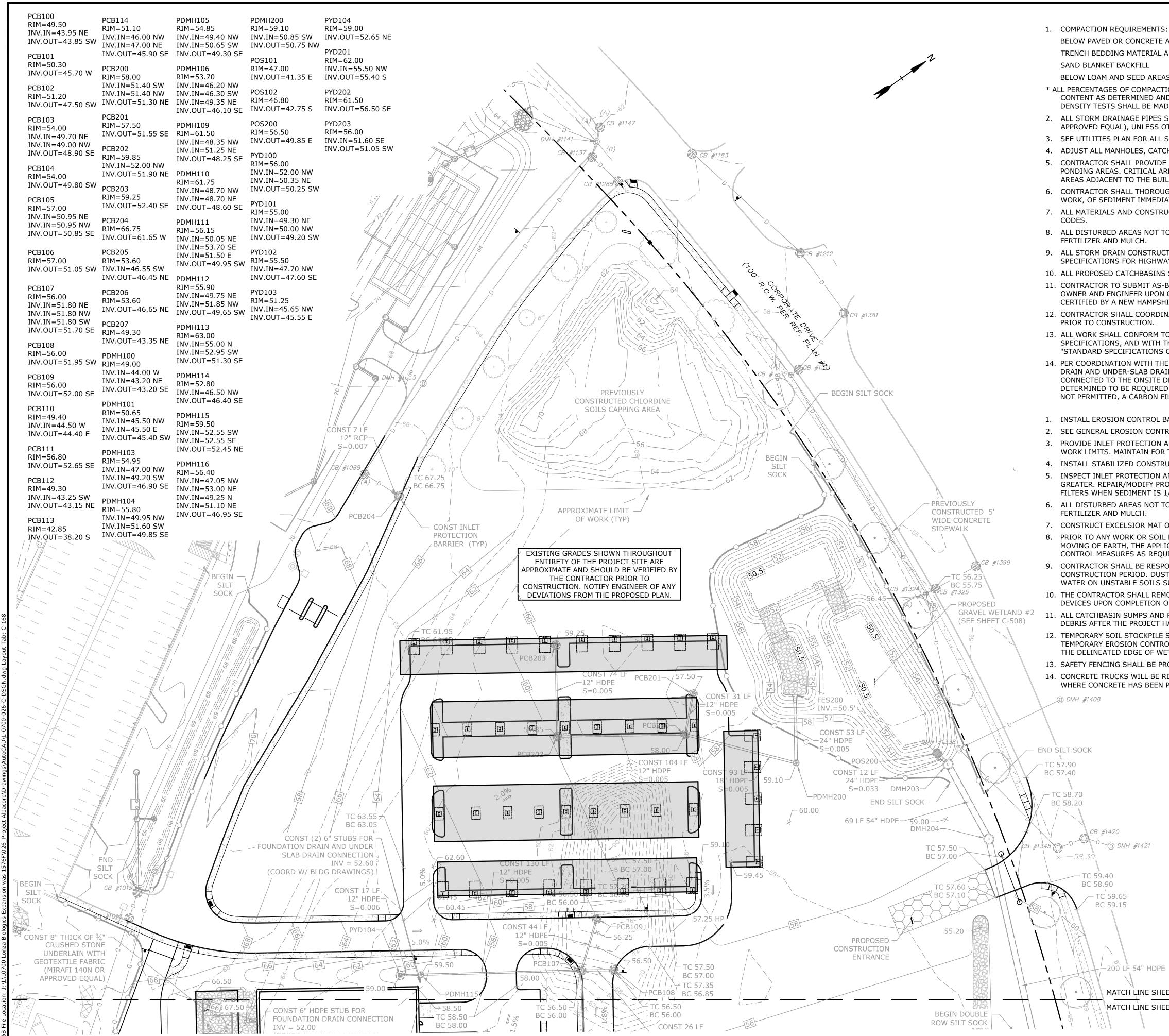
AND STOP BAR - CONST TIP DOWN RAMP - BEGIN VGC (MEET/MATCH EXISTING)

R1-1 "STOP SIGN"

MATCH LINE SHEET 1 MATCH LINE SHEET 2

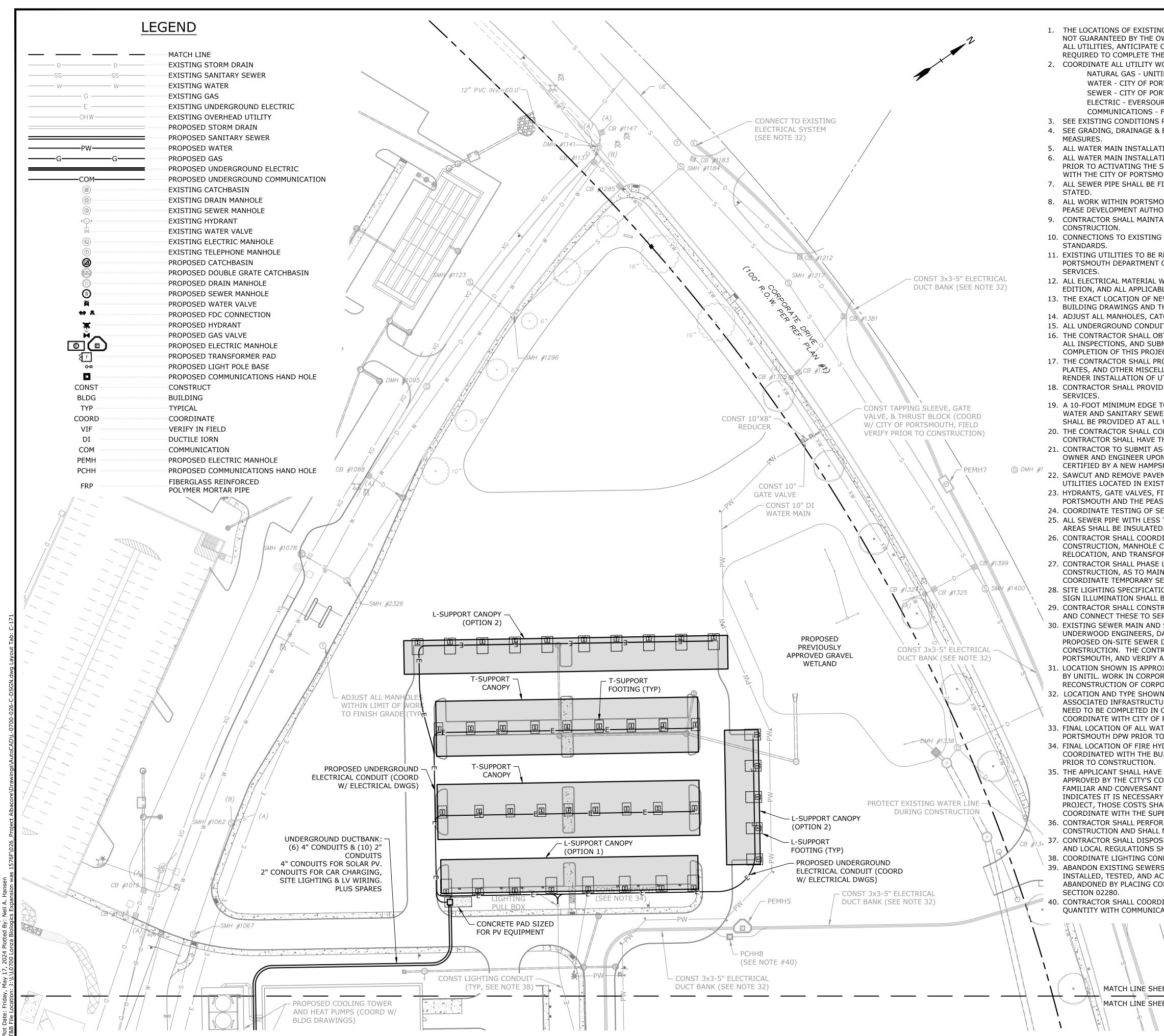


E SHEET 2



ZPS

GRADING AND DRAINAGE NOTES:		Tighe&Bond
S: AREAS 95%		
AND 95%		
AS 90%		
TION SHALL BE OF THE MAXIMUM DRY DE	ASTM D-1557, METHOD C FIELD	
DE IN ACCORDANCE WITH ASTM D-1556 SHALL BE HIGH DENSITY POLYETHYLENE		
OTHERWISE SPECIFIED. SITE UTILITY INFORMATION.		
CHBASINS, CURB BOXES, ETC. WITHIN LI	MITS OF WORK TO FINISH GRADE.	
E A FINISH PAVEMENT SURFACE AND LAW REAS INCLUDE BUILDING ENTRANCES, EX ILDING.	XITS, RAMPS AND LOADING DOCK	
JGHLY CLEAN ALL CATCHBASINS AND DRA IATELY UPON COMPLETION OF CONSTRUC RUCTION SHALL CONFORM WITH APPLICAN	TION.	
TO BE PAVED OR OTHERWISE TREATED S	HALL RECEIVE 6" LOAM, SEED	PATRICK
CTION SHALL BE IN ACCORDANCE WITH T AYS AND BRIDGES, LATEST EDITION.	HE NHDOT STANDARD	CRIMMINS No. 12378 CENSED 5/20/24
S SHALL BE EQUIPPED WITH OIL/GAS SEF		CENSED A
-BUILT PLANS IN DIGITAL FORMAT (.DWG I COMPLETION OF THE PROJECT. AS-BUIL		5/20/24/////////////////////////////////
HIRE LICENSED LAND SURVEYOR. NATE WITH THE PROJECT SURVEYOR FOR	BENCHMARK AND CONTROL POINTS	
TO THE CITY OF PORTSMOUTH DEPARTME		NEIL A. HANSEN No. 15227 HUMINING HANSEN No. 15227 HUMINING HUMININA HUMININA HUMININA HUMININA HUMINI
THE STATE OF NEW HAMPSHIRE DEPARTM	, CURRENT EDITION.	$H_{S}^{(1)} = \begin{pmatrix} A_{1} \\ HANSEN \\ No. 15227 \end{pmatrix} = H_{S}^{(1)}$
E PDA, GROUNDWATER DISCHARGE FROM	ILITY BUILDING WILL BE	HANSEN No. 15227 HANSEN No. 15227 CENSED
DRAINAGE SYSTEM. IF TREATMENT OF THE D DURING THE BUILDING PERMITTING PERMIT		UU 05/20/2024
FILTRATION SYSTEM WILL BE NEEDED.		
BARRIERS AS SHOWN AS FIRST ORDER O FROL NOTES ON DETAIL SHEETS.	F WORK.	
AROUND ALL EXISTING AND PROPOSED (R THE DURATION OF THE PROJECT UNTIL		
RUCTION ENTRANCES.		
AND SILT FENCES DAILY AND AFTER EAC ROTECTION AS NECESSARY TO MAXIMIZE		SCALE IN FEET 0 40' 80'
1/3 THE FILTER HEIGHT. TO BE PAVED OR OTHERWISE TREATED SI	HALL RECEIVE 6" LOAM, SEED,	GRAPHIC SCALE
ON ALL SLOPES STEEPER THAN 3:1.		
L DISTURBANCE COMMENCING ON THE S ICANT SHALL INSTALL ALL EROSION AND		Proposed
UIRED BY STATE AND LOCAL PERMITS AN PONSIBLE TO CONTROL DUST AND WIND		Industrial
ST CONTROL MEASURES SHALL INCLUDE, SUBJECT TO ARID CONDITIONS.		Development
MOVE AND PROPERLY DISPOSE OF ALL TE OF CONSTRUCTION AND FINAL STABALIZ		-
D PIPING SHALL BE THOROUGHLY CLEANE HAS BEEN PAVED.	D TO REMOVE ALL SEDIMENT AND	
SHALL BE SURROUNDED BY SILT FENCE		Lonza Biologics
ETLAND. ROVIDED AROUND STOCKPILES OVER 10		
REQUIRED TO WASH OUT (IF NECESSARY) SHOOTS ONLY WITHIN AREAS	
PLACED. NO OTHER WASH OUT WILL BE	allowed. GEND	
		Portsmouth,
	MATCH LINE	New Hampshire
56	PROPOSED CONTOUR LINE PROPOSED DRAIN LINE (TYP)	
	PROPOSED DRAIN LINE (TYP)	
$\hat{\mathbf{O}}$	INLET PROTECTION SILT SACK	
Ø	PROPOSED CATCHBASIN PROPOSED DOUBLE GRATE	Q 5/20/2024 Solar - Amended Approval
0	CATCHBASIN PROPOSED DRAIN MANHOLE	P4/2/2024Ph2 IFC Addendum #1O12/15/2023Ph2 Issued for Construction
CONST BLDG		N 11/9/2023 Revised P.B. Submission
ТҮР	TYPICAL	M9/27/2023P.B. SubmissionL9/1/2022Issued for Construction
COORD RD	ROOF DRAIN	K 5/27/2022 Issued for Bid MARK DATE DESCRIPTION
VIF VERIFY IN FIELD TC TOP OF CURB		PROJECT NO: L-0700-013 DATE: 04/03/2018
BC	FILE: L-0700-026-C-DSGN.dwg	
		CHECKED: NAH
=		APPROVED: PMC PHASE 2 GRADING,
_		DRAINAGE & EROSION
		CONTROL PLAN SCALE: AS SHOWN
EET 2		
		C-168

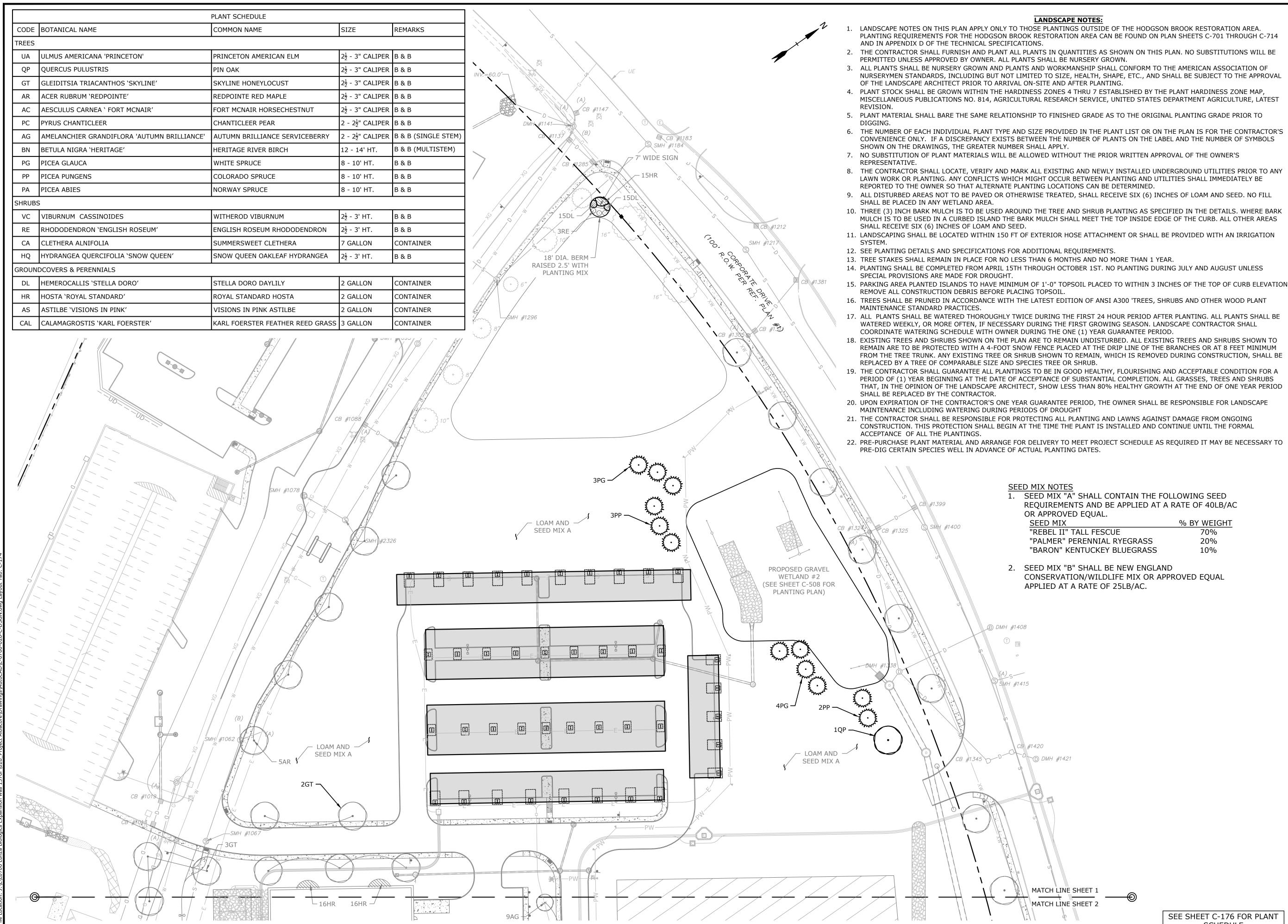


P

- NOT GUARANTEED BY THE OV ALL UTILITIES, ANTICIPATE REQUIRED TO COMPLETE THE 2. COORDINATE ALL UTILITY WO NATURAL GAS - UNITI
 - WATER CITY OF POR SEWER - CITY OF POR ELECTRIC - EVERSOUR COMMUNICATIONS -
- 3. SEE EXISTING CONDITIONS 4. SEE GRADING, DRAINAGE & E MEASURES.
- 5. ALL WATER MAIN INSTALLATI 6. ALL WATER MAIN INSTALLATI
- PRIOR TO ACTIVATING THE S WITH THE CITY OF PORTSMO 7. ALL SEWER PIPE SHALL BE FI
- STATED. 8. ALL WORK WITHIN PORTSMO
- PEASE DEVELOPMENT AUTHO 9. CONTRACTOR SHALL MAINTA
- CONSTRUCTION. 10. CONNECTIONS TO EXISTING
- STANDARDS. 11. EXISTING UTILITIES TO BE R PORTSMOUTH DEPARTMENT
- SERVICES. 12. ALL ELECTRICAL MATERIAL W
- EDITION, AND ALL APPLICABL
- 13. THE EXACT LOCATION OF NEV BUILDING DRAWINGS AND TH
- 14. ADJUST ALL MANHOLES, CAT
- 15. ALL UNDERGROUND CONDUI 16. THE CONTRACTOR SHALL OB
- ALL INSPECTIONS, AND SUBN COMPLETION OF THIS PROJEC
- 17. THE CONTRACTOR SHALL PRO PLATES, AND OTHER MISCELL RENDER INSTALLATION OF U
- 18. CONTRACTOR SHALL PROVID SERVICES.
- 19. A 10-FOOT MINIMUM EDGE T WATER AND SANITARY SEWE SHALL BE PROVIDED AT ALL
- 20. THE CONTRACTOR SHALL COI
- CONTRACTOR SHALL HAVE TH 21. CONTRACTOR TO SUBMIT AS-
- OWNER AND ENGINEER UPON CERTIFIED BY A NEW HAMPSH
- 22. SAWCUT AND REMOVE PAVE UTILITIES LOCATED IN EXIST
- 23. HYDRANTS, GATE VALVES, FI PORTSMOUTH AND THE PEAS
- 24. COORDINATE TESTING OF SE
- 25. ALL SEWER PIPE WITH LESS
- AREAS SHALL BE INSULATED. 26. CONTRACTOR SHALL COORDI
- CONSTRUCTION, MANHOLE C
- **RELOCATION, AND TRANSFOR** 27. CONTRACTOR SHALL PHASE
- CONSTRUCTION, AS TO MAIN COORDINATE TEMPORARY SE
- 28. SITE LIGHTING SPECIFICATIO SIGN ILLUMINATION SHALL
- 29. CONTRACTOR SHALL CONSTR AND CONNECT THESE TO SEF
- 30. EXISTING SEWER MAIN AND UNDERWOOD ENGINEERS, DA PROPOSED ON-SITE SEWER
- CONSTRUCTION. THE CONT PORTSMOUTH, AND VERIFY A
- 31. LOCATION SHOWN IS APPROX BY UNITIL. WORK IN CORPOR
- RECONSTRUCTION OF CORPO 32. LOCATION AND TYPE SHOWN
- ASSOCIATED INFRASTRUCTU NEED TO BE COMPLETED IN
- COORDINATE WITH CITY OF F 33. FINAL LOCATION OF ALL WAT
- PORTSMOUTH DPW PRIOR TO
- 34. FINAL LOCATION OF FIRE HYD COORDINATED WITH THE BUI PRIOR TO CONSTRUCTION.
- 35. THE APPLICANT SHALL HAVE APPROVED BY THE CITY'S CO FAMILIAR AND CONVERSANT INDICATES IT IS NECESSARY PROJECT, THOSE COSTS SHA COORDINATE WITH THE SUPE 36. CONTRACTOR SHALL PERFOR CONSTRUCTION AND SHALL 37. CONTRACTOR SHALL DISPOS
- AND LOCAL REGULATIONS SH 38. COORDINATE LIGHTING CON 39. ABANDON EXISTING SEWERS INSTALLED, TESTED, AND AC
- ABANDONED BY PLACING CO SECTION 02280.
- 40. CONTRACTOR SHALL COORDI QUANTITY WITH COMMUNICA
 - MATCH LINE SHEE
 - MATCH LINE SHEE

UTILITY NOTES: G UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE WNER OR ENGINEER. IT IS THE CONTRACTOR'S RESPONSIBILITY TO LOCATE CONFLICTS, REPAIR EXISTING UTILITIES, AND RELOCATE EXISTING UTILITIES E WORK AT NO ADDITIONAL COST TO THE OWNER. ORK WITH APPROPRIATE UTILITY COMPANY.	Tighe&Bond
IL RTSMOUTH DPW RTSMOUTH DPW RCE	
FAIRPOINT, COMCAST, FIRSTLIGHT PLAN FOR BENCHMARK INFORMATION. EROSION CONTROL PLAN FOR PROPOSED GRADING AND EROSION CONTROL	
IONS SHALL BE CLASS 52, CEMENT LINED DUCTILE IRON PIPE. IONS SHALL BE PRESSURE TESTED AND CHLORINATED AFTER CONSTRUCTION SYSTEM. CONTRACTOR SHALL COORDINATE CHLORINATION AND TESTING OUTH WATER DEPARTMENT. IBERGLASS REINFORCED POLYMER MORTAR (FRP) PIPE UNLESS OTHERWISE	
OUTH ROWS SHALL BE COORDINATED WITH CITY OF PORTSMOUTH AND THE	
DRITY. AIN UTILITY SERVICES TO ABUTTING PROPERTIES THROUGHOUT	
WATER MAIN SHALL BE CONSTRUCTED TO CITY OF PORTSMOUTH	PATRICK
EMOVED SHALL BE CAPPED AT THE MAIN AND MEET THE CITY OF OF PUBLIC WORKS STANDARDS FOR CAPPING OF WATER AND SEWER	PATRICK PATRICK CRIMMINS No. 12378
VORKMANSHIP SHALL CONFORM TO THE NATIONAL ELECTRIC CODE, LATEST LE STATE AND LOCAL CODES. W UTILITY SERVICES AND CONNECTIONS SHALL BE COORDINATED WITH THE HE UTILITY COMPANIES.	5/20/24/////////////////////////////////
CH BASINS, CURB BOXES, ETC. WITHIN LIMITS OF WORK TO FINISH GRADE. TS SHALL HAVE NYLON PULL ROPES TO FACILITATE PULLING CABLES. TAIN, PAY FOR, AND COMPLY WITH ALL REQUIRED PERMITS, ARRANGE FOR MIT COPIES OF ACCEPTANCE CERTIFICATES TO THE OWNER PRIOR TO THE CT.	NEIL A. HANSEN No. 15227 HUILING HANSEN No. 15227
OVIDE AND INSTALL ALL MANHOLES, BOXES, FITTINGS, CONNECTORS, COVER LANEOUS ITEMS NOT NECESSARILY DETAILED ON THESE DRAWINGS TO TILITIES COMPLETE AND OPERATIONAL. DE EXCAVATION, BEDDING, BACKFILL AND COMPACTION FOR NATURAL GAS	No. 15227
O EDGE HORIZONTAL SEPARATION SHALL BE PROVIDED BETWEEN ALL ER LINES. AN 18-INCH MINIMUM OUTSIDE TO OUTSIDE VERTICAL SEPARATION WATER/SANITARY SEWER CROSSINGS. WITACT "DIG-SAFE" 72 HOURS PRIOR TO COMMENCING CONSTRUCTION. THE HE "DIG-SAFE" NUMBER ON SITE AT ALL TIMES. G-BUILT PLANS IN DIGITAL FORMAT (.DWG AND .PDF FILES) ON DISK TO THE	
N COMPLETION OF THE PROJECT. AS-BUILTS SHALL BE PREPARED AND HIRE LICENSED LAND SURVEYOR. MENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL PROPOSED FING PAVEMENT AREAS TO REMAIN. ITTINGS, ETC. SHALL MEET THE REQUIREMENTS OF THE CITY OF SE DEVELOPMENT AUTHORITY.	SCALE IN FEET 0 40' 80' GRAPHIC SCALE
EWER CONSTRUCTION WITH THE CITY OF PORTSMOUTH. THAN 6' OF COVER IN PAVED AREAS OR LESS THAN 4' OF COVER IN UNPAVED	GRAFIIC SCALL
 INATE ALL ELECTRIC WORK INCLUDING BUT NOT LIMITED TO: CONDUIT CONSTRUCTION, UTILITY POLE CONSTRUCTION, OVERHEAD WIRE RMER CONSTRUCTION WITH POWER COMPANY. UTILITY CONSTRUCTION, PARTICULARLY WATER MAIN AND GAS MAIN NTAIN CONTINUOUS SERVICE TO ABUTTING PROPERTIES. CONTRACTOR SHALL ERVICES TO ABUTTERS WITH THE UTILITY COMPANY AND AFFECTED ABUTTER. ONS, CONDUIT LAYOUT AND CIRCUITRY FOR PROPOSED SITE LIGHTING AND BE PROVIDED BY THE PROJECT ELECTRICAL ENGINEER.	Proposed Industrial Development
CONSTRUCTION, UTILITY POLE CONSTRUCTION, OVERHEAD WIRE RMER CONSTRUCTION WITH POWER COMPANY. UTILITY CONSTRUCTION, PARTICULARLY WATER MAIN AND GAS MAIN NTAIN CONTINUOUS SERVICE TO ABUTTING PROPERTIES. CONTRACTOR SHALL ERVICES TO ABUTTERS WITH THE UTILITY COMPANY AND AFFECTED ABUTTER. ONS, CONDUIT LAYOUT AND CIRCUITRY FOR PROPOSED SITE LIGHTING AND BE PROVIDED BY THE PROJECT ELECTRICAL ENGINEER. RUCT ALL UTILITIES AND DRAINS TO WITHIN 10' OF THE FOUNDATION WALLS RVICE STUBS FROM THE BUILDING. STRUCTURES IN GOOSE BAY DRIVE ARE BASED ON A PROPOSED DESIGN BY ATED JULY 28, 2017, AND WAS CONSTRUCTED IN SUMMER 2018. THE DESIGN ELEVATIONS ARE BASED ON THE UNDERWOOD PLAN DURING RACTOR SHALL COORDINATE SEWER CONSTRUCTION WITH THE CITY OF ALL INVERTS PRIOR TO CONSTRUCTION. XIMATE ONLY. FINAL DESIGN OF NATURAL GAS SERVICE TO BE COMPLETED	Industrial
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CODE	BOTANICAL NAME	COMMON NAME	SIZE	REMARKS
TREES			-	_
UA	ULMUS AMERICANA 'PRINCETON'	PRINCETON AMERICAN ELM	2 ¹ / ₂ - 3" CALIPER	B & B
QP	QUERCUS PULUSTRIS	PIN OAK	$2\frac{1}{2}$ - 3" CALIPER	B & B
GT	GLEIDITSIA TRIACANTHOS 'SKYLINE'	SKYLINE HONEYLOCUST	$2\frac{1}{2}$ - 3" CALIPER	B & B
AR	ACER RUBRUM 'REDPOINTE'	REDPOINTE RED MAPLE	2 <u>1</u> - 3" CALIPER	B & B
AC	AESCULUS CARNEA ' FORT MCNAIR'	FORT MCNAIR HORSECHESTNUT	2 ¹ / ₂ - 3" CALIPER	В&В
PC	PYRUS CHANTICLEER	CHANTICLEER PEAR	2 - $2\frac{1}{2}$ " CALIPER	B & B
AG	AMELANCHIER GRANDIFLORA 'AUTUMN BRILLIANCE'	AUTUMN BRILLIANCE SERVICEBERRY	2 - 2 <u>1</u> " CALIPER	B & B (SINGLE STEM)
BN	BETULA NIGRA `HERITAGE'	HERITAGE RIVER BIRCH	12 - 14' HT.	B & B (MULTISTEM)
PG	PICEA GLAUCA	WHITE SPRUCE	8 - 10' HT.	B & B
PP	PICEA PUNGENS	COLORADO SPRUCE	8 - 10' HT.	B & B
PA	PICEA ABIES	NORWAY SPRUCE	8 - 10' HT.	B & B
SHRUB	S			
VC	VIBURNUM CASSINOIDES	WITHEROD VIBURNUM	2 <u>1</u> - 3' HT.	B & B
RE	RHODODENDRON 'ENGLISH ROSEUM'	ENGLISH ROSEUM RHODODENDRON	2 <u>1</u> - 3' HT.	B & B
CA	CLETHERA ALNIFOLIA	SUMMERSWEET CLETHERA	7 GALLON	CONTAINER
HQ	HYDRANGEA QUERCIFOLIA 'SNOW QUEEN'	SNOW QUEEN OAKLEAF HYDRANGEA	2 <u>1</u> - 3' HT.	B & B
GROUN	IDCOVERS & PERENNIALS			
DL	HEMEROCALLIS 'STELLA DORO'	STELLA DORO DAYLILY	2 GALLON	CONTAINER
HR	HOSTA 'ROYAL STANDARD'	ROYAL STANDARD HOSTA	2 GALLON	CONTAINER
AS	ASTILBE 'VISIONS IN PINK'	VISIONS IN PINK ASTILBE	2 GALLON	CONTAINER
CAL	CALAMAGROSTIS 'KARL FOERSTER'	KARL FOERSTER FEATHER REED GRASS	3 GALLON	CONTAINER



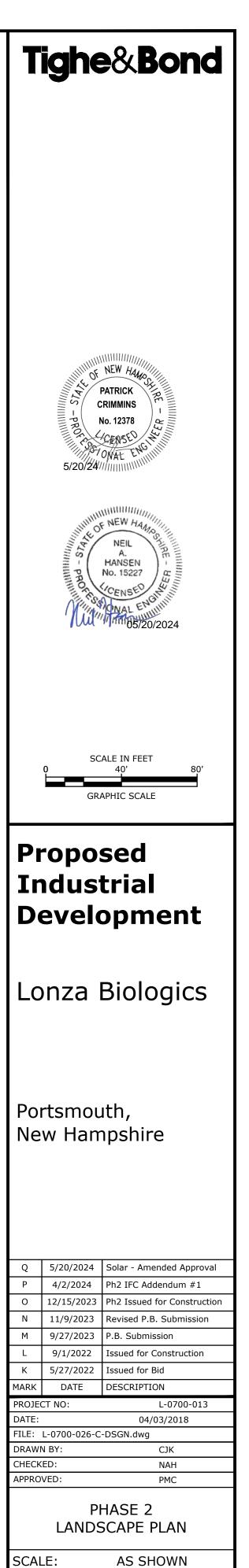
May 17, 2024 3:51 PM By May 17, 2024 Plotted By:

1. SEED MIX "A" SHALL CONTAIN THE FOLLOWING SEED REQUIREMENTS AND BE APPLIED AT A RATE OF 40LB/AC % BY WEIGHT

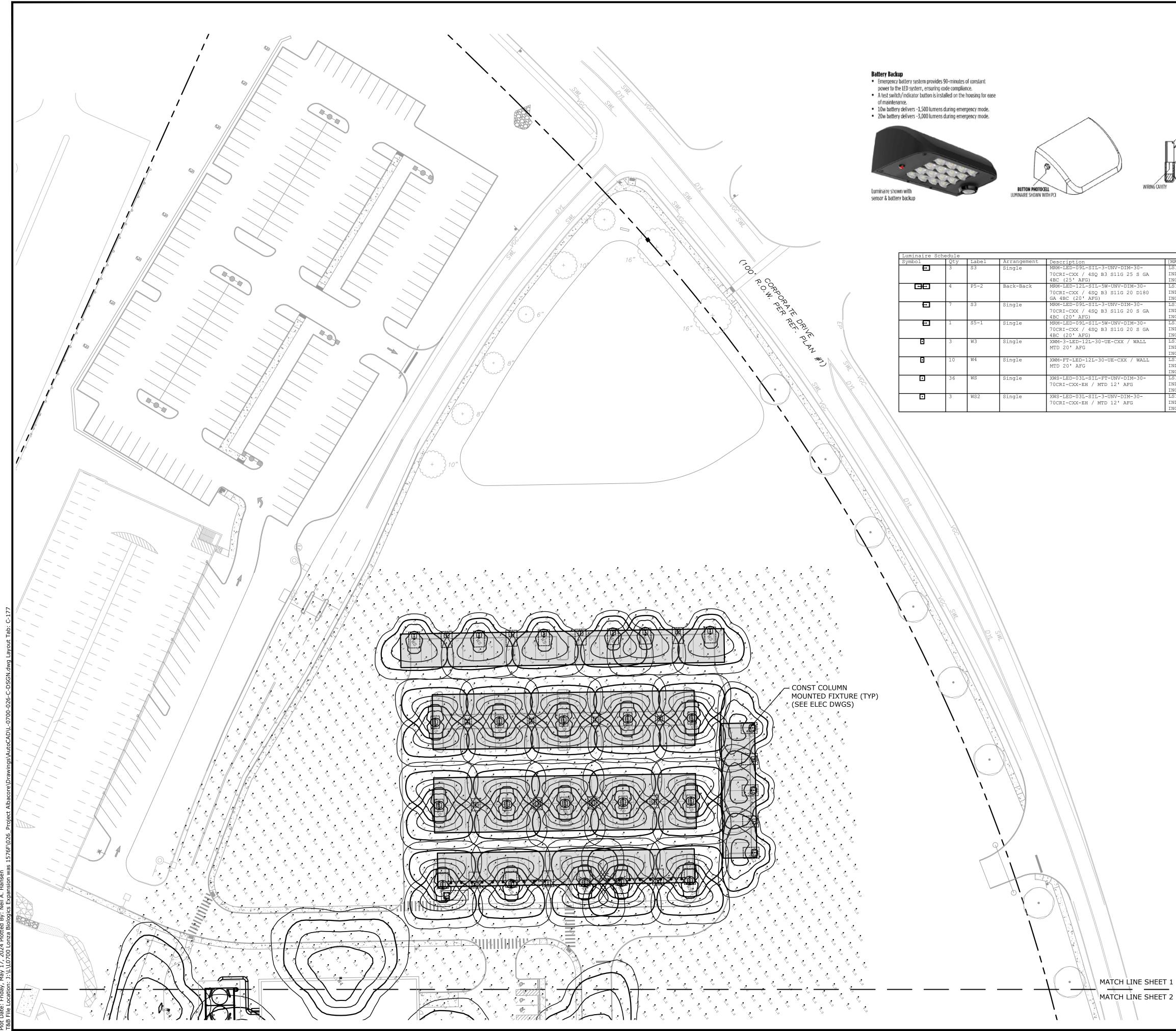
	70 DT WEIGHT
BEL II" TALL FESCUE	70%
MER" PERENNIAL RYEGRASS	20%
ON" KENTUCKEY BLUEGRASS	10%

CONSERVATION/WILDLIFE MIX OR APPROVED EQUAL

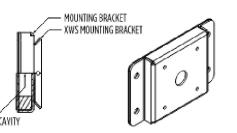
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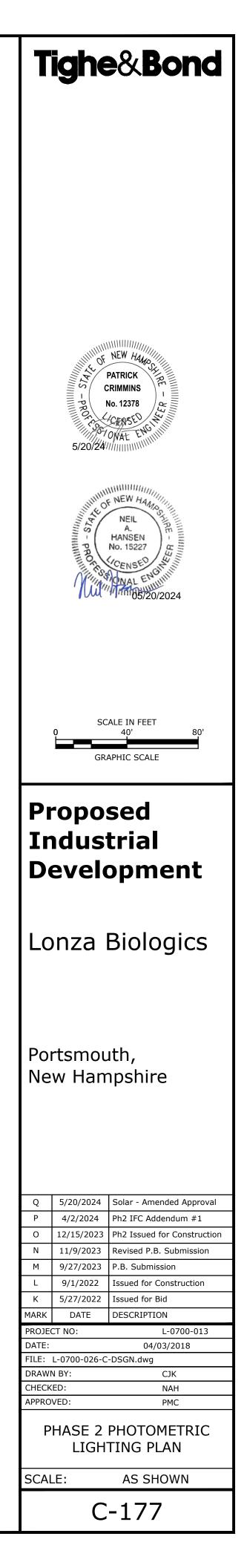
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Save Date: May 17, 2024 3:51 PM By: NAHANSEN Date: Friday, May 17, 2024 Plotted By: Neil A. Hansen Eilo Location: 1.01010001 access Biologics Expansion was 157650026 Bross



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GENERAL PROJECT INFORMATION PROJECT LESSOR: PEASE DEVELOPMENT AUTHORITY FE INTERNATIONAL DRIVE	 ALL AREAS SHALL BE STABILIZED WITHIN 45 DA WHEN CONSTRUCTION ACTIVITY PERMANENTLY
GENERAL PROJECT INFORMATIONPROJECT LESSOR:PEASE DEVELOPMENT AUTHORITY 55 INTERNATIONAL DRIVE PORTSMOUTH, NH 03801PROJECT OWNER/ APPLICANT:LONZA BIOLOGICS 101 INTERNATIONAL DRIVE PORTSMOUTH, NH 03801PROJECT ADDRESS:70 & 80 CORPORATE DRIVE PORTSMOUTH, NH 03801PROJECT LATITUDE:43°-04'-59.0"NPROJECT LONGITUDE:71°-48'-09.7"W	OF NEARBY SURFACE WATERS OR DELINEATED WITHIN SEVEN (7) DAYS OR PRIOR TO A RAIN E CEASES PERMANENTLY IN AN THESE AREAS, SIL BARRIERS AND ANY EARTH/DIKES SHALL BE REI
PORTSMOUTH, NH 03801 PROJECT ADDRESS: 70 & 80 CORPORATE DRIVE PORTSMOUTH, NH 03801	ESTABLISHED. 6. DURING CONSTRUCTION, RUNOFF WILL BE DIVE DIKES, PIPING OR STABILIZED CHANNELS WHEF
PROJECT LATITUDE: 43°-04'-59.0"N PROJECT LONGITUDE: 71°-48'-09.7"W	WILL BE FILTERED THROUGH SILT FENCES, MUL SOCKS. ALL STORM DRAIN BASIN INLETS SHALL
PROJECT DESCRIPTION THE PROJECT CONSISTS OF THE EXPANSION OF LONZA BIOLOGICS, WHICH INCLUDES THE CONSTRUCTION OF 4 PROPOSED BUILDINGS, 1 PARKING GARAGE, AND ASSOCIATED SITE IMPROVEMENTS.	AND TRASH RACKS. THE SITE SHALL BE STABIL DUST CONTROL: 1. THE CONTRACTOR SHALL BE RESPONSIBLE TO C CONSTRUCTION PERIOD.
DISTURBED AREA THE TOTAL AREA TO BE DISTURBED IS APPROXIMATELY 21.3 ACRES.	 DUST CONTROL METHODS SHALL INCLUDE, BUT EXPOSED AREAS, COVERING LOADED DUMP TRU MULCHING. DUST CONTROL MEASURES SHALL BE UTILIZED
SOIL CHARACTERISTICS BASED ON THE HIGH INTENSITY SOIL SURVEY PREPARED BY GOVE ENVIRONMENTAL SERVICES, INC. IN DECEMBER 2015, THE SITE SOILS VARY FROM WELL DRAINED TO VERY POORLY DRAINED	DUST FROM THE SITE TO ABUTTING AREAS.
AND PRIMARILY CONSIST OF SOMEWHAT POORLY DRAINED SOILS.	 LOCATE STOCKPILES A MINIMUM OF 50 FEET AW CULVERTS. ALL STOCKPILES SHOULD BE SURROUNDED WIT
THE STORM WATER RUNOFF WILL ULTIMATELY DISCHARGE INTO HODGSON BROOK	MEASURES PRIOR TO THE ONSET OF PRECIPITA 3. PERIMETER BARRIERS SHOULD BE MAINTAINED TO ACCOMMODATE THE DELIVERY AND REMOVA
 CUT AND CLEAR TREES. CONSTRUCT TEMPORARY AND PERMANENT SEDIMENT, EROSION AND DETENTION CONTROL FACILITIES. EROSION, SEDIMENT AND DETENTION MEASURES SHALL BE INSTALLED PRIOR TO ANY EARTH MOVING OPERATIONS THAT WILL INFLUENCE STORMWATER RUNOFF SUCH AS: 	INTEGRITY OF THE BARRIER SHOULD BE INSPEC 4. PROTECT ALL STOCKPILES FROM STORMWATER CONTROL MEASURES SUCH AS BERMS, SILT SOO PREVENT MIGRATION OF MATERIAL BEYOND THE
 NEW CONSTRUCTION CONTROL OF DUST NEARNESS OF CONSTRUCTION SITE TO RECEIVING WATERS CONSTRUCTION DURING LATE WINTER AND EARLY SPRING 	OFF SITE VEHICLE TRACKING: 1. THE CONTRACTOR SHALL CONSTRUCT STABILIZ ANY EXCAVATION ACTIVITIES.
 ALL PERMANENT DITCHES, SWALES, DETENTION, RETENTION AND SEDIMENTATION BASINS TO BE STABILIZED USING THE VEGETATIVE AND NON-STRUCTURAL BMPS PRIOR TO DIRECTING RUNOFF TO THEM. CLEAR AND DISPOSE OF DEBRIS. 	VEGETATION: 1. TEMPORARY GRASS COVER: A. SEEDBED PREPARATION: a. APPLY FERTILIZER AT THE RATE OF 600 PC
 CONSTRUCT TEMPORARY CULVERTS AND DIVERSION CHANNELS AS REQUIRED. GRADE AND GRAVEL ROADWAYS AND PARKING AREAS - ALL ROADS AND PARKING AREA SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE. 	LIMESTONE (EQUIVALENT TO 50 PERCENT RATE OF THREE (3) TONS PER ACRE; B. SEEDING:
 BEGIN PERMANENT AND TEMPORARY SEEDING AND MULCHING. ALL CUT AND FILL SLOPES SHALL BE SEEDED AND MULCHED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE. DAILY, OR AS REQUIRED, CONSTRUCT TEMPORARY BERMS, DRAINS, DITCHES, PERIMETER EROSION CONTROL MEASURES, SEDIMENT TRAPS, ETC., MULCH AND SEED AS REQUIRED. SEDIMENT TRAPS AND/OR BASINS SHALL BE USED AS NECESSARY TO CONTAIN RUNOFF UNTIL SOILS ARE STABILIZED. 	 a. UTILIZE ANNUAL RYE GRASS AT A RATE OF b. WHERE THE SOIL HAS BEEN COMPACTED E SOIL TO A DEPTH OF TWO (2) INCHES BEF c. APPLY SEED UNIFORMLY BY HAND, CYCLOI INCLUDING SEED AND FERTILIZER). HYDR BE LEFT ON SOIL SURFACE. SEEDING RATE
 FINISH PAVING ALL ROADWAYS AND PARKING LOTS. INSPECT AND MAINTAIN ALL EROSION AND SEDIMENT CONTROL MEASURES. COMPLETE PERMANENT SEEDING AND LANDSCAPING. REMOVE TRAPPED SEDIMENTS FROM COLLECTOR DEVICES AS APPROPRIATE AND THEN REMOVE TEMPORARY EROSION CONTROL MEASURES. 	HYDROSEEDING; C. MAINTENANCE: a. TEMPORARY SEEDING SHALL BE PERIODIC THE SOIL SURFACE SHOULD BE COVERED
SPECIAL CONSTRUCTION NOTES: 1. THE CONSTRUCTION SEQUENCE MUST LIMIT THE DURATION AND AREA OF DISTURBANCE. 2. THE PROJECT IS TO BE MANAGED IN A MANNER THAT MEETS THE REQUIREMENTS AND	EROSION OR SEDIMENTATION IS APPAREN TEMPORARY MEASURES USED IN THE INTE DAMS, ETC.). 2. VEGETATIVE PRACTICE: A. FOR PERMANENT MEASURES AND PLANTINGS
INTENT OF RSA 430:53 AND CHAPTER AGR 3800 RELATIVE TO INVASIVE SPECIES.	 a. LIMESTONE SHALL BE THOROUGHLY INCOM OF THREE (3) TONS PER ACRE IN ORDER T b. FERTILIZER SHALL BE SPREAD ON THE TOM
 ALL EROSION CONTROL MEASURES AND PRACTICES SHALL CONFORM TO THE "NEW HAMPSHIRE STORMWATER MANUAL VOLUME 3: EROSION AND SEDIMENT CONTROLS DURING CONSTRUCTION" PREPARED BY THE NHDES. PRIOR TO ANY WORK OR SOIL DISTURBANCE, CONTRACTOR SHALL SUBMIT SHOP 	SURFACE. FERTILIZER APPLICATION RATE 10-20-20 FERTILIZER; c. SOIL CONDITIONERS AND FERTILIZER SHA RATES AND SHALL BE THOROUGHLY WORK
DRAWINGS FOR EROSION CONTROL MEASURES AS REQUIRED IN THE PROJECT MANUAL. 3. CONTRACTOR SHALL INSTALL TEMPORARY EROSION CONTROL BARRIERS, INCLUDING HAY BALES, SILT FENCES, MULCH BERMS, SILT SACKS AND SILT SOCKS AS SHOWN IN THESE DRAWINGS AS THE FIRST ORDER OF WORK.	UNTIL THE SURFACE IS FINELY PULVERIZE COMPACTED TO AN EVEN SURFACE CONFO GRADES WITH APPROVED ROLLERS WEIGH POUNDS PER INCH OF WIDTH;
 SILT SACK INLET PROTECTION SHALL BE INSTALLED IN ALL EXISTING AND PROPOSED CATCH BASIN INLETS WITHIN THE WORK LIMITS AND BE MAINTAINED FOR THE DURATION OF THE PROJECT. PERIMETER CONTROLS INCLUDING SILT FENCES, MULCH BERM, SILT SOCK, AND/OR HAY 	d. SEED SHALL BE SOWN AT THE RATE SHOW CALM, DRY DAY, PREFERABLY BY MACHINI WORKMEN. IMMEDIATELY BEFORE SEEDIN
 BALE BARRIERS SHALL BE MAINTAINED FOR THE DURATION OF THE PROJECT UNTIL NON-PAVED AREAS HAVE BEEN STABILIZED. 5. THE CONTRACTOR SHALL REMOVE AND PROPERLY DISPOSE OF ALL TEMPORARY EROSION 	HALF THE SEED SHALL BE SOWN IN ONE D ANGLES TO THE ORIGINAL DIRECTION. IT A DEPTH NOT OVER 1/4 INCH AND ROLLED OVER 100 POUNDS PER LINEAR FOOT OF V
 CONTROL DEVICES UPON COMPLETION OF CONSTRUCTION. ALL DISTURBED AREAS NOT OTHERWISE BEING TREATED SHALL RECEIVE 6" LOAM, SEED AND FERTILIZER. INSPECT ALL INLET PROTECTION AND PERIMETER CONTROLS WEEKLY AND AFTER EACH RAIN 	 e. HAY MULCH SHALL BE APPLIED IMMEDIATE f. THE SURFACE SHALL BE WATERED AND KE WITHOUT WASHING AWAY THE SOIL, UNT
STORM OF 0.25 INCH OR GREATER. REPAIR/MODIFY PROTECTION AS NECESSARY TO MAXIMIZE EFFICIENCY OF FILTER. REPLACE ALL FILTERS WHEN SEDIMENT IS 1/3 THE FILTER HEIGHT.	AREAS WHICH ARE NOT SATISFACTORILY AND ALL NOXIOUS WEEDS REMOVED; g. THE CONTRACTOR SHALL PROTECT AND M ACCEPTED;
 CONSTRUCT EROSION CONTROL BLANKETS ON ALL SLOPES STEEPER THAN 3:1. STABILIZATION: AN AREA SHALL BE CONSIDERED STABLE WHEN ONE OF THE FOLLOWING HAS OCCURRED: AN AREA SHALL BE CONSIDERED STABLE WHEN ONE OF THE FOLLOWING HAS OCCURRED: 	h. A GRASS SEED MIXTURE CONTAINING THE BE APPLIED AT A RATE OF 40 LB/AC OR AP SEED MIX A
 AN AREA SHALL BE CONSIDERED STABLE WHEN ONE OF THE FOLLOWING HAS OCCORRED. A. BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED; B. A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED; C. A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH AS STONE OR RIPRAP HAS BEEN INSTALLED; 	"REBEL II" TALL FESCUE "PALMER" PERENNIAL RYEGRASS "BARON" KENTUCKEY BLUEGRASS IN NO CASE SHALL THE WEED CONTENT ES
 D. EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.; E. IN AREAS TO BE PAVED, "STABLE" MEANS THAT BASE COURSE GRAVELS MEETING THE REQUIREMENTS OF NHOOT STANDARD FOR ROAD AND BRIDGE CONSTRUCTION, 2016, 	SEED SHALL COMPLY WITH STATE AND FEI NO LATER THAN SEPTEMBER 15. IN NO CA 3. DORMANT SEEDING (SEPTEMBER 15 TO FIRST S A. FOLLOW PERMANENT MEASURES SLOPE, LIME
ITEM 304.2 HAVE BEEN INSTALLED. 2. WINTER STABILIZATION PRACTICES: A. ALL PROPOSED VEGETATED AREAS THAT DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15,	REQUIREMENTS. APPLY SEED MIXTURE AT TW INDICATED FOR PERMANENT MEASURES. CONCRETE WASHOUT AREA:
SHALL BE STABILIZED BY SEEDING AND INSTALLING EROSION CONTROL BLANKETS ON SLOPES GREATER THAN 3:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER	 THE CONCRETE DELIVERY TRUCKS SHALL, WHEN AT THEIR OWN PLANT OR DISPATCH FACILITY; IF IT IS NECESSARY, SITE CONTRACTOR SHALL DESIGN FACILITIES TO HANDLE ANTICIPATED W
 ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT EVENTS; B. ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, 	 CONTRACTOR SHALL LOCATE WASHOUT AREAS DRAINS, SWALES AND SURFACE WATERS OR DE INSPECT WASHOUT FACILITIES DAILY TO DETEC MATERIALS NEED TO BE REMOVED.
 SHALL BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS; C. AFTER NOVEMBER 15, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3 	ALLOWABLE NON-STORMWATER DISCHARGES: 1. THE FOLLOWING ARE THE ONLY NON-STORMWA NON-STORMWATER DISCHARGES ARE PROHIBIT
INCHES OF CRUSHED GRAVEL PER NHDOT ITEM 304.3, OR IF CONSTRUCTION IS TO CONTINUE THROUGH THE WINTER SEASON BE CLEARED OF ANY ACCUMULATED SNOW AFTER EACH STORM EVENT;	A. FIRE-FIGHTING ACTIVITIES;B. FIRE HYDRANT FLUSHING;C. WATERS USED TO WASH VEHICLES WHERE D
3. STABILIZATION SHALL BE INITIATED ON ALL LOAM STOCKPILES, AND DISTURBED AREAS, WHERE CONSTRUCTION ACTIVITY SHALL NOT OCCUR FOR MORE THAN TWENTY-ONE (21) CALENDAR DAYS BY THE FOURTEENTH (14TH) DAY AFTER CONSTRUCTION ACTIVITY HAS PERMANENTLY OR TEMPORARILY CEASED IN THAT AREA. STABILIZATION MEASURES TO BE	 D. WATER USED TO CONTROL DUST; E. POTABLE WATER INCLUDING UNCONTAMINAT F. ROUTINE EXTERNAL BUILDING WASH DOWN V G. PAVEMENT WASH WATERS WHERE DETERGEN
. LIN WITCH FOR TELL OF WITCH GENOLD IN THAT AREA DIADILIZATION PLADURED TO DE	G. PAVEMENT WASH WATERS WHERE DETERGEN H. UNCONTAMINATED AIR CONDITIONING/COMP

5 DAYS OF INITIAL DISTURBANCE. ITLY OR TEMPORARILY CEASES WITHIN 100 FEET ED WETLANDS, THE AREA SHALL BE STABILIZED IN EVENT. ONCE CONSTRUCTION ACTIVITY SILT FENCES, MULCH BERMS, HAY BALE REMOVED ONCE PERMANENT MEASURES ARE

DIVERTED AROUND THE SITE WITH EARTH HERE POSSIBLE. SHEET RUNOFF FROM THE SITE MULCH BERMS, HAY BALE BARRIERS, OR SILT HALL BE PROVIDED WITH FLARED END SECTIONS BILIZED FOR THE WINTER BY NOVEMBER 15.

TO CONTROL DUST THROUGHOUT THE

BUT BE NOT LIMITED TO SPRINKLING WATER ON TRUCKS LEAVING THE SITE, AND TEMPORARY

ZED SO AS TO PREVENT THE MIGRATION OF

FAWAY FROM CATCH BASINS, SWALES, AND

WITH TEMPORARY EROSION CONTROL

PITATION. NED AT ALL TIMES, AND ADJUSTED AS NEEDED IOVAL OF MATERIALS FROM THE STOCKPILE. THE SPECTED AT THE END OF EACH WORKING DAY. FER RUN-OFF USING TEMPORARY EROSION SOCK, OR OTHER APPROVED PRACTICE TO THE IMMEDIATE CONFINES OF THE STOCKPILES.

BILIZED CONSTRUCTION ENTRANCE(S) PRIOR TO

0 POUNDS PER ACRE OF 10-10-10. APPLY ENT CALCIUM PLUS MAGNESIUM OXIDE) AT A

E OF 40 LBS/ACRE; ED BY CONSTRUCTION OPERATIONS, LOOSEN BEFORE APPLYING FERTILIZER, LIME AND SEED; CLONE SEEDER, OR HYDROSEEDER (SLURRY YDROSEEDINGS, WHICH INCLUDE MULCH, MAY RATES MUST BE INCREASED 10% WHEN

DDICALLY INSPECTED. AT A MINIMUM, 95% OF RED BY VEGETATION. IF ANY EVIDENCE OF ARENT, REPAIRS SHALL BE MADE AND OTHER INTERIM (MULCH, FILTER BARRIERS, CHECK

NGS:

NCORPORATED INTO THE LOAM LAYER AT A RATE ER TO PROVIDE A PH VALUE OF 5.5 TO 6.5; TOP LAYER OF LOAM AND WORKED INTO THE ATE SHALL BE 800 POUNDS PER ACRE OF

SHALL BE APPLIED AT THE RECOMMENDED ORKED INTO THE LOAM. LOAM SHALL BE RAKED RIZED, SMOOTH AND EVEN, AND THEN NFORMING TO THE REQUIRED LINES AND EIGHING BETWEEN 4-1/2 POUNDS AND 5-1/2

HOWN BELOW. SOWING SHALL BE DONE ON A HINE, BUT IF BY HAND, ONLY BY EXPERIENCED EDING, THE SOIL SHALL BE LIGHTLY RAKED. ONE NE DIRECTION AND THE OTHER HALF AT RIGHT I. IT SHALL BE LIGHTLY RAKED INTO THE SOIL TO LLED WITH A HAND ROLLER WEIGHING NOT OF WIDTH;

IATELY AFTER SEEDING AS INDICATED ABOVE; ID KEPT MOIST WITH A FINE SPRAY AS REQUIRED, UNTIL THE GRASS IS WELL ESTABLISHED. ANY RILY COVERED WITH GRASS SHALL BE RESEEDED,

ND MAINTAIN THE SEEDED AREAS UNTIL

THE FOLLOWING SEED REQUIREMENTS SHALL R APPROVED EUQAL:

- APPLICATION RATE
- 70% 20%
- 10%

IT EXCEED ONE (1) PERCENT BY WEIGHT. ALL FEDERAL SEED LAWS. SEEDING SHALL BE DONE CASE SHALL SEEDING TAKE PLACE OVER SNOW. ST SNOWFALL):

LIME, FERTILIZER AND GRADING TWICE THE INDICATED RATE. APPLY MULCH AS

HENEVER POSSIBLE, USE WASHOUT FACILITIES

ALL DESIGNATE SPECIFIC WASHOUT AREAS AND ED WASHOUT WATER; EAS AT LEAST 150 FEET AWAY FROM STORM

R DELINEATED WETLANDS; TECT LEAKS OR TEARS AND TO IDENTIFY WHEN

1WATER DISCHARGES ALLOWED. ALL OTHER IBITED ON SITE:

RE DETERGENTS ARE NOT USED;

- INATED WATER LINE FLUSHING;
- WN WHERE DETERGENTS ARE NOT USED;
- GENTS ARE NOT USED;
- COMPRESSOR CONDENSATION; PRING WATER;
- CH ARE UNCONTAMINATED;

WASTE DISPOSAL: WASTE MATERIAL

- A. ALL WASTE MATERIALS SHALL BE COLLECTED AND STORED IN SECURELY LIDDED RECEPTACLES. ALL TRASH AND CONSTRUCTION DEBRIS FROM THE SITE SHALL BE DEPOSITED IN A DUMPSTER;
- B. NO CONSTRUCTION WASTE MATERIALS SHALL BE BURIED ON SITE;
- C. ALL PERSONNEL SHALL BE INSTRUCTED REGARDING THE CORRECT PROCEDURE FOR WASTE DISPOSAL BY THE SUPERINTENDENT.
- HAZARDOUS WASTE: A. ALL HAZARDOUS WASTE MATERIALS SHALL BE DISPOSED OF IN THE MANNER SPECIFIED BY LOCAL OR STATE REGULATION OR BY THE MANUFACTURER; B. SITE PERSONNEL SHALL BE INSTRUCTED IN THESE PRACTICES BY THE SUPERINTENDENT
- 3. SANITARY WASTE: A. ALL SANITARY WASTE SHALL BE COLLECTED FROM THE PORTABLE UNITS A MINIMUM OF ONCE PER WEEK BY A LICENSED SANITARY WASTE MANAGEMENT CONTRACTOR.

SPILL PREVENTION

- CONTRACTOR SHALL BE FAMILIAR WITH SPILL PREVENTION MEASURES REQUIRED BY LOCAL, STATE AND FEDERAL AGENCIES. AT A MINIMUM, CONTRACTOR SHALL FOLLOW THE BEST MANAGEMENT SPILL PREVENTION PRACTICES OUTLINED BELOW.
- 2. THE FOLLOWING ARE THE MATERIAL MANAGEMENT PRACTICES THAT SHALL BE USED TO REDUCE THE RISK OF SPILLS OR OTHER ACCIDENTAL EXPOSURE OF MATERIALS AND SUBSTANCES DURING CONSTRUCTION TO STORMWATER RUNOFF:
- A. GOOD HOUSEKEEPING THE FOLLOWING GOOD HOUSEKEEPING PRACTICE SHALL BE FOLLOWED ON SITE DURING CONSTRUCTION: a. ONLY SUFFICIENT AMOUNTS OF PRODUCTS TO DO THE JOB SHALL BE STORED ON
- SITE b. ALL MATERIALS STORED ON SITE SHALL BE STORED IN A NEAT, ORDERLY MANNER IN
- THEIR PROPER (ORIGINAL IF POSSIBLE) CONTAINERS AND, IF POSSIBLE, UNDER A ROOF OR OTHER ENCLOSURE; c. MANUFACTURER'S RECOMMENDATIONS FOR PROPER USE AND DISPOSAL SHALL BE
- FOLLOWED; d. THE SITE SUPERINTENDENT SHALL INSPECT DAILY TO ENSURE PROPER USE AND
- DISPOSAL OF MATERIALS; e. SUBSTANCES SHALL NOT BE MIXED WITH ONE ANOTHER UNLESS RECOMMENDED BY
- THE MANUFACTURER; f. WHENEVER POSSIBLE ALL OF A PRODUCT SHALL BE USED UP BEFORE DISPOSING OF
- THE CONTAINER. HAZARDOUS PRODUCTS - THE FOLLOWING PRACTICES SHALL BE USED TO REDUCE THE RISKS ASSOCIATED WITH HAZARDOUS MATERIALS:
- g. PRODUCTS SHALL BE KEPT IN THEIR ORIGINAL CONTAINERS UNLESS THEY ARE NOT RESEALABLE;
- h. ORIGINAL LABELS AND MATERIAL SAFETY DATA SHALL BE RETAINED FOR IMPORTANT PRODUCT INFORMATION; i. SURPLUS PRODUCT THAT MUST BE DISPOSED OF SHALL BE DISCARDED ACCORDING
- TO THE MANUFACTURER'S RECOMMENDED METHODS OF DISPOSAL C. PRODUCT SPECIFIC PRACTICES - THE FOLLOWING PRODUCT SPECIFIC PRACTICES SHALL BE FOLLOWED ON SITE:
- a. PETROLEUM PRODUCTS:
- ALL ON SITE VEHICLES SHALL BE MONITORED FOR LEAKS AND RECEIVE REGULAR PREVENTIVE MAINTENANCE TO REDUCE LEAKAGE;
- PETROLEUM PRODUCTS SHALL BE STORED IN TIGHTLY SEALED CONTAINERS WHICH ARE CLEARLY LABELED. ANY ASPHALT BASED SUBSTANCES USED ON SITE SHALL BE APPLIED ACCORDING TO THE MANUFACTURER'S RECOMMENDATIONS. b. FERTILIZERS:
- FERTILIZERS USED SHALL BE APPLIED ONLY IN THE MINIMUM AMOUNTS DIRECTED BY THE SPECIFICATIONS;
- ONCE APPLIED FERTILIZER SHALL BE WORKED INTO THE SOIL TO LIMIT EXPOSURE TO STORMWATER; • STORAGE SHALL BE IN A COVERED SHED OR ENCLOSED TRAILERS. THE CONTENTS
- OF ANY PARTIALLY USED BAGS OF FERTILIZER SHALL BE TRANSFERRED TO A SEALABLE PLASTIC BIN TO AVOID SPILLS.
- c. PAINTS: ALL CONTAINERS SHALL BE TIGHTLY SEALED AND STORED WHEN NOT REQUIRED
- FOR USE;
- EXCESS PAINT SHALL NOT BE DISCHARGED TO THE STORM SEWER SYSTEM; • EXCESS PAINT SHALL BE DISPOSED OF PROPERLY ACCORDING TO MANUFACTURER'S INSTRUCTIONS OR STATE AND LOCAL REGULATIONS.
- D. SPILL CONTROL PRACTICES IN ADDITION TO GOOD HOUSEKEEPING AND MATERIAL MANAGEMENT PRACTICES DISCUSSED IN THE PREVIOUS SECTION, THE FOLLOWING PRACTICES SHALL BE FOLLOWED FOR SPILL PREVENTION AND CLEANUP:
- a. MANUFACTURER'S RECOMMENDED METHODS FOR SPILL CLEANUP SHALL BE CLEARLY POSTED AND SITE PERSONNEL SHALL BE MADE AWARE OF THE PROCEDURES AND THE LOCATION OF THE INFORMATION AND CLEANUP SUPPLIES;
- b. MATERIALS AND EQUIPMENT NECESSARY FOR SPILL CLEANUP SHALL BE KEPT IN THE MATERIAL STORAGE AREA ON SITE. EQUIPMENT AND MATERIALS SHALL INCLUDE BUT NOT BE LIMITED TO BROOMS, DUSTPANS, MOPS, RAGS, GLOVES, GOGGLES, KITTY LITTER, SAND, SAWDUST AND PLASTIC OR METAL TRASH CONTAINERS SPECIFICALLY FOR THIS PURPOSE;
- c. ALL SPILLS SHALL BE CLEANED UP IMMEDIATELY AFTER DISCOVERY; d. THE SPILL AREA SHALL BE KEPT WELL VENTILATED AND PERSONNEL SHALL WEAR
- APPROPRIATE PROTECTIVE CLOTHING TO PREVENT INJURY FROM CONTACT WITH A HAZARDOUS SUBSTANCE; e. SPILLS OF TOXIC OR HAZARDOUS MATERIAL SHALL BE REPORTED TO THE
- APPROPRIATE LOCAL, STATE OR FEDERAL AGENCIES AS REQUIRED;
- f. THE SITE SUPERINTENDENT RESPONSIBLE FOR DAY-TO-DAY SITE OPERATIONS SHALL BE THE SPILL PREVENTION AND CLEANUP COORDINATOR.
- E. VEHICLE FUELING AND MAINTENANCE PRACTICE: a. CONTRACTOR SHALL MAKE AN EFFORT TO PERFORM EQUIPTMENT/VEHICAL FUELING
- AND MAINTENANCE AT AN OFF-SITE FACILITY; b. CONTRACTOR SHALL PROVIDE AN ON-SITE FUELING AND MAINTENANCE AREA THAT IS CLEAN AND DRY;
- c. IF POSSIBLE THE CONTRACTOR SHALL KEEP AREA COVERED; d. CONTRACTOR SHALL KEEP A SPILL KIT AT THE FUELING AND MAINTENANCE AREA;
- e. CONTRACTOR SHALL REGULARLY INSPECT VEHICLES FOR LEAKS AND DAMAGE; f. CONTRACTOR SHALL USE DRIP PANS, DRIP CLOTHS, OR ABSORBENT PADS WHEN
- REPLACING SPENT FLUID.

EROSION CONTROL OBSERVATIONS AND MAINTENANCE PRACTICES

THIS PROJECT EXCEEDS ONE (1) ACRE OF DISTURBANCE AND THUS REQUIRES A SWPPP. THE SWPPP SHALL BE PREPARED BY THE CONTRACTOR. THE CONTRACTOR SHALL BE FAMILIAR WITH THE SWPPP AND KEEP AN UPDATED COPY OF THE SWPPP ONSITE AT ALL TIMES.

- THE FOLLOWING REPRESENTS THE GENERAL OBSERVATION AND REPORTING PRACTICES THAT SHALL BE FOLLOWED AS PART OF THIS PROJECT: OBSERVATIONS OF THE PROJECT FOR COMPLIANCE WITH THE SWPPP SHALL BE MADE BY
- THE CONTRACTOR AT LEAST ONCE A WEEK OR WITHIN 24 HOURS OF A STORM 0.25 INCHES OR GREATER;
- 2. AN OBSERVATION REPORT SHALL BE MADE AFTER EACH OBSERVATION AND DISTRIBUTED TO THE ENGINEER, THE OWNER, AND THE CONTRACTOR;
- 3. A REPRESENTATIVE OF THE SITE CONTRACTOR, SHALL BE RESPONSIBLE FOR MAINTENANCE AND REPAIR ACTIVITIES;
- 4. IF A REPAIR IS NECESSARY, IT SHALL BE INITIATED WITHIN 24 HOURS OF REPORT.

- ACRE OF DRAINAGE AREA.

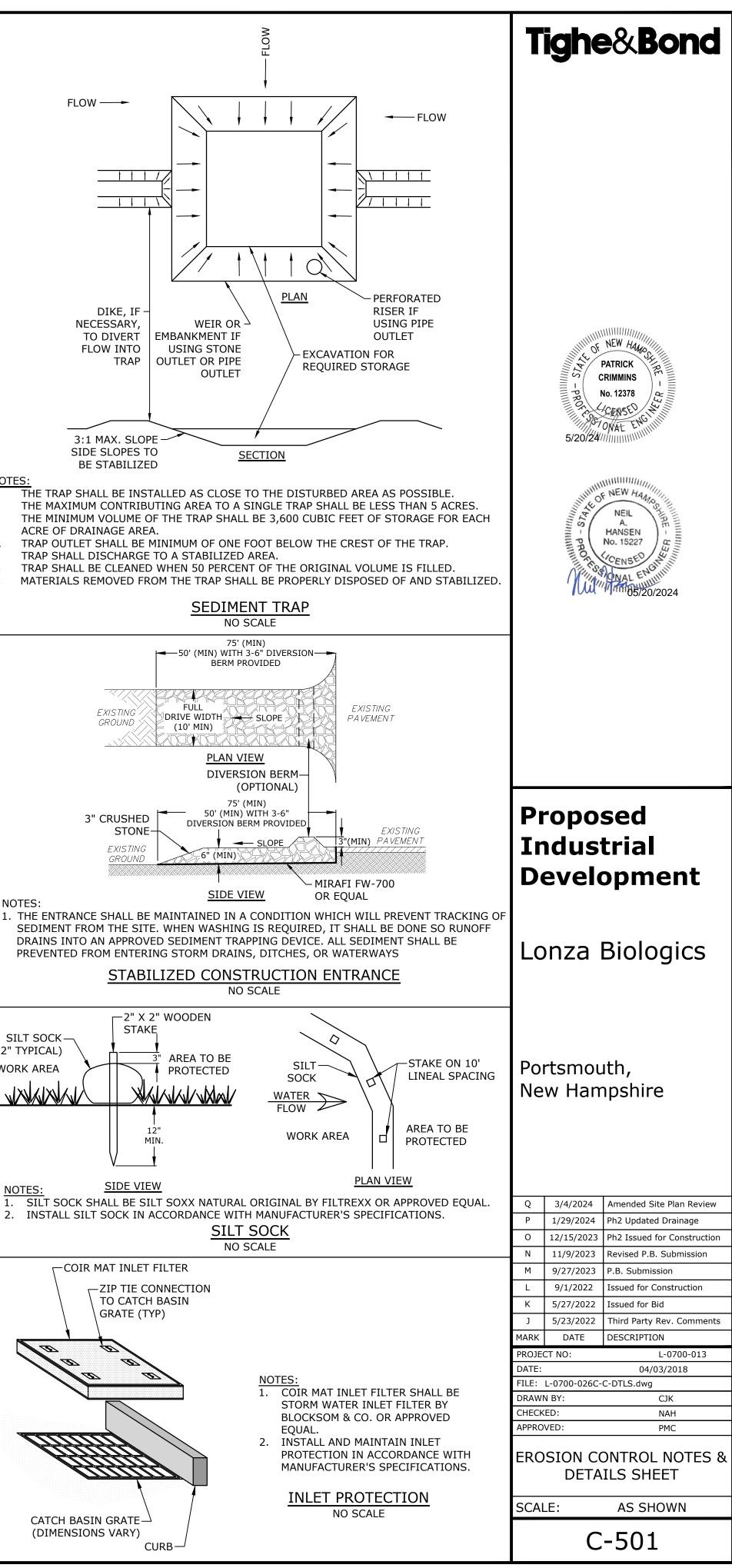
NOTES:

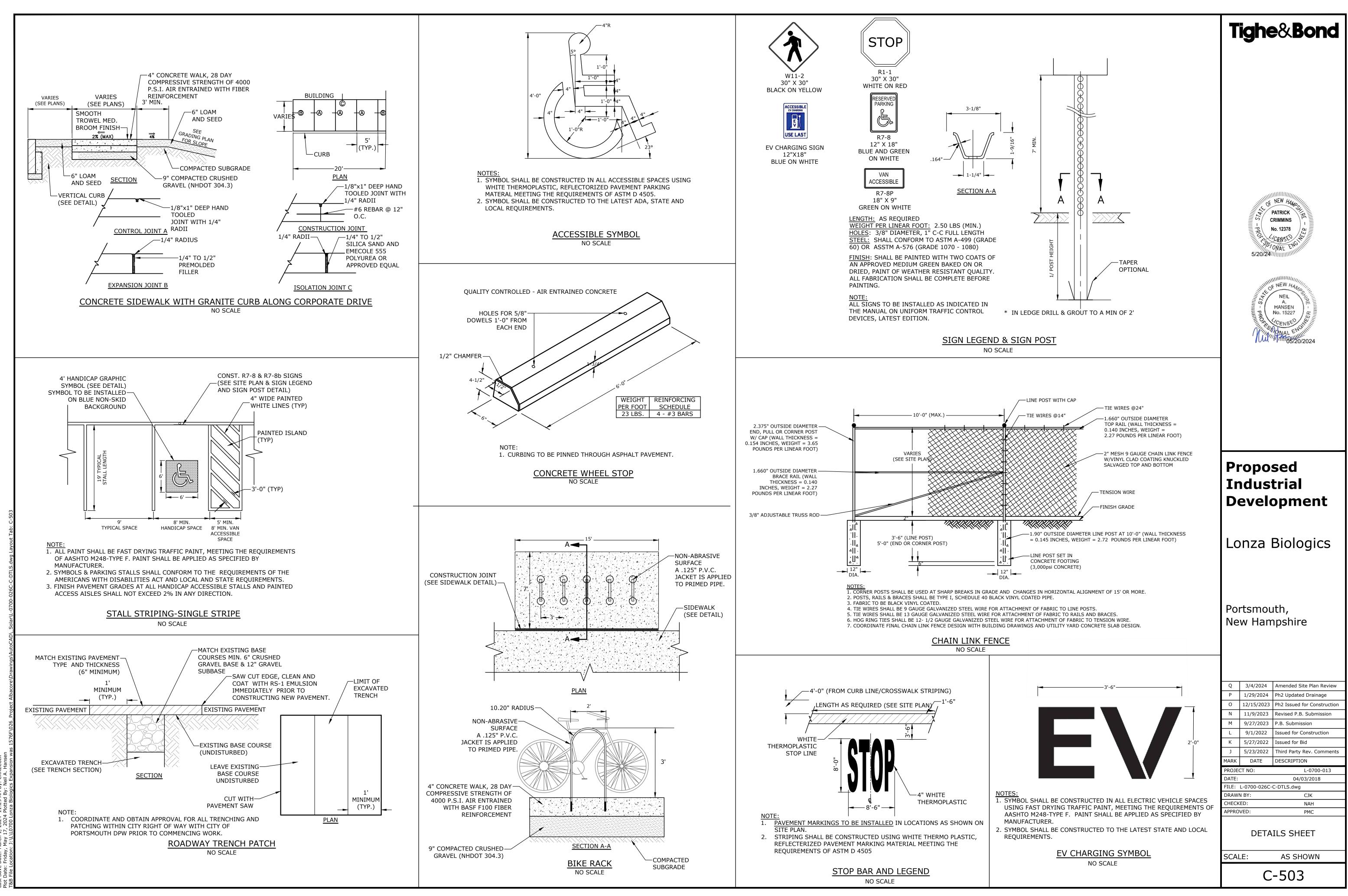
SILT SOCK – (12" TYPICAL)
WORK AREA
JAKKAK

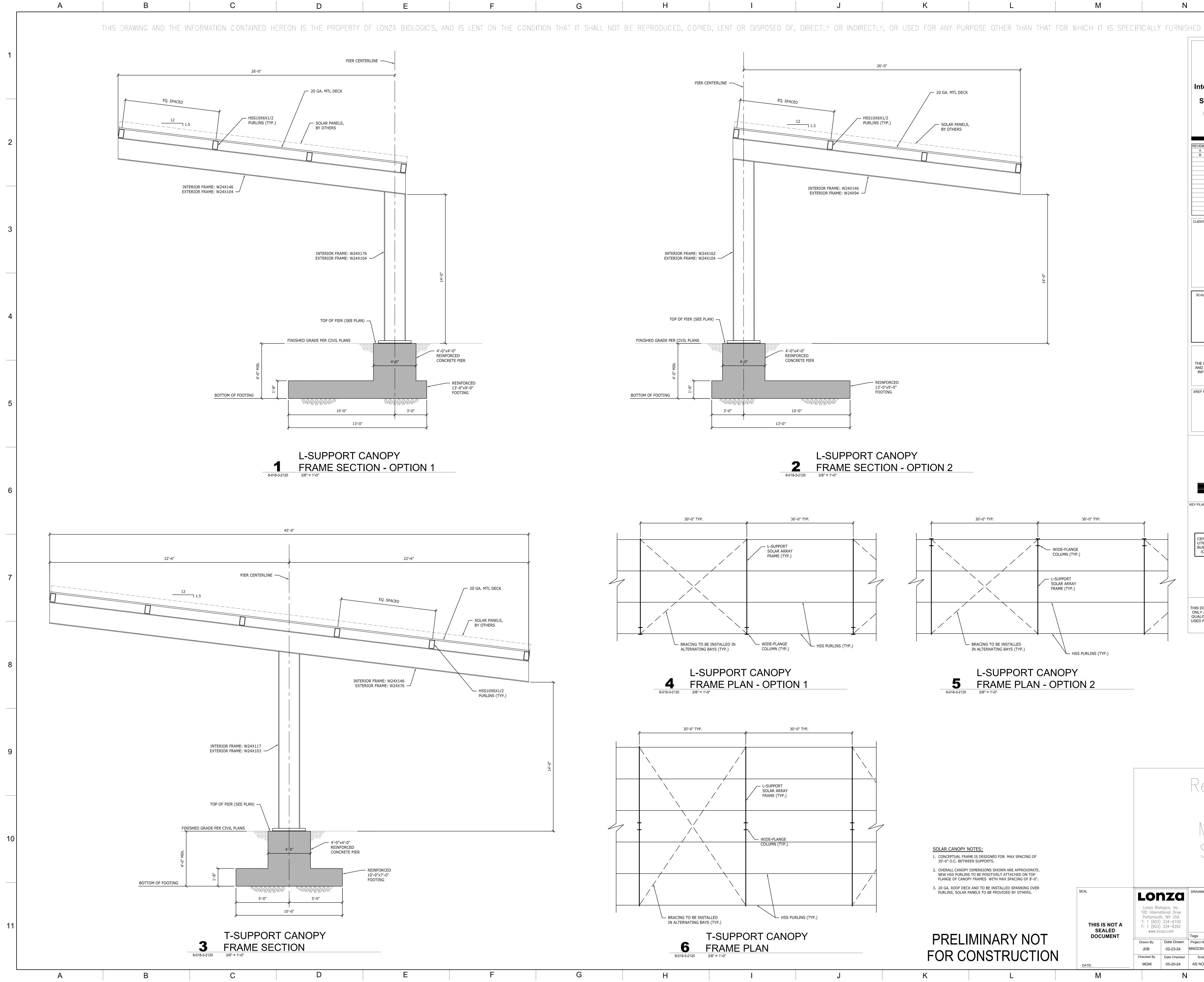
1.	<u>TES:</u> SILT SOCK SHA INSTALL SILT S	

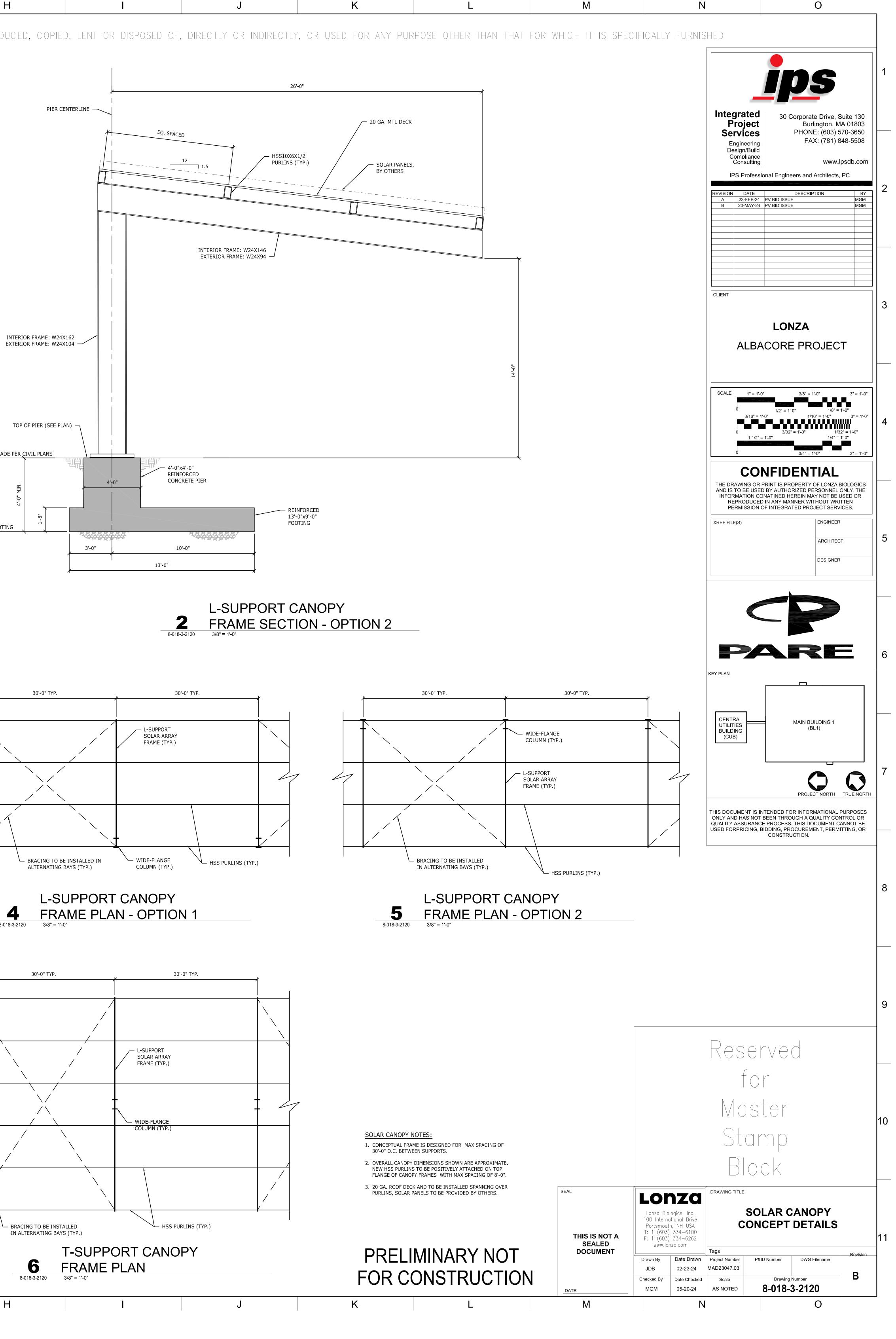
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CATCH BASIN GRATE-(DIMENSIONS VARY)









Drainage Memorandum

To:Pease Development Authority (PDA)FROM:Neil A. Hansen, PE
Patrick M. Crimmins, PECOPY:Lonza BiologicsDATE:May 20, 2024

1.0 Project Description

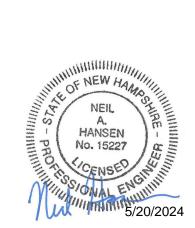
The proposed work includes the addition of Solar Canopies over the previously approved 150space surface parking lot associated with Phase 2 of the Iron Parcel Development project. These Solar Canopies are planned to be removed along with the 150-space parking lot before the execution of the Master Plan, therefore there will be no changes to the Master Plan Drainage Design.

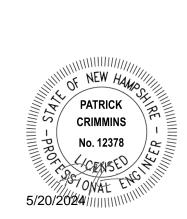
The Phase 2 drainage analysis has been updated and revised to include the 4'x4' concrete footings and 8'x22' concrete equipment pad. The proposed change includes the addition of approximately 672 SF of impervious surfaces. Although the addition of this area is very minimal in perspective to the whole watershed area (1,376,888 SF), we have prepared this technical memo to confirm that the previously approved Phase 2 drainage design and gravel wetlands are sized appropriately to accommodate this slight increase in impervious area.

2.0 Drainage Analysis

The previously approved Phase 2 Drainage Calculation has been updated to analyze the slight increase in impervious area and can be found in Attachment A. Subcatchment 1.0 has been updated to convert 304 SF of the previously grass surface to impervious surface. This additional 304 SF is approximately 0.09% of the total impervious area (314,795 SF) for this watershed.

Subcatchment 1.1 has been updated to convert 368 SF of the previously grass surface to impervious surface. This addition of 368 SF is approximately 0.7% of the total impervious area (48,674 SF) for this watershed.





2.1 Peak Rate Comparisons

The following table summarizes and compares the Phase-2 2023 Approved, proposed Phase-2 2024 Amendment, and Master Plan pre- and post-development peak runoff rates for the 2-year, 10-year, 25-year and 50-year storm events at each point of analysis. These points of analysis remain unchanged from the previously prepared and approved drainage analysis.

Table 2.1 – Peak Flow Rate Comparison							
Point of Analysis	Phase	Pre 1-Year Storm (cfs)	Pre/ Post 2-Year Storm (cfs)	Pre/ Post 10-Year Storm (cfs)	Pre/ Post 25-Year Storm (cfs)	Pre/ Post 50-Year Storm (cfs)	
	Phase 2 (2023 Approval)	16.58	24.86/ 9.25	52.70/ 31.22	76.06/ 56.26	98.56/ 74.09	
PA1	Phase 2 (2024 Amendment)	16.58	24.86/ 9.25	52.70/ 31.22	76.06/ 56.26	98.56/ 74.09	
	Master	16.58	24.86/ 9.41	52.70/ 39.92	76.06/ 66.14	98.56/ 83.35	
	Phase 2 (2023 Approval)	3.38	4.41/ 3.10	7.49/ 5.36	9.90/ 7.12	12.13/ 8.76	
PA2	Phase 2 (2024 Amendment)	3.38	4.41/ 3.10	7.49/ 5.36	9.90/ 7.12	12.13/ 8.76	
	Master	3.38	4.41/ 3.72	7.49/ 5.94	9.90/ 7.66	12.13/ 9.25	

2.2 Stormwater Treatment

Runoff from the newly created impervious surfaces will be directed to either of the previously approved Gravel Wetland 1 (POND 1.0) or Gravel Wetland 2 (POND 1.1). The following sections outline the treatment capacities of both gravel wetlands.

Gravel Wetland 1

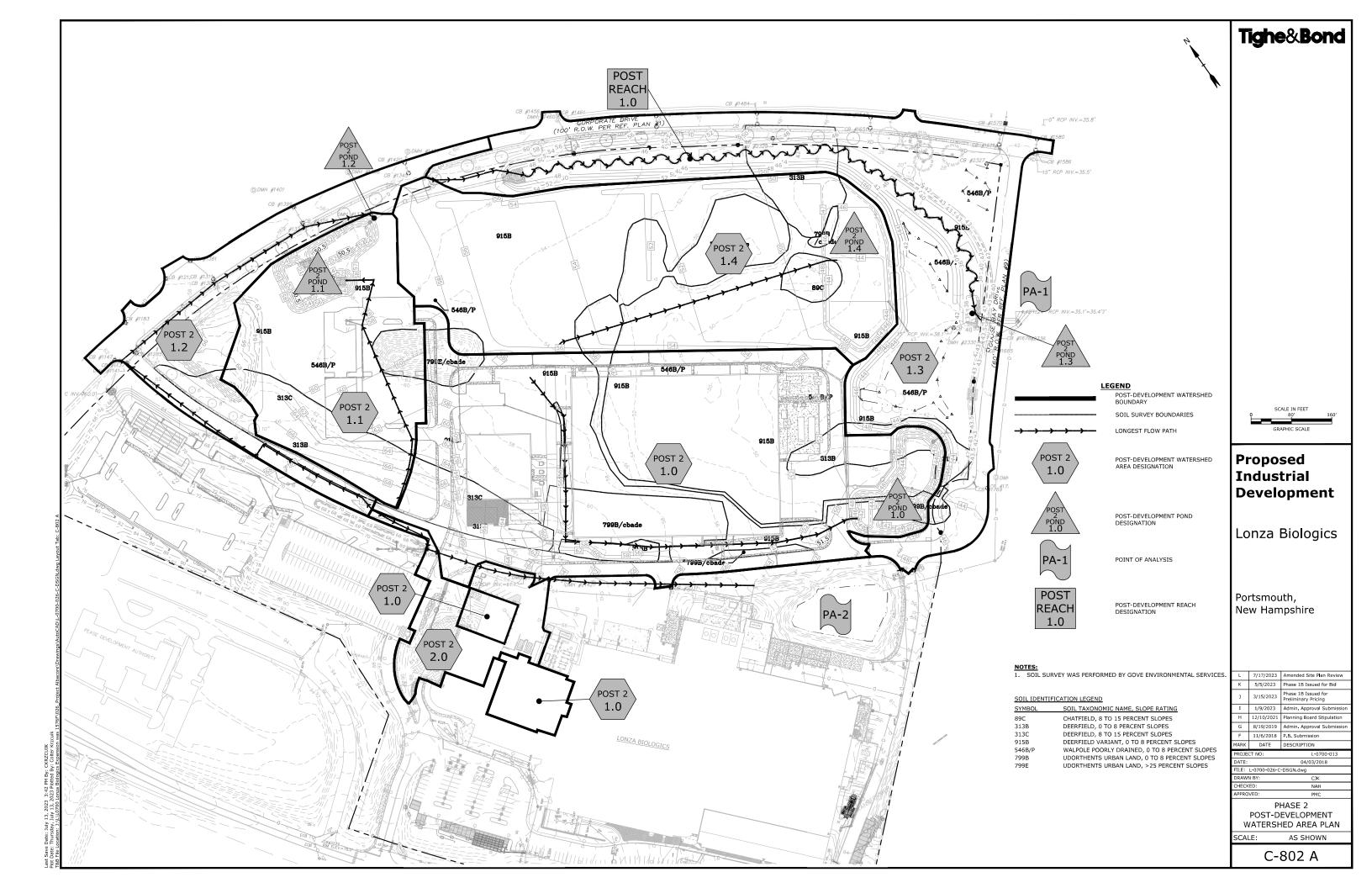
Gravel Wetland 1 has a design capacity to treat 333,950 SF of impervious area for its 462,599 SF watershed area. The proposed change is to add 304 SF of impervious surface to the previously approved 314,491 SF of impervious surface for an amended total of 314,795 SF of impervious surface. This 314,795 SF is well within the gravel wetland design capacity of 333,950 SF of impervious surface.

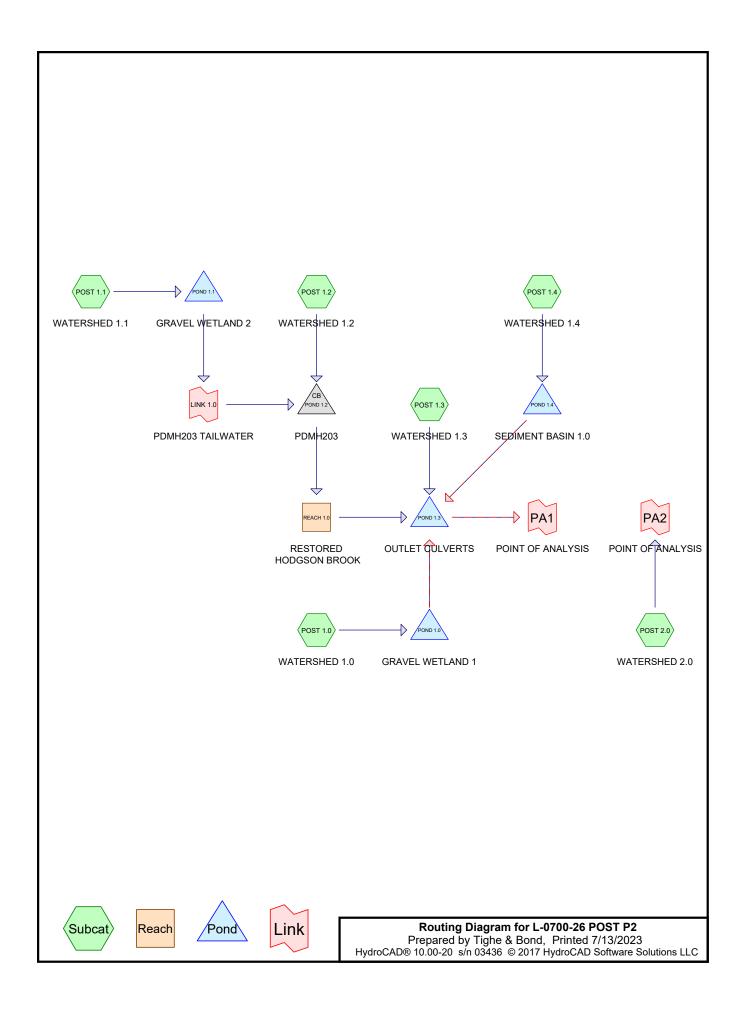
Gravel Wetland 2

Gravel Wetland 2 has a design capacity to treat 142,418 SF of impervious area for its 242,496 SF watershed area. The proposed change is to add 368 SF of impervious surface to the previously approved 48,306 SF of impervious surface for an amended total of 48,674 SF of impervious surface. This 48,674 SF is well within the gravel wetland design capacity of 142,418 SF of impervious surface.

3.0 Conclusion

The proposed amendment will result in no change to the previously approved postdevelopment peak runoff rates for Phase 2 and does not affect the Master Plan Drainage design. The net increase in impervious areas resulting from the proposed work will be directed to either Gravel Wetland 1 or Gravel Wetland 2 which both have the capacity to treat the slight increase in impervious surfaces. Phase 2 (2023 Approval) Post-Development Calculations





L-0700-26 POST P2 Prepared by Tighe & Bond HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC

Area Listing (all nodes)

	Area xres)	CN	Description (subcatchment-numbers)			
	.312	61	>75% Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3,			
			POST 1.4)			
13	.558	74	>75% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3,			
			POST 1.4, POST 2.0)			
1	.467	80	>75% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4)			
0	.514	58	Meadow, non-grazed, HSG B (POST 1.3)			
1	.662	71	Meadow, non-grazed, HSG C (POST 1.3)			
0	.639	98	Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3)			
6	.959	98	Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4,			
			POST 2.0)			
0	.137	98	Paved parking, HSG D (POST 1.0, POST 1.3)			
0	.120	98	Roofs, HSG B (POST 1.0)			
3	.526	98	Roofs, HSG C (POST 1.0, POST 2.0)			
0	.714	98	Roofs, HSG D (POST 1.0)			
31	.609	82	TOTAL AREA			

Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
3.586	HSG B	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4
25.705	HSG C	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0
2.318	HSG D	POST 1.0, POST 1.3, POST 1.4
0.000	Other	
31.609		TOTAL AREA

L-0700-26 POST P2 Type III 24-hr 2 Year Rainfall=3.68" Prepared by Tighe & Bond Printed 7/13/2023 HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC Page 4 Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>2.61" Flow Length=933' Tc=11.4 min CN=90 Runoff=25.38 cfs 2.201 af Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>1.63" SubcatchmentPOST 1.1: WATERSHED Flow Length=464' Tc=8.3 min CN=78 Runoff=6.25 cfs 0.492 af Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>2.34" SubcatchmentPOST 1.2: WATERSHED Flow Length=1,191' Tc=6.4 min CN=87 Runoff=6.94 cfs 0.511 af Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>1.62" SubcatchmentPOST 1.3: WATERSHED Flow Length=1,525' Tc=45.9 min CN=78 Runoff=5.96 cfs 0.929 af SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>1.36" Flow Length=585' Tc=13.5 min CN=74 Runoff=8.76 cfs 0.822 af SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>2.34" Flow Length=758' Tc=5.0 min CN=87 Runoff=3.10 cfs 0.221 af Avg. Flow Depth=0.63' Max Vel=2.08 fps Inflow=6.94 cfs 0.511 af Reach REACH 1.0: RESTORED n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=4.97 cfs 0.507 af Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=46.02' Storage=67,987 cf Inflow=25.38 cfs 2.201 af Primary=0.96 cfs 0.874 af Secondary=0.00 cfs 0.000 af Outflow=0.96 cfs 0.874 af Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=52.38' Storage=21,415 cf Inflow=6.25 cfs 0.492 af Outflow=0.00 cfs 0.000 af Peak Elev=50.38' Inflow=6.94 cfs 0.511 af Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=6.94 cfs 0.511 af Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' Storage=8,981 cf Inflow=9.25 cfs 3.060 af Primary=9.25 cfs 2.856 af Secondary=0.00 cfs 0.000 af Outflow=9.25 cfs 2.856 af Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=44.62' Storage=21,007 cf Inflow=8.76 cfs 0.822 af Primary=0.51 cfs 0.751 af Secondary=0.00 cfs 0.000 af Outflow=0.51 cfs 0.751 af Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af Link PA1: POINT OF ANALYSIS Inflow=9.25 cfs 2.856 af Primary=9.25 cfs 2.856 af Inflow=3.10 cfs 0.221 af Link PA2: POINT OF ANALYSIS Primary=3.10 cfs 0.221 af

> Total Runoff Area = 31.609 ac Runoff Volume = 5.176 af Average Runoff Depth = 1.96" 61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

L-0700-26 POST P2 Type III 24-hr 10 Year Rainfall=5.58" Prepared by Tighe & Bond Printed 7/13/2023 HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC Page 5 Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>4.43" Flow Length=933' Tc=11.4 min CN=90 Runoff=42.01 cfs 3.732 af Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>3.21" SubcatchmentPOST 1.1: WATERSHED Flow Length=464' Tc=8.3 min CN=78 Runoff=12.40 cfs 0.966 af Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>4.11" SubcatchmentPOST 1.2: WATERSHED Flow Length=1,191' Tc=6.4 min CN=87 Runoff=11.94 cfs 0.897 af Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>3.18" SubcatchmentPOST 1.3: WATERSHED Flow Length=1,525' Tc=45.9 min CN=78 Runoff=11.87 cfs 1.826 af SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>2.83" Flow Length=585' Tc=13.5 min CN=74 Runoff=18.77 cfs 1.708 af SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>4.11" Flow Length=758' Tc=5.0 min CN=87 Runoff=5.36 cfs 0.388 af **Reach REACH 1.0: RESTORED** Avg. Flow Depth=0.82' Max Vel=2.20 fps Inflow=11.94 cfs 0.897 af n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=6.12 cfs 0.891 af Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=46.78' Storage=83,438 cf Inflow=42.01 cfs 3.732 af Primary=9.22 cfs 2.105 af Secondary=5.86 cfs 0.170 af Outflow=15.08 cfs 2.275 af Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=54.11' Storage=42,049 cf Inflow=12.40 cfs 0.966 af Outflow=0.00 cfs 0.000 af Peak Elev=50.72' Inflow=11.94 cfs 0.897 af Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=11.94 cfs 0.897 af Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.77' Storage=13,560 cf Inflow=31.34 cfs 5.942 af Primary=31.22 cfs 5.655 af Secondary=0.00 cfs 0.000 af Outflow=31.22 cfs 5.655 af Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=45.79' Storage=50,580 cf Inflow=18.77 cfs 1.708 af Primary=0.68 cfs 0.950 af Secondary=0.00 cfs 0.000 af Outflow=0.68 cfs 0.950 af Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af Link PA1: POINT OF ANALYSIS Inflow=31.22 cfs 5.655 af Primary=31.22 cfs 5.655 af Inflow=5.36 cfs 0.388 af Link PA2: POINT OF ANALYSIS Primary=5.36 cfs 0.388 af

> Total Runoff Area = 31.609 ac Runoff Volume = 9.517 af Average Runoff Depth = 3.61" 61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

Summary for Subcatchment POST 1.0: WATERSHED 1.0

Runoff = 42.01 cfs @ 12.16 hrs, Volume= 3.732 af, Depth> 4.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

А	rea (sf)	CN D	escription					
	5,235		oofs, HSC					
	29,148							
	18,966			ing, HSG B				
	43,455		oofs, HSG					
	82,022 10,236			ing, HSG C	ood, HSG C			
1	31,119		aved park loofs, HSG		,			
	14,671				ood, HSG D			
	5,480			ing, HSG D				
4	40,332	90 V	Veighted A	verage				
	25,841			rvious Area				
3	314,491	7	1.42% Imp	pervious Ar	ea			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Decemption			
7.7	70	0.0150	0.15		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.68"			
0.2	32	0.0200	2.87		Shallow Concentrated Flow,			
0.4	40	0.0000	0.40		Paved Kv= 20.3 fps			
0.1	19	0.0200	2.12		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps			
0.8	162	0.0050	3.21	2.52				
0.0	102	0.0000	0.21	2.02	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
					n= 0.013 Corrugated PE, smooth interior			
0.4	84	0.0050	3.21	2.52	Pipe Channel,			
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
0.5	440	0.0050	0.70	4 57	n= 0.013			
0.5	113	0.0050	3.72	4.57	Pipe Channel, 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'			
					n= 0.013			
1.2	299	0.0050	4.20	7.43	Pipe Channel,			
			-	-	18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'			
					n= 0.013			
0.4	94	0.0050	4.20	7.43	Pipe Channel,			
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'			
0.1	46	0.0240	11.16	25.05	n= 0.013 Pine Channel			
0.1	40	0.0240	11.10	35.05	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'			
					n= 0.013			
0.0	5	0.0800	7.16	0.98	Pipe Channel,			
	-		-		5.0" Round Area= 0.1 sf Perim= 1.3' r= 0.10'			
					n= 0.013			
0.0	9	0.0110	9.90	69.95	Pipe Channel,			

11.4

36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'

933 Total

Summary for Subcatchment POST 1.1: WATERSHED 1.1

n= 0.013

Runoff = 12.40 cfs @ 12.12 hrs, Volume= 0.966 af, Depth> 3.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN E	Description				
	36,403	61 >	>75% Grass cover, Good, HSG B				
	3,210	98 F	Paved park	ing, HSG B	3		
	72,719	74 >	75% Gras	s cover, Go	bod, HSG C		
	45,096	98 F	Paved park	ing, HSG C			
	157,428	78 V	Veighted A	verage			
	109,122	6	9.32% Per	vious Area			
	48,306	3	80.68% Imp	pervious Ar	ea		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
5.8	100	0.0625	0.29		Sheet Flow,		
					Grass: Short n= 0.150 P2= 3.68"		
2.2	312	0.0220	2.39		Shallow Concentrated Flow,		
					Unpaved Kv= 16.1 fps		
0.3	33	0.0150	1.84		Shallow Concentrated Flow,		
					Grassed Waterway Kv= 15.0 fps		
0.0	19	0.3300	8.62		Shallow Concentrated Flow,		
					Grassed Waterway Kv= 15.0 fps		
8.3	464	Total					

Summary for Subcatchment POST 1.2: WATERSHED 1.2

Runoff = 11.94 cfs @ 12.09 hrs, Volume= 0.897 af, Depth> 4.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
9,848	61	>75% Grass cover, Good, HSG B
4,784	98	Paved parking, HSG B
37,701	74	>75% Grass cover, Good, HSG C
61,646	98	Paved parking, HSG C
113,979	87	Weighted Average
47,549		41.72% Pervious Area
66,430		58.28% Impervious Area

Type III 24-hr 10 Year Rainfall=5.58" Printed 7/13/2023

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	1.5	100	0.0100	1.12	~ /	Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.68"
	1.0	153	0.0150	2.49		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
	1.6	343	0.0050	3.47	2.73	Pipe Channel,
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
						n= 0.012 Concrete pipe, finished
	0.1	13	0.0050	3.72	4.57	Pipe Channel,
						15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
						n= 0.013 Corrugated PE, smooth interior
	1.8	453	0.0050	4.20	7.43	Pipe Channel,
						18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
						n= 0.013 Corrugated PE, smooth interior
	0.4	129	0.0050	5.91	29.00	Pipe Channel,
						30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63'
						n= 0.013 Corrugated PE, smooth interior
	64	1 101	Total			

6.4 1,191 Total

Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 11.87 cfs @ 12.63 hrs, Volume= 1.826 af, Depth> 3.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Are	ea (sf)	CN D	escription						
	1,830	61 >	75% Gras	s cover, Go	bod, HSG B				
2	2,404	58 N	58 Meadow, non-grazed, HSG B						
	896		Paved parking, HSG B						
13	1,991		>75% Grass cover, Good, HSG C						
	8,446			ing, HSG C					
	2,396			on-grazed,					
	1,638				pod, HSG D				
	499			ing, HSG D)				
	0,100		/eighted A						
	0,259			vious Area					
6	9,841	2	3.27% Imp	ervious Ar	ea				
Tc I	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Description				
10.9	100	0.0130	0.15	()	Sheet Flow,				
					Grass: Short n= 0.150 P2= 3.68"				
1.1	52	0.0130	0.80		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
0.1	27	0.2720	7.82		Shallow Concentrated Flow,				
					Grassed Waterway Kv= 15.0 fps				
33.8	1,346	0.0090	0.66		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
45.9	1,525	Total							

Page 8

Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff = 18.77 cfs @ 12.19 hrs, Volume= 1.708 af, Depth> 2.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Δ	rea (sf)	CN E	Description					
-								
	23,477							
2	243,330	74 >	·75% Gras	s cover, Go	bod, HSG C			
	1,334	98 F	98 Paved parking, HSG C					
	47,586	80 >	·75% Ġras	s cover. Go	bod, HSG D			
	0			ace, HSG D				
3	315,727		Veighted A	,				
	,		0	vious Area				
3	314,393	-			-			
	1,334	0	.42% Impe	ervious Are	a			
_								
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
8.4	100	0.0245	0.20		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.68"			
5.1	465	0.0103	1.52		Shallow Concentrated Flow,			
					Grassed Waterway Kv= 15.0 fps			
0.0	20	0.3300	8.62		Shallow Concentrated Flow,			
0.0	-0	2.0000	0.02		Grassed Waterway Kv= 15.0 fps			
12 5	EOE	Total						
13.5	585	Total						

Summary for Subcatchment POST 2.0: WATERSHED 2.0

[49] Hint: Tc<2dt may require smaller dt

Runoff = 5.36 cfs @ 12.07 hrs, Volume= 0.388 af, Depth> 4.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description				
10,145	98	Roofs, HSG C				
22,815	74	>75% Grass cover, Good, HSG C				
16,376	98	Paved parking, HSG C				
49,336	87	Weighted Average				
22,815		46.24% Pervious Area				
26,521		53.76% Impervious Area				

Type III 24-hr 10 Year Rainfall=5.58" Printed 7/13/2023

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
 1.2	100	0.0164	1.36		Sheet Flow,
	40	0.0404	0.00		Smooth surfaces n= 0.011 P2= 3.68"
0.3	48	0.0164	2.60		Shallow Concentrated Flow,
0.3	130	0.0140	7.03	12.43	Paved Kv= 20.3 fps Pipe Channel,
0.0	100	0.0110	1.00	12.10	18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
					n= 0.013
0.5	70	0.0250	2.37		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
1.3	410	0.0050	5.09	16.00	Pipe Channel,
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
 					n= 0.013

3.6 758 Total, Increased to minimum Tc = 5.0 min

Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

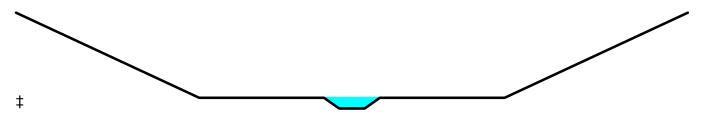
[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

Inflow Area	a =	6.231 ac, 42.27% Impervious, Inflow Depth > 1.73" for 10 Year event	
Inflow	=	11.94 cfs @ 12.09 hrs, Volume= 0.897 af	
Outflow	=	6.12 cfs @ 12.86 hrs, Volume= 0.891 af, Atten= 49%, Lag= 45.9 n	nin

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Max. Velocity= 2.20 fps, Min. Travel Time= 9.9 min Avg. Velocity = 0.85 fps, Avg. Travel Time= 25.6 min

Peak Storage= 6,846 cf @ 12.27 hrs Average Depth at Peak Storage= 0.82' Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs

Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals) Constant n= 0.040 Winding stream, pools & shoals Inlet Invert= 48.00', Outlet Invert= 36.00'



6.75

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Off	set El	Elevation		n.Depth		
(fe	et)	(feet)		(feet)		
0	.00	12.00		0.00		
18	.00	6.00		6.00		
30	.25	6.00		6.00		
31	.75	5.25		6.75		
34	.25	5.25		6.75		
35	.75	6.00		6.00		
48	.00	6.00		6.00		
66	.00	12.00		0.00		
Depth	End Ar	ea Pe	erim.	S	Storage	Discharge
(feet)	(sq-	-ft) (1	feet)	(cub	ic-feet)	(cfs)
0.00	C	0.0	2.5		0	0.00
0.75	3	8.0	30.4		3,927	2.28

68.3

Summary for Pond POND 1.0: GRAVEL WETLAND 1

2,720.29

[95] Warning: Outlet Device #4 rise exceeded

291.0

Inflow Area =	10.109 ac, 71.42% Impervious, Inflo	w Depth > 4.43" for 10 Year event
Inflow =	42.01 cfs @ 12.16 hrs, Volume=	3.732 af
Outflow =	15.08 cfs @ 12.50 hrs, Volume=	2.275 af, Atten= 64%, Lag= 20.8 min
Primary =	9.22 cfs @ 12.50 hrs, Volume=	2.105 af
Secondary =	5.86 cfs @ 12.50 hrs, Volume=	0.170 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 46.78' @ 12.50 hrs Surf.Area= 21,240 sf Storage= 83,438 cf Flood Elev= 48.00' Surf.Area= 23,557 sf Storage= 110,845 cf

380,919

Plug-Flow detention time= 226.3 min calculated for 2.275 af (61% of inflow) Center-of-Mass det. time= 125.2 min (916.2 - 791.0)

Volume	Invert	Avai	I.Storage	Storage Descr	iption	
#1	39.05'	1	10,845 cf	Custom Stage	e Data (Prismati	c) Listed below (Recalc)
Elevation (feet)		.Area sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
39.05	ę	9,855	0.0	0	0	
41.35	ç	9,855	30.0	6,800	6,800	
42.00	ç	9,855	45.0	2,883	9,683	
43.00	11	1,943	100.0	10,899	20,582	
44.00	14	4,202	100.0	13,073	33,654	
45.00	16	5,891	100.0	15,547	49,201	
46.00	19	9,752	100.0	18,322	67,522	
47.00	2	1,668	100.0	20,710	88,232	
48.00	23	3,557	100.0	22,613	110,845	

Type III 24-hr 10 Year Rainfall=5.58" Printed 7/13/2023 LLC Page 12

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Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	18.0" Round Culvert
	-		L= 30.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 41.35' / 41.20' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	41.35'	3.5" Vert. Orifice/Grate C= 0.600
#3	Device 1	45.00'	3.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	46.00'	4.0' long x 0.50' rise Sharp-Crested Rectangular Weir
			2 End Contraction(s) 0.5' Crest Height
#5	Device 1	47.00'	4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600
			Limited to weir flow at low heads
#6	Secondary	46.50'	15.0' long x 15.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=9.22 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater)

2=Orifice/Grate (Orifice Controls 0.74 cfs @ 11.06 fps)

-3=Orifice/Grate (Orifice Controls 0.30 cfs @ 6.19 fps)

-4=Sharp-Crested Rectangular Weir (Orifice Controls 8.17 cfs @ 4.19 fps)

Secondary OutFlow Max=5.85 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater) **GeBroad-Crested Rectangular Weir** (Weir Controls 5.85 cfs @ 1.41 fps)

Summary for Pond POND 1.1: GRAVEL WETLAND 2

Inflow Area =	3.614 ac, 30.68% Impervious,	Inflow Depth > 3.21" for 10 Year event
Inflow =	12.40 cfs @ 12.12 hrs, Volume	e= 0.966 af
Outflow =	0.00 cfs @ 0.00 hrs, Volume	e 0.000 af, Atten= 100%, Lag= 0.0 min
Primary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume	e= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 54.11' @ 24.00 hrs Surf.Area= 14,115 sf Storage= 42,049 cf Flood Elev= 57.00' Surf.Area= 21,643 sf Storage= 94,743 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	47.55'	117,304 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

L-0700-26 POST P2

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Elevatio	levation Surf.Area Void		s Inc.Store	Cum.Store				
(fee	et)	(sq-ft)	(%	b) (cubic-feet)	(cubic-feet)			
47.	55	6,269	0.	0 0	0			
49.8	85	6,269	30.	0 4,326	4,326			
50.	50	6,269	45.	0 1,834	6,159			
51.0	00	7,199	100.		9,526			
52.0	00	9,187	100.		17,719			
53.0		11,345	100.		27,985			
54.0		13,814	100.		40,565			
55.0		16,645	100.		55,794			
56.0		19,805			74,019			
58.0	00	23,480	100.	0 43,285	117,304			
Davias	Douting	l n	vort	Outlat Daviaga				
Device	Routing		ivert	Outlet Devices				
#1	Primary	49	9.85'	24.0" Round Culv				
					are edge headwall, Ke=			
					= 49.85' / 49.45' S= 0.03			
40	Davida d	4.0	0.00	n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf				
#2	Device 1		9.85'	2.0" Vert. Orifice/Grate C= 0.600				
#3	Device 1	53	8.50'					
#1	Davias 1	FG		2 End Contraction(
#4	Device 1	50	6.50'	Limited to weir flow	Drifice/Grate X 106.00	- 0.000		
				Limited to well now	at low neaus			

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=47.55' TW=55.07' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

2=Orifice/Grate (Controls 0.00 cfs)

-3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

-4=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond POND 1.2: PDMH203

Inflow Are	a =	6.231 ac, 42.27% Impervious, Inflow Depth > 1.73" for	10 Year event
Inflow	=	11.94 cfs @ 12.09 hrs, Volume= 0.897 af	
Outflow	=	11.94 cfs @ 12.09 hrs, Volume= 0.897 af, Atten=	0%, Lag= 0.0 min
Primary	=	11.94 cfs @ 12.09 hrs, Volume= 0.897 af	-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 50.72' @ 12.09 hrs Flood Elev= 57.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.35'	48.0" Round Culvert L= 269.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 49.35' / 48.00' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 12.57 sf

Primary OutFlow Max=11.76 cfs @ 12.09 hrs HW=50.71' TW=48.76' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 11.76 cfs @ 3.13 fps)

Summary for Pond POND 1.3: OUTLET CULVERTS

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=12) [62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.58' @ 23.95 hrs

Inflow Area =	30.477 ac, 37.69% Impervious, Inflow D	Depth > 2.34" for 10 Year event
Inflow =	31.34 cfs @ 12.51 hrs, Volume=	5.942 af
Outflow =	31.22 cfs @ 12.53 hrs, Volume=	5.655 af, Atten= 0%, Lag= 1.3 min
Primary =	31.22 cfs @ 12.53 hrs, Volume=	5.655 af
Secondary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 38.77' @ 12.53 hrs Surf.Area= 8,870 sf Storage= 13,560 cf Flood Elev= 43.50' Surf.Area= 95,977 sf Storage= 236,017 cf

Plug-Flow detention time= 56.2 min calculated for 5.642 af (95% of inflow) Center-of-Mass det. time= 29.8 min (900.3 - 870.4)

Volume	Invert	Avail.Stor	rage Storage	Description	
#1	35.00'	236,01	7 cf Custom	Stage Data (Prismatic)Listed below (Recal	c)
Elevatio	n S	urf.Area	Inc.Store	Cum.Store	
(fee	t)	(sq-ft)	(cubic-feet)	(cubic-feet)	
35.0	0	960	0	0	
36.0	0	1,428	1,194	1,194	
38.0	0	5,418	6,846	8,040	
40.0	0	14,354	19,772	27,812	
42.0		66,884	81,238	109,050	
43.0	0	92,707	79,796	188,846	
43.5	50	95,977	47,171	236,017	
Device	Routing	Invert	Outlet Device	S	
#1	Primary Secondary	35.60' 43.00'	L= 68.0' CM Inlet / Outlet I n= 0.025 Cor	0" H, R=21.5"/66.1" Pipe Arch CMP_Arch P, square edge headwall, Ke= 0.500 nvert= 35.60' / 35.30' S= 0.0044 '/' Cc= 0.9 rugated metal, Flow Area= 6.72 sf 8.0' long x 0.50' rise Sharp-Crested Vee /T	900
			Cv= 2.47 (C=	3.09)	

Primary OutFlow Max=31.11 cfs @ 12.53 hrs HW=38.77' TW=38.65' (Dynamic Tailwater) **1=CMP_Arch_1/2 42x29** (Outlet Controls 31.11 cfs @ 1.55 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=35.04' TW=38.65' (Dynamic Tailwater) 2=Sharp-Crested Vee/Trap Weir(Controls 0.00 cfs)

Summary for Pond POND 1.4: SEDIMENT BASIN 1.0

Inflow Area =	7.248 ac, 0.42% Impervious, Ir	nflow Depth > 2.83" for 10 Year event
Inflow =	18.77 cfs @ 12.19 hrs, Volume=	1.708 af
Outflow =	0.68 cfs @ 17.24 hrs, Volume=	0.950 af, Atten= 96%, Lag= 303.1 min
Primary =	0.68 cfs @ 17.24 hrs, Volume=	0.950 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Starting Elev= 44.15' Surf.Area= 18,132 sf Storage= 11,702 cf Peak Elev= 45.79' @ 17.24 hrs Surf.Area= 29,244 sf Storage= 50,580 cf (38,878 cf above start) Flood Elev= 48.50' Surf.Area= 38,802 sf Storage= 127,441 cf (115,739 cf above start)

Plug-Flow detention time= 356.9 min calculated for 0.681 af (40% of inflow) Center-of-Mass det. time= 9.2 min (846.8 - 837.5)

Volume	Invert	Avail.Sto	rage Storage	Description	
#1	43.00'	127,44	41 cf Custon	n Stage Data (Prismatic)Listed below (Rec	alc)
Elevatio (fee		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
43.0	00	1,000 17,117	0 9,059	0 9,059	
46.0 47.0 48.0	00	30,657 35,879 38,802	47,774 33,268 37,341	56,833 90,101 127,441	
Device	Routing	Invert	Outlet Device		
#1	Primary	42.75'	Inlet / Outlet	d Culvert L= 66.0' Ke= 0.500 Invert= 42.75' / 42.40' S= 0.0053 '/' Cc= (ow Area= 0.79 sf).900
#2	Device 1	43.00'	,	ifice/Grate C= 0.600	
#3	Device 1	46.80'		Horiz. Orifice/Grate C= 0.600	
#4	Secondary	47.40'			
Primary OutFlow Max=0.68 cfs @ 17.24 hrs HW=45.79' TW=38.65' (Dynamic Tailwater)					

-2=Orifice/Grate (Orifice Controls 0.68 cfs @ 7.80 fps)

3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=44.15' TW=35.04' (Dynamic Tailwater) -4=Custom Weir/Orifice (Controls 0.00 cfs)

Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.1 by 7.52' @ 0.00 hrs (23.95 cfs 41.618 af)

Inflow Area	a =	3.614 ac, 30	0.68% Impervious,	Inflow Depth = 0.0	00" for 10 Year event
Inflow	=	0.00 cfs @	0.00 hrs, Volume	e= 0.000 af	
Primary	=	0.00 cfs @	0.00 hrs, Volume	e= 0.000 af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 25	Point manual	elevation	table, To=	0.00 hrs,	dt= 1.00 hrs,	feet =		
55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07
55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07
55.07	55.07	55.07	55.07	55.07	55.07	55.07		

Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.3 by 3.61' @ 0.00 hrs (92.51 cfs 60.023 af)

Inflow Area	a =	30.477 ac, 37	.69% Impe	ervious, Inflow E	Depth > 2.23"	for 10 Year event
Inflow	=	31.22 cfs @ 1	12.53 hrs, 1	Volume=	5.655 af	
Primary	=	31.22 cfs @ 1	12.53 hrs, `	Volume=	5.655 af, At	ten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 2 Point manual elevation table, To= 0.00 hrs, dt= 24.00 hrs, feet = 38.65 38.65

Summary for Link PA2: POINT OF ANALYSIS

Inflow Area =	1.133 ac, 53.76% Impervious, Inflow	Depth > 4.11" for 10 Year event
Inflow =	5.36 cfs @ 12.07 hrs, Volume=	0.388 af
Primary =	5.36 cfs @ 12.07 hrs, Volume=	0.388 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

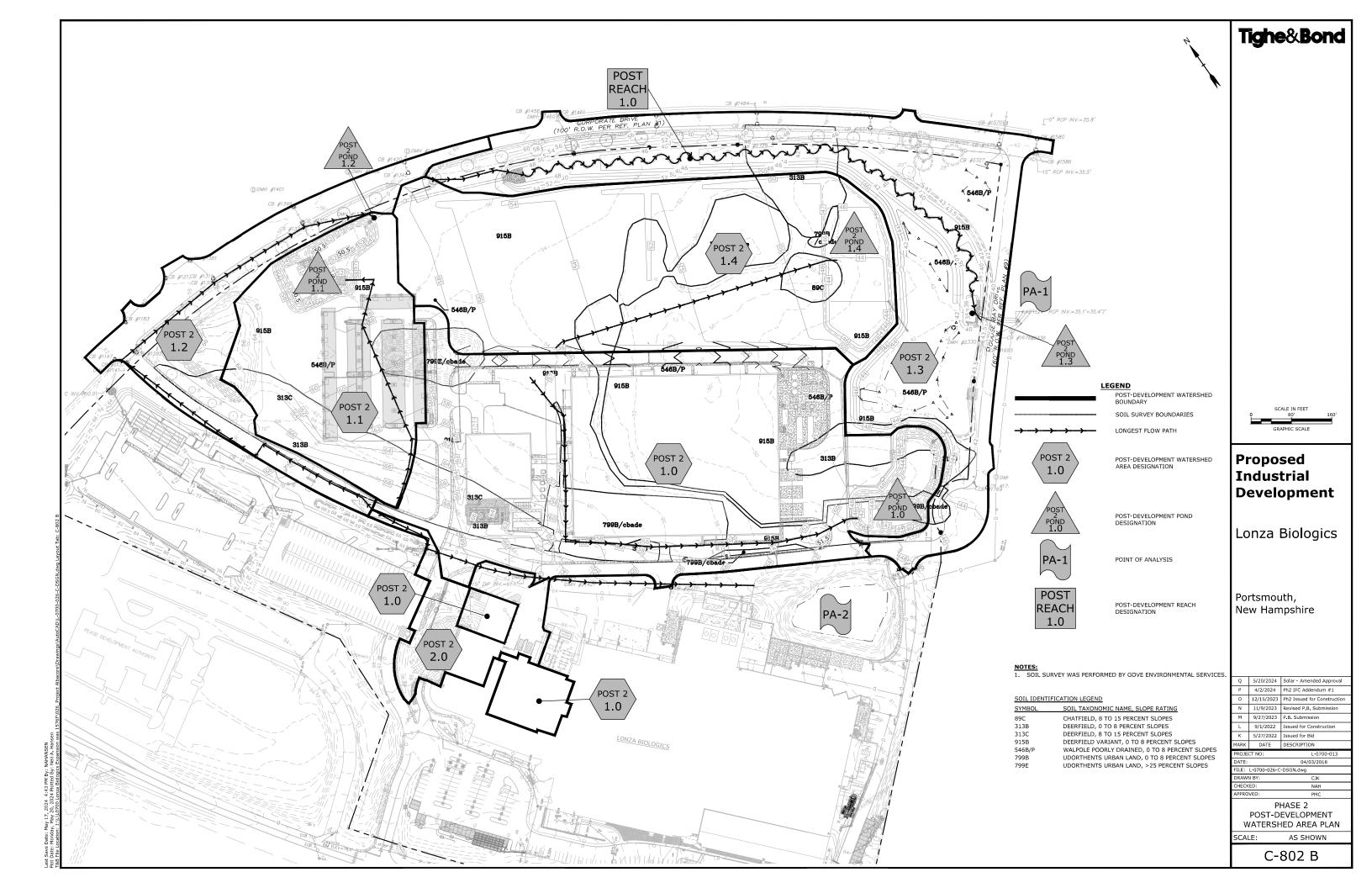
L-0700-26 POST P2 Type III 24-hr 25 Year Rainfall=7.07" Prepared by Tighe & Bond Printed 7/13/2023 HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC Page 17 Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>5.88" Flow Length=933' Tc=11.4 min CN=90 Runoff=54.93 cfs 4.956 af Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>4.53" SubcatchmentPOST 1.1: WATERSHED Flow Length=464' Tc=8.3 min CN=78 Runoff=17.44 cfs 1.365 af Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>5.54" SubcatchmentPOST 1.2: WATERSHED Flow Length=1,191' Tc=6.4 min CN=87 Runoff=15.85 cfs 1.209 af Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>4.50" SubcatchmentPOST 1.3: WATERSHED Flow Length=1,525' Tc=45.9 min CN=78 Runoff=16.75 cfs 2.583 af SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>4.09" Flow Length=585' Tc=13.5 min CN=74 Runoff=27.23 cfs 2.472 af SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>5.54" Flow Length=758' Tc=5.0 min CN=87 Runoff=7.12 cfs 0.523 af **Reach REACH 1.0: RESTORED** Avg. Flow Depth=0.87' Max Vel=2.22 fps Inflow=15.85 cfs 1.209 af n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=8.65 cfs 1.202 af Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=47.10' Storage=90,424 cf Inflow=54.93 cfs 4.956 af Primary=19.03 cfs 2.766 af Secondary=18.86 cfs 0.671 af Outflow=37.88 cfs 3.437 af Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=55.22' Storage=59,446 cf Inflow=17.44 cfs 1.365 af Outflow=0.00 cfs 0.000 af Peak Elev=50.94' Inflow=15.85 cfs 1.209 af Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=15.85 cfs 1.209 af Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.17' Storage=17,433 cf Inflow=57.33 cfs 8.292 af Primary=56.26 cfs 7.985 af Secondary=0.00 cfs 0.000 af Outflow=56.26 cfs 7.985 af Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=46.65' Storage=77,792 cf Inflow=27.23 cfs 2.472 af Primary=0.78 cfs 1.070 af Secondary=0.00 cfs 0.000 af Outflow=0.78 cfs 1.070 af Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af Link PA1: POINT OF ANALYSIS Inflow=56.26 cfs 7.985 af Primary=56.26 cfs 7.985 af Inflow=7.12 cfs 0.523 af Link PA2: POINT OF ANALYSIS Primary=7.12 cfs 0.523 af

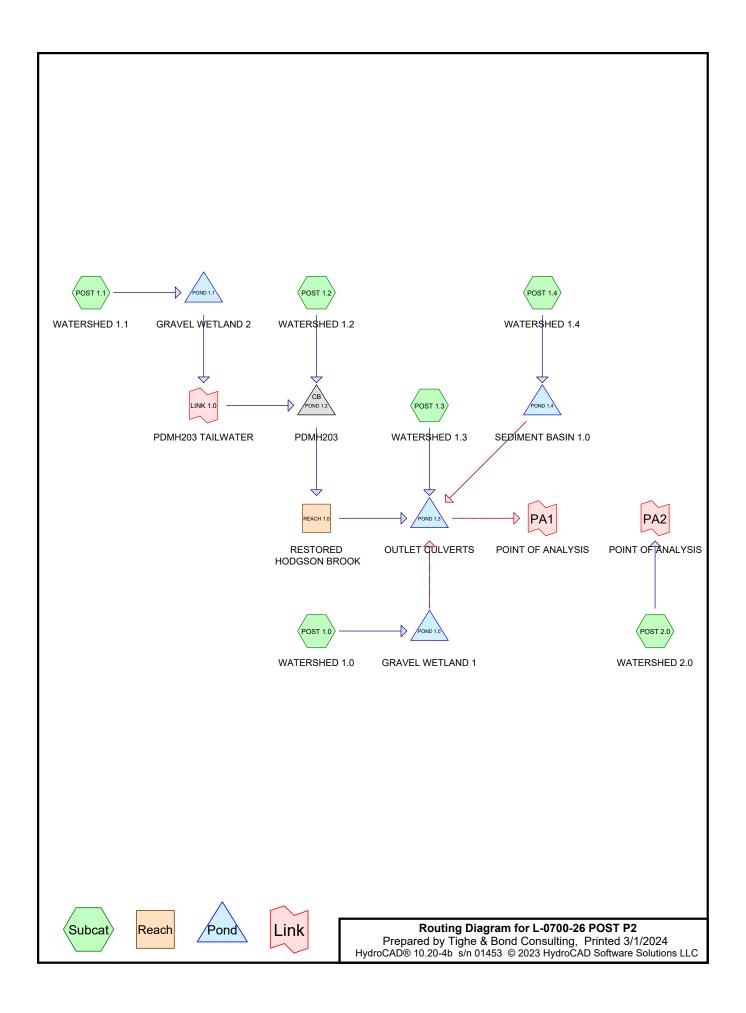
> Total Runoff Area = 31.609 ac Runoff Volume = 13.108 af Average Runoff Depth = 4.98" 61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

L-0700-26 POST P2 Type III 24-hr 50 Year Rainfall=8.46" Prepared by Tighe & Bond Printed 7/13/2023 HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC Page 18 Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>7.25" Flow Length=933' Tc=11.4 min CN=90 Runoff=66.89 cfs 6.105 af Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>5.81" SubcatchmentPOST 1.1: WATERSHED Flow Length=464' Tc=8.3 min CN=78 Runoff=22.21 cfs 1.750 af Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>6.89" SubcatchmentPOST 1.2: WATERSHED Flow Length=1,191' Tc=6.4 min CN=87 Runoff=19.47 cfs 1.503 af Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>5.77" SubcatchmentPOST 1.3: WATERSHED Flow Length=1,525' Tc=45.9 min CN=78 Runoff=21.37 cfs 3.312 af SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>5.33" Flow Length=585' Tc=13.5 min CN=74 Runoff=35.32 cfs 3.218 af SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>6.89" Flow Length=758' Tc=5.0 min CN=87 Runoff=8.76 cfs 0.651 af Reach REACH 1.0: RESTORED Avg. Flow Depth=0.92' Max Vel=2.24 fps Inflow=19.47 cfs 1.503 af n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=11.76 cfs 1.495 af Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=47.39' Storage=96,897 cf Inflow=66.89 cfs 6.105 af Primary=19.58 cfs 3.347 af Secondary=33.37 cfs 1.209 af Outflow=52.94 cfs 4.556 af Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=56.11' Storage=76,209 cf Inflow=22.21 cfs 1.750 af Outflow=0.00 cfs 0.000 af Peak Elev=51.13' Inflow=19.47 cfs 1.503 af Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=19.47 cfs 1.503 af Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.58' Storage=22,150 cf Inflow=76.91 cfs 10.982 af Primary=74.09 cfs 10.655 af Secondary=0.00 cfs 0.000 af Outflow=74.09 cfs 10.655 af Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=47.02' Storage=90,878 cf Inflow=35.32 cfs 3.218 af Primary=2.39 cfs 1.619 af Secondary=0.00 cfs 0.000 af Outflow=2.39 cfs 1.619 af Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af Link PA1: POINT OF ANALYSIS Inflow=74.09 cfs 10.655 af Primary=74.09 cfs 10.655 af Inflow=8.76 cfs 0.651 af Link PA2: POINT OF ANALYSIS Primary=8.76 cfs 0.651 af

> Total Runoff Area = 31.609 ac Runoff Volume = 16.539 af Average Runoff Depth = 6.28" 61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

Phase 2 (2024 Amended) Post-Development Calculations





Area Listing (all nodes)

Area (acres)	-	Description (subcatchment-numbers)
2.312		>75% Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3,
2.012	. 01	POST 1.4)
13.542	2 74	>75% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0)
1.467	' 80	>75% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4)
0.514		Meadow, non-grazed, HSG B (POST 1.3)
1.662	2 71	Meadow, non-grazed, HSG C (POST 1.3)
0.639	98	Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3)
6.974	98	Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4,
		POST 2.0)
0.137	' 98	Paved parking, HSG D (POST 1.0, POST 1.3)
0.120) 98	Roofs, HSG B (POST 1.0)
3.526	6 98	Roofs, HSG C (POST 1.0, POST 2.0)
0.714	98	Roofs, HSG D (POST 1.0)
31.609	82	TOTAL AREA

Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
3.586	HSG B	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4
25.705	HSG C	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0
2.318	HSG D	POST 1.0, POST 1.3, POST 1.4
0.000	Other	
31.609		TOTAL AREA

L-0700-26 POST P2 Prepared by Tighe & Bond Consulting HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solutions	Type III 24-hr 2 Year Rainfall=3.68" Printed 3/1/2024 SLLC Page 4
Time span=0.00-24.00 hrs, dt=0.05 hrs Runoff by SCS TR-20 method, UH=SCS, Reach routing by Dyn-Stor-Ind method - Pond routir	Weighted-CN
	71.49% Impervious Runoff Depth>2.61" 4 min CN=90 Runoff=25.38 cfs 2.201 af
	30.92% Impervious Runoff Depth>1.63" 3.3 min CN=78 Runoff=6.25 cfs 0.492 af
	58.28% Impervious Runoff Depth>2.34" 6.4 min CN=87 Runoff=6.94 cfs 0.511 af
	23.27% Impervious Runoff Depth>1.62" 6.9 min CN=78 Runoff=5.96 cfs 0.929 af
SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 s Flow Length=585' Tc=13	f 0.42% Impervious Runoff Depth>1.36" 5.5 min CN=74 Runoff=8.76 cfs 0.822 af
SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,336 sf Flow Length=758' Tc=5	53.76% Impervious Runoff Depth>2.34" .0 min CN=87 Runoff=3.10 cfs 0.221 af
Reach REACH 1.0: RESTORED Avg. Flow Depth=0.63' M n=0.040 L=1,309.0' S=0.0092 '/' Capacity	1ax Vel=2.08 fps Inflow=6.94 cfs 0.511 af y=2,720.29 cfs Outflow=4.97 cfs 0.507 af
Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=46.02' Stor Primary=0.96 cfs 0.874 af Secondary=0.00	rage=67,987 cf Inflow=25.38 cfs 2.201 af 0 cfs 0.000 af Outflow=0.96 cfs 0.874 af
Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=52.38' Sto	orage=21,415 cf Inflow=6.25 cfs 0.492 af Outflow=0.00 cfs 0.000 af
	Peak Elev=50.38' Inflow=6.94 cfs 0.511 af 0' S=0.0050 '/' Outflow=6.94 cfs 0.511 af
Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' S Primary=9.25 cfs 2.856 af Secondary=0.0	Storage=8,981 cf Inflow=9.25 cfs 3.060 af 0 cfs 0.000 af Outflow=9.25 cfs 2.856 af
Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=44.62' Sto Primary=0.51 cfs 0.751 af Secondary=0.0	orage=21,007 cf Inflow=8.76 cfs 0.822 af 0 cfs 0.000 af Outflow=0.51 cfs 0.751 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Link PA1: POINT OF ANALYSIS	Inflow=9.25 cfs 2.856 af Primary=9.25 cfs 2.856 af
Link PA2: POINT OF ANALYSIS	Inflow=3.10 cfs 0.221 af Primary=3.10 cfs 0.221 af
Total Runoff Area = 31.609 ac Runoff Volume =	5.176 af Average Runoff Depth = 1.96

Total Runoff Area = 31.609 acRunoff Volume = 5.176 afAverage Runoff Depth = 1.96"61.68% Pervious = 19.497 ac38.32% Impervious = 12.112 ac

L-0700-26 POST P2 Prepared by Tighe & Bond Consulting HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solution	Type III 24-hr 10 Year Rainfall=5.58" Printed 3/1/2024 ns LLC Page 5
Time span=0.00-24.00 hrs, dt=0.05 h Runoff by SCS TR-20 method, UH=SC Reach routing by Dyn-Stor-Ind method - Pond rou	S, Weighted-CN
	sf 71.49% Impervious Runoff Depth>4.43" 1.4 min CN=90 Runoff=42.01 cfs 3.732 af
	sf 30.92% Impervious Runoff Depth>3.21" 8.3 min CN=78 Runoff=12.40 cfs 0.966 af
	sf 58.28% Impervious Runoff Depth>4.11" 6.4 min CN=87 Runoff=11.94 cfs 0.897 af
	sf 23.27% Impervious Runoff Depth>3.18" 5.9 min CN=78 Runoff=11.87 cfs 1.826 af
SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 Flow Length=585' Tc=13	7 sf 0.42% Impervious Runoff Depth>2.83" 3.5 min CN=74 Runoff=18.77 cfs 1.708 af
SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,336 s Flow Length=758' Tc=	sf 53.76% Impervious Runoff Depth>4.11" =5.0 min CN=87 Runoff=5.36 cfs 0.388 af
	Max Vel=2.20 fps Inflow=11.94 cfs 0.897 af city=2,720.29 cfs Outflow=6.12 cfs 0.891 af
	torage=83,438 cf Inflow=42.01 cfs 3.732 af 86 cfs 0.170 af Outflow=15.08 cfs 2.275 af
Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=54.11' St	torage=42,049 cf Inflow=12.40 cfs 0.966 af Outflow=0.00 cfs 0.000 af
	Peak Elev=50.72' Inflow=11.94 cfs 0.897 af .0' S=0.0050 '/' Outflow=11.94 cfs 0.897 af
	torage=13,560 cf Inflow=31.34 cfs 5.942 af 00 cfs 0.000 af Outflow=31.22 cfs 5.655 af
	torage=50,580 cf Inflow=18.77 cfs 1.708 af 0.00 cfs 0.000 af Outflow=0.68 cfs 0.950 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Link PA1: POINT OF ANALYSIS	Inflow=31.22 cfs 5.655 af Primary=31.22 cfs 5.655 af
Link PA2: POINT OF ANALYSIS	Inflow=5.36 cfs 0.388 af Primary=5.36 cfs 0.388 af
Total Runoff Area = 31 609 ac Runoff Volume	= 9 517 af Average Runoff Depth = 3 61

Total Runoff Area = 31.609 ac Runoff Volume = 9.517 af Average Runoff Depth = 3.61" 61.68% Pervious = 19.497 ac 38.32% Impervious = 12.112 ac

Summary for Subcatchment POST 1.0: WATERSHED 1.0

- [47] Hint: Peak is 1668% of capacity of segment #4
- [47] Hint: Peak is 1668% of capacity of segment #5
- [47] Hint: Peak is 920% of capacity of segment #6
- [47] Hint: Peak is 566% of capacity of segment #7
- [47] Hint: Peak is 566% of capacity of segment #8
- [47] Hint: Peak is 120% of capacity of segment #9 [47] Hint: Peak is 4305% of capacity of segment #10
- Runoff = 42.01 cfs @ 12.16 hrs, Volume= 3.732 af, Depth> 4.43" Routed to Pond POND 1.0 : GRAVEL WETLAND 1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description	
5,235	98	Roofs, HSG B	
29,148	61	>75% Grass cover, Good, HSG B	
18,966	98	Paved parking, HSG B	
143,455	98	Roofs, HSG C	
81,718	74	>75% Grass cover, Good, HSG C	
110,540	98	Paved parking, HSG C	
31,119	98	Roofs, HSG D	
14,671	80	>75% Grass cover, Good, HSG D	
5,480	98	Paved parking, HSG D	
440,332	90	Weighted Average	
125,537		28.51% Pervious Area	
314,795		71.49% Impervious Area	

L-0700-26 POST P2

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Tc Length Slope Velocity Capacity Description

(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	l l
7.7	70	0.0150	0.15		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.68"
0.2	32	0.0200	2.87		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
0.1	19	0.0200	2.12		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
0.8	162	0.0050	3.21	2.52	
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013 Corrugated PE, smooth interior
0.4	84	0.0050	3.21	2.52	
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013
0.5	113	0.0050	3.72	4.57	
					15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
				- 40	n= 0.013
1.2	299	0.0050	4.20	7.43	
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
			4.00	- 40	n= 0.013
0.4	94	0.0050	4.20	7.43	
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
0.4	40	0.0040	44.40	05.05	n= 0.013
0.1	46	0.0240	11.16	35.05	Pipe Channel,
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'
~ ~	-	0 0000	740	0.00	n= 0.013
0.0	5	0.0800	7.16	0.98	Pipe Channel,

 0.0
 5
 0.0800
 7.16
 0.98
 Pipe Channel,

 5.0"
 Round Area= 0.1 sf Perim= 1.3' r= 0.10'

 n= 0.013

 0.0
 9
 0.0110
 9.90
 69.95
 Pipe Channel,

 36.0"
 Round Area= 7.1 sf Perim= 9.4' r= 0.75'

 n= 0.013

11.4 933 Total

Summary for Subcatchment POST 1.1: WATERSHED 1.1

Runoff = 12.40 cfs @ 12.12 hrs, Volume= 0.966 af, Depth> 3.21" Routed to Pond POND 1.1 : GRAVEL WETLAND 2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description				
36,403	61	>75% Grass cover, Good, HSG B				
3,210	98	Paved parking, HSG B				
72,351	74	>75% Grass cover, Good, HSG C				
45,464	98	Paved parking, HSG C				
157,428	78	Weighted Average				
108,754		69.08% Pervious Area				
48,674		30.92% Impervious Area				

Type III 24-hr 10 Year Rainfall=5.58" Printed 3/1/2024

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Type III 24-hr 10 Year Rainfall=5.58" Printed 3/1/2024 HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solutions LLC Page 8

	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	5.8	100	0.0625	0.29		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.68"
	2.2	312	0.0220	2.39		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.3	33	0.0150	1.84		Shallow Concentrated Flow,
						Grassed Waterway Kv= 15.0 fps
	0.0	19	0.3300	8.62		Shallow Concentrated Flow,
_						Grassed Waterway Kv= 15.0 fps

8.3 464 Total

Summary for Subcatchment POST 1.2: WATERSHED 1.2

- [47] Hint: Peak is 437% of capacity of segment #3
- [47] Hint: Peak is 261% of capacity of segment #4
- [47] Hint: Peak is 161% of capacity of segment #5

Runoff	=	11.94 cfs @	12.09 hrs,	Volume=
Route	d to P	ond POND 1.2 :	PDMH203	

0.897 af, Depth> 4.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Α	rea (sf)	CN D	escription					
	9,848	61 >	61 >75% Grass cover, Good, HSG B					
	4,784	98 P	98 Paved parking, HSG B					
	37,701	74 >	75% Gras	s cover, Go	bod, HSG C			
	61,646	98 P	aved park	ing, HSG C				
1	13,979	87 W	/eighted A	verage				
	47,549	4	1.72% Per	vious Area				
	66,430	5	8.28% Imp	pervious Ar	ea			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
1.5	100	0.0100	1.12		Sheet Flow,			
					Smooth surfaces n= 0.011 P2= 3.68"			
1.0	153	0.0150	2.49		Shallow Concentrated Flow,			
					Paved Kv= 20.3 fps			
1.6	343	0.0050	3.47	2.73	Pipe Channel,			
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
					n= 0.012 Concrete pipe, finished			
0.1	13	0.0050	3.72	4.57				
					15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'			
					n= 0.013 Corrugated PE, smooth interior			
1.8	453	0.0050	4.20	7.43				
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'			
					n= 0.013 Corrugated PE, smooth interior			
0.4	129	0.0050	5.91	29.00	Pipe Channel,			
					30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63'			
					n= 0.013 Corrugated PE, smooth interior			

6.4 1,191 Total

Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 11.87 cfs @ 12.63 hrs, Volume= 1.826 af, Depth> 3.18" Routed to Pond POND 1.3 : OUTLET CULVERTS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN D	escription						
	1,830	61 >	61 >75% Grass cover, Good, HSG B						
	22,404	58 N	leadow, no	on-grazed,	HSG B				
	896	98 P	aved park	ing, HSG E	3				
1	31,991	74 >	75% Gras	s cover, Go	bod, HSG C				
	68,446			ing, HSG C					
	72,396			on-grazed,					
	1,638				bod, HSG D				
	499	98 P	aved park	ing, HSG E)				
3	00,100	78 V	/eighted A	verage					
2	30,259	7	6.73% Pei	rvious Area	l				
	69,841	2	3.27% Imp	pervious Ar	ea				
_		-							
Tc	Length	Slope		Capacity	Description				
(min)									
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
10.9	(feet) 100	(ft/ft) 0.0130	(ft/sec) 0.15	(cts)	Sheet Flow,				
10.9	100	0.0130	0.15	(cts)	Grass: Short n= 0.150 P2= 3.68"				
	100			(cts)	Grass: Short n= 0.150 P2= 3.68" Shallow Concentrated Flow,				
10.9 1.1	100 52	0.0130 0.0130	0.15 0.80	(cts)	Grass: Short n= 0.150 P2= 3.68" Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps				
10.9	100	0.0130	0.15	(cts)	Grass: Short n= 0.150 P2= 3.68" Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow,				
10.9 1.1 0.1	100 52 27	0.0130 0.0130 0.2720	0.15 0.80 7.82	<u>(cts)</u>	Grass: Short n= 0.150 P2= 3.68" Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps				
10.9 1.1	100 52	0.0130 0.0130	0.15 0.80	<u>(cts)</u>	Grass: Short n= 0.150 P2= 3.68" Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps Shallow Concentrated Flow,				
10.9 1.1 0.1	100 52 27	0.0130 0.0130 0.2720	0.15 0.80 7.82	<u>(cts)</u>	Grass: Short n= 0.150 P2= 3.68" Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps				

Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff = 18.77 cfs @ 12.19 hrs, Volume= 1.708 af, Depth> 2.83" Routed to Pond POND 1.4 : SEDIMENT BASIN 1.0

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

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Type III 24-hr 10 Year Rainfall=5.58" Printed 3/1/2024 HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solutions LLC Page 10

٨	roo (of))						
A	rea (sf)		CN Description						
	23,477	61 >	61 >75% Grass cover, Good, HSG B						
2	43,330	74 >	>75% Grass cover, Good, HSG C						
	1,334	98 F	aved park	ing, HSG C					
	47,586				bod, HSG D				
	0			ace, HSG D					
	-			,					
	15,727		Veighted A	0					
3	14,393	•		vious Area					
	1,334	0	.42% Impe	ervious Are	а				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
8.4	100	0.0245	0.20	· · · · ·	Sheet Flow,				
0.4	100	0.0240	0.20		Grass: Short n= 0.150 P2= 3.68"				
E 1	165	0 0 1 0 2	1 50						
5.1	465	0.0103	1.52		Shallow Concentrated Flow,				
					Grassed Waterway Kv= 15.0 fps				
0.0	20	0.3300	8.62		Shallow Concentrated Flow,				
					Grassed Waterway Kv= 15.0 fps				
13.5	585	Total							

Summary for Subcatchment POST 2.0: WATERSHED 2.0

[49] Hint: Tc<2dt may require smaller dt

5.36 cfs @ 12.07 hrs, Volume= Runoff = Routed to Link PA2 : POINT OF ANALYSIS

0.388 af, Depth> 4.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

	Area (sf)	CN E	Description				
	10,145	98 F	98 Roofs, HSG C				
	22,815	74 >	75% Gras	s cover, Go	bod, HSG C		
	16,376	98 F	aved park	ing, HSG C			
	49,336	87 V	Veighted A	verage			
	22,815	4	6.24% Pei	vious Area			
	26,521	5	3.76% Imp	pervious Ar	ea		
Т	c Length	Slope	Velocity	Capacity	Description		
(min) (feet)	(ft/ft)	(ft/sec)	(cfs)			
1.:	2 100	0.0164	1.36		Sheet Flow,		
					Smooth surfaces n= 0.011 P2= 3.68"		
0.	3 48	0.0164	2.60		Shallow Concentrated Flow,		
					Paved Kv= 20.3 fps		
0.	3 130	0.0140	7.03	12.43	Pipe Channel,		
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'		
					n= 0.013		
0.	5 70	0.0250	2.37		Shallow Concentrated Flow,		
					Grassed Waterway Kv= 15.0 fps		
1.	3 410	0.0050	5.09	16.00			
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'		

n= 0.013

3.6 758 Total, Increased to minimum Tc = 5.0 min

Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

 Inflow Area =
 6.231 ac, 42.41% Impervious, Inflow Depth >
 1.73" for 10 Year event

 Inflow =
 11.94 cfs @
 12.09 hrs, Volume=
 0.897 af

 Outflow =
 6.12 cfs @
 12.86 hrs, Volume=
 0.891 af, Atten= 49%, Lag= 45.9 min

 Routed to Pond POND 1.3 : OUTLET CULVERTS
 0.891 af, Atten= 49%, Lag= 45.9 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Max. Velocity= 2.20 fps, Min. Travel Time= 9.9 min Avg. Velocity = 0.85 fps, Avg. Travel Time= 25.6 min

Peak Storage= 6,846 cf @ 12.27 hrs Average Depth at Peak Storage= 0.82', Surface Width= 30.44' Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs

Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals) Constant n= 0.040 Winding stream, pools & shoals Inlet Invert= 48.00', Outlet Invert= 36.00'

±

	Off	set	Eleva	tion	Cha	n.Dep	oth		
_	(fe	et)	(fe	eet)		(fe	et)		
	0	.00	12	2.00		0.	00		
	18	.00	6	6.00		6.	00		
	30	.25	6	6.00		6.	00		
	31	.75	5	5.25		6.	75		
	34	.25	5	5.25		6.	75		
	35	.75	6	6.00		6.	00		
	48	.00	6	6.00		6.	00		
	66	.00	12	2.00		0.	00		
	Depth				erim.		idth	St	-
_	(feet)	(sq-ft)	(1	eet)	(fe	eet)	(cubic	;-1
	0.00		0.0		2.5		0.0		

Depth	End Area	Perim.	Width	Storage	Discharge
(feet)	(sq-ft)	(feet)	(feet)	(cubic-feet)	(cfs)
0.00	0.0	2.5	0.0	0	0.00
0.75	3.0	30.4	30.0	3,927	2.28
6.75	291.0	68.3	66.0	380,919	2,720.29

Summary for Pond POND 1.0: GRAVEL WETLAND 1

[95] Warning: Outlet Device #4 rise exceeded

Inflow Area =	10.109 ac, 7	1.49% Impervious, Inflow	Depth > 4.43" for 10 Year event
Inflow =	42.01 cfs @	12.16 hrs, Volume=	3.732 af
Outflow =	15.08 cfs @	12.50 hrs, Volume=	2.275 af, Atten= 64%, Lag= 20.8 min
Primary =	9.22 cfs @	12.50 hrs, Volume=	2.105 af
Routed to Por	nd POND 1.3 : (OUTLET CULVERTS	
Secondary =	5.86 cfs @	12.50 hrs, Volume=	0.170 af
Routed to Por	nd POND 1.3 : (OUTLET CULVERTS	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 46.78' @ 12.50 hrs Surf.Area= 21,240 sf Storage= 83,438 cf Flood Elev= 48.00' Surf.Area= 23,557 sf Storage= 110,845 cf

Plug-Flow detention time= 226.3 min calculated for 2.275 af (61% of inflow) Center-of-Mass det. time= 125.2 min (916.2 - 791.0)

Volume	Invert	Avai	il.Stora	ge Storage Descr	iption		
#1	39.05'	1	10,845	cf Custom Stage	e Data (Prismatio	c)Listed below (Recalc)	
Elevatio (fee		urf.Area (sq-ft)	Voids (%)		Cum.Store (cubic-feet)		
39.0)5	9,855	0.0		0		
41.3	35	9,855	30.0		6,800		
42.0	00	9,855	45.0	2,883	9,683		
43.0		11,943	100.0	,	20,582		
44.(14,202	100.0	,	33,654		
45.0		16,891	100.0	,	49,201		
46.0		19,752	100.0	,	67,522		
47.0		21,668	100.0	,	88,232		
48.0	00	23,557	100.0	22,613	110,845		
Device	Routing	In	vert	Outlet Devices			
#1	Primary	41	.35'	18.0" Round Culve	ert		
	-		I	_= 30.0' CPP, squa	are edge headwa	II, Ke= 0.500	
						S= 0.0050 '/' Cc= 0.900	
						erior, Flow Area= 1.77 sf	
#2	Device 1			3.5" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads			
#3	Device 1					Limited to weir flow at low heads	
#4	Device 1	46				l Rectangular Weir	
	D · · · ·			2 End Contraction(s			
#5			4.0" x 4.0" Horiz. O		16.00 $C = 0.600$		
#6	Secondary	16		_imited to weir flow		reated Bastangular Wair	
#0	Secondary	40				rested Rectangular Weir 00 1.20 1.40 1.60	
						1 2.63 2.64 2.64 2.63	
				2.00	5 2.10 2.10 2.04	7 2.00 2.04 2.04 2.00	

Primary OutFlow Max=9.22 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater)

2=Orifice/Grate (Orifice Controls 0.74 cfs @ 11.06 fps)

-3=Orifice/Grate (Orifice Controls 0.30 cfs @ 6.19 fps)

-4=Sharp-Crested Rectangular Weir (Orifice Controls 8.17 cfs @ 4.19 fps)

-5=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=5.85 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater) -6=Broad-Crested Rectangular Weir (Weir Controls 5.85 cfs @ 1.41 fps)

Summary for Pond POND 1.1: GRAVEL WETLAND 2

Inflow Area	=	3.614 ac, 3	0.92% Impervious, In	nflow Depth > 3.21" for 10 Year event			
Inflow	=	12.40 cfs @	12.12 hrs, Volume=	0.966 af			
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 100%, Lag= 0.0 min			
Primary	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af			
Routed to Link LINK 1.0 : PDMH203 TAILWATER							

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 54.11' @ 24.00 hrs Surf.Area= 14,115 sf Storage= 42,049 cf Flood Elev= 57.00' Surf.Area= 21,643 sf Storage= 94,743 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invei	rt Ava	il.Stora	ge Storage Descr	iption			
#1	47.55	5' 1	17,304	cf Custom Stage	e Data (Prismatic)L	isted below (Recalc)		
Elevatio (fee		Surf.Area (sq-ft)	Voids (%)		Cum.Store (cubic-feet)			
47.5	1	6,269	0.0		0			
49.8	35	6,269	30.0	4,326	4,326			
50.8	50	6,269	45.0	1,834	6,159			
51.0	00	7,199	100.0	3,367	9,526			
52.0	00	9,187	100.0	,	17,719			
53.0	00	11,345	100.0		27,985			
54.0	00	13,814	100.0	,	40,565			
55.0		16,645	100.0	,	55,794			
56.0		19,805	100.0	,	74,019			
58.0	00	23,480	100.0	43,285	117,304			
Device	Routing	In	vert	Outlet Devices				
#1	Primary	49	9.85'	24.0" Round Culve	ert			
	-			L= 12.0' CPP, squa	are edge headwall,	Ke= 0.500		
				nlet / Outlet Invert=	49.85'/49.45' S=	0.0333 '/' Cc= 0.900		
				n= 0.013 Corrugate	d PE, smooth interio	or, Flow Area= 3.14 sf		
#2	Device 1	49	9.85'	5' 2.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low head				
#3	Device 1	53						
	_			2 End Contraction(s		•• • • • • • •		
#4	#4 Device 1 56.50' 4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600					00 $C = 0.600$		

Limited to weir flow at low heads

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=47.55' TW=55.07' (Dynamic Tailwater)

-2=Orifice/Grate (Controls 0.00 cfs)

-3=Sharp-Crested Rectangular Weir(Controls 0.00 cfs)

-4=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond POND 1.2: PDMH203

 Inflow Area =
 6.231 ac, 42.41% Impervious, Inflow Depth > 1.73" for 10 Year event

 Inflow =
 11.94 cfs @
 12.09 hrs, Volume=
 0.897 af

 Outflow =
 11.94 cfs @
 12.09 hrs, Volume=
 0.897 af, Atten= 0%, Lag= 0.0 min

 Primary =
 11.94 cfs @
 12.09 hrs, Volume=
 0.897 af, Atten= 0%, Lag= 0.0 min

 Primary =
 11.94 cfs @
 12.09 hrs, Volume=
 0.897 af

 Routed to Reach REACH 1.0 : RESTORED HODGSON BROOK
 0.807 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 50.72' @ 12.09 hrs Flood Elev= 57.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.35'	48.0" Round Culvert
			L= 269.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 49.35' / 48.00' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 12.57 sf

Primary OutFlow Max=11.76 cfs @ 12.09 hrs HW=50.71' TW=48.76' (Dynamic Tailwater) -1=Culvert (Inlet Controls 11.76 cfs @ 3.13 fps)

Summary for Pond POND 1.3: OUTLET CULVERTS

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=12) [62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.58' @ 23.95 hrs

Inflow Area =	30.477 ac, 37.74% Impervious, Inflow	Depth > 2.34" for 10 Year event
Inflow =	31.34 cfs @ 12.51 hrs, Volume=	5.942 af
Outflow =	31.22 cfs @ 12.53 hrs, Volume=	5.655 af, Atten= 0%, Lag= 1.3 min
Primary =	31.22 cfs @ 12.53 hrs, Volume=	5.655 af
Routed to Link	(PA1 : POINT OF ANALYSIS	
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af
Routed to Link	(PA1 : POINT OF ANALYSIS	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 38.77' @ 12.53 hrs Surf.Area= 8,870 sf Storage= 13,560 cf Flood Elev= 43.50' Surf.Area= 95,977 sf Storage= 236,017 cf

Plug-Flow detention time= 56.2 min calculated for 5.642 af (95% of inflow) Center-of-Mass det. time= 29.8 min (900.3 - 870.4)

	-201 00					
Prepare	ed by Tigh	e & Bond Co	nsulting	Prir	nted 3/1/2024	
			2023 HydroCA	IST C	Page 15	
<u>i iyaroo,</u>	10.20		2020 Hydroo, a	D Contraro Condion		
Volume	Inve	rt Avail St	orage Storage	Description		
			<u> </u>			
#1	35.0	0' 236,0	17 cf Custon	n Stage Data (Pri	smatic)Listed below (Reca	lc)
Elevatio	on d	Surf.Area	Inc.Store	Cum.Store		
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)		
35.0	00	960	0	0		
36.0	00	1,428	1,194	1,194		
38.0	00	5,418	6,846	8,040		
40.0	00	14,354	19,772	27,812		
42.0	00	66,884	81,238	109,050		
43.0	00	92,707	79,796	188,846		
43.5	50	95,977	47,171	236,017		
		, -	,) -		
Device	Routing	Invert	Outlet Device	es		
#1	Primary	35.60'	42.0" W x 29	9.0" H. R=21.5"/6	6.1" Pipe Arch CMP_Arcl	h 1/2 42x29 X 3.00
	· · · · · · · · · · · · · · · · · · ·				eadwall, Ke= 0.500	
					5.30' S= 0.0044 '/' Cc= 0.	900
					low Area= 6.72 sf	
#2	Seconda	ry 43.00'			' rise Sharp-Crested Vee/	Tran Woir
#2	Seconda	iy 43.00	Cv= 2.47 (C=			
			Uv- 2.47 (U-	- 3.09)		

Type III 24-hr 10 Year Rainfall=5.58"

Primary OutFlow Max=31.11 cfs @ 12.53 hrs HW=38.77' TW=38.65' (Dynamic Tailwater) **1=CMP_Arch_1/2 42x29** (Outlet Controls 31.11 cfs @ 1.55 fps)

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Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=35.04' TW=38.65' (Dynamic Tailwater) 2=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

Summary for Pond POND 1.4: SEDIMENT BASIN 1.0

Inflow Area =	7.248 ac,	0.42% Impervious, Inflow E	Depth > 2.83" for 10 Year event
Inflow =	18.77 cfs @	12.19 hrs, Volume=	1.708 af
Outflow =	0.68 cfs @	17.24 hrs, Volume=	0.950 af, Atten= 96%, Lag= 303.1 min
Primary =	0.68 cfs @	17.24 hrs, Volume=	0.950 af
Routed to Por	d POND 1.3	: OUTLET CULVERTS	
Secondary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af
Routed to Por	nd POND 1.3	: OUTLET CULVERTS	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Starting Elev= 44.15' Surf.Area= 18,132 sf Storage= 11,702 cf Peak Elev= 45.79' @ 17.24 hrs Surf.Area= 29,244 sf Storage= 50,580 cf (38,878 cf above start) Flood Elev= 48.50' Surf.Area= 38,802 sf Storage= 127,441 cf (115,739 cf above start)

Plug-Flow detention time= 356.2 min calculated for 0.680 af (40% of inflow) Center-of-Mass det. time= 9.2 min (846.8 - 837.5)

Volume	Invert	Avail.Storage	Storage Description
#1	43.00'	127,441 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

L-0700-26 POST P2 Prepared by Tighe & Bond Consulting

Elevatio	on S	Surf.Area	Inc.Store	Cum.Store		
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)		
43.0	00	1,000	0	0		
44.(00	17,117	9,059	9,059		
46.0	00	30,657	47,774	56,833		
47.0	00	35,879	33,268	90,101		
48.0	00	38,802	37,341	127,441		
Device	Routing	Invert	Outlet Devices	S		
#1	Primary	42.75'	12.0" Round	Culvert L= 66	.0' Ke= 0.500	
			Inlet / Outlet Ir	nvert= 42.75' / 4	2.40' S= 0.0053 '/' Cc= 0.900	
			n= 0.013, Flo	w Area= 0.79 sf		
#2	Device 1	43.00'	4.0" Vert. Ori	fice/Grate C=	0.600 Limited to weir flow at low heads	
#3 Device 1 46.80'		10.0" x 17.5" Horiz. Orifice/Grate C= 0.600				
Limited to wei				r flow at low hea	ads	
#4	Secondar	y 47.40'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28)			

Head (feet) 0.00 1.10 Width (feet) 8.00 14.60

Primary OutFlow Max=0.68 cfs @ 17.24 hrs HW=45.79' TW=38.65' (Dynamic Tailwater)

-1=Culvert (Passes 0.68 cfs of 5.16 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.68 cfs @ 7.80 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=44.15' TW=35.04' (Dynamic Tailwater) **4=Custom Weir/Orifice** (Controls 0.00 cfs)

Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.1 by 7.52' @ 0.00 hrs (23.95 cfs 41.618 af) 3.614 ac, 30.92% Impervious, Inflow Depth = 0.00" for 10 Year event Inflow Area = Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Primary 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min = Routed to Pond POND 1.2 : PDMH203 Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 25 P	oint manua	l elevation t	table, To=	0.00 hrs,	dt= 1.00 hrs,	feet =		
55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07
55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07
55.07	55.07	55.07	55.07	55.07	55.07	55.07		

Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.3 by 3.61' @ 0.00 hrs (92.51 cfs 60.023 af)

Inflow Are	a =	30.477 ac, 3	87.74% Impe	ervious,	Inflow De	epth > 2.2	23" for 10	Year event
Inflow	=	31.22 cfs @	12.53 hrs,	Volume	=	5.655 af		
Primary	=	31.22 cfs @	12.53 hrs,	Volume	=	5.655 af,	Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 2 Point manual elevation table, To= 0.00 hrs, dt= 24.00 hrs, feet = 38.65 38.65

Summary for Link PA2: POINT OF ANALYSIS

 Inflow Area =
 1.133 ac, 53.76% Impervious, Inflow Depth > 4.11" for 10 Year event

 Inflow =
 5.36 cfs @ 12.07 hrs, Volume=
 0.388 af

 Primary =
 5.36 cfs @ 12.07 hrs, Volume=
 0.388 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

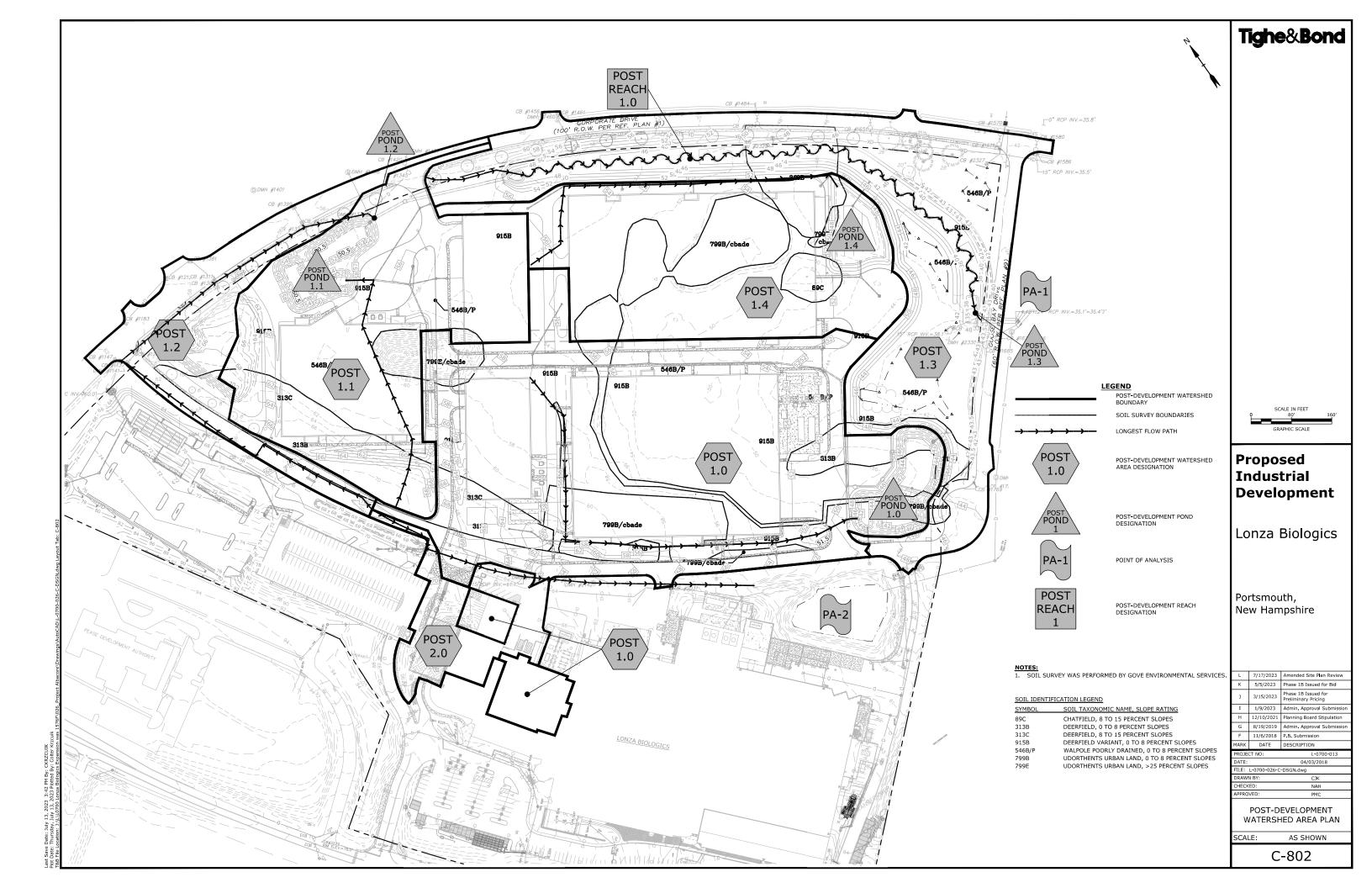
L-0700-26 POST P2 Prepared by Tighe & Bond Consulting HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solu	Type III 24-hr 25 Year Rainfall=7.07" Printed 3/1/2024 tions LLC Page 18
Time span=0.00-24.00 hrs, dt=0.04 Runoff by SCS TR-20 method, UH=S Reach routing by Dyn-Stor-Ind method - Pond r	SCS, Weighted-CN
	82 sf 71.49% Impervious Runoff Depth>5.88" =11.4 min CN=90 Runoff=54.93 cfs 4.956 af
	28 sf 30.92% Impervious Runoff Depth>4.53" c=8.3 min CN=78 Runoff=17.44 cfs 1.365 af
	79 sf 58.28% Impervious Runoff Depth>5.54" c=6.4 min CN=87 Runoff=15.85 cfs 1.209 af
	00 sf 23.27% Impervious Runoff Depth>4.50" =45.9 min CN=78 Runoff=16.75 cfs 2.583 af
SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,7 Flow Length=585' Tc:	727 sf 0.42% Impervious Runoff Depth>4.09" =13.5 min CN=74 Runoff=27.23 cfs 2.472 af
SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,33 Flow Length=758	36 sf 53.76% Impervious Runoff Depth>5.54" Tc=5.0 min CN=87 Runoff=7.12 cfs 0.523 af
	Max Vel=2.22 fps Inflow=15.85 cfs 1.209 af bacity=2,720.29 cfs Outflow=8.65 cfs 1.202 af
	Storage=90,424 cf Inflow=54.93 cfs 4.956 af 8.86 cfs 0.671 af Outflow=37.88 cfs 3.437 af
Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=55.22'	Storage=59,446 cf Inflow=17.44 cfs 1.365 af Outflow=0.00 cfs 0.000 af
Pond POND 1.2: PDMH203 48.0" Round Culvert n=0.013 L=20	Peak Elev=50.94' Inflow=15.85 cfs 1.209 af 69.0' S=0.0050 '/' Outflow=15.85 cfs 1.209 af
	Storage=17,433 cf Inflow=57.33 cfs 8.292 af 0.00 cfs 0.000 af Outflow=56.26 cfs 7.985 af
	Storage=77,792 cf Inflow=27.23 cfs 2.472 af =0.00 cfs 0.000 af Outflow=0.78 cfs 1.070 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Link PA1: POINT OF ANALYSIS	Inflow=56.26 cfs 7.985 af Primary=56.26 cfs 7.985 af
Link PA2: POINT OF ANALYSIS	Inflow=7.12 cfs 0.523 af Primary=7.12 cfs 0.523 af
Total Runoff Area = 31 609 ac Runoff Volum	a = 13.108 af Average Runoff Denth = 4.98

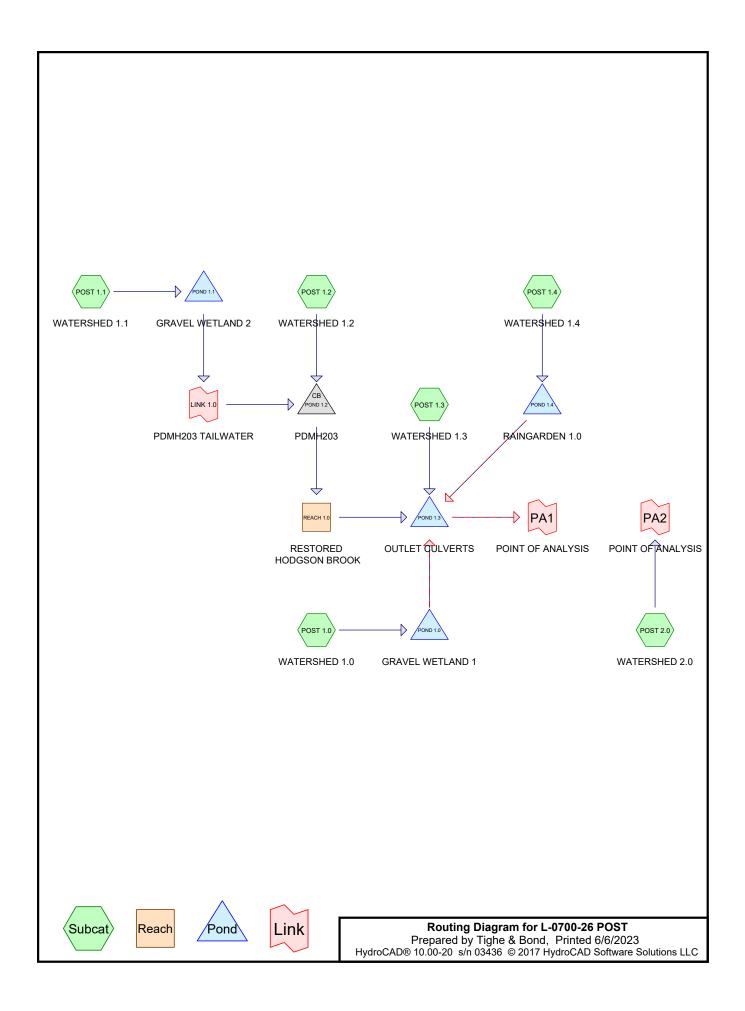
Total Runoff Area = 31.609 acRunoff Volume = 13.108 afAverage Runoff Depth = 4.98"61.68% Pervious = 19.497 ac38.32% Impervious = 12.112 ac

L-0700-26 POST P2 Prepared by Tighe & Bond Consulting HydroCAD® 10.20-4b s/n 01453 © 2023 HydroCAD Software Solution	Type III 24-hr 50 Year Rainfall=8.46" Printed 3/1/2024 ns LLC Page 19
Time span=0.00-24.00 hrs, dt=0.05 h Runoff by SCS TR-20 method, UH=SCS Reach routing by Dyn-Stor-Ind method , Pond rout	S, Weighted-CN
SubcatchmentPOST 1.0: WATERSHED Runoff Area=440,332 s Flow Length=933' Tc=11	sf 71.49% Impervious Runoff Depth>7.25" I.4 min CN=90 Runoff=66.89 cfs 6.105 af
	sf 30.92% Impervious Runoff Depth>5.81" 3.3 min CN=78 Runoff=22.21 cfs 1.750 af
SubcatchmentPOST 1.2: WATERSHED Runoff Area=113,979 s Flow Length=1,191' Tc=6	sf 58.28% Impervious Runoff Depth>6.89" 6.4 min CN=87 Runoff=19.47 cfs 1.503 af
SubcatchmentPOST 1.3: WATERSHED Runoff Area=300,100 s Flow Length=1,525' Tc=45	sf 23.27% Impervious Runoff Depth>5.77" 5.9 min CN=78 Runoff=21.37 cfs 3.312 af
SubcatchmentPOST 1.4: WATERSHED1.4 Runoff Area=315,727 Flow Length=585' Tc=13	sf 0.42% Impervious Runoff Depth>5.33" 3.5 min CN=74 Runoff=35.32 cfs 3.218 af
SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,336 s Flow Length=758' Tc=	sf 53.76% Impervious Runoff Depth>6.89" =5.0 min CN=87 Runoff=8.76 cfs 0.651 af
Reach REACH 1.0: RESTORED Avg. Flow Depth=0.92' M n=0.040 L=1,309.0' S=0.0092 '/' Capacity	/lax Vel=2.24 fps Inflow=19.47 cfs 1.503 af y=2,720.29 cfs Outflow=11.76 cfs 1.495 af
Pond POND 1.0: GRAVELWETLAND1Peak Elev=47.39' StPrimary=19.58 cfs3.347 afSecondary=33.3	torage=96,897 cf Inflow=66.89 cfs 6.105 af 37 cfs 1.209 af Outflow=52.94 cfs 4.556 af
Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=56.11' St	orage=76,209 cf Inflow=22.21 cfs 1.750 af Outflow=0.00 cfs 0.000 af
	Peak Elev=51.13' Inflow=19.47 cfs 1.503 af 0' S=0.0050 '/' Outflow=19.47 cfs 1.503 af
Pond POND 1.3: OUTLET CULVERTSPeak Elev=39.58' StoPrimary=74.09 cfs10.655 afSecondary=0.00	rage=22,150 cf Inflow=76.91 cfs 10.982 af cfs 0.000 af Outflow=74.09 cfs 10.655 af
	orage=90,878 cf Inflow=35.32 cfs 3.218 af .00 cfs 0.000 af Outflow=2.39 cfs 1.619 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=0.00 cfs 0.000 af Primary=0.00 cfs 0.000 af
Link PA1: POINT OF ANALYSIS	Inflow=74.09 cfs 10.655 af Primary=74.09 cfs 10.655 af
Link PA2: POINT OF ANALYSIS	Inflow=8.76 cfs 0.651 af Primary=8.76 cfs 0.651 af
Total Punoff Area = 31 609 ac Punoff Volume =	- 16 539 of Avorago Bunoff Donth - 6 28

Total Runoff Area = 31.609 acRunoff Volume = 16.539 afAverage Runoff Depth = 6.28"61.68% Pervious = 19.497 ac38.32% Impervious = 12.112 ac

Master Post-Development Calculations





Area Listing (all nodes)

Area	CN	Description		
 (acres)		(subcatchment-numbers)		
1.776	61	>75% Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3,		
		POST 1.4)		
6.801	74	>75% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3,		
		POST 1.4, POST 2.0)		
0.436	80	>75% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4)		
0.323	58	Meadow, non-grazed, HSG B (POST 1.3)		
3.143	71	Meadow, non-grazed, HSG C (POST 1.3)		
0.799	98	Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4)		
7.546	98	Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4,		
		POST 2.0)		
0.146	98	Paved parking, HSG D (POST 1.0, POST 1.3, POST 1.4)		
0.688	98	Roofs, HSG B (POST 1.0, POST 1.1, POST 1.4)		
8.166	98	Roofs, HSG C (POST 1.0, POST 1.1, POST 1.4, POST 2.0)		
1.737	98	Roofs, HSG D (POST 1.0, POST 1.4)		
0.049	76	Woods/grass comb., Fair, HSG C (POST 1.3)		
31.609	87	TOTAL AREA		

Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
3.586	HSG B	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4
25.705	HSG C	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0
2.318	HSG D	POST 1.0, POST 1.3, POST 1.4
0.000	Other	
31.609		TOTAL AREA

L-0700-26 POST Type Prepared by Tighe & Bond HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions LLC	e III 24-hr 2 Year Rainfall=3.68" Printed 6/6/2023 Page 4
Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 Runoff by SCS TR-20 method, UH=SCS, Weig Reach routing by Dyn-Stor-Ind method - Pond routing by	hted-CN
	9% Impervious Runoff Depth>2.71" CN=91 Runoff=27.46 cfs 2.396 af
	3% Impervious Runoff Depth>2.25" CN=86 Runoff=12.60 cfs 1.046 af
	5% Impervious Runoff Depth>2.43" CN=88 Runoff=6.37 cfs 0.471 af
	4% Impervious Runoff Depth>1.55" CN=77 Runoff=5.81 cfs 0.908 af
	5% Impervious Runoff Depth>3.01" CN=94 Runoff=15.51 cfs 1.236 af
SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,290 sf 80.99 Flow Length=758' Tc=5.0 min	9% Impervious Runoff Depth>2.91" CN=93 Runoff=3.72 cfs 0.274 af
Reach REACH 1.0: RESTORED Avg. Flow Depth=0.60' Max Ve n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,72	l=2.03 fps Inflow=6.37 cfs 0.617 af 0.29 cfs Outflow=4.54 cfs 0.608 af
Pond POND 1.0: GRAVEL WETLAND1Peak Elev=46.16' Storage=7Primary=1.57 cfs1.041 afSecondary=0.00 cfs0	70,734 cf Inflow=27.46 cfs 2.396 af 0.000 af Outflow=1.57 cfs 1.041 af
Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=53.90' Storage=3	9,230 cf Inflow=12.60 cfs 1.046 af Outflow=0.40 cfs 0.146 af
Pond POND 1.2: PDMH203 Peak El 48.0" Round Culvert n=0.013 L=269.0' S=0	ev=50.33' Inflow=6.37 cfs 0.617 af .0050 '/' Outflow=6.37 cfs 0.617 af
Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' Storage Primary=9.41 cfs 3.050 af Secondary=0.00 cfs 0	e=8,984 cf Inflow=9.25 cfs 3.255 af 0.000 af Outflow=9.41 cfs 3.050 af
Pond POND 1.4: RAINGARDEN1.0Peak Elev=47.27'Storage=3Primary=1.31 cfs0.699 afSecondary=0.00 cfs0	34,235 cf Inflow=15.51 cfs 1.236 af 0.000 af Outflow=1.31 cfs 0.699 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=0.40 cfs 0.146 af Primary=0.40 cfs 0.146 af
Link PA1: POINT OF ANALYSIS	Inflow=9.41 cfs 3.050 af Primary=9.41 cfs 3.050 af
Link PA2: POINT OF ANALYSIS	Inflow=3.72 cfs 0.274 af Primary=3.72 cfs 0.274 af
Total Bunaff Area = 21 609 ac Bunaff Valuma = 6 221	of Average Buneff Denth - 2.40

Total Runoff Area = 31.609 acRunoff Volume = 6.331 afAverage Runoff Depth = 2.40"39.63% Pervious = 12.527 ac60.37% Impervious = 19.083 ac

L-0700-26 POST Prepared by Tighe & Bond HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutions	Type III 24-hr 10 Year Rainfall=5.58"Printed 6/6/2023s LLCPage 5
Time span=0.00-24.00 hrs, dt=0.05 hrs Runoff by SCS TR-20 method, UH=SCS Reach routing by Dyn-Stor-Ind method - Pond routi	, Weighted-CN
SubcatchmentPOST 1.0: WATERSHED Runoff Area=462,599 sf Flow Length=933' Tc=11.4	72.19% Impervious Runoff Depth>4.54" 4 min CN=91 Runoff=44.88 cfs 4.017 af
	58.73% Impervious Runoff Depth>4.01" 3 min CN=86 Runoff=22.02 cfs 1.858 af
SubcatchmentPOST 1.2: WATERSHED Runoff Area=101,204 sf Flow Length=1,191' Tc=6.4	62.15% Impervious Runoff Depth>4.22" 4 min CN=88 Runoff=10.81 cfs 0.817 af
SubcatchmentPOST 1.3: WATERSHED Runoff Area=306,549 sf Flow Length=1,525' Tc=45.4	[*] 22.64% Impervious Runoff Depth>3.09" 9 min CN=77 Runoff=11.76 cfs 1.810 af
	⁻ 85.05% Impervious Runoff Depth>4.88" 5 min CN=94 Runoff=24.45 cfs 2.004 af
SubcatchmentPOST 2.0: WATERSHED 2.0 Runoff Area=49,290 sf Flow Length=758' Tc=5	^s 80.99% Impervious Runoff Depth>4.77" 5.0 min CN=93 Runoff=5.94 cfs 0.449 af
Reach REACH 1.0: RESTORED Avg. Flow Depth=0.81' Ma n=0.040 L=1,309.0' S=0.0092 '/' Capacity	ax Vel=2.20 fps Inflow=10.81 cfs 1.367 af y=2,720.29 cfs Outflow=6.07 cfs 1.355 af
Pond POND 1.0: GRAVEL WETLAND1Peak Elev=46.94' StoPrimary=7.09 cfs2.106 afSecondary=11.63	orage=86,832 cf Inflow=44.88 cfs 4.017 af 8 cfs 0.435 af Outflow=18.72 cfs 2.541 af
Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=55.08' Sto	orage=57,197 cf Inflow=22.02 cfs 1.858 af Outflow=1.76 cfs 0.550 af
	eak Elev=50.65' Inflow=10.81 cfs 1.367 af ' S=0.0050 '/' Outflow=10.81 cfs 1.367 af
Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.86' Sto Primary=39.92 cfs 6.819 af Secondary=0.00	orage=14,364 cf Inflow=40.12 cfs 7.107 af) cfs 0.000 af Outflow=39.92 cfs 6.819 af
Pond POND 1.4: RAINGARDEN1.0Peak Elev=48.07' StoPrimary=6.60 cfs1.401 afSecondary=0.0	orage=45,635 cf Inflow=24.45 cfs 2.004 af 00 cfs 0.000 af Outflow=6.60 cfs 1.401 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=1.76 cfs 0.550 af Primary=1.76 cfs 0.550 af
Link PA1: POINT OF ANALYSIS	Inflow=39.92 cfs 6.819 af Primary=39.92 cfs 6.819 af
Link PA2: POINT OF ANALYSIS	Inflow=5.94 cfs 0.449 af Primary=5.94 cfs 0.449 af

Total Runoff Area = 31.609 acRunoff Volume = 10.955 afAverage Runoff Depth = 4.16"39.63% Pervious = 12.527 ac60.37% Impervious = 19.083 ac

Summary for Subcatchment POST 1.0: WATERSHED 1.0

Runoff = 44.88 cfs @ 12.15 hrs, Volume= 4.017 af, Depth> 4.54"

Α	rea (sf)	CN D	escription		
1 4 4	5,235 22,410 19,146 57,967 90,117 14,873 31,357 16,138 5,356 62,599 28,665 33,934	98 R 61 > 98 P 98 R 74 > 98 P 98 R 80 > 98 P 91 W 2	oofs, HSG 75% Gras aved park oofs, HSG 75% Gras aved park oofs, HSG 75% Gras aved park veighted A 7.81% Per	B B s cover, Gc G C s cover, Gc ing, HSG C D s cover, Gc ing, HSG D	ood, HSG C Cood, HSG D
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	70	0.0150	0.15		Sheet Flow,
0.2	32	0.0200	2.87		Grass: Short n= 0.150 P2= 3.68" Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.1	19	0.0200	2.12		Shallow Concentrated Flow,
0.8	162	0.0050	3.21	2.52	12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
0.4	84	0.0050	3.21	2.52	n= 0.013 Corrugated PE, smooth interior Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013
0.5	113	0.0050	3.72	4.57	Pipe Channel, 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
1.2	299	0.0050	4.20	7.43	n= 0.013 Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
0.4	94	0.0050	4.20	7.43	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
0.1	46	0.0240	11.16	35.05	n= 0.013 Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
0.0	5	0.0800	7.16	0.98	n= 0.013 Pipe Channel, 5.0" Round Area= 0.1 sf Perim= 1.3' r= 0.10'
0.0	9	0.0110	9.90	69.95	n= 0.013 Pipe Channel,

36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'

11.4 933 Total

Summary for Subcatchment POST 1.1: WATERSHED 1.1

n= 0.013

Runoff = 22.02 cfs @ 12.14 hrs, Volume= 1.858 af, Depth> 4.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN E	Description						
	13,692	98 F	98 Roofs, HSG B						
	32,710	61 >	,						
	2,729	98 F	aved park	ing, HSG B					
	88,019	98 F	Roofs, HSC	Э Č					
	67,375	74 >	75% Gras	s cover, Go	bod, HSG C				
	37,971	98 F	aved park	ing, HSG C					
2	42,496	86 V	Veighted A	verage					
1	00,085		•	vious Area					
1	42,411	5	8.73% Imp	pervious Ar	ea				
			•						
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·				
7.1	100	0.0380	0.24		Sheet Flow,				
					Grass: Short n= 0.150 P2= 3.68"				
1.2	163	0.0245	2.35		Shallow Concentrated Flow,				
					Grassed Waterway Kv= 15.0 fps				
1.5	283	0.0050	3.21	2.52	Pipe Channel,				
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
					n= 0.013				
0.1	81	0.0240	9.21	16.27	Pipe Channel,				
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'				
					n= 0.013				
0.4	123	0.0050	5.09	16.00	Pipe Channel,				
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'				
					n= 0.013				
10.3	750	Total							

Summary for Subcatchment POST 1.2: WATERSHED 1.2

Runoff = 10.81 cfs @ 12.09 hrs, Volume= 0.817 af, Depth> 4.22"

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 Type III 24-hr
 10 Year Rainfall=5.58"

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	А	rea (sf)	CN D	escription						
	6,874 61 >75% Grass cover, Good, HSG B									
		4,785								
		31,436	74 >	75% Gras	s cover, Go	bod, HSG C				
_		58,109	98 P	aved park	ing, HSG C)				
	1	01,204	88 V	Veighted A	verage					
		38,310	3	7.85% Per	vious Area					
		62,894	6	2.15% Imp	pervious Ar	ea				
	Тс	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	1.5	100	0.0100	1.12		Sheet Flow,				
						Smooth surfaces n= 0.011 P2= 3.68"				
	1.0	153	0.0150	2.49		Shallow Concentrated Flow,				
				a (=	• - •	Paved Kv= 20.3 fps				
	1.6	343	0.0050	3.47	2.73					
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
	0.4	40	0 0050	0.70	4 53	n= 0.012 Concrete pipe, finished				
	0.1	13	0.0050	3.72	4.57					
						15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'				
	4.0	450	0.0050	4 00	7.40	n= 0.013 Corrugated PE, smooth interior				
	1.8	453	0.0050	4.20	7.43					
						18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'				
	0.4	400	0 0050	F 04	00.00	n= 0.013 Corrugated PE, smooth interior				
	0.4	129	0.0050	5.91	29.00					
						30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63'				
_	0.4	4 404	T . 4 . 1			n= 0.013 Corrugated PE, smooth interior				
	64	1 1 9 1	Total							

6.4 1,191 Total

Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 11.76 cfs @ 12.63 hrs, Volume= 1.810 af, Depth> 3.09"

Area (sf)	CN	Description
11,450	61	>75% Grass cover, Good, HSG B
14,068	58	Meadow, non-grazed, HSG B
908	98	Paved parking, HSG B
70,956	74	>75% Grass cover, Good, HSG C
136,905	71	Meadow, non-grazed, HSG C
2,120	76	Woods/grass comb., Fair, HSG C
68,005	98	Paved parking, HSG C
1,638	80	>75% Grass cover, Good, HSG D
499	98	Paved parking, HSG D
306,549	77	Weighted Average
237,137		77.36% Pervious Area
69,412		22.64% Impervious Area

L-0700-26 POST Prepared by Tighe & Bond

 Type III 24-hr
 10 Year Rainfall=5.58"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.9	100	0.0130	0.15		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.68"
	1.1	52	0.0130	0.80		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.1	27	0.2720	7.82		Shallow Concentrated Flow,
						Grassed Waterway Kv= 15.0 fps
	33.8	1,346	0.0090	0.66		Shallow Concentrated Flow,
_						Short Grass Pasture Kv= 7.0 fps

45.9 1,525 Total

Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff = 24.45 cfs @ 12.10 hrs, Volume= 2.004 af, Depth> 4.88"

A	rea (sf)	CN D	escription						
	11,051	98 R	loofs, HSG						
	3,902								
	7,241								
	86,748		loofs, HSC						
	26,995				ood, HSG C				
	32,822			ing, HSG C					
	44,300		loofs, HSC						
	1,206				ood, HSG D				
	499			ing, HSG D					
	14,764		Veighted A						
	32,103			rvious Area					
1	82,661	8	5.05% Imp	pervious Ar	ea				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Description				
4.9	40	0.0150	0.14	(010)	Sheet Flow,				
т.5	40	0.0100	0.14		Grass: Short n= 0.150 P2= 3.68"				
0.3	53	0.0200	2.87		Shallow Concentrated Flow,				
0.0		0.0200	2.01		Paved Kv= 20.3 fps				
0.3	65	0.0050	3.21	2.52					
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
					n= 0.013 Corrugated PE, smooth interior				
0.4	115	0.0100	4.54	3.56	Pipe Channel,				
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
					n= 0.013				
0.7	140	0.0050	3.21	2.52	Pipe Channel,				
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
• -	 -		–		n= 0.013				
0.9	275	0.0070	4.97	8.79	Pipe Channel,				
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'				
					n= 0.013				

Prepare		he & Bor		17 HydroCAl	Type III 24-hr 10 Year Rainfall=5.58"Printed 6/6/2023D Software Solutions LLCPage 10			
0.0	29	0.0550	13.94	24.63	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013			
7.5	717	Total						
Summary for Subcatchment POST 2.0: WATERSHED 2.0								
[49] Hint	: Tc<2dt	may requ	ire smaller	r dt				
Runoff	=	5.94 cfs	s @ 12.0 [°]	7 hrs, Volu	me= 0.449 af, Depth> 4.77"			
			nod, UH=S nfall=5.58'		nted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs			
A	rea (sf)	CN D	escription					
	22,995		oofs, HSC					
	9,368 16,927			ing, HSG C	ood, HSG C			
	49,290		/eighted A					
	9,368 39,922			rvious Area pervious Ar				
۲ c (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
1.2	100	0.0164	1.36		Sheet Flow,			
0.3	48	0.0164	2.60		Smooth surfaces n= 0.011 P2= 3.68" Shallow Concentrated Flow,			
0.0	40	0.0104	2.00		Paved Kv= 20.3 fps			
0.3	130	0.0140	7.03	12.43	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'			
					n= 0.013			
0.5	70	0.0250	2.37		Shallow Concentrated Flow,			
1.3	410	0.0050	5.09	16.00	Grassed Waterway Kv= 15.0 fps Pipe Channel ,			
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013			
3.6	758	Total, Iı	ncreased t	o minimum	Tc = 5.0 min			

Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

Inflow Are	a =	7.890 ac, 59.73% Impervious, Inflow Depth > 2.08" for 10 Year event
Inflow	=	10.81 cfs @ 12.09 hrs, Volume=
Outflow	=	6.07 cfs @ 12.81 hrs, Volume= 1.355 af, Atten= 44%, Lag= 42.9 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Max. Velocity= 2.20 fps, Min. Travel Time= 9.9 min Avg. Velocity = 1.04 fps, Avg. Travel Time= 21.0 min

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Peak Storage= 6,364 cf @ 12.27 hrs Average Depth at Peak Storage= 0.81' Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs

Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals) Constant n= 0.040 Winding stream, pools & shoals Inlet Invert= 48.00', Outlet Invert= 36.00'

‡

6.75

	Offset	Elevat	ion	Cha	n.Depth		
	(feet)	(fe	et)		(feet)		
	0.00	12	.00		0.00		
	18.00	6	.00		6.00		
	30.25	6	.00		6.00		
	31.75	5	.25		6.75		
	34.25	5	.25		6.75		
	35.75	6	.00		6.00		
	48.00	6	.00		6.00		
	66.00	12	.00		0.00		
Dep	oth En	d Area	Pe	erim.		Storage	Discharge
(fee	et)	(sq-ft)	(f	eet)	(cu	bic-feet)	(cfs)
0.	00	0.0		2.5		0	0.00
0.	75	3.0		30.4		3,927	2.28

68.3

Summary for Pond POND 1.0: GRAVEL WETLAND 1

2.720.29

[95] Warning: Outlet Device #4 rise exceeded

291.0

Inflow Area =	10.620 ac, 72.19% Impervious, Inflow	Depth > 4.54" for 10 Year event
Inflow =	44.88 cfs @ 12.15 hrs, Volume=	4.017 af
Outflow =	18.72 cfs @ 12.45 hrs, Volume=	2.541 af, Atten= 58%, Lag= 18.0 min
Primary =	7.09 cfs @ 12.45 hrs, Volume=	2.106 af
Secondary =	11.63 cfs $\overline{@}$ 12.45 hrs, Volume=	0.435 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 46.94' @ 12.45 hrs Surf.Area= 21,544 sf Storage= 86,832 cf Flood Elev= 48.00' Surf.Area= 23,557 sf Storage= 110,845 cf

380.919

Plug-Flow detention time= 216.6 min calculated for 2.536 af (63% of inflow) Center-of-Mass det. time= 118.8 min (906.1 - 787.3)

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 Type III 24-hr
 10 Year Rainfall=5.58"

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Volume	Invert	Avail.	Storage	Storage Descrip	tion	
#1	39.05'	110	0,845 cf	Custom Stage I	Data (Prismatic)Liste	ed below (Recalc)
Elevatio	on Su	ırf.Area ∖	Voids	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
39.0)5	9,855	0.0	0	0	
41.3	35	9,855	30.0	6,800	6,800	
42.0	00		45.0	2,883	9,683	
43.0	00		100.0	10,899	20,582	
44.0	00		100.0	13,073	33,654	
45.0	00		100.0	15,547	49,201	
46.0	00		100.0	18,322	67,522	
47.0	00	21,668 1	100.0	20,710	88,232	
48.0	00	23,557 1	100.0	22,613	110,845	
Device	Routing	Inve	ert Outl	et Devices		
#1	Primary	41.3	35' 18.0	" Round Culver	t	
	,				e edge headwall, Ke	= 0.500
					1.35' / 41.20' S= 0.0	
			n= 0	0.013 Corrugated	PE, smooth interior,	Flow Area= 1.77 sf
#2	Device 1	41.3		Vert. Orifice/Gra		
#3	Device 1	45.0	00' 3.0''	Vert. Orifice/Gra	ate C= 0.600	
#4	Device 1	46.0	00' 3.0'	long x 0.50' rise	Sharp-Crested Rec	tangular Weir
					4.0' Crest Height	0
#5	Device 1	47.0			fice/Grate X 106.00	C= 0.600
				ted to weir flow at		
#6	Secondary	46.5				d Rectangular Weir
	J				0.60 0.80 1.00 1.	
					2.70 2.70 2.64 2.63	
				(0)		
1=Cu	Primary OutFlow Max=7.09 cfs @ 12.45 hrs HW=46.93' TW=38.85' (Dynamic Tailwater) └─1=Culvert (Passes 7.09 cfs of 18.71 cfs potential flow)					
				0.75 cfs @ 11.23		
				0.32 cfs @ 6.48		
					ols 6.02 cfs @ 4.15	fps)
└── 5=	Orifice/Grat	te (Contro	ols 0.00 d	ofs)		
Secondary OutFlow Max=11.59 cfs @ 12.45 hrs HW=46.93' TW=38.85' (Dynamic Tailwater)						

Secondary OutFlow Max=11.59 cfs @ 12.45 hrs HW=46.93' TW=38.85' (Dynamic Tailwater) G=Broad-Crested Rectangular Weir (Weir Controls 11.59 cfs @ 1.78 fps)

Summary for Pond POND 1.1: GRAVEL WETLAND 2

Inflow Area =	=	5.567 ac, 58.73% Impervious, Inflow Depth > 4.01" for 10 Year event	
Inflow =	:	22.02 cfs @ 12.14 hrs, Volume= 1.858 af	
Outflow =	:	1.76 cfs @ 13.65 hrs, Volume= 0.550 af, Atten= 92%, Lag= 90.5 min	
Primary =	:	1.76 cfs @ 13.65 hrs, Volume= 0.550 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 55.08' @ 13.65 hrs Surf.Area= 16,909 sf Storage= 57,197 cf Flood Elev= 57.00' Surf.Area= 21,643 sf Storage= 94,743 cf

L-0700-26 POST

 Type III 24-hr
 10 Year Rainfall=5.58"

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Plug-Flow detention time= 357.2 min calculated for 0.550 af (30% of inflow) Center-of-Mass det. time= 218.3 min (1,021.7 - 803.4)

Volume	Inv	ert Avai	il.Storage	Storage Descrip	otion	
#1	47.	55' 1	17,304 cf	Custom Stage	Data (Prismatic)	Listed below (Recalc)
Elevatio		Surf.Area	Voids	Inc.Store	Cum.Store	
(fee		(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
47.5		6,269	0.0	0	0	
49.8		6,269	30.0	4,326	4,326	
50.5		6,269	45.0	1,834	6,159	
51.0		7,199	100.0	3,367	9,526	
52.0		9,187	100.0	8,193	17,719	
53.0		11,345	100.0	10,266	27,985	
54.0		13,814	100.0	12,580	40,565	
55.0		16,645	100.0	15,230	55,794	
56.0		19,805		18,225	74,019	
58.0	00	23,480	100.0	43,285	117,304	
Device	Routing	In	vert Out	let Devices		
#1	Primary	49	.85' 24.0	" Round Culver	rt	
	,		L= ^	2.0' CPP, squar	re edge headwall,	Ke= 0.500
						= 0.0333 '/' Cc= 0.900
			n= (0.013 Corrugated	IPE, smooth inter	ior, Flow Area= 3.14 sf
#2	Device 2	1 49		' Vert. Orifice/Gr		
#3	Device '	1 53	3.50' 4.0'	long x 2.00' rise	Sharp-Crested I	Rectangular Weir
				nd Contraction(s)	•	5
#4	Device 2	1 56			ifice/Grate X 106	6.00 C= 0.600
			Lim	ited to weir flow a	t low heads	
Primary	OutFlow	v Max=1.76	cfs @ 13.	65 hrs HW=55.0	8' TW=55.07' (C)ynamic Tailwater)
		et Controls			(,
				cfs potential flow)		
					33 cfs potential flo	ow)
		Grate (Con			•	,
		,		,		
Summary for Pond POND 1.2: PDMH203						
Inflow A	roo -	7 000	EO 720/	moonulaus	u Dopth > $2.00"$	for 10 Voor overt
Inflow A					w Depth > 2.08"	for 10 Year event
	=			nrs, Volume=	1.367 af	con=0% log=0.0 min
Outflow	=			nrs, Volume=		ten= 0%, Lag= 0.0 min
Primary	=		u 12.091	nrs, Volume=	1.367 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 50.65' @ 12.09 hrs Flood Elev= 57.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.35'	48.0" Round Culvert L= 269.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 49.35' / 48.00' S= 0.0050 '/' Cc= 0.900

n= 0.013 Corrugated PE, smooth interior, Flow Area= 12.57 sf

Primary OutFlow Max=10.64 cfs @ 12.09 hrs HW=50.64' TW=48.75' (Dynamic Tailwater) **1=Culvert** (Inlet Controls 10.64 cfs @ 3.05 fps)

Summary for Pond POND 1.3: OUTLET CULVERTS

[62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.50' @ 23.95 hrs

Inflow Area =	30.478 ac, 59.60% l	mpervious, Inflow E	Depth > 2.80"	for 10 Year event
Inflow =	40.12 cfs @ 12.47 h	nrs, Volume=	7.107 af	
Outflow =	39.92 cfs @ 12.50 h	nrs, Volume=	6.819 af, Atte	n= 0%, Lag= 1.8 min
Primary =	39.92 cfs @ 12.50 h	nrs, Volume=	6.819 af	-
Secondary =	0.00 cfs @ 0.00 h	nrs, Volume=	0.000 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 38.86' @ 12.50 hrs Surf.Area= 9,266 sf Storage= 14,364 cf Flood Elev= 43.50' Surf.Area= 95,977 sf Storage= 236,017 cf

Plug-Flow detention time= 32.3 min calculated for 6.819 af (96% of inflow) Center-of-Mass det. time= 11.6 min (905.1 - 893.5)

Volume	Inver	t Avail.Sto	rage Storage	e Description
#1	35.00	o' 236,0°	17 cf Custom	m Stage Data (Prismatic)Listed below (Recalc)
Elevatio		Surf.Area	Inc.Store	Cum.Store
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)
35.0	00	960	0	0
36.0	00	1,428	1,194	1,194
38.0	00	5,418	6,846	8,040
40.0	00	14,354	19,772	27,812
42.0	00	66,884	81,238	109,050
43.0	00	92,707	79,796	188,846
43.5	50	95,977	47,171	236,017
Device	Routing	Invert	Outlet Device	es
#1	Primary	35.60'	42.0" W x 29.	9.0" H, R=21.5"/66.1" Pipe Arch CMP_Arch_1/2 42x29 X 3.00
			L= 68.0' CM	MP, square edge headwall, Ke= 0.500
			Inlet / Outlet I	Invert= 35.60' / 35.30' S= 0.0044 '/' Cc= 0.900
			n= 0.025 Cor	prrugated metal, Flow Area= 6.72 sf
#2	Secondar	y 43.00'		18.0' long x 0.50' rise Sharp-Crested Vee/Trap Weir
		,	Cv= 2.47 (C=	
				/

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=35.00' TW=38.65' (Dynamic Tailwater) 2=Sharp-Crested Vee/Trap Weir (Controls 0.00 cfs)

Summary for Pond POND 1.4: RAINGARDEN 1.0

Inflow Area =	4.930 ac, 85.05% Impervious, Inflow	Depth > 4.88" for 10 Year event
Inflow =	24.45 cfs @ 12.10 hrs, Volume=	2.004 af
Outflow =	6.60 cfs @ 12.48 hrs, Volume=	1.401 af, Atten= 73%, Lag= 22.2 min
Primary =	6.60 cfs @ 12.48 hrs, Volume=	1.401 af
Secondary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 48.07' @ 12.48 hrs Surf.Area= 14,774 sf Storage= 45,635 cf Flood Elev= 50.00' Surf.Area= 17,790 sf Storage= 77,050 cf

Plug-Flow detention time= 233.7 min calculated for 1.398 af (70% of inflow) Center-of-Mass det. time= 143.1 min (914.3 - 771.2)

0
sf
r
30 2.00
2.64
iı 8

Primary OutFlow Max=6.59 cfs @ 12.48 hrs HW=48.07' TW=38.86' (Dynamic Tailwater) -1=Culvert (Passes 6.59 cfs of 6.77 cfs potential flow)

-2=Orifice/Grate (Passes 1.01 cfs of 2.20 cfs potential flow) -3=Exfiltration (Exfiltration Controls 1.01 cfs)

-4=Orifice/Grate (Orifice Controls 5.58 cfs @ 4.62 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=42.17' TW=35.00' (Dynamic Tailwater) **5=Broad-Crested Rectangular Weir**(Controls 0.00 cfs)

Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.1 by 7.52' @ 0.00 hrs (23.95 cfs 25.099 af)

Inflow Area =	:	5.567 ac, 5	58.73% Imp	ervious,	Inflow Deptl	h > 1.19"	for 10 Year event
Inflow =		1.76 cfs @	13.65 hrs,	Volume	= 0.	550 af	
Primary =		1.76 cfs @	13.65 hrs,	Volume	= 0.5	550 af, At	ten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 25	Point manual	elevation	table, To=	0.00 hrs,	dt= 1.00 hrs,	feet =		
55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07
55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07	55.07
55.07	55.07	55.07	55.07	55.07	55.07	55.07		

Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.3 by 3.65' @ 0.00 hrs (92.51 cfs 86.028 af)

Inflow Area	a =	30.478 ac, 59	9.60% Impe	ervious,	Inflow De	epth >	2.69"	for 10	Year event
Inflow	=	39.92 cfs @	12.50 hrs,	Volume	=	6.819 a	af		
Primary	=	39.92 cfs @	12.50 hrs,	Volume	=	6.819 a	af, At	ten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 2 Point manual elevation table, To= 0.00 hrs, dt= 24.00 hrs, feet = 38.65 38.65

Summary for Link PA2: POINT OF ANALYSIS

Inflow Area =	1.132 ac, 80.99% Impervious, Inflow E	Depth > 4.77" for 10 Year event
Inflow =	5.94 cfs @ 12.07 hrs, Volume=	0.449 af
Primary =	5.94 cfs @ 12.07 hrs, Volume=	0.449 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

L-0700-26 POST Prepared by Tighe & Bond HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solution	Type III 24-hr 25 Year Rainfall=7.07" Printed 6/6/2023 ns LLC Page 17
Time span=0.00-24.00 hrs, dt=0.05 h Runoff by SCS TR-20 method, UH=SCS Reach routing by Dyn-Stor-Ind method - Pond rout	S, Weighted-CN
SubcatchmentPOST 1.0: WATERSHED Runoff Area=462,599 s Flow Length=933' Tc=11	sf 72.19% Impervious Runoff Depth>6.00" I.4 min CN=91 Runoff=58.40 cfs 5.309 af
	sf 58.73% Impervious Runoff Depth>5.43").3 min CN=86 Runoff=29.42 cfs 2.517 af
	sf 62.15% Impervious Runoff Depth>5.66" 6.4 min CN=88 Runoff=14.27 cfs 1.095 af
	sf 22.64% Impervious Runoff Depth>4.39" 5.9 min CN=77 Runoff=16.72 cfs 2.574 af
	sf 85.05% Impervious Runoff Depth>6.35" 7.5 min CN=94 Runoff=31.40 cfs 2.610 af
SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,290 s Flow Length=758' Tc=	sf 80.99% Impervious Runoff Depth>6.24" =5.0 min CN=93 Runoff=7.66 cfs 0.588 af
	Max Vel=2.20 fps Inflow=14.27 cfs 2.076 af http=2,720.29 cfs Outflow=7.67 cfs 2.061 af
Pond POND 1.0: GRAVEL WETLAND1 Peak Elev=47.21' St Primary=19.23 cfs 2.787 af Secondary=24.1	orage=92,932 cf Inflow=58.40 cfs 5.309 af 6 cfs 0.988 af Outflow=43.41 cfs 3.776 af
Pond POND 1.1: GRAVEL WETLAND2 Peak Elev=55.71' St	orage=68,356 cf Inflow=29.42 cfs 2.517 af Outflow=4.20 cfs 0.981 af
	Peak Elev=50.86' Inflow=14.27 cfs 2.076 af 0' S=0.0050 '/' Outflow=14.27 cfs 2.076 af
Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.33' Sto Primary=66.14 cfs 10.071 af Secondary=0.00	rage=19,198 cf Inflow=67.56 cfs 10.378 af) cfs 0.000 af Outflow=66.14 cfs 10.071 af
	torage=58,248 cf Inflow=31.40 cfs 2.610 af .00 cfs 0.000 af Outflow=7.29 cfs 1.966 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=4.20 cfs 0.981 af Primary=4.20 cfs 0.981 af
Link PA1: POINT OF ANALYSIS	Inflow=66.14 cfs 10.071 af Primary=66.14 cfs 10.071 af
Link PA2: POINT OF ANALYSIS	Inflow=7.66 cfs 0.588 af Primary=7.66 cfs 0.588 af

Total Runoff Area = 31.609 acRunoff Volume = 14.693 afAverage Runoff Depth = 5.58"39.63% Pervious = 12.527 ac60.37% Impervious = 19.083 ac

L-0700-26 POST Prepared by Tighe & Bond HydroCAD® 10.00-20 s/n 03436 © 2017 HydroCAD Software Solutio	Type III 24-hr 50 Year Rainfall=8.46" Printed 6/6/2023 ons LLC Page 18
Time span=0.00-24.00 hrs, dt=0.05 h Runoff by SCS TR-20 method, UH=SC Reach routing by Dyn-Stor-Ind method - Pond rou	S, Weighted-CN
	sf 72.19% Impervious Runoff Depth>7.37" 1.4 min CN=91 Runoff=70.91 cfs 6.521 af
	sf 58.73% Impervious Runoff Depth>6.77" 0.3 min CN=86 Runoff=36.28 cfs 3.140 af
	sf 62.15% Impervious Runoff Depth>7.01" 6.4 min CN=88 Runoff=17.48 cfs 1.358 af
	sf 22.64% Impervious Runoff Depth>5.65" 5.9 min CN=77 Runoff=21.42 cfs 3.313 af
	sf 85.05% Impervious Runoff Depth>7.73" 7.5 min CN=94 Runoff=37.84 cfs 3.177 af
SubcatchmentPOST 2.0: WATERSHED2.0 Runoff Area=49,290 Flow Length=758' Tc	sf 80.99% Impervious Runoff Depth>7.62" =5.0 min CN=93 Runoff=9.25 cfs 0.718 af
	Max Vel=2.19 fps Inflow=17.48 cfs 2.679 af ty=2,720.29 cfs Outflow=10.33 cfs 2.662 af
Pond POND 1.0: GRAVEL WETLAND1Peak Elev=47.48' SPrimary=19.73 cfs3.345 afSecondary=38.7	torage=98,793 cf Inflow=70.91 cfs 6.521 af 14 cfs 1.616 af Outflow=57.87 cfs 4.961 af
Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=56.45' S	torage=83,107 cf Inflow=36.28 cfs 3.140 af Outflow=6.58 cfs 1.321 af
	Peak Elev=51.03' Inflow=17.48 cfs 2.679 af .0' S=0.0050 '/' Outflow=17.48 cfs 2.679 af
Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.77' Sto Primary=83.35 cfs 13.109 af Secondary=0.00	orage=24,643 cf Inflow=87.04 cfs 13.437 af 0 cfs 0.000 af Outflow=83.35 cfs 13.109 af
	torage=69,290 cf Inflow=37.84 cfs 3.177 af .60 cfs 0.039 af Outflow=9.29 cfs 2.500 af
Link LINK 1.0: PDMH203 TAILWATER	Inflow=6.58 cfs 1.321 af Primary=6.58 cfs 1.321 af
Link PA1: POINT OF ANALYSIS	Inflow=83.35 cfs 13.109 af Primary=83.35 cfs 13.109 af
Link PA2: POINT OF ANALYSIS	Inflow=9.25 cfs 0.718 af Primary=9.25 cfs 0.718 af
Total Dunoff Area = 21 600 as Dunoff Valuma	- 49 997 of Average Duraff Dauth - 6 00

Total Runoff Area = 31.609 acRunoff Volume = 18.227 afAverage Runoff Depth = 6.92"39.63% Pervious = 12.527 ac60.37% Impervious = 19.083 ac



Proposed Solar Project

Portsmouth International Airport

Portsmouth, NH Glare Study Results

Photovoltaic (Solar) Project in Portsmouth, Rockingham County, NH

February 22, 2024

Prepared for:

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Appendix



Conclusion

Collier's Engineering & Design (CED) performed an analysis on the array areas of the proposed rooftop and carport solar project site in Portsmouth, Rockingham County, NH.

Through extensive cross-checking, it was found that at a 5-degree resting angle or above for the rooftop system panels, there is no predicted glare throughout the entire project area. Small amounts of green glare predicted from the carports onto a route directly next to the proposed project are easily mitigated.

The study area is presented in the graphic below. Red Markers represent Observation Points, Turquoise Lines are the roads in and around the proposed project area, and Brown Lines represent the existing foliage in the area and/or the proposed landscaping lines. The Brown Lines around the rooftop systems represent the parapets that run the entire perimeter of the buildings.



A closer view of the immediate project area:





The triangulation of the proposed project in relation to Portsmouth International Airport is provided below. Because of the proximity to the airport and the Air Traffic Control Tower, the client specifically requested a full study to be certain that no glare of any kind would affect the Tower.



To establish a <u>worst-case scenario</u> baseline, a 15-degree angle for the proposed rooftop system facing 214 degrees (azimuth) was programmed on the rooftops of two buildings. For the proposed carports, four array areas were programmed facing 124 degrees (azimuth) and one carport was programmed facing 214 degrees (azimuth). The project was modeled <u>without</u> local foliage lines and other large buildings between the proposed project and the ATCT in the area programmed.



The Air Traffic Control Tower was modeled at a dual height of 130 feet and 120 feet to cover broader possibilities of the proposed project's sightline to anyone in the tower structure.



With the above settings, the modelling predicts ZERO minutes of YELLOW glare over the course of an entire year and ~4,474 minutes of GREEN glare over the course of an entire year. The glare results include ~1,863 minutes of GREEN glare on the Air Traffic Control Tower at Portsmouth International Airport from Carports 1, 3 and 4. **No glare whatsoever is predicted from the rooftop systems onto the ATCT or onto any other point in the study.**

At the proposed working settings of a 5-degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

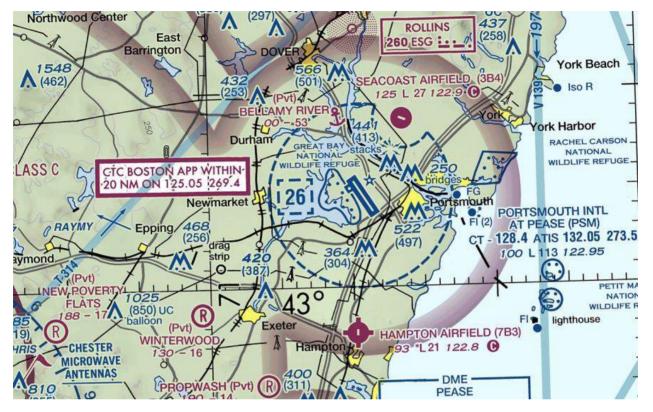
At the proposed working settings of a 10-degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

At the proposed working settings of a 13-degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

At the proposed working settings of a 15-degree racking tilt on the rooftop systems, and the same settings for the carports components, but WITH all local area foliage, buildings and other obstructions, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.



A review of the Federal Aviation Administration's (FAA) New York area Visual Flight Rules (VFR) charts shows no restricted airspace in or around the proposed project area.



A review of Military Training Route (MTR) charts was performed utilizing an additional online resource and the proposed project falls entirely **OUTSIDE** of known training route areas.





The above conclusion is arrived at by utilizing the worst-case scenario results provided by the *ForgeSolar* software, and then manually layering back into each modeling scenario all real-world factors in the area of the proposed site location.

Full technical reporting output by the *ForgeSolar* program is included in the Appendix of this report.

Sincerely,

Colliers Engineering & Design, Inc. (DBA Maser Consulting)

Elizabeth Claire Myers, PMP Project Manager, Electrical Engineering Certified Glare Analyst through Sims Industries

cc: Lee Hill, PE, Colliers Engineering & Design (via email)

R:\Projects\2024\24000681A_IPS_Portsmouth\24000681A_IPS_PortsmouthNH_GlareStudy_DRAFTREPORT.docx



Resources

Federal Aviation Administration – Publicly Available Visual Flight Rules (VFR) Charts <u>https://www.faa.gov/air_traffic/flight_info/aeronav/digital_products/vfr/</u>

• Utilized to obtain FAA-approved VFR charts of the project area for inclusion and consideration in this study.

U.S. Military Training Routes (MTRs) and buffers - May 4, 2018 (Last modified Oct 6, 2021) Uploaded by South Atlantic Blueprint <u>https://salcc.databasin.org/datasets/4c81852be18444b997f8f860ee568c54/</u>

• Utilized to obtain detail and graphic of US-wide Military Training Routes and location specific data for this study.

Ho, C. K., Ghanbari, C. M., and Diver, R. B., 2011, **Methodology to Assess Potential Glint and Glare Hazards From Concentrating Solar Power Plants: Analytical Models and Experimental Validation**, *ASME J. Sol. Energy Eng.*, *133*.

Solar Glare Hazard Analysis Tool (SGHAT) Technical Reference Manual



Details of Glare Study Methodology

(Source Information: https://forgesolar.com/help/#intro)

Collier's Engineering & Design (CED) offers staff specifically trained on glare analyses utilizing *ForgeSolar*, a web-based interactive software that provides a quantified assessment of (1) when and where glare is predicted to occur throughout the year for a prescribed solar installation, and (2) potential effects on the human eye at locations where glare is predicted to occur. *ForgeSolar* is based on the Solar Glare Hazard Analysis Tool ("SGHAT") licensed from Sandia National Laboratories.

These tools meet the FAA standards for glare analysis.

Determination of glare occurrence requires knowledge of the following: sun position, observer location, and the tilt, orientation, location, extent, and optical properties of the modules in the solar array. Vector algebra is then used to determine if glare is likely to be visible from the prescribed observation points.

If glare is predicted, the software calculates the retinal irradiance and subtended angle (size/distance) of the glare source to predict potential ocular hazards ranging from temporary afterimage to more severe possible retinal damage. These results are presented in a simple, easy-tointerpret plot that specifies when glare is predicted to occur throughout the year, with color codes indicating the potential ocular hazard.



Background Information

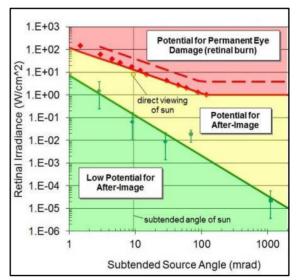
Glint is typically defined as a momentary flash of bright light, often caused by a reflection off a moving source. A typical example of glint is a momentary solar reflection from a moving car, or "catching" something bright out of the corner of your eye.

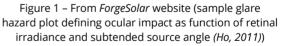
Glare is defined as a continuous source of bright light. Glare is generally associated with stationary objects, which, due to the slow relative movement of the sun, reflect sunlight for a longer duration.

The difference between glint and glare is duration. Industry-standard glare analysis tools evaluate the occurrence of glare on a minute-by-minute basis; accordingly, they generally refer to solar hazards as 'glare.'

The ocular impact of solar glare is quantified into three categories (Ho, 2011):

- 1. Green Unproblematic shine. Low potential to cause after-image. This type of glare can be compared to noticing something shiny in the distance.
- 2. Yellow Potential to cause temporary afterimage (flash blindness). This type of glare is much like sunrise and sunset glare for drivers who struggle to find the perfect angle for car visors so they can continue to operate their vehicle safely while traveling through areas of such glare.
 - Standard levels of yellow glare can, for the most part, be handled with relative ease utilizing slatted fencing or localfoliage landscape mitigation measures.
 - b. Only extremely high levels of this type of glare (in the area of the chart to the right labeled as "direct viewing of the sun" which is uncommon to find with PV installations) would be considered an insurmountable hurdle to a PV installation of any size.
 - c. High levels/intensities and long durations are different factors.





- 3. Red Potential to cause retinal burn (permanent eye damage). PV modules do not focus reflected sunlight and therefore retinal burn (RED glare) is typically not possible.
 - d. This is the ONLY type of glare that would be considered an insurmountable hurdle to a PV installation of any size.

These categories assume a typical blink response in the observer.



Note that retinal burn is typically not possible for PV glare since PV modules do not focus reflected sunlight. They are, in fact, designed to absorb as much sunlight as possible.

To further put glare into perspective, the following is presented.

YELLOW glare such as in the graphic to the right could only be seen when standing directly next to project panels at the perfect angle when the sun is in a perfect place—indeed the point of a photographer standing directly by these panels and waiting for the perfect moment to capture this image. It is also possible that the panels in the picture shown do not have an anti-reflective coating.



Solar panel showing solar glare

GREEN glare, as illustrated directly to the right, is the more common occurrence with solar projects—a noticeable shiny area (in the northwest area) as compared to panels where the sun is not quite in perfect alignment yet.

Even so, the effect of this noticeable shine to certain areas of the project area is still seen from a relatively close up vantage point and at the optimal height this image was captured, possibly by a drone. A similarly sized project in the



distance, closer to the horizon of the photo would be unlikely to show even the levels of green glare that the system in the foreground reflects.



Executive Summary

The purpose of the glare study requested by IPS – Integrated Project Service, LLC (IPS) and their client is to closely examine a proposed solar project in Portsmouth, Rockingham County, NH and to provide feedback regarding areas that may warrant closer examination in order to mitigate possible problematic predicted glare to the businesses, residences, and roads surrounding the project area.

Information was provided by IPS and their client in order to complete this study. The project's rooftop PV systems were programmed to a 15-degree tilt axis facing 214 degrees at a height of 88 feet for the smaller structure and 93.83 feet for the larger building. The parapets for these buildings were programmed at heights of 93.21 feet and 99.3 feet respectively.

Four of the projects five carport systems were programmed with two top heights (20.17 feet and 22.48 feet) and a lower edge of 14 feet, facing 124 degrees southeast. A final carport was programmed with a 20.17 foot high edge, a 14 foot lower edge and facing 214 degrees.

It was further assumed that the panels used throughout the proposed project are constructed of Smooth Glass with an Anti-Reflective coating.

Seven (7) Observation Points were placed at different points around the site and programmed to an average height of 5 and a half (5.5) feet to model someone standing in these spots, and to a height of 15 to 20 feet to model a 5.5-foot person standing on the second floor of a home/business with 8-foot ceilings and a 1.5-foot plenum space.





The building directly southwest of the proposed project is industrial in nature, and an examination of the portion that will be facing the project shows that it is industrial in nature with very few windows. One OP was programmed here at a height of 40 feet.

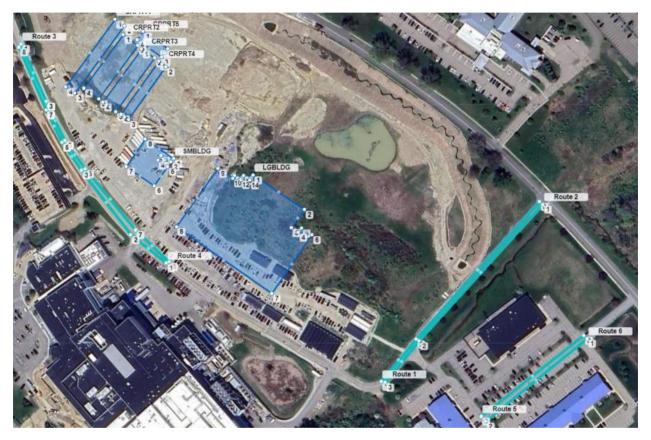






Two Observation Points representing the Air Traffic Control Tower at Portsmouth International Airport were programmed to heights of 130 feet and 120 feet.

Six (6) Route Receptors were programmed for two-way traffic to heights of 4.5 feet and 8.5 feet, effectively representing the eyeline of an average person sitting on/in any vehicle from a bike to a motorcycle, a standard car or SUV, through to the approximated seated height in the cab of an 18-wheeler truck.



While it is impossible to study every possible point and/or angle surrounding a photovoltaic (solar) project, Collier's Engineering & Design (CED) has modeled the project and surrounding areas as best as possible with the most likely points of concern.

PV modules do not focus reflected sunlight and therefore retinal burn is typically not possible. They are, in fact, designed to absorb as much sunlight as possible. Modern photovoltaic panels actually cause less glare than standard home window glass; and research has shown that they reflect less light than snow, white concrete and energy-efficient white rooftops.

The YELLOW glare we are looking to identified with this study is much like sunrise and sunset glare for drivers who struggle to find the perfect angle for car visors so they can continue to operate their vehicle safely while traveling through areas of such glare. In general, photovoltaic panel systems of any size produce some glare predominately during early sunrise and sunset throughout the Spring



through Fall months—although glare is possible throughout each day as well as throughout the entire year.

ForgeSolar now allows the programming of obstructions. It was utilized in this study to model in existing treelines, local warehouses and other buildings and the parapets of the proposed new buildsings for this project with estimated heights. Local foliage lines were modeled at a conservative height of 17 to 30 feet in height. Local warehouses were modeled conservatively at 20 to 30 feet high.



After examining each point and then factoring in additionally recommended foliage, distance, and elevation changes, points where predicted glare is blocked by natural obstructions were removed from the listing of points to be examined more closely. Finally, if any glare continues to be predicted in any area, this analyst will address the areas that present the <u>most</u> possibility for likely glare.

ASSUMPTIONS

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.*
- Glare analyses do not account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographic obstructions.
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Glare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.



Results of this Study

WORST CASE SCENARIO without Local Foliage - RESULTS at 15 Degree Resting Angle

To establish a worst-case scenario baseline, the project was modeled <u>without</u> any local foliage lines or building obstructions between the proposed project and the Air Traffic Control Tower at the Portsmouth International Airport. The modelling predicts ZERO minutes of YELLOW glare over the course of an entire year and ~4,474 minutes of GREEN glare over the course of an entire year. The glare results include ~1,855 minutes of GREEN glare on the Air Traffic Control Tower at Portsmouth International Airport from Carports 1, 3 and 4. No glare whatsoever is predicted from the rooftop systems onto the ATCT or onto any other point in the study.

RESULTS at 5 Degree Angle

At the proposed working settings of a 5-degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

RESULTS at 10 Degree Resting Angle

At the proposed working settings of a 10-degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

RESULTS at 13 Degree Resting Angle

At the proposed working settings of a 13-degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.

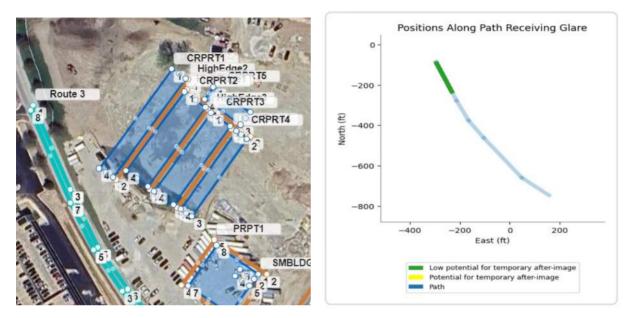
RESULTS at 15 Degree Resting Angle

At the proposed working settings of a 15-degree racking tilt on the rooftop systems, and the same settings for the carports components, the modelling predicts zero minutes of YELLOW glare over the course of an entire year and ~802 minutes of GREEN glare over the course of an entire year. This glare is exclusively from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.



AREAS OF GLARE

In ALL results, the areas of glare from Carport 3 and Carport 4 onto Routes 3 (4.5 feet) and 4 (8.5 feet) which run directly in front of the proposed project area.



A final run scenario with a small planting of trees at the area marked in green in the "Positions Along Path Receiving Glare" shows that a screen of 9 feet at initial planting will completely mitigate any glare shown.

PV Name	Tilt	Orientation	"Green" Glare	
	deg	deg	min	
CRPRT1	0.0	124.0	0	
CRPRT2	0.0	124.0	0	
CRPRT3	0.0	124.0	0	
CRPRT4	0.0	124.0	0	
CRPRT5	0.0	214.0	0	
LGBLDG	10.0	214.0	0	
SMBLDG	10.0	214.0	0	

Summary of Results No glare predicted!





Summary of FAA-Level Flight Path Screening Results

Portsmouth International Airport sits under 1 mile away from the project on the western side. All obstructions were kept in place for the FAA screening and the project was modeled at the 10 degree rooftop PV system tilt.

FEDERAL AVIATION ADMINISTRATION (FAA) SCREENS

An FAA-level glare analysis was performed and a report specific to this request can be found in Appendix A of this report. The Air Traffic Control Tower at Portsmouth International Airport is modeled for this study at its height of 130 feet. Additionally, a second point was modeled at 120 feet to be certain of the glare study results.

Per the FAA's most recent 2021 policy regarding solar around airports, this project PASSES.

Project: ALBACORE, Portsmouth, NH

Site configuration: Albacore_10DegreeTilt_124Carports_ATCT_FAAReport

Created 22 Feb, 2024 Updated 22 Feb, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg DNI peaks at 1,000.0 W/m² Site ID 112738.19298

Ocular transmission coefficient 0.5 Pupil diameter 0.002 m Eye focal length 0.017 m Sun subtended angle 9.3 mrad PV analysis methodology V2



Glare Policy Adherence

The following table estimates the policy adherence of this glare analysis according to the 2021 U.S. Federal Aviation Administration Policy:

Review of Solar Energy System Projects on Federally-Obligated Airports

This policy may require the following criteria be met for solar energy systems on airport property:

- · No glare of any kind for Air Traffic Control Tower(s) ("ATCT") at cab height.
- · Default analysis and observer characteristics, including 1-minute time step.

ForgeSolar is not affiliated with the U.S. FAA and does not represent or speak officially for the U.S. FAA. ForgeSolar cannot approve or deny projects - results are informational only. Contact the relevant airport and FAA district office for information on policy and requirements.

COMPONENT	STATUS	DESCRIPTION
Analysis parameters	PASS	Analysis time interval and eye characteristics used are acceptable
ATCT(s)	PASS	Receptor(s) marked as ATCT do not receive glare

The complete updated FAA Policy can be read at: https://www.federalregister.gov/d/2021-09862

NOTE: ForgeSolar does not represent or speak officially for the FAA and cannot approve or deny projects. Results are informational only.



On May 26, 2021, the Federal Aviation Administration updated their policies regarding the installation of solar on and/or near regulated airports/airstrips.

While this policy of the Federal Aviation Administeration does not apply to solar energy systems on airports that do not have an Air Traffic Control Tower (ATCT), airports that are not federally-obligated, or solar energy systems not located on airport property—it does provide a high benchmark to meet to ensure that proposed solar installations do not create glare that poses any sort of safety hazard for pilots.

The brief of this FAA policy update states:

"The Federal Aviation Administration (FAA) published a final policy aimed at ensuring that airport solar projects don't create hazardous glare. The policy requires airports to measure the visual impact of such projects on pilots and air traffic control personnel.

The policy applies to proposed solar energy systems at federally obligated airports with control towers. Federally obligated airports are public airports that have accepted federal assistance either in the form of grants of property conveyances

As more airports invests in this technology for environmental and economic benefits, the FAA wants to make sure that the reflection from the systems' glass surfaces do not create a glare that poses a safety hazard for pilots and air traffic controllers.

Under the final policy, airports are no longer required to submit the results of an ocular analysis to FAA. Instead, the airport must file a Notice of Proposed Construction or Alteration Form 7460-1 that includes a statement that the project will not cause any visual impact. The airport submits the form to the FAA for review and approval.

The FAA relies on the airport to confirm via the form that it has sufficiently analyzed the potential for glint and glare and determined there is no potential for ocular impact to the airport traffic control tower cab. If any impacts are discovered after construction, the airport must mitigate the impact at its expense. The airport may also face compliance action for failure to address visual impacts that create aviation safety hazards. As such, the agency encourages an airport to conduct sufficient analysis before installing a solar energy system.

The FAA is also withdrawing the recommended tool for measuring the ocular impact of potential glint and glare effects on pilots and air traffic controllers."

Additionally:

"Initially, FAA believed that solar energy systems could introduce a novel glint and glare effect to pilots on final approach. FAA has subsequently concluded that in most cases, the glint and glare from solar energy systems to pilots on final approach is similar to glint and glare pilots routinely experience from water bodies, glass-façade buildings, parking lots, and similar features. However, FAA has continued to receive reports of potential glint and glare from on-airport solar energy systems on personnel working in ATCT cabs. Therefore, FAA has determined the scope of agency policy should be focused on the impact of on-airport solar energy systems to federally-obligated towered airports, specifically the airport's ATCT cab."



Appendix

Appendix A | Detailed Glare Study Result Reports

The following pages are the full reporting results delivered directly from *ForgeSolar*.



FORGESOLAR GLARE ANALYSIS

Project: ALBACORE, Portsmouth, NH

Site configuration: Albacore_10DegreeTilt_124Carports_ATCT_FAAReport

Client: Lonza

Created 22 Feb, 2024 Updated 22 Feb, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg DNI peaks at 1,000.0 W/m² Site ID 112738.19298

Ocular transmission coefficient 0.5 Pupil diameter 0.002 m Eye focal length 0.017 m Sun subtended angle 9.3 mrad PV analysis methodology V2



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- No glare of any kind for Air Traffic Control Tower(s) ("ATCT") at cab height.
- Default analysis and observer characteristics, including 1-minute time step.

ForgeSolar is not affiliated with the U.S. FAA and does not represent or speak officially for the U.S. FAA. ForgeSolar cannot approve or deny projects - results are informational only. Contact the relevant airport and FAA district office for information on policy and requirements.

COMPONENT	STATUS	DESCRIPTION
Analysis parameters	PASS	Analysis time interval and eye characteristics used are acceptable
ATCT(s)	PASS	Receptor(s) marked as ATCT do not receive glare

The referenced policy can be read at https://www.federalregister.gov/d/2021-09862



Component Data

This report includes results for PV arrays and Observation Point ("OP") receptors marked as ATCTs. Components that are not pertinent to the policy, such as routes, flight paths, and vertical surfaces, are excluded.

PV Arrays

Name: CRPRT1 Axis tracking: Fixed (no rotation) Tilt: 0.0° Orientation: 124.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.085650	-70.803723	57.92	20.17	78.09
2	43.085595	-70.803619	57.81	14.00	71.81
3	43.085032	-70.804187	64.54	14.00	78.54
4	43.085084	-70.804291	66.68	20.17	86.85

Name: CRPRT2 Axis tracking: Fixed (no rotation) Tilt: 0.0° Orientation: 124.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.085519	-70.803626	57.88	22.48	80.36
2	43.085431	-70.803461	56.75	14.00	70.75
3	43.084981	-70.803912	58.98	14.00	72.98
4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Axis tracking: Fixed (no rotation) Tilt: 0.0° Orientation: 124.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
43.085400	-70.803418	56.90	22.48	79.38
43.085325	-70.803271	56.23	14.00	70.23
43.084876	-70.803716	58.56	14.00	72.56
43.084953	-70.803866	59.01	22.48	81.49
	43.085400 43.085325 43.084876	43.085400 -70.803418 43.085325 -70.803271 43.084876 -70.803716	43.085400 -70.803418 56.90 43.085325 -70.803271 56.23 43.084876 -70.803716 58.56	43.085400 -70.803418 56.90 22.48 43.085325 -70.803271 56.23 14.00 43.084876 -70.803716 58.56 14.00

Name: CRPRT4

Axis tracking: Fixed (no rotation) Tilt: 0.0° Orientation: 124.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52



Name: CRPRT5 Axis tracking: Fixed (no rotation) Tilt: 0.0° Orientation: 214.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



2 43.085404 -70.803116 55.16 20.17 7	7.02
	5.32
3 43.085334 -70.803188 55.25 14.00 6	9.25
4 43.085478 -70.803470 57.01 14.00 7	1.01

Name: LGBLDG Axis tracking: Fixed (no rotation)

Tilt: 10.0° Orientation: 214.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52



Name: SMBLDG Axis tracking: Fixed (no rotation) Tilt: 10.0° Orientation: 214.0° Rated power: -Panel material: Smooth glass with AR coating Reflectivity: Vary with sun Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	43.084480	-70.803051	56.19	88.00	144.19
2	43.084450	-70.803081	56.31	88.00	144.31
3	43.084506	-70.803193	56.74	88.00	144.74
4	43.084466	-70.803232	56.81	88.00	144.81
5	43.084412	-70.803118	56.55	88.00	144.55
6	43.084252	-70.803275	58.91	88.00	146.91
7	43.084414	-70.803594	61.58	88.00	149.58
8	43.084643	-70.803375	58.79	88.00	146.79

Observation Point ATCT Receptors

Name	ID	Latitude (°)	Longitude (°)	Elevation (ft)	Height (ft)
1-ATCT	1	43.084384	-70.818882	89.93	130.00
6-ATCT	6	43.084349	-70.818856	89.97	120.00

Map image of 1-ATCT



Map image of 6-ATCT





Obstruction Components

Name: BLDG1 Top height: 12.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.084600	-70.810084	76.71
2	43.084703	-70.809846	77.63
3	43.084534	-70.809702	77.38
4	43.084428	-70.809944	77.34
5	43.084600	-70.810084	76.71

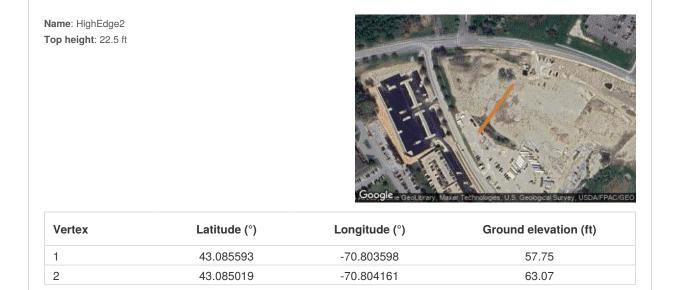
Name: BLDG2 Top height: 20.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.084955	-70.806346	99.52
2	43.085031	-70.806408	98.08
3	43.084866	-70.806801	99.55
4	43.084555	-70.806565	99.98
5	43.084608	-70.806439	99.85
6	43.084444	-70.806325	99.64
7	43.084592	-70.806011	99.08
8	43.084965	-70.806346	99.43



ame: HighEdge1 op height: 22.0 ft			
			N. C. March
Vertex	Latitude (°)	Google _{ie} Gest winy Longitude (°)	Ground elevation (ft)
Vertex	Latitude (°) 43.085534	Coogle :: Geol With W	







Name: HighEdge4 Top height: 20.2 ft

Name: PRPT1 Top height: 93.2 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Gogle is GeoLurary, Maxai Technologies, U.S. Geological Survey, USDA/FPAC/GEO

Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96



Name: PRPT2 Top height: 99.3 ft



1	43.084580	-70.802457	53.31
		101002101	00.01
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

Name: TREELINE Top height: 35.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97



op height: 30.0 ft			
		and the second	
Vertex	Latitude (°)	Google _{le Geolbrary, T} Longitude (°)	laxar Technologies, U.S. Geological Survey, USDAFPAC Ground elevation (ft)
Vertex	Latitude (°) 43.083891		

Name: Trees Top height: 17.0 ft		Google Geolegy	Asxar Technologies, U.S. Geological Survey, USDA/FRAC/GEO
Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085036	-70.807176	92.20



Name: Trees1 Top height: 40.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

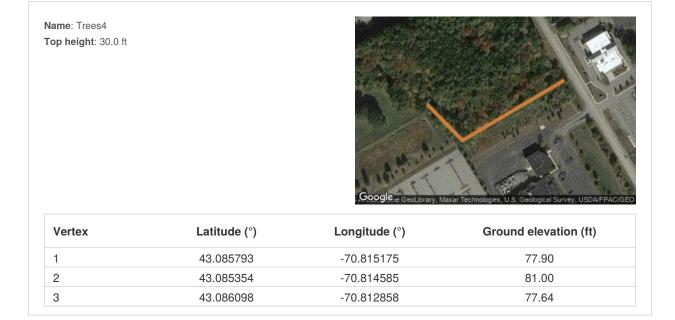
Name: Trees2 Top height: 60.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.084443	-70.818109	84.34
2	43.084602	-70.818167	84.74
3	43.084354	-70.818474	88.75



Name: Trees3
Top height: 100.0 ftImage: State of the s





Name: Trees5 Top height: 45.0 ft



1 43.084411		
1 43.084411	-70.807233	89.30
2 43.084554	-70.807316	89.33
3 43.084677	-70.807358	89.54
4 43.084730	-70.807552	87.97

Name: Trees6 Fop height: 20.0 ft		Coogle - Gecle yray, I	Maxar Technologies, U.S. Geological Survey, USDA/FPA/
	Latitude (°)	Longitude (°)	Ground elevation (ft)
Vertex			
Vertex	43.085286	-70.814633	80.07



≀ame : Trees7 ⊺op height : 30.0 ft			
		Google is GepLarary, I	Maxar Technologies, U.S. Geological Survey, USDA/FPAC/GE
Vertex	Latitude (°)	Google ie Geollarary, f Longitude (°)	Jaxar Technologies, U.S. Geological Survey, USDAFPACIGE Ground elevation (ft)
Vertex 1	Latitude (°) 43.083527		

Name: WRHSE1 Top height: 30.0 ft



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26



Name: WRHSE2 Top height: 30.0 ft



Latitude (°)	Longitude (°)	Ground elevation (ft)
43.084916	-70.813107	81.43
43.084740	-70.813499	81.62
43.084705	-70.813466	81.64
43.084630	-70.813662	81.71
43.084174	-70.813292	81.76
43.084399	-70.812785	81.68
43.084501	-70.812860	81.70
43.084540	-70.812758	81.66
43.084916	-70.813107	81.43
	43.084916 43.084740 43.084705 43.084630 43.084630 43.084399 43.084399 43.084501 43.084540	43.084916 -70.813107 43.084740 -70.813499 43.084705 -70.813466 43.084630 -70.813662 43.084174 -70.813292 43.084399 -70.812785 43.084501 -70.812860 43.084540 -70.812758



PV Array	Tilt	Orient	Annual Gr	een Glare	Annual Ye	low Glare	Energy
	0	o	min	hr	min	hr	kWh
CRPRT1	0.0	124.0	0	0.0	0	0.0	-
CRPRT2	0.0	124.0	0	0.0	0	0.0	-
CRPRT3	0.0	124.0	0	0.0	0	0.0	-
CRPRT4	0.0	124.0	0	0.0	0	0.0	-
CRPRT5	0.0	214.0	0	0.0	0	0.0	-
LGBLDG	10.0	214.0	0	0.0	0	0.0	-
SMBLDG	10.0	214.0	0	0.0	0	0.0	-

Summary of Results No glare predicted

Total annual glare received by each receptor; may include duplicate times of glare from multiple reflective surfaces.

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0.0	0	0.0

PV: CRPRT1

Receptor	Annual Green Glare		Annual Yellow Glare		
	min	hr	min	hr	
1-ATCT	0	0.0	0	0.0	
6-ATCT	0	0.0	0	0.0	

CRPRT1 and **1-ATCT**

CRPRT1 and 6-ATCT

Receptor type: ATCT Observation Point **No glare found**

Receptor type: ATCT Observation Point **No glare found**

PV: CRPRT2

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0.0	0	0.0



CRPRT2 and **1-ATCT**

Receptor type: ATCT Observation Point **No glare found**

CRPRT2 and 6-ATCT

Receptor type: ATCT Observation Point **No glare found**

PV: CRPRT3

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0 0.0		0.0

CRPRT3 and 1-ATCT

CRPRT3 and 6-ATCT

Receptor type: ATCT Observation Point **No glare found**

Receptor type: ATCT Observation Point No glare found

PV: CRPRT4

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0.0	0	0.0

CRPRT4 and 1-ATCT

Receptor type: ATCT Observation Point **No glare found**

CRPRT4 and 6-ATCT

Receptor type: ATCT Observation Point **No glare found**

PV: CRPRT5

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0 0.0		0.0

CRPRT5 and **1-ATCT**

Receptor type: ATCT Observation Point **No glare found**

CRPRT5 and 6-ATCT

Receptor type: ATCT Observation Point **No glare found**



PV: LGBLDG

Receptor	Annual Gr	Annual Green Glare		llow Glare
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0.0	0	0.0

LGBLDG and 1-ATCT

LGBLDG and 6-ATCT

Receptor type: ATCT Observation Point **No glare found**

Receptor type: ATCT Observation Point **No glare found**

PV: SMBLDG

Receptor	Annual Green Glare		Annual Yellow Glare	
	min	hr	min	hr
1-ATCT	0	0.0	0	0.0
6-ATCT	0	0.0	0	0.0

SMBLDG and 1-ATCT

Receptor type: ATCT Observation Point **No glare found**

SMBLDG and 6-ATCT

Receptor type: ATCT Observation Point **No glare found**



Assumptions

"Green" glare is glare with low potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. "Yellow" glare is glare with potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.

The algorithm does not rigorously represent the detailed geometry of a system; detailed features such as gaps between modules, variable height of the PV array, and support structures may impact actual glare results. However, we have validated our models against several systems, including a PV array causing glare to the air-traffic control tower at Manchester-Boston Regional Airport and several sites in Albuquerque, and the tool accurately predicted the occurrence and intensity of glare at different times and days of the year. Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare. This primarily

affects V1 analyses of path receptors.

Random number computations are utilized by various steps of the annual hazard analysis algorithm. Predicted minutes of glare can vary between runs as a result. This limitation primarily affects analyses of Observation Point receptors, including ATCTs. Note that the SGHAT/ ForgeSolar methodology has always relied on an analytical, qualitative approach to accurately determine the overall hazard (i.e. green vs. yellow) of expected glare on an annual basis.

The analysis does not automatically consider obstacles (either man-made or natural) between the observation points and the prescribed solar installation that may obstruct observed glare, such as trees, hills, buildings, etc.

The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)

The variable direct normal irradiance (DNI) feature (if selected) scales the user-prescribed peak DNI using a typical clear-day irradiance profile. This profile has a lower DNI in the mornings and evenings and a maximum at solar noon. The scaling uses a clear-day irradiance profile based on a normalized time relative to sunrise, solar noon, and sunset, which are prescribed by a sun-position algorithm and the latitude and longitude obtained from Google maps. The actual DNI on any given day can be affected by cloud cover, atmospheric attenuation, and other environmental factors.

The ocular hazard predicted by the tool depends on a number of environmental, optical, and human factors, which can be uncertain. We provide input fields and typical ranges of values for these factors so that the user can vary these parameters to see if they have an impact on the results. The speed of SGHAT allows expedited sensitivity and parametric analyses.

The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.

Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid based on aggregated research data. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.

Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.

Refer to the Help page at www.forgesolar.com/help/ for assumptions and limitations not listed here.

Default glare analysis parameters and observer eye characteristics (for reference only):

- · Analysis time interval: 1 minute
- Ocular transmission coefficient: 0.5
- Pupil diameter: 0.002 meters
- Eye focal length: 0.017 meters
- · Sun subtended angle: 9.3 milliradians

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ALBACORE, Portsmouth, NH Albacore_10DegreeTilt_124Carports_ATCT_FAAReport

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112738.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



Misc. Analysis Settings

DNI: varies (1,000.0 W/m² peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

Summary of Results No glare predicted!

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	0	0	-
CRPRT4	0.0	124.0	0	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	10.0	214.0	0	0	-
SMBLDG	10.0	214.0	0	0	-

PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Latitude	Longitude	Ground elevation	Height above ground	Total elevation
deg	deg	ft	ft	ft
43.085400	-70.803418	56.90	22.48	79.38
43.085325	-70.803271	56.23	14.00	70.23
43.084876	-70.803716	58.56	14.00	72.56
43.084953	-70.803866	59.01	22.48	81.49
	deg 43.085400 43.085325 43.084876	deg deg 43.085400 -70.803418 43.085325 -70.803271 43.084876 -70.803716	deg deg ft 43.085400 -70.803418 56.90 43.085325 -70.803271 56.23 43.084876 -70.803716 58.56	deg deg ft ft 43.085400 -70.803418 56.90 22.48 43.085325 -70.803271 56.23 14.00 43.084876 -70.803716 58.56 14.00

Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
STREE STREET	8	43.084643	-70.803375	58.79	88.00	146.79

Discrete Observation Receptors

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97

1-ATCT map image



6-ATCT map image



Obstruction Components

Name: BLDG1 Upper edge height: 12.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084600	-70.810084	76.71
2	43.084703	-70.809846	77.63
3	43.084534	-70.809702	77.38
4	43.084428	-70.809944	77.34
5	43.084600	-70.810084	76.71

Name: BLDG2 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084955	-70.806346	99.52
2	43.085031	-70.806408	98.08
3	43.084866	-70.806801	99.55
4	43.084555	-70.806565	99.98
5	43.084608	-70.806439	99.85
6	43.084444	-70.806325	99.64
7	43.084592	-70.806011	99.08
8	43.084965	-70.806346	99.43

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085593	-70.803598	57.75
2	43.085019	-70.804161	63.07

Name: HighEdge3 Upper edge height: 22.5 ft



deg	deg	ft
1 43.085	424 -70.803445	56.71
2 43.084	960 -70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

Name: TREELINE Upper edge height: 35.0 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.085164	-70.808848	82.83
43.085454	-70.807942	81.22
43.085373	-70.807765	82.86
43.085040	-70.807564	86.97
	deg 43.085164 43.085454 43.085373	deg deg 43.085164 -70.808848 43.085454 -70.807942 43.085373 -70.807765

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085036	-70.807176	92.20
2	43.084131	-70.806567	95.41

Name: Trees1 Upper edge height: 40.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.084443	-70.818109	84.34
43.084602	-70.818167	84.74
43.084354	-70.818474	88.75
	deg 43.084443 43.084602	deg deg 43.084443 -70.818109 43.084602 -70.818167

Name: Trees3 Upper edge height: 100.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084287	-70.810576	72.89
2	43.084550	-70.810195	75.28

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085286	-70.814633	80.07
2	43.083793	-70.813418	79.96

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26

Name: WRHSE2 Upper edge height: 30.0 ft



/ertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
	43.084916	-70.813107	81.43
2	43.084740	-70.813499	81.62
3	43.084705	-70.813466	81.64
ł	43.084630	-70.813662	81.71
5	43.084174	-70.813292	81.76
	43.084399	-70.812785	81.68
•	43.084501	-70.812860	81.70
}	43.084540	-70.812758	81.66
	43.084916	-70.813107	81.43

Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	0	0	-	-
CRPRT4	0.0	124.0	0	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	10.0	214.0	0	0	-	-
SMBLDG	10.0	214.0	0	0	-	-

PV & Receptor Analysis Results

Results for each PV array and receptor

CRPRT1 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

CRPRT2 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

CRPRT3 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

CRPRT4 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

CRPRT5 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0

No glare found

Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi
 obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous
 modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
 PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, nc discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.

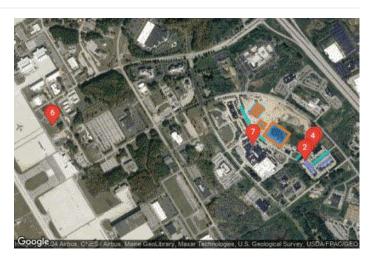


ALBACORE, Portsmouth, NH ALBCR_15Tilt_124Carports_NOObstrctns_2ATCT_AddOP

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112714.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



Misc. Analysis Settings

DNI: varies (1,000.0 W/m² peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

Summary of Results Glare with low potential for temporary after-image predicted

PV Name	Tilt	Orientation	"Green" Glare "Yellow" Glare		Energy Produced	
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	1,543	0	-	
CRPRT2	0.0	124.0	0	0	-	
CRPRT3	0.0	124.0	1,314	0	-	
CRPRT4	0.0	124.0	1,617	0	-	
CRPRT5	0.0	214.0	0	0	-	
LGBLDG	15.0	214.0	0	0	-	
SMBLDG	15.0	214.0	0	0	-	

PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Latitude	Longitude	Ground elevation	Height above ground	Total elevation
deg	deg	ft	ft	ft
43.085400	-70.803418	56.90	22.48	79.38
43.085325	-70.803271	56.23	14.00	70.23
43.084876	-70.803716	58.56	14.00	72.56
43.084953	-70.803866	59.01	22.48	81.49
	deg 43.085400 43.085325 43.084876	deg deg 43.085400 -70.803418 43.085325 -70.803271 43.084876 -70.803716	deg deg ft 43.085400 -70.803418 56.90 43.085325 -70.803271 56.23 43.084876 -70.803716 58.56	deg deg ft ft 43.085400 -70.803418 56.90 22.48 43.085325 -70.803271 56.23 14.00 43.084876 -70.803716 58.56 14.00

Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 15.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 15.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
E MEN A	8	43.084643	-70.803375	58.79	88.00	146.79

Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082313	-70.799503	41.53	4.50	46.03
2	43.082995	-70.798326	37.86	4.50	42.36

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

Discrete Observation Receptors

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083312	-70.803940	70.10	40.00	110.10

1-ATCT map image



6-ATCT map image



Obstruction Components

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085593	-70.803598	57.75
2	43.085019	-70.804161	63.07

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.084580	-70.802457	53.31
43.083953	-70.801212	46.09
43.083224	-70.801856	52.36
43.083866	-70.803165	61.10
43.084580	-70.802457	53.31
	deg 43.084580 43.083953 43.083224 43.083866	deg deg 43.084580 -70.802457 43.083953 -70.801212 43.083224 -70.801856 43.083866 -70.803165

Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	1,543	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	1,314	0	-	-
CRPRT4	0.0	124.0	1,617	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	15.0	214.0	0	0	-	-
SMBLDG	15.0	214.0	0	0	-	-

Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

PV	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
crprt1 (green)	0	0	105	292	0	0	0	81	319	0	0	0
crprt1 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt3 (green)	0	88	142	137	0	0	0	1	281	86	0	0
crprt3 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt4 (green)	0	139	219	103	0	0	0	0	273	187	0	0
crprt4 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0

PV & Receptor Analysis Results

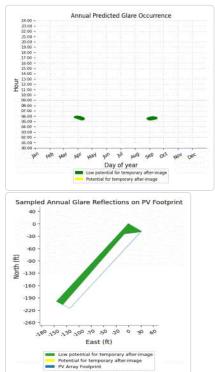
Results for each PV array and receptor

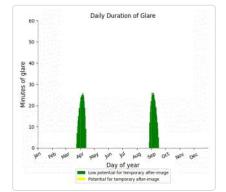
CRPRT1 low potential for temporary after-image

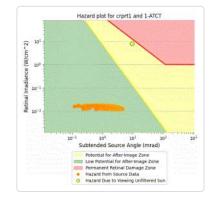
Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	783	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	760	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT1: 1-ATCT

- PV array is expected to produce the following glare for this receptor:
 783 minutes of "green" glare with low potential to cause temporary after-image.
 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT1: OP 2

No glare found

CRPRT1: OP 3

No glare found

CRPRT1: OP 4

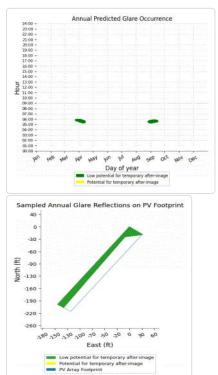
No glare found

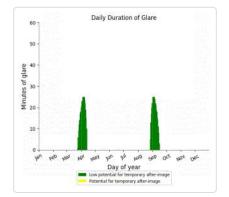
CRPRT1: OP 5

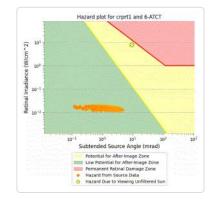
No glare found

CRPRT1: 6-ATCT

- PV array is expected to produce the following glare for this receptor: 760 minutes of "green" glare with low potential to cause temporary after-image.
 - 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT1: OP 7

No glare found

CRPRT1: Route 1

No glare found

CRPRT1: Route 2

No glare found

CRPRT1: Route 3

No glare found

CRPRT1: Route 4

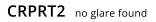
No glare found

CRPRT1: Route 5

No glare found

CRPRT1: Route 6

No glare found



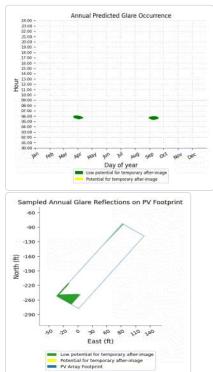
Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

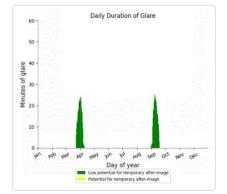
CRPRT3 low potential for temporary after-image

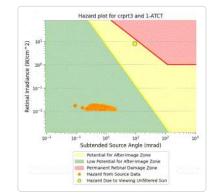
Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	548	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	530	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	78	0
Route: Route 4	158	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT3: 1-ATCT

- PV array is expected to produce the following glare for this receptor:
 548 minutes of "green" glare with low potential to cause temporary after-image.
 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT3: OP 2

No glare found

CRPRT3: OP 3

No glare found

CRPRT3: OP 4

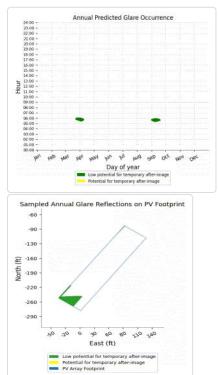
No glare found

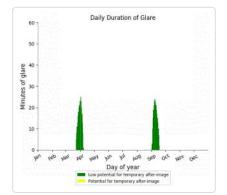
CRPRT3: OP 5

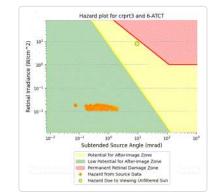
No glare found

CRPRT3: 6-ATCT

- PV array is expected to produce the following glare for this receptor:
 530 minutes of "green" glare with low potential to cause temporary after-image.
 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT3: OP 7

No glare found

CRPRT3: Route 1

No glare found

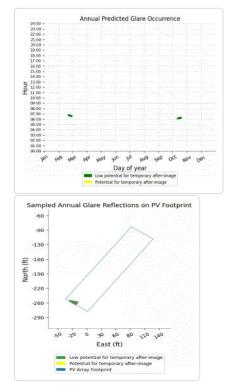
CRPRT3: Route 2

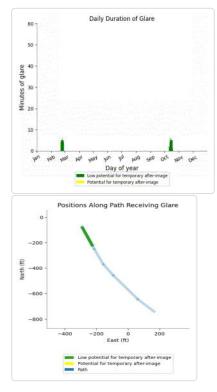
No glare found

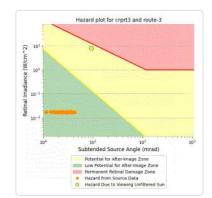
CRPRT3: Route 3

PV array is expected to produce the following glare for this receptor: • 78 minutes of "green" glare with low potential to cause temporary after-image.

- 0 minutes of "yellow" glare with potential to cause temporary after-image.



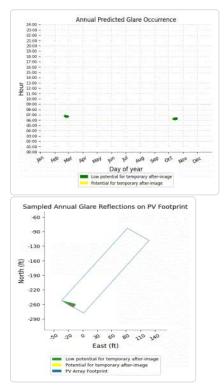


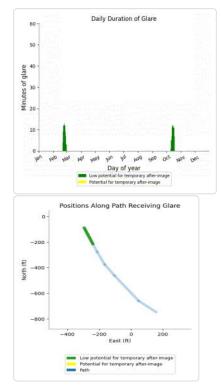


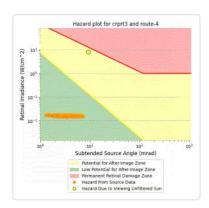
CRPRT3: Route 4

PV array is expected to produce the following glare for this receptor:

- 158 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT3: Route 5

No glare found

CRPRT3: Route 6

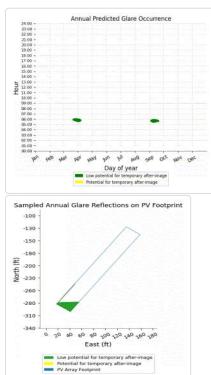
No glare found

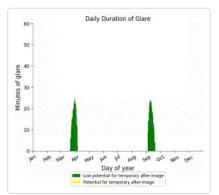
CRPRT4 low potential for temporary after-image

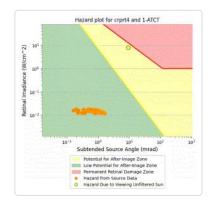
Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	532	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	514	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	314	0
Route: Route 4	257	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT4: 1-ATCT

- PV array is expected to produce the following glare for this receptor: 532 minutes of "green" glare with low potential to cause temporary after-image.
 - 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT4: OP 2

No glare found

CRPRT4: OP 3

No glare found

CRPRT4: OP 4

No glare found

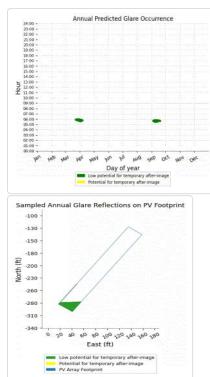
CRPRT4: OP 5

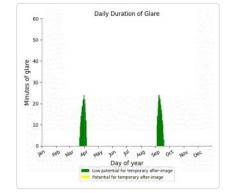
No glare found

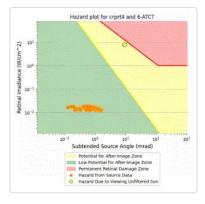
CRPRT4: 6-ATCT

PV array is expected to produce the following glare for this receptor:

- 514 minutes of "green" glare with low potential to cause temporary after-image.
 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT4: OP 7

No glare found

CRPRT4: Route 1

No glare found

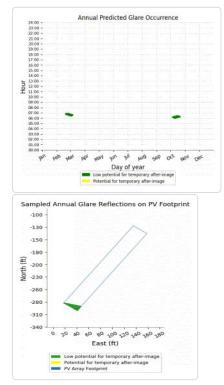
CRPRT4: Route 2

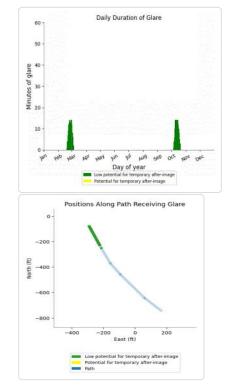
No glare found

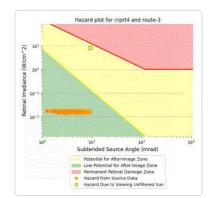
CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 314 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.



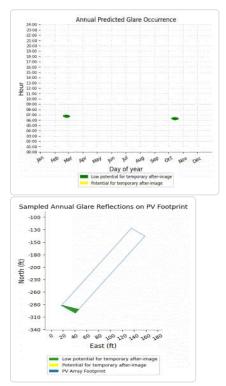


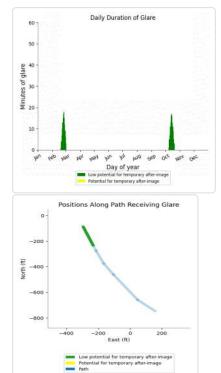


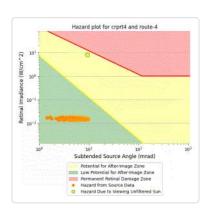
CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 257 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT4: Route 5

No glare found

CRPRT4: Route 6

No glare found

CRPRT5 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
 PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no discrete, spectrum.
- · Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.

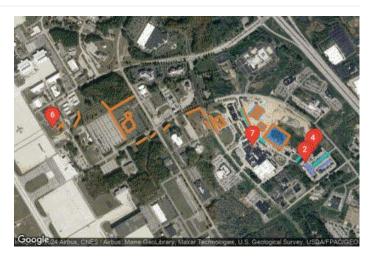


ALBACORE, Portsmouth, NH ALBCR_10Tilt_124Carports_Obstrctns_2ATCT_AddOP

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112715.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



Misc. Analysis Settings

DNI: varies (1,000.0 W/m² peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

Summary of Results No glare predicted!

PV Name	Tilt	Orientation	"Green" Glare "Yellow" Glare		Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	0	0	-
CRPRT4	0.0	124.0	0	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	10.0	214.0	0	0	-
SMBLDG	10.0	214.0	0	0	-

PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Latitude	Longitude	Ground elevation	Height above ground	Total elevation
deg	deg	ft	ft	ft
43.085400	-70.803418	56.90	22.48	79.38
43.085325	-70.803271	56.23	14.00	70.23
43.084876	-70.803716	58.56	14.00	72.56
43.084953	-70.803866	59.01	22.48	81.49
	deg 43.085400 43.085325 43.084876	deg deg 43.085400 -70.803418 43.085325 -70.803271 43.084876 -70.803716	deg deg ft 43.085400 -70.803418 56.90 43.085325 -70.803271 56.23 43.084876 -70.803716 58.56	deg deg ft ft 43.085400 -70.803418 56.90 22.48 43.085325 -70.803271 56.23 14.00 43.084876 -70.803716 58.56 14.00

Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
EIGHEN AND STATES	8	43.084643	-70.803375	58.79	88.00	146.79

Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082313	-70.799503	41.53	4.50	46.03
2	43.082995	-70.798326	37.86	4.50	42.36

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

Discrete Observation Receptors

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083343	-70.803962	70.10	40.00	110.10

1-ATCT map image



6-ATCT map image



Obstruction Components

Name: BLDG2 Upper edge height: 20.0 ft	Vertex	Latitude	Longitude	Ground elevation
		deg	deg	ft
	1	43.084955	-70.806346	99.52
	2	43.085031	-70.806408	98.08
	3	43.084866	-70.806801	99.55
	4	43.084555	-70.806565	99.98
	5	43.084608	-70.806439	99.85
A CARLES CONTRACTOR	6	43.084444	-70.806325	99.64
	7	43.084592	-70.806011	99.08
	8	43.084965	-70.806346	99.43

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085593	-70.803598	57.75
2	43.085019	-70.804161	63.07

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PLANTING Upper edge height: 9.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085446	-70.804721	64.24
2	43.084717	-70.804268	69.47
3	43.084592	-70.804158	69.46

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.084580	-70.802457	53.31
43.083953	-70.801212	46.09
43.083224	-70.801856	52.36
43.083866	-70.803165	61.10
43.084580	-70.802457	53.31
	deg 43.084580 43.083953 43.083224 43.083866	deg deg 43.084580 -70.802457 43.083953 -70.801212 43.083224 -70.801856 43.083866 -70.803165

Name: TREELINE Upper edge height: 35.0 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.085164	-70.808848	82.83
43.085454	-70.807942	81.22
43.085373	-70.807765	82.86
43.085040	-70.807564	86.97
	deg 43.085164 43.085454 43.085373	deg deg 43.085164 -70.808848 43.085454 -70.807942 43.085373 -70.807765

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation	
	deg	deg	ft	
1	43.085036	-70.807176	92.20	_
2	43.084131	-70.806567	95.41	

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees1 Upper edge height: 40.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Latitude	Longitude	Ground elevation
deg	deg	ft
43.084443	-70.818109	84.34
43.084602	-70.818167	84.74
43.084354	-70.818474	88.75
	deg 43.084443 43.084602	deg deg 43.084443 -70.818109 43.084602 -70.818167

Name: Trees3 Upper edge height: 100.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084287	-70.810576	72.89
2	43.084550	-70.810195	75.28

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085286	-70.814633	80.07
2	43.083793	-70.813418	79.96

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26

Name: WRHSE2 Upper edge height: 30.0 ft



/ertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
	43.084916	-70.813107	81.43
2	43.084740	-70.813499	81.62
3	43.084705	-70.813466	81.64
ł	43.084630	-70.813662	81.71
5	43.084174	-70.813292	81.76
	43.084399	-70.812785	81.68
•	43.084501	-70.812860	81.70
}	43.084540	-70.812758	81.66
	43.084916	-70.813107	81.43

Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	0	0	-	-
CRPRT4	0.0	124.0	0	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	10.0	214.0	0	0	-	-
SMBLDG	10.0	214.0	0	0	-	-

PV & Receptor Analysis Results

Results for each PV array and receptor

CRPRT1 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

CRPRT2 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT3 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

CRPRT4 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT5 no glare found

Component	Green glare (min)	Yellow glare (min)	
OP: 1-ATCT	0	0	
OP: OP 2	0	0	
OP: OP 3	0	0	
OP: OP 4	0	0	
OP: OP 5	0	0	
OP: 6-ATCT	0	0	
OP: OP 7	0	0	
Route: Route 1	0	0	
Route: Route 2	0	0	
Route: Route 3	0	0	
Route: Route 4	0	0	
Route: Route 5	0	0	
Route: Route 6	0	0	

No glare found

LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
 Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated. The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. . Actual values and results may vary.

- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous • modeling methods. Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
- PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no • discrete, spectrum.
- Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.

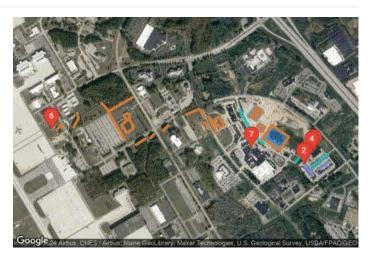


ALBACORE, Portsmouth, NH ALBCR_5Tilt_124Carports_Obstrctns_2ATCT_NoPlant

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112718.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



Misc. Analysis Settings

DNI: varies (1,000.0 W/m² peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

Summary of Results Glare with low potential for temporary after-image predicted

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	236	0	-
CRPRT4	0.0	124.0	566	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	5.0	214.0	0	0	-
SMBLDG	5.0	214.0	0	0	-

PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Latitude	Longitude	Ground elevation	Height above ground	Total elevation
deg	deg	ft	ft	ft
43.085400	-70.803418	56.90	22.48	79.38
43.085325	-70.803271	56.23	14.00	70.23
43.084876	-70.803716	58.56	14.00	72.56
43.084953	-70.803866	59.01	22.48	81.49
	deg 43.085400 43.085325 43.084876	deg deg 43.085400 -70.803418 43.085325 -70.803271 43.084876 -70.803716	deg deg ft 43.085400 -70.803418 56.90 43.085325 -70.803271 56.23 43.084876 -70.803716 58.56	deg deg ft ft 43.085400 -70.803418 56.90 22.48 43.085325 -70.803271 56.23 14.00 43.084876 -70.803716 58.56 14.00

Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating

Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 5.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 5.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
C-INF MARK	8	43.084643	-70.803375	58.79	88.00	146.79

Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082313	-70.799503	41.53	4.50	46.03
2	43.082995	-70.798326	37.86	4.50	42.36

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

Discrete Observation Receptors

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083343	-70.803962	70.10	40.00	110.10

1-ATCT map image



6-ATCT map image



Obstruction Components

Name: BLDG2 Upper edge height: 20.0 ft	Vertex	Latitude	Longitude	Ground elevation
		deg	deg	ft
	1	43.084955	-70.806346	99.52
	2	43.085031	-70.806408	98.08
	3	43.084866	-70.806801	99.55
	4	43.084555	-70.806565	99.98
	5	43.084608	-70.806439	99.85
A CARLES CONTRACTOR	6	43.084444	-70.806325	99.64
	7	43.084592	-70.806011	99.08
	8	43.084965	-70.806346	99.43

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085593	-70.803598	57.75
2	43.085019	-70.804161	63.07

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

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and the	1.48		

Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085036	-70.807176	92.20
2	43.084131	-70.806567	95.41

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees1 Upper edge height: 40.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084443	-70.818109	84.34
2	43.084602	-70.818167	84.74
3	43.084354	-70.818474	88.75

Name: Trees3 Upper edge height: 100.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084287	-70.810576	72.89
2	43.084550	-70.810195	75.28
2			

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085286	-70.814633	80.07
2	43.083793	-70.813418	79.96

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26

Name: WRHSE2 Upper edge height: 30.0 ft



/ertex	Latitude Longitude		Ground elevation	
	deg	deg	ft	
	43.084916	-70.813107	81.43	
	43.084740	-70.813499	81.62	
	43.084705	-70.813466	81.64	
	43.084630	-70.813662	81.71	
	43.084174	-70.813292	81.76	
	43.084399	-70.812785	81.68	
	43.084501	-70.812860	81.70	
	43.084540	-70.812758	81.66	
	43.084916	-70.813107	81.43	

Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare "Yellow" Glare		Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	236	0	-	-
CRPRT4	0.0	124.0	566	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	5.0	214.0	0	0	-	-
SMBLDG	5.0	214.0	0	0	-	-

Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

PV	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
crprt3 (green)	0	87	0	0	0	0	0	0	0	85	0	0
crprt3 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt4 (green)	0	139	48	0	0	0	0	0	0	186	0	0
crprt4 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0

PV & Receptor Analysis Results

Results for each PV array and receptor

CRPRT1 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT2 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

CRPRT3 low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	79	0
Route: Route 4	157	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT3: 1-ATCT

No glare found

CRPRT3: OP 2

No glare found

CRPRT3: OP 3

No glare found

CRPRT3: OP 4

No glare found

CRPRT3: OP 5

No glare found

CRPRT3: 6-ATCT

No glare found

CRPRT3: OP 7

No glare found

CRPRT3: Route 1

No glare found

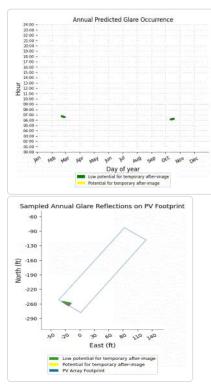
CRPRT3: Route 2

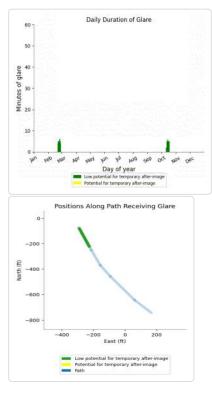
No glare found

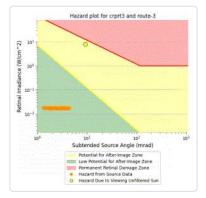
CRPRT3: Route 3

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image. 0 minutes of "yellow" glare with potential to cause temporary after-image. •

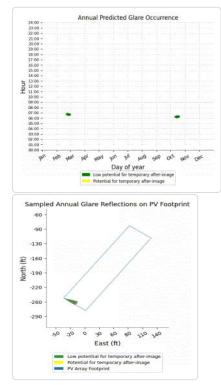


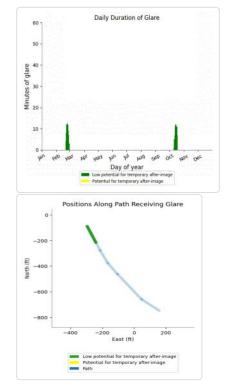


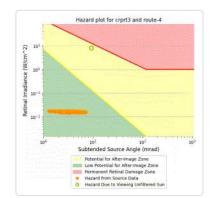


CRPRT3: Route 4

- PV array is expected to produce the following glare for this receptor: 157 minutes of "green" glare with low potential to cause temporary after-image.
 - 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT3: Route 5

No glare found

CRPRT3: Route 6

No glare found

CRPRT4 low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	311	0
Route: Route 4	255	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT4: 1-ATCT

No glare found

CRPRT4: OP 2

No glare found

CRPRT4: OP 3

No glare found

CRPRT4: OP 4

No glare found

CRPRT4: OP 5

No glare found

CRPRT4: 6-ATCT

No glare found

CRPRT4: OP 7

No glare found

CRPRT4: Route 1

No glare found

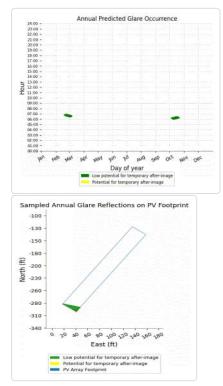
CRPRT4: Route 2

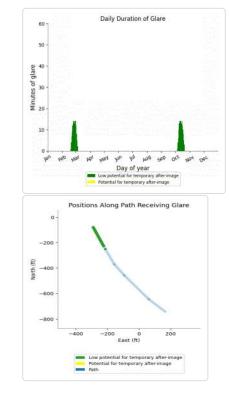
No glare found

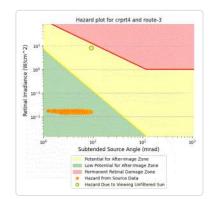
CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.



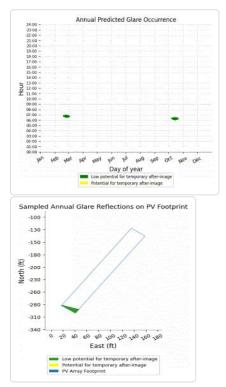


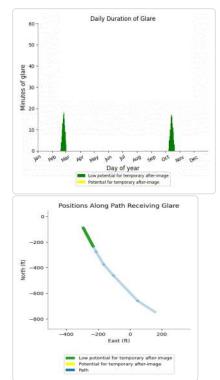


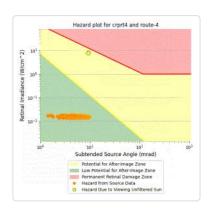
CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT4: Route 5

No glare found

CRPRT4: Route 6

No glare found

CRPRT5 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
 PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no discrete, spectrum.
- · Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.



ALBACORE, Portsmouth, NH ALBCR_10Tilt_124Carports_Obstrctns_2ATCT_NoPlant

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112717.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



Misc. Analysis Settings

DNI: varies (1,000.0 W/m² peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

Summary of Results Glare with low potential for temporary after-image predicted

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	236	0	-
CRPRT4	0.0	124.0	566	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	10.0	214.0	0	0	-
SMBLDG	10.0	214.0	0	0	-

PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Latitude	Longitude	Ground elevation	Height above ground	Total elevation
deg	deg	ft	ft	ft
43.085400	-70.803418	56.90	22.48	79.38
43.085325	-70.803271	56.23	14.00	70.23
43.084876	-70.803716	58.56	14.00	72.56
43.084953	-70.803866	59.01	22.48	81.49
	deg 43.085400 43.085325 43.084876	deg deg 43.085400 -70.803418 43.085325 -70.803271 43.084876 -70.803716	deg deg ft 43.085400 -70.803418 56.90 43.085325 -70.803271 56.23 43.084876 -70.803716 58.56	deg deg ft ft 43.085400 -70.803418 56.90 22.48 43.085325 -70.803271 56.23 14.00 43.084876 -70.803716 58.56 14.00

Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Ground elevation Height above ground	
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation	
	deg	deg	ft	ft	ft	
1	43.084344	-70.802133	51.60	93.83	145.44	
2	43.084054	-70.801543	49.18	93.83	143.01	
3	43.083901	-70.801690	49.39	93.83	143.22	
4	43.083859	-70.801609	49.20	93.83	143.03	
5	43.083897	-70.801574	49.27	93.83	143.10	
6	43.083839	-70.801453	47.35	93.83	141.18	
7	43.083345	-70.801919	51.93	93.83	145.76	
8	43.083906	-70.803019	59.40	93.83	153.23	
9	43.084395	-70.802537	54.24	93.83	148.07	
10	43.084315	-70.802368	51.53	93.83	145.36	
11	43.084337	-70.802347	51.04	93.83	144.87	
12	43.084303	-70.802278	52.48	93.83	146.31	
13	43.084336	-70.802245	52.51	93.83	146.34	
14	43.084297	-70.802171	51.69	93.83	145.52	

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 10.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
EIGHEN AND STATES	8	43.084643	-70.803375	58.79	88.00	146.79

Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082313	-70.799503	41.53	4.50	46.03
2	43.082995	-70.798326	37.86	4.50	42.36

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

Discrete Observation Receptors

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083343	-70.803962	70.10	40.00	110.10

1-ATCT map image



6-ATCT map image



Obstruction Components

Name: BLDG2 Upper edge height: 20.0 ft	Vertex	Latitude	Longitude	Ground elevation
		deg	deg	ft
	1	43.084955	-70.806346	99.52
	2	43.085031	-70.806408	98.08
	3	43.084866	-70.806801	99.55
	4	43.084555	-70.806565	99.98
	5	43.084608	-70.806439	99.85
A CARLES CONTRACTOR	6	43.084444	-70.806325	99.64
	7	43.084592	-70.806011	99.08
	8	43.084965	-70.806346	99.43

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085593	-70.803598	57.75
2	43.085019	-70.804161	63.07

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

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and the	1.48		

Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation	
	deg	deg	ft	
1	43.085036	-70.807176	92.20	
2	43.084131	-70.806567	95.41	

Name: Trees1 Upper edge height: 40.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084443	-70.818109	84.34
2	43.084602	-70.818167	84.74
3	43.084354	-70.818474	88.75

Name: Trees3 Upper edge height: 100.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084287	-70.810576	72.89
2	43.084550	-70.810195	75.28
2			

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085286	-70.814633	80.07
2	43.083793	-70.813418	79.96

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26

Name: WRHSE2 Upper edge height: 30.0 ft



/ertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
	43.084916	-70.813107	81.43
	43.084740	-70.813499	81.62
	43.084705	-70.813466	81.64
	43.084630	-70.813662	81.71
	43.084174	-70.813292	81.76
	43.084399	-70.812785	81.68
	43.084501	-70.812860	81.70
	43.084540	-70.812758	81.66
	43.084916	-70.813107	81.43

Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	236	0	-	-
CRPRT4	0.0	124.0	566	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	10.0	214.0	0	0	-	-
SMBLDG	10.0	214.0	0	0	-	-

Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

PV	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
crprt3 (green)	0	87	0	0	0	0	0	0	0	85	0	0
crprt3 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt4 (green)	0	139	48	0	0	0	0	0	0	186	0	0
crprt4 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0

PV & Receptor Analysis Results

Results for each PV array and receptor

CRPRT1 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT2 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

CRPRT3 low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	79	0
Route: Route 4	157	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT3: 1-ATCT

No glare found

CRPRT3: OP 2

No glare found

CRPRT3: OP 3

No glare found

CRPRT3: OP 4

No glare found

CRPRT3: OP 5

No glare found

CRPRT3: 6-ATCT

No glare found

CRPRT3: OP 7

No glare found

CRPRT3: Route 1

No glare found

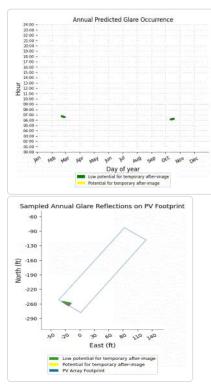
CRPRT3: Route 2

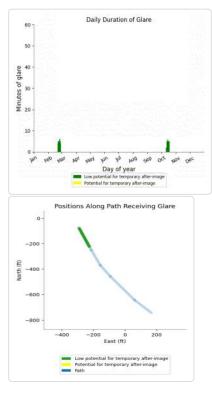
No glare found

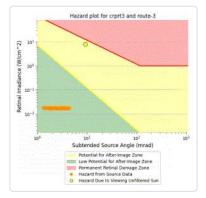
CRPRT3: Route 3

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image. 0 minutes of "yellow" glare with potential to cause temporary after-image. •

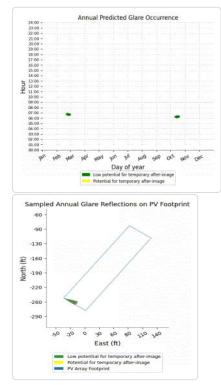


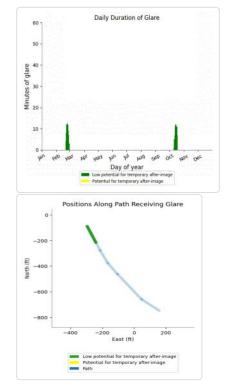


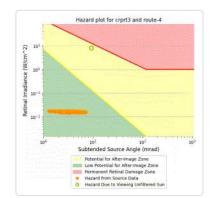


CRPRT3: Route 4

- PV array is expected to produce the following glare for this receptor: 157 minutes of "green" glare with low potential to cause temporary after-image.
 - 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT3: Route 5

No glare found

CRPRT3: Route 6

No glare found

CRPRT4 low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	311	0
Route: Route 4	255	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT4: 1-ATCT

No glare found

CRPRT4: OP 2

No glare found

CRPRT4: OP 3

No glare found

CRPRT4: OP 4

No glare found

CRPRT4: OP 5

No glare found

CRPRT4: 6-ATCT

No glare found

CRPRT4: OP 7

No glare found

CRPRT4: Route 1

No glare found

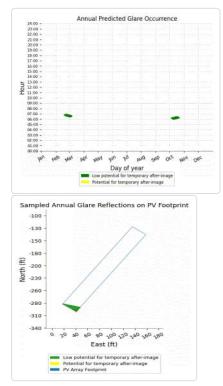
CRPRT4: Route 2

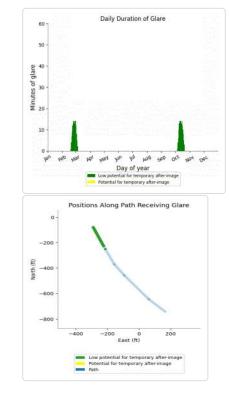
No glare found

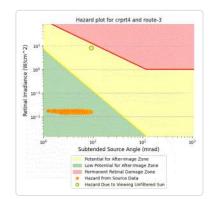
CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.



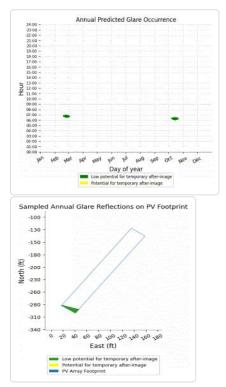


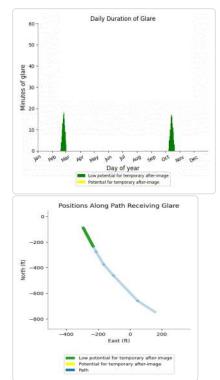


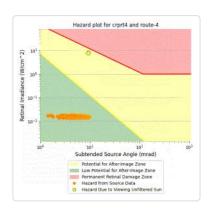
CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT4: Route 5

No glare found

CRPRT4: Route 6

No glare found

CRPRT5 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
 PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no discrete, spectrum.
- · Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.



ALBACORE, Portsmouth, NH ALBCR_13Tilt_124Carports_Obstrctns_2ATCT_NoPlant

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112727.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



Misc. Analysis Settings

DNI: varies (1,000.0 W/m² peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

Summary of Results Glare with low potential for temporary after-image predicted

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	236	0	-
CRPRT4	0.0	124.0	566	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	13.0	214.0	0	0	-
SMBLDG	13.0	214.0	0	0	-

PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Latitude	Longitude	Ground elevation	Height above ground	Total elevation
deg	deg	ft	ft	ft
43.085400	-70.803418	56.90	22.48	79.38
43.085325	-70.803271	56.23	14.00	70.23
43.084876	-70.803716	58.56	14.00	72.56
43.084953	-70.803866	59.01	22.48	81.49
	deg 43.085400 43.085325 43.084876	deg deg 43.085400 -70.803418 43.085325 -70.803271 43.084876 -70.803716	deg deg ft 43.085400 -70.803418 56.90 43.085325 -70.803271 56.23 43.084876 -70.803716 58.56	deg deg ft ft 43.085400 -70.803418 56.90 22.48 43.085325 -70.803271 56.23 14.00 43.084876 -70.803716 58.56 14.00

Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 13.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Ground elevation Height above ground	
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 13.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
	8	43.084643	-70.803375	58.79	88.00	146.79

Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082313	-70.799503	41.53	4.50	46.03
2	43.082995	-70.798326	37.86	4.50	42.36

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

Discrete Observation Receptors

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083343	-70.803962	70.10	40.00	110.10

1-ATCT map image



6-ATCT map image



Obstruction Components

Name: BLDG2 Upper edge height: 20.0 ft	Vertex	Latitude	Longitude	Ground elevation
		deg	deg	ft
	1	43.084955	-70.806346	99.52
	2	43.085031	-70.806408	98.08
	3	43.084866	-70.806801	99.55
	4	43.084555	-70.806565	99.98
	5	43.084608	-70.806439	99.85
A CARLES CONTRACTOR	6	43.084444	-70.806325	99.64
	7	43.084592	-70.806011	99.08
	8	43.084965	-70.806346	99.43

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085593	-70.803598	57.75
2	43.085019	-70.804161	63.07

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

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Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085036	-70.807176	92.20
2	43.084131	-70.806567	95.41

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees1 Upper edge height: 40.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084443	-70.818109	84.34
2	43.084602	-70.818167	84.74
3	43.084354	-70.818474	88.75

Name: Trees3 Upper edge height: 100.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084287	-70.810576	72.89
2	43.084550	-70.810195	75.28
2			

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085286	-70.814633	80.07
2	43.083793	-70.813418	79.96

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Vertex	Latitude l	Longitude	Ground elevation ft
		deg	
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26

Name: WRHSE2 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
	43.084916	-70.813107	81.43
	43.084740	-70.813499	81.62
	43.084705	-70.813466	81.64
	43.084630	-70.813662	81.71
	43.084174	-70.813292	81.76
	43.084399	-70.812785	81.68
	43.084501	-70.812860	81.70
	43.084540	-70.812758	81.66
	43.084916	-70.813107	81.43

Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	236	0	-	-
CRPRT4	0.0	124.0	566	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	13.0	214.0	0	0	-	-
SMBLDG	13.0	214.0	0	0	-	-

Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

PV	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
crprt3 (green)	0	87	0	0	0	0	0	0	0	85	0	0
crprt3 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt4 (green)	0	139	48	0	0	0	0	0	0	186	0	0
crprt4 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0

PV & Receptor Analysis Results

Results for each PV array and receptor

CRPRT1 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT2 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

CRPRT3 low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	79	0
Route: Route 4	157	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT3: 1-ATCT

No glare found

CRPRT3: OP 2

No glare found

CRPRT3: OP 3

No glare found

CRPRT3: OP 4

No glare found

CRPRT3: OP 5

No glare found

CRPRT3: 6-ATCT

No glare found

CRPRT3: OP 7

No glare found

CRPRT3: Route 1

No glare found

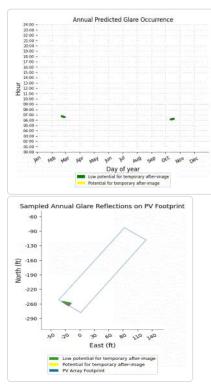
CRPRT3: Route 2

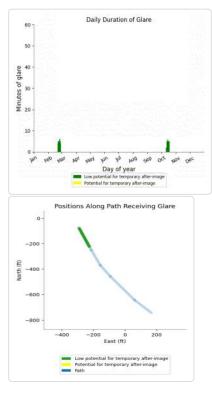
No glare found

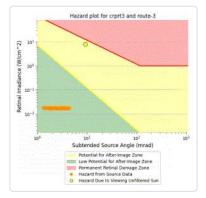
CRPRT3: Route 3

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image. 0 minutes of "yellow" glare with potential to cause temporary after-image. •

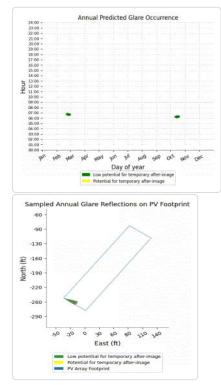


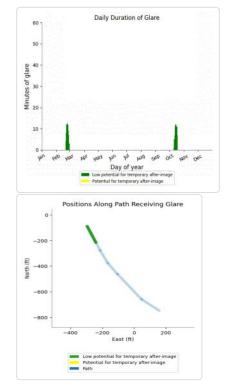


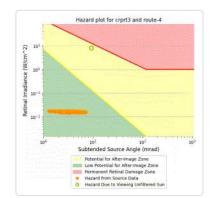


CRPRT3: Route 4

- PV array is expected to produce the following glare for this receptor: 157 minutes of "green" glare with low potential to cause temporary after-image.
 - 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT3: Route 5

No glare found

CRPRT3: Route 6

No glare found

CRPRT4 low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	311	0
Route: Route 4	255	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT4: 1-ATCT

No glare found

CRPRT4: OP 2

No glare found

CRPRT4: OP 3

No glare found

CRPRT4: OP 4

No glare found

CRPRT4: OP 5

No glare found

CRPRT4: 6-ATCT

No glare found

CRPRT4: OP 7

No glare found

CRPRT4: Route 1

No glare found

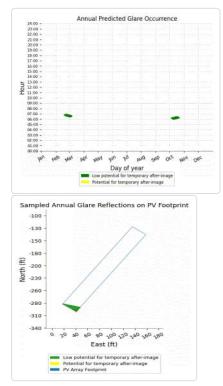
CRPRT4: Route 2

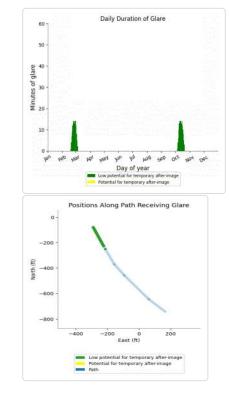
No glare found

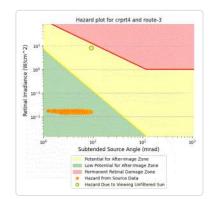
CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.



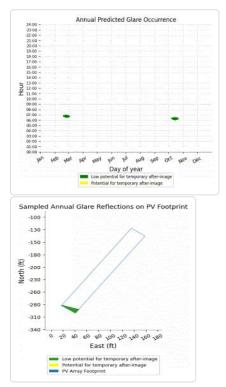


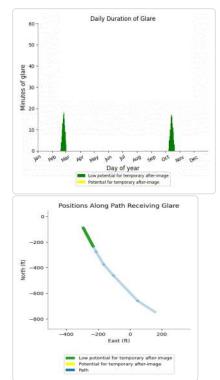


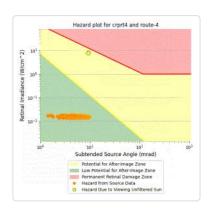
CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT4: Route 5

No glare found

CRPRT4: Route 6

No glare found

CRPRT5 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
 PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no discrete, spectrum.
- · Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.



ALBACORE, Portsmouth, NH ALBCR_15Tilt_124Carports_Obstrctns_2ATCT_NoPlant

Client: Lonza

Created Feb 22, 2024 Updated Feb 22, 2024 Time-step 1 minute Timezone offset UTC-5 Minimum sun altitude 0.0 deg Site ID 112723.19298

Project type Advanced Project status: active Category 1 MW to 5 MW



Misc. Analysis Settings

DNI: varies (1,000.0 W/m² peak) Ocular transmission coefficient: 0.5 Pupil diameter: 0.002 m Eye focal length: 0.017 m Sun subtended angle: 9.3 mrad PV Analysis Methodology: Version 2 Enhanced subtended angle calculation: On

Summary of Results Glare with low potential for temporary after-image predicted

PV Name	Tilt	Orientation	"Green" Glare	"Yellow" Glare	Energy Produced
	deg	deg	min	min	kWh
CRPRT1	0.0	124.0	0	0	-
CRPRT2	0.0	124.0	0	0	-
CRPRT3	0.0	124.0	236	0	-
CRPRT4	0.0	124.0	566	0	-
CRPRT5	0.0	214.0	0	0	-
LGBLDG	15.0	214.0	0	0	-
SMBLDG	15.0	214.0	0	0	-

PV Array(s)

Name: CRPRT1

Tilt: 0.0 deg

Rated power: -

Total PV footprint area: 3.1 acres

Footprint area: 0.20 acre Vertex Latitude Longitude Ground elevation Height above ground Total elevation Axis tracking: Fixed (no rotation) deg deg ft ft ft Orientation: 124.0 deg 43.085650 -70.803723 78.09 1 57.92 20.17 Panel material: Smooth glass with AR coating 2 43.085595 -70.803619 57.81 14.00 71.81 Vary reflectivity with sun position? Yes 3 43.085032 -70.804187 64.54 14.00 78.54 Correlate slope error with surface type? Yes 4 20.17 Slope error: 8.43 mrad 43.085084 -70.804291 66.68 86.85



Name: CRPRT2 Footprint area: 0.26 acre Axis tracking: Fixed (no rotation)	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Tilt: 0.0 deg Orientation: 124.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.085519	-70.803626	57.88	22.48	80.36
Panel material: Smooth glass with AR coating	2	43.085431	-70.803461	56.75	14.00	70.75
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084981	-70.803912	58.98	14.00	72.98
Slope error: 8.43 mrad	4	43.085070	-70.804083	59.73	22.48	82.20



Name: CRPRT3 Footprint area: 0.23 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Latitude	Longitude	Ground elevation	Height above ground	Total elevation
deg	deg	ft	ft	ft
43.085400	-70.803418	56.90	22.48	79.38
43.085325	-70.803271	56.23	14.00	70.23
43.084876	-70.803716	58.56	14.00	72.56
43.084953	-70.803866	59.01	22.48	81.49
	deg 43.085400 43.085325 43.084876	deg deg 43.085400 -70.803418 43.085325 -70.803271 43.084876 -70.803716	deg deg ft 43.085400 -70.803418 56.90 43.085325 -70.803271 56.23 43.084876 -70.803716 58.56	deg deg ft ft 43.085400 -70.803418 56.90 22.48 43.085325 -70.803271 56.23 14.00 43.084876 -70.803716 58.56 14.00

Name: CRPRT4 Footprint area: 0.13 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 124.0 deg

Rated power: -

Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: CRPRT5 Footprint area: 0.07 acre Axis tracking: Fixed (no rotation) Tilt: 0.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Name: LGBLDG Footprint area: 2.0 acres Axis tracking: Fixed (no rotation) Tilt: 15.0 deg Orientation: 214.0 deg

Rated power: -Panel material: Smooth glass with AR coating Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes Slope error: 8.43 mrad



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085298	-70.803223	56.02	20.17	76.19
2	43.085253	-70.803139	56.21	14.00	70.21
3	43.084808	-70.803572	58.45	14.00	72.45
4	43.084851	-70.803658	58.35	20.17	78.52

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.085549	-70.803405	56.86	20.17	77.02
2	43.085404	-70.803116	55.16	20.17	75.32
3	43.085334	-70.803188	55.25	14.00	69.25
4	43.085478	-70.803470	57.01	14.00	71.01

Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084344	-70.802133	51.60	93.83	145.44
2	43.084054	-70.801543	49.18	93.83	143.01
3	43.083901	-70.801690	49.39	93.83	143.22
4	43.083859	-70.801609	49.20	93.83	143.03
5	43.083897	-70.801574	49.27	93.83	143.10
6	43.083839	-70.801453	47.35	93.83	141.18
7	43.083345	-70.801919	51.93	93.83	145.76
8	43.083906	-70.803019	59.40	93.83	153.23
9	43.084395	-70.802537	54.24	93.83	148.07
10	43.084315	-70.802368	51.53	93.83	145.36
11	43.084337	-70.802347	51.04	93.83	144.87
12	43.084303	-70.802278	52.48	93.83	146.31
13	43.084336	-70.802245	52.51	93.83	146.34
14	43.084297	-70.802171	51.69	93.83	145.52

Name: SMBLDG Footprint area: 0.22 acre	Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
Axis tracking: Fixed (no rotation) Tilt: 15.0 deg Orientation: 214.0 deg		deg	deg	ft	ft	ft
Rated power: -	1	43.084480	-70.803051	56.19	88.00	144.19
Panel material: Smooth glass with AR coating	2	43.084450	-70.803081	56.31	88.00	144.31
Vary reflectivity with sun position? Yes Correlate slope error with surface type? Yes	3	43.084506	-70.803193	56.74	88.00	144.74
Slope error: 8.43 mrad	4	43.084466	-70.803232	56.81	88.00	144.81
	5	43.084412	-70.803118	56.55	88.00	144.55
	6	43.084252	-70.803275	58.91	88.00	146.91
	7	43.084414	-70.803594	61.58	88.00	149.58
E M F.M.	8	43.084643	-70.803375	58.79	88.00	146.79

Route Receptor(s)

Name: Route 1 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082607	-70.800659	43.16	4.50	47.66
2	43.082965	-70.800254	39.75	4.50	44.25
3	43.084118	-70.798835	40.69	4.50	45.19

Name: Route 2 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.084096	-70.798795	40.76	8.50	49.26
2	43.082949	-70.800223	39.72	8.50	48.22
3	43.082597	-70.800616	42.88	8.50	51.38

Name: Route 3 Route type Two-way View angle: 50.0 deg



Vertex Latitude Longitude Ground elevation Height above ground Total elevation ft ft ft deg deg 43.085442 -70.804811 63.97 4.50 68.47 1 2 43.084962 -70.804519 67.50 4.50 72.00 3 43.084962 -70.804519 72.00 67.50 4.50 4 43.084630 -70.804302 69.07 4.50 73.57 5 -70.804302 73.57 43.084630 69.07 4.50 6 43.084394 -70.804068 68.75 4.50 73.25 7 43.083881 -70.803489 64.40 4.50 68.90 8 43.083614 -70.803103 60.85 4.50 65.35

Name: Route 4 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.083602	-70.803135	60.76	8.50	69.26
2	43.083841	-70.803542	64.38	8.50	72.88
3	43.084382	-70.804111	68.76	8.50	77.26
4	43.084618	-70.804339	69.09	8.50	77.59
5	43.084618	-70.804339	69.09	8.50	77.59
6	43.084888	-70.804519	67.86	8.50	76.36
7	43.084888	-70.804519	67.86	8.50	76.36
8	43.085416	-70.804830	64.17	8.50	72.67

Name: Route 5 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082313	-70.799503	41.53	4.50	46.03
2	43.082995	-70.798326	37.86	4.50	42.36

Name: Route 6 Route type Two-way View angle: 50.0 deg



Vertex	Latitude	Longitude	Ground elevation	Height above ground	Total elevation
	deg	deg	ft	ft	ft
1	43.082966	-70.798285	37.86	8.50	46.36
2	43.082274	-70.799457	41.51	8.50	50.01

Discrete Observation Receptors

Number	Latitude	Longitude	Ground elevation	Height above ground	Total Elevation
	deg	deg	ft	ft	ft
1-ATCT	43.084384	-70.818882	89.93	130.00	219.93
OP 2	43.082455	-70.800057	42.02	20.00	62.02
OP 3	43.082529	-70.799934	41.99	30.00	71.99
OP 4	43.083085	-70.799471	39.01	6.00	45.01
OP 5	43.083191	-70.799294	38.75	15.00	53.75
6-ATCT	43.084349	-70.818856	89.97	120.00	209.97
OP 7	43.083343	-70.803962	70.10	40.00	110.10

1-ATCT map image



6-ATCT map image



Obstruction Components

Name: BLDG2 Upper edge height: 20.0 ft	Vertex	Latitude	Longitude	Ground elevation
		deg	deg	ft
	1	43.084955	-70.806346	99.52
	2	43.085031	-70.806408	98.08
	3	43.084866	-70.806801	99.55
	4	43.084555	-70.806565	99.98
	5	43.084608	-70.806439	99.85
A CARLES CONTRACTOR	6	43.084444	-70.806325	99.64
	7	43.084592	-70.806011	99.08
	8	43.084965	-70.806346	99.43

Name: HighEdge1 Upper edge height: 22.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085534	-70.803609	57.89
2	43.085267	-70.803116	55.50

Name: HighEdge2 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085593	-70.803598	57.75
2	43.085019	-70.804161	63.07

Name: HighEdge3 Upper edge height: 22.5 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085424	-70.803445	56.71
2	43.084960	-70.803895	59.16

Name: HighEdge4 Upper edge height: 20.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085307	-70.803260	56.28
2	43.084860	-70.803684	58.42

Name: PRPT1 Upper edge height: 93.2 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084674	-70.803390	58.96
2	43.084478	-70.802983	56.11
3	43.084211	-70.803240	59.29
4	43.084415	-70.803648	62.46
5	43.084674	-70.803390	58.96

Name: PRPT2 Upper edge height: 99.3 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084580	-70.802457	53.31
2	43.083953	-70.801212	46.09
3	43.083224	-70.801856	52.36
4	43.083866	-70.803165	61.10
5	43.084580	-70.802457	53.31

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and the	1.48		

Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085164	-70.808848	82.83
2	43.085454	-70.807942	81.22
3	43.085373	-70.807765	82.86
4	43.085040	-70.807564	86.97

Name: Trees Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083891	-70.811509	72.86
2	43.084095	-70.811240	67.62

Name: Trees Upper edge height: 17.0 ft



Vertex	Latitude	Longitude	Ground elevation	
	deg	deg	ft	
1	43.085036	-70.807176	92.20	_
2	43.084131	-70.806567	95.41	

Name: Trees1 Upper edge height: 40.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085261	-70.816979	84.00
2	43.084955	-70.816877	84.48
3	43.084477	-70.817247	78.24

Name: Trees2 Upper edge height: 60.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084443	-70.818109	84.34
2	43.084602	-70.818167	84.74
3	43.084354	-70.818474	88.75

Name: Trees3 Upper edge height: 100.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084287	-70.810576	72.89
2	43.084550	-70.810195	75.28
2			

Name: Trees4 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085793	-70.815175	77.90
2	43.085354	-70.814585	81.00
3	43.086098	-70.812858	77.64

Name: Trees5 Upper edge height: 45.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.084411	-70.807233	89.30
2	43.084554	-70.807316	89.33
3	43.084677	-70.807358	89.54
4	43.084730	-70.807552	87.97

Name: Trees6 Upper edge height: 20.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085286	-70.814633	80.07
2	43.083793	-70.813418	79.96

Name: Trees7 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.083527	-70.812571	74.50
2	43.083829	-70.811932	72.49

Name: WRHSE1 Upper edge height: 30.0 ft



Vertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
1	43.085129	-70.813496	81.26
2	43.085227	-70.813254	81.50
3	43.085137	-70.813085	81.35
4	43.084986	-70.813064	81.23
5	43.084886	-70.813292	81.62
6	43.085129	-70.813496	81.26

Name: WRHSE2 Upper edge height: 30.0 ft



/ertex	Latitude	Longitude	Ground elevation
	deg	deg	ft
	43.084916	-70.813107	81.43
	43.084740	-70.813499	81.62
	43.084705	-70.813466	81.64
	43.084630	-70.813662	81.71
	43.084174	-70.813292	81.76
	43.084399	-70.812785	81.68
	43.084501	-70.812860	81.70
	43.084540	-70.812758	81.66
	43.084916	-70.813107	81.43

Summary of PV Glare Analysis

PV configuration and total predicted glare

PV Name	Tilt	Orientation	"Green" Glare "Yellow" Glare		Energy Produced	Data File
	deg	deg	min	min	kWh	
CRPRT1	0.0	124.0	0	0	-	-
CRPRT2	0.0	124.0	0	0	-	-
CRPRT3	0.0	124.0	236	0	-	-
CRPRT4	0.0	124.0	566	0	-	-
CRPRT5	0.0	214.0	0	0	-	-
LGBLDG	15.0	214.0	0	0	-	-
SMBLDG	15.0	214.0	0	0	-	-

Distinct glare per month

Excludes overlapping glare from PV array for multiple receptors at matching time(s)

PV	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec
crprt3 (green)	0	87	0	0	0	0	0	0	0	85	0	0
crprt3 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0
crprt4 (green)	0	139	48	0	0	0	0	0	0	186	0	0
crprt4 (yellow)	0	0	0	0	0	0	0	0	0	0	0	0

PV & Receptor Analysis Results

Results for each PV array and receptor

CRPRT1 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT2 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

CRPRT3 low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	79	0
Route: Route 4	157	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT3: 1-ATCT

No glare found

CRPRT3: OP 2

No glare found

CRPRT3: OP 3

No glare found

CRPRT3: OP 4

No glare found

CRPRT3: OP 5

No glare found

CRPRT3: 6-ATCT

No glare found

CRPRT3: OP 7

No glare found

CRPRT3: Route 1

No glare found

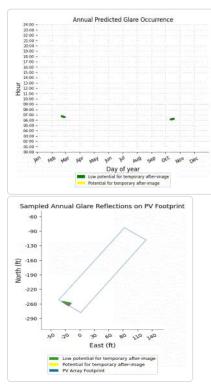
CRPRT3: Route 2

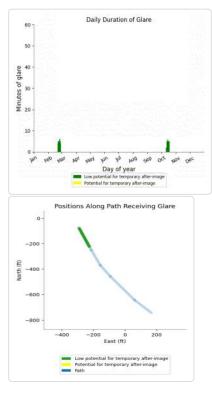
No glare found

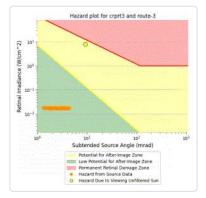
CRPRT3: Route 3

PV array is expected to produce the following glare for this receptor:

- 79 minutes of "green" glare with low potential to cause temporary after-image. 0 minutes of "yellow" glare with potential to cause temporary after-image. •

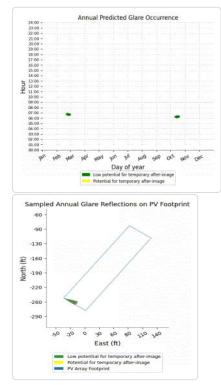


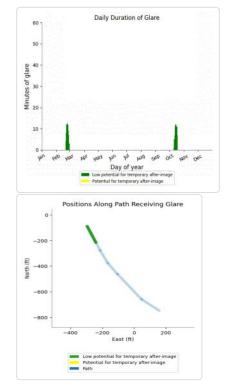


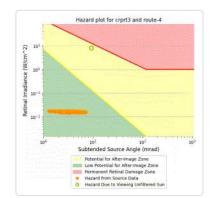


CRPRT3: Route 4

- PV array is expected to produce the following glare for this receptor: 157 minutes of "green" glare with low potential to cause temporary after-image.
 - 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT3: Route 5

No glare found

CRPRT3: Route 6

No glare found

CRPRT4 low potential for temporary after-image

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	311	0
Route: Route 4	255	0
Route: Route 5	0	0
Route: Route 6	0	0

CRPRT4: 1-ATCT

No glare found

CRPRT4: OP 2

No glare found

CRPRT4: OP 3

No glare found

CRPRT4: OP 4

No glare found

CRPRT4: OP 5

No glare found

CRPRT4: 6-ATCT

No glare found

CRPRT4: OP 7

No glare found

CRPRT4: Route 1

No glare found

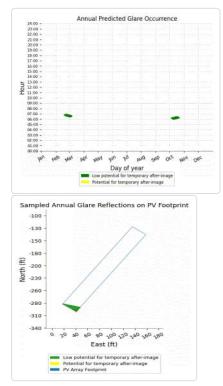
CRPRT4: Route 2

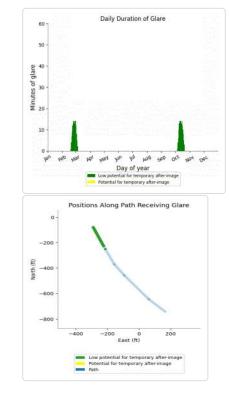
No glare found

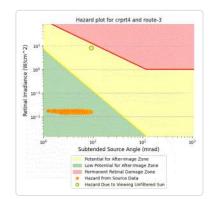
CRPRT4: Route 3

PV array is expected to produce the following glare for this receptor:

- 311 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.



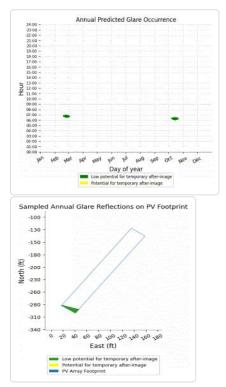


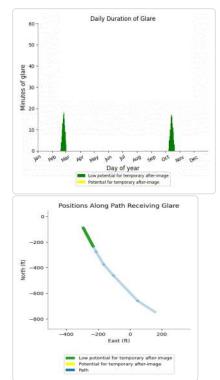


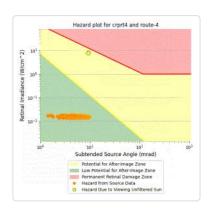
CRPRT4: Route 4

PV array is expected to produce the following glare for this receptor:

- 255 minutes of "green" glare with low potential to cause temporary after-image.
- 0 minutes of "yellow" glare with potential to cause temporary after-image.







CRPRT4: Route 5

No glare found

CRPRT4: Route 6

No glare found

CRPRT5 no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

LGBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

SMBLDG no glare found

Component	Green glare (min)	Yellow glare (min)
OP: 1-ATCT	0	0
OP: OP 2	0	0
OP: OP 3	0	0
OP: OP 4	0	0
OP: OP 5	0	0
OP: 6-ATCT	0	0
OP: OP 7	0	0
Route: Route 1	0	0
Route: Route 2	0	0
Route: Route 3	0	0
Route: Route 4	0	0
Route: Route 5	0	0
Route: Route 6	0	0

No glare found

Assumptions

- Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
- Glare analyses do not automatically account for physical obstructions between reflectors and receptors. This includes buildings, tree cover and geographi obstructions.
- Detailed system geometry is not rigorously simulated.
- The glare hazard determination relies on several approximations including observer eye characteristics, angle of view, and typical blink response time. Actual values and results may vary.
- The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
- Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for larg
 PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare.
- The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
- Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, no discrete, spectrum.
- · Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
- Refer to the Help page for detailed assumptions and limitations not listed here.



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Findings of Fact | Wetland Conditional Use Permit City of Portsmouth Planning Board

Date: July 18, 2024 Property Address: 50 Andrew Jarvis Dr. Application #: LU-24-50 Decision: Approve Deny Approve with Conditions

Findings of Fact:

Per RSA 676:3, I: The local land use board shall issue a final written decision which either approves or disapproves an application for a local permit and make a copy of the decision available to the applicant. The decision shall include specific written findings of fact that support the decision. Failure of the board to make specific written findings of fact supporting a disapproval shall be grounds for automatic reversal and remand by the superior court upon appeal, in accordance with the time periods set forth in RSA 677:5 or RSA 677:15, unless the court determines that there are other factors warranting the disapproval. If the application is not approved, the board shall provide the applicant with written reasons for the disapproval. If the application of all conditions necessary to obtain final approval.

Ordinanc	e.		
	Zoning Ordinance Sector 10.1017.50 Criteria for Approval	Finding (Meets Criteria for Approval)	Supporting Information
1	1. The land is reasonably suited to the use activity or alteration.	Meets Does Not Meet	This area is already heavily used as a recreation area for high school students and other recreation leagues. The addition of baseball/softball equipment will allow for more teams to utilize the space.
2	2. There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use, activity or alteration.	Meets Does Not Meet	While there is an alternative location in this area that would create minimal disturbance and be outside the buffer, it would create a safety hazard due to its proximity to buildings and parking areas. The chosen location within the buffer is already used as a recreational field and it does not receive any harmful maintenance such as fertilizer or chemical use, only occasional mowing. The conversion to a baseball/softball field will not change how the buffer has been used historically.

In order to grant Wetland Conditional Use permit approval the Planning Board shall find the application satisfies criteria set forth in the Section 10.1017.50 (Criteria for Approval) of the Zoning Ordinance.

	Zoning Ordinance Sector 10.1017.50 Criteria for Approval	Finding (Meets Criteria for Approval)	Supporting Information
3	3. There will be no adverse impact on the wetland functional values of the site or surrounding properties.	Meets Does Not Meet	The infield mix proposed for the new field will be a permeable mix that should not have a noticeable impact on infiltration within this buffer area. The adjacent wetland is well forested and should not see an impact from this field conversion.
4	4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals.	Meets Does Not Meet	The only vegetation proposed to be removed is a portion of existing grass lawn. This will be replaced with a permeable sand/silt/clay infield mix.
5	5. The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this section.	Meets Does Not Meet	The proposal minimizes impacts to the buffer by proposing a permeable infield mix and minimal permanent equipment. On-site alternatives would require greater disturbance to areas that are not already used as recreational fields.
6	6. Any area within the vegetated buffer strip will be returned to a natural state to the extent feasible.	Meets Does Not Meet	No work is proposed within the 25' vegetated buffer.
7	Other Board Findings:		



Date: April 9, 2024

To: Wetland Conservation Committee

From: Ken Linchey, Director of Building's and Ground's

Re: Tennis Courts Walkthrough Questions

The Portsmouth High Schools Athletic Department is requesting permission to enhance the usage of one their practice fields. The softball and baseball teams are always juggling field usage between the high school fields, Granite Street softball field, Leary field, and Cough field. Making changes to this practice field will allow some relief to the scheduling and practice needs for all of Portsmouth School programs.

Project details:

- Remove 3" of sod & loam to create a skinned infield diamond.
- Replaced skinned area with a native infield softball/baseball infield mix. The mixture is made up a clay, silt, and sand.
- Installation of a backstop that would minimize softballs from being hit into the wetland.
- Backstop installation would consist of driving posts into the ground vs using concrete.

In summary, we evaluated how can we accommodate all of our programs within the original field structure year-round. We believe that this is just a slight adjustment with how we layout our field usage within the existing field structure.

Sincerely'

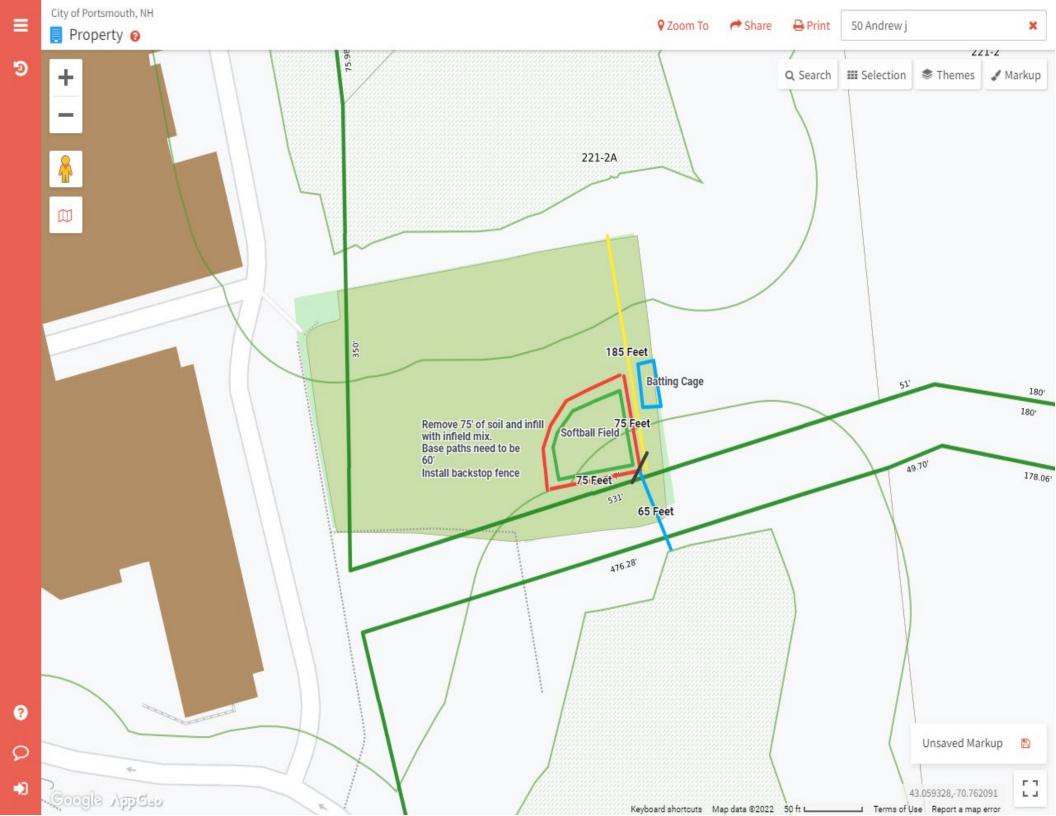
Ken Linchey

Ken Linchey Portsmouth School Department Director of Building's & Ground's

"THE PURPOSE OF THE PORTSMOUTH SCHOOLS IS TO EDUCATE ALL STUDENTS BY CHALLENGING THEM TO BECOME THINKING, RESPONSIBLE, CONTRIBUTING CITIZENS WHO CONTINUE TO LEARN THROUGHOUT THEIR LIVES,"

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Findings of Fact | Wetland Conditional Use Permit City of Portsmouth Planning Board

Date: July 18, 2024 Property Address: <u>0 Maplewood Ave.</u> Application #: LU-24-102 Decision: Approve Deny Approve with Conditions

Findings of Fact:

Per RSA 676:3, I: The local land use board shall issue a final written decision which either approves or disapproves an application for a local permit and make a copy of the decision available to the applicant. The decision shall include specific written findings of fact that support the decision. Failure of the board to make specific written findings of fact supporting a disapproval shall be grounds for automatic reversal and remand by the superior court upon appeal, in accordance with the time periods set forth in RSA 677:5 or RSA 677:15, unless the court determines that there are other factors warranting the disapproval. If the application is not approved, the board shall provide the applicant with written reasons for the disapproval. If the application of all conditions necessary to obtain final approval.

Orainance	Ordinance.				
	Zoning Ordinance Sector 10.1017.50 Criteria for Approval	Finding (Meets Criteria for Approval)	Supporting Information		
1	1. The land is reasonably suited to the use activity or alteration.	Meets Does Not Meet	This work is an in-kind repair job. The damaged wall is structurally integral to keeping the cemetery border and fill contained.		
2	2. There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use, activity or alteration.	Meets Does Not Meet	There is no alternative location to rebuild this wall in. The safety of the tomb and burials behind the wall is reliant on the structure of this wall and it must be fortified in order to prevent further erosion, or worse, collapse.		
3	3. There will be no adverse impact on the wetland functional values of the site or surrounding properties.	Meets Does Not Meet	The applicant used professional services to access the area and wall from the adjacent property, so as not to disturb the hallowed ground. This may have impacts on the pathway of any necessary construction vehicles. The applicant shall restore any disturbed soils with native wetland buffer conservation seed mix and monitor for establishment.		

In order to grant Wetland Conditional Use permit approval the Planning Board shall find the application satisfies criteria set forth in the Section 10.1017.50 (Criteria for Approval) of the Zoning Ordinance.

	Zoning Ordinance Sector 10.1017.50 Criteria for Approval	Finding (Meets Criteria for Approval)	Supporting Information
4	4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals.	Meets Does Not Meet	The natural vegetated state was disturbed in order to get construction equipment onto the site. This area should be stabilized with erosion controls, along with the wall, and should be reseeded at the end of construction with a native wetland buffer conservation seed mix.
5	5. The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this section.	Meets Does Not Meet	The alternatives to not repairing this wall would be allowing it, and the fill, and historic infrastructure to erode and/or slide into the North Mill Pond. The repair of this wall was an emergency repair.
6	6. Any area within the vegetated buffer strip will be returned to a natural state to the extent feasible.	Meets Does Not Meet	All areas disturbed within the 25' vegetated buffer shall be reseeded at the end of construction with a native wetland buffer conservation seed mix.
7	Other Board Findings:		I

City of Portsmouth

Department of Public Works

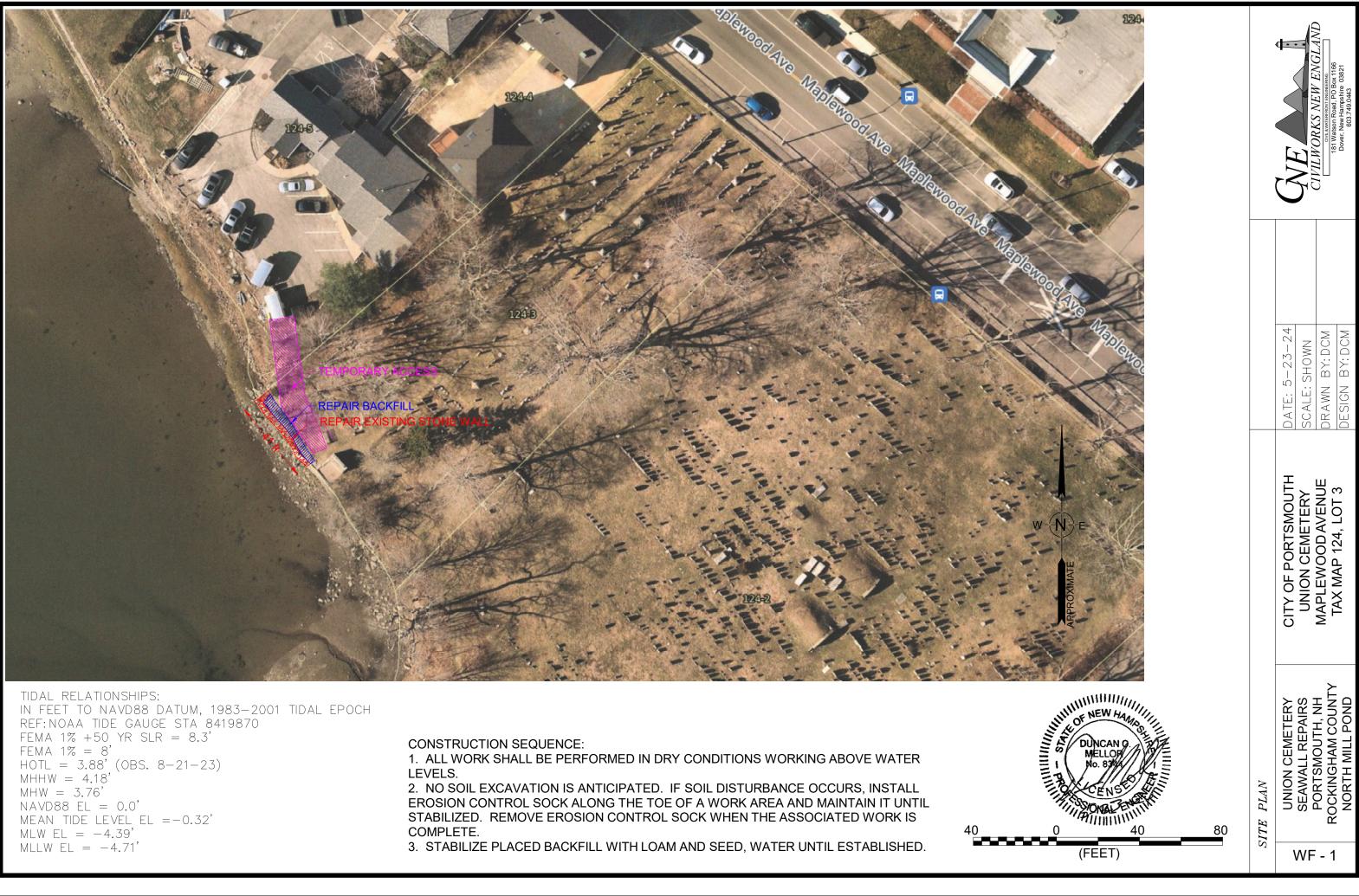
MEMORANDUM

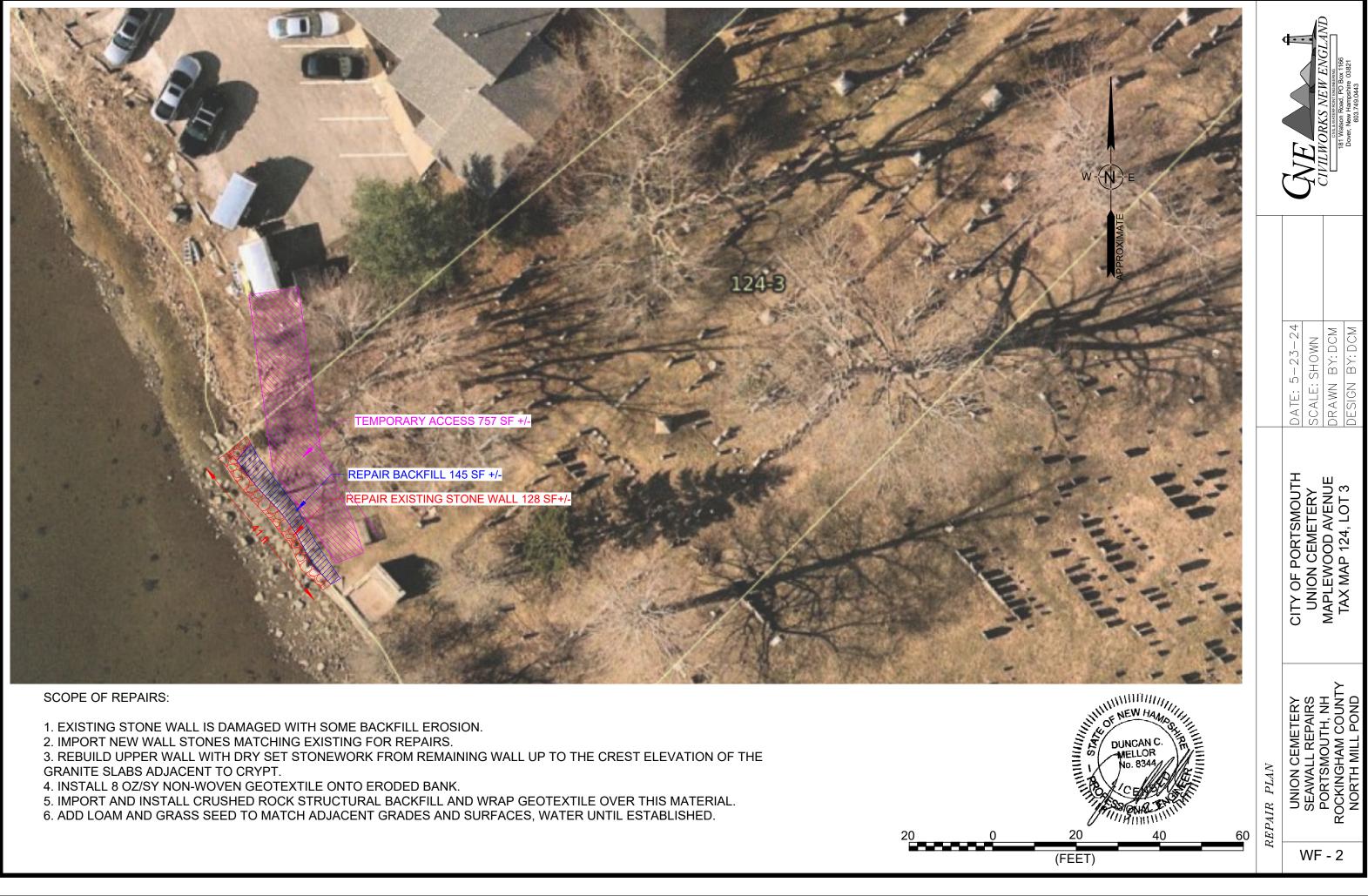
TO:	Samantha Collins, Conservation Commission Chair
CC:	Peter Britz, Director of Planning and Sustainability Kate Homet, Associate Environmental Planner
FROM:	Christine Sproviero, Project Manager
DATE:	June 7, 2024
SUBJECT:	Union Cemetery Emergency Shore Wall Repair

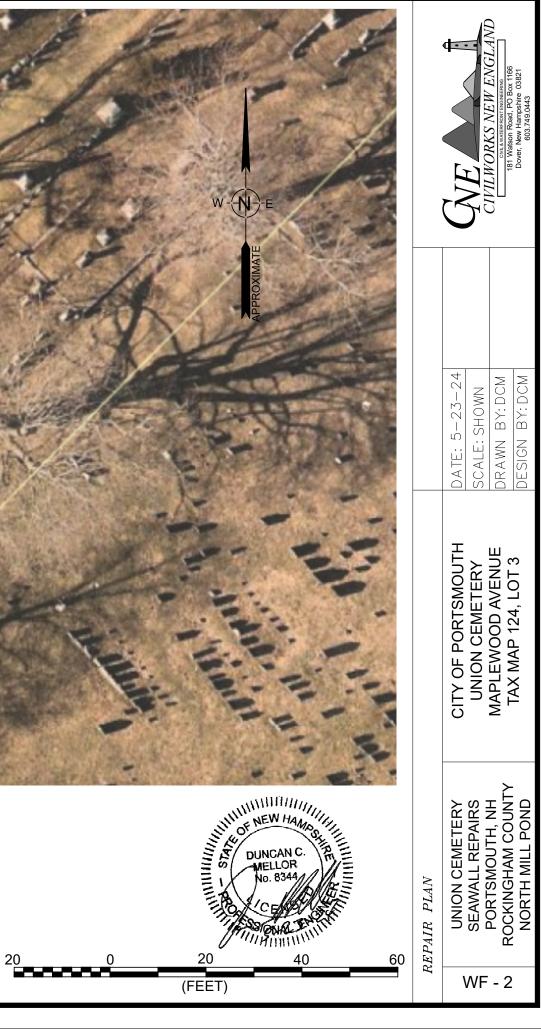
The Union Cemetery shore wall has sustained damage and erosion over multiple years due to large storm and tidal events. On 4/26/24, it was observed that multiple sections of the wall have fallen into the tidal area below. The City immediately filed a wetlands emergency authorization request to the New Hampshire Department of Environmental Services (NHDES) to perform repairs on the 41' section of shore wall, as shown in the plans attached, before further degradation occurs. The City received authorization from NHDES on 5/16/24 which is attached. Once authorization was granted, the City engaged Riverside & Pickering Marine Contractors to schedule the emergency repair "in kind" work which is scheduled to begin on 6/10/24. Following the completion of the re-construction of the wall, the City will submit post work photos as required by the Emergency Authorization.

Kind Regards,

Christine Sproviero









The State of New Hampshire Department of Environmental Services

Robert R. Scott, Commissioner



EMERGENCY AUTHORIZATION VERIFICATION

FILE NUMBER:	2024-01385
OWNER:	CITY OF PORTSMOUTH
SITE LOCATION:	UNION CEMETERY MAPLEWOOD AVE, PORTSMOUTH
AGENT/CONTRACTOR:	TBD
AUTHORIZATION DATE:	MAY 16, 2024
WATERBODY:	TIDAL BUFFER ZONE

This is to confirm that New Hampshire Department of Environmental Services (NHDES) Wetlands Bureau has given emergency authorization in accordance with NH Administrative Rule Env-Wt 315 to the owner/agent to conduct the following work in the NHDES Wetlands Bureau jurisdiction (under RSA 482-A):

DESCRIPTION: Emergency authorization for the in-kind repair to an existing retaining wall.

This authorization is subject to the following conditions:

- 1. The applicant/contractor shall file a follow up report describing the work performed under this authorization including pre-construction and post-construction photos to NHDES by June 24, 2024; the need for additional permitting will then be determined by NHDES (if no further impacts are needed).
- 2. Work shall be conducted in a manner so as to minimize turbidity and sedimentation to surface waters and wetlands.
- 3. Appropriate siltation, erosion controls, turbidity, and sedimentation controls shall be utilized.
- 4. Extreme precautions shall be taken within riparian areas to limit unnecessary removal of vegetation for access.
- 5. Construction equipment shall be inspected daily for leaking fuel, oil, and hydraulic fluid prior to working near surface waters or wetlands.
- 6. Faulty equipment shall be repaired prior to working near jurisdictional areas.
- 7. The contractor shall have appropriate oil spill kits on site and readily accessible at all times during construction and each operator shall be trained in its use.
- 8. This form shall be properly posted at the work site.
- 9. This authorization does not convey a property right, nor authorize any injury to property of others, nor invasion of rights of others.

THIS AUTHORIZATION EXPIRES ON June 17, 2024. All work must be completed by this date. This authorization has been given file number **2024-01385**. Please use this number in all future correspondence.

Signed:

& ml

Eben M. Lewis Southeast Region Supervisor Land Resources Management, Water Division

ec: Portsmouth Conservation Commission US Army Corps of Engineers (<u>Richard.C.Kristoff@usace.army.mil</u>) NH HSEM Planning (<u>hsemplanning@dos.nh.gov</u>) NHPA (<u>DOS.nhpa@dos.nh.gov</u>)

www.des.nh.gov

29 Hazen Drive • PO Box 95 • Concord, NH 03302-0095 NHDES Main Line: (603) 271-3503 • Subsurface Fax: (603) 271-6683 • Wetlands Fax: (603) 271-6588 TDD Access: Relay NH 1 (800) 735-2964

Christine R. Sproviero

From:	Christine R. Sproviero
Sent:	Wednesday, May 22, 2024 9:05 AM
То:	Duncan Mellor
Subject:	Authorization for Civilworks New England

Good morning Duncan,

Please consider this as an authorization for Civilworks New England to act as an authorized agent for the City of Portsmouth in regard to the Union Cemetery Shore Wall Project.

Regards,

Christine R. Sproviero Project Manager City of Portsmouth Public Works Department 680 Peverly Hill Road Portsmouth, NH 03801 Office: (603) 766-1755 Mobile: (603) 380-4805 Email: crSproviero@cityofportsmouth.com

CIVILWORKS NEW ENGLAND 181 WATSON ROAD P.O. BOX 1166 DOVER, NH 03821-1166 PHONE: 603.749.0443

MEMORANDUM

Date: June 25, 2024

- To: Portsmouth Planning Board
- Re: DES 2024-01385, City of Portsmouth, Union Cemetery wall repairs
- From: Duncan Mellor, PE

Civilworks New England

The damaged stone wall at Union Cemetery in Portsmouth on the bank of North Mill Pond has been repaired in-kind with dry set stonework in the Tidal Buffer Zone. All work was performed in the dry and was above and inshore of the high tide line. The disturbed lawn area was seeded with the City wetland buffer seed mix. Concurrently the project was approved by the Portsmouth Conservation Commission (letter attached).

Before Photograph:



Photo 1 Main span removal for localized member removal and observation



CIVILWORKS NEW ENGLAND 181 WATSON ROAD P.O. BOX 1166 DOVER, NH 03821-1166 PHONE: 603.749.0443

After Photographs:



Photo 2 Repaired wall looking north 6-18-24



Photo 3 Disturbed area erosion controls and seeding 6-18-24



CIVILWORKS NEW ENGLAND 181 WATSON ROAD P.O. BOX 1166 DOVER, NH 03821-1166 PHONE: 603.749.0443



Photo 4 Disturbed area erosion control matting over City wetland buffer seed mix 6-18-24.

In accordance with the Portsmouth Conservation Commission WCUP approval conditions, dated June 17, 2024, this area will be reseeded if growth is not successful, and native wetland buffer shrubs will be planted along the temporary access area.

\\cneserver2\Users\Dmellor\Documents\R&Pickering\Union Cemetery\CUP\Union cemetery completion report 6-25-24.docx





CITY OF PORTSMOUTH

Planning & Sustainability Department 1 Junkins Avenue Portsmouth, New Hampshire 03801 (603) 610-7216

CONSERVATION COMMISSION

June 17, 2024

City of Portsmouth

PO BOX 628 Portsmouth, NH 03802

RE: Wetland Conditional Use Permit for property located at 0 Maplewood Avenue

Dear Owner:

The Conservation Commission, at its regularly scheduled meeting of **Wednesday**, **June 12**, **2024**, considered your application for an after the fact Wetland Conditional Use Permit due to the emergency authorization for repair of the stone wall alongside the North Cemetery. This application is for the restoration and repair of the wall in-kind which includes installation of new stone, installing non-woven geotextile along the eroded bank, importing structural backfill, and loam and seeding the disturbed areas once finished. Said property is shown on Assessor Map 124, Lot 3 and lies within the Municipal (M). As a result of said consideration, the Commission voted to **approve** the Wetland Conditional Use Permit with the following stipulations.

1. Applicant shall monitor the success of reseeded areas to ensure stabilization. If stabilization is not successful within 30 days of seeding, the area will need to be reseeded.

2. Native wetland buffer shrub plantings shall be installed within the temporary accessway area in the Fall of 2024. This should be included in updated plan set for the Planning Board submission.

This matter will be placed on the agenda for the Planning Board meeting scheduled for **Thursday, July 18, 2024**. One (1) hard copy of any revised plans and/or exhibits as well as an updated electronic file (in a PDF format) must be filed in the Planning & Sustainability Department and uploaded to the online permit system no later than Wednesday, June 26, 2024.

The minutes and audio recording of this meeting are available by contacting the Planning & Sustainability Department.

Very truly yours,

ÇOQ

Samantha Collins, Chair Conservation Commission

cc:

Findings of Fact | Home Occupation 2 Conditional Use Permit City of Portsmouth Planning Board

Date: July 18, 2024 Property Address: <u>32 Boss Ave.</u> Application #: <u>LU-24-117</u> Decision: Approve Deny App

□ Approve with Conditions

Findings of Fact:

Per RSA 676:3, I: The local land use board shall issue a final written decision which either approves or disapproves an application for a local permit and make a copy of the decision available to the applicant. The decision shall include specific written findings of fact that support the decision. Failure of the board to make specific written findings of fact supporting a disapproval shall be grounds for automatic reversal and remand by the superior court upon appeal, in accordance with the time periods set forth in RSA 677:5 or RSA 677:15, unless the court determines that there are other factors warranting the disapproval. If the application is not approved, the board shall provide the applicant with written reasons for the disapproval. If the application of the all conditions, the board shall include in the written decision a detailed description of the all conditions necessary to obtain final approval.

Home Occupation 2 Conditional Use Permit

10.242.10 The Planning Board may grant a conditional use permit if the application is found to be in compliance with the general criteria in Section 10.243 or, if applicable, the specific standards or criteria set forth in this Ordinance for the particular use or activity.

	Home Occupation 2 Conditional Use Permit 10.243 Requirements	Finding (Meets Criteria/Requirement)	Supporting Information
1	10.243.21 The design of proposed structures, their height and scale in relation to the site's surroundings, the nature and intensity of the proposed use or activity, and the layout and design of the site will be compatible with adjacent and nearby properties, buildings and uses, will complement or enhance the character of surrounding development, and will encourage the appropriate and orderly development and use of land and buildings in the surrounding area.	Meets Does Not Meet	The home occupation will be in an existing studio which is contained within the existing dwelling.
2	10.243.22 All necessary public and private utility infrastructure	Meets	The art classes will require minimal water and electricity usage from the existing
	and services will be available and adequate to serve the	Does Not Meet	services that serve the dwelling.

	Home Occupation 2 Conditional Use Permit 10.243 Requirements	Finding (Meets Criteria/Requirement)	Supporting Information
	proposed use.		
3	10.243.23 The site and surrounding streets will have adequate vehicular and pedestrian infrastructure to serve the proposed use consistent with the City's Master Plan.	Meets Does Not Meet	There are three different routes to access the location in addition to lighted sidewalks. The property has 155 feet of street frontage. The Master Plan supports expanding opportunities for home-based businesses.
4	10.243.24 The proposed structures, uses, or activities will not have significant adverse impacts on abutting and surrounding properties on account of traffic, noise, odors, vibrations, dust, fumes, hours of operation, and exterior lighting and glare.	Meets Does Not Meet	The classes will be a few hours in length and will not have any significant adverse impact on abutting and surrounding properties on account of traffic, noise, odors, vibrations, dust, fumes, hours of operation and exterior lighting glare.
5	10.243.25 The proposed structures and uses will not have significant adverse impacts on natural or scenic resources surrounding the site, including wetlands, floodplains, and significant wildlife habitat.	Meets Does Not Meet	The art studio is fully contained within the home and will not impact the wetlands, floodplains or wildlife habitats.
6	10.243.26 The proposed use will not cause or contribute to a significant decline in property values of adjacent properties.	Meets Does Not Meet	Granting a conditional use permit to allow small art classes will be an asset to the neighborhood and will not cause a decline in property values.
6	Other Board Findings: Additional Conditions of Approv		
	Additional Conditions of Approv	<u>uı</u> .	

June 19, 2024

Rick Chellman, Chair City of Portsmouth Planning Board 1 Junkins Avenue Portsmouth, NH 03801

RE: Home Occupation 2 Request for 32 Boss Ave

Dear Mr. Chellman and members of the Planning Board:

I am requesting approval for a **Home Occupation 2 Conditional Use Permit** so I may provide small art classes (up to 6 students) in my home studio. Proposed number of classes will not exceed 1-2 classes per day and each class will generally be ~2-3 hours in length. Anticipated hours for art classes will fall between 8am-5pm M-F (as currently allowed by Home Occupation ordinance). To accommodate working adults/parents, I would like to request flexibility in offering classes in the evenings ~6-9pm 1-2 days a week and one day on the weekend.

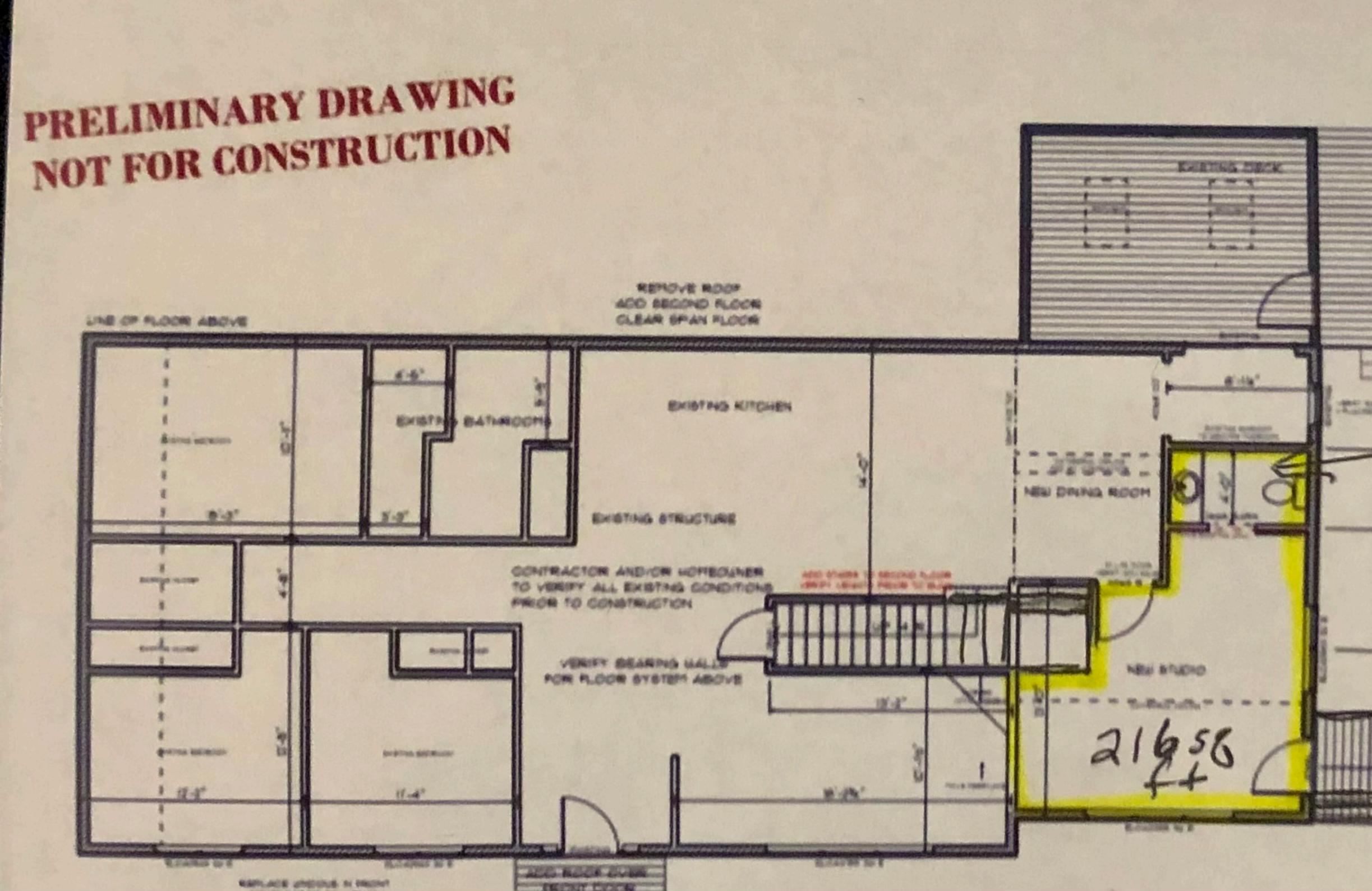
Based on current parking spot standards, 3 cars can fit at the base of our driveway in front of our garage, and if needed, 1 in the neck of our driveway (see photos marked Exhibit A). As part of this conditional use permit, I am requesting 2 additional parking spots on the street (1 is currently allowed by Home Occupation Ordinance) so I can best accommodate seniors and those with mobility challenges*. I have over 155 linear feet of open space on the street directly in front of our home (see property map) which can easily fit 7-8 cars. In addition, I will strongly encourage carpooling whenever possible and install a bike rack next to my studio entrance.

Sincerely,

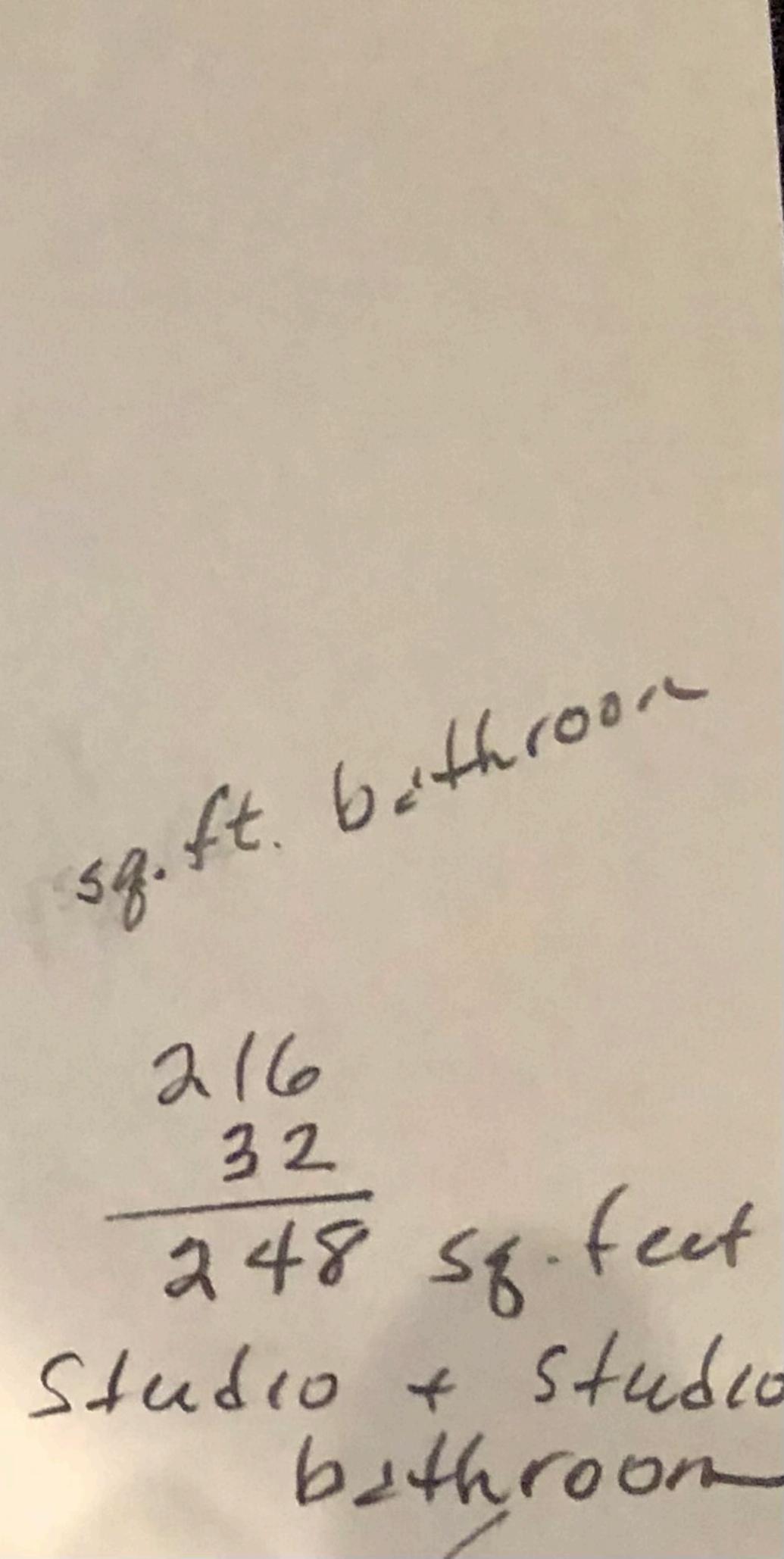
Karen Rosania 32 Boss Ave Portsmouth, NH

*Currently, we don't have a walkway extending from street to studio entrance – however, if granted a Conditional Use Permit, we will take necessary steps to have a porous brick walkway installed.





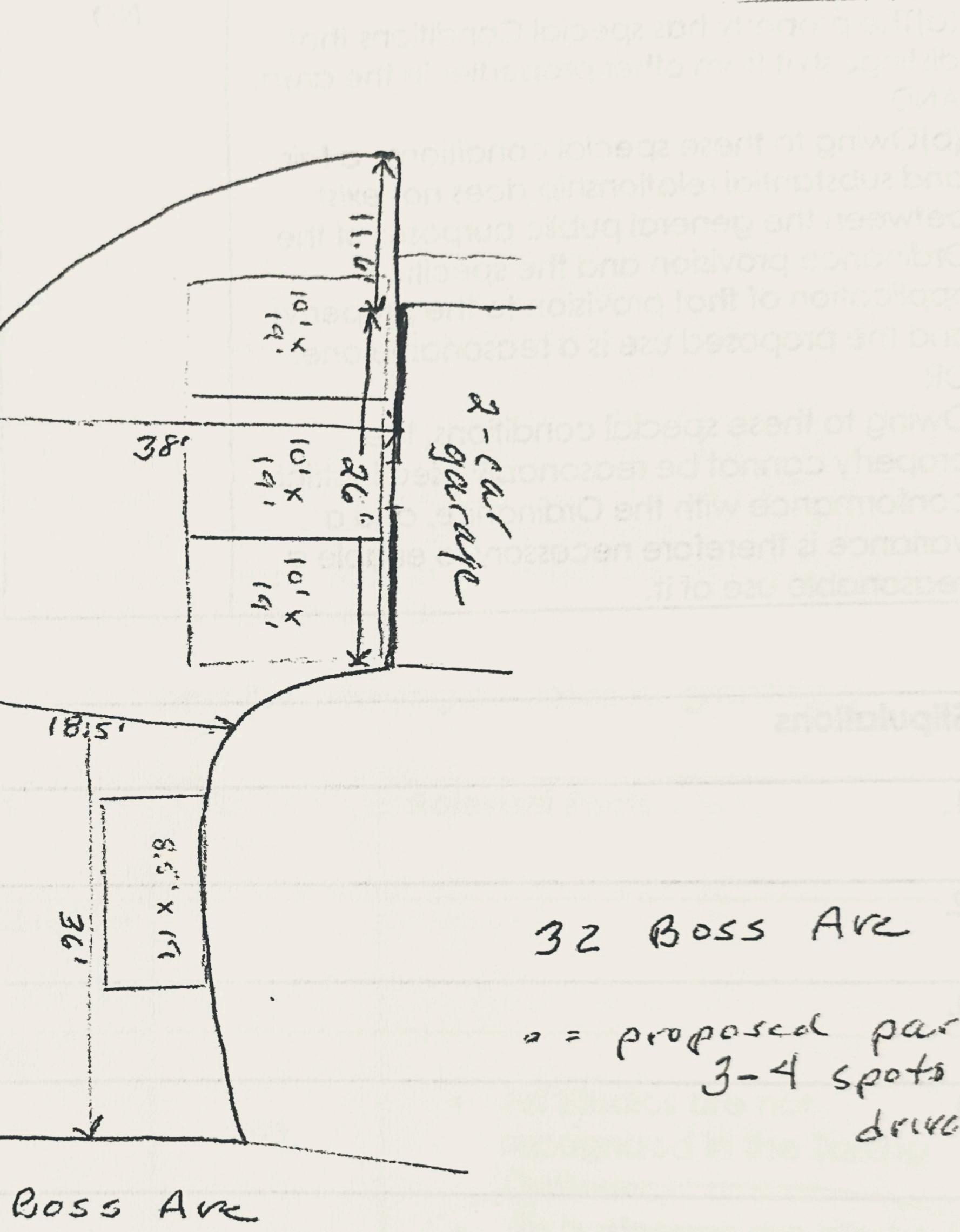
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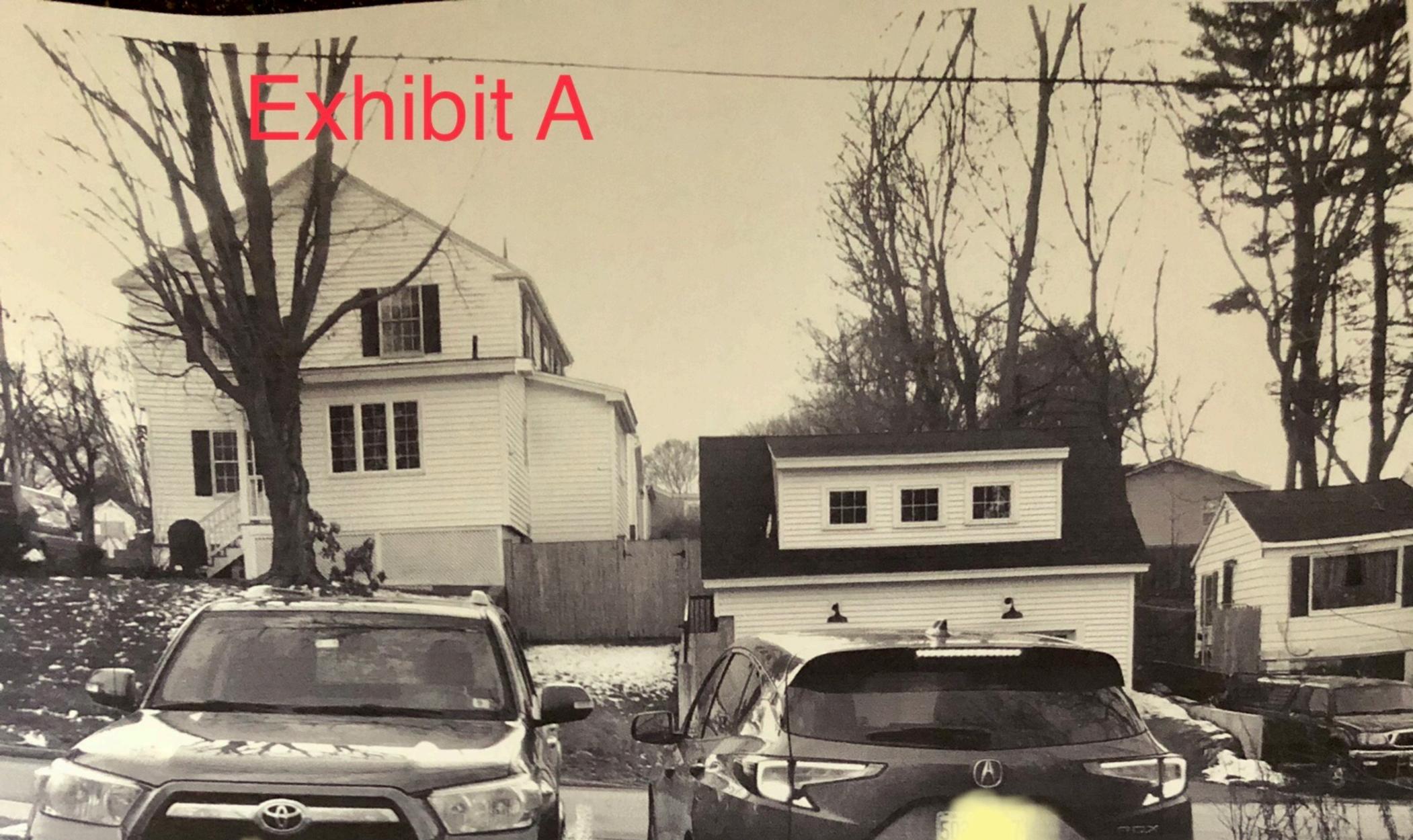
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Exhibit A



20.97 910191941 21 9 32 Boss Are = proposed parking 3-4 spots in driveway





C

Sufficient room for another car to pass



Findings of Fact | Detached Accessory Dwelling Unit City of Portsmouth Planning Board

Date: July 18. 2024 Property Address: <u>480 Dennett Street</u> Application #: <u>LU-24-120</u> Decision: Approve Deny Approve with Conditions

Findings of Fact:

Per RSA 676:3, I: The local land use board shall issue a final written decision which either approves or disapproves an application for a local permit and make a copy of the decision available to the applicant. The decision shall include specific written findings of fact that support the decision. Failure of the board to make specific written findings of fact supporting a disapproval shall be grounds for automatic reversal and remand by the superior court upon appeal, in accordance with the time periods set forth in RSA 677:5 or RSA 677:15, unless the court determines that there are other factors warranting the disapproval. If the application is not approved, the board shall provide the applicant with written reasons for the disapproval. If the application of the all conditions, the board shall include in the written decision a detailed description of the all conditions necessary to obtain final approval.

Zoning Ordinance -10.814.60: Before granting a conditional use permit for a detached ADU, the Planning Board shall make the following findings:

	Section 10.814.62	Finding (Meets Requirement/ Criteria)	Supporting Information
1	10.814.621 The ADU complies with all applicable standards of this Section 10.814 or as may be modified by the conditional use permit.	Meets Does Not Meet	The DADU complies with the standards in Section 10.814 with no requested modifications.
2	10.814.622 The exterior design of the ADU is architecturally consistent with or similar	Meets	The design of the DADU is compatible with the existing principal dwelling.
	in appearance to the existing principal dwelling on a lot.	Does Not Meet	
3	10.814.623 The site plan provides adequate and appropriate open space and landscaping for both the ADU and the principal dwelling unit and complies with the off-street parking requirements of 10.814.26.	Meets Does Not Meet	The site plan provides adequate open space and the parking on the lot will exceed the requirement for the DADU.
4	10.814.624 The ADU will maintain a compatible relationship with the character of adjacent and neighborhood properties in terms of location, design, and off-street parking layout, and will not significantly reduce the privacy of adjacent properties.	Meets Does Not Meet	The new conforming location of the DADU will be compatible with the existing neighborhood and will not reduce the privacy of adjacent properties. The DADU will be located within the existing fenced yard in a conforming location.
5	Other Board Findings:		

Planning Department City of Portsmouth

Re: 480 Dennett St

The property at 480 Dennett St is owned by the applicant and spouse. The house is occupied by the owner and family of three generations.

There is no plan for any change of ownership.

The application is for a detached ADU. The ADU will be occupied by the property owner and spouse. The primary residence will continue to be occupied by the owner's daughter and children.

There will not be a business operated from the residence per city regulations.

The property is currently connected to city water and sewer. No additional connections to city services. All connections for ADU will be provided by the primary residence.

The proposed DADU will be a one bedroom, one bathroom self contained standalone structure with separate access. All zoning requirements for lot coverage and lot line setbacks will be satisfied for an accessory structure.

There will be 4 off road parking spaces provided. There is also city planned on street parking directly in front of the residence.



Left side of backyard.

Backyard from deck.





Left side of front yard.

Right side of front yard.



DIMENSIONAL STANDARDS:

	REQUIRED:	EXISTING:	PROPOSED:
MIN. LAND AREA	7500 SQ FT	7648 SQ FT	7648 SQ FT
MIN. STREET FRONTAGE:	100'	64'	64'
MIN. LOT DEPTH:	70'	120'	120'
FRONT SETBACK:	15'	15'	15'
SIDE SETBACK:	10'	~8' (EXISTING HOUSE)	10' (ADU)
REAR SETBACK:	20'	24'	11'-4"
MAX. BUIDLING HEIGHT:	35'	15'	15'
MAX. BUILDING LENGTH:	N/A		
MAX. BUILDING FOOTPRINT:	N/A		
MAX. BUILDING COVEREAGE:	25%	18.40%	24.86%
LOT AREA/DWELLING UNIT	7500 SQ FT	7648 SQ FT	7648 SQ FT
MIN OPEN SPACE:	N/A		

Address: 480 Dennett St. Portsmouth, NH

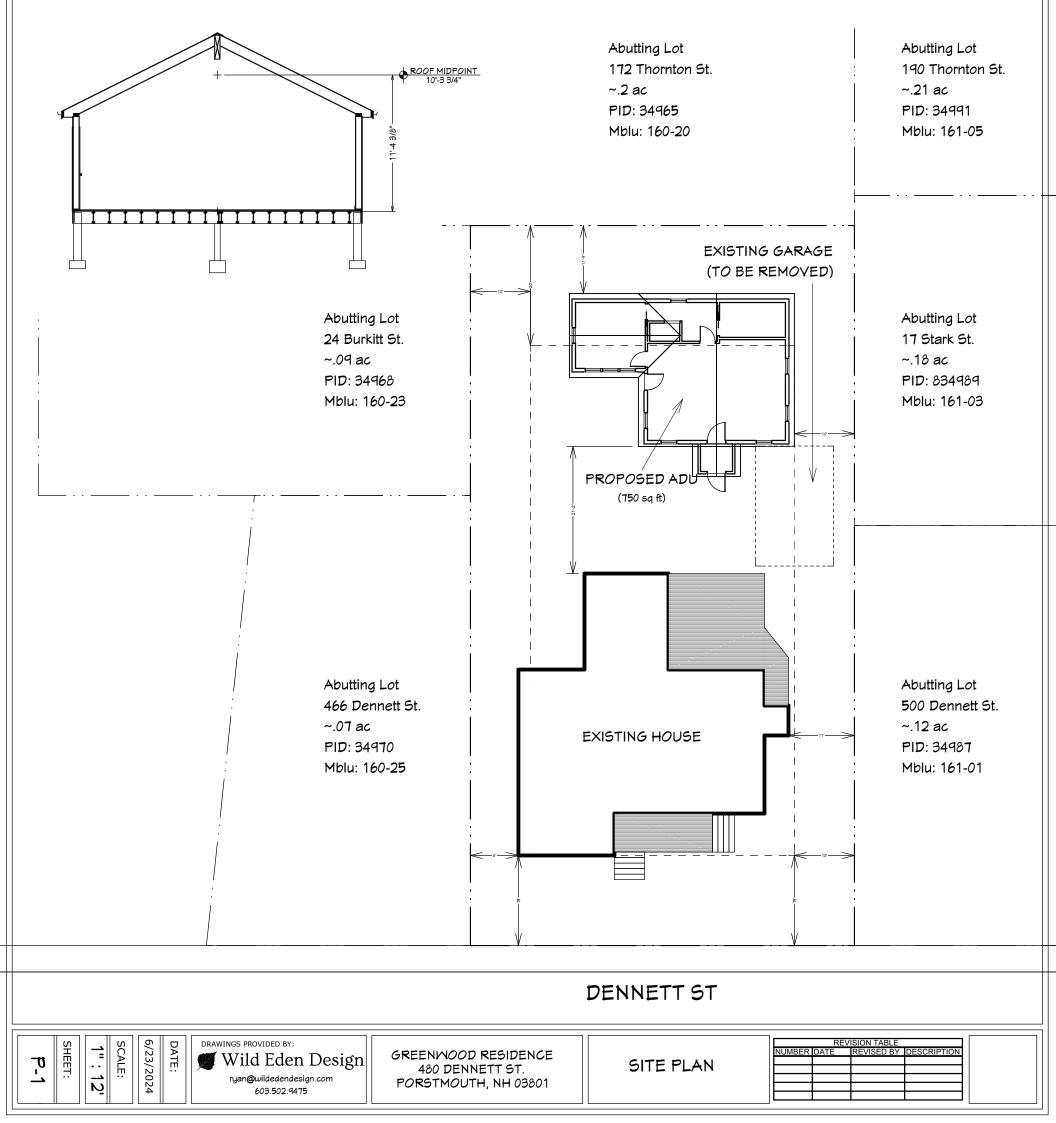
Zone: GRA

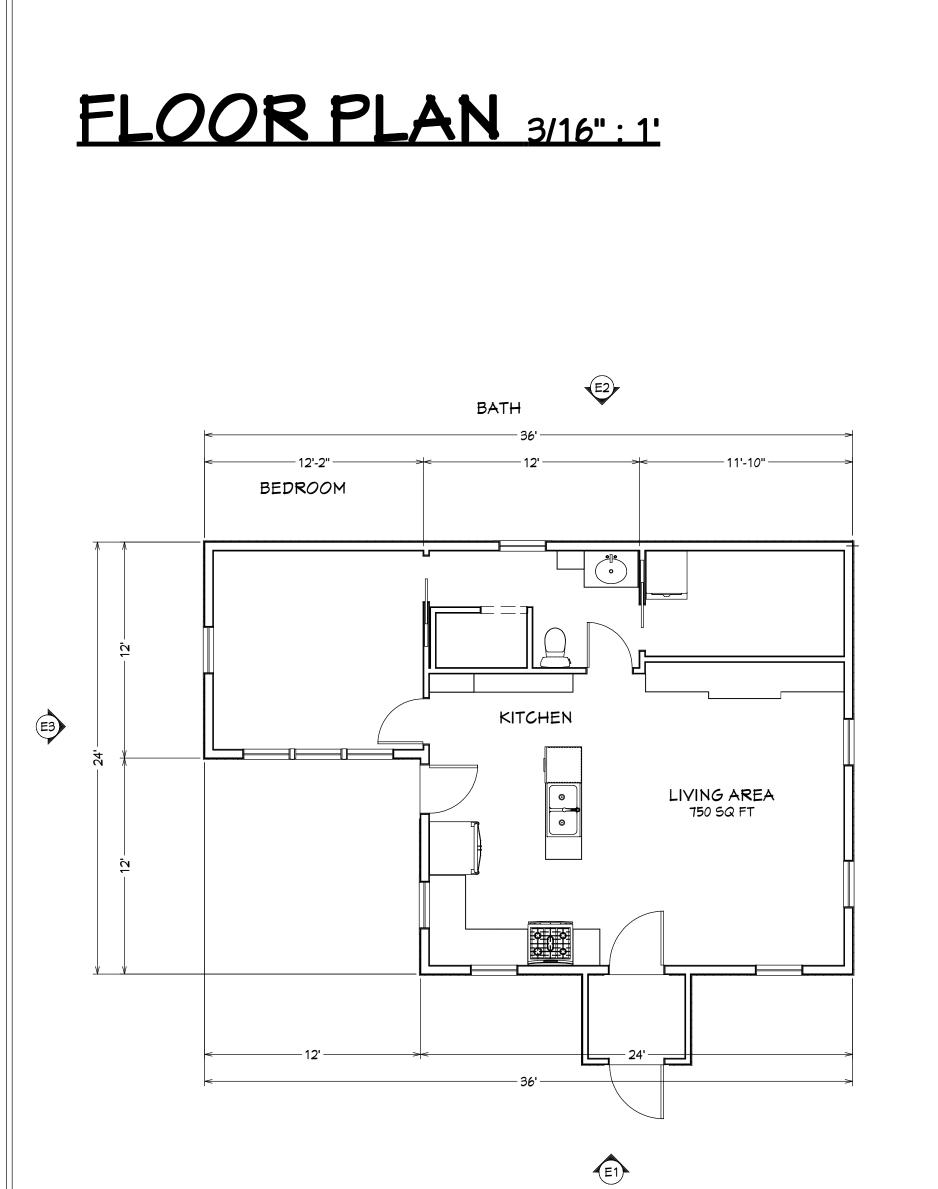
Proposal: D-ADU

Proposal area: 750 sq. ft.

Bedrooms: 1

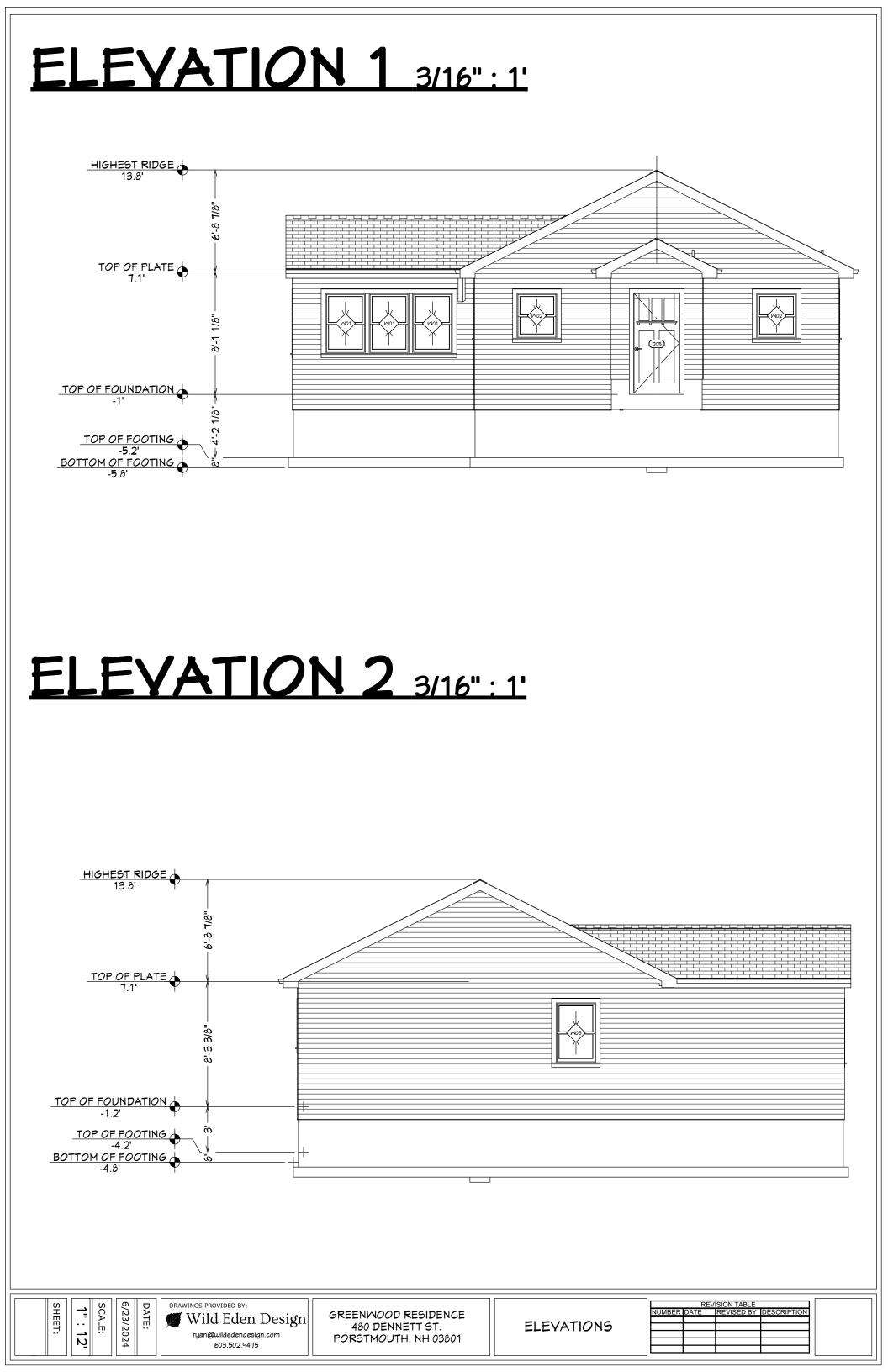
Bathrooms: 1

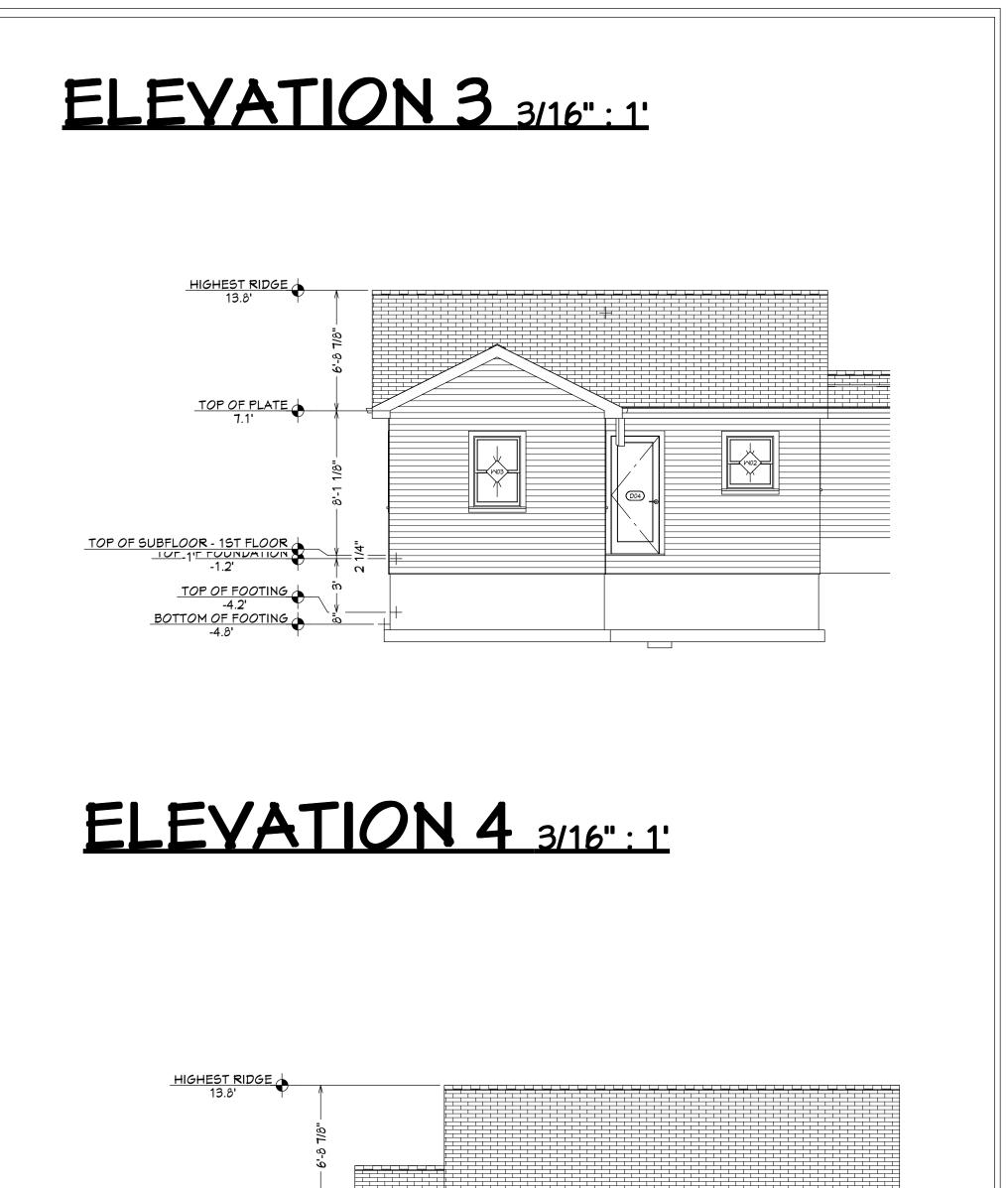


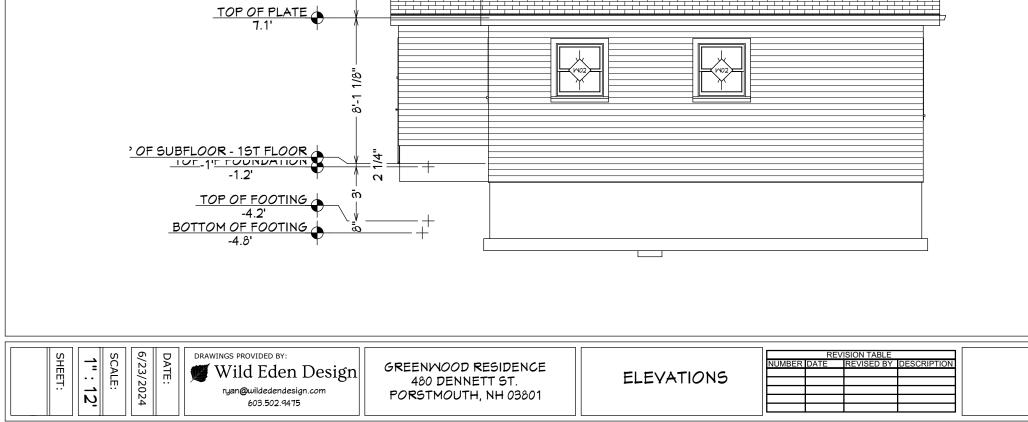


E4

SHEET: 1 SCALE: 0 DATE: Wild Eden Design: Image: Comparison of the state	A GREENWOOD RESIDENCE 480 DENNETT ST. PORSTMOUTH, NH 03801	FLOOR PLAN	REVISION TABLE NUMBER DATE REVISED BY DESCRIPTION Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2" Image: Colspan="2"







Findings of Fact | Outdoor Dining Conditional Use Permit City of Portsmouth Planning Board

Date: July 18, 2024 Property Address: 125 Brewery Lane Application #: LU-24-108 Decision: Approve Deny Approve with Conditions

Findings of Fact:

Per RSA 676:3, I: The local land use board shall issue a final written decision which either approves or disapproves an application for a local permit and make a copy of the decision available to the applicant. The decision shall include specific written findings of fact that support the decision. Failure of the board to make specific written findings of fact supporting a disapproval shall be grounds for automatic reversal and remand by the superior court upon appeal, in accordance with the time periods set forth in RSA 677:5 or RSA 677:15, unless the court determines that there are other factors warranting the disapproval. If the application is not approved, the board shall provide the applicant with written reasons for the disapproval. If the application of the all conditions, the board shall include in the written decision a detailed description of the all conditions necessary to obtain final approval.

Outdoor Dining Conditional Use Permit

10.242.10 The Planning Board may grant a conditional use permit if the application is found to be in compliance with the general criteria in Section 10.243 or, if applicable, the specific standards or criteria set forth in this Ordinance for the particular use or activity.

	Outdoor Dining Conditional Use Permit 10.243 Requirements	Finding (Meets Criteria/Requirement)	Supporting Information
1	10.243.21 The design of proposed structures, their height and scale in relation to the site's surroundings, the nature and intensity of the proposed use or activity, and the layout and design of the site will be compatible with adjacent and nearby properties, buildings and uses, will complement or enhance the character of surrounding development, and will encourage the appropriate and orderly development and use of land and buildings in the surrounding area.	Meets Does Not Meet	The proposed patio, located behind the building at 125 Brewery Lane, will consist of an approximately 470 square foot gravel patio. Seating will consist of picnic tables and bistro tables and seating. One table will be adjacent to the concrete space to allow for handicap access. Seating will consist of approximately 1-2 picnic tables and 1-3 bistro tables and chairs and/or an assortment of lawn chairs.
2	10.243.22 All necessary public and private utility infrastructure	Meets	No alteration to public and/or private utility infrastructure is required as part of
	and services will be available and adequate to serve the	Does Not Meet	the proposed use.

	Outdoor Dining Conditional Use Permit 10.243 Requirements	Finding (Meets Criteria/Requirement)	Supporting Information
	proposed use.		
3	10.243.23 The site and surrounding streets will have adequate vehicular and pedestrian infrastructure to serve the proposed use consistent with the City's Master Plan.	Meets Does Not Meet	There will be no impact to vehicular or pedestrian infrastructure as part of the proposed use of the space.
4	10.243.24 The proposed structures, uses, or activities will not have significant adverse impacts on abutting and surrounding properties on account of traffic, noise, odors, vibrations, dust, fumes, hours of operation, and exterior lighting and glare.	Meets Does Not Meet	Sufficient parking is available at the business address. Additional parking is located in nearby lots during business hours. No outdoor speakers or live music will be offered on the patio. Hours of operation are between 10am - 8pm.
5	10.243.25 The proposed structures and uses will not have significant adverse impacts on natural or scenic resources surrounding the site, including wetlands, floodplains, and significant wildlife habitat.	Meets Does Not Meet	No wetlands, floodplains, wildlife habitats, or other natural or scenic resources are present at the site of the proposed patio.
6	10.243.26 The proposed use will not cause or contribute to a significant decline in property values of adjacent properties.	Meets Does Not Meet	The proposed patio will not cause or contribute to a significant decline in property value of the adjacent properties.
6	Other Board Findings:		
7	Additional Conditions of Approve	<u>al</u> :	

Conditional Use Permit Narrative

For TREELINE OUTFITTERS 125 Brewery Lane

* 10.243.21 The design of proposed structures, their height and scale in relation to the site's surroundings, the nature and intensity of the proposed use or activity, and the layout and design of the site will be compatible with adjacent and nearby properties, buildings and uses, will complement or enhance the character of surrounding development, and will encourage the appropriate and orderly development and use of land and buildings in the surrounding area.

The proposed patio, located behind the building at 125 Brewery Lane, will consist of an approximately 470 square foot gravel patio. Seating will consist of picnic tables and bistro tables and seating. One table will be adjacent to the concrete space to allow for handicap access. Seating will consist of approximately 1-2 picnic tables and 1-3 bistro tables and chairs and/or an assortment of lawn chairs.

* 10.243.22 All necessary public and private utility infrastructure and services will be available and adequate to serve the proposed use.

No alteration to public and/or private utility infrastructure is required as part of the proposed use.

* 10.243.23 The site and surrounding streets will have adequate vehicular and pedestrian infrastructure to serve the proposed use consistent with the City's Master Plan.

There will be no impact to vehicular or pedestrian infrastructure as part of the proposed use of the space.

* 10.243.24 The proposed structures, uses, or activities will not have significant adverse impacts on abutting and surrounding properties on account of traffic, noise, odors, vibrations, dust, fumes, hours of operation, and exterior lighting and glare.

Sufficient parking is available at the business address. Additional parking is located in nearby lots during business hours. No outdoor speakers or live music will be offered on the patio. Hours of operation are between 10am - 8pm.

* 10.243.25 The proposed structures and uses will not have significant adverse impacts on natural or scenic resources surrounding the site, including wetlands, floodplains, and significant wildlife habitat.

No wetlands, floodplains, wildlife habitats, or other natural or scenic resources are present at the site of the proposed patio.

* 10.243.26 The proposed use will not cause or contribute to a significant decline in property values of adjacent properties.

The proposed patio will not cause or contribute to a significant decline in property value of the adjacent properties.



Photo 1: Existing gravel patio with concrete walkway and landscaped areas.



Photo 2: Existing gravel patio and landscaped area. The proposed plan includes a) removing the arborvitae (center of the photo) and overgrown weeds; b) laying gravel over the area with grass and overgrown weeds; and c) leaving the mulched area, lilies, and maple tree.



Photo 3: Rear of the building at 125 Brewery Lane with existing gravel patio, landscaped area, and overgrown weeds. The proposed plan includes removing the arborvitae (left) and overgrown weeds (right) and laying gravel over the area with grass and overgrown weeds. The granite curb demarcating the current grass and gravel patio will be removed.



Civil Site Planning Environmental Engineering 133 Court Street Portsmouth, NH 03801-4413

July 8, 2024

Rick Chellman, Chairman City of Portsmouth Planning Board City of Portsmouth Municipal Complex 1 Junkins Avenue Portsmouth, New Hampshire 03801

Re: Application for Preliminary/Conceptual Review Assessor's Map 222, Lot 11 550 Sagamore Avenue Altus Project No. 5591

Dear Mr. Chellman,

On behalf of Green and Company (Green), Altus Engineering, LLC (Altus) is pleased to submit an application for the Planning Board Conceptual/Preliminary Review. Green has an agreement to purchase the property located at 550 Sagamore Avenue from The Frances E. Mouflouze Revocable Trust of 2015. They are proposing to construct a new subdivision roadway to access three new residential house lots.

Enclosed is the Existing Conditions Survey Plan and the Conceptual Subdivision Plan for discussion at the July 19, 2024 Planning Board meeting.

There is a single residence on the 1.44-acre parcel. The parcel lies within the Single Resident B Zoning District which has a minimum 15,000 SF lot size requirement. By area, the parcel can support 4-homes. Multiple dwelling units on a lot is not permitted in the zone. The current Owner applied for variances on two occasions to allow 4 then 3 dwelling units on the parcel without subdivision with the concept to preserve and protect the majority of the forested area. The Board of Adjustment denied the variances in both scenarios leaving the only viable alternative to develop the parcel as a conventional subdivision.

The majority of the parcel is forested with some ledge outcrops. There is a small wetland system along the northerly boundary that is not a vernal pool and does not require any buffer protection. Enclosed is documentation from Joseph Noel, Wetlands Scientist, confirming the wetland status.

We are proposing to construct a private 40-foot wide with a 20-foot-wide paved surface roadway to access the lots. All of the lots will be accessed from the new private street. A homeowner's

association will maintain the roadway and stormwater management system. The lots will be serviced with municipal water and sewer.

On June 11th, we presented the proposal to the Technical Advisory Committee to obtain their feedback and input. They gave us guidance on the technical aspects of the design should we decide to proceed with permitting.

We look forward to getting input from the Board. Please feel free to call or email me directly should you have any questions or need any additional information in advance of the meeting.

Sincerely,

ALTUS ENGINEERING, LLC

110

Enclosures

eCopy: Michael Green Jenna Green

wde/5591.00 7-8-24 cvr ltr.docx

Letter of Authorization

I/We, <u>Ted W Alex and Patricia Cameron</u> trustees of <u>The Frances E Mouflouze Revocable Trust</u> of 2015 u/d/t dated September 24, 2015, as owner of certain real property situated in <u>Portsmouth, NH</u> further described <u>1.48 +/- acres of land with single family home located at 550 Sagamore Avenue with</u> <u>140' of frontage on Sagamore Avenue, as shown in Tax Assessors Map 222 Lot 11 and further defined</u> <u>by legal description found at the Rockingham County Registry of Deeds Book 5660 Page 2227 dated</u> <u>October 7th, 2015. (hereinafter, "Property")</u> do hereby authorize Green & Company Building and Development Corp. and its Affiliates, Agents, Assigns and Engineers to act on my/our behalf and to appear before the zoning board of adjustment and/or the planning board of said city/town and/or any of its boards or commissions, in my/our behalf for the purpose of seeking any regulatory relief that may be requested by the person I/we have above authorized, including variances, special exceptions, dimensional waivers, site plan approval, lot line adjustment approval and subdivision approval, hereby ratifying any actions taken by him/her/them to obtain any such relief. I/We authorize Green & Company Building and Development Corp. and its Affiliates, Agents, Assigns and Engineers to act in my/our behalf in all matters concerning the development and approval process, without limitation, for the above stated property, to include any required signatures.

I/We shall cooperate fully with Green & Company Building and Development Corp. and its Affiliates, Agents, Assigns and Engineers in seeking timely public approvals and for the completion of the sale contemplated herein. I/We agree to use my/our good faith efforts to provide any assistance I/we reasonably can to Green & Company Building and Development Corp. and its Affiliates, Agents, Assigns and Engineers throughout the development process, including but not limited to signing permit applications as needed.

DocuSigned by: Sharon L. Hartford

Witness

DocuSigned by: Sharon L. Hartford

DocuSigned by: Oment

DocuSigned by:

5/29/2024

5/29/2024

Date

Witness

Owner:

Owner:

Date

JOSEPH W. NOEL P.O. BOX 174 SOUTH BERWICK, MAINE 03908 (207) 384-5587

CERTIFIED SOIL SCIENTIST * WETLAND SCIENTIST * LICENSED SITE EVALUATOR

June 15, 2024

Mr. Eric D. Weinrieb, P.E. Altus Engineering 133 Court Street Portsmouth, New Hampshire 03801

RE: Wetland Delineation, 550 Sagamore Avenue, Portsmouth, New Hampshire, JWN #24-58

Dear Eric:

On May 10, 2024, an on-site was made to the above-referenced property (per your request). The purpose was to determine if there were any areas on the lot that would classify as a wetland. A residential home is situated near Sagamore Avenue with the eastern side of the lot being wooded with sporadic bedrock outcrops. One small isolated basin, centrally located on the northern property line did qualify as a wetland. Six sequentially numbered pink and black striped flags (labelled EOW1 thru EOW6) were placed along the wetland-upland boundary.

To determine the wetland boundary, the methodologies in the U.S. Army Corps of Engineers document Corps of Engineers Wetlands Delineation Manual (1987) along with the required Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Northcentral and Northeast Region, (Version 2.0) were used. Wetlands were identified based on soils, vegetation, and hydrology. Except in special cases, all three factors (hydric soils, hydrophytic vegetation, and wetland hydrology) must be present for an area to classify as wetland.

The wetland area was not ponded with surface water on the day of the site visit. There was evidence of occasional surface water (i.e., water marks) along with blackened leaves and orientated pine needles on the soil surface. The lack of surface water eliminated this area, in my opinion, from being a potential vernal pool. There appears to be a limited watershed that contributes run-off to this basin. Also, there is some evidence that the abutting lot has added fill material that may have blocked the natural runoff from this basin to downslope areas. To be a viable vernal pool surface water needs to be present in the early spring and the hydroperiod needs to be long enough for the breeding amphibians to complete the early life cycle to a juvenile age. This spring there were a number of rain events that filled most vernal pools and this basin did not contain water on May 10, 2024.

This basin does classify as a wetland based on: the poorly drained soil conditions (i.e., hydric soils), evidence of soil saturation and occasional ponding (evidence of wetland hydrology), and

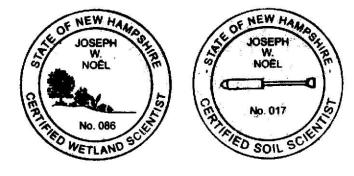
while vegetation was limited in the basin, a few red maples (*Acer* rubrum) were observed (i.e., hydrophytic vegetation).

I hope this letter is sufficient for your planning purposes. Please do not hesitate to call with any questions or concerns.

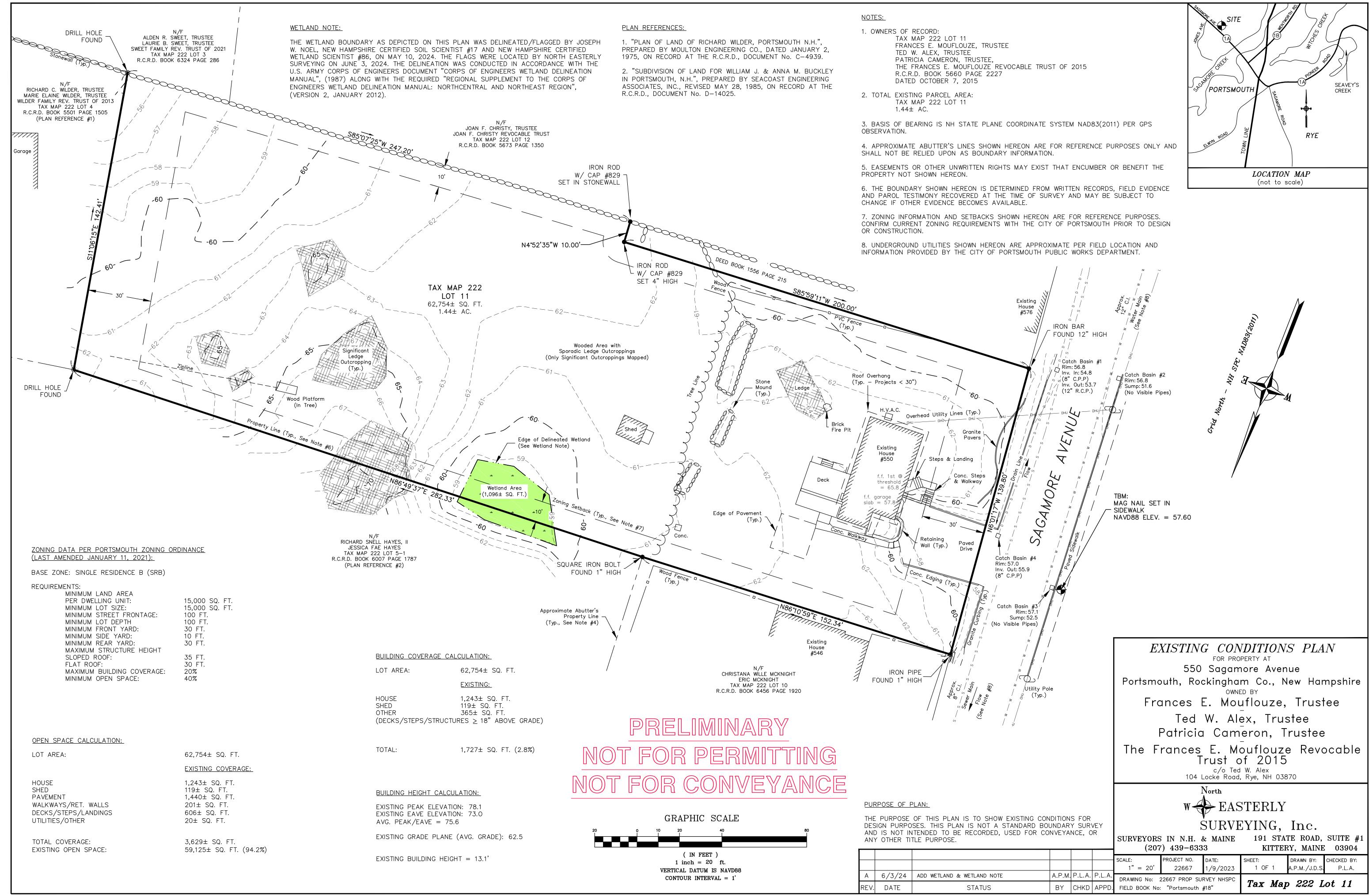
Sincerely,

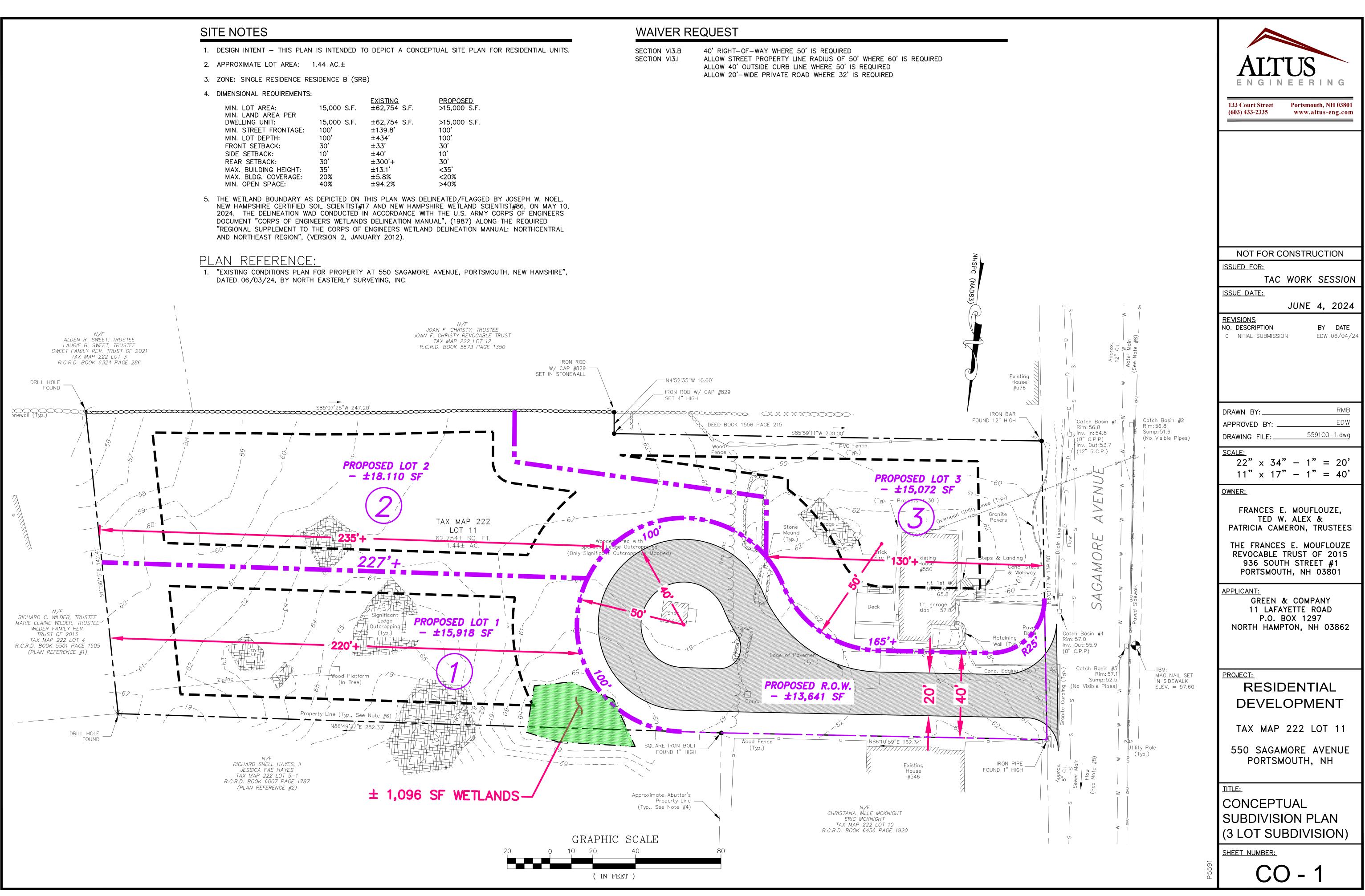
Jorh W. Mil

Joseph W. Noel NH Certified Soil Scientist #017 NH Certified Wetland Scientist #086



June 15, 2024 JWN #24-58 Page 2 of 2







July 3, 2024

Mr. Rick Chellman, Chair City of Portsmouth Planning Board 1 Junkins Avenue Portsmouth, NH 03801 John K. Bosen Admitted in NH & MA

Christopher P. Mulligan Admitted in NH & ME

Molly C. Ferrara Admitted in NH & ME

> Austin Mikolaities Admitted in NH

Bernard W. Pelech

1949-2021

Re: Preliminary Conceptual Consultation / Design Review Completion 361 Hanover Street

Dear Chairman Chellman:

On behalf of 361 Hanover Steam Factory, LLC, we are pleased to submit one (1) set of hard copies and one electronic file of the following information to support a second request for a Preliminary Conceptual Consultation and a request to complete the Design Review process for the above referenced project:

Design Review Plans, dated July 3, 2024

Since the initial Preliminary Conceptual Consultation, we have listened to the comments and concerns of this Board and the abutters and redesigned the site to include four (4) buildings in order to allow more light and air into property and give it an overall neighborhood look and feel. As a result, we believe a second Preliminary Conceptual Consultation is warranted. Also, as the completion of the Design Review process included a Public Hearing and site walk we hereby request that these plans be the subject of this process.

The Site Plan depicts Building A as an 18,082 S.F, 4 story building with a Penthouse. It will have 34 dwelling units and 3 workforce housing units. Building B is a 3,116 S.F. two $(2 \ 1/2)$ story building with 4 dwelling units, Building C is a 2,280 two (2) story building with 2 dwelling units (Duplex) and Building D is a 4,320 S.F. three (3 1/2) story building with 8 dwelling units. The project will also provide a total of 69 parking spaces.

The applicant respectfully requests to be placed on the July 18, 2024 Planning Board meeting agenda. If you have any questions or concerns, please do not hesitate to call or email me at <u>jbosen@bosenandassociates.com</u>

Very truly your John K. Bosen

cc: client John Chagnon Nicholas Cracknell

PORTSMOUTH STEAM FACTORY PROJECT

PRELIMINARY CONCEPTUAL REVIEW - ALTERNATIVE CUP PLAN -



361 HANOVER STREET, PORTSMOUTH, NH HAMPSHIRE DEVELOPMENT CORPORATION

July 18TH 2024

To: Rick Chellman, Planning Board ChairRe: Preliminary Conceptual Review – Building and Site Design Revisions for 361 Hanover St.

Purpose

The purpose of this submission for Preliminary Conceptual Review is three-fold. First, we would like to present an alternative building and site plan from the so-called "as-of-right" plan that was recently approved for Design Review (see Figure 1).



Figure 1 – Proposed "As-of-Right Plan" showing a large Mixed-Use Building fronting on Hanover St.

As a response to your feedback, we developed an alternative building and site plan – "the CUP Plan" that we believe better addresses your comments, suggestions, and the many issues and concerns expressed by members of the public during the Preliminary Conceptual and Design Review meetings.



Figure 2 – Proposed "CUP Plan" showing three traditionally-designed buildings along Hanover St.

Secondly, we would like to receive input and feedback on our proposed CUP Plan in order to make any final design adjustments prior to filing a formal Site Plan Application. Finally, realizing that we will require zoning relief to implement the CUP Plan, we would like to request the Board consider informally supporting our alternative CUP plan prior to us filing a variance application in August.

Site Plan Elements

As discussed during the Design Review phase of the project, the site planning issues of parking, loading, solid waste, deliveries, drainage, utilities, lighting, landscaping, off-site improvements, and the location of all mechanical equipment will all be formally addressed when a site plan is updated and reviewed by both the Technical Advisory Committee and the Planning Board. We would refer the Board to our submission packet and project narrative, dated April 4th, 2002, and on file with the Planning Department for any questions pertaining to those issues.

Issues Raised during Design Review

As you recall, as part of the public hearing within the Design Review process, several core issues of concern were expressed from both Planning Board members, neighbors, and members of the general public. The core issues included the height, scale, volume, and massing of the proposed buildings. Additionally, there were also concerns about the prospect of ground-floor commercial uses and their potential impact on spill-over street parking, lighting, and noise. Other issues included emergency access concerns via the proposed tunnel, parking and loading areas, and whether the proposed buildings and zoning requirements were consistent with the North End Vision Plan. Other issues of concern related to pedestrian access to Foundry Place, improving on-site drainage, and consideration for a better building design to reflect the historic quality and character of the smaller historic structures within the surrounding neighborhood.

Our Preliminary Response

As discussed during the Design Review process, we listened to Board and public feedback and have reevaluated the proposed building and site design and re-examined the density, dimensional, and the architectural character of the surrounding neighborhood. Additionally, we have revisited the existing zoning regulations and the goals and objectives of the North End Vision Plan in order to refine the design to better reflect the goals of both the Board and the surrounding neighborhood. In doing so, we reconsidered the five (5) following elements as follows: 1) the goals and objectives of the North End Vision Plan; 2) the existing neighborhood context (density and design); 3) the surrounding land use pattern (especially on the ground-floor); 4) the pedestrian circulation; and, 5) the building placement, volume, and design.

1. North End Vision Plan

As listed in Figure 3, the goals and objectives of the North End Vision Plan were focused on generating building and site designs that were both respectful and sensitive to the surrounding context. In particular, the buildings were intended to step up or down in transitional areas like the property at 361 Hanover Street. This stepping element is exactly why the North End Overlay District does not carry over to the parking lot portion of the property along Hanover Street. Additionally, the Vision Plan encourages ground-floor commercial uses to active the sidewalk and enhance the

pedestrian experience. Thus, the Downtown Overlay District (DOD) was extended into much of the North End. Streets were also encouraged to support multi-modal traffic with an emphasis of nonvehicular use of new streets and driveways. Finally, to achieve more vibrant, walkable streets and sidewalks, the zoning also includes incentives for public or civic spaces like shared streets, wide public sidewalks, or public park areas.

Despite the zoning for the North End allowing taller and larger buildings than the surrounding context and mandating ground-floor commercial uses, we developed an alternative plan - the "CUP Plan" – that we believe better reflects the goals and objectives of the North End Vision Plan. The CUP Plan seeks to step the buildings down from the taller buildings along Hill and Hanover Streets to the much shorter and smaller building types along Rock Street.

PLAN PORTSMOUTH

NORTH END PRELIMINARY VISION PLAN

DESIGN NARRATIVE worth exits is envisioned over the iong term to grow sa a competentiarly extension stronghr is downown. Unlike many other areas of the Cally within the former Urban wal area, very little historical context remains. This fact, coupled with several large in parcies, makes this distinct ripe for nedevelopment opportunities close to down-inglementation of this vision will likely require a wide array of innovative land use ations, policies and programs. The North End Vision Plan has four main components:

CIVIC SPACE

CIVIC SPACE The Pain necoportains an edensive network of parks, plazas, paths, playgrounds, tr, and open space. One essential feature is the waterfront tail network along the perg very of the fort MH (Paod. WH) several landcaged fingers, the network is designed to pall the waterfront. Deak into the Korth End and provide public access to and alon be waterfront. To celetaring the unque heativy of this area, a contrait diver space to clocated adjacent to the former shipbuilding and launch ramp as a series of hardscap glazas, greens and waterfront esplanades for acceleration adjacent to the former shipbuilding and launch ramp as a series of hardscap glazas, greens and waterfront esplanades for accelera adjacesting the recension. Access process, growns and waterfront esplanades for active and passive recreation Maplewood Avenue bridge, the existing City-owned boat launch site on M expanded into a new park. The trail network also includes a path through North Cemeteries.

BUILDING DESIGN

e massing strategy of the vision plan is to respond to the surrounding context an which by strategy of the vision plan is to respond to the surrounding context and strategy bases in sociators. When he returns and is downlown is not in historical con-transpondence of the surrounding strategy and the surrounding plane. The program balance grades, which here, mathematism and a weld available of balance humes and massing lactionaus in the North End. The purposeful distinction will discher her North End as a unque entity while complementing and contrasting will toric character of the larger downlown.

LAND USE

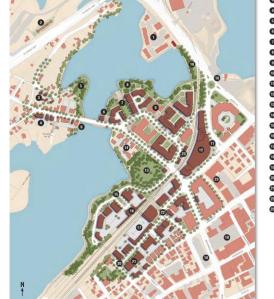
ND USE dues in the North End will include a variety of residential, office and commercial dues in the North End will include a variety of mode-dues building types from smalle holmes and Interwork units to mid-tee buildings. Ground Rott courses will be com-ciail in order to activate stretestoges and to keep residences out of potential flood ends. I. bailty, these residential units will incorporate a ful frange of housing opportu-from affordable workforce housing to kaury units. Paixing will be located in the r due, in subtername angines or in wrapped parking structures to be concolled for In sourcenanean garages or in wrapped parking structures to be concealed from view. There may be an opportunity to support infill housing on the former PSNH tion parcel now that much of the equipment has been removed or consolidated. nally, the plan envisions the eventual removal of the overhead transmission linea.

TRANSPORTATION & INFRASTRUCTURE

one vasion i van anticipales a harmonious integration of various modes of transpo-inclusing pedestrata, bicycle, verlicular and transt connections in the form of loss tituer passenger at lines. All throoghtens are designed to be polisitian-inform where possible. The Orly is planning to relative the Maglewood Avenue tridge on North MI Prod. Univer this is done, there may be opportunities to integrate new ings and waterfront diring to better connect the Dennett Street area with the North North MI Prod.

© 2014 Town Planning & Urban Design Collabo

Figure 3 – North End Vision Plan





1 NOBLE'S ISLAND

2. Neighborhood Context

Project density can be defined in a number of ways including, but not limited to, the number of dwelling units, or the height, volume, footprint, or massing of the buildings. When looking at density as a function of the number of dwelling units, Figure 4 illustrates the transition from the highdensity developments and land use pattern within the character-district zoning along Foundry Place and Hill Street in the North End with the lower density traditional neighborhoods along Rock or Sudbury Street in the abutting Islington Creek Neighborhood.



Figure 4 – Existing Neighborhood Density (Estimated Units / Acre)

When looking at the existing and allowed densities in terms of building height, scale, and volume, the variation within the surrounding neighborhood is even more dramatic. For example, within the CD5, buildings are permitted to have footprints as large as 20,000 SF and heights between 40-60' depending on overlay districts. In contrast, new buildings in the abutting CD4-L1 are restricted to much smaller footprints of 2,500 SF (about the size of the Pearl Street Church) and heights of 40-42' (again about the height of the Pearl Street Church). Interestingly, like the character-based zoning, the abutting General Residence C District allows for new buildings to be between 35-43' in height depending on whether parking is provided within the ground-floor of the building.

Perhaps the biggest difference between the GRC, CD4-L1, and the CD5 is the coverage and open space requirements as buildings in the CD5 are allowed to occupy 95% of the lot area and thus, do not require significant open space areas whereas the GRC and CD4-L1 require between 40% and 65% of the lot area to be remain undeveloped for parking or open space.

Coupled with the size of the footprints allowed in the CD5, the high coverage allowance promotes and encourage buildings that are significantly larger than those permitted in the abutting GRC District. Importantly, the allowable density (as reflected by the allowable footprints and building heights) transitions from a high density along Foundry Place and Hill Street (the CD5 district with large footprints and a 50-60' height limitation) to a moderate density along Hanover Street (the CD4-L1 district with smaller footprints and a 40' height limitation) and to a much lower density along Tanner, Pearl, and Parker Streets (the GRC district with small footprints and a 35-43' height limitation) before increasing to a moderate density allows along Islington Street (the CD4-L2). Thus, our evaluation of the surrounding context suggests that we consider reconfiguring the density and volume of the so-called "As-of-Right Plan" to substantially reduce the building height, volume, and footprints along Hanover Street.

3. Ground-Floor Commercial Uses

Although the Downtown Overlay District (DOD) includes the total land area of 361 Hanover Street it is important to acknowledge that there are no other properties fronting on Hanover Street included in the DOD. Within Downtown Portsmouth, DOD requires ground-floor commercial uses with the intention to activate the street edge and enhance the pedestrian experience.



Figure 5 – Existing Streetscape showing Residential Land Use Pattern on Hanover St.

Unfortunately, in this particular area along Hanover Street Figure 6 shows that only 293 Hanover Street is designed for and used as a commercial use. Moreover, except for the non-conforming Peral Street Church property, all other nearby properties on Hanover Street and the intersecting streets are all residential uses (see Figure 5).



Figure 6- Commercial Use at 293 Hanover Street

To the east, Bridge Street is essentially the edge of the downtown commercial district and Islington Street – a mixed-use commercial corridor linking the downtown to the West End – provides intermittent commercial uses that support the adjacent neighborhoods (see Figure 7).



Figure 7 - Commercial Use at 63 Islington Street

Thus, along with the question of the economic viability of this location, the concerns and compatibility issues with the surrounding residential neighborhood led us to continue to evaluate the more suitable ground-floor use of residential dwelling units; consistent with the existing neighborhood context.

4. Pedestrian Circulation

During the Design Review process suggestions were made to consider and provide for pedestrian connections between the proposed project and the public parking garage on Foundry Place. In review of the serious physical challenges of opening the City's existing retaining wall along Foundry Place to introduce a stairway to Foundry Place we evaluated other less-challenging options. In particular, we reviewed the approved site plans for the abutting 53 unit project at 89 Foundry Place. The approved plans show a 6-8' wide public pedestrian accessway connecting the entrance of the public parking garage on Foundry Place with Hill Street (see Figure 8 below). The entrance to the public parking garage is less than 300 feet from the proposed multi-modal way that is proposed within the project. Thus, visitors and any spillover parking can utilize this pedestrian passageway to easily access the Foundry Place Public Parking Garage.

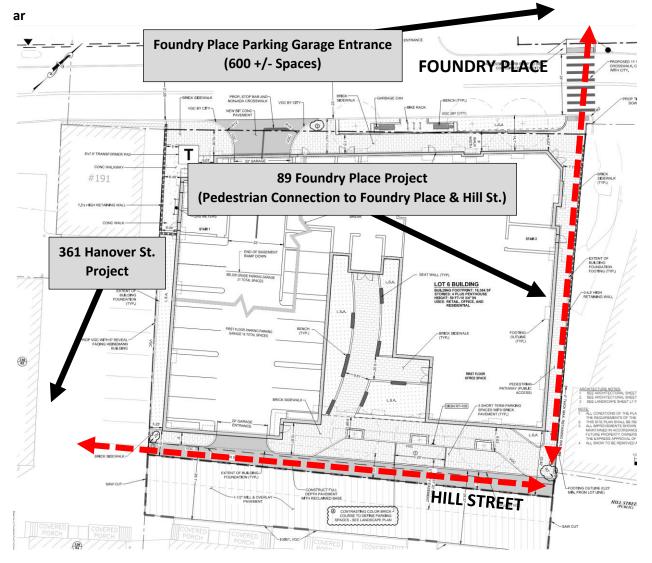


Figure 8 – Pedestrian Connector at 89 Foundry Place

5. Building Design

Some Board members and most members of the public suggested we reevaluate the proposed architectural style of the proposed building(s) along Hanover Street with a clear preference for buildings that are more consistent with the quality and historic character of the surrounding historic buildings. More specifically, suggestions were made for smaller building footprints, reduced height and volume, and the application of traditional building principles that would better reflect the historic architecture of the surrounding neighborhood.

Alternative CUP Plan

Overall Building and Site Design

The alternative CUP Plan seeks to address the core issues listed above by adhering to the goals and objectives of the North End Vision Plan. Moreover, it also seeks to redevelop the property by employing a context-sensitive approach that steps down and transitions from a high-density newer development along Foundry Place and Hill Street to a moderate density along Hanover Street and lower density along Rock and Sudbury Streets.



Figure 9 – Proposed "As-of-Right Plan" showing a large Mixed-Use Building fronting on Hanover St.

Figure 9 illustrates how the previously proposed 3 ½ story mansard building along Hanover Street occupies the full street frontage along Hanover Street and overpowers some of the smaller abutting buildings. In contrast, Figure 10 illustrates the alternative CUP Plan where the larger building has been broken into three separate buildings with reduced height and volume to better align with the lower density context of the western side of the site.

As we discussed within the Design Review process, the CUP Plan also proposes to increase the height of the Kearsarge Building along Foundry Place – in a historically sensitive manner – to reestablish the volume, height, and historic character of the building and support the transfer of development rights from Hanover Street to Foundry Place as intended in the North End Vision Plan and the Character-Based Zoning.



Figure 10 – Proposed Lower-Scale, Traditionally-Designed Buildings along Hanover Street

Ground-Floor Residential Uses

Given the questions of economic viability and the potential for adverse impacts on the surrounding neighborhood (i.e. spillover parking, noise, and light pollution), the CUP Plan proposes a residential ground-floor use in all four buildings.

Building Placement & Open Space

As shown in Figure 11, there is parking available on-site to support up to 48 dwelling units within the four (4) proposed buildings.

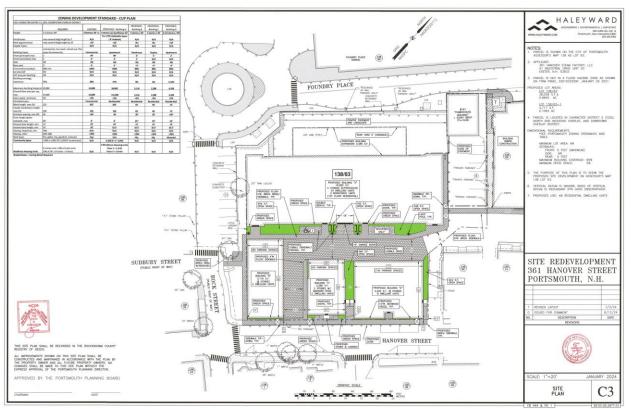


Figure 11 – Alternative CUP Plan showing Proposed Buildings and Driveways and Open Space

DRAFT Project Narrative – Preliminary Conceptual for 361 Hanover Street Project

Building Design

As shown in Figures 12-15, all four buildings have been redesigned to be more consistent with the historic character of the surrounding neighborhood. Understanding this property is located outside the Historic District, we have intentionally redesigned these buildings to reference the historic elements in the surrounding context versus the more contemporary buildings being constructed along Foundry Place and Deer Street in the North End.



Figure 12 – Building A: 4½-Story "Apartment" Building (the Kearsarge Building)



Figure 13 – Building B: 3-Story "Rowhouse" Building



Figure 14 – Building C: 3-Story "Duplex" Building



Figure 15 - Building D: 3½-Story "Apartment" Building

Community Space

As required under the CUP, at least 10% (3,853 SF +/-) of the property would be deeded as Community Space. As shown on Figure 16, the proposed Community Space would be a 4,500 +/- SF Shared Multi-Modal Way connecting Rock Street to Hill Street. The shared street would include formal landscaping, lighting and street furniture.

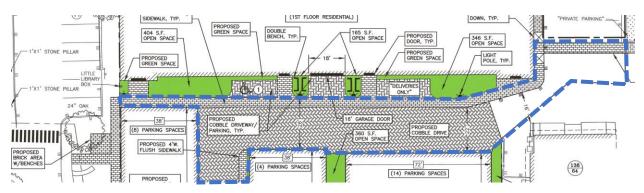


Figure 16 – Proposed Community Space - Multi-Modal Way

Workforce Housing

As required under the CUP, at least 10% of the proposed dwelling units would be deed restricted as rental Workforce Housing Units and be rented to a household with an income of no more than 60% of the median family income for a 3-person household. Such units will be at least 600 SF in GFA and are proposed to be located within the 1st and 2nd floor of Building A (the only building located within the North End Incentive Overlay District).

Zoning Relief

Table 1 shows now	r the proposed tour	(4) buildings align	with the developmen	t standards for the CD5.

والمراجع والمترين ورورته والمراجع والمراتين

	ZONIN	G DEVELOPME	NT STANDARD - CU	JP PLAN		
CD5: CHARACTER DISTRICT 5, E	DOD: DOWNTOWN OVERLAY DISTRICT					
	REQUIRED	EXISTING	PROPOSED - Building A	PROPOSED - Building B	PROPOSED - Building C	PROPOSED - Building
Height	2-3 stories 40'	2 Stories/ 18' +/-	4 stories w/ penthouse 52'	3 stories / 36'	3 stories / 36'	3 1/2 stories / 40'
			Yes (75% Habitable Space			
Penthouses	may exceed bldg height by 2'	N/A	/ 8' Setback)	N/A	N/A	N/A
Roof appurtenance	may exceed bldg height by 10'	<10'	<10'	No	No	<10'
açade Types		N/A	N/A	N/A	N/A	N/A
	commercial, live-work, mixed use, flex					
Building Types	space & community.	Commerical	Apartment	Rowhouse	Duplex	Apartment
Front (principle) max	5	99'	99'	0'	5'	2'
Front (secondary) max	5	0'	0'	2'	N/A	N/A
Side	NR	NR	NR	NR	NR	NR
Rear yard	5'	0'	0'	>5'	>5'	>5'
Front lotline buildout	80% min	100%	100%	80%	80%	80%
ot area (sf)	NR	N/A	N/A	N/A	N/A	N/A
OT area per dwelling	NR	N/A	N/A	N/A	N/A	N/A
Building coverage, maximum	95%	38%	47%	8%	6%	11.0%
Maximum building footprint	20,000	14,808	18,082	3,116	2,280	4,320
Ground floor area per use, ma: Open space, minimum	x 15,000 5%	14,808 <5%	<15,000 >5%	3,116 >5%	2,280 >5%	4,320 >5%
Permitted uses		Commercial	Residential	Residential	Residential	Residential
Block length, max (ft)	225	205'	205'	82'	40'	72'
açade modulation length, ma		200				
(ft)	100	205	205	82'	40'	72'
Entrance spacing, max (ft)	50	>50'	50	20'	20'	<50'
Floor height above sidewalk,						
max	36"	0'	0'	24"	24"	24'
Ground story height, min	12'	10'	10'	12'	12'	12'
Second story height, min	10'	10'	10.5'	10.5'	10.5'	10.5'
Glazing, shopfront, min	70%	N/A	N/A	N/A	N/A	N/A
Glazing, other	20%-50%	>20%	>20%	>20%	>20%	>20%
Roof types	flat, gable, hip, gambrel, mansard	Flat	Flat	Hip	Hip	Mansard
Community Space	>10% or 3,852 SF (1,926 SF as pervious)	N/A	4,250 SF +/- (12%)	N/A	N/A	N/A
	If rental units =10% of total units.		3 Workforce Housing Units Floor 1 = 1 Unit			

Table 1 – Zoning Table showing Development Standards for each Building

As illustrated with the shaded boxes in Table 1, to support the CUP Plan, zoning relief from the Board of Adjustment (BOA) will be necessary. The following variances are required to permit and construct the plan:

1. To allow the ground-floor use of the buildings to be residential.

- 2. To allow for an "apartment", "rowhouse", and "duplex" building type in the CD5.
- 3. To allow the ground floor height of Building A (the Kearsarge Building) to be 10' versus 12'.
- 4. To allow the penthouse level of Building A (the Kearsarge Building) to exceed 50% of the total floor area of the floor below and have a setback of 8' from the roof edge.

Summary

After consideration of the many valuable comments, issues, concerns, and suggestions provided by the Board and members of the public within the Design Review process for the "As-of-Right Plan", we believe the proposed CUP Plan meets the goals and objectives of the North End Vision Plan and, subject to the granting of zoning relief from the Board of Adjustment, exceeds the findings and criteria needed for approval of a CUP.

In closing, we would respectfully request the Board consider an informal vote in support for the CUP Plan. Doing so would not only acknowledge our collective efforts to address the concerns raised during the Design Review process but also "right-size" this development and demonstrate our common goals to make this project a success for urban infill and redevelopment in downtown Portsmouth. Moreover, it would also be likely to have a positive effect on the BOA's review and provide them a deeper appreciation and understanding of how these design changes were collaboratively developed. In the end, we believe this CUP Plan better aligns with the Board's and the public's strong desire for a more balanced, respectful, and context-sensitive, redevelopment of this property; one that also includes Community Space and Workforce Housing.

PROPOSED DEVELOPMENT 361 HANOVER STREET PORTSMOUTH, NEW HAMPSHIRE **DESIGN REVIEW PLANS**

OWNER/APPLICANT:

361 HANOVER STEAM FACTORY, LLC 41 INDUSTRIAL DRIVE UNIT 20 EXETER, NH 03833 TEL. (603) 235-5475

CIVIL ENGINEER/LAND SURVEYOR:

AMBIT ENGINEERING, INC. 200 GRIFFIN ROAD, UNIT 3 PORTSMOUTH, N.H. 03801 TEL. (603) 430-9282

ARCHITECT:

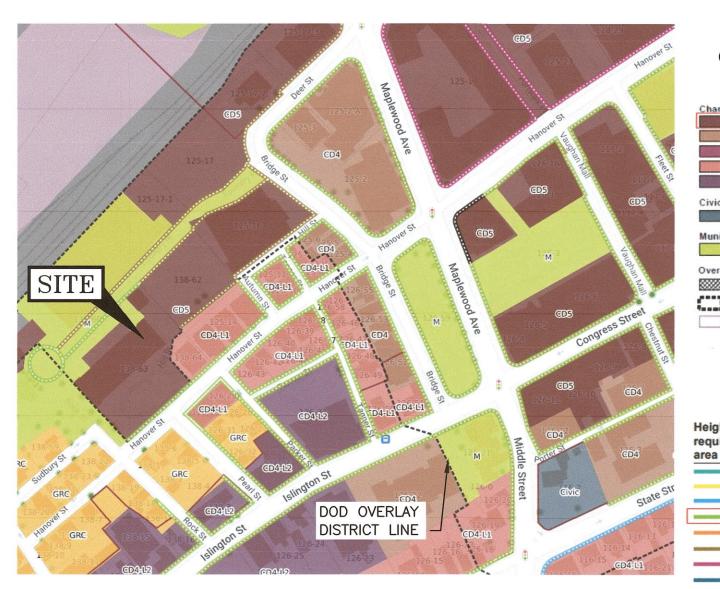
SCOTT BROWN 29 WATER STREET, SUITE 209 NEWBURYPORT, MA 01950 TEL. (978) 465-3535

PLANNING CONSULTANT:

NICHOLAS CRACKNELL TEL. (978) 270-4789

LAND USE ATTORNEY:

BOSEN & ASSOCIATES 266 MIDDLE STREET PORTSMOUTH, N.H. 03801 TEL. (603) 427-5500



MAP 10.5A21A CHARACTER DISTRICTS AND CIVIC DISTRICTS

haracter Districts

Character District 5 CD4 Character District 4 CD4W Character District 4-W CD4-L1 Character District 4-L1 CD4-L2 Character District 4-L2

Civic District

Civic District Municipal District

Municipal District **Overlay Districts**

OLOD Osprey Landing Overlay District Downtown Overlay District

Historic District

MAP 10.5A21B BUILDING HEIGHT STANDARDS

Heigh requir area	rement	Maximum building height*		
pine and a	1 Story	20'		
	2 Stories	35'		
	2 Stories (short 3rd*)	35'		
oteo official	2-3 Stories	40'		
Non-contraction of	2-3 Stories (short 4th	*) 45'		
	2-4 Stories	50'		
	2-4 Stories (short 5th)	*) 60'		
	2-5 Stories	60'		
*Pentho	use Levels may exceed the	e building height		

by 2 feet

DWG NO.

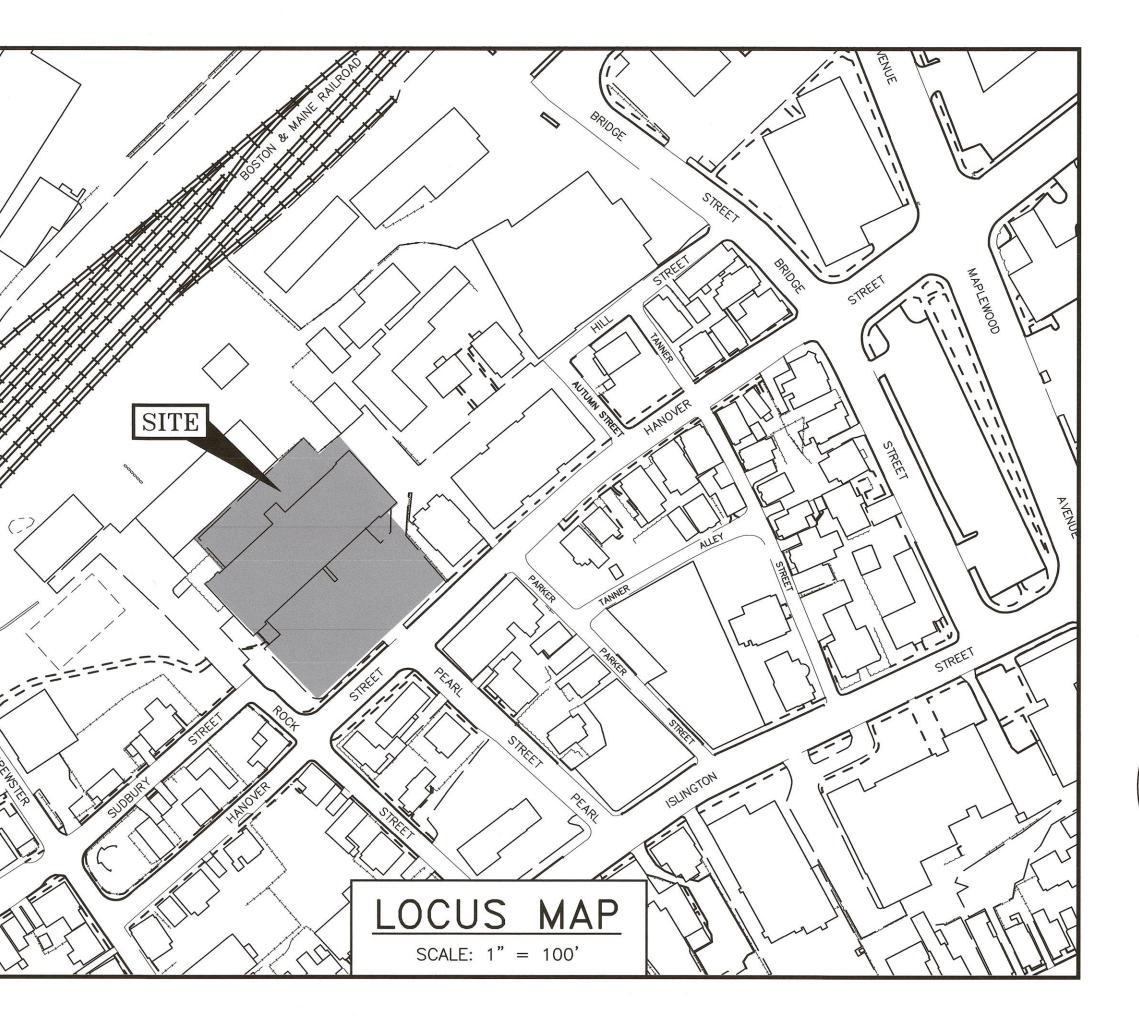
INDEX OF SHEETS

	SUBDIVISION PLAN
	SITE ORTHOPHOTO
C1	EXISTING CONDITIONS PLAN
C2	DEMOLITION PLAN
С3	SITE PLAN
-	LICENSE AREA PLAN

PORTSMOUTH APPROVAL CONDITIONS NOTE: ALL CONDITIONS ON THIS PLAN SET SHALL REMAIN IN EFFECT IN PERPETUITY PURSUANT TO THE REQUIREMENTS OF THE CITY OF PORTSMOUTH SITE PLAN REVIEW REGULATIONS.

APPROVED BY THE PORTSMOUTH PLANNING BOARD

DATE





UTILITY CONTACTS

ELECTRIC:

EVERSOURCE 1700 LAFAYETTE ROAD PORTSMOUTH, N.H. 03801 Tel. (603) 436-7708, Ext. 555.5678 ATTN: MICHAEL BUSBY, P.E. (MANAGER)

SEWER & WATER: PORTSMOUTH DEPARTMENT OF PUBLIC WORKS 680 PEVERLY HILL ROAD PORTSMOUTH, N.H. 03801 Tel. (603) 427-1530 ATTN: JIM TOW

NATURAL GAS: UNITIL 325 WEST ROAD PORTSMOUTH, N.H. 03801 Tel. (603) 294-5144 ATTN: DAVE BEAULIEU

COMMUNICATIONS: FAIRPOINT COMMUNICATIONS JOE CONSIDINE 1575 GREENLAND ROAD GREENLAND, N.H. 03840 Tel. (603) 427-5525

CABLE: COMCAST 155 COMMERCE WAY PORTSMOUTH, N.H. 03801 Tel. (603) 679-5695 (X1037) ATTN: MIKE COLLINS

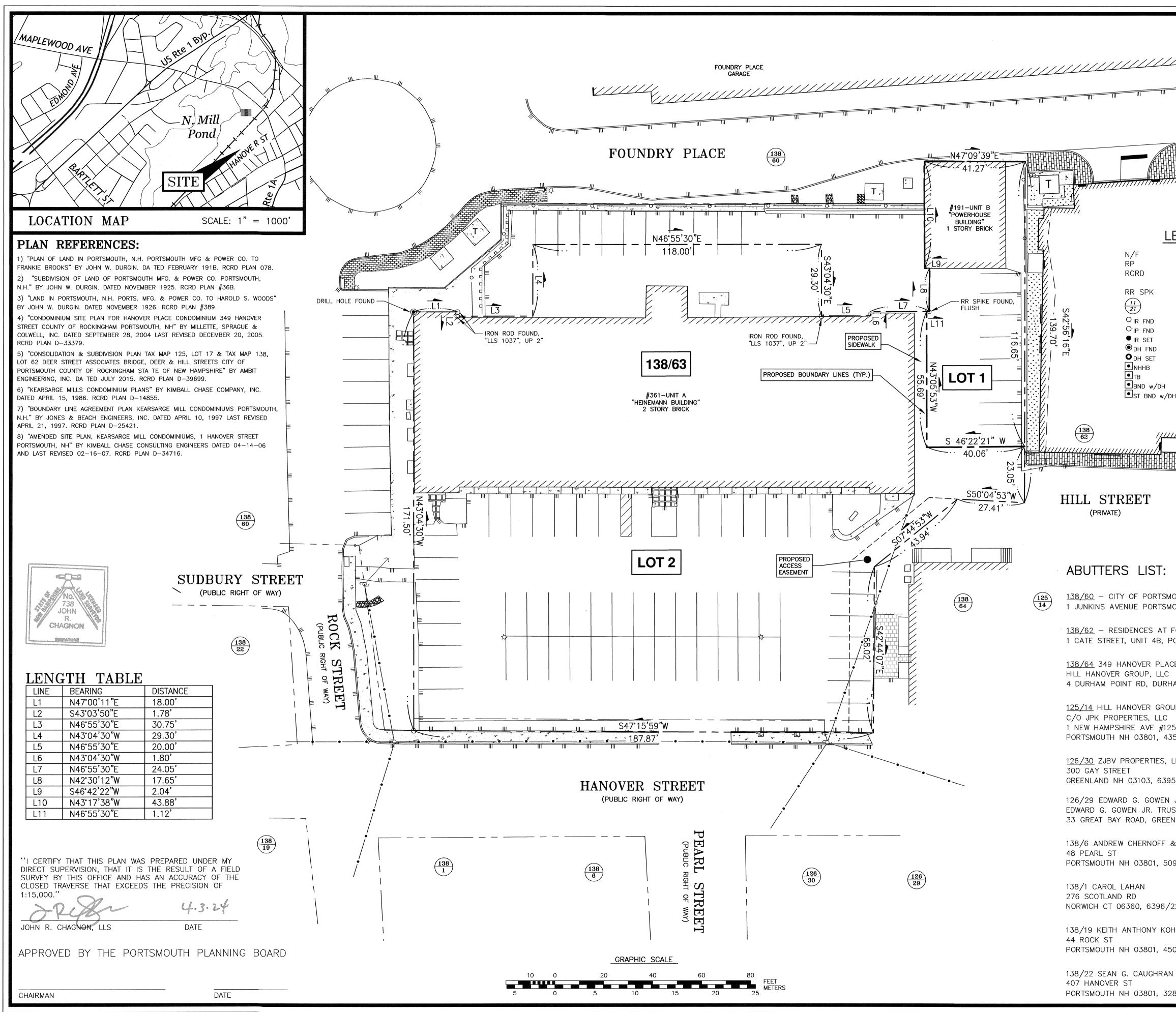
PERMIT LIST:	
PORTSMOUTH HDC:	
PORTSMOUTH ZONING BOARD:	
PORTSMOUTH SITE REVIEW:	
PORTSMOUTH CONDITIONAL USE PER	RMIT:

к. 	LEGEI	ND:
EXISTING	PROPOSED	
·		PROPERTY LINE
	S	SETBACK SEWER PIPE
SL	SL	SEWER LATERAL
G	G	GAS LINE STORM DRAIN
W	W	WATER LINE
WS UGE	WS UGE	WATER SERVICE UNDERGROUND ELECTRIC
—— онw ——	OHW	OVERHEAD ELECTRIC/WIRES
m	UD	FOUNDATION DRAIN
	<u>100</u>	EDGE OF PAVEMENT (EP) CONTOUR
97x3 - 	98×0	SPOT ELEVATION UTILITY POLE
-Ŏ- '''''		WALL MOUNTED EXTERIOR LIGHTS
		TRANSFORMER ON CONCRETE PAD
		ELECTRIC HANDHOLD
450 GS0	NSO GSO	SHUT OFFS (WATER/GAS)
\bowtie	GV	GATE VALVE
-@-	+++	HYDRANT
CB	СВ	CATCH BASIN
\bigcirc	● ^{SMH}	SEWER MANHOLE
	DMH	DRAIN MANHOLE
1	() TMH	TELEPHONE MANHOLE
14)	(14)	PARKING SPACE COUNT
PM		PARKING METER
LSA	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	LANDSCAPED AREA
TBD CI	TBD CI	TO BE DETERMINED CAST IRON PIPE
COP	COP	COPPER PIPE
DI PVC	DI PVC	DUCTILE IRON PIPE POLYVINYL CHLORIDE PIPE
RCP	RCP	REINFORCED CONCRETE PIPE
AC VC	– VC	ASBESTOS CEMENT PIPE VITRIFIED CLAY PIPE
EP	EP	EDGE OF PAVEMENT
EL. FF	EL. FF	ELEVATION FINISHED FLOOR
INV S =	INV S =	INVERT SLOPE FT/FT
TBM TYP	TBM TYP	TEMPORARY BENCH MARK
(11*	111-	

DESIGN APPLICATION PLANS PROPOSED DEVELOPMENT **361 HANOVER STREET** PORTSMOUTH, N.H.

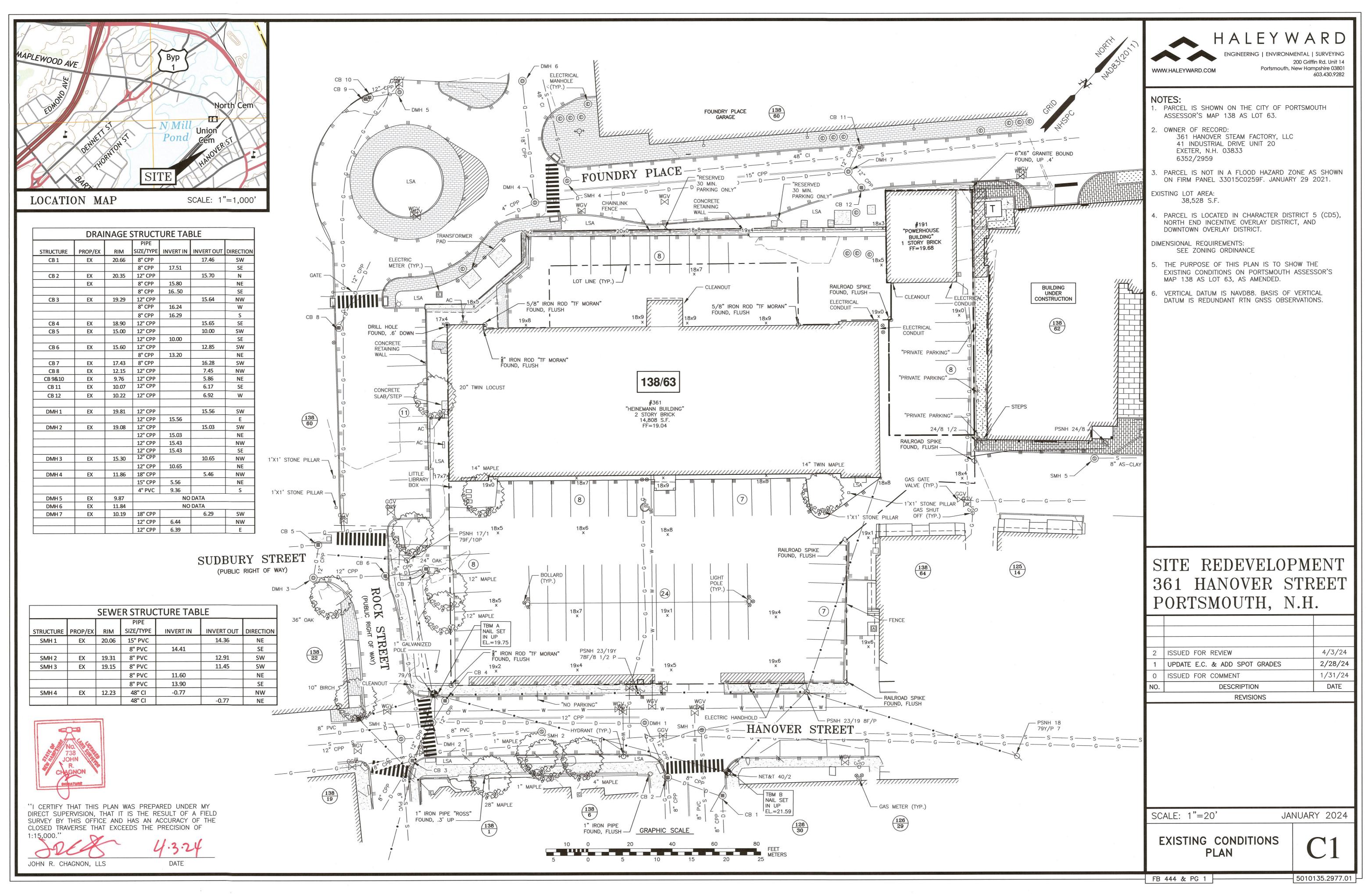


PLAN SET SUBMITTAL DATE: 3 JULY 2024



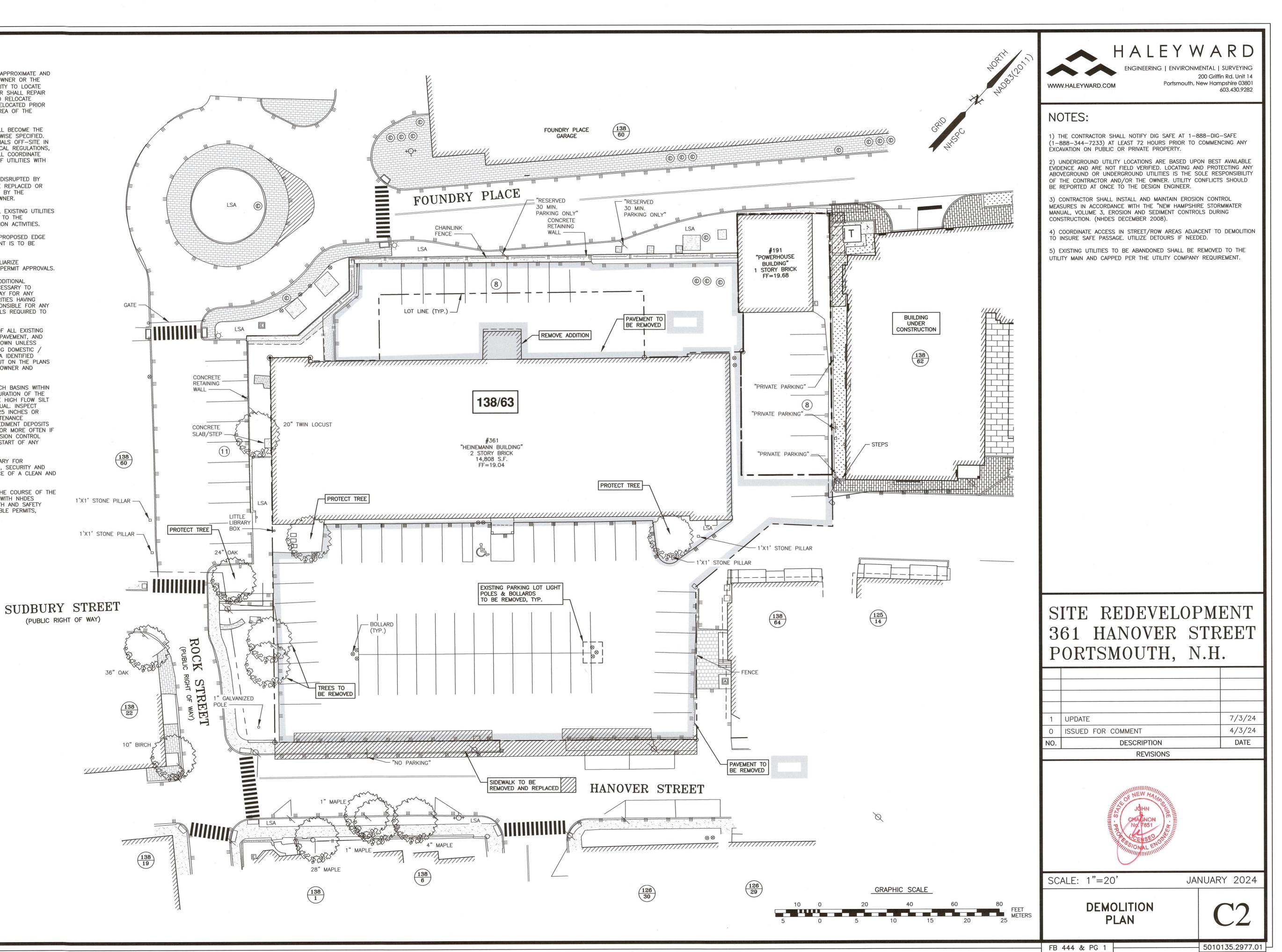
	r		
NO21H NO22011)	AMBIT ENGI A DIVISION OF HAL		
- The NAU	WWW.HALEYWARD.COM	200 Griffin Road, Unit 3 Portsmouth, NH 03801 603.436.2315	
CRIP AHSPC	NOTES: 1) PARCEL IS SHOWN ON THE CITY ASSESSORS MAP 138 AS LOT 63.	OF PORTSMOUTH	
	2) OWNERS OF RECORD: <u>UNIT_A:</u> 361 HANOVER STEAM I 41 INDUSTRIAL DRIVE EXETER, N.H. 03833 6352/2959		
LEGEND	<u>UNIT B:</u> POWERHOUSE REALTY TR C/O ADAMS DAVID B. TR 210 GATES STREET PORTSMOUTH, NH 03801 5419/1223		
NOW OR FORMERLY RECORD OF PROBATE ROCKINGHAM COUNTY REGISTRY OF DEEDS	3) PARCEL IS NOT IN A SPECIAL FL SHOWN ON FIRM PANEL 33015C025 2021.		
RAILROAD SPIKE MAP 11/LOT 21 IRON ROD FOUND	4) LOT AREAS: <u>EXISTING</u> 43,245 S.F. 0.9928 AC.		
IRON PIPE FOUND IRON ROD SET DRILL HOLE FOUND DRILL HOLE SET	PROPOSED LOT 1 4,717 S.F. 0.1083 AC.		
NHDOT BOUND FOUND TOWN BOUND H BOUND WITH DRILL HOLE /DH STONE BOUND WITH DRILL HOLE	<u>PROPOSED</u> LOT 2 38,528 S.F. 0.8845 AC.		
////	5) PARCEL IS LOCATED IN CHARACT END INCENTIVE OVERLAY DISTRICT (N OVERLAY DISTRICT.	• •	
	6) THE PURPOSE OF THIS PLAN IS SUBDIVISION OF TAX MAP 139, LOT INTO 2 LOTS.		
	7) PARCEL IS BURDENED BY THE F	OLLOWING EASEMENTS:	
	A) ACCESS EASEMENT TO THE TO ALLOW ACCESS TO A PA SEE R.C.R.D. 4735/2971		
	B) ACCESS EASEMENT TO HAI CONDOMINIUM ASSOCIATION. T BE RE-DEFINED AS SHOWN H	HIS EASEMENT TO	
SMOUTH SMOUTH NH 03801, 5848/0666	8) THE PARCEL HAS THE BENEFIT OF A REVOCABLE LICENSE BETWEEN THE CITY OF PORTSMOUTH AND THE KEARSARGE MILL UNIT ON THE PLAN ENTITLED "KEARSARGE MILL CONDOMINIUMS HANOVER STREET, PORTSMOUTH, NH SITE PLAN AMENDMENT" PREPARED BY KIMBALL CHASE CONSULTING ENGINEERS DATED APRIL 14, 2006, LICENSE AND SITE PLAN ARE AVAILABLE WITH		
FOUNDRY PLACE, LLC PORTSMOUTH NH 03801, 6475/1570	THE RECORDS OF THE CITY OF POR REFERENCE #6. 9) PROPERTY CORNERS WILL BE SE		
ACE CONDOS MASTER CARD C RHAM NH 03824, 4356/0010			
OUP, LLC.			
C 125 125 (0010			
4356/0010	0 ISSUED FOR COMMENT	4/3/24	
, LLC	NO. DESCRIPTION	DATE	
395/1921 N JR. REVOCABLE LIVING TRUST	REVISION	S	
RUSTEE ENLAND, NH 03840, 4327/2531	SUBDIVISIO TAX MAP 138		
& REBEKAH CHERNOFF			
5096/0104	KEARSAGE MILL ASSOCIA		
/2229	OWNERS: 361 HAI FACTORY, LLC & POW TRUS	ERHOUSE REALTY	
COHLER & NICOLE GABRIELLE LAPIERRE	TRUST FOUNDRY PLACE & HANOVER STREET		
4505/0807	CITY OF POR COUNTY OF RC	OCKINGHAM	
AN 3289/1071	STATE OF NEW		
	SCALE: 1"=20' FB 444 PG 1	JANUARY 2024	
		5010135.2977.01	





DEMOLITION NOTES

- A) THE LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE NOT GUARANTEED BY THE OWNER OR THE DESIGNER. IT IS THE CONTRACTORS' RESPONSIBILITY TO LOCATE UTILITIES AND ANTICIPATE CONFLICTS. CONTRACTOR SHALL REPAIR EXISTING UTILITIES DAMAGED BY THEIR WORK AND RELOCATE EXISTING UTILITIES THAT ARE REQUIRED TO BE RELOCATED PRIOR TO COMMENCING ANY WORK IN THE IMPACTED AREA OF THE PROJECT.
- B) ALL MATERIALS SCHEDULED TO BE REMOVED SHALL BECOME THE PROPERTY OF THE CONTRACTORS UNLESS OTHERWISE SPECIFIED. THE CONTRACTOR SHALL DISPOSE OF ALL MATERIALS OFF-SITE IN ACCORDANCE WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS, ORDINANCES AND CODES. THE CONTRACTOR SHALL COORDINATE REMOVAL, RELOCATION, DISPOSAL, OR SALVAGE OF UTILITIES WITH THE OWNER AND APPROPRIATE UTILITY COMPANY.
- C) ANY EXISTING WORK OR PROPERTY DAMAGED OR DISRUPTED BY CONSTRUCTION/ DEMOLITION ACTIVITIES SHALL BE REPLACED OR REPAIRED TO THE ORIGINAL EXISTING CONDITIONS BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.
- D) THE CONTRACTOR SHALL VERIFY LOCATION OF ALL EXISTING UTILITIES AND CALL DIG SAFE AT LEAST 72 HOURS PRIOR TO THE COMMENCEMENT OF ANY DEMOLITION/CONSTRUCTION ACTIVITIES.
- E) SAWCUT AND REMOVE PAVEMENT ONE FOOT OFF PROPOSED EDGE OF PAVEMENT TRENCH IN AREAS WHERE PAVEMENT IS TO BE REMOVED.
- F) IT IS THE CONTRACTOR'S RESPONSIBILITY TO FAMILIARIZE THEMSELVES WITH THE CONDITIONS OF ALL THE PERMIT APPROVALS.
- G) THE CONTRACTOR SHALL OBTAIN AND PAY FOR ADDITIONAL CONSTRUCTION PERMITS, NOTICES AND FEES NECESSARY TO COMPLETE THE WORK AND ARRANGE FOR AND PAY FOR ANY INSPECTIONS AND APPROVALS FROM THE AUTHORITIES HAVING JURISDICTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY ADDITIONAL AND OFF-SITE DISPOSAL OF MATERIALS REQUIRED TO COMPLETE THE WORK.
- H) THE CONTRACTOR SHALL REMOVE AND DISPOSE OF ALL EXISTING STRUCTURES, CONCRETE, UTILITIES, VEGETATION, PAVEMENT, AND CONTAMINATED SOIL WITHIN THE WORK LIMITS SHOWN UNLESS SPECIFICALLY IDENTIFIED TO REMAIN. ANY EXISTING DOMESTIC / IRRIGATION SERVICE WELLS IN THE PROJECT AREA IDENTIFIED DURING THE CONSTRUCTION AND NOT CALLED OUT ON THE PLANS SHALL BE BROUGHT TO THE ATTENTION OF THE OWNER AND ENGINEER FOR PROPER CAPPING / RE–USE.
- I) PROVIDE INLET PROTECTION BARRIERS AT ALL CATCH BASINS WITHIN CONSTRUCTION LIMITS AND MAINTAIN FOR THE DURATION OF THE PROJECT. INLET PROTECTION BARRIERS SHALL BE HIGH FLOW SILT SACK BY ACF ENVIRONMENTAL OR APPROVED EQUAL. INSPECT BARRIERS WEEKLY AND AFTER EACH RAIN OF 0.25 INCHES OR GREATER. CONTRACTOR SHALL COMPLETE A MAINTENANCE INSPECTION REPORT AFTER EACH INSPECTION. SEDIMENT DEPOSITS SHALL BE REMOVED AFTER EACH STORM EVENT OR MORE OFTEN IF WARRANTED OR FABRIC BECOMES CLOGGED. EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO THE START OF ANY CLEARING OR DEMOLITION ACTIVITIES.
- J) THE CONTRACTOR SHALL PAY ALL COSTS NECESSARY FOR TEMPORARY PARTITIONING, BARRICADING, FENCING, SECURITY AND SAFELY DEVICES REQUIRED FOR THE MAINTENANCE OF A CLEAN AND SAFE CONSTRUCTION SITE.
- K) ANY CONTAMINATED MATERIAL REMOVED DURING THE COURSE OF THE WORK WILL REQUIRE HANDLING IN ACCORDANCE WITH NHDES REGULATIONS. CONTRACTOR SHALL HAVE A HEALTH AND SAFETY PLAN IN PLACE, AND COMPLY WITH ALL APPLICABLE PERMITS, APPROVALS, AUTHORIZATIONS, AND REGULATIONS



\5010135-Hampshire_Development\2977.01-Hanover St., Portsmouth-JRC\N 2977\2024 Site Plan\Plans & Specs\Site\2977.01 Site Option B.dwg, 7/2/2

	ZONING DEVEL	OPMENT S	TANDARD - CUP P	LAN		
CD5: CHARACTER DISTRICT 5,	DOD: DOWNTOWN OVERLAY DISTRICT			and the second		
				PROPOSED -	PROPOSED -	PROPOSED -
	REQUIRED	EXISTING	PROPOSED - Building A	Building B	Building C	Building D
Height	2-3 stories 40'	2 Stories/ 18' +/-	4 stories w/ penthouse 52'	3 stories / 36'	3 stories / 36'	3 1/2 stories / 40
			Yes (75% Habitable Space			
Penthouses	may exceed bldg height by 2'	N/A	/ 8' Setback)	N/A	N/A	N/A
Roof appurtenance	may exceed bldg height by 10'	<10'	<10'	No	No	<10'
Façade Types		N/A	N/A	N/A	N/A	N/A
	commercial, live-work, mixed use, flex					
Building Types	space & community.	Commerical	Apartment	Rowhouse	Duplex	Apartment
Front (principle) max	5	99'	99'	0'	5'	2'
Front (secondary) max	5	0'	0'	2'	N/A	N/A
Side	NR	NR	NR	NR	NR	NR
Rear yard	5'	0'	0'	>5'	>5'	>5'
Front lotline buildout	80% min	100%	100%	80%	80%	80%
Lot area (sf)	NR	N/A	N/A	N/A	N/A	N/A
LOT area per dwelling	NR	N/A	N/A	N/A	N/A	N/A
Building coverage,						
maximum	95%	38%	47%	8%	6%	11.0%
Maximum building footprint	20,000	14,808	18,082	3,116	2,280	4,320
Ground floor area per use,						
max	15,000	14,808	<15,000	3,116	2,280	4,320
Open space, minimum	5%	<5%	>5%	>5%	>5%	>5%
Permitted uses		Commercial	Residential	Residential	Residential	Residential
Block length, max (ft)	225	205'	205'	82'	40'	72'
Façade modulation length,						
max (ft)	100	205	205	82'	40'	72'
Entrance spacing, max (ft)	50	>50'	50	20'	20'	<50'
Floor height above						
sidewalk, max	36"	0'	0'	24"	24"	24'
Ground story height, min	12'	10'	10'	12'	12'	12'
Second story height, min	10'	10'	10.5'	10.5'	10.5'	10.5'
Glazing, shopfront, min	70%	N/A	N/A	N/A	N/A	N/A
Glazing, other	20%-50%	>20%	>20%	>20%	>20%	>20%
Roof types	flat, gable, hip, gambrel, mansard	Flat	Flat	Hip	Hip	Mansard
Community Space	>10% or 3,852 SF (1,926 SF as pervious)	N/A	4,250 SF +/- (12%)	N/A	N/A	N/A
			3 Workforce Housing Units			
	If rental units =10% of total units.		Floor 1 = 1 Unit			
Wokforce Housing Units	10% of 36 = 3.4 Units = 3 Units)	N/A	Floor 2 = 2 Units	N/A	N/A	N/A

Shaded Boxes = Zoning Relief Required

SUDBURY STREET (PUBLIC RIGHT OF WAY)

(1<u>38</u> 60)

1'X1' STONE PILLAR -

1'X1' STONE PILLAR -

36" OAK

1111111111111

138

10" BIRCH

7//////

138

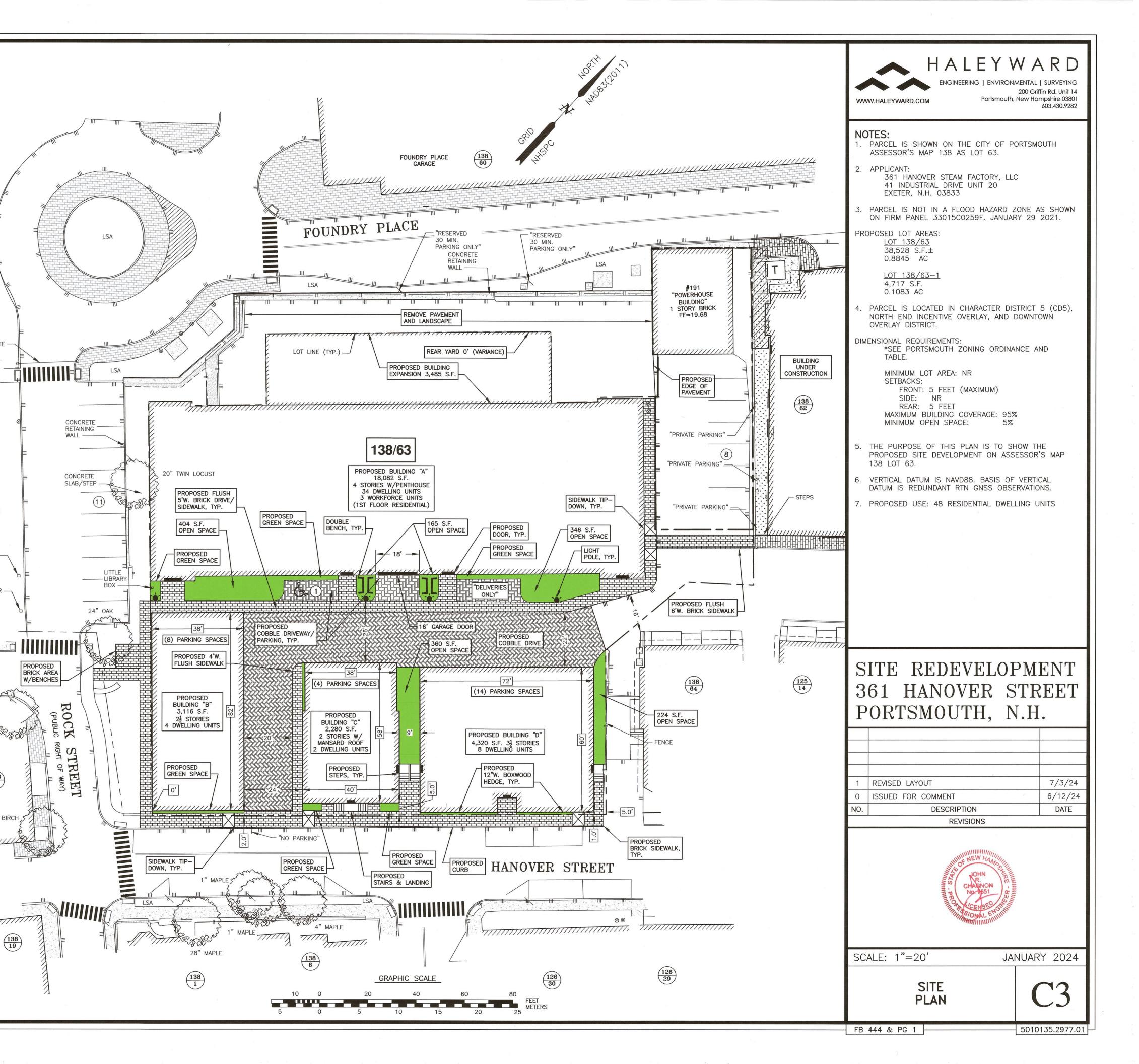
THIS SITE PLAN SHALL BE RECORDED IN THE ROCKINGHAM COUNTY REGISTRY OF DEEDS.

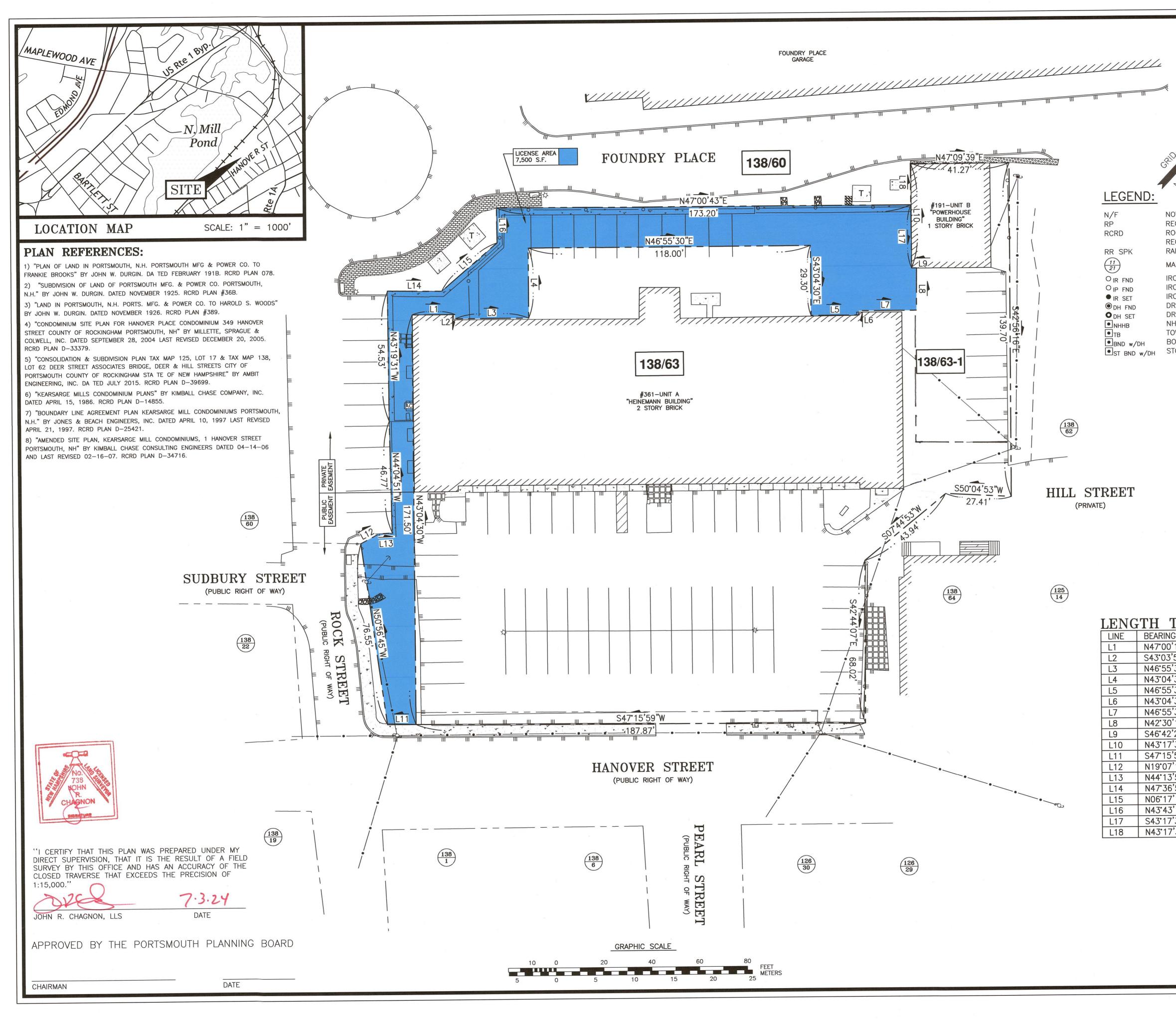
ALL IMPROVEMENTS SHOWN ON THIS SITE PLAN SHALL BE CONSTRUCTED AND MAINTAINED IN ACCORDANCE WITH THE PLAN BY THE PROPERTY OWNER AND ALL FUTURE PROPERTY OWNERS. NO CHANGES SHALL BE MADE TO THIS SITE PLAN WITHOUT THE EXPRESS APPROVAL OF THE PORTSMOUTH PLANNING DIRECTOR.

APPROVED BY THE PORTSMOUTH PLANNING BOARD

CHAIRMAN

DATE





GRID LAND AND AND AND AND AND AND AND AND AND
NOW OR FORMERLY RECORD OF PROBATE ROCKINGHAM COUNTY REGISTRY OF DEEDS RAILROAD SPIKE
MAP 11/LOT 21
IRON ROD FOUND IRON PIPE FOUND IRON ROD SET DRILL HOLE FOUND DRILL HOLE SET NHDOT BOUND FOUND TOWN BOUND BOUND WITH DRILL HOLE OH STONE BOUND WITH DRILL HOL

LENGTH TABLE

BEARING	DISTANCE
N47°00'11"E	18.00'
S43°03'50"E	1.78'
N46°55'30"E	30.75 '
N43°04'30"W	29.30'
N46°55'30"E	20.00'
N43°04'30"W	1.80'
N46°55'30"E	24.05'
N42°30'12"W	17.65'
S46°42'22"W	2.04'
N43°17'38"W	43.88'
S47°15'59"W	11.91'
N19°07'18"E	8.76'
N44°13'52"E	5.50'
N47°36'57"E	22.64'
N06°17'18"E	30.79'
N43°43'16"W	14.55'
S43°17'38"E	26.46'
N43°17'38"W	17.42'

AMBIT A DIVISION	CNOIN			INIA
	ENDIN	ECHI		INL
			7	-
A DIVISION	I OF HALE	Y WARD,	INC.	~~

A DIVISION OF HALEY WARD, INC.

200 Griffin Road, Unit 3 Portsmouth, NH 03801 603.436.2315

WWW.HALEYWARD.COM

NOTES: 1) PARCEL IS SHOWN ON THE CITY OF PORTSMOUTH ASSESSORS MAP 138 AS LOT 60.

2) OWNERS OF RECORD: LOT 60 CITY OF PORTSMOUTH JUNKINS AVENUE PORTSMOUTH, NH 03801

> LOT 63 - UNIT A 361 HANOVER STEAM FACTORY, LLC 41 INDUSTRIAL DRIVE UNIT 20 EXETER, N.H. 03833 6352/2959

3) PARCEL IS NOT IN A SPECIAL FLOOD HAZARD AREA AS SHOWN ON FIRM PANEL 33015C0259F. EFFECTIVE JANUARY 29, 2021.

4) LOT AREA: 38,528 S.F.

5) PARCEL IS LOCATED IN CHARACTER DISTRICT 5 (CD5) AND DOWNTOWN OVERLAY DISTRICT.

6) THE PURPOSE OF THIS PLAN IS TO SHOW A PROPOSED LICENSE AREA ON TAX MAP 138, LOT 60 TO BENEFIT TAX MAP 138, LOT 63 IN PORTSMOUTH, NH.

7) THE LICENSE AGREEMENT BETWEEN THE CITY OF PORTSMOUTH AND 361 HANOVER STEAM FACTORY, LLC WILL REPLACE THE EXISTING PARKING LICENSE AGREEMENT RECORDED AT DEED BOOK 4735 PAGE 2971 AND PROVIDE A PUBLIC AND PRIVATE LANDSCAPING EASEMENT TO 361 HANOVER STEAM FACTORY, LLC.

1	REPLOT	7/3/24		
0	ISSUED FOR COMMENT	3/21/24		
NO.	DESCRIPTION	DATE		
REVISIONS				
Contraction of the				

PROPOSED LICENSE AREA PLAN TAX MAP 138 - LOT 63 CITY OF PORTSMOUTH TO 361 HANOVER STEAM FACTORY, LLC FOUNDRY PLACE & ROCK STREET CITY OF PORTSMOUTH

COUNTY OF ROCKINGHAM STATE OF NEW HAMPSHIRE

SCALE: 1"=20'

DECEMBER 2022 5010135.2977.01