Pease Development Authority 55 International Drive, Portsmouth, NH 03801, (603) 433-6088



Conditional Use Permit Application

Date Submitted:				
Applicant Information Address: I Gagent: Tighe & Bond Address: Address: Address: Address: Dusiness Phone: 6803-433-6100 Business Phone: 6803-433-6118 Mobile Phone: Fax: Fax: Fax: Fortamouth Tax Map: 305 Lot #: 1 & 2 Zone: Alport Business and Commercial Address / Location of Work: 70 & 80 Corporate Drive Activity Information Proposed Activity (check all that apply) X New Structure Expansion of Existing Structure Other site alteration (specify): Total area of wetland on subject lot: Total area of wetland buffer on subject lot: Total area of wetland buffer on subject lot: Total area of wetland impacted: Area of wetland impacted: Area of wetland impacted: Area of wetland buffer impacted: Total area of wetland buffer impacted:	For PDA Use Only			
Applicant Information Applicant: Lonza Biologics Address: Iddress: Iddress	Date Submitted:	Municipal Review:	Fee:	
Applicant: Lonza Biologics Address: 101 International Drive Portsmouth, NH 03801 Business Phone: 603-334-6100 Business Phone: 603-334-6100 Business Phone: 603-433-8818 Mobile Phone: Fax: Fax: Fortsmouth, NH 03801 Mobile Phone: Fax: Fortsmouth Tax Map: 305 Lot #: 1 & 2 Zone: Alport Business and Commercial Address / Location of Work: 70 & 80 Corporate Drive Activity Information Proposed Activity (check all that apply) X New Structure Expansion of Existing Structure Other site alteration (specify): Total area of wetland on subject lot: Total area of wetland buffer on subject lot: Distance of proposed structure or activity to edge of wetland: Off subject lot Area of wetland buffer impacted: Fortal area of wetland buffer impacted: Fortal area of wetland buffer impacted: Fortal area of wetland and wetland buffer impacted: Fortal area of wetland sand wetland buffer impac	Application Complete:	Date Forwarded:	Paid:	Check #:
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L-0700-013 May 30, 2018

Mr. Steve Miller, Chairman Conservation Commission City of Portsmouth Planning Department 1 Junkins Avenue Portsmouth, New Hampshire 03801

Re: Lonza Biologics - Proposed Industrial Development
Conservation Commission

Dear Steve:

On behalf of Lonza Biologics, we are pleased to submit the following information to the Conservation Commission to support a request for recommendation of approval to the Pease Development Authority (PDA) for Conditional Use Permit application for a proposed industrial development located at 70 and 80 Corporate Drive on Pease International Tradeport:

- Ten (10) copies of the PDA Conditional Use Permit Application dated May 25, 2018;
- Ten (10) copies of the Site Plan package last revised May 21, 2018;
- Ten (10) copies of the Hodgson Brook Restoration Report prepared by Streamworks dated May 28, 2018;
- Ten (10) copies of the Drainage Memorandum dated May 21, 2018;
- Ten (10) copies of the Wetland Functions and Values Report prepared by GES dated June 16, 2016;
- Ten (10) copies of the Aerial Site Plan Overlay dated May 2018;
- Ten (10) copies of the 1992 Aerial Wetland Overlay Exhibit dated July 1, 2016;
- One (1) copy of the Abutters List;
- One (1) CD containing digital copies (PDF) of the information list above;
- One (1) check in the amount of \$1,000 for the Conditional Use Permit Application fee.

The proposed project will expand Lonza Biologics' facility to support its growing product development services to the pharmaceutical and biologic industries. The proposed project is located on a vacant 24-acre parcel, referred to as the Iron Parcel, that once consisted of row housing and streets for Pease Air Force Base. The houses and roads were removed in the mid to late 1990's as part of the Civil Redevelopment Plan for Pease after the closure of the Air Force Base. These demolition activities resluted in pockets of wetlands that did not previously exist in 1992.

Lonza's existing facilities are located at 101 International Drive which is across Goose Bay Drive from the proposed project site. The existing facility is approximately 800,000 SF in gross floor area and includes approximately 800 employees. Lonza maximized its potential building footprint growth at the 101 International Drive with the completion of a 300,000 SF building expansion project in 2008. In order to continue its growth to further serve existing and new customer demand, Lonza will need to expand its facilities across Goose Bay Drive.

The project will merge 101 International Drive with 70 and 80 Corporate Drive to create a 43-acre parcel for Lonza's campus. This will require that 1,700LF of Goose Bay Drive be abondoned as a public right-of-way and merged with these parcels. The total master plan build-out of the proposed industrial development will include three (3) new buildings totaling approximately 1 milloion square feet of gross floor area and two (2) new parking



garages. The full master plan build-out has the potential to create approximately 1,000 new jobs. This master plan will be constructed in phases with the shell of Proposed Building #1, the building closest to Lonza's existing facility, being constructed as the first phase.

The project will also consist of site improvements that include drive aisles, sidewalks utilities, lighting, landscaping and a stormwater management system with three (3) gravel wetlands and one (1) rain garden.

The project will result in 55,555 SF of wetland impact and 66,852 SF of impacts in Pease Development Authority's 25 FT wetland buffer. As depicted in the enclosed 1992 Aerial Overlay Plan, most of these wetlands did not previously exist when the site consisted of the row housing and streets for the Pease Air Force Base. To mitigate impacts, the project will include a stream restoration project for Hodgson Brook. There is an existing 50-Inch culvert that bisects the parcel which is a buried portion of Hodgson Brook. The project will remove this culvert and daylight the flow through a new 1,000 LF stream channel. This will result in approximately 42,500 SF of restoration area that has a higher function and value than the existing wetlands on site.

Part 304-A.08 of the PDA Zoning Requirements, indicate that the following criteria shall be addressed for a Conditional Use Permit:

1. The land is reasonably suited to the use;

The land is reasonably suited as it is located in the Aiport Business Commercail District and the proposed use is allowed. The parcel is located to the rear of Lonza's exisisting parcel, which allows for expansion of their facility given there is no more room to expand on their existing parcel.

2. There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use;

There is no alterative location outside the wetland buffer given the size and scale of the project. As noted above and shown on the enclosed 1992 Aerial Wetland Overlay Plan, this parcel and most of the wetland buffers proposed to be impacted did not exist 20 years ago, as this site was previously developed with row housing and streets for the Air Force Base.

3. There will be no adverse impact on the wetland functional values of the site or surrounding properties;

The impacted wetland areas are scrub shrub/emergent wetlands with functions and values that are limited to only some potential for groundwater recharge/discharge, flood flow alteration and nutrient removal in small areas. The proposed stream will have a higher function and value. In addition, the proposed Low Impact Design (LID) stormwater management practices will provide stormwater treatment and recharge as described in the enclosed Drainage Memorandum.

4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals;

Alteration of the natural vegetative state will only occur within the limits of the proposed development area. Areas adjacent to existing wetlands along the east portion of Goose Bay Drive will not be disturbed and will be kept in



their existing vegetative state. In addition, the detailed Wetland Planting Plan has been included for the proposed stream.

5. Potential impacts have been avoided to the maximum extent practicable and unavoidable impacts have been minimized.

Potential impacts have been avodied to the maximum extent practicable given the size and scale of the proposed project. To the extent possible, the site design avoids impacts to an existing portion of wetland area closest to Goose Bay Drive that appears to have been a wetland when the row housing and streets existed for the Air Force Base. As shown in the 1992 Aerial Wetland Overlay Plan, the remaining wetlands that are being impacted did not exist when this site was previously developed for the Air Force Base. In addition, impacts to wetlands are being mitigated with the construction of a new 1,000 LF stream channel that will result in approximately 42,500 SF of restoration area that has a higher function and value than the existing wetlands on site that will be impacted.

We respectfully request to be placed on the June 13, 2018 Conservation Commission agenda. If you have any questions or need any additional information, please contact me at 603.433.8818 or pmcrimmins@tighebond.com.

Very truly yours,

TIGHE & BOND, INC.

Patrick M. Crimmins, P.E.

Project Manager

Enclosures

Cc: Lonza Biologics (via email)

DTC Lawyers (via email) Streamworks (via email)

Gove Environmental Services (via email)

Pease Development Authority (via email)



June 16, 2016

Patrick Crimmins, P.E. Tighe & Bond 177 Corporate Drive Portsmouth, NH 03801

Re: Lonza, Corporate Drive, Portsmouth

Subject: Wetland Delineation Report

Dear Mr. Crimmins:

Per your request, this letter is to verify that Gove Environmental Services, Inc., performed a site inspection to identify functions and values for the wetlands delineated at the above-referenced property.

The site consists of predominantly open land once used as row housing. These houses and associated roads and driveways were removed decades ago, as well as the smoothing of the site. This is still evident today through a layer of smooth fill material across the site. Dominant vegetation across the site is grass, and a few mature trees. A large detention pond is located on the site in the central portion, with a riprap bottom and berms along the edge. A large stockpile of material is also present on site and is stable and well vegetated.

Additionally on site are 5 wetland areas. These wetland areas are all isolated on site with some drainage from wetland 4, which drains to the west through a culvert and into Hogdson Brook. Hydrology is predominantly through ground water and some minor influence through sheet flow over the grass surface.

Wetland areas 1 and 4 are similar in make up and are classified as PSS/EM1E, scrub shrub/emergent wetlands, with dominant vegetation of Red maple and American elm in the tree layer, highbush blueberry, speckled alder and gray dogwood in the shrub layer and Cinnamon and sensitive fern, grasses and sedges in the herbaceous layer. Primary functions and values are Groundwater Recharge/Discharge, Flood flow Alteration, Nutrient Removal.

Wetland areas, 2,3,and 5 are also similar in make up and are classified as PEM1E, emergent wetlands, with dominant vegetation of grasses and sedges. Primary functions and values are Primary functions and values are Groundwater Recharge/Discharge, Flood flow Alteration, Nutrient Removal.

Copies of the USACE Highway Methodology sheets are included

If you have any questions or need anything else, please let me know.

Sincerely,

Luke D. Hurley, CWS, SSA

Vice President

Gove Environmental Services, Inc.



Wetland Function-Value Evaluation Form

Total area of wetland: 28,915 sf

Human made? No

Is wetland part of a wildlife corridor? no

or a 'habitat island'?

Wetland ID: 1,4

Adjacent land use Commercial/Industrial

Distance to nearest roadway or other development 50 feet

Latitude Longitude Prepared by: LDH Date 1/7/16

Dominant wetland systems present PEM1E

Contiguous undeveloped buffer zone present no

Wetland Impact: 28,915

Area

Is the wetland a separate hydraulic system? No

Type PEM1E Evaluation based on:

If not, where does the wetland lie in the drainage basin? Lower

Office

How many tributaries contribute to the wetland? 0

Wildlife & vegetation diversity/abundance (see attached list)

Field X Corps manual wetland delineation

completed? Y X

Function/Value	Occurrence Y/N	Rationale (Reference #)*	Princ Func	ipal Comments
Groundwater Recharge/Discharge	Y	1,2,5,6,7,8,15,	Y	This wetland has some Groundwater Recharge/Discharge potential
Floodflow Alteration	Y	3,4,5,6,8,9,10,13,14,16,18	Y	This wetland has some Floodflow Alteration potential
Fish and Shellfish Habitat	N		N	
Sediment/Toxicant Retention	N	1,4	N	This wetland has some Sediment/Toxicant Retention potential
Nutrient Removal	Y	5,6,7,8,9,10,11,12,13	N	This wetland has some potential for Nutrient Removal, but only in small areas
Production Export	N		N	
Sediment/Shoreline Stabilization	N		N	This is not associated with a watercourse
Wildlife Habitat	N	7,8.18,21	N	
Recreation	N			
Educational/Scientific Value	N		N	This wetland has no scientific or educational value
Uniqueness/Heritage	N			
Visual Quality/Aesthetics	N		N	
Endangered Species Habitat	N			
Other				

Notes:

*Refer to backup list of numbered considerations.

Wetland Function-Value Evaluation Form

Total area of wetland: 24,759 sf

Human made? No

Is wetland part of a wildlife corridor? no

or a 'habitat island'?

Wetland ID: 2,3,5

Adjacent land use Commercial/Industrial

Distance to nearest roadway or other development 50 feet

Latitude Longitude

Prepared by: LDH Date 1/7/16

Dominant wetland systems present PEM1E

Contiguous undeveloped buffer zone present no

Wetland Impact: 26,640 Type PEM1E Area

Is the wetland a separate hydraulic system? No

If not, where does the wetland lie in the drainage basin? Lower

Evaluation based on:

How many tributaries contribute to the wetland? 0

Wildlife & vegetation diversity/abundance (see attached list)

Office Field X

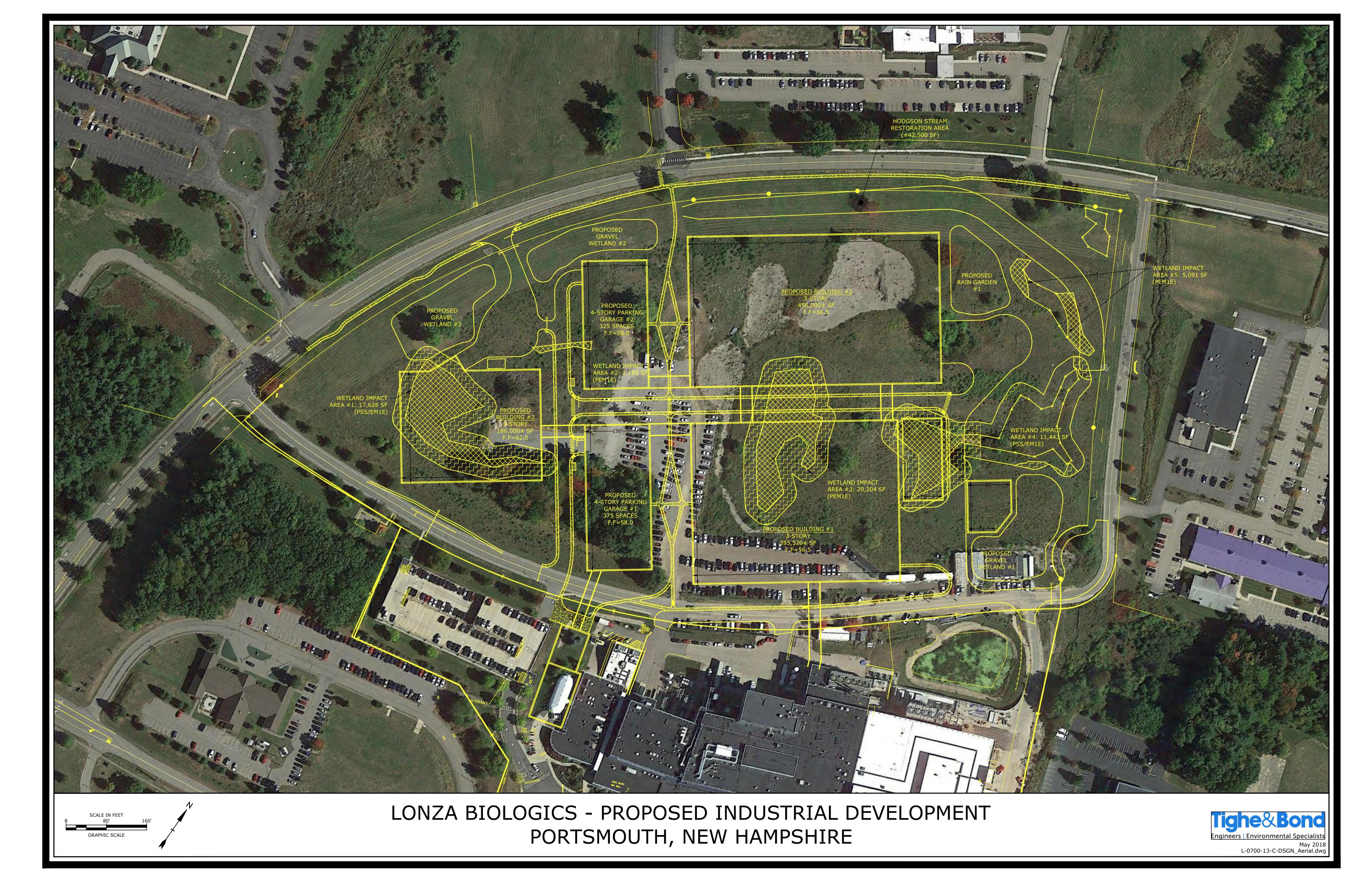
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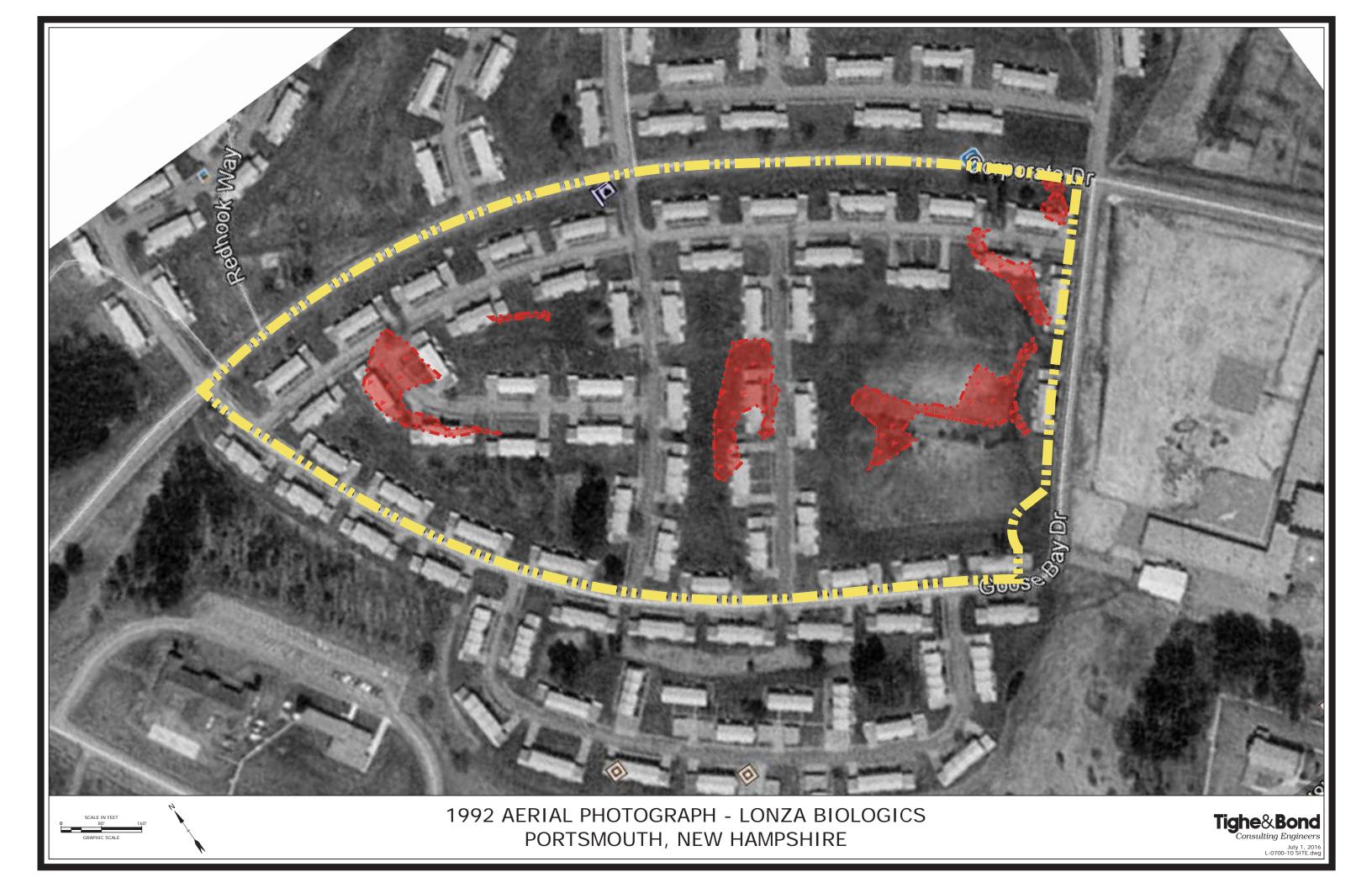
Corps manual wetland delineation

Function/Value	Occurrence Y/N	Rationale (Reference #)*	Princ Funct	ipal Comments
Groundwater Recharge/Discharge	Y	1,2,5,6,7,8,15,	Y	This wetland has some Groundwater Recharge/Discharge potential
Floodflow Alteration	Y	3,4,5,6,8,9,10,13,14,16,18	Y	This wetland has some Floodflow Alteration potential
Fish and Shellfish Habitat	N		N	
Sediment/Toxicant Retention	N	1,4	N	This wetland has little Sediment/Toxicant Retention potential
Nutrient Removal	Y	5,6,7,8,9,10,11,12,13	N	This wetland has some potential for Nutrient Removal, but only in small areas
Production Export	N		N	
Sediment/Shoreline Stabilization	N		N	This is not associated with a watercourse
Wildlife Habitat	N		N	
Recreation	N			
Educational/Scientific Value	N		N	This wetland has no scientific or educational value
Uniqueness/Heritage	N			
Visual Quality/Aesthetics	N		N	
Endangered Species Habitat	N			
Other				

Notes:

*Refer to backup list of numbered considerations.





The Restoration of Hodgson Brook at the Iron Rail Parcel at Pease Tradeport in Portsmouth, NH

28 May 2018

The benefits of stream restoration

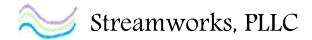
Collecting and processing reference data

Design metrics for the stream and floodplain using natural channel design

Construction sequencing

Planting plan for the floodplain and riparian corridor

Five year monitoring plan and methods



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The Benefits of Stream Restoration

The benefits to stream restoration are numerous to an ecosystem, especially so when land that had been developed into an urban area is reconstructed and allowed to grow more naturally again. This is case throughout history of Hodgson Brook, a stream whose watershed has been almost entirely developed. The watershed for the stream begins at the Pease Tradeport in Newington (though most of the watershed, including the site, is in Portsmouth), and ends in the tidal waters of North Mill Pond in Portsmouth. At the project site and upstream, other than flowing through open drainage ditches and some wetlands, the stream is buried through a network of pipes that carry water flowing directly off impervious surfaces. This system prevents precipitation from filtering into the ground and recharging the groundwater table, a process which otherwise would filter the water from the urban contaminates it collects along its path. With the reduction of water lost into the ground, the amount that ends up directly in the waterway is increased, and commonly, the time it spends in a healthier environment is reduced. The time the water does spend in open channels, is spent under a lack of natural cover where it warms due to a lack of shade and a lack of cooler groundwater inflows that recharge the base flow, and moderate biogeochemical processes. The drainage ditch that is now Hodgson Brook is also poor habitat, lacking a diversity of flora and fauna that exist in a more natural setting.

This project proposes to daylight a section (~1,000 feet along the valley, ~1,200 feet of stream) of Hodgson Brook where it currently lies buried in a 4.5-foot diameter culvert before exiting the project site into a drainage ditch; this stream restoration will result in approximately 42,500 sf of stream and riparian buffer being created.

Daylighting the stream will restore a more natural riffle-pool sequence to a system that when it is presently in the open, is unnaturally straight, having been relocated and straightened to make way for development. The new stream corridor will provide an opportunity for storm flows to enter into the channel and adjacent floodplain, providing a connection for water to reenter and filter into the ground, in addition to being filtered and used by vegetation. The stream and corridor are hydraulically rougher and longer than the existing pipe, and will create a slower travel time over the same valley distance, in addition to increased storage volume. The corridor will benefit from native, riparian vegetation that will be allowed to grow unmaintained, encouraging wildlife use, nutrient/pollutant removal, and shade to keep the water cool. The habitat will help filter out common pollutants such as nitrogen and phosphorous, all while reducing the amount of contaminated water that enters North Mill Pond. Obviously this is one piece of a greater system between the Tradeport and North Mill Pond, therefore while the benefits of this specific projects are very high, it should be recognized that there are other impairments along the watershed also in need of attention.

The restoration work will provide a reconnection for a portion of a watercourse that has been heavily altered in the past, and hopefully provide an example of how a stream corridor may be restored in an urban environment and serve as a reference for the future.

Collecting and Processing Existing Data

Natural Channel Design involves obtaining metrics that are measured on natural, healthy systems (reference stream) which are then employed to serve as a template for the design metrics to the impaired watercourse, as long as the watersheds and streams have similar properties. It is not uncommon for this reference stream section to exist in healthy sections of the same stream, or at sections of adjacent streams. In the case of Hodgson Brook, unfortunately there is no existing healthy/natural/undeveloped section to observe, as most of the stream and its watershed exhibit significant urbanization and lack of stormwater management. There also exist few nearby streams that meet the criteria of being healthy, natural, and relatively unaltered that also share similar watershed characteristics; arguably, there exist few healthy, natural, and relatively unaltered streams anywhere that have highly impervious watersheds and little vegetation with such low stream slopes and are located near the New Hampshire coast. Simply put, there aren't many healthy streams (to say nothing of natural) that exist in an urban environment. In this case, the stream should aim to mimic its historic, natural system as best as possible while accounting for the upstream watershed conditions.

Luckily, there exists a relative wealth of information that has already been collected about the history of the Hodgson Brook watershed, the development over the years, how it exists now, and goals for restoring it. A 2004 restoration plan for Hodgson Brook was prepared by D. B. Truslow Associates with cooperation from the Hodgson Brook Local Advisory Committee, with funding provided by NHDES. This publication (among others) is available online at the DES' website for the watershed. The publication contains much information about the history of the watershed, which provides a good place to start in order to find a relevant reference reach.

After reading the report, two sites were identified as having been restored at Pease – Grafton Ditch and Railroad Brook. Upon investigation of the two sites, and taking some brief measurements, neither site was suitable for use as a reference reach for Hodgson Brook. Stream form measurements were taken on Hodgson Brook, immediately at the outlet from the Iron Rail Parcel – where the stream is in no way natural or healthy, but years of flowing through the drainage ditch there has allowed the confined brook to erode some of the banks, and establish some plan form geometry, and can provide metrics on what the channel is able to pass currently. Classification of this section of stream, and the parameters used for evaluating the classification, may be seen in Table 2 below. The pipe system through the site was also surveyed, which provided the controlling upstream and downstream elevation, as well as the valley length.

Knowing the valley slope, the historic properties of the watershed, and approximate metrics from the regional geomorphic curves developed for New Hampshire, a dozen or so reference reaches were walked and visually assessed around the seacoast area. The most representative of all the reference reaches, Hutchins Creek in Kittery (43.106989°N, 70.705805°W), was then surveyed for plan form, cross sections, profile, and geomorphic properties. Overall, a 150-foot section of Hutchins Creek was surveyed (channel and floodplain). Planform geometry was collected for seven riffle-pool sequences over four

¹ The website is located at: https://www.des.nh.gov/organization/divisions/water/wmb/was/hodgson/index.htm

meander wavelengths along the valley. Profiles of the thalweg, top of bank, bankfull, and water surface elevation were all collected. A total of 11 cross sections (7 riffles and 4 pools) were taken at locations where bankfull indicators were evident, and for each section all stream and floodplain widths, depths, and ratios were extracted and calculated. Of those, the sections were weighted according to which appeared to be the healthiest and most stable in the field.

The parameters for the Hodgson Brook and Hutchins Creek watersheds may be found in Table 1, and the geomorphic metrics for the profile, cross section, and planform of Hutchins Creek in Table 3 and Lower Hodgson Brook in Table 2b. Select values from the observed particle size distribution (done by pebble counts) for Lower Hodgson Brook may be found in Table 2a — with a plot of the data found in Figure 1. Additionally, planform and cross sectional definitions are shown on pages A1 and A2 of the Appendix, for reference.

Table 1 - Watershed Properties								
Property	Code	Units	Lower Hodgson Brook	Hutchins Creek				
Drainage Area	DA	mi ²	0.32	0.4				
2-yr Peak Flow	Q2	cfs	6.80	6.46				
5-Yr Peak Flow	Q5	cfs	11.1	14.332				
10-yr Peak Flow	Q10	cfs	15.5	18.359				
25-yr Peak Flow	Q25	cfs	24.0	24.008				
50-yr Peak Flow	Q50	cfs	38.2	28.463				
100-yr Peak Flow	Q100	cfs	53.0	33.409				
Pipe/Valley Slope	S	ft/ft	0.01057	0.00176				

Table 2a - Particle Size Results Pebble Counts at Lower Hodgson Brook						
Particle	Size (mm)	Size (in)				
D10	0.19	0.007				
D50	0.38	0.015				
D80	1.5	0.059				
D90	7	0.276				
D95	14	0.551				

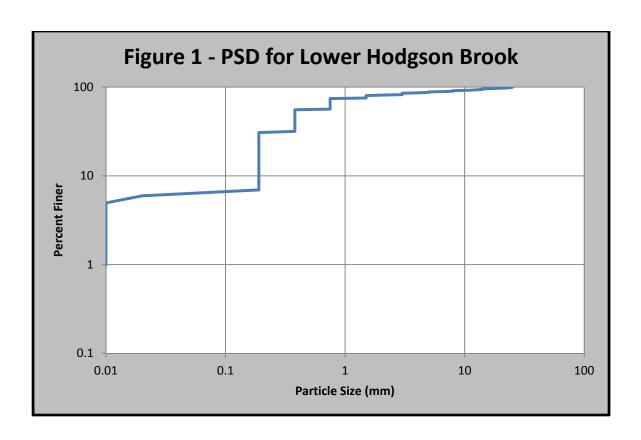


	Table 2b - Lower	Hodgso	n Brook	Referenc	e Reach D	ata	
	Characteristic	Code	Units	Lower Hodgson Brook Observatio			
	Characteristic	Code	Units	1	2	3	4
	Stream Slope	S	ft/ft	0.00316			
е	Valley Slope	V_s	ft/ft	0.00565			
Profile	Sinuosity	k		1.072			
P	Pool Length	L_p	ft	9.2	5.3	20.6	10.6
	Pool to Pool Spacing	P-P	ft	18.7	11.1	22.6	37.6
	Bankfull Width	W_{bkf}	ft	5.76	4.60	3.69	5.54
ion	Floodprone Width	W_{fp}	ft	7.03	9.35	6.26	9.67
Cross Section	Maximum Bankfull Depth	D _{max}	ft	0.89	0.76	0.62	0.80
SS S	Average Bankfull Depth	D_{avg}	ft	0.55	0.44	0.51	0.40
Cro	Entrenchment Ratio	ER	ft/ft	1.21882	2.03221	1.69578	1.74704
	Width to Depth Ratio	W/D	ft/ft	10.4979	10.486	7.21621	13.8066
	Radius of Curvature	R_c	ft	40.66	15.81	22.41	8.93
	Arc Length		ft				
	Average Bankfull Width	W_{bkf}	ft	5.8	5.5	5	4.6
8	Rc:Wbkf Ratio		ft/ft	7.01	2.87	4.48	1.94
Plan Form	Meander Belt Width	MBW	ft	13.1	16.9	14.7	
an	Average Bankfull Width	W_{bkf}	ft	4.6	5	5.8	
Ы	MBW/Wbkf		ft/ft	2.85	3.38	2.53	
	Meander Length	ML	ft	56.04	56.53	46.32	
	Average Bankfull Width	W_{bkf}	ft	5.8	5	4.6	
	ML/Wbkf		ft/ft	9.66	11.31	10.07	
	Entrenchment Ratio	ER	ft/ft	1.21882	2.03221	1.69578	1.74704
Classification	Width to Depth Ratio	W/D	ft/ft	10.4979	10.486	7.21621	13.8066
	Sinuosity	k		1.072	1.072	1.072	1.072
	Stream Slope	S	ft/ft	0.00316	0.00316	0.00316	0.00316
Cla	Bed Material	-	-	Sand	Sand	Sand	Sand
	Classification	-	-	G5c	B5c	G5c	G5c

	Table 3 - Hutchins Creek Reference Reach Data													
	C	Hutchins Creek Observations												
	Characteristic	Code	Units	1	2	3	4	5	6	7	8	9	10	11
	Stream Slope	S	ft/ft	0.00165										
e	Valley Slope	V_s	ft/ft	0.00176										
Profile	Sinuosity	k		1.20										
Ы	Pool Length	L_p	ft	10.9	7.3	1.4	9.8	11.5	10.3	3.7				
	Pool to Pool Spacing	P-P	ft	24.4	13.5	14.6	15.1	15.1	21					
	Bankfull Width	W_{bkf}	ft	7	6.5	6.5	5	5	7	5.5	5.5	6	5.5	5.0
ion	Floodprone Width	W_{fp}	ft	25	18	20	30	20	30	20	20	25	39.1	37.8
Section	Maximum Bankfull Depth	D_{max}	ft	0.68	0.62	0.55	0.65	0.58	0.96	0.87	0.65	0.64	0.69	0.74
	Average Bankfull Depth	D_{avg}	ft	0.476	0.434	0.385	0.455	0.406	0.672	0.609	0.455	0.448	0.38	0.48
Cross	Entrenchment Ratio	ER	ft/ft	3.57	2.77	3.08	6.00	4.00	4.29	3.64	3.64	4.17	7.11	7.60
	Width to Depth Ratio	W/D	ft/ft	14.71	14.98	16.88	10.99	12.32	10.42	9.03	12.09	13.39	14.42	10.38
	Radius of Curvature	R_c	ft	11.8	7.6	8.3	9.6	7.6	15.3	3.7	13.6			
	Arc Length		ft	16.3	7.0	10.1	11.6	8.1	13.6	7.4	12.0			
	Average Bankfull Width	W_{bkf}	ft	4.8	4.0	4.0	4.6	3.3	3.8	3.4	5.0			
_	Rc:Wbkf Ratio		ft/ft	2.48	1.91	2.07	2.08	2.33	4.02	1.10	2.72			
Form	Meander Belt Width	MBW	ft	14.5	13.5	10.0	10.5	9.0	17.0					
Plan	Average Bankfull Width	W_{bkf}	ft	5.0	4.5	4.5	4.0	4.0	5.0					
Ы	MBW/Wbkf		ft/ft	2.90	3.00	2.22	2.63	2.25	3.40					
	Meander Length	ML	ft	40.1	23.8	27.2	30.4	30.3	36.0					
	Average Bankfull Width	W_{bkf}	ft	5.0	4.5	4.5	4.0	4.0	5.0					
	ML/Wbkf		ft/ft	8.02	5.28	6.04	7.59	7.57	7.20					

Design Metrics for Stream and Floodplain Using Natural Channel Design

The natural channel design process uses the collected reference reach data to develop proposed metrics to create a design which is controlled by site constraints (usually things like incoming flows, upstream and downstream invert elevations, valley width, sediment supply, etc.). The site constraints control selected design metrics, which then are used to calculate – often quite iteratively – the remaining metrics within a range, determined by the reference reach data. The constraints at the project site include the stream inverts at the start and end, the valley width, the watershed properties, and the flows incoming to the site. The most difficult of all the constraints to calculate for this project were the flows incoming to the site. Upstream of the site, the watershed is extremely developed, and in order to calculate flows using common methods (Rational Method, SCS Curve Number Method, regression equations, etc.), a full watershed model would have been necessary. Such a model could have been developed, but the output may not have been very applicable to determining channel-forming flows. The dominant channel-forming flow is referred to as the bankfull flow, and for undeveloped watersheds is commonly in the range of the 1.5 to 2 year peak flow. However, this is just an approximation, and is not globally true for all watersheds and streams. The actual channel-forming flow may have a more or less common return period, and that is the flow to which the channel should be designed.

In order to appropriately estimate what this flow might be, a more site-specific method was used. Immediately downstream of the site, Hodgson Brook has – for decades – existed in an overly deep drainage ditch with no access to a floodplain. Over those years, it has eroded the banks during larger flows, and created some observable bankfull indicators. Using the survey data taken at this location, with specific data taken at bankfull locations, flows could be calculated to estimate what the channelforming and larger flows likely would be. The flows that formed the more natural sections of the unnatural drainage ditch may be assumed to be the same as what would flow in Hodgson Brook at the site. The return period of these flows were not estimated; rather, the flows which caused bankfull indicators were called the bankfull flows. In theory, the bankfull flow is the flow at which sediment is transported most efficiently; or the discharge at which channel maintenance is most effective. This happens in healthy streams, on average, around the 1.5- to 2-yr flow. For the stream and watershed at the site – the watershed being highly impervious, and lacking a consistent sediment supply – the rate of return of the bankfull flow would be much harder to state in terms of return period. This is why the use of indicators downstream of the site, coupled with the survey of those indicators and the stream, was determined the best way to account for the bankfull flow. These calculated bankfull flows may be found in Table 1. Similarly, the maximum flow - though there is no return period placed on it - can be determined by the constraining factors of the stream system upstream of the restoration. The proposed pipe diameter, material, and slope were used to assume inlet control (no effect of the stream system on the pipe's ability to move water), and calculate the maximum amount of water which may be seen in the system. A quick Manning's Equation check showed that that flow would not overtop the stream corridor valley walls. Regardless of when this flow or any other flow higher than the bankfull overtop the stream banks, the goal of the design metrics were to use as much floodplain as possible, allowing the

flows to interact with the floodplain as frequently as they will, while containing the bankfull flow (regardless of return period).

Knowing all the constraints at the site, the metrics controlled by the constraints were calculated, and the remaining design metrics were iteratively determined to conform to the flows as best as possible. The calculated metrics and constraining variables may be found in Table 4. These proposed metrics were given as a guide for design – they don't have to be followed exactly, but should be near to or within the range of values shown in the table. They are dependent on the controlling factors, such as inlet and outlet inverts, which may adjust the values within the ranges shown (or, if outside the ranges, the metrics may be adjusted based off the ratios shown: entrenchment ratio, width to depth ratio, poo

In addition to the designed stream metrics, several other site-specific factors are important to consider, and should be accounted for in the design. Due to the highly developed nature of the watershed, the sediment supply to the site will be quite limited. There is not much of a source of sediment, other than construction activities and sanding during the winter. Thus, the sediment supply is sure to be of a much finer gradation and in much more limited supply than the natural stream used to have. Because of this, vegetation will be very important to maintaining the stream structure, and the sediment gradation used for construction will need to be sized and mixed well to prevent against vertical erosion of the restored stream. In addition to the vegetation and sediment, in-stream structures (log cross vanes) are recommended to help keep the stream in place, and floodplain sills are recommended to help prevent against avulsion. To help the stream keep its form while vegetation is allowed to grow, the banks may be constructed out of biodegradable compost sock. These usually have a lifespan of 3-5 years before they begin to degrade, which should allow enough growing seasons for faster growing riparian vegetation and plants to take root and hold the stream form. Please refer to Figure 2 for a better idea of how these banks are to be used, and what one such project looks like four years after construction. These coir log banks should also provide stability, and help prevent against any avulsions, though the floodplain and channel should be able to handle them on their own.

Some of the design metrics may be seen on pages A3 and A4 of the Appendix, for reference of what part of the stream they apply to, and their values. A more complete table of the proposed metrics may be found on pages A15 and A16 Conceptual details for constructing a log cross vane and a floodplain sill may also be found in the Appendix, on pages A5 and A6.



Figure 2 - Coir Log Rolls along Restored Pettee Brook, near Adams Towers on UNH Campus in Durham, four years after construction. Note how the coir logs are still intact, and have trapped sediment. Roots and grasses have grown into and through them.

Та	ble 4 – Hodgson Brook Propo	sed Stre	am Me	trics and f	Ranges	
	Property	Code Units Value Rai (+,				
	Maximum Bankfull Depth	Dmax	ft	0.75	0.1	
tion	Average Bankfull Depth	Davg	ft	0.50	0.1	
ion	Floodprone Depth	Dfp	ft	1.50	0.2	
Cross Section	Bankfull Width	Wbkf	ft	5.5	0.5	
58 5	Floodprone Width	Wfp	ft	30.0	2	
Cro	Width/Depth Ratio	W/D	-	11.0	1.3	
	Entrenchment Ratio	ER	-	5.5	0.1	
	Bankfull Area	Abkf	sqft	2.75	0.8	
	Sinuosity	k	-	1.23	0.05	
	Meander Belt Width	MBW	ft	18.0	2	
٦	Meander Length	ML	ft	40.0	5	
Forr	Radius of Curvature	Rc	ft	12.5	2.5	
Plan Form	Pool Length	Lp	ft	16.2	4	
	Pool to Pool Spacing	P2P	ft	24.5	4.5	
	Stream Slope	Slope	ft/ft	0.00946	0.0020	
	Valley Slope	VS	ft/ft	0.01160	0.0010	
,	Low Flow	Qlf	cfs	0.2	0.1	
Flow	Bankfull Flow	Q	cfs	6.9	0.4	
ш	Floodprone Flow	Qfp	cfs	32	2	
	Low Flow - Rosgen	RDIf	in	0.7	-	
	Bankfull - Rosgen	RDbkf	in	2.5	-	
	Floodprone - Rosgen	RDfp	in	2.8	-	
ze ze	Full Flow - Rosgen	RD100	in	5.7	-	
e Si	Low Flow - LWM	LDIf	in	0.2	-	
ticl	Bankfull - LWM	LDbkf	in	0.9	-	
Par	Floodprone - LWM	LDfp	in	1.1	-	
Stable Particle Size	Full Flow - LWM	LD100	in	2.9	-	
	Low Flow	LDIf	in	0.4	0.3	
	Bankfull	LDbkf	in	1.7	0.8	
	Floodprone	LDfp	in	1.9	0.9	
	Full Flow	LD100	in	4.3	1.4	

Construction Sequencing

In general, stream restoration begins at the upstream end of the project and works downstream. At the site, the proposed stream corridor does not follow the path of the existing piping carrying Hodgson Brook, but will be reconnected to the infrastructure at the start and end of the project. This is beneficial, as the stream can be constructed in the dry and temporarily stabilized before being opened up to flows and fully vegetated. As this is a part of a larger development project as a whole, the construction sequence below details only activities pertaining to the stream corridor. It does not include activities that might usually be included in such a sequence, such as (but not limited to) clearing and grubbing, construction layout, traffic control, erosion control, and material disposal. The sequence is subject to change to integrate fluidly with the entire project, and may change to the desires of the contractor, as they see best fit. Any changes shall be discussed, cleared, and/or proposed by project engineers, and may be made in the field during construction. This construction sequence assumes that the existing drainage infrastructure is to remain in place until the stream is built, and that proposed drainage infrastructure that will direct flows into the stream will have already been installed. An overview of the sequence is listed below, followed by a detailed sequence which describes each step in greater detail.

Stream Corridor Construction Sequence Overview:

- 1. Excavate and grade the stream corridor from the top of the valley, down to the top of the floodplain, and on down towards the center of the corridor.
- 2. Perform fine grading of stream channel, banks, structures, and sills.
- 3. Seed the site with temporary stabilization and allow to grow.
- 4. Open up stream at each end to flows.
- 5. Seed and plant the site fully.
- 6. Establish monitoring locations and components.

Detailed Stream Corridor Construction Sequence:

- 1. Excavate and grade the stream corridor, from the top of the valley, down to the top of the floodplain and into the center of the corridor, leaving an access ramp at the start and end of the project. If required, the grade may be set lower to allow for backfilling of loam, should the existing earth be of poor material. Do not over-compact floodplain or valley slopes; compact only by track-walking or applying pressure with the bucket of the excavator. The floodplain and slopes should be left rough, to allow seed to grow more easily. Leave an access path along the top of the valley to one or both sides, to allow for the transport and temporary staging of instream materials and movement of heavy equipment. This may also be done by using the upstream access ramp to deliver materials behind the excavator, using the corridor as the path. This is not preferred, since over-compaction is likely to occur resulting from the excessive use.
- 2. Because the construction will be performed in the dry, construction will start at the downstream end of the restored Hodgson Brook. Starting at the downstream end of the stream, begin by excavating the pool which will redirect water into the existing culverts below Goose Bay Drive from upstream of the pool. Working from upstream of the section under construction, begin the fine grading of the stream channel. This may be done by over-excavating the channel and banks,

then installing the compost log roll stream banks. Initially the bed slope of the stream is graded uniform, and then riffles and pools graded near the finishing steps. The lower compost log should sit below the thalweg of the stream, and once set in place at the correct elevation, may have fill placed behind the rolls. The stream channel should then be backfilled at the riffles and pools with appropriately graded material, leaving the pools as deeper features in the stream channel. As construction continues upstream, merging the compost log rolls should be done such that the upstream-most end of the rolls is curled out from the bank, such that the next upstream rolls may be placed linearly into the bank, and flows will be directed as to not cause erosion or avulsion between the rolls (shiplapped construction). Extra heavy attachment (connections) of the rolls at these locations should be performed with biodegradable materials. While construction continues, backfilling of any floodplain loam – should it be deemed necessary - should be performed to the final grade of the floodplain. Construct in-stream structures (log cross vanes) as they are reached, as well as floodplain sills. Additional floodplain features may be constructed at this time, such as habitat logs and boulders, tree stands, and vernal pools (all optional, but recommended). Construction materials may be provided ondemand using the access path along the top of the valley. Materials (logs, rebar, geotextile, riffle material, compost rolls, etc.) may be set outside the stream corridor, and gathered by the excavator from inside the corridor, or less preferably, placed behind the excavator in the corridor. All fine grading and structures should be checked for elevations and geomorphic metrics before starting the next upstream section.

- 3. Seed and mulch the corridor and top of valley with the temporary stabilization seed mix (preferably a conservation mix with at least 10% wildflower seeds, though may be of a perennial ryegrass). Seed to the amounts as specified by the seed manufacturer with greater application on the steeper valley slopes and mulch with wood chips (90% ground coverage) or straw (to a depth of 1 inch). Water as specified by the seed manufacturer, if drought persists longer than the recommended watering rate. Allow the grass to grow to a height of 2 inches before proceeding to the next step. If any bare patches exist, reseed and mulch to ensure stabilization. This step may be performed as a section of stream is constructed, which may reduce the overall construction duration, though it may come at a cost of increased watering effort.
- 4. When all previous steps have been completed, the stream should be opened up to flows. First, the existing drainage culvert at the downstream end should be excavated and removed. Grade and temporarily stabilize the incoming flows to the downstream pool. Proceed to the inlet to the stream and construct (if not already done in step 2) the inlet pool and grading. Flows may then be directed into the stream channel, in a manner that shall be determined in the field, based on the manner in which the incoming culvert and upstream infrastructure is being constructed. Allowing incoming flows to the stream may be performed concurrently with that of the outlet, provided the contractor has the labor and equipment available. However, caution should be exercised to ensure that flows are able to exit the corridor fully and appropriately, to prevent damage and/or flooding to the site.
- 5. With the stream now carrying flows, the entire site should be seeded and planted as specified in the planting plan. This may be done completely or partially as construction of the stream takes place. At this point the temporary stabilization grass should have taken hold enough to provide

some cover for seeds, and keep in moisture during the day. This step should only be done during a growing season and not in mid-summer or winter, to help ensure planting success. This step may be done after step 6, if construction ends before a planting season is set to begin. This step should be performed when the appropriate equipment is available. This may help expedite the process, rather than performing it all completely by hand.

6. Finally, monitoring devices and components should be installed, measurements recorded, and instruments calibrated as necessary. Please refer to the monitoring plan section of this report for more details on the monitoring methods and schedules.

As noted in the detailed construction sequencing, some aspects of construction may overlap, or may be done concurrently, per the desires of the contractor. For example, backfilling of loam may be reserved for after the stream has been constructed, if it is desired to be performed from the top of the valley. Planting of livestakes and other riparian plants may be done as the stream is constructed. This may require watering to be performed regularly, especially lower on the floodplain, to ensure the vegetation has enough water to grow without any baseflow in the stream. It may also require longer stagnant time for the plants, which would have to be kept healthy during the duration of the construction. More detailed information and planting notes may be found in the following section. Habitat features (floodplain boulders, logs, vernal pools, etc.) may be constructed after the stream is finished, from the top of the valley. As stated before, any alterations to the construction sequence will first be cleared by the project engineers before implementing them during construction.

Planting Plan for the Floodplain and Riparian Corridor

The stream corridor has two distinct zones for planting: the floodplain (Zone 1) and the upland, or valley slopes (Zone 2). These two zones are set as such, based on the available water, rate of inundation, and the drain rate. The two zones were broken down even further, with each zone having a Lower and an Upper part (1L, 1U; 2L, 2U). Furthermore, Zone 1L contains an additional sub-zone that refers to the stream banks, just up onto the top of the banks. Here, grasses and groundcover is often not successful, but shrubs may, and these are to be planted differently than the rest of Zone 1L, resulting in its own classification. This sub-zone contains two sections, one along the outer bank of each bend, and the other containing all the other banks (inner bend and riffles). The outer bank of each pool is referred to as Zone 1Lp, and the other banks are in Zone 1Lb. The difference in the two zones is only to differentiate between planting densities, and to help determine quantities.

Table 5 – Planting Plan Species							
	Planting Species	Common Name	Zone				
	Lolium Perenne	Perennial Ryegrass	1, 2				
	Cornus canadensis	Bunchberry	1U				
Grasses	Solidago spp.	Goldenrod	1				
	Impatiens capensis	Jewelweed	1				
	Mitchella repens	Partridgeberry	1U, 2				
	Asclepias incarnata	Swamp Milkweed	1				
	Thalictrum polyganum	Tall Meadow Rue	1				
	Prunus virginiana	Chokecherry	1U, 2				
	Cornus racemosa	Gray Dogwood	1U, 2				
	Viburnum alnifolium	Hobblebush	1				
	Vaccinium angustifolium	Lowbush Blueberry	2				
sqr	Salix discolor	Pussy Willow	1				
Shrubs	Rubus idaeus	Raspberry	2				
0,	Cornus stolonifera	Red Osier Dogwood	1				
	Cornus amomum	Silky Dogwood	1				
	Alnus rugosa	Speckled Alder	1				
	Hammamelis virginiana	Witch Hazel	1				
	Salix nigra	Black Willow	2U				
	Prunus serotine	Black Cherry	2U				
Trees	Acer rubrum	Red Maple	2U				
Tre	Quercus alba	White Oak	2U				
	Fraxinus americana	White Ash	2U				

The species selected for the project are listed in Table 5, and are sorted by the type of species – grasses and ground cover, bush-like trees and shrubs, and trees. Each species is listed by both their common name and Latin name, as well as the zone at which it is to be planted. The zone for each may be listed specifically (1L), or more broadly (2). These species were selected from the list of Native Shoreland/Riparian Buffer Plantings for New Hampshire; a table species which are both native and non-

invasive, which was published by the NH Department of Environmental Services. While this list provides many species, the final species used in construction of the site may not be limited to those listed. Any other species will be checked and approved by the engineer before being ordered, or placed in the field. This is especially true of any seed mix that may be used at the site; the selected mix (mixes) that the contractor shall use should be checked by the engineer before placement, or before ordering any such seed mix.

A list of densities and species to be planted in each zone may be found in Table 6, for quick reference.

	Table 6 – F	Planting Plan Details	
Planting Zone	Zone Description	Species	Density
1Lр	On the outer bend of a pool from the point of curvature to the point of tangency, beginning at the mid-bank elevation, up over the top of the bank, and offset from the top of the bank 1 foot.	Livestakes of Pussy Willow, Red Dogwood, Silky Dogwood, and Speckled Alder	2 livestakes per 1 sf
1Lb	From the mid-bank elevation up over the top of the bank and back 1 foot, for all stream banks other than Zone 1Lp	Livestakes of Pussy Willow, Red Dogwood, Silky Dogwood, and Speckled Alder	1 livestake per 2 sf
1L	From one outer bend of the channel down one meander wavelength to the next outer bend of the channel, inwards along the top of the bank.	Perennial Rye (temporary stabilization); Native Wetland Seed Mix including but not limited to: Tall Meadow Rue, Goldenrod, Swamp Milkweed, Jewelweed, and Ryegrass; Hobblebush, Pussy Willow, Red Dogwood, Silky Dogwood, Speckled Alder, and Witch Hazel	Rye: per seed mix Wetland Mix: per seed mix Shrubs: 1 plant per 75 sf
10	On the floodplain bench, outside the meander belt width corridor, up to the top of the floodplain bench	Perennial Rye (temporary stabilization); Native Wetland Seed Mix (as described previously); Bunchberry, Partridgeberry, Swamp Milkweed, Chokecherry, Gray Dogwood, Hobblebush, Pussy Willow, Witch Hazel	Rye: per seed mix Wetland Mix: per seed mix Shrubs: 1 plant per 50 sf
2L	From the top of the floodplain bench, up 1/4 of the way up the riparian corridor slope	Perennial Rye (temporary stabilization); Native Conservation Seed Mix; Partridgeberry, Chokecherry, Gray Dogwood, Lowbush Blueberry, Raspberry, Black Willow	Rye: per seed mix Shrubs: 1 plant per 20 lf
2U	From the top of Zone 2L, up over the top of the riparian corridor and back 1 foot.	Perennial Rye (temporary stabilization); Native Conservation Seed Mix; Lowbush Blueberry, Raspberry; Black Willow, Black Cherry, Red Maple, White Oak, White Ash	Rye: per seed mix Shrubs: 1 plant per 25 lf Trees: 1 tree per 40 lf

Vegetating the project site will be done using several types of planting methods. Closest to the stream, livestakes should be placed, rather than planting full shrubs. Livestakes are relatively straight clippings two to four feet in length and no greater than an inch in diameter at the base, cut from live and healthy species, and should be cleared from leaves and smaller branches. Leaves left on the livestake cause it to dry out more easily. From places where branches and buds are removed, roots and new branches will sprout from the clipping. Livestakes should be soaked in water for at least two days prior to installation, if at all possible, long enough for roots to sprout. To plant a livestake, first create a hole using a sledge hammer and a hammer rod (a piece of 1" diameter rebar works as well), to a depth of one third the length of the livestake. Gently place the livestake in the hole without damaging the base, and tampdown the ground around the hole with a hand or foot. Livestakes should be kept wet for the first two weeks, until they have had the opportunity to sprout roots.

Seed will also be placed and mulched as described following, all along the floodplain and upland slopes. Seeding will first be done with a rye grass to stabilize any bare earth expected to exist longer than 5 days. The floodplain may then be seeded with a wetland, riparian, or conservation seed mix that contains no invasive or non-native species. Seeding with such a mix should follow the manufacturer's guidelines. A general specification for the final seeding is a conservation mix with at least 10% wildflower seeds.

Finally, planting of trees and shrubs (and flowering plants, should no wetland/riparian seed mix be used) will be performed throughout the floodplain and upland areas. It is preferable to have mature plants over planting seeds, and more mature plants are preferred to saplings. Younger plants are more vulnerable to being transplanted, and do not recover well – if at all – from grazing. Again, trees and shrubs should be placed in their appropriate zones, and should be planted in a non-linear fashion.

To begin the planting, first the grounds should be checked for any invasives, or any debris/trash, and cleared. Seeding should occur over the entire construction area, and should begin with temporary stabilization. Stabilization should be of a Rye seed mix, which should be mulched with straw, preferably (to a depth of 1"). The mulch should be clean and free of invasives and any other contaminants. The grounds should be watered as necessary, or as specified by the seed manufacturer. At the same time, livestakes (if they were not already set during construction) may be placed in the stream banks and at the top of the banks.

After the grass has been allowed to grow, and any bare spots have been reseeded, planting and seeding of the remaining site may be performed, beginning at the lowest part of the floodplain, on up to the top of the valley slopes. Protective tubing may be desirable to help prevent any young plants from grazing before they reach a more adult size. Support stakes and twine may also be used, to help stabilize the plants until they develop larger root systems. Planting instructions for each plant should be followed, as some require more specific needs than others, and may even have different planting seasons when they should be installed. The instructions for each may be very important, as a survival rate of 75% within the first 3 years is commonly determined to be the goal of a restoration project in New Hampshire.

When performing the final planting, it is important to note that the densities shown are for an average over the corridor, and to help determine quantities. Plantings should be performed in a non-linear (irregular) fashion, and should avoid being homogenous. Some areas should be more or less dense, with greater or fewer different species than other areas. Trees in the upland should be planted at the top of the valley, and partway down the slope; bushes may be clumped together near or far from the channel; livestakes should be planted mid-bank and to the top of the bank. The zones and densities are shown for reference, but are not firm constraints. Natural systems are usually very diverse and random, and projects should attempt to embrace and mimic that variability. In addition to Tables 5 and 6, a list of the wildlife which benefit from the planting species, as well as the food value each species provide, may be found in Table A1, on pages A7 and A8 in the Appendix.

Five Year Monitoring Plan and Methods

Hodgson Brook is the main source of fresh water to North Mill Pond in Portsmouth, and as such, the health of the stream is important to several local organizations (Advocates for the North Mill Pond [ANMP], Hodgson Brook Local Advisory Committee [HB LAC], Pease Development Authority [PDA]), and governments (city of Portsmouth, NH DES). There have been several studies completed on the watershed that are publicly available, and quite a few documents published that cover the history, water quality, and goals for restoring the watershed. Some of the publicly available documents include²: an Environmental Quality Characterization for Hodgson Brook in Portsmouth, New Hampshire (2003), a Watershed Restoration Plan for Hodgson Brook (2004), a Hodgson Brook Watershed Monitoring Plan — A guide for Monitoring Environmental Quality (2004), and an Implementation Plan for Hodgson Brook Watershed Restoration (2005). These documents provide detailed accounts of the history of the watershed, the current use and quality, and sets goals for restoring the watershed and methods to achieve those goals. The information provided in those documents was used to help develop the monitoring plan for the site. Monitoring of the site will be performed for five years after the construction of the project.

The NH DES lists water quality standards that provide a framework for assessing surface waters in the state, based on seven designated uses. The standards are divided into three parts: designated uses, water quality criteria, and antidegradation. The seven designated uses represent the ways in which the surface water is intended to be used: aquatic life, fish consumption, shellfish consumption, drinking water supply, primary contact recreation, secondary contact recreation, and wildlife. The water quality criteria are defined for each designated use by markers and limits, aimed at protecting each surface water use. Finally, the antidegradation provision is set to protect existing uses and to prevent any degradation to any surface water in terms of the existing water quality or designated uses.

Hodgson Brook (as detailed in the Watershed Monitoring Plan [WMP]), has been assigned three designated uses for which monitoring should be performed: Primary and Secondary Contact Recreation, and Aquatic Life. Indicators for each, and the recommended monitoring methods, were defined in the WMP, and are listed below. The methods and indicators below were cropped to eliminate indicators and methods that the report either did not recommend, or were considered not applicable. Also not included are some of the recommended monitoring methods that may not be applicable or may be included within other methods. Some of the monitoring frequencies have been adjusted in order to provide better data for a restoration project, and not existing conditions. In addition to the recommended monitoring methods given in the WMP, methods for monitoring the vegetation and stability of the constructed stream were developed. The full list of monitoring methods, schedules, and frequencies may be found in Table 7.

An annual monitoring report shall be produced and sent to all interested parties (ANMP, HB LAC,NH DES, etc.) and all data provided to NH DES for inclusion in the state databases at the same time. Please

² All four documents may be found at the DES website for Hodgson Brook: https://www.des.nh.gov/organization/divisions/water/wmb/was/hodgson/reports.htm

refer to state protocols for data reporting; different data may require different protocols. DES may also provide sampling kits and training for collecting select methods and indicators (1, 2, 3, 4, 5, and 10) through their Volunteer River Assessment Program (VRAP). The monitoring report should be produced annually in January or February, which gives enough time to process all the data collected during the previous year, and is after any sampling, vegetation monitoring, or surveying is likely to be done.

		Table 7 - Iron Rail P	arcel Restoration Monitoring Method	s and Sche	duling	
	cator nber	Indicator	Monitoring Method	Events per Year	Number of Locations	Total Events
on	1	Bacteria	Minimum of 4 (2 dry and 2 wet) E. Coli samples collected annually between 6/1 and 9/15	4	2	40
Recreation	2	Various Indicators	During sampling dates, record water color and the presence of any of the following on the field data sheet: algal bloom, foam, debris, scum, slicks, odors, and surface floating solids	4	2	40
	3	Dissolved Oxygen	Minimum of 4 (2 dry and 2 wet) measurements taken annually from 6/1 to 9/15 between 5:00 am and 8:00 am	4	2	40
a .	4	рН	Taken at the same schedule as DO	4	2	40
Aquatic Life	5	Habitat Assessment	Complete using DES Habitat Assessment Field Data Sheets annually during late fall	1	1	5
Ac	6	Flow	Monitor flow conditions to determine baseflow and stormwater discharge for a range of flows may be done concurrently with sampling events, or as required to obtain enough flows to develop a comprehensive rating curve	4	2	40
	7	Stream Stability	Full site survey of all topographic features performed once as an as built, then again in years 3 and 5	1	1	3
Additional Indicators	8	Planting Success	Visual site assessment for any high- mortality areas, assessment of 4 vegetation plots three times; once after the first full growing season, then every other year (may be done during full survey)	1	4	12
Addit	9	Visual Health Assessment	Pictures taken at set photo points twice per year, during the spring and the fall	2	1	10
	10	Other Indicators (Temperature, Turbidity, Conductivity)	Taken at the same schedule as DO	4	2	40

In addition to the monitoring methods shown, per the request of DES and the local conservation commission, trash shall be removed from the stream and site as part of the scheduled maintenance for the landscaping at the site. If trash is observed during regular maintenance, it shall be removed and disposed of properly.

Monitoring locations for each of the methods listed in Table 7 should be determined either as construction is ongoing, or after completion. A map of suggested monitoring locations may be found on page A14 of the Appendix. Not all locations shown on the map are definite; many will be determined and set in the field, after construction is completed. For example, benchmarks and photo points will need to be located in locations with good viewing angles, and away from trafficked or maintained areas; staff gages (or monitoring probes) should be set in easily accessible locations, but in permanent water; vegetation plots should be set at areas of high interest, or in locations that represent a diverse range of variables (species, zones, sunlight, infrastructure, etc.), among other things. Detailed descriptions of the monitoring methods, recommended locations, and data are as follows:

Sampling

Sampling is recommended at two locations at the parcel: first at the existing junction box, located where the stream first enters the parcel (access may be obtained via the manhole cover and into the large junction box); the second, at the downstream end of the project where the stream empties into a pool which routes the water under Goose Bay Drive. If the first location is considered too dangerous, or no permission is granted to enter the box, sampling may occur at the outlet of the 54" HDPE pipe directing Hodgson Brook into the proposed stream corridor. It is preferred to sample at the junction box, as the water there has not come into contact with any proposed infrastructure (LID stormwater outfalls, stream corridor). This would be very useful to compare the quality of the water before the project and after. Sampling during high flows may easily be performed from outside the junction box, using sampling rods with attached sample containers. On sampling days, samples should first be taken at the downstream location, then upstream to minimize possible sample disturbance contamination.

Performing the sampling should be completed in one day, with as little difference in time and climatic conditions as possible. Concurrent sampling is recommended. All sampling should conform to DES VRAP protocols, unless not available, in which case they should follow any State or EPA guidelines.

Sampling will be performed in two manners, with another set of data being collected observationally. Sampling for bacteria (E. Coli) will be conducted by obtaining samples collected in the field, preserved for transport, and having samples analyzed at a lab, reported in counts per 100 mL. For fresh water, DES has a limit of 126 counts per mL for E. Coli. Sampling for other indicators (Dissolved Oxygen, pH, Temperature, Turbidity, and Conductivity) will be done using probes or meters which can detect each parameter. Kits containing these devices may be available through the DES' VRAP program, and training for using the kit and contents may be available as well. Observational data to be taken at the same time as the samples include the weather, as well as other indicators of stream health: water color, algal bloom, foam, debris, scum, slicks, odors, or surface floating solids. These can be noted and recorded along with all the other indicators – except for bacteria – on the sample Hodgson Brook Field Data

Sheets, seen on pages A12 and A13 in the Appendix. These data sheets were adjusted slightly from the data sheets given as part of the VRAP program.

In the Hodgson Brook WMP document, it is recommended that at least five samples are taken every other year (between 5/24 and 9/15 for E. Coli and 6/1 to 9/30 for all others) at locations defined in the paper. One of the locations is just downstream of the site, on the brook to the east of the intersection of Corporate Drive and Rye Street. This location has quite a bit of environmental monitoring data (EMD) available publicly from the DES' OneStop data server, dating from 2005 to 2016. Sampling for the monitoring of this project is recommended to be performed four times each year – twice during 'dry' weather, and twice during 'wet' weather. Dry weather sampling should occur on a day without precipitation the day of sampling as well as the three full days prior to the sampling date. Wet weather sampling should occur during or immediately after a storm with a precipitation depth of >0.2 inches, when flows are elevated from the baseflow. Sampling during wet and dry weather provides a comparison of the water quality during baseflow and storm events, may help identify sources of contamination, and will show the performance of the site. It is preferable that sampling of all metrics be done at the same time, and to make the timing more easily defined, all sampling should be done between the latest start date and earliest end date defined in the WMP; thus sampling should take place from 6/1 to 9/15 between the hours of 5:00 am and 8:00 am.

Observations and Visual Assessments

Other data that will be taken at the site should assess the stream system health, and should include vegetation plots, photo points, habitat assessments, and flows. Photo points should be set after the construction has been completed, and should be marked at locations that can be repeated in subsequent years by both location and direction, so that pictures may be compared through the years. The photo points should capture the entire site, as well as any notable features, such as the vegetation plots, or any culvert inverts (to show scour, perhaps). Photo points should be taken twice per year, in the spring and fall, and should be included in the annual reports.

The habitat assessments will be performed using the Habitat Assessment Field Data Sheets for Low Gradient Streams. The assessment rates habitat parameters for health on a scale of 0 to 20, using descriptions to guide the assessor as to what to look for. The data should be compiled in the field, using any pictures as evidence and a field book for notes, and should be performed once each year in the fall, during a period of low flow. These sheets were obtained from the DES' VRAP website, and may be found reproduced here in the Appendix, on pages A9-A11.

Vegetation plots should be set after construction and the complete planting and seeding of the site has been completed, and should not be assessed until after one full growing season has passed. It is recommended that four vegetation plots be set, representing a thorough sample of variables; sunlight, planting zones, species density, etc. Two vegetation plots should span the width of the stream corridor, and two should be located in 10'x10' squares on the floodplain. These plots should be assessed for mortality of planted plants, coverage, invasives, and species diversity. In addition to the four plots, a site-wide visual assessment for the mortality of any of the planted plants should be conducted, tallied, and reported. A goal of 75% survival is usually recommended for projects of this type. The reason for the

mortality of any plants should also be recorded to the most accurate extent possible – water content, sunlight, trampling, foraging, animal burrowing, etc.

Finally, flows should be observed, recorded, or downloaded from pressure transducers during each of the sampling events, at a minimum. More data is recommended to help create an accurate rating curve for each location. It is recommended to have two flow locations at the same two sampling locations. To begin, theoretical hydraulic rating curves (water depth versus discharge) for each site should be developed. Over time, and with base flows and storm flows measurements, the curves may be more accurately empirically developed. Flow calibration should be performed at both sites for a range of flows, with a concentration of measurements at the low-flows. Calibration may be performed using a flow meter in the stream, or in a pipe, surveying a pipe and calculating the flow based on the flow depth, or by calibrated weirs or flumes that will give accurate flows, provided the water upstream has filled the reservoir created by the device. For each site, a minimum of 8 calibration flows are recommended for the empirical rating curve, and more points are encouraged. Early and frequent, accurate rating curve calibration will make the collection of this data go much more quickly in subsequent years.

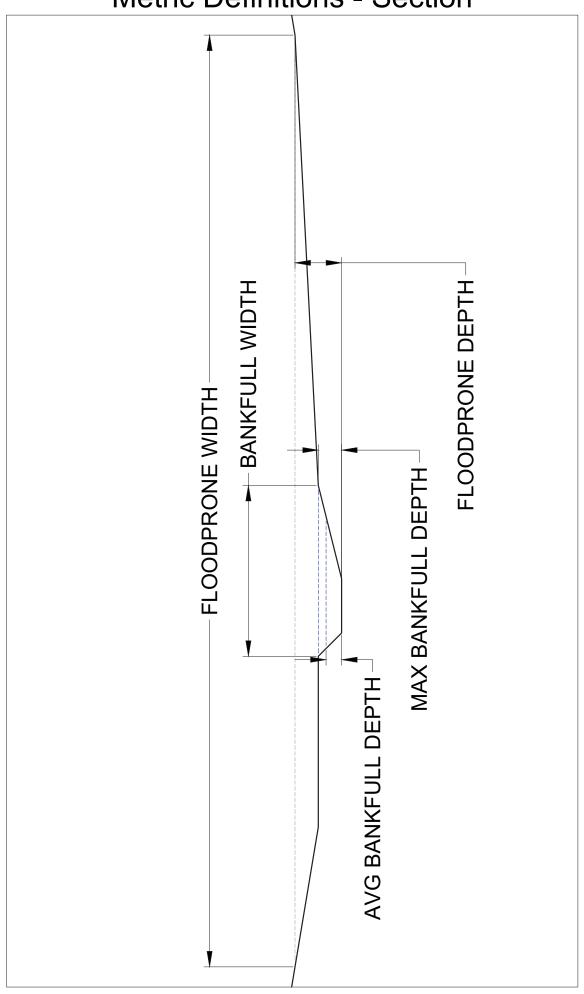
Site Survey

The final monitoring method will be to perform a full site topographic survey, making sure to include all relevant and important features, such as: benchmarks, sampling locations, staff gages, infrastructure, instream structures, stream and corridor features, floodplain features, photo points, and all topographic features. From this survey, maps should be produced that display all monitoring locations, comparisons of the stream features from year-to-year, and any other relevant information. Stream comparisons may include stream profiles, cross sections, as well as any notable failures. A full site survey should be conducted first as an as-built survey of the site, then again in years 3 and 5, following the completion of the project. The products built from the site surveys should be included in the annual reports, during the years they are performed.

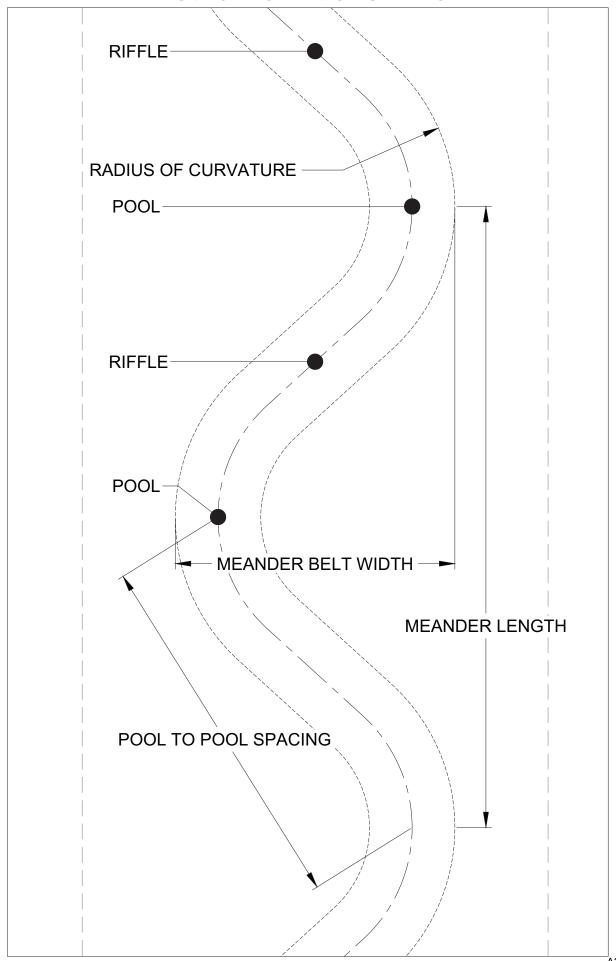
Appendix

- A1. Metric Definitions Section
- A2. Metric Definitions Plan
- A3. Planting Zones
- A4. Proposed Stream Metrics Section and Plan
- A5. Generic Log Cross Vane Detail
- A6. Generic Floodplain Sill Detail
- A7. Table A1 Associated Birds & Mammals, and Food Value of Planting Species
- A8. Table A1 Associated Birds & Mammals, and Food Value of Planting Species (Cont.)
- A9. Habitat Assessment Field Data Sheet Page 1
- A10. Habitat Assessment Field Data Sheet Page 2
- A11. Habitat Assessment Field Data Sheet Page 3
- A12. Field Data Sheet Page 1
- A13. Field Data Sheet Page 2
- A14. Example Monitoring Locations
- A15. Complete Table of Proposed Metrics

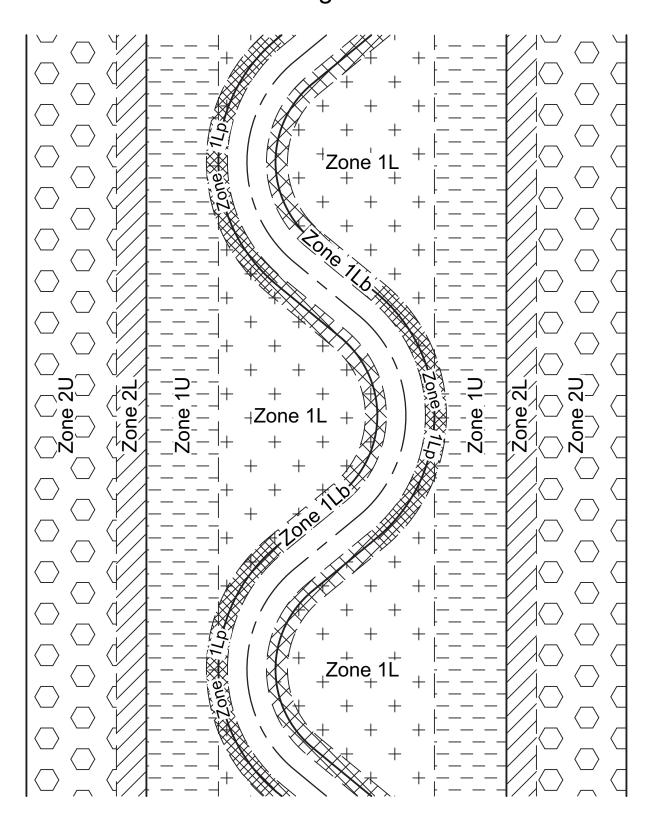
Metric Definitions - Section



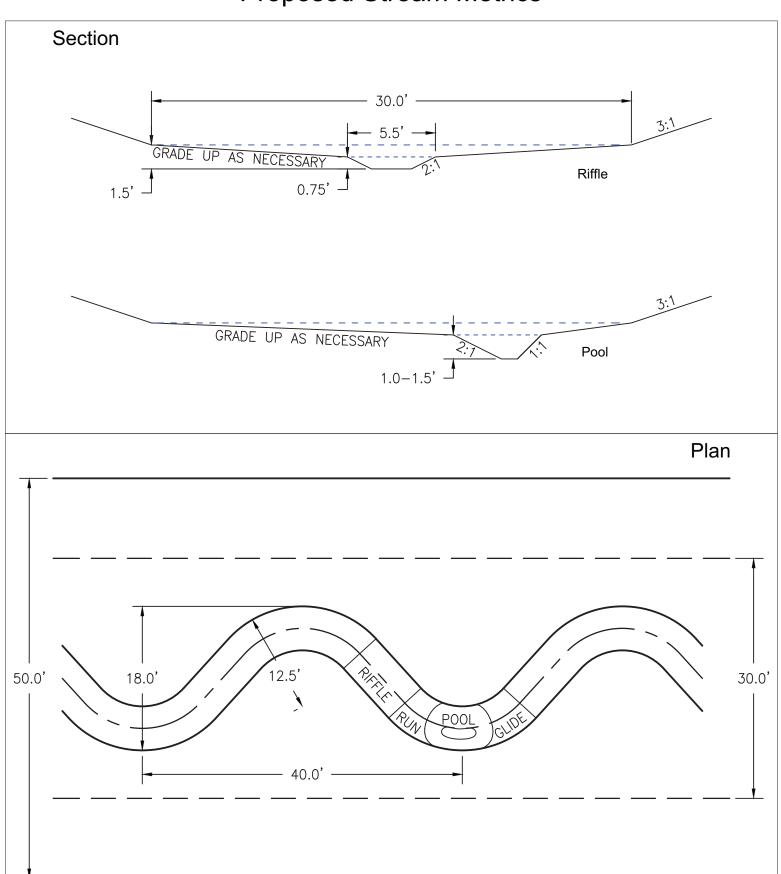
Metric Definitions - Plan



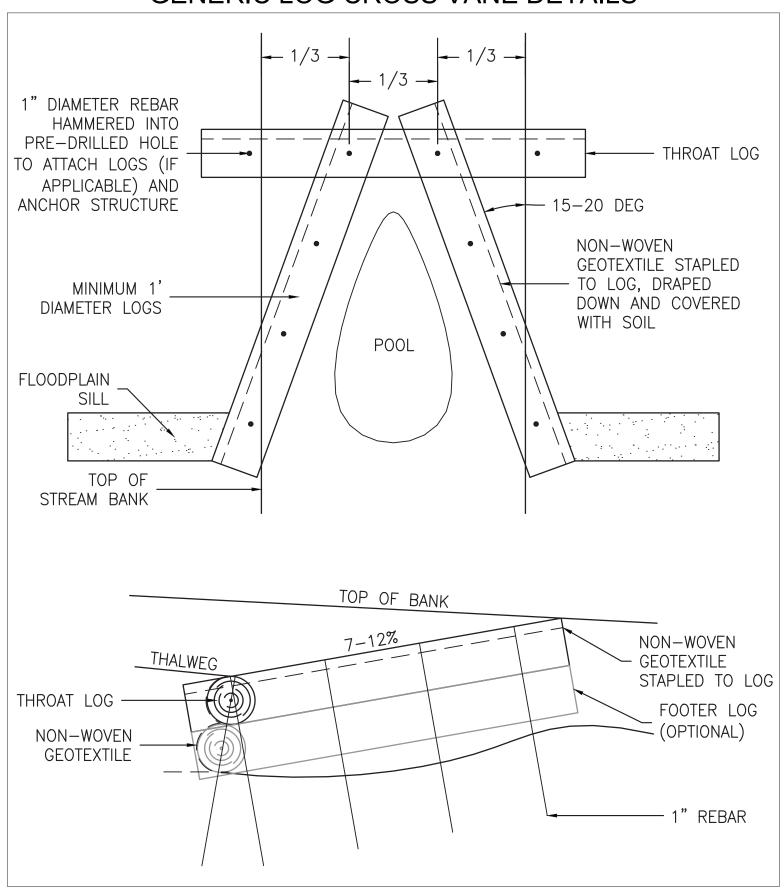
Planting Zones



Proposed Stream Metrics



GENERIC LOG CROSS VANE DETAILS



GENERIC FLOODPLAIN SILL DETAILS

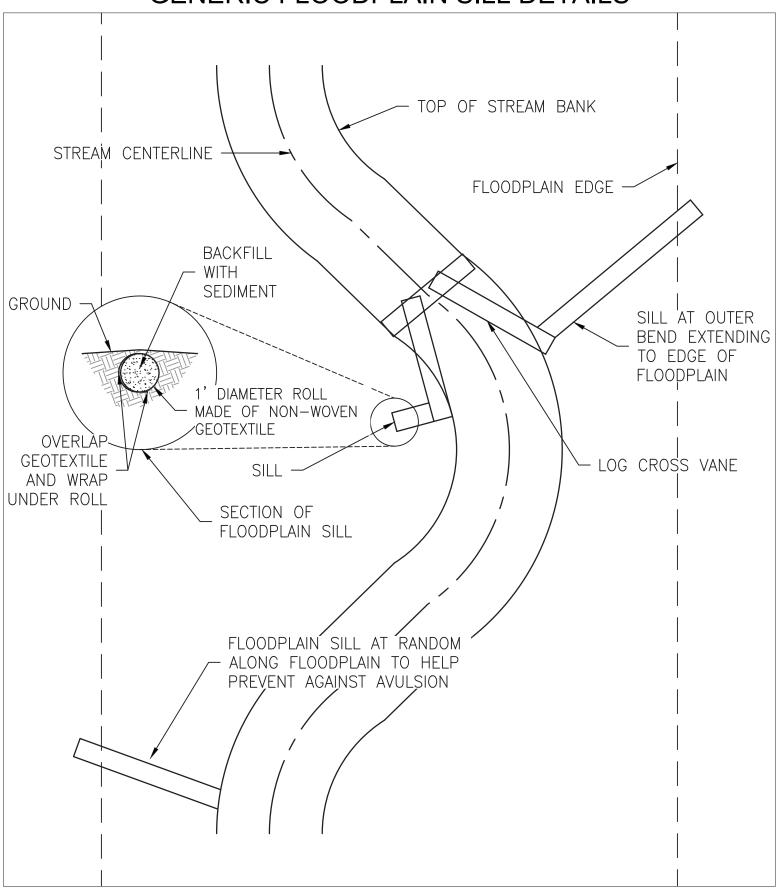


Table A1 -	- Associated Birds & Mammals, and Food Value
Species	Wildlife and Food Value
Ryegrass	Temporary stabilization
Bunchberry	Wildlife: sharp-tailed grouse, spruce-grouse, moose Food: fruit, buds
Goldenrod	<u>Wildlife:</u> goldfinch, junco, ruffed grouse, swamp sparrow, butterflies and other insects, cottontail, meadow mice <u>Food:</u> seeds, nectar
Jewelweed	Wildlife: ring-necked pheasant, stuffed grouse, ruby-throated hummingbird, veery, butterflies and insects, white-footed mouse Food: nectar, seeds
Partridgeberry	Wildlife: grouse, mammals Food: berries
Swamp Milkweed	<u>Wildlife:</u> black duck, mallards, red-winged blackbird, ruby-throated hummingbird, monarch butterfly, other butterflies and insects, muskrat <u>Food:</u> nectar, seeds
Tall Meadow Rue	Wildlife: bees, butterflies Food: nectar
Chokecherry	Wildlife: bluebird, brown thrasher, catbird, crow, eastern kingbird, evening grosbeak, orioles, pileated woodpecker, ring-necked pheasant, robin, rose grosbeak, ruffed grouse, thrushes, yellow-bellied sapsucker, rabbit, squirrel Food: berries, buds, foliage
Gray Dogwood	Wildlife: blue jay, cardinal, catbird, cedar warwing, eastern kingbird, finch, flycatcher, grosbeak, hairy woodpecker, northern flicker, phoebe, pileated woodpecker, pine grosbeak, pine warbler, red-bellied woodpecker, ring-necked pheasant, robin, ruffed grouse, starling, swamp sparrow, tufted titmouse, veery, vireo, wild turkey, wood duck, wood thrush, woodcock, yellowbellied sapsucker, chipmunk, deer, red fox, rabbit, squirrel Food: berries, twigs
Hobblebush	<u>Wildlife:</u> brown thrasher, cardinal, cedar warwing, evening grosbeak, robin <u>Food:</u> fruit
Lowbush Blueberry	Wildlife: blue jay, grouse, kingbird, oriole, robin, tangers, woodpeckers, squirrel Food: berries, foliage, twigs
Pussy Willow	<u>Wildlife:</u> American goldfinch, ruffed grouse, beaver, hare, rabbits, squirrel <u>Food:</u> buds, catkins, twigs, bark

Table A1 – As	sociated Birds & Mammals, and Food Value (cont.)
Raspberry	<u>Wildlife:</u> songbirds and mammals Food: fruits
Red Osier Dogwood	Wildlife: bluebird, brown thrasher, cardinal, catbird, cedar waxwing, downy woodpecker, eastern kingbird, finches, northern flicker, pine warbler, purple finch, ringed-neck pheasant, ruffed grouse, vireo, wild turkey, woodpeckers, wood duck, chipmunk, deer, rabbit, squirrel Food: berries, twigs
Silky Dogwood	Wildlife: baltimore oriole, black-capped chickadee, blue jay, brown thrasher, cardinal, catbird, cedar waxwing, downy woodpecker, eastern kingbird, flycatcher, mockingbird, northern flicker, pine warbler, purple finch, red-bellied woodpecker, ringed-neck pheasant, robin, rose-breasted grosbeak, ruffed grouse, song sparrow, starlings, tufted-titmouse, wild turkey, wood duck, wood thrush, veery, chipmunk, deer, rabbit, raccoon, skunk, squirrel, white-footed mouse Food: buds, twigs, bark, leaves
Speckled Alder	Wildlife: alder flycatcher, catbird, goldfinch, mallards, pheasant, pine siskin, red-winged blackbird, ruffed grouse, swamp sparrow, yellow-bellied flycatcher, woodcock, bear, beaver, deer, cottontail, moose, muskrat, snowshoe hare Food: buds, twigs, bark, leaves
Witch Hazel	Wildlife: cardinal, ring-necked pheasant, ruffed grouse, wild turkey, deer, squirrels Food: seeds, buds, twigs, bark
Black Willow	Wildlife: songbirds and mammals Food: buds, catkins
Black Cherry	Wildlife: bluebird, blue jay, brown thrasher, cardinal, catbird, cedar waxwing, common crow, eastern kingbird, evening grosbeak, mockingbird, northern flicker, northern oriole, robin, ruffed grouse, sparrows, thrushes, veery, vireo, yellow-bellied sapsucker, bear, chipmunk, deer, fox, raccoon, squirrel Food: berries, buds, sap
Red Maple	Wildlife: cardinal, chickadee, evening and pine grosbeaks, finches, robin, yellow-bellied sapsucker, beaver, chipmunk, deer, opossum, squirrel, snowshoe hare Food: seeds, buds, bark, twigs, sap
White Oak	Wildlife: blue jay, brown thrasher, nuthatch, quail, ruffed grouse, towhee, wild turkey, wood duck, woodpecker, chipmunk, bear, deer, gopher, opossum, raccoon, squirrel Food: acorns
White Ash	Wildlife: finches, grosbeaks, red-winged blackbird, wood duck, deer, squirrel Food: seeds, foliage

Habitat Assessment Field Data Sheet Low Gradient Streams

Stream Name				
Station #	Rivermile	_		
Lat	Long	_		
Storet #				
Form Completed B	Зу	Date AM F	PM	
Habit Parameter				
1. Epifaunal Substrate/ Available Cover	Greater than 50% of substrate favorable for epifaunal colonization and fish cover, mix of snags, submerged logs, undercut banks, cobble or other stable habitat and at stage to allow full colonization potential (i.e., logs/snags that are not new fall and not transient).	30 - 50% mix of stable habitat; well-suited for full colonization potential; adequate habitat for maintenance of populations; presence of additional substrate in the form of newfall, but not yet prepared for colonization (may rate at high end of scale).	10 - 30% mix of stable habitat; habitat availability less than desirable; substrate frequently disturbed or removed.	Less than 10% stable habitat; lack of habitat is obvious; substrate unstable or lacking.
SCORE	20 19 18 17 16	15 14 13 12 11	10 9 8 7 6	
2. Pool Substrate Characterization	Mixture of substrate materials, with gravel and firm sand prevalent; root mats and submerged vegetation common.	Mixture of soft sand, mud, or clay; mud may be dominant; some root mats and submerged vegetation present.	All mud or clay or sand bottom; little or no root mat; no submerged vegetation.	Hard-pan clay or bedrock; no root mat or vegetation.
SCORE	20 19 18 17 16	15 14 13 12 11	10 9 8 7 6	
3. Pool Variability	Even mix of large- shallow, large-deep, small-shallow, small- deep pools present.	Majority of pools large-deep; very few shallow.	Shallow pools much more prevalent than deep pools.	Majority of pools small-shallow or pools absent.
SCORE	20 19 18 17 16	15 14 13 12 11	10 9 8 7 6	

4. Sediment Deposition	Little or no enlargement of islands or point bars and less than 5% (<20% for low-gradient streams) of the bottom affected by sediment deposition.	Some new increase in bar formation, mostly from gravel, sand or fine sediment; 5-30% (20-50% for low-gradient) of the bottom affected; slight deposition in pools.	Moderate deposition of new gravel, sand or fine sediment on old and new bars; 30-50% (50%-80% for low-gradient) of the bottom affected; sediment deposits at obstructions, constrictions, and bends; moderate deposition of pools prevalent.	Heavy deposits of fine material, increased bar development; more than 50% (80% for low-gradient) of the bottom changing frequently; pools almost absent due to substantial sediment deposition.
SCORE	20 19 18 17 16	15 14 13 12 11	10 9 8 7 6	5 4 3 2 1 0
5. Channel Flow Status	Water reaches base of both lower banks, and minimal amount of channel substrate is exposed.	Water fills >75% of the available channel; or <25% of channel substrate is exposed.	Water fills 25-75% of the available channel, and/or riffle substrates are mostly exposed.	Very little water in channel and mostly present as standing pools.
SCORE	20 19 18 17 16	15 14 13 12 11	10 9 8 7 6	5 4 3 2 1 0
6. Channel Alteration	Channelization or dredging absent or minimal; stream with normal pattern.	Some channelization present, usually in areas of bridge abutments; evidence of past channelization, i.e., dredging, (greater than past 20 yr) may be present, but recent channelization is not present.	Channelization may be extensive; embankments or shoring structures present on both banks; and 40 to 80% of stream reach channelized and disrupted.	Banks shored with gabion or cement; over 80% of the stream reach channelized and disrupted. Instream habitat greatly altered or removed entirely.
SCORE	20 19 18 17 16	15 14 13 12 11	10 9 8 7 6	5 4 3 2 1 0
7.Channel Sinuosity	The bends in the stream increase the stream length 3 to 4 times longer than if it was in a straight line. (Note-channel braiding is considered normal in coastal plains and other lowlying areas. This parameter is not easily rated in these areas.	The bends in the stream length 2 to 3 times longer than if it was in a straight line.	The bends in the stream increase the stream length 2 to 1 times longer than if it was in a straight line.	Channel straight; waterway has been channelized for a long distance.
SCORE	20 19 18 17 16	15 14 13 12 11	10 9 8 7 6	5 4 3 2 1 0
8. Bank Stability (score each bank)	Banks stable: evidence of erosion or bank failure absent or minimal; little potential for future problems. <5% of bank affected.	Moderately stable; infrequent, small areas of erosion mostly healed over. 5-30% of bank in reach has areas of erosion.	Moderately unstable; 30-60% of bank in reach has areas of erosion; high erosion potential during floods.	Unstable; many eroded areas; "raw" areas frequent along straight sections and bends; obvious bank sloughing; 60-100% of bank has erosional scars.
SCORE (LB)	Left Bank 10 9	8 7 6	5 4 3	2 1 0
SCORE (RB)	Right Bank 10 9	8 7 6	5 4 3	2 1 0

9. Vegetative Protection (score each bank) Note: determine left or right side by facing downstream.	More than 90% of the streambank surfaces and immediate riparian zone covered by native vegetation, including trees, understory shrubs, or nonwoody macrophytes; vegetative disruption through grazing or mowing minimal or not evident; almost all plants allowed to grow naturally	70-90% of the streambank surfaces covered by native vegetation, but one class of plants is not well represented; disruption evident but not affecting full plant growth potential to any great extent; more than one-half of the potential plant stubble height remaining	50-70% of the streambank surfaces covered by vegetation; disruption obvious; patches of bare soil or closely cropped vegetation common; less than one-half of the potential plant stubble height remaining.	Less than 50% of the streambank surfaces covered by vegetation; disruption of streambank vegetation is very high; vegetation has been removed to 5 centimeters or less in average stubble height.
SCORE (LB)	Left Bank 10 9	8 7 6	5 4 3	2 1 0
SCORE (RB)	Right Bank 10 9	8 7 6	5 4 3	2 1 0
10. Riparian Vegetative Zone Width (score each bank riparian zone)	Width of riparian zone >18 meters; human activities (i.e., parking lots, roadbeds, clearcuts, lawns, or crops) have not impacted zone.	Width of riparian zone 12-18 meters; human activities have impacted zone only minimally.	Width of riparian zone 6-12 meters; human activities have impacted zone a great deal.	Width of riparian zone <6 meters; little or no riparian vegetation due to human activities.
SCORE(LB)	Left Bank 10 9	8 7 6	5 4 3	2 1 0
SCORE (RB)	Right Bank 10 9	8 7 6	5 4 3	2 1 0

Page 1

Hodgson Brook Field Data Sheet

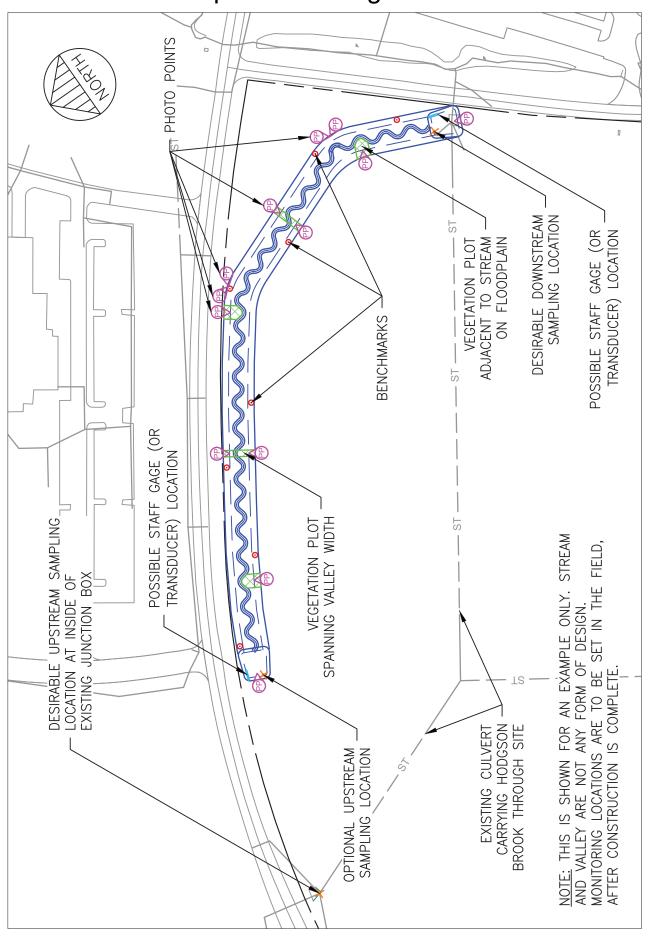
Customized from the Volunteer River Assessment Program - Hodgson Brook Field Data Sheet, published by NH DES

Date:			Start	Time:			End Time:	ime:				
Kit #:			Data	Data Collected By:	;							
Initial Turb	Initial Turbidity Calibration Value:	/alue:					Time Dissol	Time Dissolved Oxygen Meter Turned On:	Meter Turn	ed On:		
Initial Conc	Initial Conductivity Calibration Value (175-225 μS):	on Value (17	.5-225 µS):				Time of Firs	Time of First Dissolved Oxygen Calibration:	Oxygen Cali	bration:		
Loca-tion Code	Location Name	Time Sampled (HH:MM)	Turbidity (NTU)	pH Cal. Slope ("SLP" = 92-102%)	рН (std. units)	Water Temp (°C)	Dissolved Oxygen Cal. (96-100%)	Dissolved Oxygen (mg/L)	Dissolved Oxygen (% sat.)	Dissolved Oxygen (% sat. in chamber)	Air Temp (°C)	Specific Conductance (µS)
Zero Oxyge	Zero Oxygen Reading (mg/L):	<u></u>		(% sat.):	t.):			Station:			Time:	
6.0 pH Buf	6.0 pH Buffer Reading (5.8-6.3):	.3):					Station:			Time:		
DI Blank Tu	DI Blank Turbidity Reading:						Station:			Time:		

Hodgson Brook Field Data Sheet

Weather Condition: Current Weather (circle one)	Clear	Partly Cloudy	Overcast	Foggy	Нагу	Showers	Downpour	Snow	Other:
Decrible the nast three days' local weather (days prior):	al weather	(dave prior).	.			,		'n	
وعدانات والمعاد الناجة طعرع الادم	א מפרוני	(days prior).	i					ا ا	
Sampling Preparation Checklist (check if complete):	neck if con	nplete):		1					
Scribe:					Indicat	e Presence o	f Visual Indicato	ors for Each S	Indicate Presence of Visual Indicators for Each Sampling Station
				<u> </u>				Site	
Check Maintenance Log Fresh Solutions				ū	Indicator				
Batteries					Color				
Post Calibrations: pH Cal. Slope:		Ī			Algal Bloom				
DO Cal. Turbidity (1.0 std.)		1 1		_	Foam				
Conductivity (200 µS std.)		l			Debris				
End of the Day (check if completed): All meters dry and off:	; ;				Scum				
DO probe in chamber with wet sponge: pH probe upright in storage solution	onge: on			•	Slicks				
Turbidity sample vial rinsed and filled with DI water Conductivity probe cleaned and in chamber	led with DI chamber	water		Ü	Odors				
Kit clean of kimwipes, dirt, moisture NOTES:	ē			<u> </u>	Surface Floating Solids				
				B	Benthic Deposits				

Example Monitoring Locations



	Property	Units	Symbol/Equation	Proposed Design
	Maximum Bankfull Depth	ft	Dmax	0.75
	Average Bankfull Depth	ft	Davg	0.50
	Floodprone Depth	ft	Dfp	1.5
	Bankfull Width	ft	Wbkf	5.5
	Floodprone Width	ft	Wfp	30.0
	Width/Depth Ratio	-	W/D	11.00
	Entrenchment Ratio	-	ER	5.45
rics	Bankfull Area	sqft	Abkf	2.75
Proposed Metrics	Sinuosity	-	k	1.226
20	Meander Belt Width	ft	MBW	18.0
ose	Belt Width Ratio	-	MBW/Wbkf	3.27
rop	Meander Length	ft	ML	40.0
_	Meander Length Ratio	_	ML/Wbkf	7.27
	Radius of Curvature	ft	Rc	12.5
	Radius of Curvature Ratio	_	Rc/Wbkf	2.27
	Pool Length	ft	Lp	16.22
	Pool Length Ratio	-	Lp/Wbkf	2.95
	Pool to Pool Spacing	ft	P2P	24.52
	Pool Spacing Ratio	_	P2P/Wbkf	4.46
	Stream Length	ft	SL	1204
	Stream Slope	ft/ft	Slope	0.00946
	Valley Slope	ft/ft	VS	0.01160
	Valley Length	ft	VL	982.5
	Invert In	ft	INVin	47.70
	Invert Out	ft	INVout	36.31
	Bankfull Wetted Perimeter	ft	Р	5.85
	Bankfull Hydraulic Radius	ft	Rh	0.47
	Bankfull Manning's n	-	n	0.035
lue	Bankfull Velocity	fps	V	2.50
ted Values	Bankfull Flow	cfs	Q	6.87
ted	Floodprone Wetted Perimeter	ft	Pfp	30.4
Calcula	Floodprone Area	sqft	Afp	18.4
Salc	Floodprone Hydraulic Radius	ft	RHfp	0.60
	Floodprone Velocity	fps	Vfp	1.72
	Floodprone Manning's n	-	nfp	0.06
	Floodprone Flow	cfs	Qfp	31.6
	High Flow Wetted Perimeter	ft	P50	39.6
	High Flow Area	sqft	A50	44.3
	High Flow Hydraulic Radius	ft	RH50	1.12
	High Flow Manning's n	- £	n50	0.08
	High Flow Velocity	fps	V50	2.16
	High Flow	cfs	Q50	95.4

Full Flow Wetted Perimeter	ft	P100	48.7
Full Flow Area	sqft	A100	76.9
Full Flow Hydraulic Radius	ft	RH100	1.58
Full Flow Manning's n	-	n100	0.09
Full Flow Velocity	fps	V100	2.41
Full Flow	cfs	Q100	185.4
Low Flow Wetted Perimeter	ft	Plf	2.95
Low Flow Area	sqft	Alf	0.27
Low Flow Hydraulic Radius	ft	RHIf	0.09
Low Flow Manning's n	-	nlf	0.035
Low Flow Velocity	fps	VIf	0.84
Low Flow	cfs	Qlf	0.23
Bankfull Stable Particle - Rosgen	in	RDbkf	2.49
Low Flow Stable Particle - Rosgen	in	RDIf	0.70
Floodprone Stable Particle - Rosgen	in	RDfp	2.80
Full Flow Stable Particle - Rosgen	in	RD100	5.68
Bankfull Stable Particle - LWM	in	LDbkf	0.88
Low Flow Stable Particle - LWM	in	LDIf	0.15
Floodprone Stable Particle - LWM	in	LDfp	1.05
Full Flow Stable Particle - LWM	in	LD100	2.85

Lonza Biologics - Drainage Analysis

To: City of Portsmouth Technical Advisory Committee (TAC)

FROM: Patrick M. Crimmins, P.E.

COPY: Lonza Biologics

DATE: May 21, 2018

1.0 Project Description

The proposed project is located on a vacant 24-acre parcel, refered to as the Iron Parcel, that once consisted of row housing and streets for Pease Air Force Base. The houses and roads were removed in the mid to late 1990's as part of the Civil Redevelopment Plan for Pease after the closure of the Air Force Base.

Lonza's existing facilities are located at 101 International Drive which is across Goose Bay Drive from the proposed project site. The project will merge 101 International Drive with 70 and 80 Corporate Drive to create a 43-acre parcel for Lonza's campus. This will require that 1,700LF of Goose Bay Drive be abondoned as a public right-of-way and merged with these parcels. The total master plan build-out of the proposed industrial development will include three (3) new buildings totaling approximately 1 million square feet of gross floor area and two (2) new parking garages.

The project will also consist of site improvements that include drive aisles, sidewalks utilities, lighting, landscaping and a stormwater management system with three (3) gravel wetlands and one (1) rain garden. In addition, the project will include a stream restoration project for Hodgson Brook. There is an existing 50-Inch culvert that bisects the parcel which is a buried portion of Hodgson Brook. The project will remove this culvert and daylight the flow through a new 1,000 LF stream channel. The project will result in 55,555 SF of wetland impact.

The proposed project will require a New Hampshire Department of Environmental Services (NHDES) Alteration of Terrain (AoT) Permit.

2.0 Drainage Analysis

2.1 Calculation Methods

The parcel's on-site watersheds were analyzed under this section. The design storms analyzed in this study are the 2-year, 10-year and 50-year 24-hour duration storm as per NHDES AoT Regulations (Env-Wq 1500.) The stormwater modeling system, HydroCAD 10.0 was utilized to predict the peak runoff rates from these storm events. A Type III storm pattern was used in the model.

The time of concentration was computed using the TR-55 Method, which provides a means of determining the time for an entire watershed to contribute runoff to a specific location via sheet flows, shallow concentrated flow and channel flow. Runoff curve numbers were calculated by estimating the coverage areas and then summing the curve number for the coverage area as a percent of the entire watershed.

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References

1. HydroCAD Stormwater Modeling System, by HydroCAD Software Solutions LLC, Chocorua, New Hampshire.

2. New Hampshire Stormwater Management Manual, Volume 2, Post-Construction Best Management Practices Selection and Design, December 2008.

2.2 Pre-Development Calculations

In order to analyze the pre-development condition, the site has been divided into two watershed areas modeled at two points of analysis. Enclosed with this memorandum are the Pre-Development Watershed Plan, HydroCAD model and Soil Plan for these two (2) points of analysis.

Each of the points of analysis and their contributing watershed areas are described below:

Point of Analysis (PA1)

PRE 1.0 makes up almost the entire area to be developed. This area consists of the entire undeveloped parcel, as well as, a portion of Corporate Drive that drains onto the parcel via a closed drainage system. Currently the watershed is an undeveloped field area that with a portion of the site being used as a temporary construction parking area with associated stormwater management controls near the center of the parcel. This parcel was previously developed as military housing that was demolished in the mid to late 1990's. Runoff from this area travels southeast via overland flow to Point of Analysis 1 located at the existing Hodgson Brook outlet headwall.

Point of Analysis (PA2)

PRE 2.0 is comprised mostly of runoff from Goose Bay Drive that is located between the undeveloped parcel and the existing Lonza facility. Runoff from this area travels via overland flow to the existing stormwater basin located at the existing Lonza facility. Point of Analysis 2 (PA2) is located at the existing basin.

2.3 Post-Development Calculations

The post-development condition was analyzed by dividing the watersheds into seven sub-catchment areas. Stormwater runoff from these sub-catchment areas flow to three gravel wetlands and one rain garden for treatment prior to infiltration or discharging to the existing Hodgson Brook outlet. Flows from these sub-catchment areas are modeled at the same two points of analysis that were modeled in the pre-development analysis, PA1 and PA2. Enclosed with this memorandum are the Pre-Development Watershed Plan, HydroCAD model and Soil Plan for these two (2) points of analysis.

Each of the points of analysis and their contributing watershed areas are described below:

Point of Analysis (PA1)

Point of Analysis 1 (PA1) is located at the existing Hodgson Brook outlet headwall. For the purposes of this analysis, the area contributing to Point of Analysis 1 (PA1) has been divided into six sub-catchment areas (see plan C-802). Sub-catchments POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4 and POST 1.5 contribute to this point of analysis and consist of grass, paved parking lots, concrete sidewalks, and roof areas. Runoff generated in these sub-catchment areas is collected via one rain garden and three gravel wetlands which treat and discharge stormwater runoff either to infiltration or to PA1. Runoff from sub-catchments POST

TECHNICAL MEMORANDUM Tighe&Bond

1.0, 1.1, 1.2 and 1.5 flow via overland flow to the closed drainage then flows via underground piping to one of the gravel wetlands or rain garden. Flows from sub-catchment POST 1.3 flows via overland flow to the Hodgson Brook restoration area (REACH 1.3) then flows via the brook until reach PA1. Runoff from POND 1.1 and POND 1.2 also flows via REACH 1.3 to PA1. Runoff from sub-catchment area POST 1.4 flows via overland flow to PA1. PA1 is shown on the Post-Development Watershed Plan (C-802).

Point of Analysis (PA2)

POST 2.1 is comprised mostly of runoff from Goose Bay Drive that is located between the undeveloped parcel and the existing Lonza facility. Runoff from this area travels via overland flow to the existing stormwater basin located at the existing Lonza facility. Point of Analysis 2 (PA2) is located at the existing basin.

2.4 Peak Rate Comparisons

The following table summarizes and compares the pre- and post-development peak runoff rates for the 2-year, 10-year, 25-year and 50-year storm events at each point of analysis. The pre-development 1-year storm event is also included for channel protection requirements.

Point of Analysis	Pre 1-Year Storm (cfs)	Pre/ Post 2-Year Storm (cfs)	Pre/ Post 10-Year Storm (cfs)	Pre/ Post 25-Year Storm (cfs)	Pre/ Post 50-Year Storm (cfs)
PA1	16.94	25.44/ 13.07	54.47/ 41.55	79.11/ 64.50	102.71/ 92.68
PA2	1.59	1.99/ 0.22	3.18/ 0.33	4.09/ 0.42	4.94/ .051

As depicted in Table 2.4.1, post-development peak runoff rates are less than the predevelopment condition for PA1 and PA2.

2.5 Stormwater Treatment

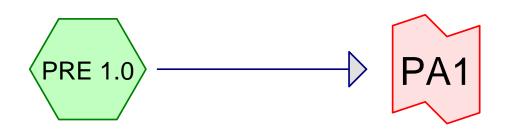
The stormwater management system has been designed to provide stormwater treatment as required by the City of Portsmouth Site Review Regulations and NHDES AoT Regulations (Env-Wq 1500).

Runoff generated from impervious area will be treated three (3) gravel wetlands and one (1) rain garden. The proposed gravel wetlands and rain garden have been designed in accordance with the New Hampshire Stormwater Manual and meet NHDES AoT requirements (Env-Wq 1500) for required water quality volume (WQV) and groundwater recharge volume (GRV)

Enclosed with this memorandum are copies of BMP and GRV worksheets.

4.0 Conclusion

The proposed project will result in a reduction in post-development peak runoff rates from the pre-development condition. The impervious area resulting from the proposed project will be treated by the three (3) gravel wetlands and one (1) rain garden. The project will require an NHDES AoT Permit. A complete copy of the AoT Permit Application will be provided to the City of Portsmouth when it is submitted to NHDES.



WATERSHED 1.0

POINT OF ANALYSIS



WATERSHED 2.0

POINT OF ANALYSIS









Printed 2/9/2018 Page 2

Area Listing (selected nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.122	74	>75% Grass cover, Good, HSG C (PRE 2.0)
0.835	89	Gravel roads, HSG C (PRE 1.0)
0.103	58	Meadow, non-grazed, HSG B (PRE 1.0)
22.611	71	Meadow, non-grazed, HSG C (PRE 1.0)
1.605	78	Meadow, non-grazed, HSG D (PRE 1.0)
3.322	98	Paved parking, HSG C (PRE 1.0, PRE 2.0)
0.101	55	Woods, Good, HSG B (PRE 1.0)
1.067	70	Woods, Good, HSG C (PRE 1.0)
0.126	77	Woods, Good, HSG D (PRE 1.0)
29.892	75	TOTAL AREA

Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.204	HSG B	PRE 1.0
27.957	HSG C	PRE 1.0, PRE 2.0
1.732	HSG D	PRE 1.0
0.000	Other	
29.892		TOTAL AREA

Prepared by Tighe & Bond

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment PRE 1.0: WATERSHED 1.0 Runoff Area=1,275,757 sf 9.69% Impervious Runoff Depth>0.93" Flow Length=1,634' Tc=30.4 min CN=74 Runoff=16.94 cfs 2.276 af

Subcatchment PRE 2.0: WATERSHED 2.0 Runoff Area=26,354 sf 79.76% Impervious Runoff Depth>2.30" Flow Length=650' Slope=0.0250 '/' Tc=5.0 min CN=93 Runoff=1.59 cfs 0.116 af

Link PA1: POINT OF ANALYSIS Inflow=16.94 cfs 2.276 af Primary=16.94 cfs 2.276 af

Link PA2: POINT OF ANALYSIS

Inflow=1.59 cfs 0.116 af
Primary=1.59 cfs 0.116 af

Total Runoff Area = 29.892 ac Runoff Volume = 2.392 af Average Runoff Depth = 0.96" 88.89% Pervious = 26.571 ac 11.11% Impervious = 3.322 ac Prepared by Tighe & Bond

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment PRE 1.0: WATERSHED 1.0 Runoff Area=1,275,757 sf 9.69% Impervious Runoff Depth>1.36" Flow Length=1,634' Tc=30.4 min CN=74 Runoff=25.44 cfs 3.308 af

Subcatchment PRE 2.0: WATERSHED 2.0 Runoff Area=26,354 sf 79.76% Impervious Runoff Depth>2.91" Flow Length=650' Slope=0.0250 '/' Tc=5.0 min CN=93 Runoff=1.99 cfs 0.147 af

Link PA1: POINT OF ANALYSIS Inflow=25.44 cfs 3.308 af Primary=25.44 cfs 3.308 af

Link PA2: POINT OF ANALYSIS

Inflow=1.99 cfs 0.147 af
Primary=1.99 cfs 0.147 af

Total Runoff Area = 29.892 ac Runoff Volume = 3.455 af Average Runoff Depth = 1.39" 88.89% Pervious = 26.571 ac 11.11% Impervious = 3.322 ac Prepared by Tighe & Bond

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Page 6

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment PRE 1.0: WATERSHED 1.0 Runoff Area=1,275,757 sf 9.69% Impervious Runoff Depth>2.82" Flow Length=1,634' Tc=30.4 min CN=74 Runoff=54.47 cfs 6.875 af

Subcatchment PRE 2.0: WATERSHED 2.0 Runoff Area=26,354 sf 79.76% Impervious Runoff Depth>4.77" Flow Length=650' Slope=0.0250 '/' Tc=5.0 min CN=93 Runoff=3.18 cfs 0.240 af

Link PA1: POINT OF ANALYSISInflow=54.47 cfs 6.875 af
Primary=54.47 cfs 6.875 af

Link PA2: POINT OF ANALYSIS

Inflow=3.18 cfs 0.240 af
Primary=3.18 cfs 0.240 af

Total Runoff Area = 29.892 ac Runoff Volume = 7.115 af Average Runoff Depth = 2.86" 88.89% Pervious = 26.571 ac 11.11% Impervious = 3.322 ac

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Page 7

Summary for Subcatchment PRE 1.0: WATERSHED 1.0

Runoff = 54.47 cfs @ 12.43 hrs, Volume= 6.875 af, Depth> 2.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

	Α	rea (sf)	CN D	escription			
_	4,505 58			leadow, no	on-grazed,	HSG B	
	4,387 55			Woods, Good, HSG B			
	9	84,919			on-grazed,	HSG C	
	1	23,673			ing, HSG C		
		36,380		ravel road			
		46,463		Woods, Good, HSG C			
		69,928			on-grazed,		
		5,502			od, HSG D		
	1.2	75,757	74 V	Veighted A	verage		
		52,084			vious Area		
		23,673	9	.69% Impe	ervious Area	a	
		•		•			
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	4.4	50	0.0400	0.19		Sheet Flow,	
						Grass: Short n= 0.150 P2= 3.06"	
	1.2	80	0.0250	1.11		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
	21.4	1,089	0.0147	0.85		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
	3.2	368	0.0160	1.90		Shallow Concentrated Flow,	
						Grassed Waterway Kv= 15.0 fps	
	0.2	47	0.0050	4.03	4.95	Pipe Channel,	
						15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'	
_						n= 0.012 Concrete pipe, finished	
	20.4	1 62 /	Total				

30.4 1,634 Total

Summary for Subcatchment PRE 2.0: WATERSHED 2.0

Runoff = 3.18 cfs @ 12.07 hrs, Volume= 0.240 af, Depth> 4.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf) CN	Description	
21,02	1 98	B Paved parking, HSG C	
5,333	3 74	>75% Grass cover, Good, HSG C	
26,354	4 93	Weighted Average	
5,333	3	20.24% Pervious Area	
21,02	1	79.76% Impervious Area	

Type III 24-hr 10 Year Rainfall=5.58"

L-0700-10 PRE

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Page 8

Tc	Length	Slope	Velocity	Capacity	Description
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
1.1	100	0.0250	1.47		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.06"
2.9	550	0.0250	3.21		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
4.0	650	Total, li	ncreased t	o minimum	Tc = 5.0 min

Summary for Link PA1: POINT OF ANALYSIS

Inflow Area = 29.287 ac, 9.69% Impervious, Inflow Depth > 2.82" for 10 Year event

Inflow = 54.47 cfs @ 12.43 hrs, Volume= 6.875 af

Primary = 54.47 cfs @ 12.43 hrs, Volume= 6.875 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Link PA2: POINT OF ANALYSIS

Inflow Area = 0.605 ac, 79.76% Impervious, Inflow Depth > 4.77" for 10 Year event

Inflow = 3.18 cfs @ 12.07 hrs, Volume= 0.240 af

Primary = 3.18 cfs @ 12.07 hrs, Volume= 0.240 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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Page 9

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment PRE 1.0: WATERSHED 1.0 Runoff Area=1,275,757 sf 9.69% Impervious Runoff Depth>5.31" Flow Length=1,634' Tc=30.4 min CN=74 Runoff=102.71 cfs 12.958 af

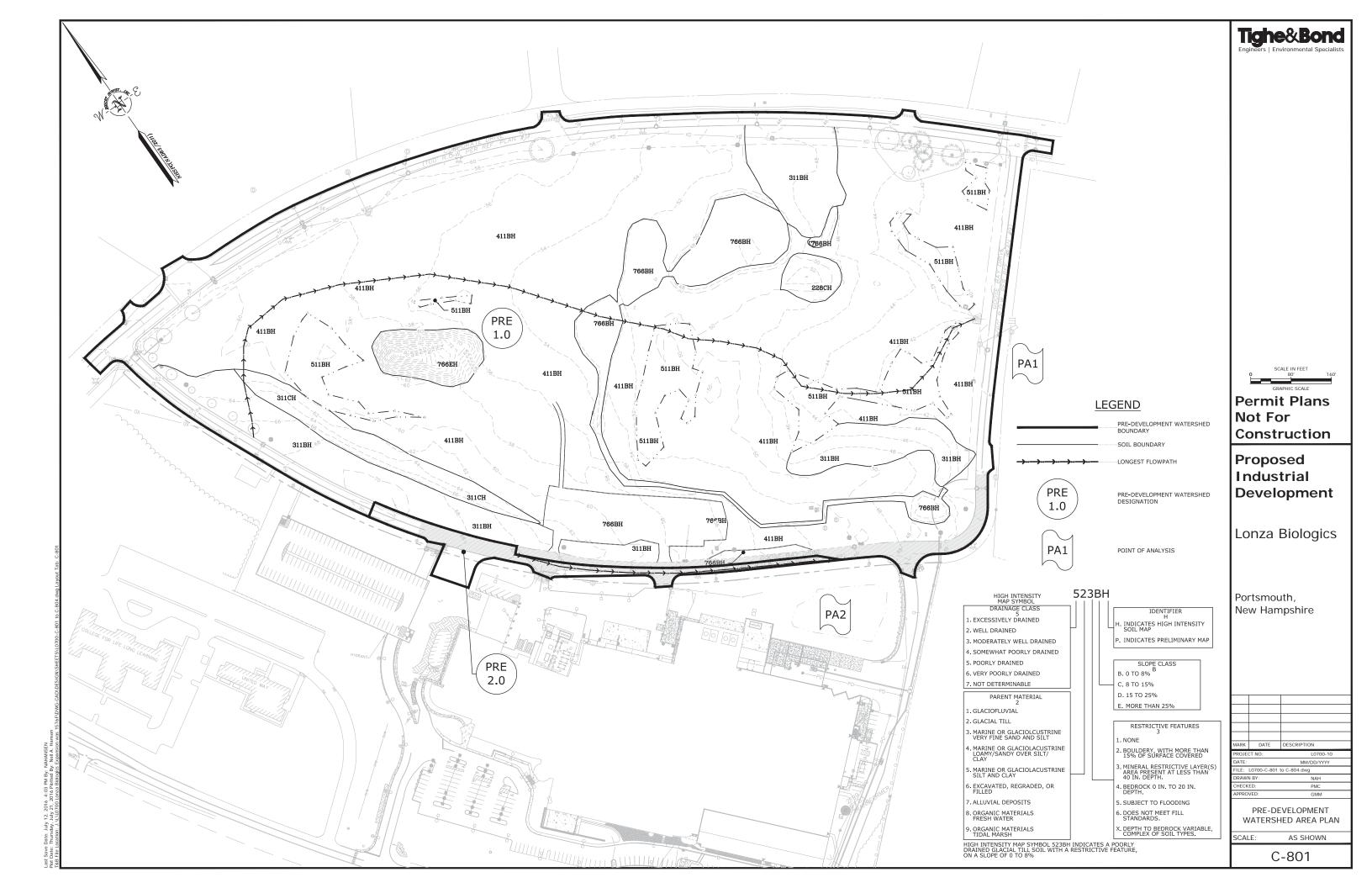
Subcatchment PRE 2.0: WATERSHED 2.0 Runoff Area=26,354 sf 79.76% Impervious Runoff Depth>7.62" Flow Length=650' Slope=0.0250 '/' Tc=5.0 min CN=93 Runoff=4.94 cfs 0.384 af

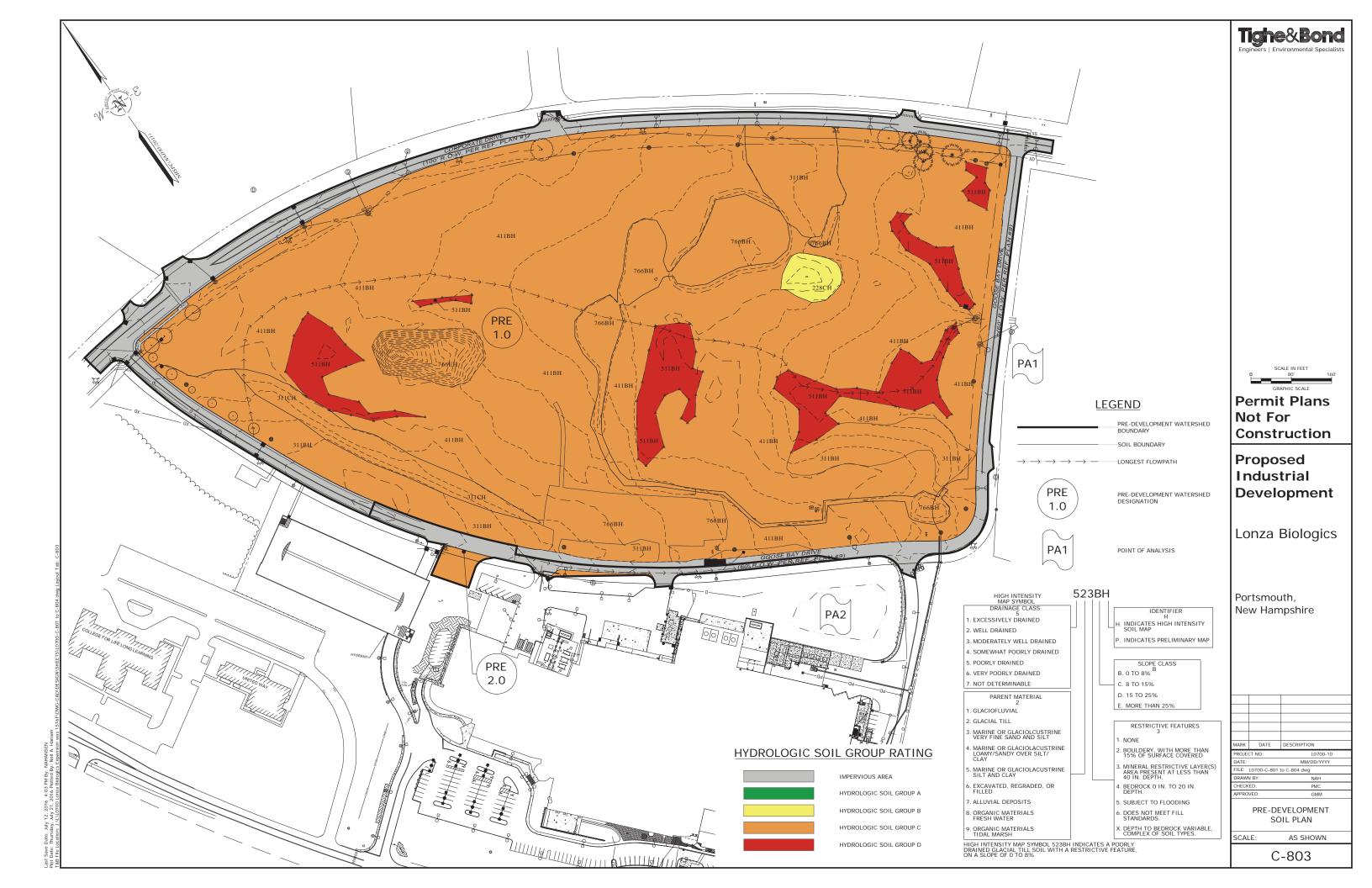
Link PA1: POINT OF ANALYSIS Inflow=102.71 cfs 12.958 af Primary=102.71 cfs 12.958 af

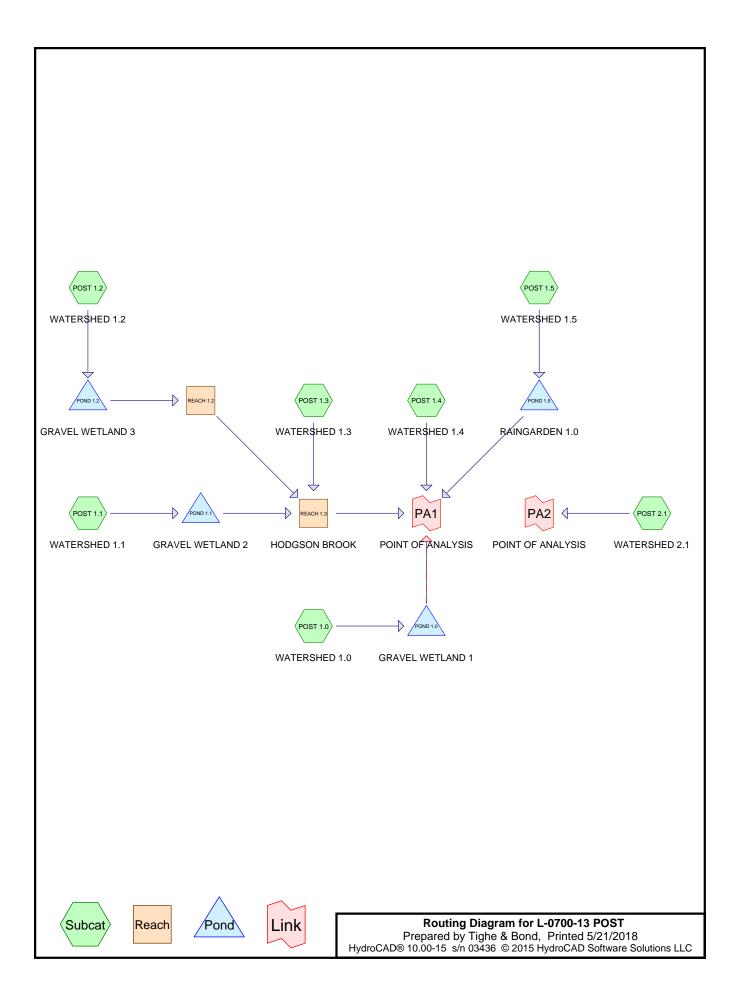
Link PA2: POINT OF ANALYSIS

Inflow=4.94 cfs 0.384 af
Primary=4.94 cfs 0.384 af

Total Runoff Area = 29.892 ac Runoff Volume = 13.341 af Average Runoff Depth = 5.36" 88.89% Pervious = 26.571 ac 11.11% Impervious = 3.322 ac







Area Listing (selected nodes)

	Area	CN	Description
(a	cres)		(subcatchment-numbers)
	0.025	61	>75% Grass cover, Good, HSG B (POST 1.5)
12	2.422	74	>75% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3,
			POST 1.4, POST 1.5)
C).222	80	>75% Grass cover, Good, HSG D (POST 1.0, POST 1.1, POST 1.2, POST 1.4)
C	0.504	78	Meadow, non-grazed, HSG D (POST 1.4)
C	0.037	98	Paved parking, HSG B (POST 1.5)
6	6.876	98	Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4,
			POST 1.5, POST 2.1)
C	0.295	98	Paved parking, HSG D (POST 1.0, POST 1.1, POST 1.2)
C	0.142	98	Roofs, HSG B (POST 1.5)
8	3.659	98	Roofs, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.5)
().710	98	Roofs, HSG D (POST 1.0, POST 1.1, POST 1.2, POST 1.5)
29	9.892	88	TOTAL AREA

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Page 3

Soil Listing (selected nodes)

A	rea Soil	Subcatchment
(acr	es) Group	Numbers
0.0	000 HSG A	
0.2	204 HSG B	POST 1.5
27.9	57 HSG C	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 1.5, POST 2.1
1.7	32 HSG D	POST 1.0, POST 1.1, POST 1.2, POST 1.4, POST 1.5
0.0	000 Other	
29.8	392	TOTAL AREA

Outflow=0.18 cfs 0.175 af

Page 4

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

- Subcatchment POST 1.0: WATERSHED Runoff Area=412,828 sf 74.83% Impervious Runoff Depth>2.80" Flow Length=1,013' Tc=16.2 min CN=92 Runoff=22.26 cfs 2.213 af
- Subcatchment POST 1.1: WATERSHED 1.1 Runoff Area=93,833 sf 45.41% Impervious Runoff Depth>2.17" Flow Length=738' Tc=13.6 min CN=85 Runoff=4.28 cfs 0.389 af
- Subcatchment POST 1.2: WATERSHED Runoff Area=196,367 sf 41.29% Impervious Runoff Depth>2.09" Flow Length=641' Tc=11.1 min CN=84 Runoff=9.27 cfs 0.784 af
- **Subcatchment POST 1.3: WATERSHED 1.3** Runoff Area=89,680 sf 65.38% Impervious Runoff Depth>2.61" Flow Length=1,602' Tc=7.3 min CN=90 Runoff=5.86 cfs 0.449 af
- Subcatchment POST 1.4: WATERSHED Runoff Area=290,401 sf 21.74% Impervious Runoff Depth>1.77" Flow Length=1,388' Tc=32.9 min CN=80 Runoff=7.49 cfs 0.982 af
- Subcatchment POST 1.5: WATERSHED Runoff Area=216,369 sf 79.15% Impervious Runoff Depth>2.90" Flow Length=1,088' Tc=15.7 min CN=93 Runoff=12.11 cfs 1.201 af
- Subcatchment POST 2.1: WATERSHED 2.1 Runoff Area=2,635 sf 100.00% Impervious Runoff Depth>3.44"

 Tc=5.0 min CN=98 Runoff=0.22 cfs 0.017 af
- **Reach REACH 1.2:** Avg. Flow Depth=0.12' Max Vel=1.63 fps Inflow=0.18 cfs 0.175 af 54.0" Round Pipe n=0.013 L=395.0' S=0.0059 '/' Capacity=151.68 cfs Outflow=0.18 cfs 0.174 af
- **Reach REACH 1.3: HODGSON BROOK** Avg. Flow Depth=0.60' Max Vel=2.01 fps Inflow=6.01 cfs 0.771 af n=0.040 L=1,211.0' S=0.0091 '/' Capacity=2,707.81 cfs Outflow=4.46 cfs 0.760 af
- Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=45.31' Storage=56,791 cf Inflow=22.26 cfs 2.213 af Primary=3.22 cfs 1.458 af Secondary=0.00 cfs 0.000 af Outflow=3.22 cfs 1.458 af
- Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=51.63' Storage=11,984 cf Inflow=4.28 cfs 0.389 af Outflow=0.16 cfs 0.149 af
- Pond POND 1.2: GRAVEL WETLAND 3 Peak Elev=52.94' Storage=26,894 cf Inflow=9.27 cfs 0.784 af
- Pond POND 1.5: RAINGARDEN 1.0 Peak Elev=46.84' Storage=27,217 cf Inflow=12.11 cfs 1.201 af
- Discarded=0.08 cfs 0.102 af Primary=1.34 cfs 0.988 af Outflow=1.42 cfs 1.090 af
- Link PA1: POINT OF ANALYSIS

 Inflow=13.07 cfs 4.188 af
 Primary=13.07 cfs 4.188 af
- Link PA2: POINT OF ANALYSIS

 Inflow=0.22 cfs 0.017 af
 Primary=0.22 cfs 0.017 af

Total Runoff Area = 29.892 ac Runoff Volume = 6.036 af Average Runoff Depth = 2.42" 44.07% Pervious = 13.174 ac 55.93% Impervious = 16.719 ac

Page 5

Summary for Subcatchment POST 1.0: WATERSHED 1.0

Runoff = 35.97 cfs @ 12.21 hrs, Volume= 3.670 af, Depth> 4.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

	Α	rea (sf)	CN E	Description						
	1	58,334	98 F	98 Roofs, HSG C						
		98,983	74 >	75% Gras	s cover, Go	ood, HSG C				
	1	08,837	98 F	Paved park	ing, HSG C					
		11,206	98 F	Roofs, HSG	B D					
		4,917			•	ood, HSG D				
		12,560		•	ing, HSG D					
_		17,991	98 F	Paved park	ing, HSG C					
	4	12,828	92 V	Veighted A	verage					
	1	03,900	2	25.17% Pei	vious Area					
	3	08,928	7	'4.83% lmp	pervious Ar	ea				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	11.2	100	0.0150	0.15		Sheet Flow,				
						Grass: Short n= 0.150 P2= 3.06"				
	8.0	100	0.0200	2.12		Shallow Concentrated Flow,				
						Grassed Waterway Kv= 15.0 fps				
	4.2	813	0.0050	050 3.21 2.52		Pipe Channel,				
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
_						n= 0.013 Corrugated PE, smooth interior				
	16.2	1 013	Total							

16.2 1,013 Total

Summary for Subcatchment POST 1.1: WATERSHED 1.1

Runoff = 7.59 cfs @ 12.19 hrs, Volume= 0.700 af, Depth> 3.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
32,905	98	Roofs, HSG C
50,995	74	>75% Grass cover, Good, HSG C
9,307	98	Paved parking, HSG C
245	98	Roofs, HSG D
231	80	>75% Grass cover, Good, HSG D
150	98	Paved parking, HSG D
93,833	85	Weighted Average
51,226		54.59% Pervious Area
42,607		45.41% Impervious Area

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Page 6

	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-				(10/300)	(013)	
	10.2	93	0.0167	0.15		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.06"
	3.4	645	0.0050	3.21	2.52	Pipe Channel,
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
_						n= 0.013 Corrugated PE, smooth interior
	13.6	738	Total			

Summary for Subcatchment POST 1.2: WATERSHED 1.2

Runoff = 16.69 cfs @ 12.15 hrs, Volume= 1.427 af, Depth> 3.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN D	escription						
	46,063	98 F	98 Roofs, HSG C						
1	14,389	74 >	75% Gras	s cover, Go	ood, HSG C				
	17,726	98 F	aved park	ing, HSG C					
	17,158	98 F	Roofs, HSG	G D					
	904	80 >	75% Gras	s cover, Go	ood, HSG D				
	127	98 F	aved park	ing, HSG D)				
1	96,367	84 V	Veighted A	verage					
1	15,293	5	8.71% Pei	vious Area					
	81,074	4	41.29% Impervious Area						
_		01		.	B 1.1				
Tc	Length	Slope	Velocity		Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
8.3	72	0.0167	0.14		Sheet Flow,				
					Grass: Short n= 0.150 P2= 3.06"				
0.2	68	0.1129	5.04		Shallow Concentrated Flow,				
				Grassed Waterway Kv= 15.0 fps					
2.6	501	0.0050	3.21	2.52					
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
					n= 0.013 Corrugated PE, smooth interior				
11.1	641	Total							

Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 9.69 cfs @ 12.10 hrs, Volume= 0.761 af, Depth> 4.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

 Area (sf)	CN	Description
31,051	74	>75% Grass cover, Good, HSG C
 58,629	98	Paved parking, HSG C
89,680	90	Weighted Average
31,051		34.62% Pervious Area
58,629		65.38% Impervious Area

F	⊃a	a	е

Tc	Length	Slope	Velocity		Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
1.6	100	0.0100	1.02		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.06"
1.0	153	0.0150	2.49		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
1.6	343	0.0050	3.47	2.73	Pipe Channel,
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.012 Concrete pipe, finished
0.1	13	0.0050	3.72	4.57	Pipe Channel,
					15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31'
					n= 0.013 Corrugated PE, smooth interior
1.8	453	0.0050	4.20	7.43	Pipe Channel,
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
					n= 0.013 Corrugated PE, smooth interior
0.4	129	0.0050	5.91	29.00	Pipe Channel,
					30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63'
					n= 0.013 Corrugated PE, smooth interior
0.8	411	0.0050	8.08	101.57	Pipe Channel,
					48.0" Round Area= 12.6 sf Perim= 12.6' r= 1.00'
					n= 0.013 Corrugated PE, smooth interior
7.3	1,602	Total			

Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff 14.39 cfs @ 12.45 hrs, Volume= 1.880 af, Depth> 3.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN E	escription					
201,658 74 >75% Grass cover, Good, HSG C								
	63,139 98 Paved parking, HSG C							
	3,633 80 >75% Grass cover, Good, HSG D							
21,971 78 Meadow, non-grazed, HSG D								
2	90,401	80 V	Veighted A	verage				
	27,262		•	vious Area				
	63,139	2	1.74% Imp	ervious Ar	ea			
	,							
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>			
1.2	84	0.0150	1.16		Sheet Flow,			
					Smooth surfaces n= 0.011 P2= 3.06"			
1.2	62	0.0150	0.86		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
0.1	31	0.3230	8.52		Shallow Concentrated Flow,			
					Grassed Waterway Kv= 15.0 fps			
30.4	1,211	0.0090	0.66		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
32.9	1,388	Total						

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Page 8

Summary for Subcatchment POST 1.5: WATERSHED 1.5

Runoff = 19.34 cfs @ 12.21 hrs, Volume= 1.969 af, Depth> 4.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

Ar	ea (sf)	CN E	Description					
6,192 98 Roofs, HSG B								
	1,098	61 >	75% Gras	s cover, Go	ood, HSG B			
	1,601	98 F	Paved park	ing, HSG B				
13	39,882	98 F	Roofs, HSG	G C				
2	14,025			,	ood, HSG C			
2	21,245			ing, HSG C				
	2,326	98 F	Roofs, HSG	6 D				
21	16,369	93 V	Veighted A	verage				
۷	15,123	2	20.85% Pervious Area					
17	71,246	7	79.15% Impervious Area					
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
10.5	92	0.0150	0.15		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.06"			
5.2	996	0.0050	3.21	2.52	Pipe Channel,			
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
					n= 0.013 Corrugated PE, smooth interior			
15.7	1,088	Total						

Summary for Subcatchment POST 2.1: WATERSHED 2.1

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 5.34"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Year Rainfall=5.58"

A	rea (sf)	CN E	Description				
	2,635	98 F	98 Paved parking, HSG C				
	2,635	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
5.0					Direct Entry,		

Summary for Reach REACH 1.2:

Inflow Are	a =	4.508 ac, 4	I1.29% Impervio	us, Inflow Depth >	1.76"	for 10 Ye	ar event
Inflow	=	2.12 cfs @	12.95 hrs, Volu	me= 0.66′	1 af		
Outflow	=	2.12 cfs @	12.97 hrs, Volu	me= 0.660	af, Atte	en= 0%, La	ag= 1.4 min

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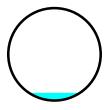
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Page 9

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Max. Velocity= 3.39 fps, Min. Travel Time= 1.9 min Avg. Velocity = 2.15 fps, Avg. Travel Time= 3.1 min

Peak Storage= 246 cf @ 12.97 hrs Average Depth at Peak Storage= 0.37' Bank-Full Depth= 4.50' Flow Area= 15.9 sf, Capacity= 151.68 cfs

54.0" Round Pipe n= 0.013 Corrugated PE, smooth interior Length= 395.0' Slope= 0.0059 '/' Inlet Invert= 49.35', Outlet Invert= 47.00'



Summary for Reach REACH 1.3: HODGSON BROOK

Inflow Area = 8.721 ac, 47.99% Impervious, Inflow Depth > 2.30" for 10 Year event

Inflow = 9.96 cfs @ 12.10 hrs, Volume= 1.669 af

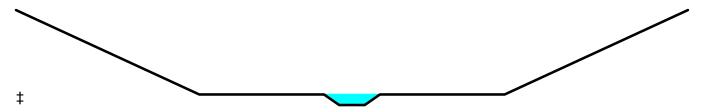
Outflow = 6.62 cfs @ 12.09 hrs, Volume= 1.655 af, Atten= 34%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.24 fps, Min. Travel Time= 9.0 min Avg. Velocity = 1.01 fps, Avg. Travel Time= 19.9 min

Peak Storage= 5,572 cf @ 12.32 hrs Average Depth at Peak Storage= 0.80' Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,707.81 cfs

Custom cross-section, Length= 1,211.0' Slope= 0.0091 '/' (101 Elevation Intervals) Constant n= 0.040 Winding stream, pools & shoals Inlet Invert= 47.00', Outlet Invert= 36.00'



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Page 10

Offset	Elevation	Chan.Depth	
(feet)	(feet)	(feet)	
0.00	12.00	0.00	
18.00	6.00	6.00	
30.25	6.00	6.00	
31.75	5.25	6.75	
34.25	5.25	6.75	
35.75	6.00	6.00	
48.00	6.00	6.00	
66.00	12.00	0.00	

Depth	End Area	Perim.	Storage	Discharge
(feet)	(sq-ft)	(feet)	(cubic-feet)	(cfs)
0.00	0.0	2.5	0	0.00
0.75	3.0	30.4	3,633	2.27
6.75	291.0	68.3	352,401	2,707.81

Summary for Pond POND 1.0: GRAVEL WETLAND 1

Inflow Area = 9.477 ac, 74.83% Impervious, Inflow Depth > 4.65" for 10 Year event

35.97 cfs @ 12.21 hrs, Volume= Inflow 3.670 af

21.51 cfs @ 12.47 hrs, Volume= 2.804 af, Atten= 40%, Lag= 15.4 min Outflow

21.51 cfs @ 12.47 hrs, Volume= Primary 2.804 af 0.00 cfs @ 0.00 hrs, Volume= Secondary = 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 46.34' @ 12.47 hrs Surf.Area= 20,404 sf Storage= 76,594 cf Flood Elev= 48.00' Surf.Area= 23,557 sf Storage= 113,085 cf

Plug-Flow detention time= 215.1 min calculated for 2.804 af (76% of inflow)

Center-of-Mass det. time= 134.4 min (921.7 - 787.3)

23,557 100.0

48.00

Volume	Invert	Avail.Storage	Storage Descr	iption	
#1	39.05'	113,085 cf	Custom Stage	e Data (Prismatic)	Listed below (Recalc)
Elevation (feet)	Surf.Ar (sq		Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
39.05	9,8	54 0.0	0	0	
41.35	9,8	54 30.0	6,799	6,799	
42.00	9,8	54 80.0	5,124	11,923	
43.00	11,9	43 100.0	10,899	22,822	
44.00	14,2	02 100.0	13,073	35,894	
45.00	16,8	91 100.0	15,547	51,441	
46.00	19,7	52 100.0	18,322	69,762	
47.00	21,6	68 100.0	20,710	90,472	

22,613

113,085

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Page 11

Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	24.0" Round Culvert
	-		L= 30.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 41.35' / 41.20' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf
#2	Device 1	41.35'	3.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	43.40'	4.0" Vert. Orifice/Grate X 2.00 C= 0.600
#4	Device 1	45.00'	3.0' long x 0.50' rise Sharp-Crested Rectangular Weir
			2 End Contraction(s)
#5	Device 1	46.25'	4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600
			Limited to weir flow at low heads
#6	Secondary	46.50'	20.0' long x 26.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=20.19 cfs @ 12.47 hrs HW=46.33' TW=0.00' (Dynamic Tailwater)

1=Culvert (Passes 20.19 cfs of 30.19 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.52 cfs @ 10.61 fps)

-3=Orifice/Grate (Orifice Controls 1.40 cfs @ 8.01 fps)

-4=Sharp-Crested Rectangular Weir (Orifice Controls 7.38 cfs @ 5.09 fps)

-5=Orifice/Grate (Weir Controls 10.89 cfs @ 0.94 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=39.05' TW=0.00' (Dynamic Tailwater) 6=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond POND 1.1: GRAVEL WETLAND 2

Inflow Area =	2.154 ac, 45.41% Impervious, Inflow Depth > 3.90" for 10 Year event	
Inflow =	7.59 cfs @ 12.19 hrs, Volume= 0.700 af	
Outflow =	0.45 cfs @ 14.92 hrs, Volume= 0.248 af, Atten= 94%, Lag= 164.3	min
Primary =	0.45 cfs @ 14.92 hrs, Volume= 0.248 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 52.92' @ 14.92 hrs Surf.Area= 8,402 sf Storage= 21,360 cf Flood Elev= 56.00' Surf.Area= 15,452 sf Storage= 57,777 cf

Plug-Flow detention time= 363.1 min calculated for 0.248 af (35% of inflow) Center-of-Mass det. time= 235.5 min (1,044.5 - 809.0)

Volume	Invert	Avail.Storage	Storage Description
#1	47.05'	57,777 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Printed 5/21/2018 Page 12

Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
47.05	3,293	0.0	0	0
49.35	3,293	30.0	2,272	2,272
50.00	3,643	80.0	1,803	4,076
51.00	5,106	100.0	4,375	8,450
52.00	6,739	100.0	5,923	14,373
53.00	8,541	100.0	7,640	22,013
54.00	10,628	100.0	9,585	31,597
55.00	13,140	100.0	11,884	43,481
56.00	15,452	100.0	14,296	57,777

Device	Routing	Invert	Outlet Devices
#1	Primary	49.35'	18.0" Round Culvert
	•		L= 33.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 49.35' / 47.55' S= 0.0545 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	49.35'	2.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	52.85'	4.0' long x 2.00' rise Sharp-Crested Rectangular Weir
			2 End Contraction(s)
#4	Device 1	55.50'	4.0" W x 4.0" H Vert. Orifice/Grate X 106.00 C= 0.600

Primary OutFlow Max=0.45 cfs @ 14.92 hrs HW=52.92' TW=47.39' (Dynamic Tailwater)

1=Culvert (Passes 0.45 cfs of 14.30 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.20 cfs @ 8.99 fps)

—3=Sharp-Crested Rectangular Weir (Weir Controls 0.26 cfs @ 0.88 fps)

-4=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond POND 1.2: GRAVEL WETLAND 3

Inflow Area = 4.508 ac, 41.29% Impervious, Inflow Depth > 3.80" for 10 Year event

Inflow = 16.69 cfs @ 12.15 hrs, Volume= 1.427 af

Outflow = 2.12 cfs @ 12.95 hrs, Volume= 0.661 af, Atten= 87%, Lag= 47.5 min

Primary = 2.12 cfs @ 12.95 hrs, Volume= 0.661 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Peak Elev= 53.78' @ 12.95 hrs Surf.Area= 12,619 sf Storage= 36,585 cf

Flood Elev= 56.00' Surf.Area= 19,100 sf Storage= 71,490 cf

Plug-Flow detention time= 263.5 min calculated for 0.661 af (46% of inflow)

Center-of-Mass det. time= 148.6 min (958.5 - 809.9)

Volume	Invert	Avail.Storage	Storage Description
#1	47.55'	71,490 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Page 13

Elevation	Surf.Area	Voids	Inc.Store	Cum.Store
(feet)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)
47.55	5,882	0.0	0	0
49.85	5,882	30.0	4,059	4,059
50.50	5,882	80.0	3,059	7,117
51.00	6,616	100.0	3,125	10,242
52.00	8,580	100.0	7,598	17,840
53.00	10,713	100.0	9,647	27,486
54.00	13,157	100.0	11,935	39,421
55.00	15,940	100.0	14,549	53,970
56.00	19,100	100.0	17,520	71,490

Device	Routing	Invert	Outlet Devices
#1	Primary	49.85'	24.0" Round Culvert
	·		L= 22.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 49.85' / 49.45' S= 0.0182 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf
#2	Device 1	49.85'	2.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	53.50'	4.0' long x 2.00' rise Sharp-Crested Rectangular Weir
			2 End Contraction(s)
#4	Device 1	55.50'	4.0" W x 4.0" H Vert. Orifice/Grate X 106.00 C= 0.600

Primary OutFlow Max=2.12 cfs @ 12.95 hrs HW=53.78' TW=49.72' (Dynamic Tailwater)

1=Culvert (Passes 2.12 cfs of 25.89 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.21 cfs @ 9.44 fps)

-3=Sharp-Crested Rectangular Weir (Weir Controls 1.91 cfs @ 1.73 fps)

-4=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond POND 1.5: RAINGARDEN 1.0

Inflow Area =	4.967 ac, 79.15% Impervious, Inflo	ow Depth > 4.76" for 10 Year event
Inflow =	19.34 cfs @ 12.21 hrs, Volume=	1.969 af
Outflow =	1.67 cfs @ 13.74 hrs, Volume=	1.665 af, Atten= 91%, Lag= 91.7 min
Discarded =	0.09 cfs @ 13.74 hrs, Volume=	0.123 af
Primary =	1.58 cfs @ 13.74 hrs, Volume=	1.541 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 48.42' @ 13.74 hrs Surf.Area= 13,235 sf Storage= 46,447 cf Flood Elev= 50.00' Surf.Area= 15,470 sf Storage= 69,161 cf

Plug-Flow detention time= 293.4 min calculated for 1.665 af (85% of inflow) Center-of-Mass det. time= 229.3 min (1,011.9 - 782.6)

Volume	Invert	Avail.Storage	Storage Description
#1	41.35'	69,161 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Page 14

Elevation	Surf.Area	Voids	Inc.Store	Cum.Store
(feet)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)
41.35	8,830	0.0	0	0
43.50	8,830	40.0	7,594	7,594
45.00	8,830	10.0	1,325	8,918
46.00	10,045	100.0	9,438	18,356
48.00	12,645	100.0	22,690	41,046
50.00	15,470	100.0	28,115	69,161

Device	Routing	Invert	Outlet Devices
#1	Primary	42.42'	6.0" Round Culvert
	_		L= 48.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 42.42' / 42.20' S= 0.0046 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf
#2	Primary	49.25'	10.0' long x 12.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.58 2.63 2.70 2.67 2.66 2.67 2.66 2.63
#3	Discarded	41.35'	0.300 in/hr Exfiltration over Surface area Phase-In= 0.01

Discarded OutFlow Max=0.09 cfs @ 13.74 hrs HW=48.42' (Free Discharge) **3=Exfiltration** (Exfiltration Controls 0.09 cfs)

Primary OutFlow Max=1.58 cfs @ 13.74 hrs HW=48.42' TW=0.00' (Dynamic Tailwater)

1=Culvert (Barrel Controls 1.58 cfs @ 8.04 fps)

—2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Link PA1: POINT OF ANALYSIS

Inflow Area = 29.832 ac, 55.84% Impervious, Inflow Depth > 3.17" for 10 Year event

Inflow = 41.55 cfs @ 12.47 hrs, Volume= 7.880 af

Primary = 41.55 cfs @ 12.47 hrs, Volume= 7.880 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Link PA2: POINT OF ANALYSIS

Inflow Area = 0.060 ac,100.00% Impervious, Inflow Depth > 5.34" for 10 Year event

Inflow = 0.33 cfs @ 12.07 hrs, Volume= 0.027 af

Primary = 0.33 cfs @ 12.07 hrs, Volume= 0.027 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

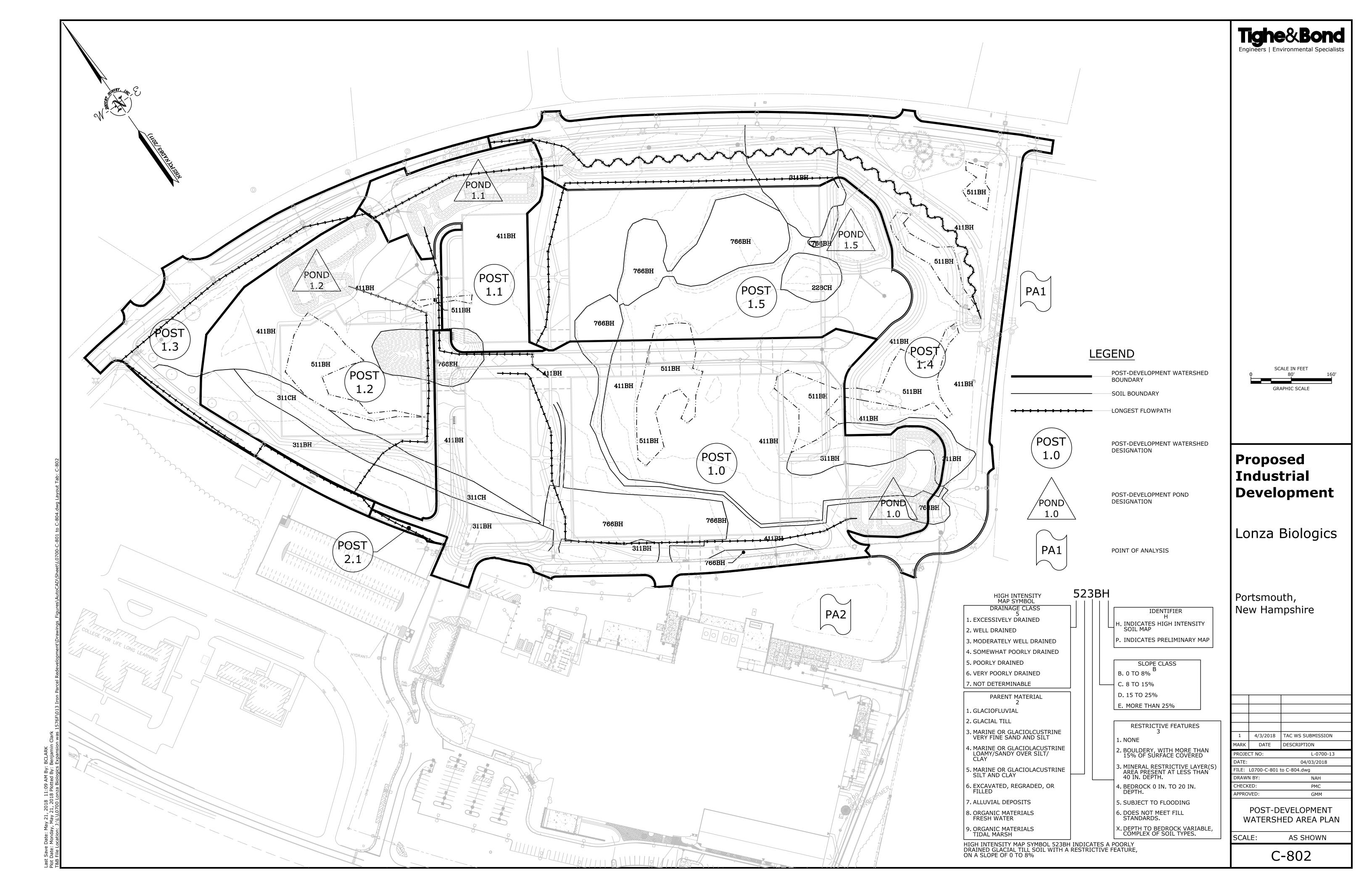
- Subcatchment POST 1.0: WATERSHED Runoff Area=412,828 sf 74.83% Impervious Runoff Depth>7.48" Flow Length=1,013' Tc=16.2 min CN=92 Runoff=56.44 cfs 5.910 af
- Subcatchment POST 1.1: WATERSHED 1.1 Runoff Area=93,833 sf 45.41% Impervious Runoff Depth>6.64" Flow Length=738' Tc=13.6 min CN=85 Runoff=12.64 cfs 1.193 af
- Subcatchment POST 1.2: WATERSHED Runoff Area=196,367 sf 41.29% Impervious Runoff Depth>6.53" Flow Length=641' Tc=11.1 min CN=84 Runoff=28.04 cfs 2.452 af
- Subcatchment POST 1.3: WATERSHED 1.3 Runoff Area=89,680 sf 65.38% Impervious Runoff Depth>7.25" Flow Length=1,602' Tc=7.3 min CN=90 Runoff=15.42 cfs 1.244 af
- **Subcatchment POST 1.4: WATERSHED** Runoff Area=290,401 sf 21.74% Impervious Runoff Depth>6.02" Flow Length=1,388' Tc=32.9 min CN=80 Runoff=25.27 cfs 3.346 af
- Subcatchment POST 1.5: WATERSHED Runoff Area=216,369 sf 79.15% Impervious Runoff Depth>7.60" Flow Length=1,088' Tc=15.7 min CN=93 Runoff=30.14 cfs 3.147 af
- Subcatchment POST 2.1: WATERSHED 2.1 Runoff Area=2,635 sf 100.00% Impervious Runoff Depth>8.22"

 Tc=5.0 min CN=98 Runoff=0.51 cfs 0.041 af
- **Reach REACH 1.2:** Avg. Flow Depth=0.92' Max Vel=5.94 fps Inflow=13.83 cfs 1.677 af 54.0" Round Pipe n=0.013 L=395.0' S=0.0059 '/' Capacity=151.68 cfs Outflow=13.82 cfs 1.675 af
- **Reach REACH 1.3: HODGSON BROOK** Avg. Flow Depth=1.04' Max Vel=2.24 fps Inflow=23.77 cfs 3.638 af n=0.040 L=1,211.0' S=0.0091 '/' Capacity=2,707.81 cfs Outflow=21.77 cfs 3.621 af
- Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=46.90' Storage=88,237 cf Inflow=56.44 cfs 5.910 af Primary=32.25 cfs 4.616 af Secondary=13.47 cfs 0.285 af Outflow=45.72 cfs 4.901 af
- Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=53.40' Storage=25,553 cf Inflow=12.64 cfs 1.193 af Outflow=5.33 cfs 0.718 af
- Pond POND 1.2: GRAVEL WETLAND 3 Peak Elev=54.56' Storage=47,298 cf Inflow=28.04 cfs 2.452 af Outflow=13.83 cfs 1.677 af
- Pond POND 1.5: RAINGARDEN 1.0 Peak Elev=49.71' Storage=64,778 cf Inflow=30.14 cfs 3.147 af Discarded=0.10 cfs 0.141 af Primary=10.10 cfs 2.362 af Outflow=10.21 cfs 2.504 af
- Link PA1: POINT OF ANALYSIS

 Inflow=92.68 cfs 14.231 af
 Primary=92.68 cfs 14.231 af
- Link PA2: POINT OF ANALYSIS

 Inflow=0.51 cfs 0.041 af
 Primary=0.51 cfs 0.041 af

Total Runoff Area = 29.892 ac Runoff Volume = 17.334 af Average Runoff Depth = 6.96" 44.07% Pervious = 13.174 ac 55.93% Impervious = 16.719 ac







GRAVEL WETLAND DESIGN CRITERIA (Env-Wq 1508.05)

Type/Node Name: Gravel Wetland 1 (POND 1.0)

Enter the node name in the drainage analysis if applicable

9.48		A = Area draining to the practice	
7.09	ac	A_{I} = Impervious area draining to the practice	
0.75	decimal	I = percent impervious area draining to the practice, in decimal form	
0.72	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
6.85	ac-in	WQV=1" x Rv x A	
24,883	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
2,488	cf	10% x WQV (check calc for sediment forebay and micropool volume)	
11,197	cf	45% x WQV (check calc for gravel wetland treatment bay volume)	
3,205	cf	V_{SED} = sediment forebay volume	$\leftarrow \geq 10\% WQV$
14,269	cf	V_{TB1} = volume of treatment bay 1	$\leftarrow \geq 45\% WQV$
20,912	cf	V_{TB2} = volume of treatment bay 2	$\leftarrow \geq 45\% WQV$
43.17	ft	E_{WQV} = elevation of WQV (attach stage-storage table)	
0.31	cfs	Q_{WQV} = discharge at the E_{WQV} (attach stage-discharge table)	\leftarrow <2Q _{avg}
44.59	hours	T_{ED} = drawdown time of extended detention = $2WQV/Q_{WQV}$	← ≥ 24-hrs
3.00	:1	Pond side slopes	← ≥3:1
39.50	ft	Elevation of SHWT	
41.35	ft	Epp = Elevation of the permanent pool (elevation of lowest orifice) ²	$\leftarrow \geq E_{SHWT}$ - 2 ft
87.00	ft	Length of the flow path between the inlet and outlet in each cell	← ≥ 15 ft
		What mechanism is proposed to prevent the outlet structure from clogg	ing (applicable for
Trasl	h rack	orifices/weirs with a dimension of ≤ 6 ")?	
46.90	ft	Peak elevation of the 50-year storm event (E_{50})	
48.00	ft	Berm elevation of the pond	
YES		$E_{50} \le$ the berm elevation?	← yes
Qualified 1	professional	that developed the planting plan:	
	rofession:		
1 17 1	1 1	the watland soil and below the high flow by pass	

1. Volume stored above the wetland soil and below the high flow by-pass.

-		

Last Revised: February 2018

Designer's Notes:

^{2. 4&}quot; to 8" below the wetland soil. If lowest orifice is less than 2 feet below SHWT, and saturated hydraulic conductivity (Ksat) is greater than 0.005 in/hr, the system must be lined.

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Stage-Area-Storage for Pond POND 1.0: GRAVEL WETLAND 1

Floretion	Curfoso	Ctorogo	L Florestion	Curtoso	Ctorogo
Elevation	Surface	Storage	Elevation	Surface	Storage
(feet) 39.05	(sq-ft) 9,854	(cubic-feet) 0	(feet) 44.35	(sq-ft) 15,143	(cubic-feet) 41,030
39.05 39.15	9,854 9,854	296	44.35 44.45	15,143	42,558
39.15	9,854 9,854	591	44.55	15,681	44,112
39.35	9,854 9,854	887	44.65	15,950	45,694
39.45	9,854 9,854	1,182	44.75	16,219	47,302
39.55	9,854 9,854	1,478	44.75 44.85	16,488	48,937
39.65	9,854 9,854	1,774	44.85 44.95	16,757	50,600
39.75	9,854 9,854	2,069	45.05	17,034	52,289
39.85	9,854	2,365	45.05 45.15	17,320	54,007
39.95	9,854 9,854	2,565 2,661	45.15 45.25	17,606	55,753
40.05	9,854	2,956	45.35	17,892	57,528
40.15	9,854	3,252	45.45	18,178	59,331
40.25	9,854	3,547	45.55	18,465	61,164
40.35	9,854	3,843	45.65	18,751	63,024
40.45	9,854	4,139	45.75	19,037	64,914
40.55	9,854	4,434	45.85	19,323	66,832
40.65	9,854	4,730	45.95	19,609	68,778
40.75	9,854	5,026	46.05	19,848	70,752
40.85	9,854	5,321	46.15	20,039	72,747
40.95	9,854	5,617	46.25	20,231	74,760
41.05	9,854	5,912	46.35	20,423	76,793
41.15	9,854	6,208	46.45	20,614	78,845
41.25	9,854	6,504	46.55	20,806	80,916
41.35	9,854	6,799	46.65	20,997	83,006
41.45	9,854	7,588	46.75	21,189	85,115
41.55	9,854	8,376	46.85	21,381	87,244
41.65	9,854	9,164	46.95	21,572	89,391
41.75	9,854	9,953	47.05	21,762	91,558
41.85	9,854	10,741	47.15	21,951	93,744
41.95	9,854	11,529	47.25	22,140	95,948
42.05	9,958	12,419	47.35	22,329	98,172
42.15	10,167	13,425	47.45	22,518	100,414
42.25	10,376	14,452	47.55	22,707	102,675
42.35	10,585	15,500	47.65	22,896	104,956
42.45	10,794	16,569	47.75	23,085	107,255
42.55	11,003	17,659	47.85	23,274	109,573
42.65	11,212	18,770	47.95	23,463	111,909
42.75	11,421	19,901			
42.85	11,630	21,054			
42.95	11,839	22,227			
43.05	12,056	23,422			
43.15	12,282	24,639			
43.25	12,508	25,878			
43.35	12,734	27,140			
43.45	12,960	28,425			
43.55	13,185	29,732			
43.65	13,411	31,062			
43.75	13,637	32,414			
43.85	13,863	33,789			
43.95	14,089	35,187			
44.05	14,336	36,608			
44.15	14,605	38,055			
44.25	14,874	39,529			
		ļ	1		

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Stage-Discharge for Pond POND 1.0: GRAVEL WETLAND 1

Elevation	Discharge	Primary	Secondary	Elevation	Discharge	Primary	Secondary
(feet)	(cfs)	(cfs)	(cfs)	(feet)	(cfs)	(cfs)	(cfs)
39.05	0.00	0.00	0.00	44.35	1.14	1.14	0.00
39.15	0.00	0.00	0.00	44.45	1.20	1.20	0.00
39.25	0.00	0.00	0.00	44.55	1.25	1.25	0.00
39.35	0.00	0.00	0.00	44.65	1.30	1.30	0.00
39.45	0.00	0.00	0.00	44.75	1.34	1.34	0.00
39.55	0.00	0.00	0.00	44.85	1.39	1.39	0.00
39.65	0.00	0.00	0.00	44.95	1.43	1.43	0.00
39.75	0.00	0.00	0.00	45.05	1.58	1.58	0.00
39.85	0.00	0.00	0.00	45.15	2.07	2.07	0.00
39.95	0.00	0.00	0.00	45.25	2.76	2.76	0.00
40.05	0.00	0.00	0.00	45.35	3.57	3.57	0.00
40.15	0.00	0.00	0.00	45.45	4.50	4.50	0.00
40.25	0.00	0.00	0.00	45.55	5.42	5.42	0.00
40.35	0.00	0.00	0.00	45.65	6.11	6.11	0.00
40.45	0.00	0.00	0.00	45.75	6.70	6.70	0.00
40.55	0.00	0.00	0.00	45.85	7.23	7.23	0.00
40.65	0.00	0.00	0.00	45.95	7.72	7.72	0.00
40.75	0.00	0.00	0.00	46.05	8.16	8.16	0.00
40.85	0.00	0.00	0.00	46.15	8.59	8.59	0.00
40.95	0.00	0.00	0.00	46.25	8.99	8.99	0.00
41.05	0.00	0.00	0.00	46.35	23.98	23.98	0.00
41.15	0.00	0.00	0.00	46.45	30.63	30.63	0.00
41.25	0.00	0.00	0.00	46.55	31.60	31.00	0.60
41.35	0.00	0.00	0.00	46.65	34.48	31.37	3.11
41.45	0.02	0.02	0.00	46.75	38.44	31.73	6.71
41.55	0.06	0.06	0.00	46.85	43.25	32.09	11.16
41.65	0.10	0.10	0.00	46.95	48.74	32.44	16.30
41.75	0.12	0.12	0.00	47.05	54.82	32.79	22.03
41.85	0.14	0.14	0.00	47.15	61.28	33.14	28.14
41.95	0.16	0.16	0.00	47.25	67.97	33.48	34.49
42.05	0.18	0.18	0.00	47.35	75.16	33.82	41.34
42.15	0.19	0.19	0.00	47.45	82.91	34.16	48.75
42.25	0.21	0.21	0.00	47.55	91.14	34.49	56.65
42.35	0.22	0.22	0.00	47.65	99.88	34.82	65.05
42.45	0.23	0.23	0.00	47.75	108.94	35.15	73.79
42.55	0.25	0.25	0.00	47.85	118.30	35.48	82.82
42.65	0.26	0.26	0.00	47.95	127.90	35.80	92.10
42.75	0.27	0.27	0.00				
42.85	0.28	0.28	0.00				
42.95	0.29	0.29	0.00				
43.05	0.30	0.30	0.00				
43.15	0.31	0.31	0.00				
43.25	0.31	0.31	0.00				
43.35	0.32	0.32	0.00				
43.45	0.34	0.34	0.00				
43.55 43.65	0.44	0.44	0.00 0.00				
43.65	0.59 0.72	0.59 0.72	0.00				
43.75	0.72	0.72	0.00				
43.95	0.89	0.81	0.00				
44.05	0.89	0.89	0.00				
44.05	1.03	1.03	0.00				
44.25	1.09	1.03	0.00				
5			5.00				



GRAVEL WETLAND DESIGN CRITERIA (Env-Wq 1508.05)

Type/Node Name: Gravel Wetland 2 (POND 1.1)

Enter the node name in the drainage analysis if applicable

3.88 ac	A = Area draining to the practice	
2.70 ac	A_{I} = Impervious area draining to the practice	
0.70 decimal	I = percent impervious area draining to the practice, in decimal form	
0.68 unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
2.62 ac-in	WQV= 1" x Rv x A	
9,524 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
952 cf	10% x WQV (check calc for sediment forebay and micropool volume)	
4,286 cf	45% x WQV (check calc for gravel wetland treatment bay volume)	
2,210 cf	V _{SED} = sediment forebay volume	$\leftarrow \geq 10\% \text{WQV}$
8,799 cf	V_{TB1} = volume of treatment bay 1	$\leftarrow \geq 45\% WQV$
12,883 cf	V_{TB2} = volume of treatment bay 2	$\leftarrow \geq 45\% WQV$
51.21 ft	E_{WQV} = elevation of WQV (attach stage-storage table)	
0.14 cfs	Q_{WQV} = discharge at the E_{WQV} (attach stage-discharge table)	\leftarrow <2Q _{avg}
37.80 hours	T_{ED} = drawdown time of extended detention = $2WQV/Q_{WQV}$	← ≥ 24-hrs
3.00 :1	Pond side slopes	← ≥3:1
46.00 ft	Elevation of SHWT	
49.35 ft	Epp = Elevation of the permanent pool (elevation of lowest orifice) ²	$\leftarrow \geq E_{SHWT} - 2 \text{ ft}$
105.00 ft	Length of the flow path between the inlet and outlet in each cell	$\leftarrow \geq 15 \text{ ft}$
	What mechanism is proposed to prevent the outlet structure from clogg	ing (applicable for
Trash rack	orifices/weirs with a dimension of ≤ 6 ")?	
53.59 ft	Peak elevation of the 50-year storm event (E_{50})	
56.00 ft	Berm elevation of the pond	
YES	$E_{50} \le$ the berm elevation?	← yes
Qualified professiona	al that developed the planting plan:	
Name, Profession:		
	the westland soil and helow the high flow by mass	

1. Volume stored above the wetland soil and below the high flow by-pass.

Designer's Notes:			

Last Revised: February 2018

^{2. 4&}quot; to 8" below the wetland soil. If lowest orifice is less than 2 feet below SHWT, and saturated hydraulic conductivity (Ksat) is greater than 0.005 in/hr, the system must be lined.

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Stage-Area-Storage for Pond POND 1.1: GRAVEL WETLAND 2

Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
47.05	3,293	0	52.35	7,370	16,842
47.15	3,293	99	52.45	7,550	17,588
47.25	3,293	198	52.55	7,730	18,352
47.35	3,293	296	52.65	7,910	19,134
47.45	3,293	395	52.75	8,091	19,934
47.55	3,293	494	52.85	8,271	20,752
47.65	3,293	593	52.95	8,451	21,588
47.75	3,293	692	53.05	8,645	22,442
47.85	3,293	790	53.15	8,854	23,317
47.95	3,293	889	53.25	9,063	24,213
48.05	3,293	988	53.35	9,271	25,130
48.15	3,293	1,087	53.45	9,480	26,067
48.25	3,293	1,185	53.55	9,689	27,026
48.35	3,293	1,284	53.65	9,898	28,005
48.45	3,293	1,383	53.75	10,106	29,005
48.55	3,293	1,482	53.85	10,315	30,026
48.65	3,293	1,581	53.95	10,524	31,068
48.75	3,293	1,679	54.05	10,754	32,132
48.85	3,293	1,778	54.15	11,005	33,219
48.95	3,293	1,877	54.25	11,256	34,333
49.05	3,293	1,976	54.35	11,507	35,471
49.15	3,293	2,075	54.45	11,758	36,634
49.25	3,293	2,173	54.55	12,010	37,822
49.35	3,293	2,272	54.65	12,261	39,036
49.45	3,347	2,538	54.75	12,512	40,275
49.55 40.65	3,401	2,808	54.85	12,763	41,538
49.65 40.75	3,455	3,082	54.95	13,014	42,827
49.75	3,508	3,360	55.05	13,256	44,141 45,479
49.85 40.05	3,562	3,643	55.15	13,487	45,478 46,939
49.95 50.05	3,616	3,930	55.25 55.35	13,718	46,838
50.05 50.15	3,716 3,862	4,260 4,638	55.45	13,949 14,180	48,222 49,628
50.15	4,009	5,032	55.55	14,180	51,058
50.35	4,155	5,440	55.65	14,643	52,510
50.45	4,301	5,863	55.75	14,874	53,986
50.55	4,448	6,300	55.85	15,105	55,485
50.65	4,594	6,753	55.95	15,336	57,007
50.75	4,740	7,219	00.00	10,000	01,001
50.85	4,887	7,701			
50.95	5,033	8,197			
51.05	5,188	8,707			
51.15	5,351	9,234			
51.25	5,514	9,778			
51.35	5,678	10,337			
51.45	5,841	10,913			
51.55	6,004	11,505			
51.65	6,167	12,114			
51.75	6,331	12,739			
51.85	6,494	13,380			
51.95	6,657	14,038			
52.05	6,829	14,712			
52.15	7,009	15,404			
52.25	7,190	16,114			
			•		

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Stage-Discharge for Pond POND 1.1: GRAVEL WETLAND 2

Elevation	Primary	Elevation	Primary
(feet)	(cfs)	(feet)	(cfs)
47.05	0.00	52.35	0.18
47.15	0.00	52.45	0.18
47.25	0.00	52.55	0.19
47.35 47.45	0.00 0.00	52.65 52.75	0.19 0.19
47.45 47.55	0.00	52.75 52.85	0.19
47.65	0.00	52.95	0.13
47.75	0.00	53.05	1.36
47.85	0.00	53.15	2.32
47.95	0.00	53.25	3.45
48.05	0.00	53.35	4.72
48.15	0.00	53.45	6.11
48.25	0.00	53.55	7.61
48.35	0.00	53.65	9.20
48.45 48.55	0.00 0.00	53.75 53.85	10.88 12.65
48.65	0.00	53.95	14.48
48.75	0.00	54.05	16.39
48.85	0.00	54.15	17.12
48.95	0.00	54.25	17.33
49.05	0.00	54.35	17.54
49.15	0.00	54.45	17.75
49.25	0.00	54.55	17.95
49.35	0.00	54.65	18.15
49.45 49.55	0.01 0.04	54.75 54.85	18.35 18.54
49.65	0.04	54.95	18.74
49.75	0.06	55.05	18.93
49.85	0.07	55.15	19.12
49.95	0.08	55.25	19.31
50.05	0.08	55.35	19.50
50.15	0.09	55.45	19.68
50.25	0.09	55.55	19.86
50.35 50.45	0.10 0.11	55.65 55.75	20.05
50.45 50.55	0.11	55.75 55.85	20.23 20.40
50.65	0.11	55.95	20.40 20.58
50.75	0.12	00.00	20.00
50.85	0.13		
50.95	0.13		
51.05	0.13		
51.15	0.14		
51.25	0.14		
51.35 51.45	0.15 0.15		
51.45 51.55	0.15		
51.65	0.15		
51.75	0.16		
51.85	0.16		
51.95	0.17		
52.05	0.17		
52.15	0.17		
52.25	0.18		



GRAVEL WETLAND DESIGN CRITERIA (Env-Wq 1508.05)

Type/Node Name: Gravel Wetland 3 (POND 1.2)

Enter the node name in the drainage analysis if applicable

A = Area draining to the practice	
A_I = Impervious area draining to the practice	
WQV= 1" x Rv x A	
WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
10% x WQV (check calc for sediment forebay and micropool volume))
45% x WQV (check calc for gravel wetland treatment bay volume)	
V_{SED} = sediment forebay volume	$\leftarrow \geq 10\% WQV$
V_{TB1} = volume of treatment bay 1	$\leftarrow \geq 45\% WQV$
V_{TB2} = volume of treatment bay 2	$\leftarrow \geq 45\% WQV$
E_{WQV} = elevation of WQV (attach stage-storage table)	
Q_{WQV} = discharge at the E_{WQV} (attach stage-discharge table)	← <2Q _{avg} ← ≥ 24-hrs
T_{ED} = drawdown time of extended detention = $2WQV/Q_{WQV}$	← ≥ 24-hrs
Pond side slopes	← ≥3:1
Elevation of SHWT	
Epp = Elevation of the permanent pool (elevation of lowest orifice) ²	$\leftarrow \geq E_{SHWT} - 2 \text{ ft}$
Length of the flow path between the inlet and outlet in each cell	$\leftarrow \geq 15 \text{ ft}$
What mechanism is proposed to prevent the outlet structure from clog	ging (applicable for
orifices/weirs with a dimension of ≤ 6 ")?	
Peak elevation of the 50-year storm event (E_{50})	
Berm elevation of the pond	_
$E_{50} \le$ the berm elevation?	← yes
n:	
	A _I = Impervious area draining to the practice I = percent impervious area draining to the practice, in decimal form Rv = Runoff coefficient = $0.05 + (0.9 \text{ x I})$ WQV= 1" x Rv x A WQV conversion (ac-in x 43,560 sf/ac x 1ft/12") 10% x WQV (check calc for sediment forebay and micropool volume) 45% x WQV (check calc for gravel wetland treatment bay volume) V _{SED} = sediment forebay volume V _{TB1} = volume of treatment bay 1 V _{TB2} = volume of treatment bay 2 E _{WQV} = elevation of WQV (attach stage-storage table) Q _{WQV} = discharge at the E _{WQV} (attach stage-discharge table) T _{ED} = drawdown time of extended detention = $2WQV/Q_{WQV}$ Pond side slopes Elevation of SHWT Epp = Elevation of the permanent pool (elevation of lowest orifice) ² Length of the flow path between the inlet and outlet in each cell What mechanism is proposed to prevent the outlet structure from clog orifices/weirs with a dimension of ≤ 6 ")? Peak elevation of the 50-year storm event (E ₅₀) Berm elevation of the pond

1. Volume stored above the wetland soil and below the high flow by-pass.

Designer's Notes:			

Last Revised: February 2018

^{2. 4&}quot; to 8" below the wetland soil. If lowest orifice is less than 2 feet below SHWT, and saturated hydraulic conductivity (Ksat) is greater than 0.005 in/hr, the system must be lined.

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Stage-Area-Storage for Pond POND 1.2: GRAVEL WETLAND 3

Elevation	Surface	Storago	Elevation	Surface	Storago
(feet)	(sq-ft)	Storage (cubic-feet)	(feet)	(sq-ft)	Storage (cubic-feet)
47.55	5,882	0	52.85	10,393	25,903
47.65	5,882	176	52.95	10,606	26,953
47.75	5,882	353	53.05	10,835	28,025
47.85	5,882	529	53.15	11,080	29,121
47.95	5,882	706	53.25	11,324	30,241
48.05	5,882	882	53.35	11,568	31,385
48.15	5,882	1,059	53.45	11,813	32,555
48.25	5,882	1,235	53.55	12,057	33,748
48.35	5,882	1,412	53.65	12,302	34,966
48.45	5,882	1,588	53.75	12,546	36,208
48.55	5,882	1,765	53.85	12,790	37,475
48.65	5,882	1,941	53.95	13,035	38,766
48.75	5,882	2,118	54.05	13,296	40,083
48.85	5,882	2,294	54.15	13,574	41,426
48.95	5,882	2,470	54.25	13,853	42,797
49.05	5,882	2,647	54.35	14,131	44,197
49.15	5,882	2,823	54.45	14,409	45,624
49.25	5,882	3,000	54.55	14,688	47,078
49.35	5,882	3,176	54.65	14,966	48,561
49.45	5,882	3,353	54.75	15,244	50,072
49.55	5,882	3,529	54.85	15,523	51,610
49.65	5,882	3,706	54.95	15,801	53,176
49.75	5,882	3,882	55.05	16,098	54,771
49.85	5,882	4,059	55.15	16,414	56,396
49.95	5,882	4,529	55.25	16,730	58,053
50.05	5,882	5,000	55.35	17,046	59,742
50.15	5,882	5,470	55.45	17,362	61,463
50.25	5,882	5,941	55.55 55.65	17,678	63,215
50.35	5,882	6,411	55.65	17,994	64,998
50.45	5,882	6,882	55.75	18,310	66,813
50.55	5,955 6 102	7,413	55.85	18,626	68,660 70 530
50.65 50.75	6,102 6,249	8,016 8,634	55.95	18,942	70,539
50.85	6,396	9,266			
50.95	6,543	9,913			
51.05	6,714	10,575			
51.15	6,911	11,256			
51.25	7,107	11,957			
51.35	7,303	12,678			
51.45	7,500	13,418			
51.55	7,696	14,178			
51.65	7,893	14,957			
51.75	8,089	15,756			
51.85	8,285	16,575			
51.95	8,482	17,413			
52.05	8,687	18,271			
52.15	8,900	19,151			
52.25	9,113	20,051			
52.35	9,327	20,973			
52.45	9,540	21,917			
52.55	9,753	22,881			
52.65	9,966	23,867			
52.75	10,180	24,875			
		•			

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Stage-Discharge for Pond POND 1.2: GRAVEL WETLAND 3

Elevation	Primary	Elevation	Primary	Elevation	Primary	Elevation	Primary
(feet)	(cfs)	(feet)	(cfs)	(feet)	(cfs)	(feet)	(cfs)
47.55	0.00	49.67	0.00	51.79	0.14	53.91	3.57
47.59	0.00	49.71	0.00	51.83	0.14	53.95	4.07
47.63	0.00	49.75	0.00	51.87	0.15	53.99	4.59
47.67	0.00	49.79	0.00	51.91	0.15	54.03	5.13
47.71	0.00	49.83	0.00	51.95	0.15	54.07	5.68
47.75	0.00	49.87	0.00	51.99	0.15	54.11	6.26
47.79	0.00	49.91	0.01	52.03	0.15	54.15	6.85
47.83	0.00	49.95	0.01	52.07	0.15	54.19	7.45
47.87	0.00	49.99	0.02	52.11	0.15	54.23	8.08
47.91	0.00	50.03	0.03	52.15	0.16	54.27	8.72
47.95	0.00	50.07	0.04	52.19	0.16	54.31	9.37
47.99	0.00	50.11	0.04	52.23	0.16	54.35	10.04
48.03	0.00	50.15	0.05	52.27	0.16	54.39	10.72
48.07	0.00	50.19	0.05	52.31	0.16	54.43	11.41
48.11	0.00	50.23	0.06	52.35	0.16	54.47	12.11
48.15	0.00	50.27	0.06	52.39	0.16	54.51	12.83
48.19	0.00	50.31	0.06	52.43	0.17	54.55	13.56
48.23	0.00	50.35	0.07	52.47	0.17	54.59	14.30
48.27	0.00	50.39	0.07	52.51	0.17	54.63	15.05
48.31	0.00	50.43	0.07	52.55	0.17	54.67	15.81
48.35	0.00	50.47	0.08	52.59	0.17	54.71	16.59
48.39	0.00	50.51	0.08	52.63	0.17	54.75	17.37
48.43	0.00	50.55	0.08	52.67	0.17	54.79	18.16
48.47	0.00	50.59	0.09	52.71	0.18	54.83	18.96
48.51	0.00	50.63	0.09	52.75	0.18	54.87	19.77
48.55	0.00	50.67	0.09	52.79	0.18	54.91	20.59
48.59	0.00	50.71	0.09	52.83	0.18	54.95	21.42
48.63	0.00	50.75	0.09	52.87	0.18	54.99	22.25
48.67	0.00	50.79	0.10	52.91	0.18	55.03	23.10
48.71	0.00	50.83	0.10	52.95	0.18	55.07	23.95
48.75	0.00	50.87	0.10	52.99	0.18	55.11	24.81
48.79	0.00	50.91	0.10	53.03	0.18	55.15	25.68
48.83	0.00	50.95	0.11	53.07	0.19	55.19	26.55
48.87	0.00	50.99	0.11	53.11	0.19	55.23	27.43
48.91	0.00	51.03	0.11	53.15	0.19	55.27	28.32
48.95	0.00	51.07	0.11	53.19	0.19	55.31	29.21
48.99	0.00	51.11	0.11	53.23	0.19	55.35	30.11
49.03	0.00	51.15	0.12	53.27	0.19	55.39	31.02
49.07	0.00	51.19	0.12	53.31	0.19	55.43	31.93
49.11	0.00	51.23	0.12	53.35	0.19	55.47	32.51
49.15	0.00	51.27	0.12	53.39	0.20	55.51	32.65
49.19	0.00	51.31	0.12	53.43	0.20	55.55	32.79
49.23	0.00	51.35	0.13	53.47	0.20	55.59	32.93
49.27	0.00	51.39	0.13	53.51	0.21	55.63	33.07
49.31	0.00	51.43	0.13	53.55	0.35	55.67	33.21
49.35	0.00	51.47	0.13	53.59	0.55	55.71	33.35
49.39	0.00	51.51	0.13	53.63	0.81	55.75	33.48
49.43	0.00	51.55	0.13	53.67	1.11	55.79	33.62
49.47	0.00	51.59	0.14	53.71	1.45	55.83	33.76
49.51	0.00	51.63	0.14	53.75	1.82	55.87	33.89
49.55	0.00	51.67	0.14	53.79	2.22	55.91	34.03
49.59	0.00	51.71	0.14	53.83	2.65	55.95	34.16
49.63	0.00	51.75	0.14	53.87	3.10	55.99	34.29



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name: Rain Garden 1.0 (POND 1.5)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable

Yes		Have you reviewed the restrictions on unlined systems outlined in Env-W	q 1508.07(a)?
4.97 a	.c	A = Area draining to the practice	
3.93 ac	c	A_{I} = Impervious area draining to the practice	
0.79 d	lecimal	I = percent impervious area draining to the practice, in decimal form	
0.76 u	nitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
3.79 ac		WQV=1" x Rv x A	
13,741 ct		WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
3,435 ct		25% x WQV (check calc for sediment forebay volume)	
10,306 ct	f	75% x WQV (check calc for surface sand filter volume)	
Deep su	ımps	Method of Pretreatment? (not required for clean or roof runoff)	
ct	f	V_{SED} = sediment forebay volume, if used for pretreatment	$\leftarrow \geq 25\% WQV$
8,830 st	f	A_{SA} = surface area of the practice	
0.30 ip	ph	$I_{DESIGN} = design infiltration rate1$	
Yes Y	es/No	If I_{DESIGN} is < 0.50 iph, has an underdrain been provided?	
62.2 h	ours	$T_{DRAIN} = drain time = V / (A_{SA} * I_{DESIGN})$	← <u>≤</u> 72-hrs
43.50 fe	eet	E_{FC} = elevation of the bottom of the filter course material ²	
42.42 fe	eet	E_{UD} = invert elevation of the underdrain (UD), if applicable	
39.00 fe	eet	$E_{SHWT} = elevation$ of SHWT (if none found, enter the lowest elevation	of the test pit)
36.50 fe	eet	E_{ROCK} = elevation of bedrock (if none found, enter the lowest elevation	of the test pit)
1.08 fe	eet	$D_{FC \text{ to UD}}$ = depth to UD from the bottom of the filter course	← ≥ 1'
7.00 fe	eet	$D_{FC \text{ to ROCK}}$ = depth to bedrock from the bottom of the filter course	← ≥ 1'
4.50 fe	eet	$D_{FC \text{ to SHWT}} = \text{depth to SHWT from the bottom of the filter course}$	<u>← ≥</u> 1'
49.71 ft	t	Peak elevation of the 50-year storm event (infiltration can be used in a	nalysis)
50.00 ft	t	Elevation of the top of the practice	
YES		50 peak elevation \leq Elevation of the top of the practice	← yes

If a surface sand filter or underground sand filter is proposed:

	YES	ac	Drainage Area check.	← < 10 ac
		cf	V = volume of storage ³ (attach a stage-storage table)	← \geq 75%WQV
		inches	D_{FC} = filter course thickness	← 18", or 24" if within GPA
ľ	Sheet		Note what sheet in the plan set contains the filter course specification	
		Yes/No	Access grate provided?	← yes

If a bioretention area is proposed:

	1 1	
YES ac	Drainage Area no larger than 5 ac?	← yes
34,000 cf	V = volume of storage ³ (attach a stage-storage table)	$\leftarrow \geq WQV$
inches	D_{FC} = filter course thickness	← 18", or 24" if within GPA
Sheet	Note what sheet in the plan set contains the filter course specification	
3.0 :1	Pond side slopes	← <u>>3</u> :1
Sheet C-508	Note what sheet in the plan set contains the planting plans and surface	cover

If porous pavement is proposed:

		Type of pavement proposed (concrete? Asphalt? Pavers? Etc)	
	acres	A_{SA} = surface area of the pervious pavement	
1.0	:1	ratio of the contributing area to the pervious surface area	← 5:1
	inches	D_{FC} = filter course thickness	← 12", or 18" if within GPA
Shee	et et	Note what sheet in the plan set contains the filter course spec.	← 304.1 sand

- 1. Rate of the limiting layer (either the filter course or the underlying soil). See Env-Wq 1504.14 for guidance on determining the infiltration rate.
- 2. See lines 34, 40 and 48 for required depths of filter media.
- 3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:			
<u> </u>			
<u> </u>	·	·	

NHDES Alteration of Terrain

Last Revised: December 2017



Groundwater Recharge Volume (GRV) Calculation

Г	-	ac	Area of HSG A soil that was replaced by impervious cover	0.40"
	0.18	ac	Area of HSG B soil that was replaced by impervious cover	0.25"
	9.52	ac	Area of HSG C soil that was replaced by impervious cover	0.10"
	1.01	ac	Area of HSG D soil or impervious cover that was replaced by impervious cover	0.0"
	0.09	inches	Rd = weighted groundwater recharge depth	
	0.997	ac-in	GRV = AI * Rd	
	3,619	cf	GRV conversion (ac-in x 43,560 sf/ac x 1ft/12")	

Provide calculations below showing that the project meets the groundwater recharge requirements (Env-Wq 1507.04):

Rain Garden #1:
Area of Practice $= 8,830 \text{ sf}$
Depth of Stone Below U.D. = 13"
Voids = 40%
GRV = 8,830 sf x 40% = 3,826 cf

PROPOSED INDUSTRIAL DEVELOPMENT

70 & 80 CORPORATE DRIVE PORTSMOUTH, NEW HAMPSHIRE PROJECT NO: L-0700-13

MAY 21, 2018

COVER SHEET	05/21/2018	
EXISTING CONDITIONS PLAN	08/03/2016	
DEMOLITION PLAN	05/21/2018	
DEMOLITION PLAN	05/21/2018	
DEMOLITION PLAN	05/21/2018	Broom
OVERALL SITE PLAN	05/21/2018	
SITE PLAN	05/21/2018	Ricker
SITE PLAN	05/21/2018	
SITE PLAN	05/21/2018	
GRADING, DRAINAGE & EROSION CONTROL PLAN	05/21/2018	
GRADING, DRAINAGE & EROSION CONTROL PLAN	05/21/2018	
GRADING, DRAINAGE & EROSION CONTROL PLAN	05/21/2018	
UTILITIES PLAN	05/21/2018	
UTILITIES PLAN	05/21/2018	
UTILITIES PLAN	05/21/2018	100
LANDSCAPE PLAN	05/21/2018	
LANDSCAPE PLAN	05/21/2018	
LANDSCAPE PLAN	05/21/2018	
PHOTOMETRIC LIGHTING PLAN	05/21/2018	
PHOTOMETRIC LIGHTING PLAN	05/21/2018	
·		

LAST REVISED

05/21/2018

05/21/2018

05/21/2018

05/21/2018

05/21/2018

05/21/2018

05/21/2018

05/21/2018

05/21/2018

05/21/2018

05/21/2018

05/21/2018

LIST OF DRAWINGS

SHEET TITLE

SHEET NO.

1 of 4

2 of 4

3 of 4

C-101

C-103

C-104

C-106

C-107

C-108

C-109

C-110

C-111

C-112

C-113

C-114

C-115

C-116

C-117

C-118

C-119

C-501

C-502

C-503

C-504

C-505

C-506

C-507

C-508

C-701

C-702

PHOTOMETRIC LIGHTING PLAN

DETAILS SHEET

DETAILS SHEET

DETAILS SHEET

DETAILS SHEET

DETAILS SHEET

DETAILS SHEET

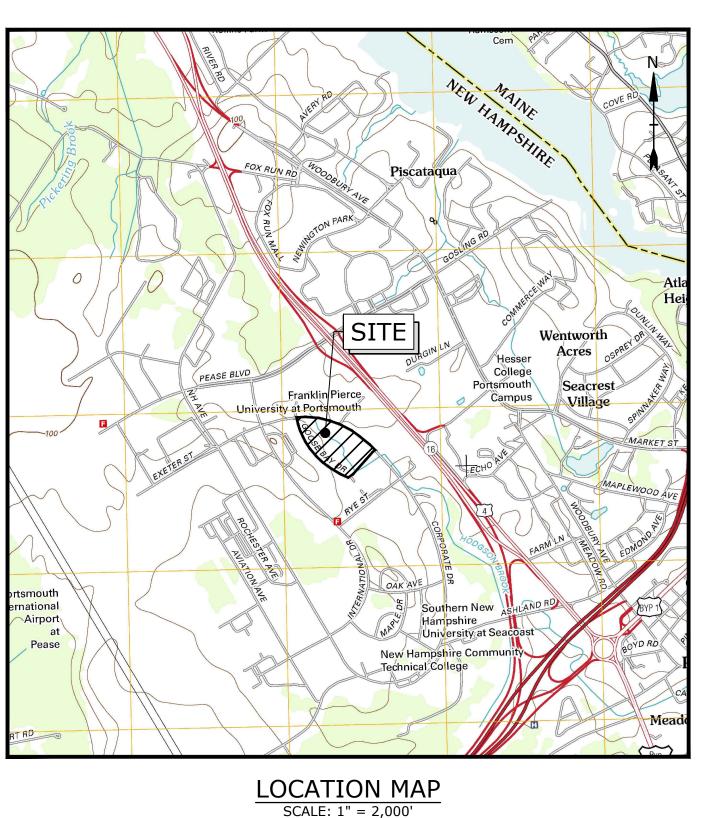
DETAILS SHEET

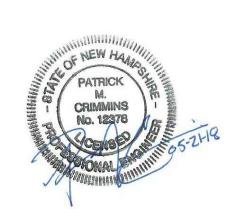
EROSION CONTROL NOTES & DETAILS SHEET

HODGSON BROOK WETLAND PLANTING PLAN

HODGSON BROOK DETAILS SHEET

HODGSON BROOK GRADING, DRAINAGE & EROSION CONTROL PLAN







OWNER: PEASE DEVELOPMENT AUTHORITY

55 INTERNATIONAL DRIVE

PORTSMOUTH, NEW HAMPSHIRE 03801

CLIENT: LONZA BIOLOGICS

101 INTERNATIONAL DRIVE PORTSMOUTH, NH 03801

CIVIL ENGINEER: Tighe&Bond
Engineers | Environmental Specialists

Engineers | Environmental Specialists

177 CORPORATE DRIVE

PORTSMOUTH, NEW HAMPSHIRE 03801

SURVEYOR: DOUCET SURVEY, INC.

102 KENT PLACE

NEWMARKET, NEW HAMPSHIRE 03857

WETLAND SCIENTIST: GOVE ENVIRONMENTAL SERVICES, INC.

8 CONTINENTAL DRIVE, UNIT H EXETER, NEW HAMPSHIRE 03833

STREAM DESIGN STRI
CONSULTANT: MADB

STREAMWORKS, PLLC
MADBURY, NEW HAMPSHIRE 03823

COMPLETE SET 35 SHEETS

DRAINAGE STRUCTURE TABLE			
CB #1013	CBR #1324	CB #1461	CB #1732
RIM ELEV.=68.4'	RIM ELEV.=55.7'	" RIM ELEV.=57.9'	RIM ELEV.=39.1'
(1019) 18" HDPE INV.=64.4'	(A) 12" RCP INV.=52.3'	(1460) 12" RCP INV.=53.2"	(1695) 10" RCP INV.=37.3'
(A) 18" HDPE INV.=64.4'	(1325) 12" RCP INV.=51.9'	,	
(1,7) 10 11.12 11.11 0 11.1	(1305) 15" RCP INV.=51.9'	CB #1478	CBR #1733
CB #1019	(B) 22" RCP INV.=51.7'	RIM ELEV.=54.2'	RIM ELEV.=39.1
RIM ELEV.=68.5'	(6) 22 113, 1111, 511,	(1515) 12" RCP INV.=47.2'	STRUCTURE DAMAGED
(A) 18" HDPE INV.=65.1'	CB #1325	(10.0) 12 1111 1111 1111	• · · · · · · · · · · · · · · · · · · ·
• •		CB #1484	DMH #1755
(1013) 18" HDPE INV.=64.7'	RIM ELEV.=55.7'	RIM ELEV.=49.0'	RIM ELEV.=42'
OD #4000	(1399) 15" RCP INV.=51.9'	BROKEN GRATE - NOT OPENED	(A) 24" RCP INV.=37.2'
CB #1088	(1324) 12" RCP INV.=51.8'	BROKEN GRATE - NOT OFENED	(B) 24" RCP INV.=37.1'
RIM ELEV.=66.6'	0.00.4.44.7.7.0	OD #3504	(B) 24 RCF INV.—37.1
(A) 6" HDPE INV.=62.0'	DMH #1338	CB #1504	OD #1756
(1111) 12" RCP INV.=61.6'	RIM ELEV.=57.7'	RIM ELEV.=48.9'	CB #1756
(1095) 12" RCP INV.=61.6"	(SUMP)=49.9' (LARGE VAULT)	(A) 12" RCP INV.=42.7'	RIM ELEV.=42.5'
		(1484) 12" RCP INV.=42.6'	(1769) 12" RCP INV.=39.2'
DMH #1095	CB #1345		05 #4700
RIM ELEV.=65.2'	RIM ELEV.=58.1'	CB #1515	CB #1769
(1088) 12" RCP INV.=60.0'	(1420) 12" RCP INV.=53.9"	RIM ELEV.=54.1'	RIM ELEV.=42.5'
(1137) 12" RCP INV.=59.7'		BROKEN GRATE - NOT OPENED	(1756) 12" RCP INV.=38.1'
	CB #1381		(A) 12" RCP INV.=33.5'
CB #1111	RIM ELEV.=57.2'	CB #1542	
RIM ELEV.=66.8'	(1212) 15" RCP INV.=54.3'	RIM ELEV.=44.4'	CB #1935
(1088) 12" RCP INV.=61.9'	(1311) 15" RCP INV.=54.4"	(1651) 12" RCP INV.=41.0"	RIM ELEV.=49.7'
			NOT OPENED - SILT SOCK
CB #1137	CB #1399	CB #1570	
RIM ELEV.=60.7'	RIM ELEV.=55.5	RIM ELEV.=40.7'	CB #2031
(1095) 12" RCP INV.=57.3'	(1325) 15" RCP INV.=52.3"	(A) 18" RCP INV.=36.2'	RIM ELEV.=59.0'
(1285) 15" RCP INV.=56.8'		(B) 18" RCP INV.=36.2'	NOT OPENED - SILT SOCK
(1141) 15" RCP INV.=56.8'	DMH #1401		
	RIM ELEV.=58.3'	CB #1572	DMH #2142
DMH #1141	NOT OPENED - OFF SITE	RIM ELEV.=42.2'	RIM ELEV.=62.8'
RIM ELEV.=61.1'		(1611) 12" RCP INV.=38.2'	(A) 24" HDPE INV.=58.2'
(1300) 12" RCP INV.=57.2'	DMH #1408		(B) 24" HDPE INV.=56.8'
(1137) 15" RCP INV.=56.9"	RIM ELEV.=56.8'	CB #1580	
(1147) 15" RCP INV.=56.6"	NOT OPENED OFF SITE	RIM ELEV.=41.7'	CB #2152
(A) 15" RCP INV.=56.4'		(1586) 15" RCP INV.=36.8'	RIM ELEV.=64.3'
(B) 18" ASB INV.=56.3'	CB #1420	, ,	NOT OPENED - SILT SOCK
(6) 16 7.65 1111 00.15	RIM ELEV.=58.1'	CB #1586	
CB #1147	(1345) 12" RCP INV.=54.4'	RIM ELEV.=41.9'	DMH #2153
RIM ELEV.=61.5'	(1421) 12" HDPE INV.=54.1'	(1580) 15" RCP INV.=36.4'	RIM ELEV.=64.5
(A) 15" RCP INV.=57.2'	(1121) 12 11512 11111 3111	(A) 15" RCP INV.=36.6'	(SUMP) INV.=53.9'
	DMH #1421	(7) 10 1101 1111 0010	FULL OF WATER
(1141) 15" RCP INV.=57.1"	•	CB #1611	TOLE OF WITHER
CB #1183	RIM ELEV.=57.4' (1420) 12" RCP INV.=54.3'	RIM ELEV.=42.4'	CB #2170
	,	(1572) 12" RCP INV.=37.8'	RIM ELEV.=65.7'
RIM ELEV.=60.1'	SUMP=53.4' (FULL OF SILT)	(A) 12" RCP INV.=37.5'	NOT OPENED - SILT SOCK
(1212) 15" RCP INV.=55.7'	DML #4470	(A) 12 ROF 114V.—37.3	NOT OF INED - SILT SOCK
CD #1010	DMH #1438	CB #1651	CB #2246
CB #1212	RIM ELEV.=50.2'	*	RIM ELEV.=65.5'
RIM ELEV.=57.5'	(A) 12" RCP INV.=44.6'	RIM ELEV.=44.6' (1542) 12" RCP INV.=39.5'	NOT OPENED - SILT SOCK
(1183) 15" RCP INV.=54.8"	(1439) 12" RCP INV.=44.6'	•	NOT OF EINED - SIET SOOK
(1381) 15" RCP INV.=54.6'	(B) UNK. CMP INV.=42.9'	(A) 12" RCP INV.=39.5"	CBR #2327
	(C) UNK. CMP INV.=42.9'	00 #4679	"
CB #1285		CB #1678	RIM ELEV.=40.2'
RIM ELEV.=60.7'	CBR #1439	RIM ELEV.=39.2'	(A) 12" RCP INV.=38.3'
(1137) 15" RCP INV.=57.0'	RIM ELEV.=47.4'	(TOP OF WATER) INV.=36.5	
	(1438) 12" RCP INV.=45.2'	(A) 12" RCP INV.=35.4'	CBR #2329
CBR #1305			RIM ELEV.=47.4'
RIM ELEV.=56.7'	CBR #1444	CB #1685	(A) 12" RCP INV.=42.0'
(1311) 12" RCP INV.=52.8'	RIM ELEV.=48.3'	RIM ELEV.=39.2'	SILT=41.9'
(A) 15" RCP INV.=52.7'	12" HDPE INV.=46.4'	(TOP OF WATER) INV.=36.6'	
(1324) 15" RCP INV.=52.7'	(SUMP) INV.=42.8'	(2330) 12" RCP INV.=36.4'	DMH #2330
			RIM ELEV.=40.4'
CB #1311	CB #1456	DMH #1695	(1685) 12" RCP INV.=36.5'
RIM ELEV.=57.1'	RIM ELEV.=58.1'	RIM ELEV.=42.8'	(A) 12" RCP INV.=36.3'
(1381) 15" RCP INV.=53.4'	(1460) 12" RCP INV.=52.5"	(1732) 10" RCP INV.=36.4"	(B) 15" RCP INV.=36.1'
(1305) 12" RCP INV.=53.0'		(A) 48" RCP INV.=35.9'	
	DMH #1460	(B) NOT MEASURED	DMH #2336
	RIM ELEV.=58'	(RECESSED — LARGE VAULT)	RIM ELEV.=39.7'
	(1461) 12" RCP INV.=51.6'	· ·	(A) 18" RCP INV.=36.1'
	(1456) 12" RCP INV.=51.5"		(B) 24" RCP INV.=35.4'

SEWER STRUCTURE TABLE	
SMH #1062	SMH #1551
RIM ELEV.=69.8'	RIM ELEV.=43.6'
(A) 6" CLAY INV.=63.9'	(A) 8" PVC INV.=35.6'
(B) 6" CLAY INV.=63.7'	(B) 12" UNK. INV.=34.2'
(1067) 8" CLAY INV.=62.6'	(C) 12" UNK. INV.=34.1'
SMH #1067	SMH #1691
RIM ELEV.=68.6'	RIM ELEV.=39.9'
(1062) 8" CLAY INV.=60.4"	(1784) UNK. INV.=34.2'
(2242) 8" UNK. INV.=60.3"	(1722) UNK. INV.=34.1'
SMH #1078	SMH #1722
RIM ELEV.=69.0'	RIM ELEV.=41.1'
COULD NOT OPEN	(A) 6" CLAY INV.=33.2"
SMH #1123	(1691) UNK. CLAY INV.=33.
RIM ELEV.=64'	SMH #1784
(1295) 8" PVC INV.=55.8'	RIM ELEV.=41.1'
	(1921) 10" UNK. INV.=35.4
SMH #1169	(1691) 10" UNK. INV.=35.5
RIM ELEV.=65.2'	
(1184) 15" STEEL INV.=53.8'	SMH #1921
(A) 15" STEEL INV.=53.8'	RIM ELEV.=44.8'
ONALL MARCA	(1953) UNK. INV.=37'
SMH #1184	(1784) UNK. INV.=36.9'
RIM ELEV.=60.4' (1206) 8" CLAY INV -54.2'	SMH #1953
(1296) 8" CLAY INV.=54.2' (1217) 15" STEEL INV.=52.7'	RIM ELEV.=50.1'
(1169) 15" STEEL INV.=52.7'	(A) 6" CLAY INV.=42.4'
THOUSE OF THE HANGES	(2080) UNK. INV.=42.2'
SMH #1217	(1921) UNK. INV.=42.2'
RIM ELEV.=57.9'	, , ,
(1184) 15" STEEL INV.=52.3'	SMH #2080
(1400) 15" STEEL INV.=52.2'	RIM ELEV.=57.9'
	(A) 8" UNK. INV.=50.1"
SMH #1296	2187) 8" UNK. INV.=50.1"
RIM ELEV.=63.7'	(1953) 8" UNK. INV.=49.9'
(1123) 8" PVC INV.=55.5'	
(2326) 8" UNK. INV.=55.0'	SMH #2187
(1184) 8" UNK. INV.=55.0"	RIM ELEV.=63'
	(A) 6" PVC INV.=54.9'
SMH #1400	(2242) 8" PVC INV.=54.9"
RIM ELEV.=55.6'	(2080) 8" PVC INV,=54.9'
(1217) 15" ASB INV.=49.3'	
(1415) 15" ASB INV.=49.3'	SMH #2242
	RIM ELEV.=65.0'
SMH #1415	(1067) 8" CLAY INV.=56.8"
RIM ELEV.=57.9'	(2187) 8" CLAY INV.=57.0"
(A) 12" PVC INV.=48.3'	
(1400) 18" UNK. INV.=47.9'	SMH #2326
(1450) 18" PVC INV.=48.0'	RIM ELEV.=68.1'
	(1078) 8" PVC INV.=62.2'
SMH #1450	(1296) 8" ASB INV.=62.1'
•	
RIM ELEV.=60.5	01//1 //0===
•	SMH #2328 RIM ELEV.=43.1'

(1001) 12 UNK 1144.=32. (A) 18" UNK INV.=32.3' SMH #1459 RIM ELEV.=58.8' (A) 8" PVC INV.=48.4' (1450) 18" PVC INV.=47.1' (B) 18" PVC INV.=47.1'



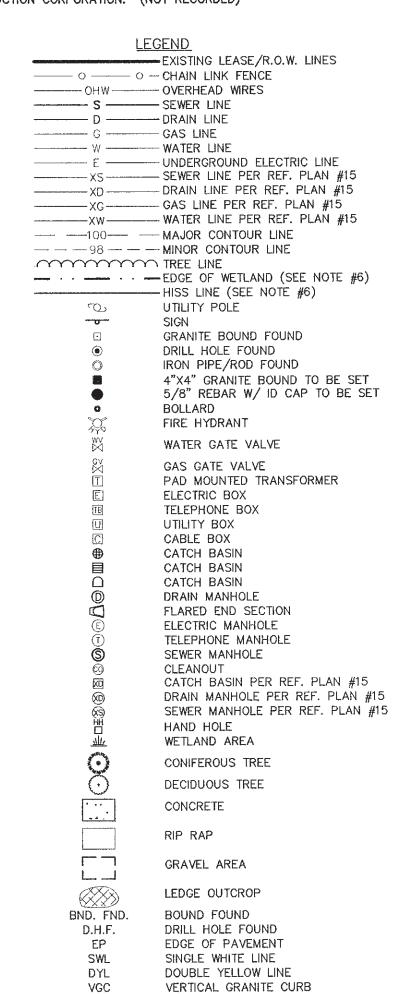
- 1. "R.O.W. WORKSHEET, CORPORATE DRIVE PREPARED FOR PEASE DEVELOPMENT AUTHORITY" DATED DEC. 21, 1992 BY RICHARD D. BARTLETT & ASSOCIATES, INC. SHEETS 1 AND 2.
- 2. "PEASE A.F.B. / PORTSMOUTH, N.H. REPAVE BASE STREETS, PORTSMOUTH AVE, ROCKINGHAM AVE." DATED 7 DEC 82 BY STRATETIC AIR COMMAND CIVIL ENGINEERING. SHEET 4 OF 5
- 3. "PORTSMOUTH AIR FORCE BASE, PORTSMOUTH, N.H. ROADS AND STORAGE AREA FY-56" DATED

DEC 1955 BY WHITMAN & HOWARD ENGINEERS. INDEX PAGE AND SHEETS 2 - 5 OF 11.

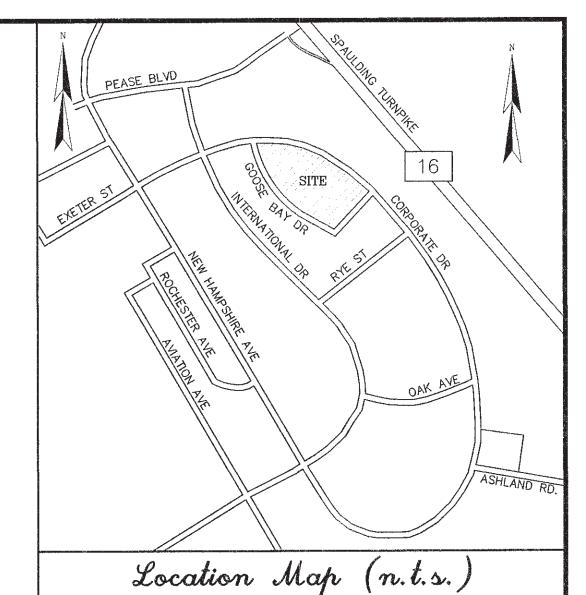
- 4. "PEASE INTERNATIONAL TRADEPORT SUBDIVISION PLAT, INTERNATIONAL DRIVE LOTS BC11-001 & BC11-002, PORTSMOUTH, N.H." DATED FEBRUARY 5, 1993 BY RICHARD D. BARTLETT & ASSOCIATES INC. R.C.R.D. PLAN #D22536.
- 5. "SUBDIVISION PLAN OF LAND FOR REDHOOK ALE BREWERY, INC. CORPORATE DRIVE, COUNTY OF ROCKINGHAM, PORTSMOUTH, N.H." DATED DECEMBER 10, 1994 BY RICHARD P. MILLETTE AND ASSOCIATES. R.C.R.D. PLAN #D-23978.
- 6. "ALTA/ACSM LAND TITLE SURVEY FOR RESPORT, LLC, ONE INTERNATIONAL DRIVE, COUNTY OF ROCKINGHAM, PORTSMOUTH, N.H." DATED FEBRUARY 27, 1998 BY MILLETTE, SPRAGUE &

COLWELL, INC. R.C.R.D. PLAN #D-26125.

- 7. "FRANKLIN PIERCE COLLEGE, PEASE INTERNATIONAL TRADEPORT, 73 CORPORATE DRIVE, PORTSMOUTH, NH" DATED JANUARY 15, 1998 BY RONALD R. BURD. R.C.R.D. PLAN #D-26427.
- 8. "SUBDIVISION PLAN FOR LAND LEASED BY PEASE DEVELOPMENT AUTHORITY & KNOWN AS #119 INTERNATIONAL DRIVE LOCATED AT PEASE INTERNATIONAL TRADEPORT, PORTSMOUTH, N.H." DATED MARCH 1, 2000 BY KNIGHT HILL LAND SURVEYING SERVICES, INC. R.C.R.D. PLAN
- 9. "SUBDIVISION PLAT PREPARED FOR 80 CORPORATE DRIVE LLC C/O BOULOS PROPERTY MANAGEMENT, LOCATION CORPORATE & GOOSE BAY DRIVES, PEASE INTERNATIONAL TRADEPORT -PORTSMOUTH, NH" DATED APRIL 11, 2000 BY FWS LAND SURVEYING P.L.L.C. R.C.R.D. PLAN #D-28447.
- 10. "LEASE LINE REVISION PLAN FOR LONZA BIOLOGICS, INC. 101 INTERNATIONAL DRIVE, PORTSMOUTH, NEW HAMPSHIRE" DATED FEB. 5, 2001 BY DOUCET SURVEY, INC. R.C.R.D. PLAN #D-28955.
- 11. "LEASE LINE REVISION PLAN FOR LONZA BIOLOGICS, INC. 101 INTERNATIONAL DRIVE, PORTSMOUTH, NEW HAMPSHIRE" DATED SEPT. 17, 2001 BY DOUCET SURVEY, INC. R.C.R.D. PLAN #D-29538.
- 12. "SUBDIVISION PLAN OF LAND OF PEASE DEVELOPMENT AUTHORITY TO BE LEASED TO NORTHEAST 1. REFERENCE: REHABILITATION (A PORTION OF TAX MAP 303, LOT 6) 105 & 121 CORPORATE DRIVE, PEASE TRADEPORT, PORTSMOUTH, NEW HAMPSHIRE" DATED NOV. 5, 2008 BY DOUCET SURVEY, INC. R.C.R.D. PLAN #D-35869.
- 13. "CONDOMINIUM SITE & FLOOR PLAN PREPARED FOR PIONEER NEW HAMPSHIRE, LLC, LAND OF PEASE DEVELOPMENT AUTHORITY, TAX MAP PARCEL 305-3 (108, 110, 112 & 114 CORPORATE DRIVE) PORTSMOUTH, NEW HAMPSHIRE" DATED APRIL 12, 2013 BY FIELDSTONE LAND CONSULTANTS, PLLC. SHEET 1 OF 5. R.C.R.D. PLAN #D-37765.
- 14. "SUBDIVISION PLAN FOR PEASE DEVELOPMENT AUTHORITY, (TAX MAP 303, LOT 4) 67 CORPORATE DRIVE, PEASE TRADEPORT, PORTSMOUTH NEW HAMPSHIRE" DATED MAY 29, 2009 BY DOUCET SURVEY, INC. (NOT RECORDED)
- 15. "EXISTING CONDITIONS, BUILDING A, 80 CORPORATE DRIVE AND BUILDING B, 70 CORPORATE DRIVE, PORTSMOUTH, NH" DATED 4/14/2000 AND REVISED 6/05/2000 BY OPECHEE CONSTRUCTION CORPORATION. (NOT RECORDED)



HISS SOIL TYPE



TAX MAP 305, LOT 1 PHYSICAL ADDRESS: 70 CORPORATE DRIVE TAX MAP 305, LOT 2 PHYSICAL ADDRESS: 80 CORPORATE DRIVE

2. TOTAL PARCEL AREA: TAX MAP 305, LOT 1: 443,578 SQ. FT. OR 10.183 AC. TAX MAP 305, LOT 2: 604,273 SQ. FT. OR 13.872 AC. TOTAL AREA: 1,047,851 SQ. FT. OR 24.055 AC.

OWNER OF RECORD:

TAX MAP 305, LOTS 1 & 2 PEASE DEVELOPMENT AUTHORITY 55 INTERNATIONAL DRIVE PORTSMOUTH, NEW HAMPSHIRE 03801 R.C.R.D. BOOK 4227, PAGE 001

- 4. ZONE: AIRPORT, BUSINESS & COMMERCIAL (ABC)
- 5. FIELD SURVEY PERFORMED BY J.M.L, E.J.S., J.P.E., J.F.K., AND N.J.M. DURING NOVEMBER 2015 USING A TRIMBLE RS SURVEY GRADE GPS UNIT AND A TRIMBLE S6 ROBOTIC TOTAL STATION WITH A TRIMBLE TSC3
- 6. JURISDICTIONAL WETLANDS DELINEATED BY GOVE ENVIRONMENTAL SERVICES, INC. DURING FALL 2014 IN ACCORDANCE WITH 1987 CORPS OF ENGINEERS WETLANDS DELINEATIONS MANUAL, TECHNICAL REPORT Y-87-1. HISS MAPPING COMPLETED BY GOVE ENVIRONMENTAL SERVICES DURING DECEMBER 2015.
- 7. FLOOD HAZARD ZONE: "X", PER FIRM MAP #33015C0260E, DATED MAY 17, 2005.
- 8. HORIZONTAL DATUM BASED ON NH STATE PLANE 2800(NAD83/86) PER REFERENCE PLANS #10, #11, & #12.
- 9. VERTICAL DATUM IS BASED ON NGVD29 PER REFERENCE PLANS #10, #11, & #12.

MAINTAINING A DRAINAGE LINE. (SHOWN PER REFERENCE PLAN #9)

- 10. PROPER FIELD PROCEDURES WERE FOLLOWED IN ORDER TO GENERATE CONTOURS AT 2' INTERVALS. ANY MODIFICATION OF THIS INTERVAL WILL DIMINISH THE INTEGRITY OF THE DATA, AND DOUCET SURVEY, INC. WILL NOT BE RESPONSIBLE FOR ANY SUCH ALTERATION PERFORMED BY THE USER.
- 11. UNDERGROUND UTILITIES SHOWN HEREON ARE BASED ON OBSERVABLE PHYSICAL EVIDENCE AND PAINT MARKS FOUND ON-SITE. THE SITE WAS NOT MARKED FOR THE PURPOSES OF THIS SURVEY. SOME UTILITIES ARE SHOWN PER REFERENCE PLANS AS NOTED IN THE LEGEND.
- 12. THE ACCURACY OF MEASURED UTILITY INVERTS AND PIPE SIZES/TYPES IS SUBJECT TO NUMEROUS FIELD CONDITIONS, INCLUDING; THE ABILITY TO MAKE VISUAL OBSERVATIONS, DIRECT ACCESS TO THE VARIOUS ELEMENTS, MANHOLE CONFIGURATION, ETC.
- 13. THE INTENT OF THIS PLAN IS TO SHOW THE LOCATION OF BOUNDARIES IN ACCORDANCE WITH AND IN RELATION TO THE CURRENT LEGAL DESCRIPTION, AND IS NOT AN ATTEMPT TO DEFINE UNWRITTEN RIGHTS, DETERMINE THE EXTENT OF OWNERSHIP, OR DEFINE THE LIMITS OF TITLE.
- 14. TAX MAP 305, LOTS 1 & 2 ARE EITHER SUBJECT TO OR IN BENEFIT OF, BUT NOT LIMITED TO, THE FOLLOWING EASEMENTS/RIGHTS OF RECORD: 14.A. 50' WIDE ACCESS EASEMENT FOR THE BENEFIT OF LOT 305-2. (SHOWN PER REFERENCE PLAN #9) 14.B. APPROXIMATE LOCATION OF 20' WIDE LICENSE TO THE CITY OF PORTSMOUTH FOR THE PURPOSES OF
- 15. FINAL MONUMENTATION MAY BE DIFFERENT THAN THE PROPOSED MONUMENTATION SHOWN HEREON, DUE TO THE FACT THAT SITE CONDITIONS WILL DICTATE THE ACTUAL LOCATION AND TYPE OF MONUMENTS INSTALLED IN THE FIELD. PLEASE REFER TO EITHER THE "MONUMENTATION LOCATION PLAN" TO BE RECORDED OR CONTACT DOUCET SURVEY, INC. FOR CLARIFICATION OF MONUMENTS SET. (A RECORDED PLAN WILL BE PRODUCED AT THE DISCRETION OF DOUCET SURVEY, INC.).



EXISTING CONDITIONS PLAN FOR

TIGHE & BOND AND LONZA LAND OF PEASE DEVELOPMENT AUTHORITY

(TAX MAP 305, LOTS 1 & 2) GOOSE BAY DRIVE & CORPORATE DRIVE

PORTSMOUTH, NEW HAMPSHIRE

DRAWN BY: 4375A J. A. G. CHECKED BY



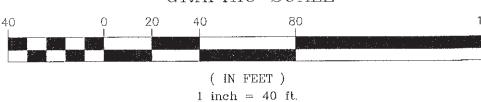
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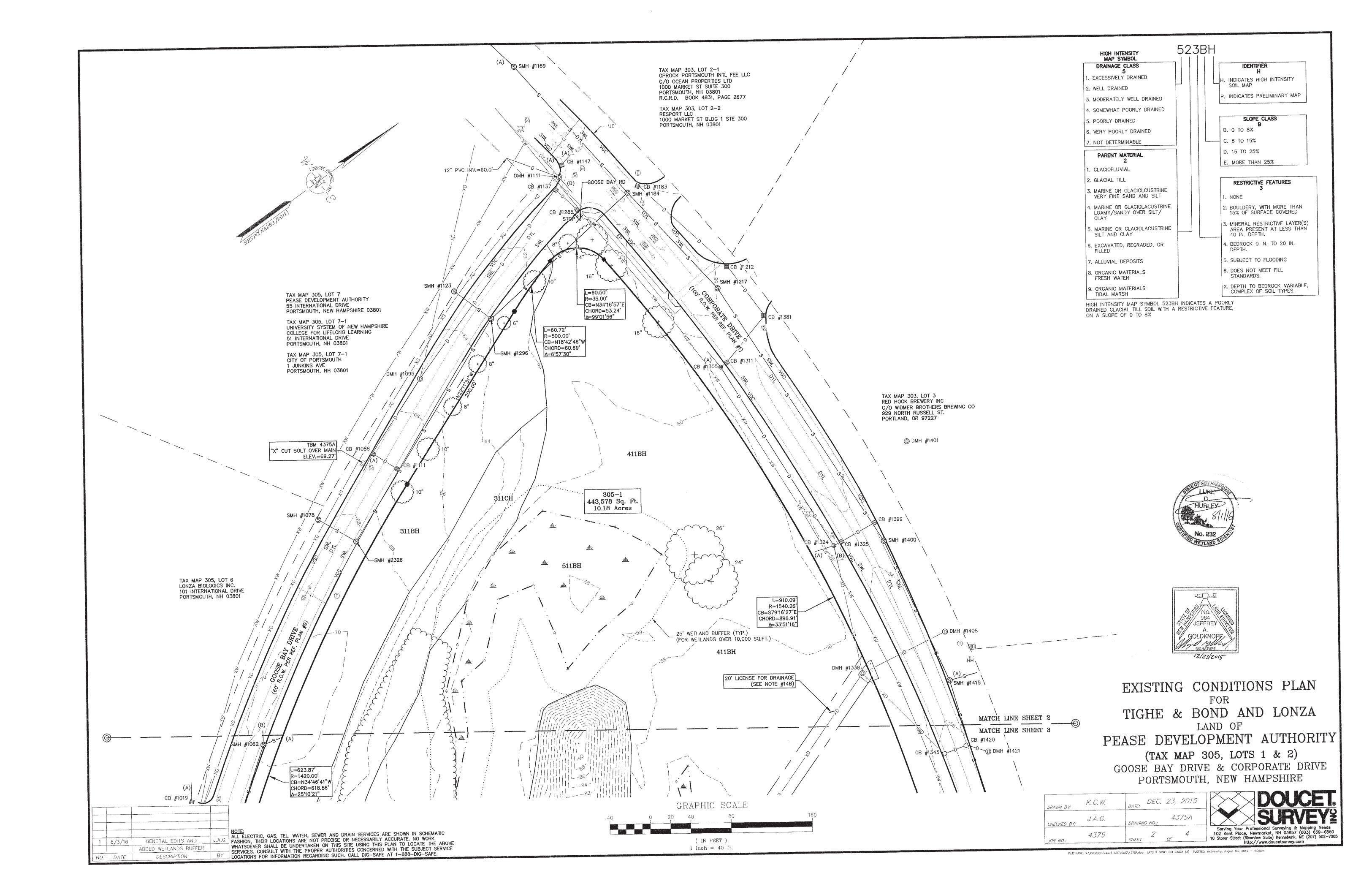
ALL ELECTRIC, GAS, TEL. WATER, SEWER AND DRAIN SERVICES ARE SHOWN IN SCHEMATIC FASHION, THEIR LOCATIONS ARE NOT PRECISE OR NECESSARILY ACCURATE. NO WORK WHATSOEVER SHALL BE UNDERTAKEN ON THIS SITE USING THIS PLAN TO LOCATE THE ABOVE SERVICES. CONSULT WITH THE PROPER AUTHORITIES CONCERNED WITH THE SUBJECT SERVICE LOCATIONS FOR INFORMATION REGARDING SUCH. CALL DIG-SAFE AT 1-888-DIG-SAFE.

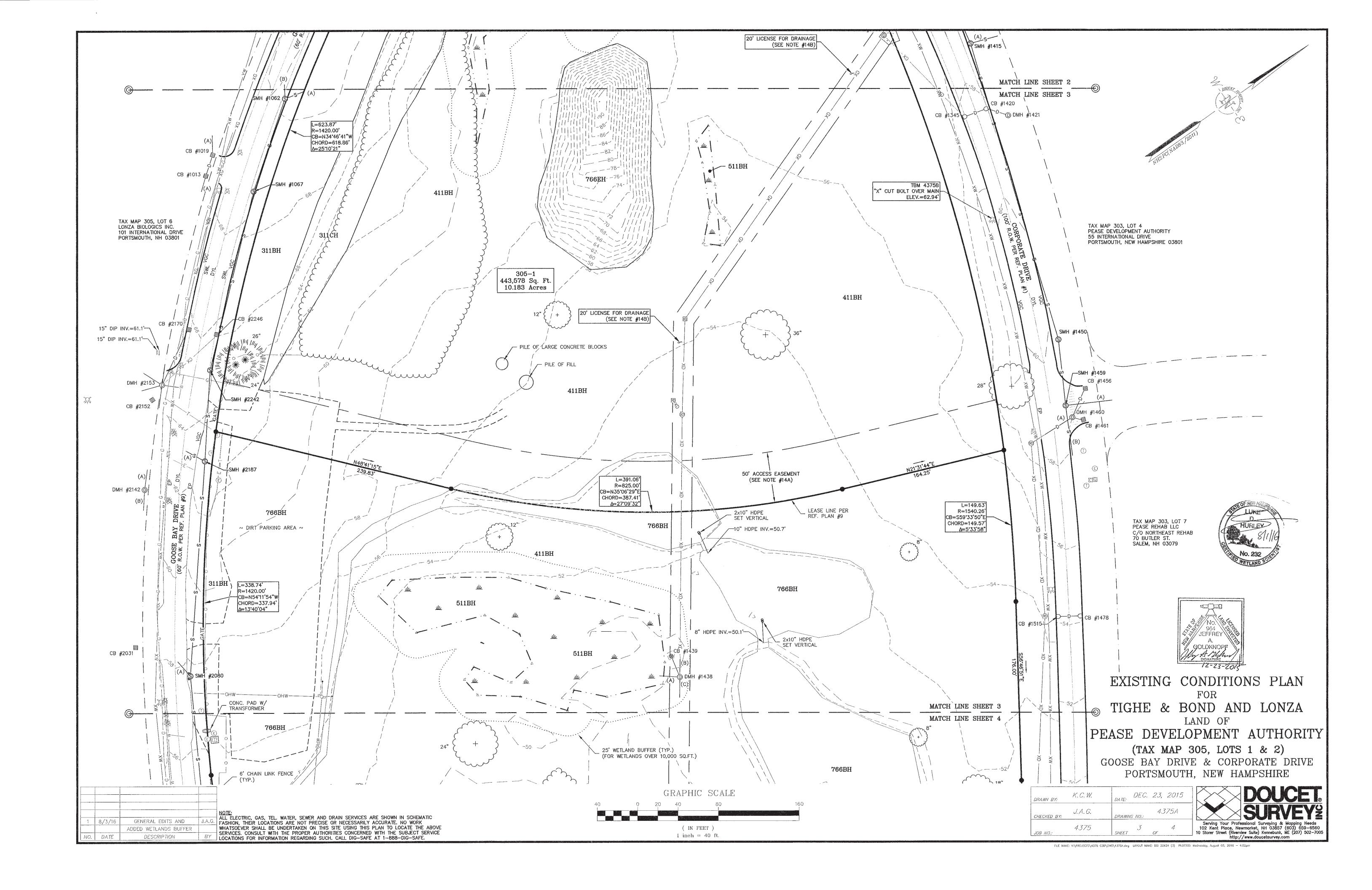
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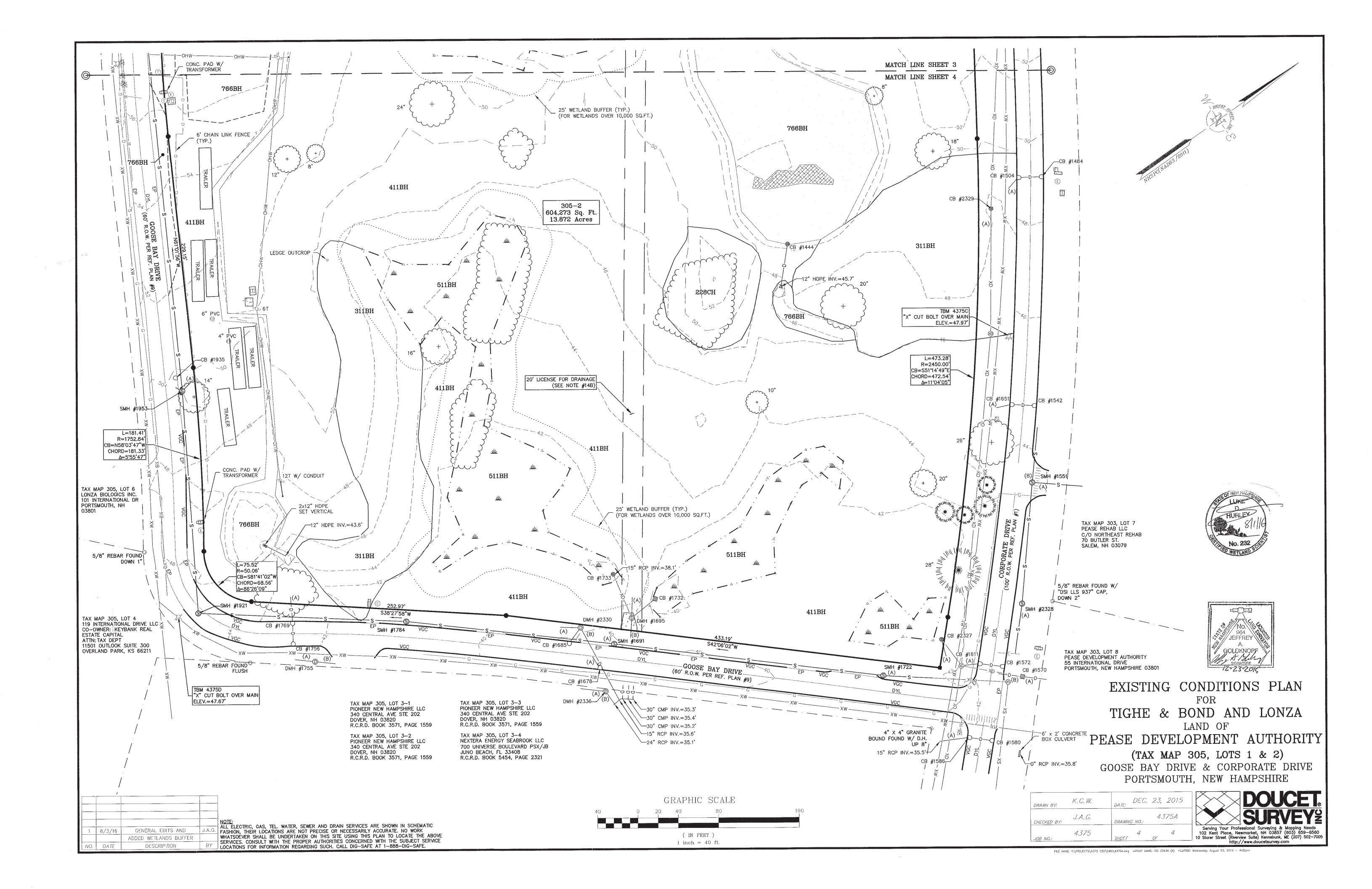
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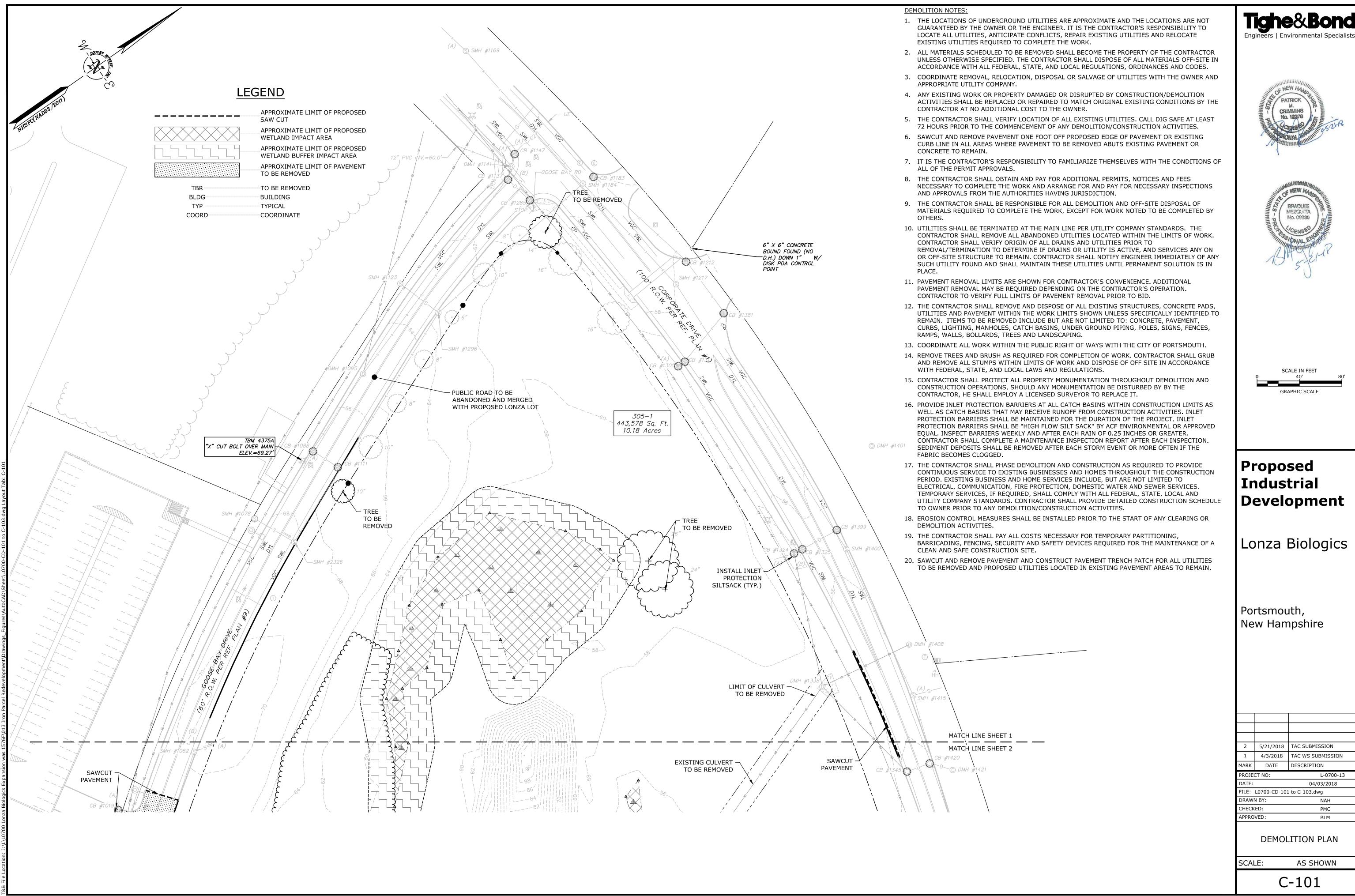
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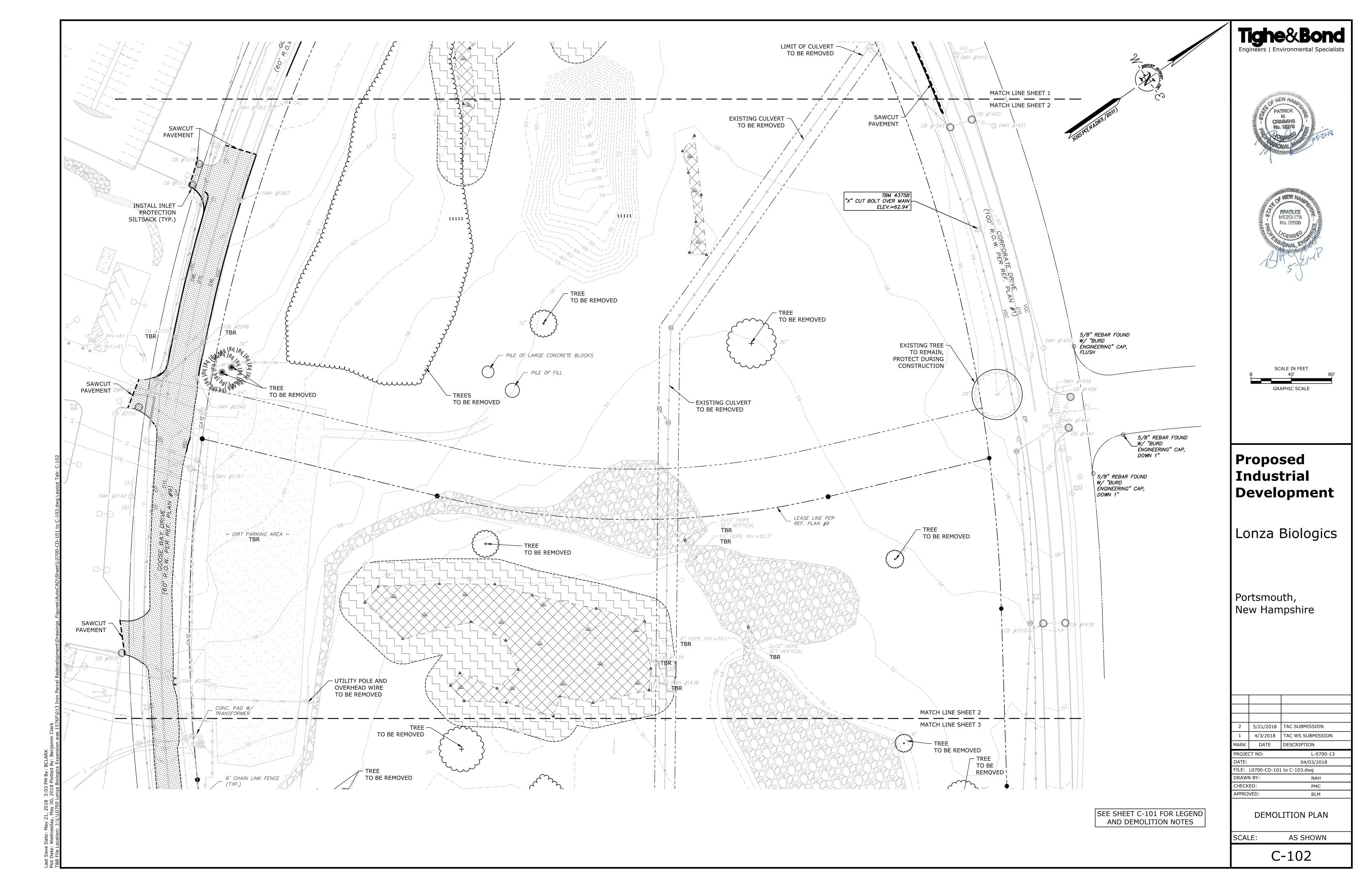


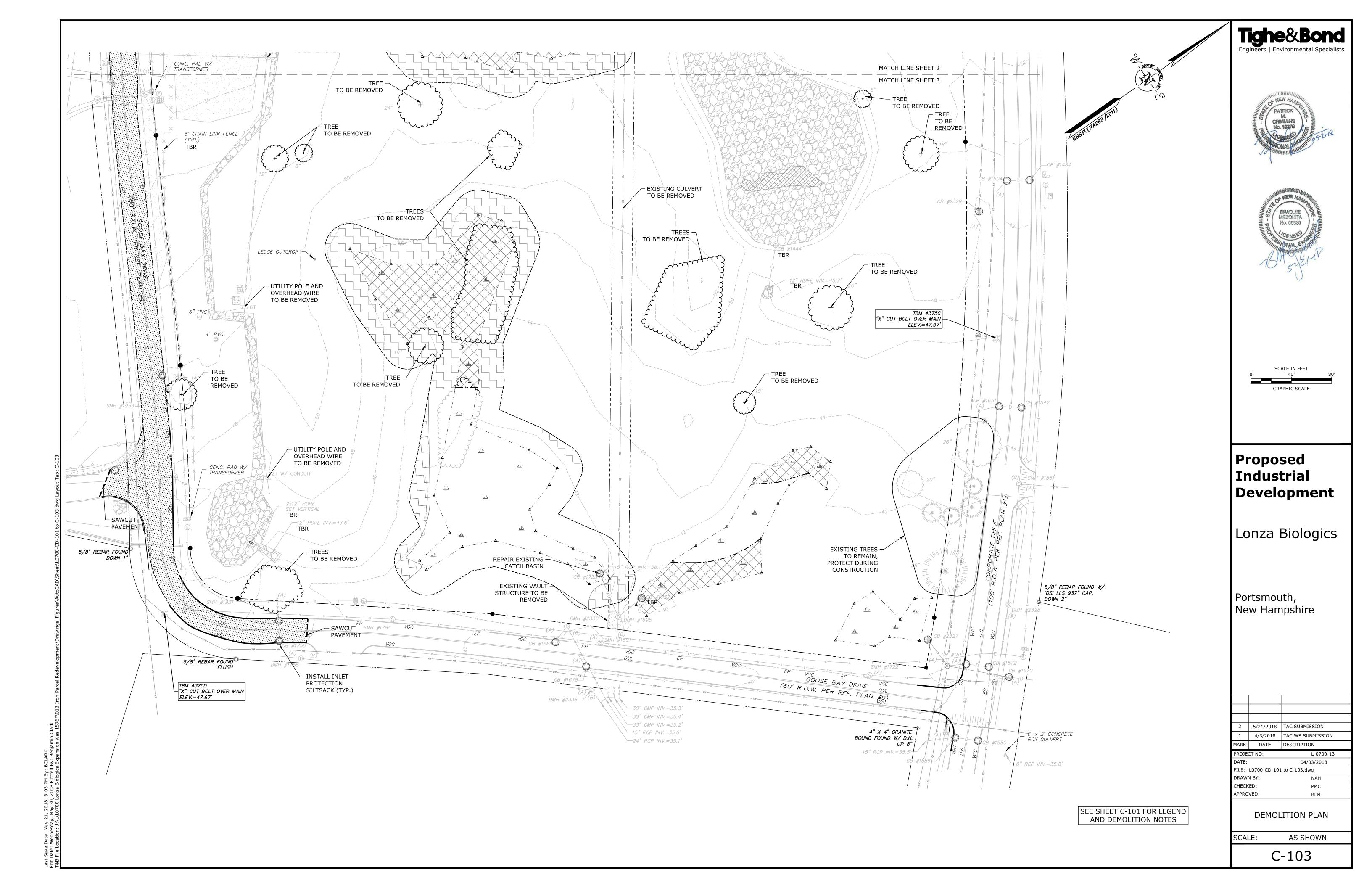


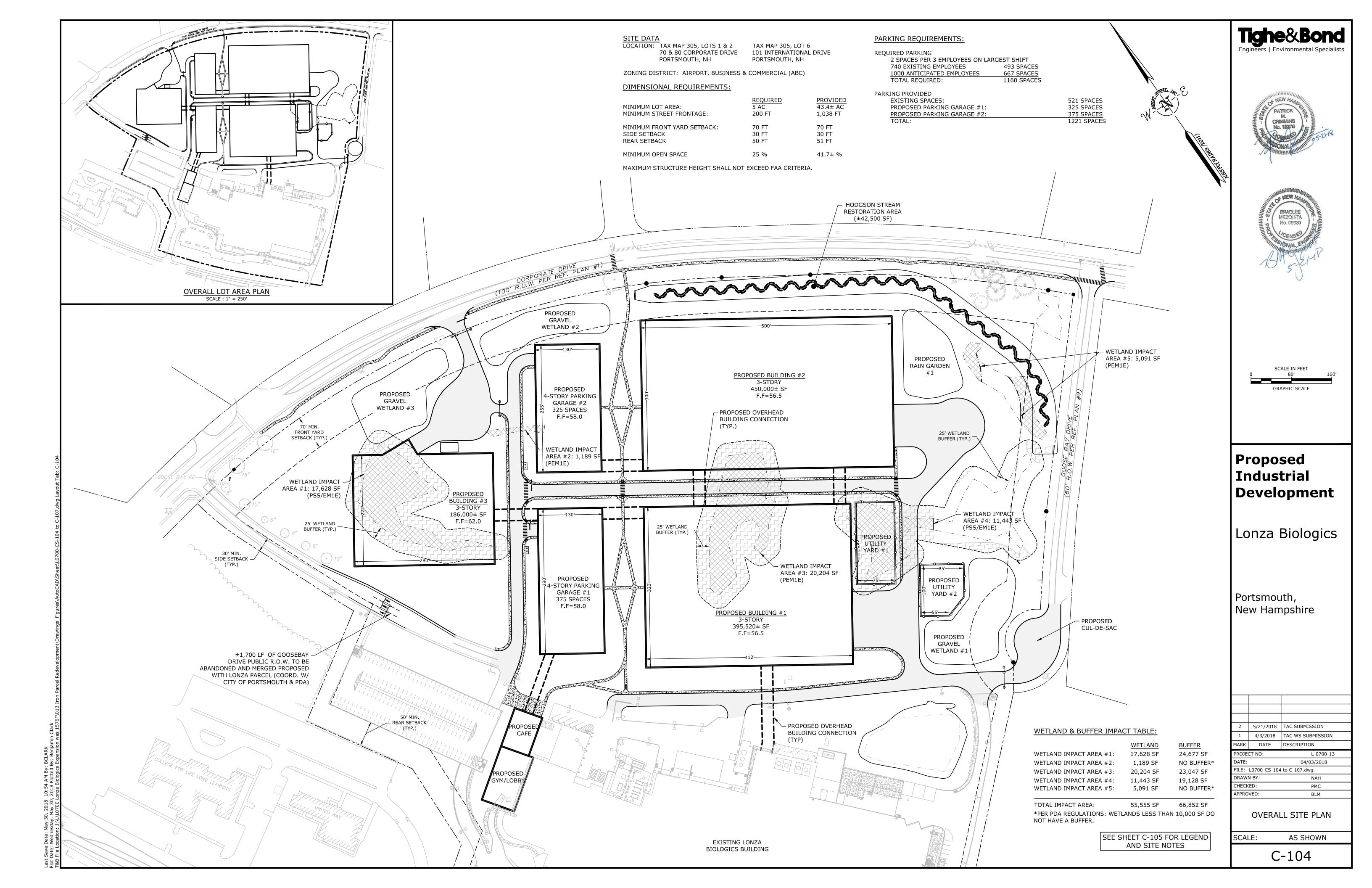


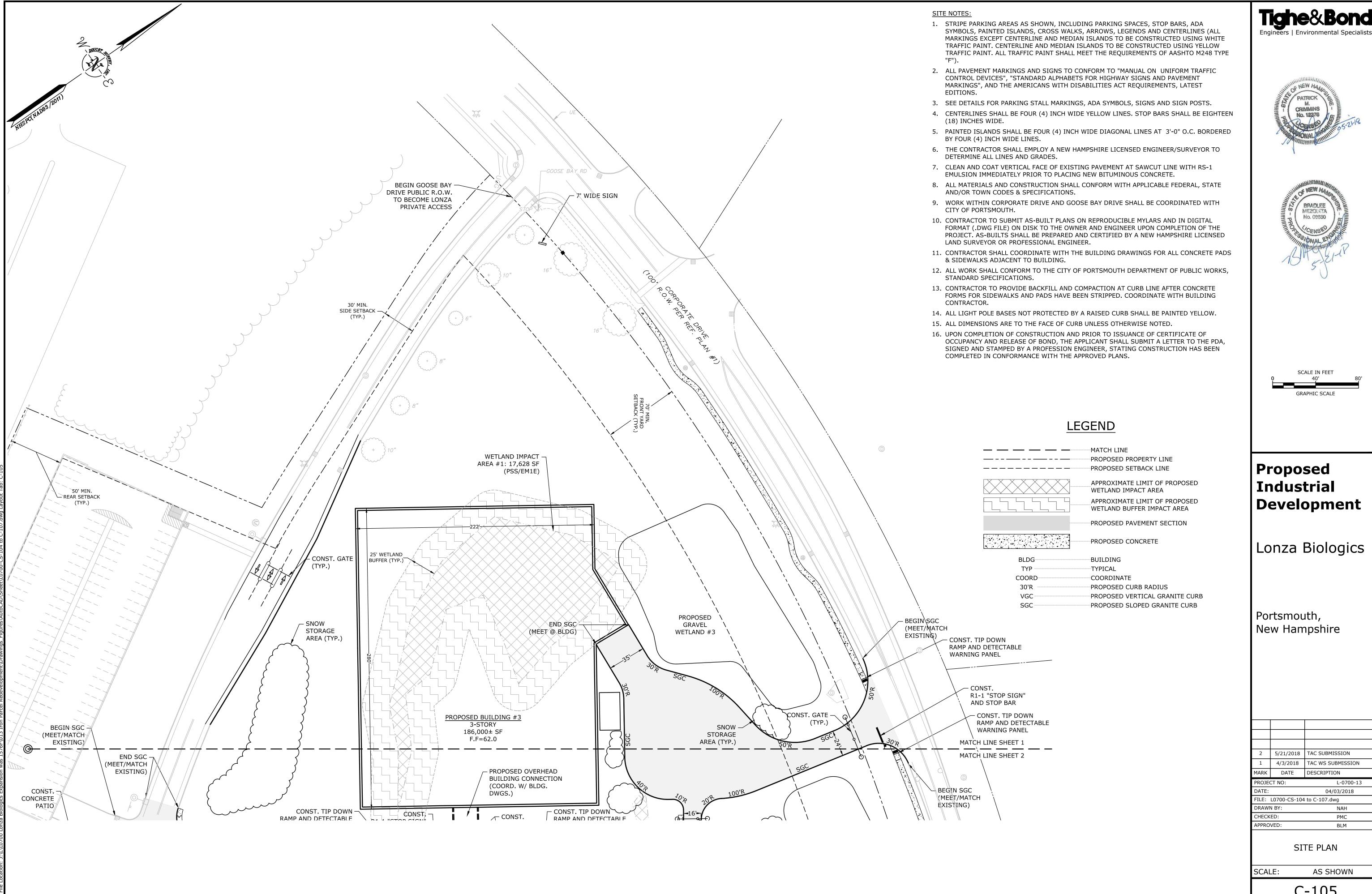


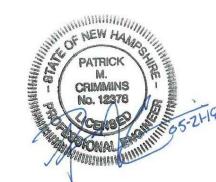
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MARK	DATE	DESCRIPTION
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DATE:		04/03/2018

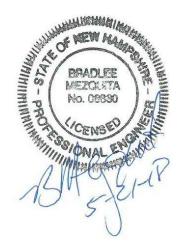


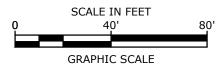












Industrial Development

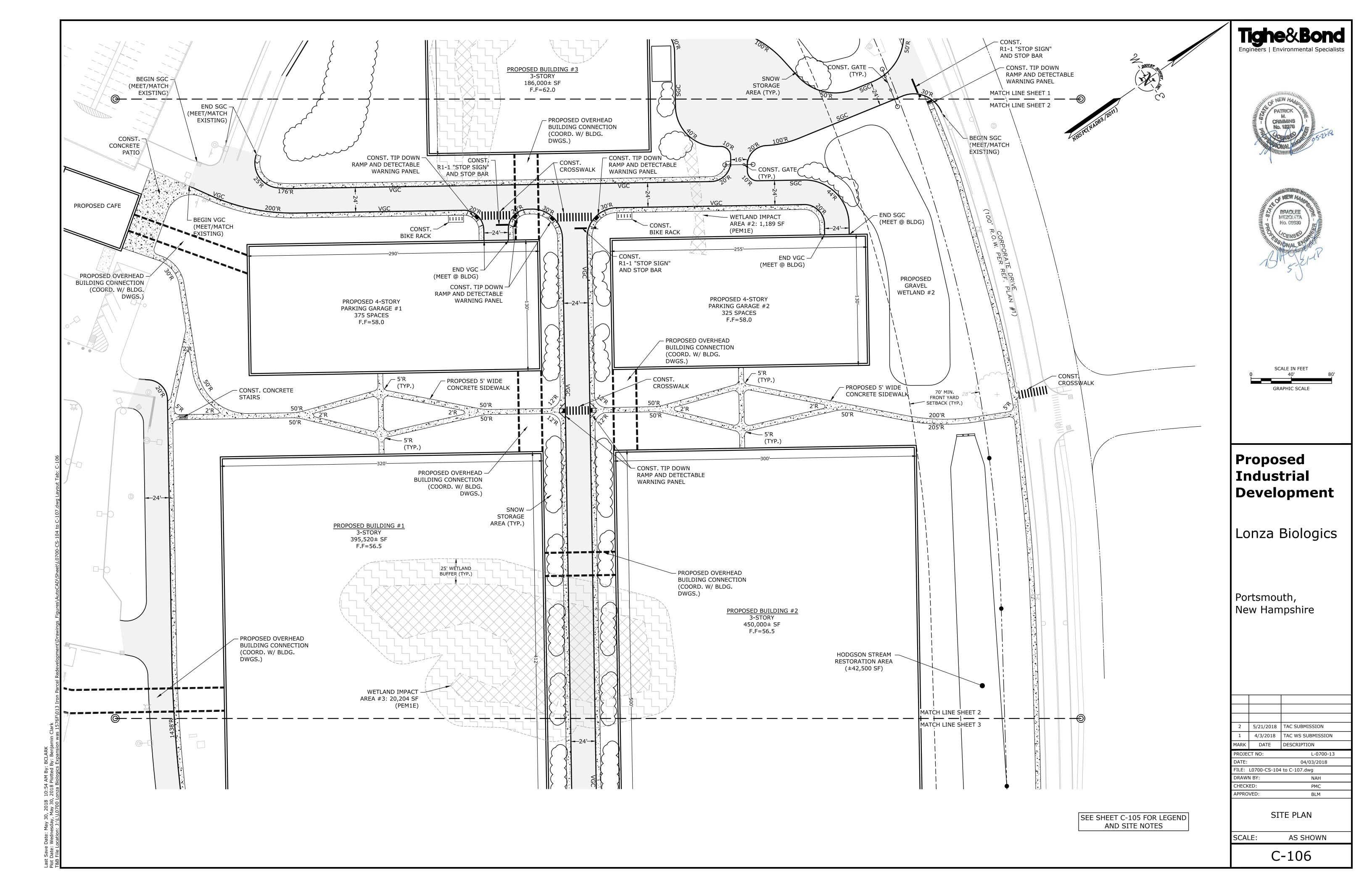
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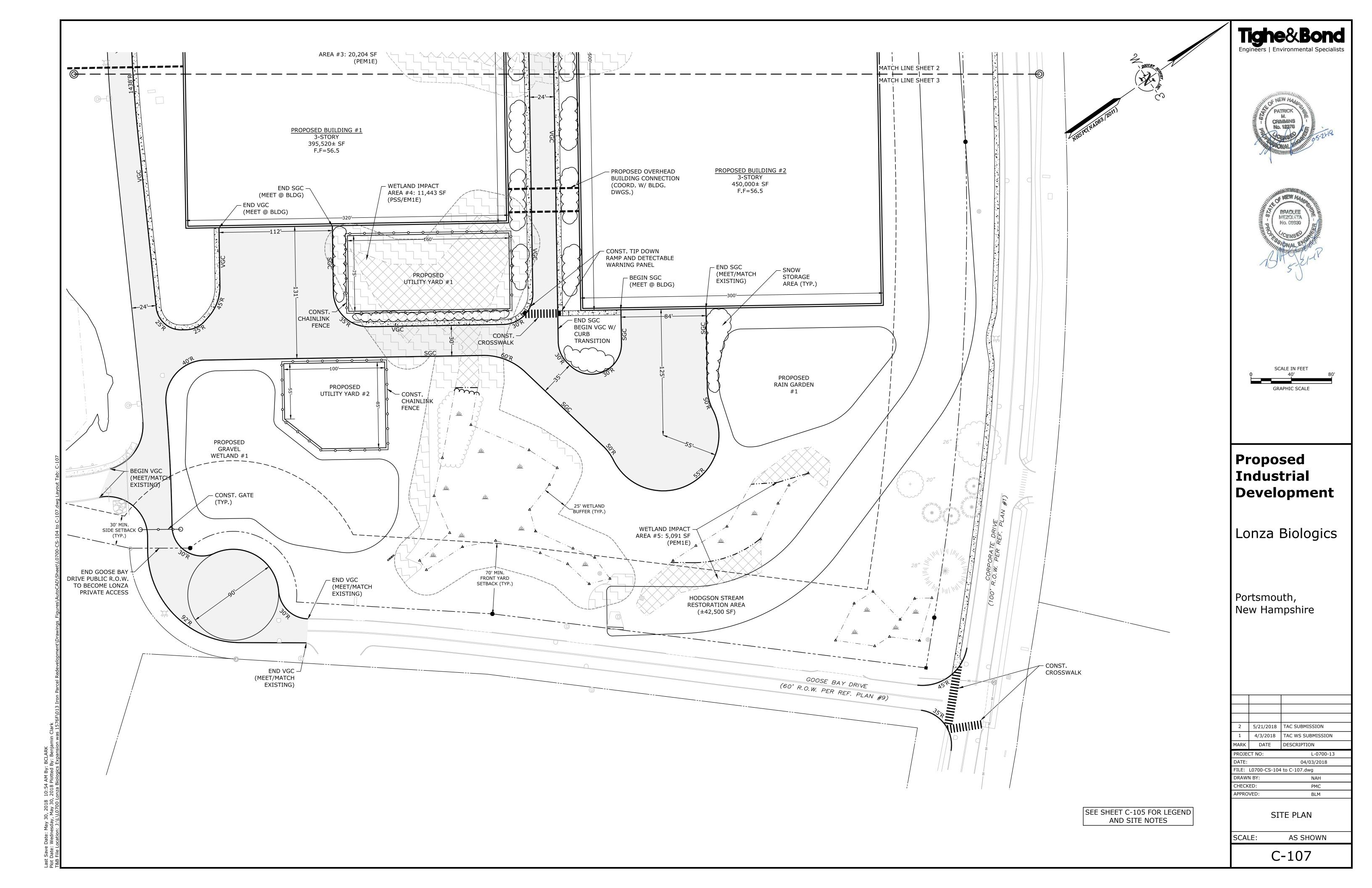
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DATE: 04/03/2018				
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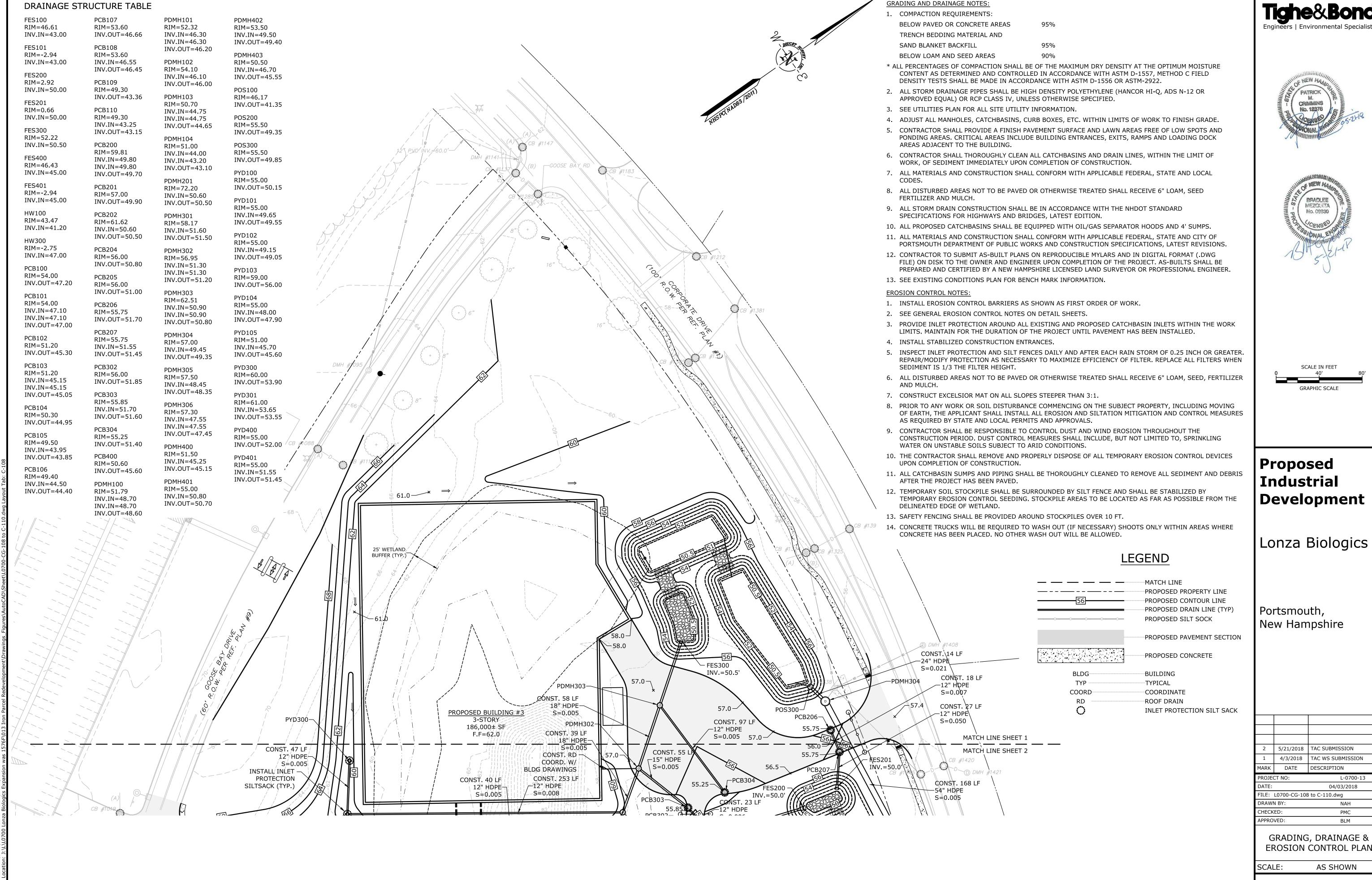
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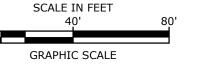
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AS SHOWN

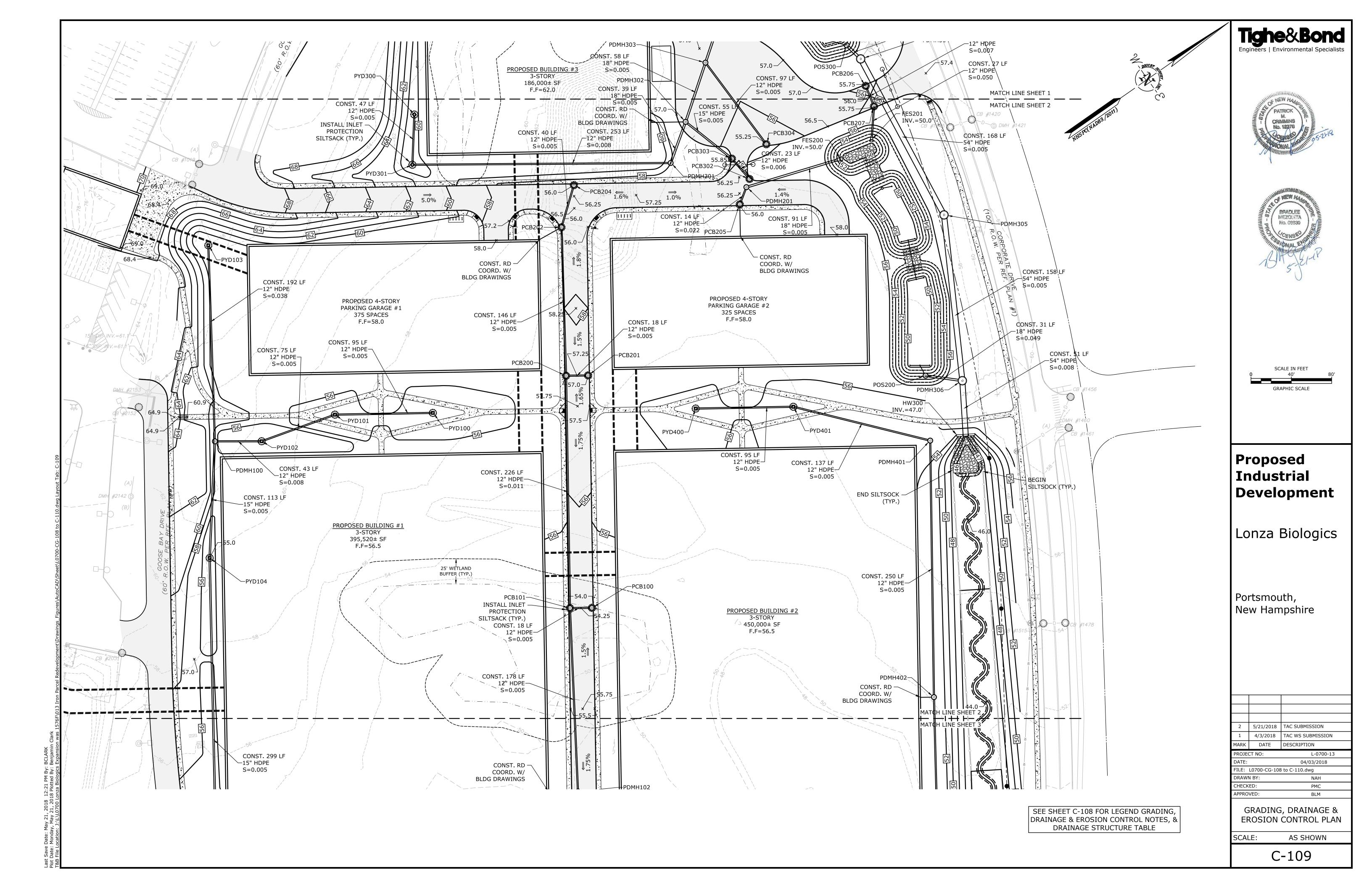


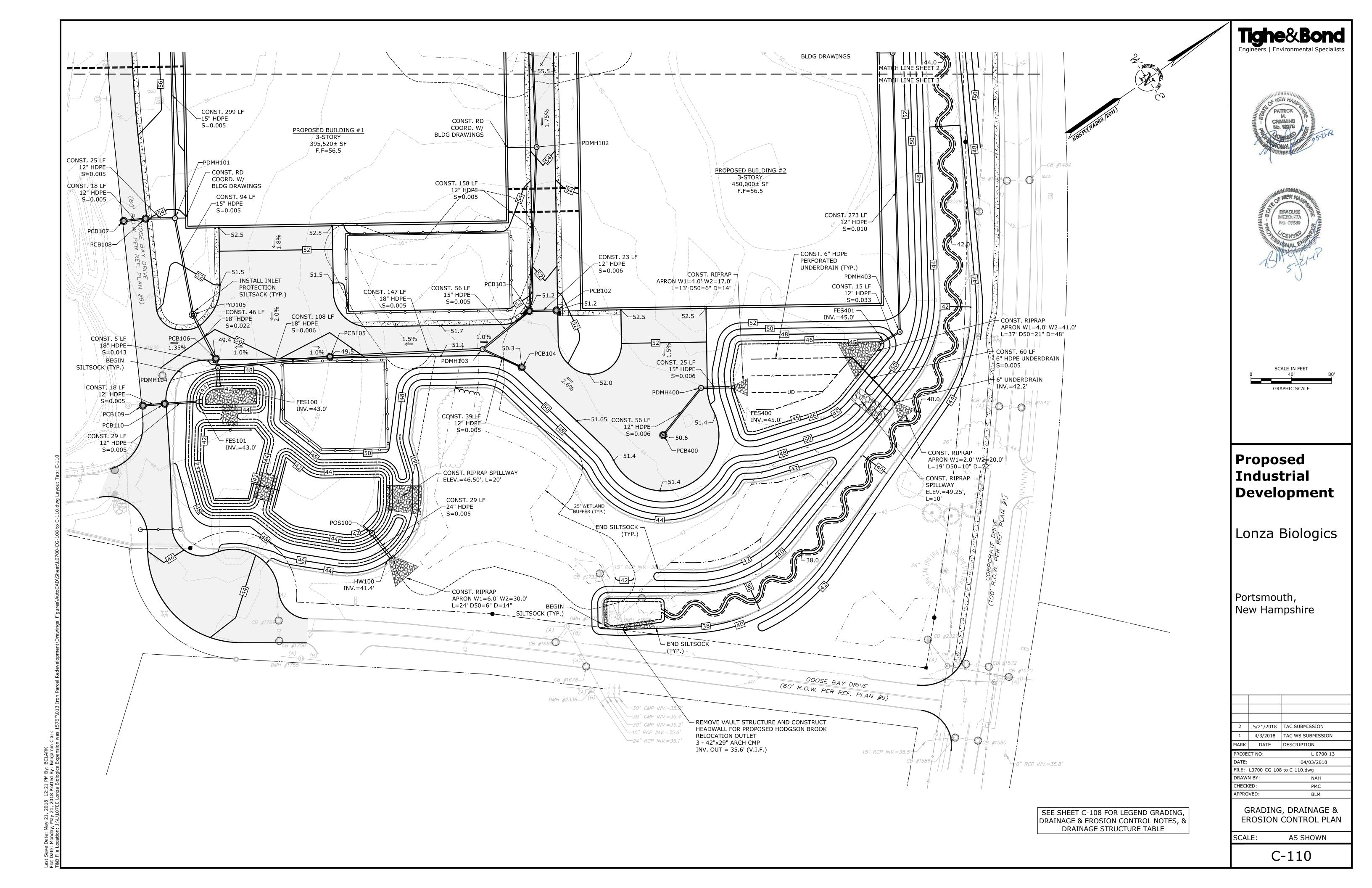


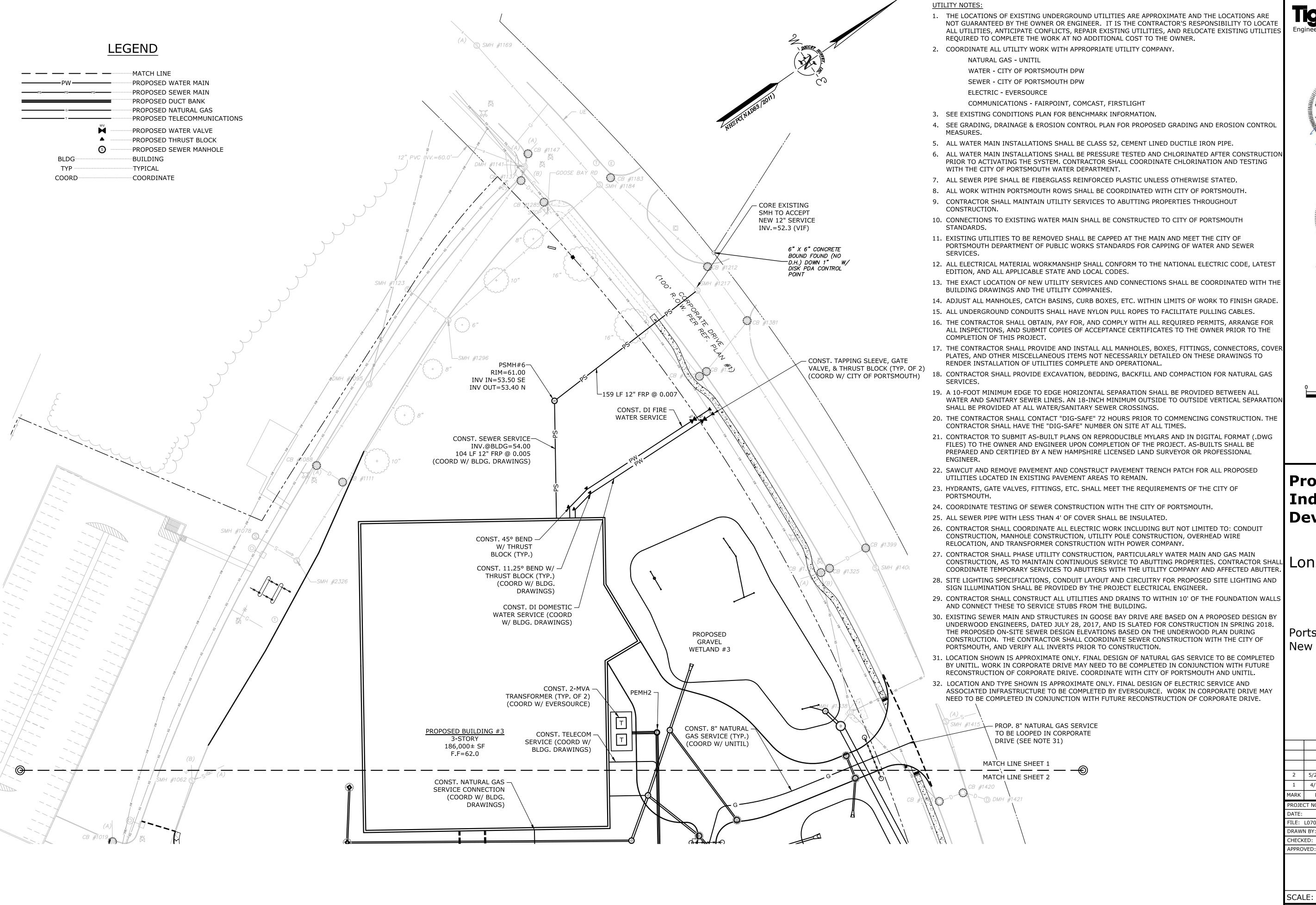




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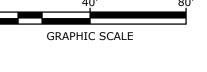




Tighe&Bond







Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

2	5/21/2018	TAC SUBMISSION	
1	4/3/2018	TAC WS SUBMISSION	
MARK	DATE	DESCRIPTION	
PROJECT NO:		L-0700-13	

DATE: 04/03/2018

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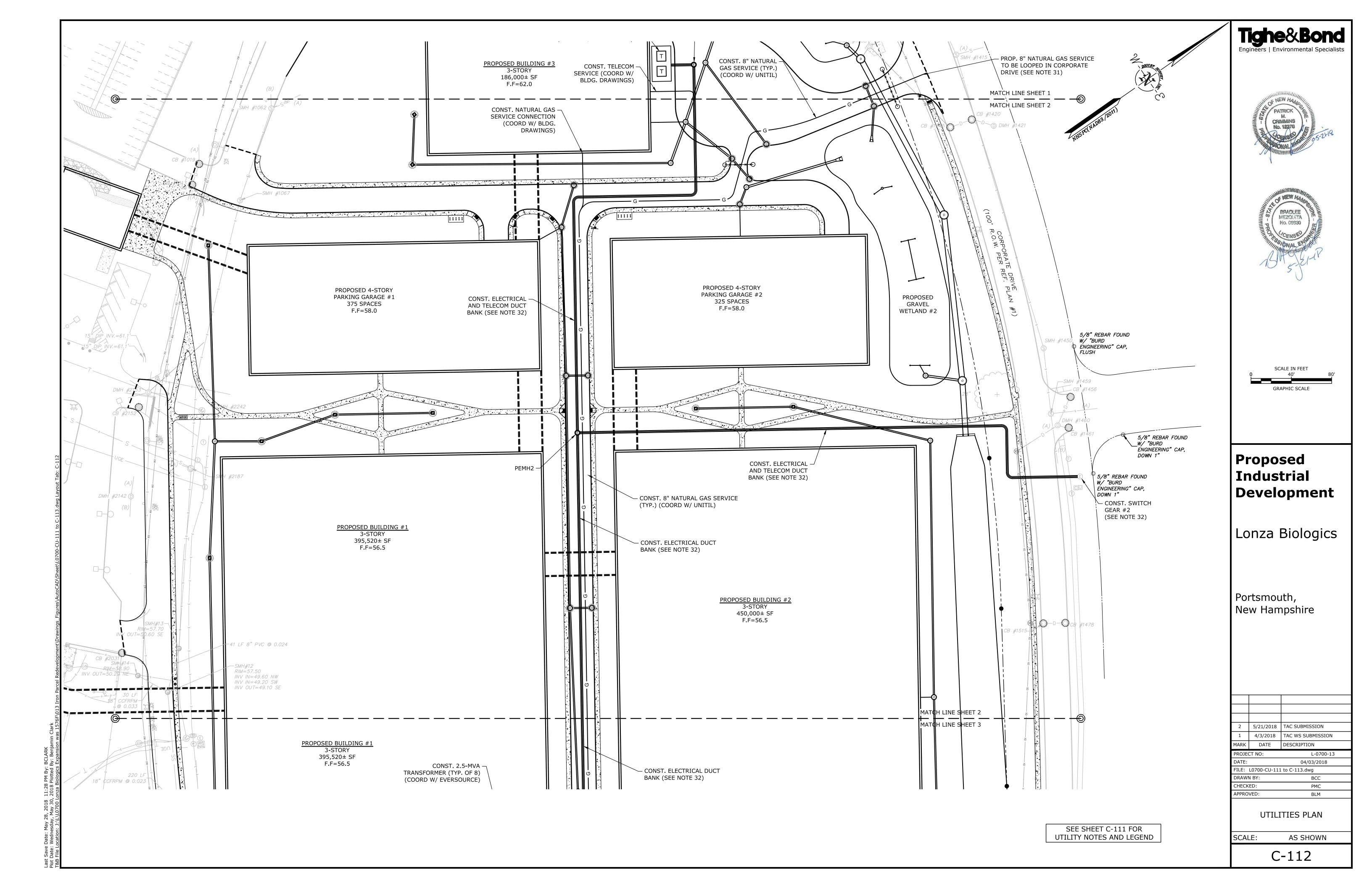
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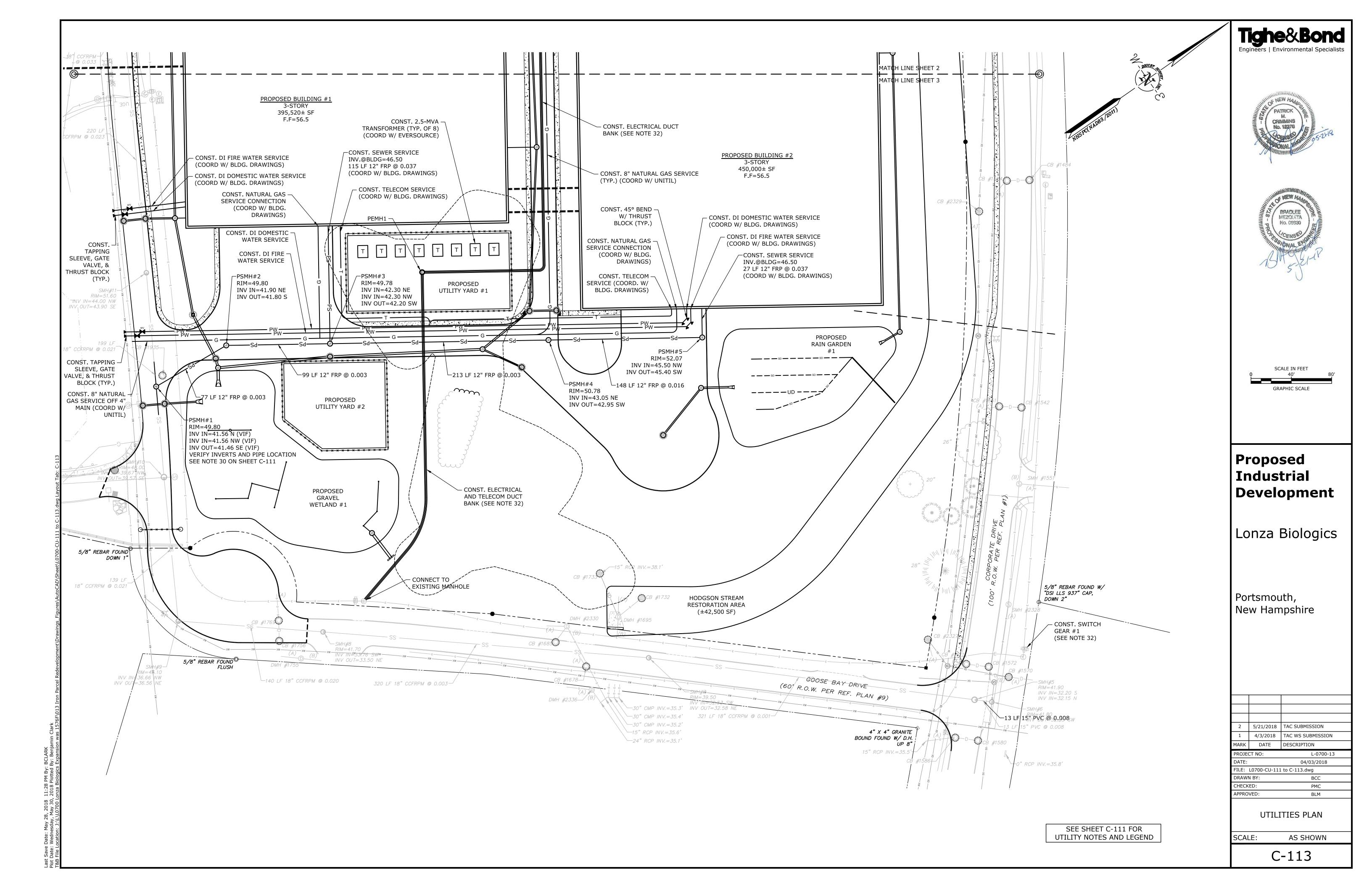
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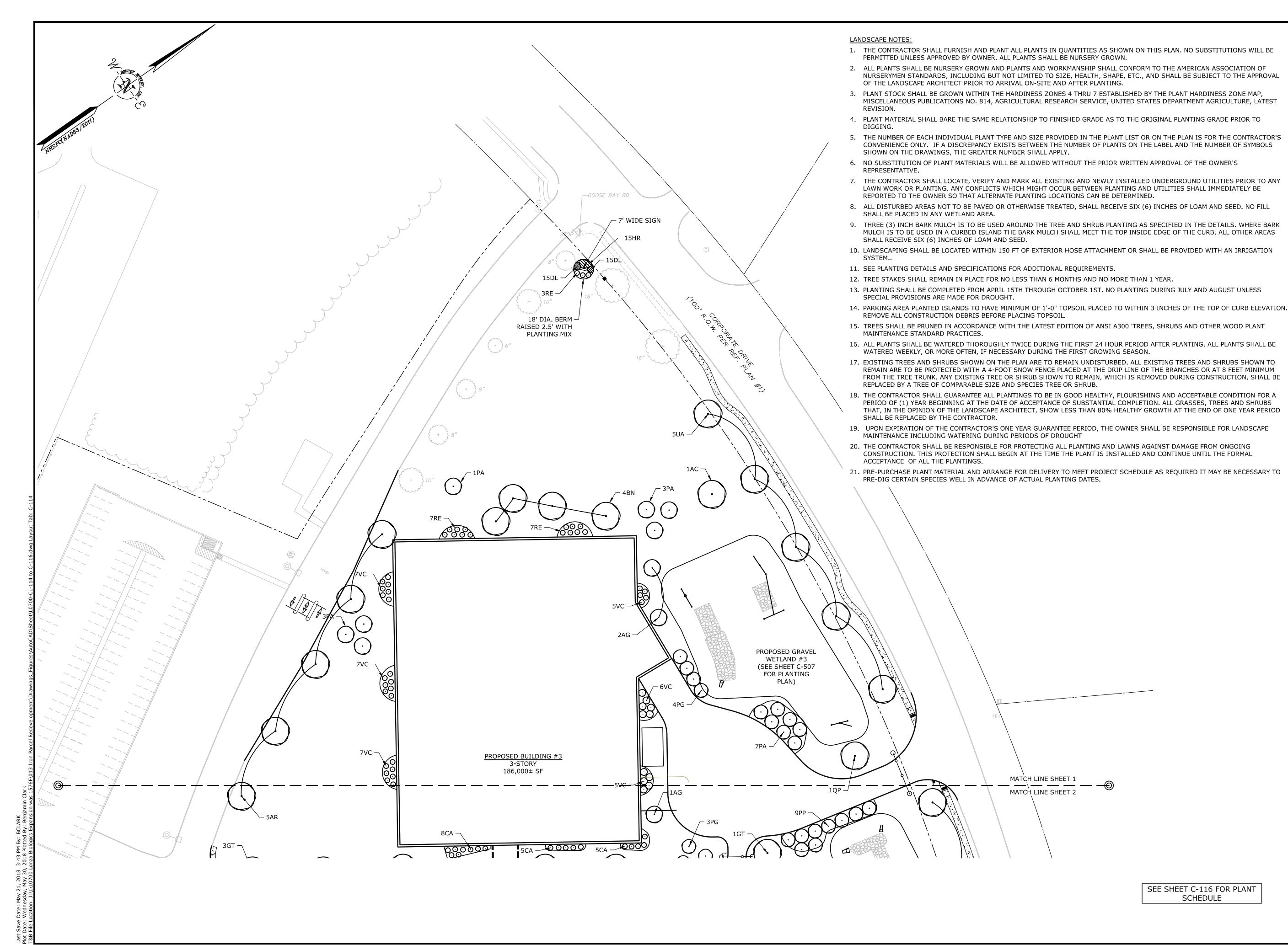
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UTILITIES PLAN

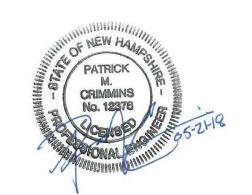
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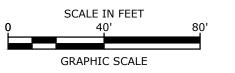




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Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

2	5/21/2018	TAC SUBMISSION
1	4/3/2018	TAC WS SUBMISSION
MARK	DATE	DESCRIPTION
PROJE	CT NO:	L-0700-13
DATE:		04/03/2018

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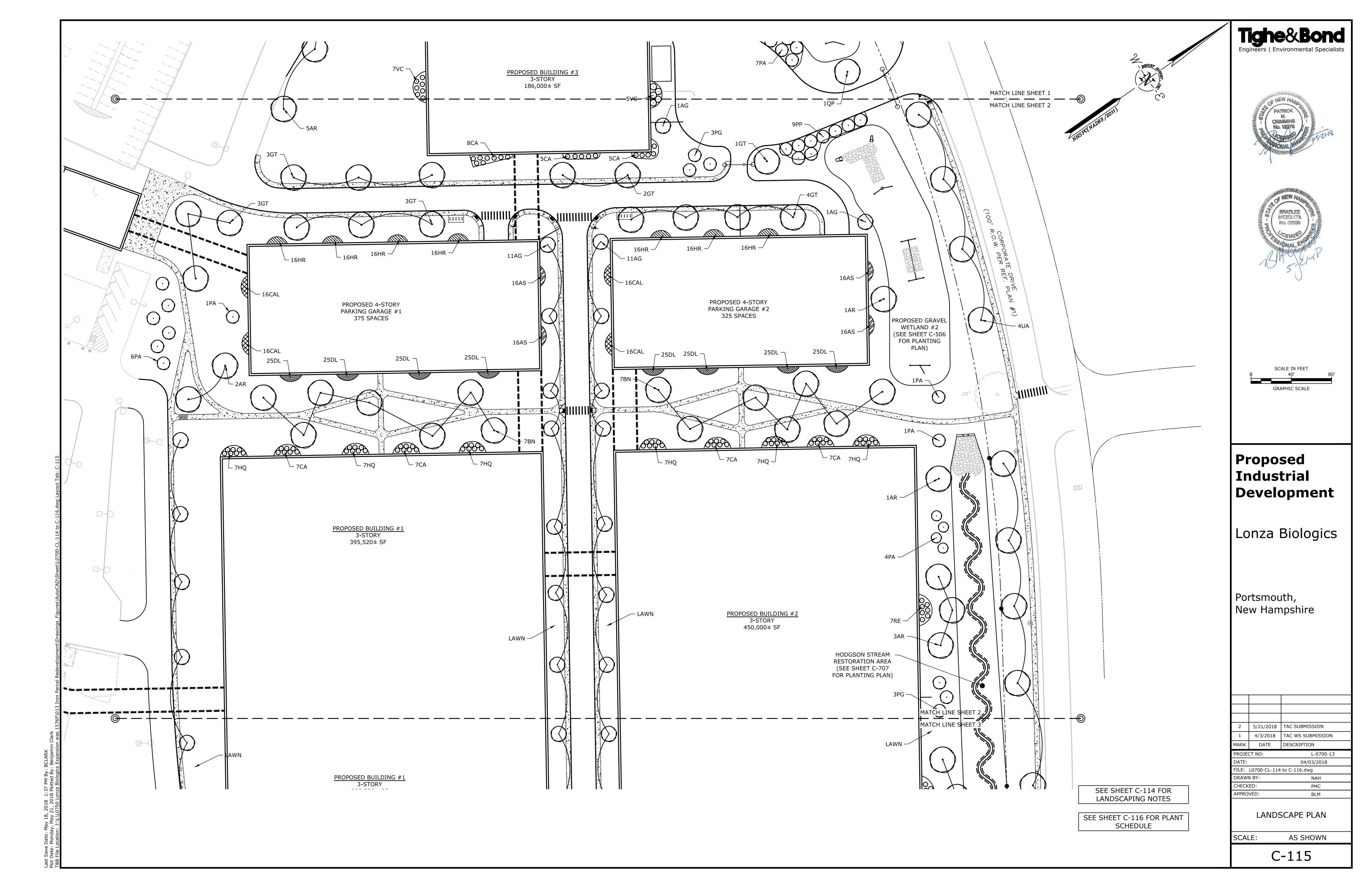
LANDSCAPE PLAN

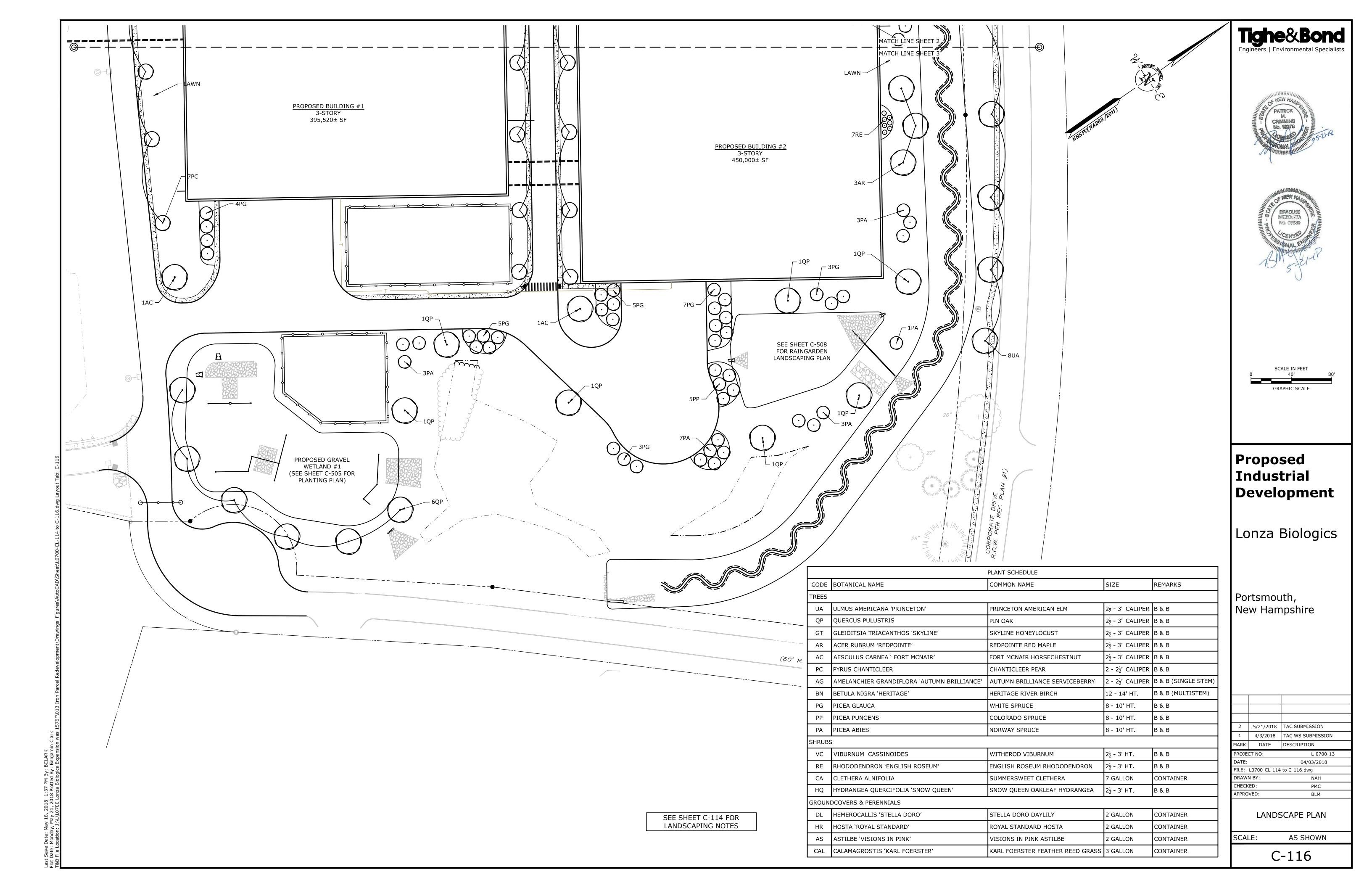
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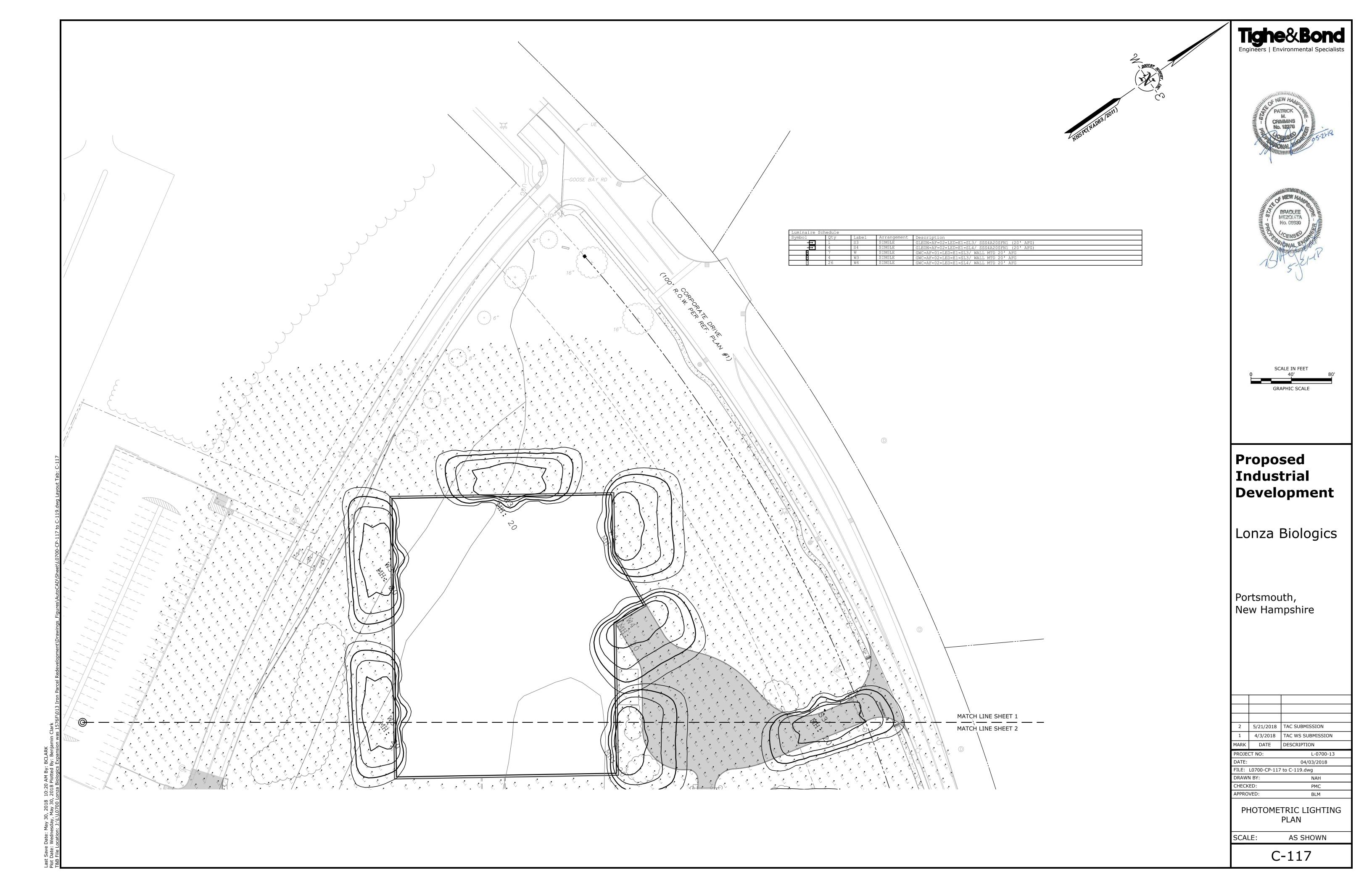
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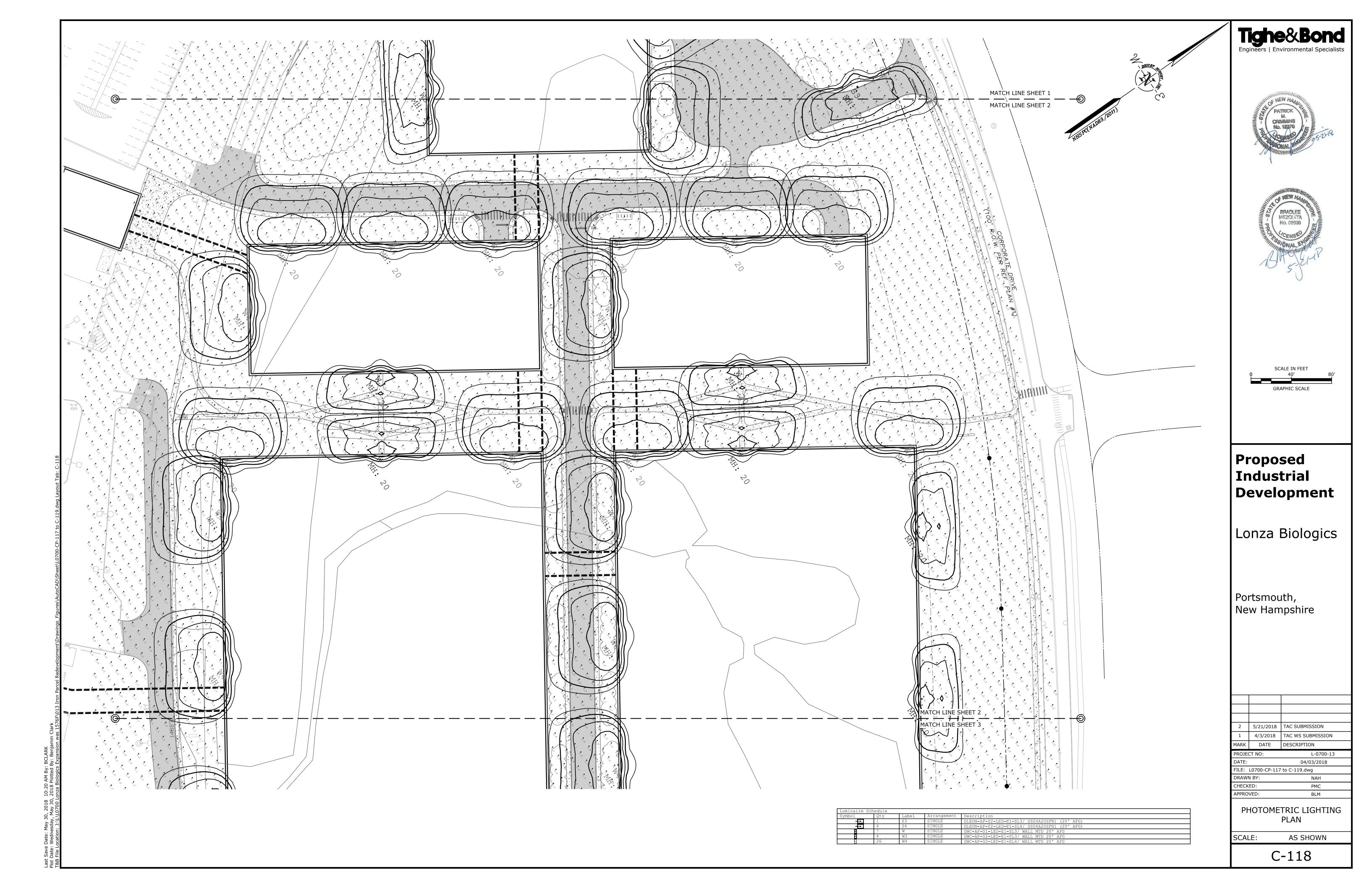
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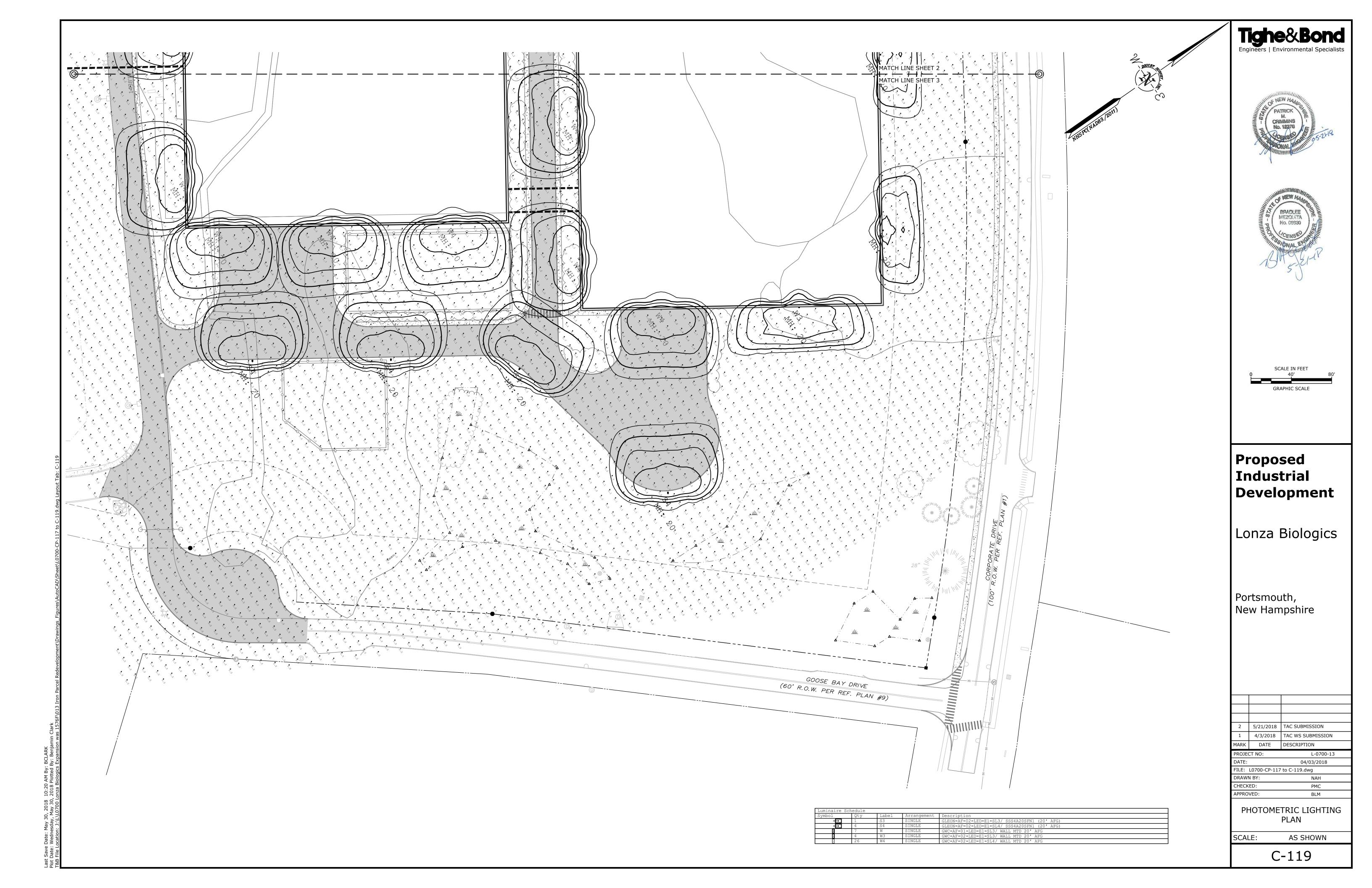
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PORTSMOUTH, NH 03801

DESCRIPTION
THE PROJECT CONSISTS OF THE EXPANSION OF LONZA BIOLOGICS, WHICH INCLUDES THE

<u>DISTURBED AREA</u>
THE TOTAL AREA TO BE DISTURBED IS APPROXIMATELY 23 ACRES.

SOIL CHARACTERISTIC

BASED ON THE HIGH INTENSITY SOIL SURVEY PREPARED BY GOVE ENVIRONMENTAL SERVICES, INC. IN DECEMBER 2015, THE SITE SOILS VARY FROM WELL DRAINED TO VERY POORLY DRAINED AND PRIMARILY CONSIST OF SOMEWHAT POORLY DRAINED SOILS.

NAME OF RECEIVING WATERS

THE STORM WATER RUNOFF WILL ULTIMATELY DISCHARGE INTO HODGSON BROOK

SEQUENCE OF MAJOR ACTIVITIES

- CUT AND CLEAR TREES.
- CONSTRUCT TEMPORARY AND PERMANENT SEDIMENT, EROSION AND DETENTION CONTROL FACILITIES. EROSION, SEDIMENT AND DETENTION MEASURES SHALL BE INSTALLED PRIOR TO ANY EARTH MOVING OPERATIONS THAT WILL INFLUENCE STORMWATER RUNOFF SUCH AS: - NEW CONSTRUCTION
 - DEVELOPMENT OF BORROW PIT AREAS
 - DISPOSAL OF SEDIMENT SPOIL, STUMP AND OTHER SOLID WASTE - STREAM CHANNEL MODIFICATIONS
 - CONTROL OF DUST
 - CONSTRUCTION OF ACCESS ROAD - NEARNESS OF CONSTRUCTION SITE TO RECEIVING WATERS
- CONSTRUCTION DURING LATE WINTER AND EARLY SPRING
- ALL PERMANENT DITCHES, SWALES, DETENTION, RETENTION AND SEDIMENTATION BASINS TO BE STABILIZED USING THE VEGETATIVE AND NON-STRUCTURAL BMPS PRIOR TO DIRECTING RUNOFF TO THEM.
- CLEAR AND DISPOSE OF DEBRIS
- CONSTRUCT TEMPORARY CULVERTS AND DIVERSION CHANNELS AS REQUIRED. GRADE AND GRAVEL ROADWAYS AND PARKING AREAS - ALL ROADS AND PARKING AREA
- SHALL BE STABILIZED IMMEDIATELY AFTER THEIR CONSTRUCTION.
- BEGIN PERMANENT AND TEMPORARY SEEDING AND MULCHING. ALL CUT AND FILL SLOPES HALL BE SEEDED AND MULCHED IMMEDIATELY AFTER THEIR CONSTRUCTION.
- DAILY, OR AS REQUIRED, CONSTRUCT TEMPORARY BERMS, DRAINS, DITCHES, SILT FENCES,
- SEDIMENT TRAPS, ETC., MULCH AND SEED AS REQUIRED.
- 9. FINISH PAVING ALL ROADWAYS AND PARKING LOTS.
- 10. INSPECT AND MAINTAIN ALL EROSION AND SEDIMENT CONTROL MEASURES. 11. COMPLETE PERMANENT SEEDING AND LANDSCAPING.
- 12. REMOVE TRAPPED SEDIMENTS FROM COLLECTOR DEVICES AS APPROPRIATE AND THEN REMOVE TEMPORARY EROSION CONTROL MEASURES.

NOTE: THE CONSTRUCTION SEQUENCE MUST LIMIT THE DURATION AND AREA OF DISTURBANCE.

- ALL EROSION CONTROL MEASURES AND PRACTICES SHALL CONFORM TO THE "NEW HAMPSHIRE STORMWATER MANUAL VOLUME 3: EROSION AND SEDIMENT CONTROLS DURING CONSTRUCTION" PREPARED BY THE NHDES
- PRIOR TO ANY WORK OR SOIL DISTURBANCE, CONTRACTOR SHALL SUBMIT SHOP DRAWINGS FOR EROSION CONTROL MEASURES AS REQUIRED IN THE PROJECT MANUAL.
- CONTRACTOR SHALL INSTALL TEMPORARY EROSION CONTROL BARRIERS, INCLUDING, SILT FENCES, SILT SACKS AND SILT SOCKS, AS SHOWN IN THESE DRAWINGS AS THE FIRST
- SILT SACK INLET PROTECTION SHALL BE INSTALLED IN ALL EXISTING AND PROPOSED CATCH BASIN INLETS WITHIN THE WORK LIMITS AND BE MAINTAINED FOR THE DURATION OF THE
- PERIMETER CONTROLS INCLUDING SILT FENCES, AND/OR SILT SOCKS SHALL MAINTAINED FOR THE DURATION OF THE PROJECT UNTIL NON-PAVED AREAS HAVE BEEN STABILIZED.
- THE CONTRACTOR SHALL REMOVE AND PROPERLY DISPOSE OF ALL TEMPORARY EROSION CONTROL DEVICES UPON COMPLETION OF CONSTRUCTION.
- ALL DISTURBED AREAS NOT OTHERWISE BEING TREATED SHALL RECEIVE 6" LOAM, SEED, INSPECT ALL INLET PROTECTION AND PERIMETER CONTROLS WEEKLY AND AFTER EACH RAIN STORM OF 0.25 INCH OR GREATER. REPAIR/MODIFY PROTECTION AS NECESSARY TO
- MAXIMIZE EFFICIENCY OF FILTER. REPLACE ALL FILTERS WHEN SEDIMENT IS 1/3 THE FILTER
- CONSTRUCT EROSION CONTROL BLANKETS ON ALL SLOPES STEEPER THAN 3:1.

- AN AREA SHALL BE CONSIDERED STABLE WHEN ONE OF THE FOLLOWING HAS OCCURRED: A. BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED.
- B. A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED.
- C. A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH AS STONE OR RIPRAP HAS BEEN INSTALLED
- D. EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.

WINTER STABILIZATION PRACTICES:

- A. ALL PROPOSED POST-DEVELOPMENT VEGETATED AREAS WHICH DO NOT EXHIBIT A MINIMUM OF 85% VEGETATED GROWTH BY NOVEMBER 15TH, OR WHICH ARE DISTURBED AFTER NOVEMBER 15TH, SHALL BE STABILIZED BY SEEDING AND INSTALLING EROSION CONTROL BLANKETS ON SLOPES GREATER THAN 4:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHOR NETTING, ELSEWHERE.
- ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85% VEGETATIVE GROWTH BY OCTOBER 15TH, OR WHICH ARE DISTURBED AFTER OCTOBER 15TH, SHALL BE STABILIZED WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITION.
- AFTER NOVEMBER 15TH, INCOMPLETE ROAD SURFACES SHALL BE PROTECTED WITH A MINIMUM OF 3-INCHES OF CRUSHED GRAVEL PER NHDOT ITEM 304.3, OR IF CONSTRUCTION IS TO CONTINUE THROUGH THE WINTER SEASON BE CLEARED OF ANY ACCUMULATED SNOW AFTER EACH STORM EVENT.
- STABILIZATION SHALL BE INITIATED ON ALL LOAM STOCKPILES, AND DISTURBED AREAS, WHERE CONSTRUCTION ACTIVITY SHALL NOT OCCUR FOR MORE THAN TWENTY-ONE (21) CALENDAR DAYS BY THE FOURTEENTH (14TH) DAY AFTER CONSTRUCTION ACTIVITY HAS PERMANENTLY OR TEMPORARILY CEASED IN THAT AREA. STABILIZATION MEASURES TO BE **USED INCLUDE:**
- A. TEMPORARY SEEDING

B. MULCHING

- WHEN CONSTRUCTION ACTIVITY PERMANENTLY OR TEMPORARILY CEASES WITHIN 100 FEET OF NEARBY SURFACE WATERS OR DELINEATED WETLANDS, THE AREA SHALL BE STABILIZED WITHIN SEVEN (7) DAYS OR PRIOR TO A RAIN EVENT. ONCE CONSTRUCTION ACTIVITY CEASES PERMANENTLY IN AN THESE AREAS, SILT FENCES AND HAY BALE BARRIERS AND ANY EARTH/DIKES SHALL BE REMOVED ONCE PERMANENT MEASURES ARE ESTABLISHED.
- DURING CONSTRUCTION, RUNOFF WILL BE DIVERTED AROUND THE SITE WITH EARTH DIKES, PIPING OR STABILIZED CHANNELS WHERE POSSIBLE. SHEET RUNOFF FROM THE SITE WILL BE FILTERED THROUGH HAY BALE BARRIERS AND SILT FENCES OR SILT SOCKS. ALL STORM DRAIN BASIN INLETS SHALL BE PROVIDED WITH FLARED END SECTIONS AND TRASH RACKS. THE SITE SHALL BE STABILIZED FOR THE WINTER BY NOVEMBER 15.

DUST CONTROL METHODS SHALL INCLUDE, BUT BE NOT LIMITED TO SPRINKLING WATER ON

- THE CONTRACTOR SHALL BE RESPONSIBLE TO CONTROL DUST THROUGHOUT THE
- EXPOSED AREAS, COVERING LOADED DUMP TRUCKS LEAVING THE SITE, AND TEMPORARY MULCHING. DUST CONTROL MEASURES SHALL BE UTILIZED SO AS TO PREVENT THE MIGRATION OF DUST
- FROM THE SITE TO ABUTTING AREAS INCLUDING.

LOCATE STOCKPILES A MINIMUM OF 50 FEET AWAY FROM CATCH BASINS, SWALES, AND

- 2. ALL STOCKPILES SHOULD BE SURROUNDED WITH TEMPORARY EROSION CONTROL MEASURES PRIOR TO THE ONSET OF PRECIPITATION.
- PERIMETER BARRIERS SHOULD BE MAINTAINED AT ALL TIMES, AND ADJUSTED AS NEEDED TO ACCOMMODATE THE DELIVERY AND REMOVAL OF MATERIALS FROM THE STOCKPILE. THE
- INTEGRITY OF THE BARRIER SHOULD BE INSPECTED AT THE END OF EACH WORKING DAY. 4. PROTECT ALL STOCKPILES FROM STORMWATER RUN-OFF USING TEMPORARY EROSION CONTROL MEASURES SUCH AS BERMS, SILT SOCK, OR OTHER APPROVED PRACTICE TO PREVENT MIGRATION OF MATERIAL BEYOND THE IMMEDIATE CONFINES OF THE STOCKPILES.

THE CONTRACTOR SHALL CONSTRUCT STABILIZED CONSTRUCTION ENTRANCE(S) PRIOR TO ANY

EXCAVATION ACTIVITIES.

- TEMPORARY GRASS COVER
- A. SEEDBED PREPARATION APPLY FERTILIZER AT THE RATE OF 600 POUNDS PER ACRE OF 10-10-10. APPLY LIMESTONE (EQUIVALENT TO 50 PERCENT CALCIUM PLUS MAGNESIUM OXIDE) AT A RATE OF THREE (3) TONS PER ACRE.
- SEEDING 1. UTILIZE ANNUAL RYE GRASS AT A RATE OF 40 LBS/ACRE.
- 2. WHERE THE SOIL HAS BEEN COMPACTED BY CONSTRUCTION OPERATIONS, LOOSEN SOIL TO A DEPTH OF TWO (2) INCHES BEFORE APPLYING FERTILIZER, LIME AND
- 3. APPLY SEED UNIFORMLY BY HAND, CYCLONE SEEDER, OR HYDROSEEDER (SLURRY INCLUDING SEED AND FERTILIZER). HYDROSEEDINGS, WHICH INCLUDE MULCH, MAY BE LEFT ON SOIL SURFACE. SEEDING RATES MUST BE INCREASED 10% WHEN HYDROSEEDING.
- C. MAINTENANCE TEMPORARY SEEDING SHALL BE PERIODICALLY INSPECTED. AT A MINIMUM, 95% OF THE SOIL SURFACE SHOULD BE COVERED BY VEGETATION. IF ANY EVIDENCE OF EROSION OR SEDIMENTATION IS APPARENT, REPAIRS SHALL BE MADE AND OTHER TEMPORARY MEASURES USED IN THE INTERIM (MULCH, FILTER BARRIERS, CHECK DAMS, ETC.).

- A. FOR PERMANENT MEASURES AND PLANTINGS.
 - 1. LIMESTONE SHALL BE THOROUGHLY INCORPORATED INTO THE LOAM LAYER AT A RATE OF THREE (3) TONS PER ACRE IN ORDER TO PROVIDE A PH VALUE OF 5.5 TO
- 2. FERTILIZER SHALL BE SPREAD ON THE TOP LAYER OF LOAM AND WORKED INTO THE SURFACE. FERTILIZER APPLICATION RATE SHALL BE 800 POUNDS PER ACRE OF 10-20-20 FERTILIZER.
- 3. SOIL CONDITIONERS AND FERTILIZER SHALL BE APPLIED AT THE RECOMMENDED RATES AND SHALL BE THOROUGHLY WORKED INTO THE LOAM. LOAM SHALL BE RAKED UNTIL THE SURFACE IS FINELY PULVERIZED, SMOOTH AND EVEN, AND THEN COMPACTED TO AN EVEN SURFACE CONFORMING TO THE REQUIRED LINES AND GRADES WITH APPROVED ROLLERS WEIGHING BETWEEN 4-1/2 POUNDS AND 5-1/2 POUNDS PER INCH OF WIDTH.
- 4. SEED SHALL BE SOWN AT THE RATE SHOWN BELOW. SOWING SHALL BE DONE ON A CALM, DRY DAY, PREFERABLY BY MACHINE, BUT IF BY HAND, ONLY BY EXPERIENCED WORKMEN. IMMEDIATELY BEFORE SEEDING, THE SOIL SHALL BE LIGHTLY RAKED. ONE HALF THE SEED SHALL BE SOWN IN ONE DIRECTION AND THE OTHER HALF AT RIGHT ANGLES TO THE ORIGINAL DIRECTION. IT SHALL BE LIGHTLY RAKED INTO THE SOIL TO A DEPTH NOT OVER 1/4 INCH AND ROLLED WITH A HAND ROLLER WEIGHING NOT OVER 100 POUNDS PER LINEAR FOOT OF WIDTH.
- 5. HAY MULCH SHALL BE APPLIED IMMEDIATELY AFTER SEEDING AS INDICATED ABOVE. 6. THE SURFACE SHALL BE WATERED AND KEPT MOIST WITH A FINE SPRAY AS REQUIRED, WITHOUT WASHING AWAY THE SOIL, UNTIL THE GRASS IS WELL ESTABLISHED. ANY AREAS WHICH ARE NOT SATISFACTORILY COVERED WITH GRASS SHALL BE RESEEDED, AND ALL NOXIOUS WEEDS REMOVED.
- 7. THE CONTRACTOR SHALL PROTECT AND MAINTAIN THE SEEDED AREAS UNTIL 8. A GRASS SEED MIXTURE CONTAINING THE FOLLOWING SEED REQUIREMENTS SHALL
- BE APPLIED AT THE INDICATED RATE: SEEDING RATE CREEPING RED FESCUE
 - 20 LBS/ACRE 20 LBS/ACRE TALL FESCUE 2 LBS/ACRE
- IN NO CASE SHALL THE WEED CONTENT EXCEED ONE (1) PERCENT BY WEIGHT. ALL SEED SHALL COMPLY WITH STATE AND FEDERAL SEED LAWS. SEEDING SHALL BE DONE NO LATER THAN SEPTEMBER 15. IN NO CASE SHALL SEEDING TAKE PLACE OVER SNOW.
- DORMANT SEEDING (SEPTEMBER 15 TO FIRST SNOWFALL)
- FOLLOW PERMANENT MEASURES SLOPE, LIME, FERTILIZER AND GRADING REQUIREMENTS. APPLY SEED MIXTURE AT TWICE THE INDICATED RATE. APPLY MULCH AS INDICATED FOR PERMANENT MEASURES.

ONCRETE WASHOUT AREA

- THE FOLLOWING ARE THE ONLY NON-STORMWATER DISCHARGES ALLOWED. ALL OTHER NON-STORMWATER DISCHARGES ARE PROHIBITED ON SITE. A. THE CONCRETE DELIVERY TRUCKS SHALL, WHENEVER POSSIBLE, USE WASHOUT
 - FACILITIES AT THEIR OWN PLANT OR DISPATCH FACILITY. B. IF IT IS NECESSARY, SITE CONTRACTOR SHALL DESIGNATE SPECIFIC WASHOUT AREAS
 - AND DESIGN FACILITIES TO HANDLE ANTICIPATED WASHOUT WATER. C. CONTRACTOR SHALL LOCATE WASHOUT AREAS AT LEAST 150 FEET AWAY FROM STORM
 - DRAINS, SWALES AND SURFACE WATERS OR DELINEATED WETLANDS. D. INSPECT WASHOUT FACILITIES DAILY TO DETECT LEAKS OR TEARS AND TO IDENTIFY WHEN MATERIALS NEED TO BE REMOVED.

ALLOWABLE NON-STORMWATER DISCHARGE

- DISCHARGES FROM FIRE-FIGHTING ACTIVITIES 2. FIRE HYDRANT FLUSHINGS
- WATERS USED TO WASH VEHICLES WHERE DETERGENTS ARE NOT USED WATER USED TO CONTROL DUST
- POTABLE WATER INC. UNCONTAMINATED WATER LINE FLUSHINGS
- ROUTINE EXTERNAL BUILDING WASH DOWN -NO DETERGENTS PAVEMENT WASH WATERS -NO SPILLS OR DETERGENTS
- UNCONTAMINATED AIR CONDITIONING/COMPRESSOR CONDENSATE
- 9. UNCONTAMINATED GROUND WATER OR SPRING WATER 10. FOUNDATION OR FOOTING DRAINS -NOT CONTAMINATED
- 11. UNCONTAMINATED EXCAVATION DEWATERING

12. LANDSCAPE IRRIGATION

- A. ALL WASTE MATERIALS SHALL BE COLLECTED AND STORED IN SECURELY LIDDED RECEPTACLES. ALL TRASH AND CONSTRUCTION DEBRIS FROM THE SITE SHALL BE DEPOSITED IN A DUMPSTER.
- NO CONSTRUCTION WASTE MATERIALS SHALL BE BURIED ON SITE.
- C. ALL PERSONNEL SHALL BE INSTRUCTED REGARDING THE CORRECT PROCEDURE FOR WASTE DISPOSAL BY THE SUPERINTENDENT. HAZARDOUS WASTE
- A. ALL HAZARDOUS WASTE MATERIALS SHALL BE DISPOSED OF IN THE MANNER SPECIFIED BY LOCAL OR STATE REGULATION OR BY THE MANUFACTURER. SITE PERSONNEL SHALL BE INSTRUCTED IN THESE PRACTICES BY THE SUPERINTENDENT. SANITARY WASTE
 - A. ALL SANITARY WASTE SHALL BE COLLECTED FROM THE PORTABLE UNITS A MINIMUM OF ONCE PER WEEK BY A LICENSED SANITARY WASTE MANAGEMENT CONTRACTOR.

SPILL PREVENTIO

- CONTRACTOR SHALL BE FAMILIAR WITH SPILL PREVENTION MEASURES REQUIRED BY LOCAL, STATE AND FEDERAL AGENCIES. AT A MINIMUM, CONTRACTOR SHALL FOLLOW THE BEST MANAGEMENT SPILL PREVENTION PRACTICES OUTLINED BELOW. 2. THE FOLLOWING ARE THE MATERIAL MANAGEMENT PRACTICES THAT SHALL BE USED TO
- REDUCE THE RISK OF SPILLS OR OTHER ACCIDENTAL EXPOSURE OF MATERIALS AND SUBSTANCES DURING CONSTRUCTION TO STORMWATER RUNOFF:

- A. GOOD HOUSEKEEPING: THE FOLLOWING GOOD HOUSEKEEPING PRACTICES SHALL BE FOLLOWED ON SITE
- DURING THE CONSTRUCTION PROJECT: 1. ONLY SUFFICIENT AMOUNTS OF PRODUCTS TO DO THE JOB SHALL BE STORED ON
- 2. ALL MATERIALS STORED ON SITE SHALL BE STORED IN A NEAT, ORDERLY MANNER
- IN THEIR PROPER (ORIGINAL IF POSSIBLE) CONTAINERS AND, IF POSSIBLE, UNDER A ROOF OR OTHER ENCLOSURE.
- 3. MANUFACTURER'S RECOMMENDATIONS FOR PROPER USE AND DISPOSAL SHALL BE
- 4. THE SITE SUPERINTENDENT SHALL INSPECT DAILY TO ENSURE PROPER USE AND DISPOSAL OF MATERIALS. 5. SUBSTANCES SHALL NOT BE MIXED WITH ONE ANOTHER UNLESS RECOMMENDED BY
- 6. WHENEVER POSSIBLE ALL OF A PRODUCT SHALL BE USED UP BEFORE DISPOSING OF
- THE CONTAINER.
- B. HAZARDOUS PRODUCTS THE FOLLOWING PRACTICES SHALL BE USED TO REDUCE THE RISKS ASSOCIATED WITH HAZARDOUS MATERIALS:
 - 1. PRODUCTS SHALL BE KEPT IN THEIR ORIGINAL CONTAINERS UNLESS THEY ARE NOT
 - RESEALABLE. 2. ORIGINAL LABELS AND MATERIAL SAFETY DATA SHALL BE RETAINED FOR
- IMPORTANT PRODUCT INFORMATION. 3. SURPLUS PRODUCT THAT MUST BE DISPOSED OF SHALL BE DISCARDED ACCORDING TO THE MANUFACTURER'S RECOMMENDED METHODS OF DISPOSAL
- C. PRODUCT SPECIFICATION PRACTICES THE FOLLOWING PRODUCT SPECIFIC PRACTICES SHALL BE FOLLOWED ON SITE:
- 1. PETROLEUM PRODUCTS: a. ALL ON SITE VEHICLES SHALL BE MONITORED FOR LEAKS AND RECEIVE
- REGULAR PREVENTIVE MAINTENANCE TO REDUCE LEAKAGE. b. PETROLEUM PRODUCTS SHALL BE STORED IN TIGHTLY SEALED CONTAINERS WHICH ARE CLEARLY LABELED. ANY ASPHALT BASED SUBSTANCES USED ON SITE SHALL BE APPLIED ACCORDING TO THE MANUFACTURER'S RECOMMENDATIONS.
- FERTILIZERS: FERTILIZERS USED SHALL BE APPLIED ONLY IN THE MINIMUM AMOUNTS
- DIRECTED BY THE SPECIFICATIONS. b. ONCE APPLIED FERTILIZER SHALL BE WORKED INTO THE SOIL TO LIMIT EXPOSURE TO STORMWATER.
- STORAGE SHALL BE IN A COVERED SHED OR ENCLOSED TRAILERS. THE CONTENTS OF ANY PARTIALLY USED BAGS OF FERTILIZER SHALL BE TRANSFERRED TO A SEALABLE PLASTIC BIN TO AVOID SPILLS.
- a. ALL CONTAINERS SHALL BE TIGHTLY SEALED AND STORED WHEN NOT
- REQUIRED FOR USE. EXCESS PAINT SHALL NOT BE DISCHARGED TO THE STORM SEWER SYSTEM.

IN ADDITION TO GOOD HOUSEKEEPING AND MATERIAL MANAGEMENT PRACTICES

- EXCESS PAINT SHALL BE DISPOSED OF PROPERLY ACCORDING TO MANUFACTURER'S INSTRUCTIONS OR STATE AND LOCAL REGULATIONS. D. SPILL CONTROL PRACTICES
- DISCUSSED IN THE PREVIOUS SECTION, THE FOLLOWING PRACTICES SHALL BE FOLLOWED FOR SPILL PREVENTION AND CLEANUP: MANUFACTURER'S RECOMMENDED METHODS FOR SPILL CLEANUP SHALL BE CLEARLY
- POSTED AND SITE PERSONNEL SHALL BE MADE AWARE OF THE PROCEDURES AND THE LOCATION OF THE INFORMATION AND CLEANUP SUPPLIES. 2. MATERIALS AND EQUIPMENT NECESSARY FOR SPILL CLEANUP SHALL BE KEPT IN THE MATERIAL STORAGE AREA ON SITE. EQUIPMENT AND MATERIALS SHALL INCLUDE BUT NOT BE LIMITED TO BROOMS, DUSTPANS, MOPS, RAGS, GLOVES, GOGGLES, KITTY LITTER, SAND, SAWDUST AND PLASTIC OR METAL TRASH CONTAINERS

APPROPRIATE PROTECTIVE CLOTHING TO PREVENT INJURY FROM CONTACT WITH A

- SPECIFICALLY FOR THIS PURPOSE. ALL SPILLS SHALL BE CLEANED UP IMMEDIATELY AFTER DISCOVERY 4. THE SPILL AREA SHALL BE KEPT WELL VENTILATED AND PERSONNEL SHALL WEAR
- HAZARDOUS SUBSTANCE. 5. SPILLS OF TOXIC OR HAZARDOUS MATERIAL SHALL BE REPORTED TO THE APPROPRIATE LOCAL, STATE OR FEDERAL AGENCIES AS REQUIRED.
- SHALL BE THE SPILL PREVENTION AND CLEANUP COORDINATOR. E. VEHICLE FUELING AND MAINTENANCE PRACTICE: 1. CONTRACTOR SHALL MAKE AN EFFORT TO PERFORM EQUIPTMENT/VEHICAL FUELING

6. THE SITE SUPERINTENDENT RESPONSIBLE FOR DAY-TO-DAY SITE OPERATIONS

- AND MAINTENANCE AT AN OFF-SITE FACILITY. 2. CONTRACTOR SHALL PROVIDE AN ON-SITE FUELING AND MAINTENANCE AREA THAT IS CLEAN AND DRY.
- IF POSSIBLE THE CONTRACTOR SHALL KEEP AREA COVERED. 4. CONTRACTOR SHALL KEEP A SPILL KIT AT THE FUELING AND MAINTENANCE AREA.
- 5. CONTRACTOR SHALL VEHICLES SHALL BE INSPECTED REGULARLY FOR LEAKS AND 6. CONTRACTOR SHALL USE DRIP PANS, DRIP CLOTHS, OR ABSORBENT PADS WHEN REPLACING SPENT FLUID.

SWPPP SHALL BE PREPARED BY THE ENGINEER (CONTRACTOR). THE CONTRACTOR SHALL BE FAMILIAR WITH THE SWPPP AND KEEP AN UPDATED COPY OF THE SWPPP ONSITE AT ALL TIMES.

THIS PROJECT EXCEEDS ONE (1) ACRE OF DISTURBANCE AND THUS REQUIRES A SWPPP. THE

EROSION CONTROL OBSERVATIONS AND MAINTENANCE PRACTICES

- THE FOLLOWING REPRESENTS THE GENERAL OBSERVATION AND REPORTING PRACTICES THAT SHALL BE FOLLOWED AS PART OF THIS PROJECT. OBSERVATIONS OF THE PROJECT FOR COMPLIANCE WITH THE SWPPP SHALL BE MADE BY THE ENGINEER (CONTRACTOR) AT LEAST ONCE A WEEK OR WITHIN 24 HOURS OF A STORM 0.25
- AN OBSERVATION REPORT SHALL BE MADE AFTER EACH OBSERVATION AND DISTRIBUTED TO THE ENGINEER, THE OWNER, AND THE CONTRACTOR.
- A REPRESENTATIVE OF THE SITE CONTRACTOR, SHALL BE RESPONSIBLE FOR MAINTENANCE AND REPAIR ACTIVITIES.

4. IF A REPAIR IS NECESSARY, IT SHALL BE INITIATED WITHIN 24 HOURS OF REPORT.

- IF MORE THAN 5000 CUBIC YARDS ARE TO BE BLASTED A BLASTING PLAN SHALL BE
- PROVIDED. BLASTING PLAN SHALL INCLUDE: A. LOCATION AND IDENTIFICATION OF DRINKING WATER WELLS LOCATED WITHIN 2000 FEET OF THE PROPOSED BLASTING ACTIVITIES.
- B. A GROUNDWATER QUALITY SAMPLING PROGRAM, APPROVED BY NHDES PRIOR TO INITIATING BLASTING, TO MONITOR FOR NITRATE AND NITRITE EITHER IN THE DRINKING WATER SUPPLY WELLS OR IN OTHER WELLS THAT ARE REPRESENTATIVE OF THE DRINKING WATER SUPPLY WELLS IN THE AREA.

2. THE FOLLOWING BEST MANAGEMENT PROCEDURES FOR BLASTING SHALL BE COMPLIED

1. THE GROUNDWATER SAMPLING PROGRAM MUST BE IMPLEMENTED ONCE APPROVED BY NHDES.

- A. LOADING PRACTICES. THE FOLLOWING BLASTHOLE LOADING PRACTICES TO MINIMIZE ENVIRONMENTAL EFFECTS SHALL BE FOLLOWED
- 1. DRILLING LOGS SHALL BE MAINTAINED BY THE DRILLER AND COMMUNICATED DIRECTLY TO THE BLASTER. THE LOGS SHALL INDICATE DEPTHS AND LENGTHS OF VOIDS, CAVITIES, AND FAULT ZONES OR OTHER WEAK ZONES ENCOUNTERED AS WELL AS GROUNDWATER CONDITIONS.
- 2. EXPLOSIVE PRODUCTS SHALL BE MANAGED ON-SITE SO THAT THEY ARE EITHER USED IN THE BOREHOLE, RETURNED TO THE DELIVERY VEHICLE, OR PLACED IN SECURE CONTAINERS FOR OFF-SITE DISPOSAL.
- PLACEMENT IN SECURED CONTAINERS FOR OFF-SITE DISPOSAL 4. LOADED EXPLOSIVES SHALL BE DETONATED AS SOON AS POSSIBLE AND SHALL NOT BE LEFT IN THE BLASTHOLES OVERNIGHT, UNLESS WEATHER OR OTHER SAFETY

3. SPILLAGE AROUND THE BOREHOLE SHALL EITHER BE PLACED IN THE BOREHOLE OR

CLEANED UP AND RETURNED TO AN APPROPRIATE VEHICLE FOR HANDLING OR

- CONCERNS REASONABLY DICTATE THAT DETONATION SHOULD BE POSTPONED. 5. LOADING EQUIPMENT SHALL BE CLEANED IN AN AREA WHERE WASTEWATER CAN BE PROPERLY CONTAINED AND HANDLED IN A MANNER THAT PREVENTS RELEASE OF
- CONTAMINANTS TO THE ENVIRONMENT. 6. EXPLOSIVES SHALL BE LOADED TO MAINTAIN GOOD CONTINUITY IN THE COLUMN LOAD TO PROMOTE COMPLETE DETONATION. INDUSTRY ACCEPTED LOADING PRACTICES FOR PRIMING, STEMMING, DECKING AND COLUMN RISE NEED TO BE
- ATTENDED TO. B. EXPLOSIVE SELECTION
- THE FOLLOWING BMPS SHALL BE FOLLOWED TO REDUCE THE POTENTIAL FOR GROUNDWATER CONTAMINATION WHEN EXPLOSIVES ARE USED:
- 1. EXPLOSIVE PRODUCTS SHALL BE SELECTED THAT ARE APPROPRIATE FOR SITE CONDITIONS AND SAFE BLAST EXECUTION.
- 2. EXPLOSIVE PRODUCTS SHALL BE SELECTED THAT HAVE THE APPROPRIATE WATER RESISTANCE FOR THE SITE CONDITIONS PRESENT TO MINIMIZE THE POTENTIAL FOR HAZARDOUS EFFECT OF THE PRODUCT UPON GROUNDWATER
- C. PREVENTION OF MISFIRES. APPROPRIATE PRACTICES SHALL BE DEVELOPED AND IMPLEMENTED TO PREVENT MISFIRES.
- D. MUCK PILE MANAGEMENT MUCK PILES (THE BLASTED PIECES OF ROCK) AND ROCK PILES SHALL BE MANAGED IN A MANNER TO REDUCE THE POTENTIAL FOR CONTAMINATION BY IMPLEMENTING THE
- FOLLOWING MEASURES 1. REMOVE THE MUCK PILE FROM THE BLAST AREA AS SOON AS REASONABLY
- 2. MANAGE THE INTERACTION OF BLASTED ROCK PILES AND STORMWATER TO PREVENT CONTAMINATION OF WATER SUPPLY WELLS OR SURFACE WATER.
- E. SPILL PREVENTION MEASURES AND SPILL MITIGATION SPILL PREVENTION AND SPILL MITIGATION MEASURES SHALL BE IMPLEMENTED TO PREVENT THE RELEASE OF FUEL AND OTHER RELATED SUBSTANCES TO THE
 - ENVIRONMENT. THE MEASURES SHALL INCLUDE AT A MINIMUM: 1. THE FUEL STORAGE REQUIREMENTS SHALL INCLUDE:
 - a. STORAGE OF REGULATED SUBSTANCES ON AN IMPERVIOUS SURFACE; b. SECURE STORAGE AREAS AGAINST UNAUTHORIZED ENTRY;
 - LABEL REGULATED CONTAINERS CLEARLY AND VISIBLY; INSPECT STORAGE AREAS WEEKLY;
 - COVER REGULATED CONTAINERS IN OUTSIDE STORAGE AREAS; WHEREVER POSSIBLE, KEEP REGULATED CONTAINERS THAT ARE STORED OUTSIDE MORE THAN 50 FEET FROM SURFACE WATER AND STORM DRAINS, 75 FEET FROM PRIVATE WELLS, AND 400 FEET FROM PUBLIC WELLS; AND
 - SECONDARY CONTAINMENT IS REQUIRED FOR CONTAINERS CONTAINING REGULATED SUBSTANCES STORED OUTSIDE, EXCEPT FOR ON PREMISE USE HEATING FUEL TANKS, OR ABOVEGROUND OR UNDERGROUND STORAGE TANKS OTHERWISE REGULATED.
 - 2. THE FUEL HANDLING REQUIREMENTS SHALL INCLUDE: a EXCEPT WHEN IN USE, KEEP CONTAINERS CONTAINING REGULATED

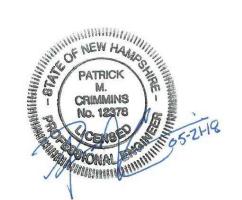
DOCUMENTS/DWGB-22-6.PDF)

- SUBSTANCES CLOSED AND SEALED; PLACE DRIP PANS UNDER SPIGOTS, VALVES, AND PUMPS;
- c. HAVE SPILL CONTROL AND CONTAINMENT EQUIPMENT READILY AVAILABLE IN ALL WORK AREAS;
- USE FUNNELS AND DRIP PANS WHEN TRANSFERRING REGULATED SUBSTANCES PERFORM TRANSFERS OF REGULATED SUBSTANCES OVER AN IMPERVIOUS SURFACE.
- 3. THE TRAINING OF ON-SITE EMPLOYEES AND THE ON-SITE POSTING OF RELEASE RESPONSE INFORMATION DESCRIBING WHAT TO DO IN THE EVENT OF A SPILL OF REGULATED SUBSTANCES. 4. FUELING AND MAINTENANCE OF EXCAVATION, EARTHMOVING AND OTHER CONSTRUCTION RELATED EQUIPMENT SHALL COMPLY WITH THE REGULATIONS OF
- PRACTICES FOR FUELING AND MAINTENANCE OF EXCAVATION AND EARTHMOVING EQUIPMENT" OR ITS SUCCESSOR DOCUMENT. (SEE HTTP://DES.NH.GOV/ORGANIZATION/COMMISSIONER/PIP/FACTSHEETS/DWGB/

REQUIREMENTS ARE SUMMARIZED IN WD-DWGB-22-6 BEST MANAGEMENT

THE NEW HAMPSHIRE DEPARTMENT OF ENVIRONMENTAL SERVICES THESE







Proposed **Industrial** Development

Lonza Biologics

Portsmouth, New Hampshire

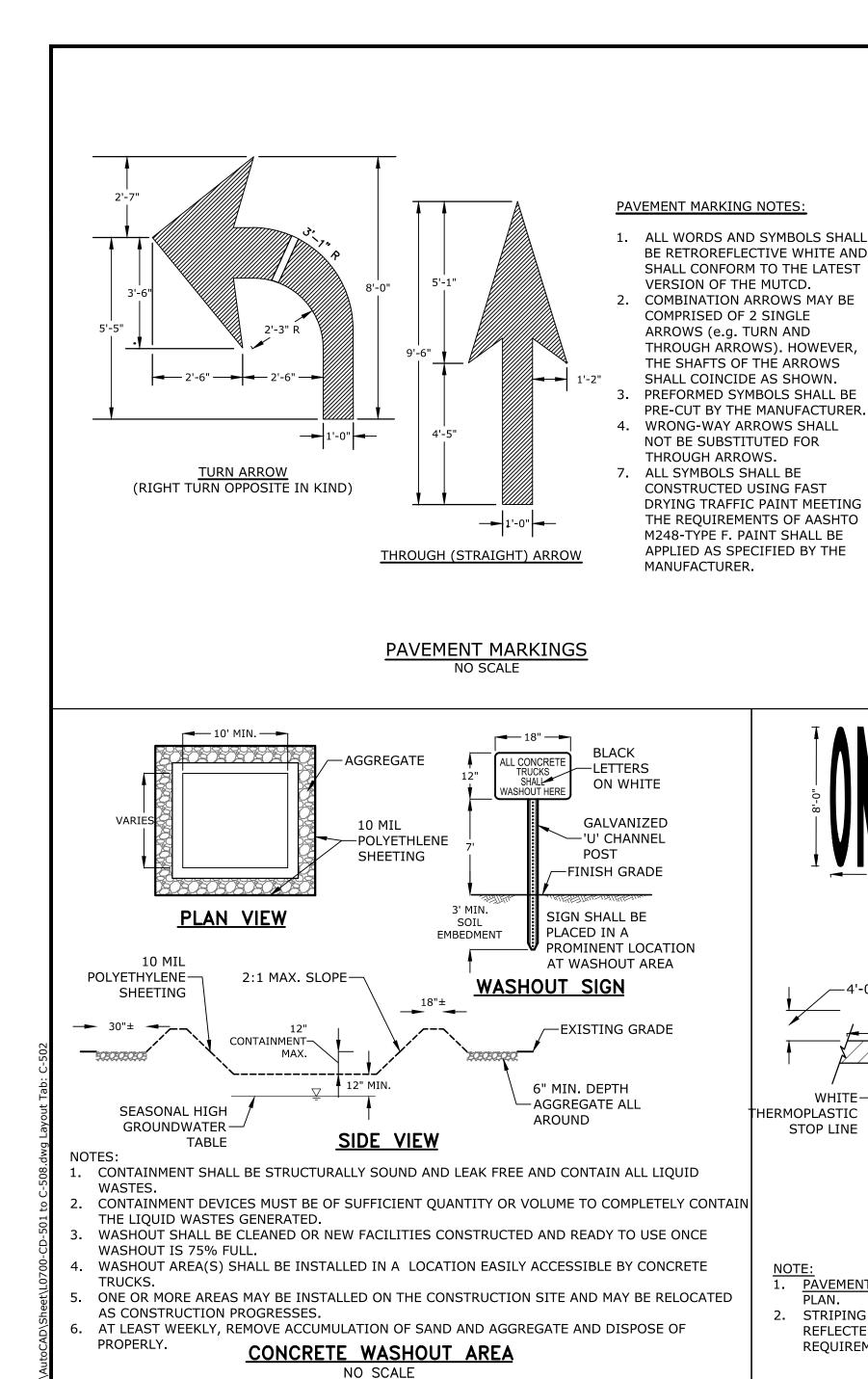
2	5/21/2018	TAC SUBMISSION		
1	4/3/2018	TAC WS SUBMISSION		
MARK	DATE	DESCRIPTION		
PROJE	PROJECT NO: L-0700-13			
DATE:	DATE: 04/03/2018			
FILE: L0700-CD-501 to C-508.dwg				
DRAWI	DRAWN BY: NAH			

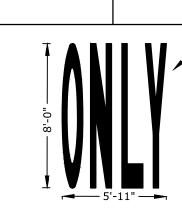
EROSION CONTROL NOTES

BLM

AS SHOWN

SCALE:





THERMOPLASTIC

PAVEMENT MARKINGS TO BE INSTALLED IN LOCATIONS AS SHOWN ON SITE PLAN. STRIPING SHALL BE CONSTRUCTED USING WHITE THERMO PLASTIC,

REFLECTERIZED PAVEMENT MARKING

REQUIREMENTS OF ASTM D 4505

MATERIAL MEETING THE

CONTROL LANE GENERAL NOTES:

THIS DRAWING IS NOT TO BE USED FOR ELECTRICAL CIRCUITRY, REFER TO ELECTRICAL DRAWINGS.

DENOTES CONDUIT AND WIRE BY ELECTRICAL CONTRACTOR.

5. STUB-UP CONDUIT 8" ABOVE TOP OF CONCRETE ISLAND PLUS 3'-0" OF WIRE FOR PARKING EQUIPMENT SUPPLIER.

ELECTRICAL CONTRACTOR SHALL VERIFY WITH PARKING EQUIPMENT SUPPLIER AS TO THE ACTUAL POWER REQUIREMENTS TO EACH LOCATION BEFORE START OF WORK.

ELECTRICAL CONTRACTOR SHALL VERIFY WITH INTERCOM SYSTEM SUPPLIER AS TO THE ACTUAL CONDUIT SIZE REQUIRED BEFORE START OF WORK.

9. FOR ADDITIONAL PARKING EQUIPMENT REQUIREMENTS, REFER TO

4. C.O. (CONDUIT ONLY) DENOTES CONDUIT AND PULL WIRE.

8. CONCRETE CURBS SHALL BE 6" HIGH UNO.

10. COORDINATE WITH ELECTRICAL DRAWINGS.

1A - ARMING LOOP DETECTOR ASSEMBLY

1E - CLOSING LOOP DETECTOR ASSEMBLY

FOR POWER & DATA

1" Ø C.O., ARCNET CABLE (DATA)

② 22/4 CAT3, PVC (VOICE)

1G - INGROUND JUNCTION BOXES (8"x8"x4")

3 3/4" ø C.O., 22/8 CABLE O.S., PVC (DATA)

4 ONE (1) 115VAC, 20AMP CIRCUIT (POWER)

1B - ENTRY/EXIT COLUMN UNLIMITED (See Detail)

PARKING CONTROL EQUIPMENT LIST

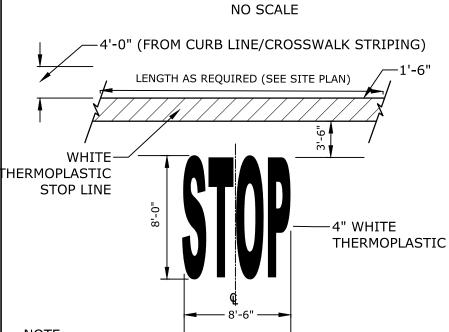
1C - TWO-WAY INTERCOM UNIT

1D - BARRIER GATE (See Detail)

CONTROL LANE # 1 (E) or (X)

1F - PROTECTION POST

ONLY LEGEND



1. PAVEMENT MARKINGS TO BE INSTALLED IN LOCATIONS AS SHOWN ON SITE

2. STRIPING SHALL BE CONSTRUCTED USING WHITE THERMO PLASTIC, REFLECTERIZED PAVEMENT MARKING MATERIAL MEETING THE REQUIREMENTS OF ASTM D 4505

STOP BAR AND LEGEND NO SCALE

LV: (1) 1" MIN Ø C.O. FOR DATA/VOICE TO PARKING OFFICE/TELCO ROOM HV: POWER SUPPLY FROM THE NEAREST RESOURCE (1)-120 VAC, 20 AMP CKT PROPOSED (N) 6" H

3/4" CONDUIT W/ LOOP WIRE FROM DETECTOR IN

GATE TO FACE OF CONC.

CURB, THEN SAW CUT

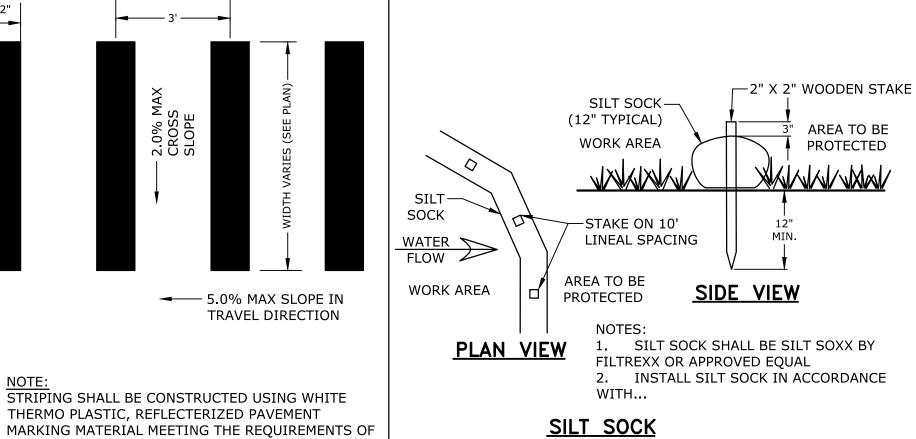
LOOP LEAD WIRE INTO

CONC. SLAB, TYP.

TYPICAL BARRIER GATE DETAILS NO SCALE

<u>EXIT</u>

NO SCALE



. THE LANES, ISLANDS, AND GATE CONTROL LOCATIONS SHOWN

ON THE PLAN ARE FOR GRAPHICAL PURPOSES ONLY, AND ARE

2. FINAL BARRIER GATE DESIGN AND PREFERRED VENDOR TO BE

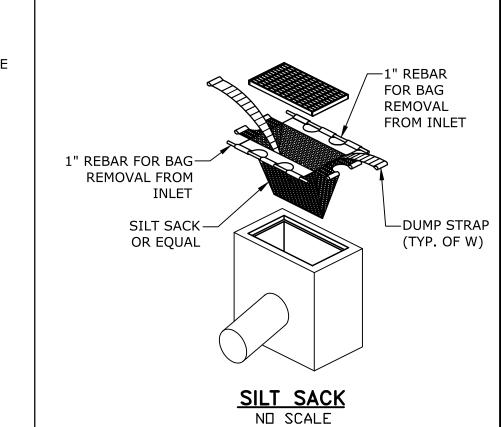
COORDINATED WITH LONZA PRIOR TO CONSTRUCTION.

CROSSWALK STRIPING

NO SCALE

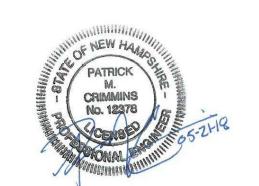
CONTROL THAT IS DESIRED.

INTENDED TO GENERALLY CONVEY THE INTENT OF THE ACCESS



RAISED CONCRETE ISLAND

Engineers | Environmental Specialists





Proposed **Industrial Development**

Lonza Biologics

Portsmouth, New Hampshire

10.20" RADIUS— NON-ABRASIVE SURFACE A .125" P.V.C. JACKET IS APPLIED TO PRIMED PIPE.-DEDICATED FOOTPRINT— SECTION A-A B◀

EXISTING 36" HDPE PIPE ∠25° BATTER 12" CRUSHED STONE-NHDOT ITEM 304.4

ASTM D 4505

1.5' <u>PLAN</u> **BIKE RACK**

NO SCALE

2 5/21/2018 TAC SUBMISSION 4/3/2018 TAC WS SUBMISSION MARK DATE DESCRIPTION PROJECT NO: L-0700-13 04/03/2018 FILE: L0700-CD-501 to C-508.dwg DRAWN BY: NAH CHECKED: PMC APPROVED: BLM

DETAILS SHEET

AS SHOWN

C-502

SCALE:

NOTE:

SEE GRADING

SLOPE LIMITS—

COMPACTED

COMMON FILL—

PLAN FOR

1. FINAL PAVEMENT DESIGN TO BE BASED ON GEOTECH REPORT.

-COMPACTED

SUBGRADE

2. SEE GRADING, DRAINAGE AND EROSION CONTROL PLAN FOR PAVEMENT SLOPE AND CROSS-SLOPE. 3. A TACK COAT SHALL BE PLACED ON TOP OF BINDER COURSE PAVEMENT PRIOR TO PLACING WEARING COURSE.

4. CONTRACTOR SHALL HAVE THE OPTION OF RECLAIMING THE EXISTING PAVEMENT AND REMOVING THE

VARIES

-6" CRUSHED GRAVEL BASE

(SLOPE TO MATCH PAVEMENT SLOPE)

(SLOPE TO MATCH PAVEMENT SLOPE)

NHDOT ITEM #304.3

-12" GRAVEL SUBBASE

NHDOT ITEM #304.2

-NHDOT ITEM #403.11

3" NOMINAL

HOT BITUMINOUS PAVEMENT

1.5" WEARING COURSE TYPE E 1.5" BINDER COURSE TYPE B

MATERIAL, THEN REUSING THE RECLAIMED MATERIAL AS A PAVEMENT SUBBASE.

STANDARD DUTY PAVEMENT SECTION

-SEE CURB DETAIL AND

SITE PLAN FOR

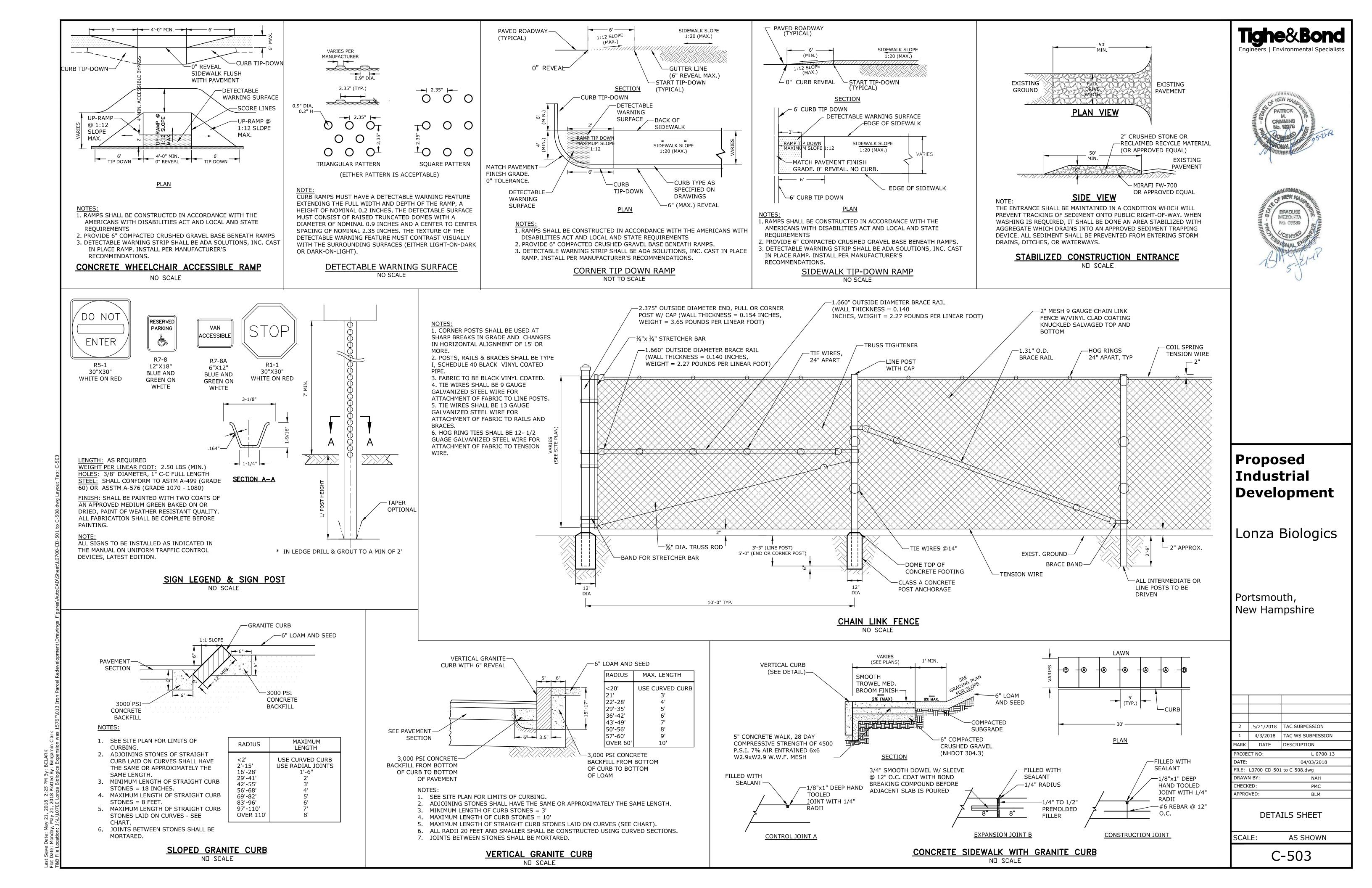
LOCATIONS

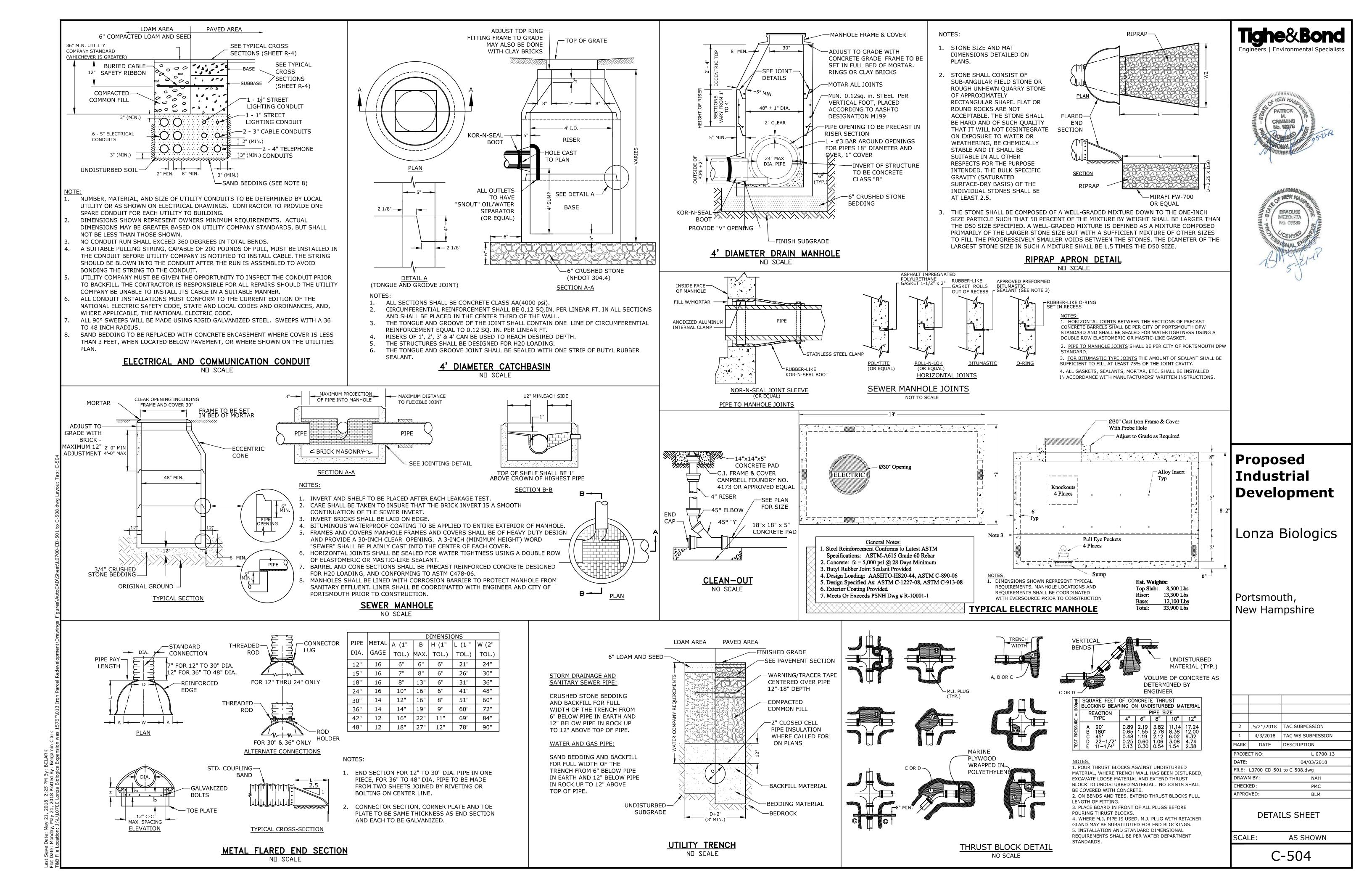
SEE GRADING PLAN FOR SLOPE LIMITS

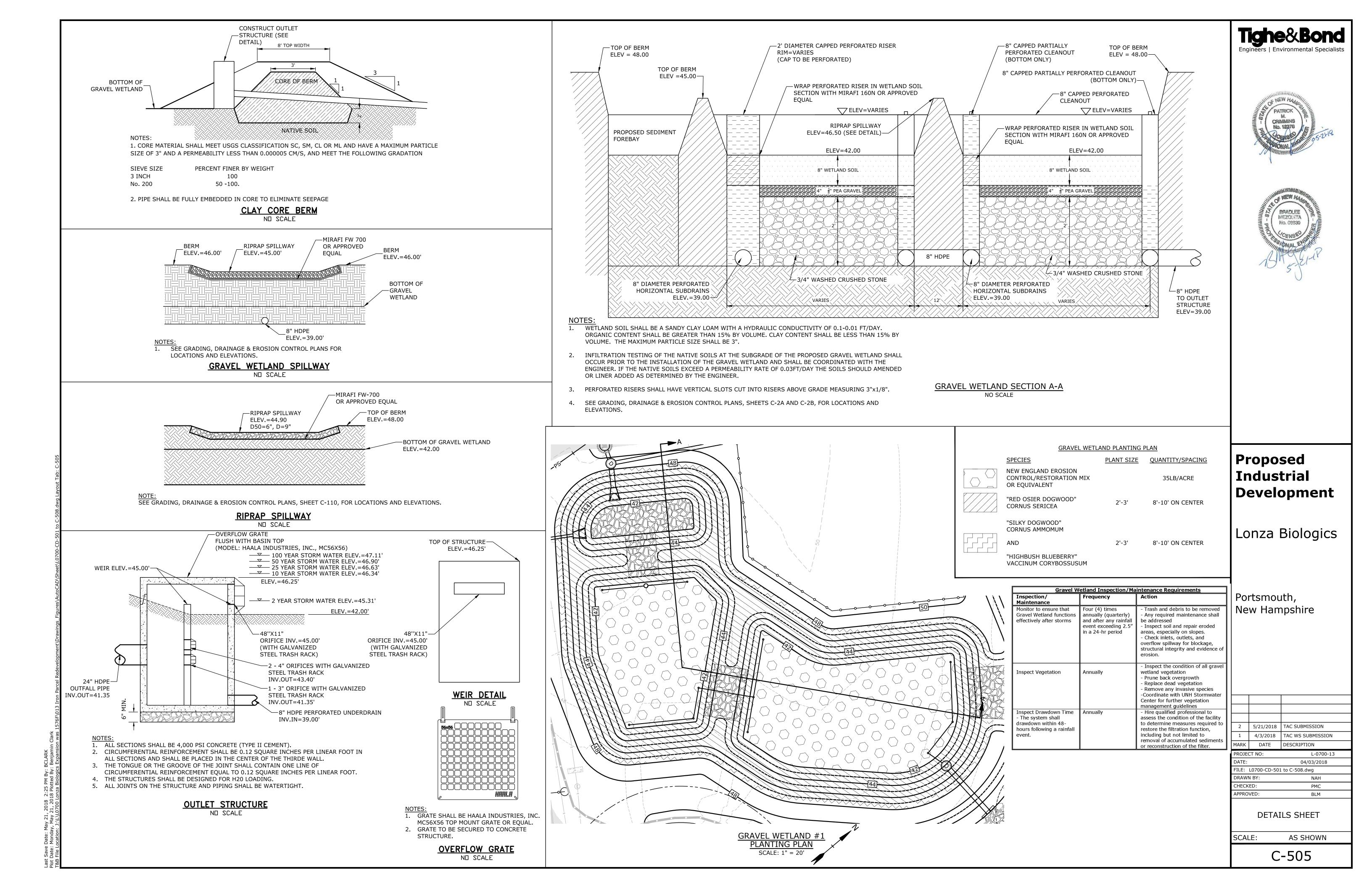
> 1. CONTRACTOR SHALL SUBMIT REBAR CAGE LAYOUT FOR APPROVAL PRIOR

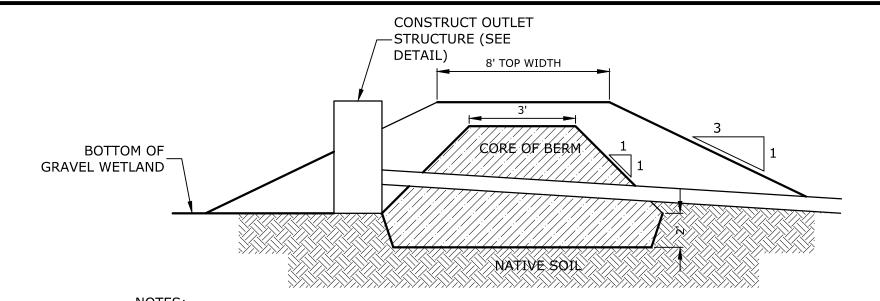
TO CONSTRUCTION.

CONCRETE HEADWALL NO SCALE









No. 200

1. CORE MATERIAL SHALL MEET USGS CLASSIFICATION SC, SM, CL OR ML AND HAVE A MAXIMUM PARTICLE SIZE OF 3" AND A PERMEABILITY LESS THAN 0.000005 CM/S, AND MEET THE FOLLOWING GRADATION

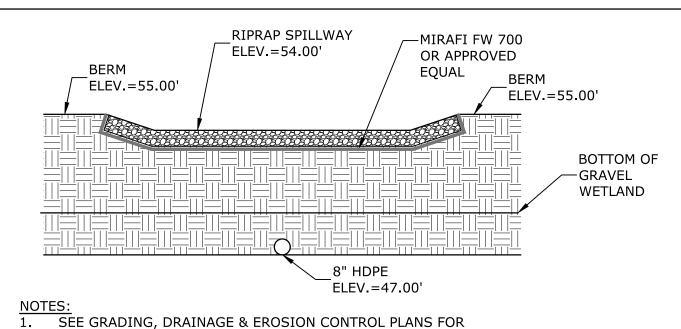
PERCENT FINER BY WEIGHT SIEVE SIZE 3 INCH 100

2. PIPE SHALL BE FULLY EMBEDDED IN CORE TO ELIMINATE SEEPAGE

50 -100

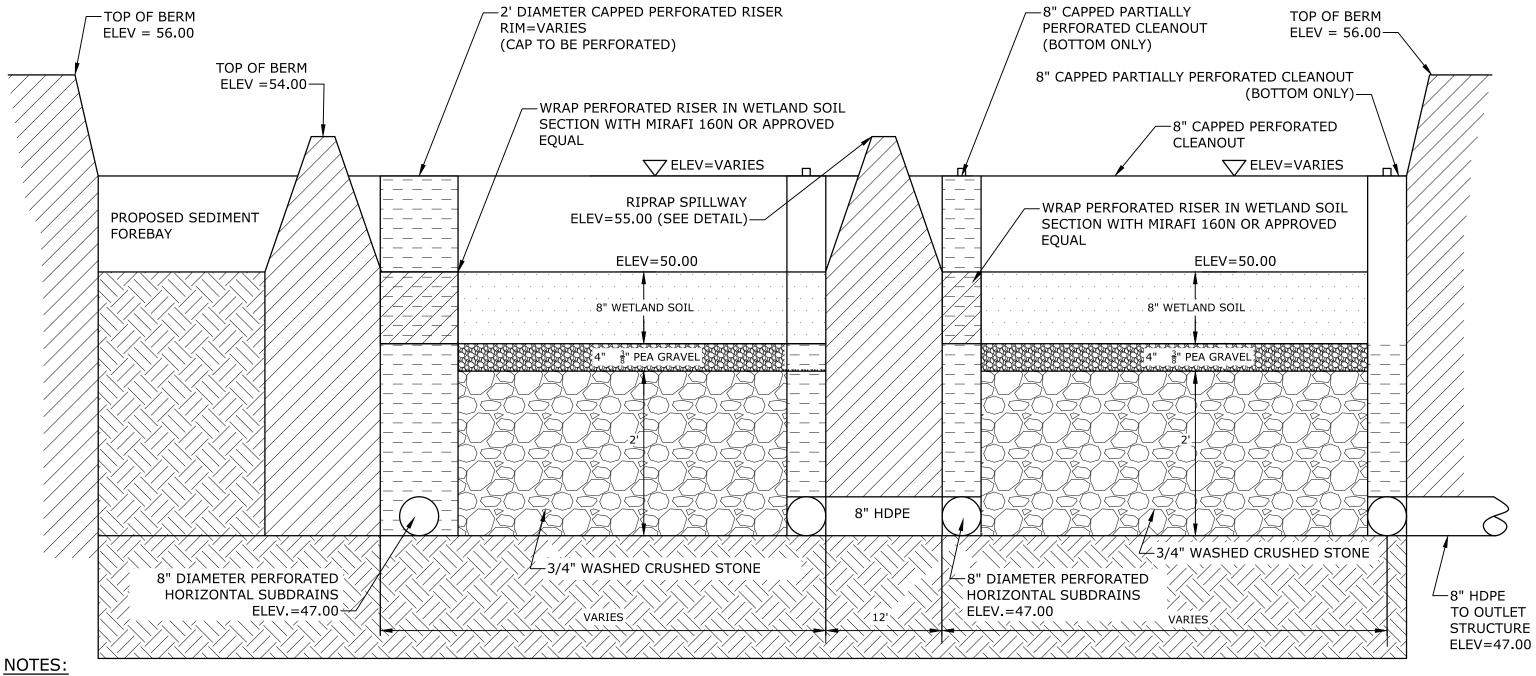
LOCATIONS AND ELEVATIONS.

CLAY CORE BERM



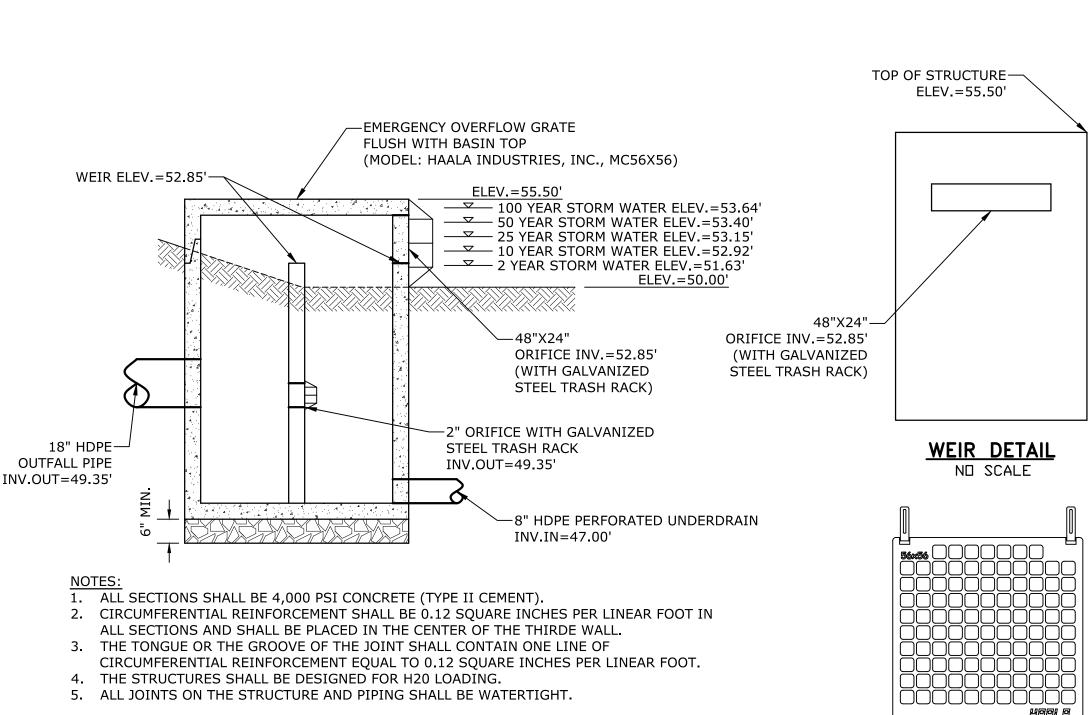
GRAVEL WETLAND SPILLWAY

NO SCALE



- WETLAND SOIL SHALL BE A SANDY CLAY LOAM WITH A HYDRAULIC CONDUCTIVITY OF 0.1-0.01 FT/DAY. ORGANIC CONTENT SHALL BE GREATER THAN 15% BY VOLUME. CLAY CONTENT SHALL BE LESS THAN 15% BY VOLUME. THE MAXIMUM PARTICLE SIZE SHALL BE 3".
- INFILTRATION TESTING OF THE NATIVE SOILS AT THE SUBGRADE OF THE PROPOSED GRAVEL WETLAND SHALL OCCUR PRIOR TO THE INSTALLATION OF THE GRAVEL WETLAND AND SHALL BE COORDINATED WITH THE ENGINEER. IF THE NATIVE SOILS EXCEED A PERMEABILITY RATE OF 0.03FT/DAY THE SOILS SHOULD AMENDED OR LINER ADDED AS DETERMINED BY THE ENGINEER.
- 3. PERFORATED RISERS SHALL HAVE VERTICAL SLOTS CUT INTO RISERS ABOVE GRADE MEASURING 3"x1/8".
- 4. SEE GRADING, DRAINAGE & EROSION CONTROL PLANS, SHEETS C-2A AND C-2B, FOR LOCATIONS AND ELEVATIONS.

GRAVEL WETLAND SECTION A-A



Insp Mair Moni Grav effec HARLA , MC56X56 TOP MOUNT GRATE OR EQUAL.

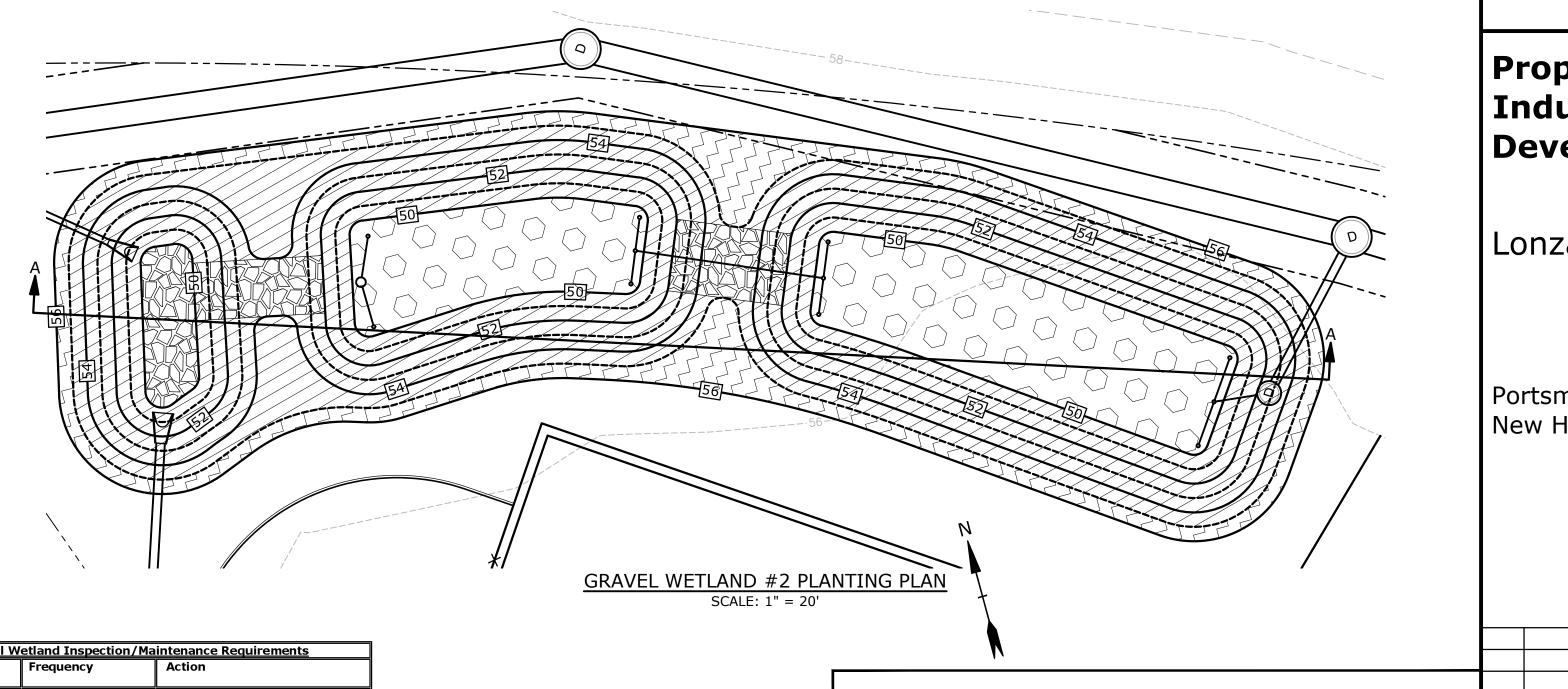
OUTLET STRUCTURE

NO SCALE

NOTES:
1. GRATE SHALL BE HAALA INDUSTRIES, INC.

2. GRATE TO BE SECURED TO CONCRETE STRUCTURE.

> **OVERFLOW GRATE** NO SCALE



Proposed **Industrial Development**

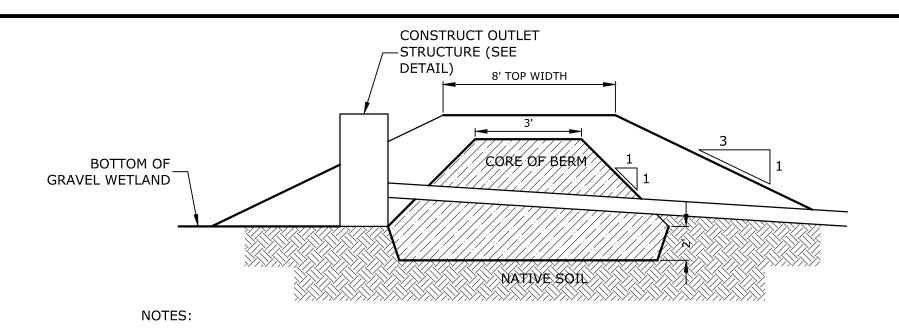
MEZICLETA

Lonza Biologics

Portsmouth, New Hampshire

Gravel W	etland Inspection/Ma	intenance Requirements
Inspection/ Maintenance	Frequency	Action
Monitor to ensure that Gravel Wetland functions effectively after storms	Four (4) times annually (quarterly) and after any rainfall event exceeding 2.5" in a 24-hr period	- Trash and debris to be removed - Any required maintenance shall be addressed - Inspect soil and repair eroded areas, especially on slopes Check inlets, outlets, and overflow spillway for blockage, structural integrity and evidence of erosion.
Inspect Vegetation	Annually	- Inspect the condition of all gravel wetland vegetation - Prune back overgrowth - Replace dead vegetation - Remove any invasive species -Coordinate with UNH Stormwater Center for further vegetation management guidelines
Inspect Drawdown Time - The system shall drawdown within 48- hours following a rainfall event.	Annually	- Hire qualified professional to assess the condition of the facility to determine measures required to restore the filtration function, including but not limited to removal of accumulated sediments or reconstruction of the filter.

11					
GRAVEL WETLA	AND PLANTING F	PI AN	2	5/21/2018	TAC SUBMISSION
			1	4/3/2018	TAC WS SUBMISSION
SPECIES	PLANT SIZE	QUANTITY/SPACING	MARK	DATE	DESCRIPTION
NEW ENGLAND EROSION			PROJE	CT NO:	L-0700-13
CONTROL/RESTORATION MIX		35LB/ACRE	DATE:		04/03/2018
OR EQUIVALENT			FILE:	L0700-CD-501	to C-508.dwg
"RED OSIER DOGWOOD"			DRAWI	N BY:	NAH
CORNUS SERICEA	2'-3'	8'-10' ON CENTER	CHECK	ED:	PMC
			APPRO	VED:	BLM
"SILKY DOGWOOD" CORNUS AMMOMUM				DETAI	LS SHEET
AND	2'-3'	8'-10' ON CENTER			
"HIGHBUSH BLUEBERRY"			SCAL	E:	AS SHOWN
VACCINUM CORYBOSSUSUM				_	



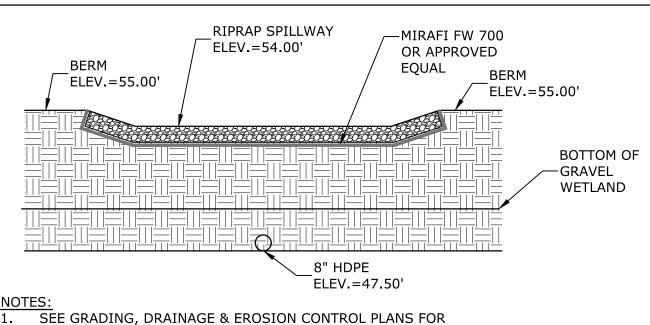
1. CORE MATERIAL SHALL MEET USGS CLASSIFICATION SC, SM, CL OR ML AND HAVE A MAXIMUM PARTICLE SIZE OF 3" AND A PERMEABILITY LESS THAN 0.000005 CM/S, AND MEET THE FOLLOWING GRADATION

SIEVE SIZE PERCENT FINER BY WEIGHT

3 INCH 100 No. 200 50 -100.

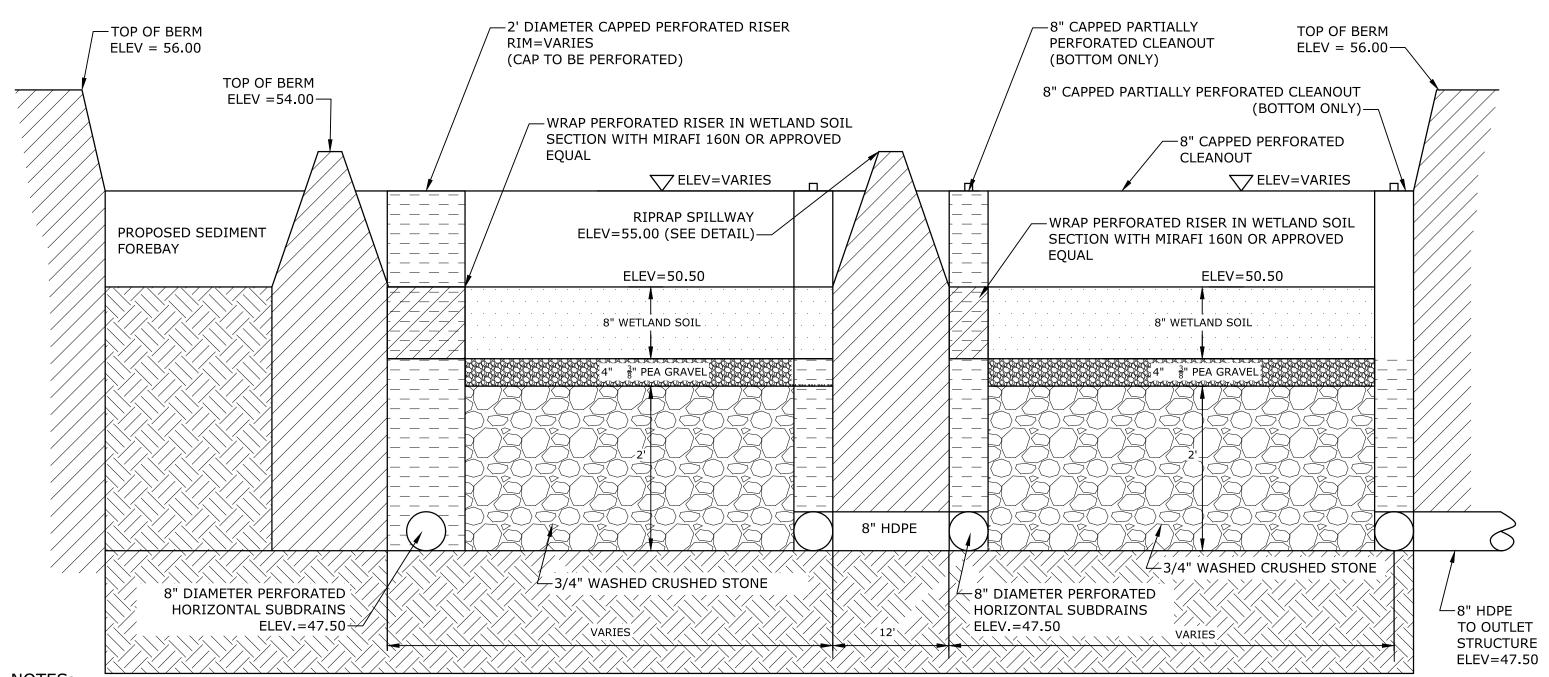
2. PIPE SHALL BE FULLY EMBEDDED IN CORE TO ELIMINATE SEEPAGE

CLAY CORE BERM



LOCATIONS AND ELEVATIONS.

GRAVEL WETLAND SPILLWAY



NOTES:

MC56X56 TOP MOUNT GRATE OR EQUAL.

OVERFLOW GRATE

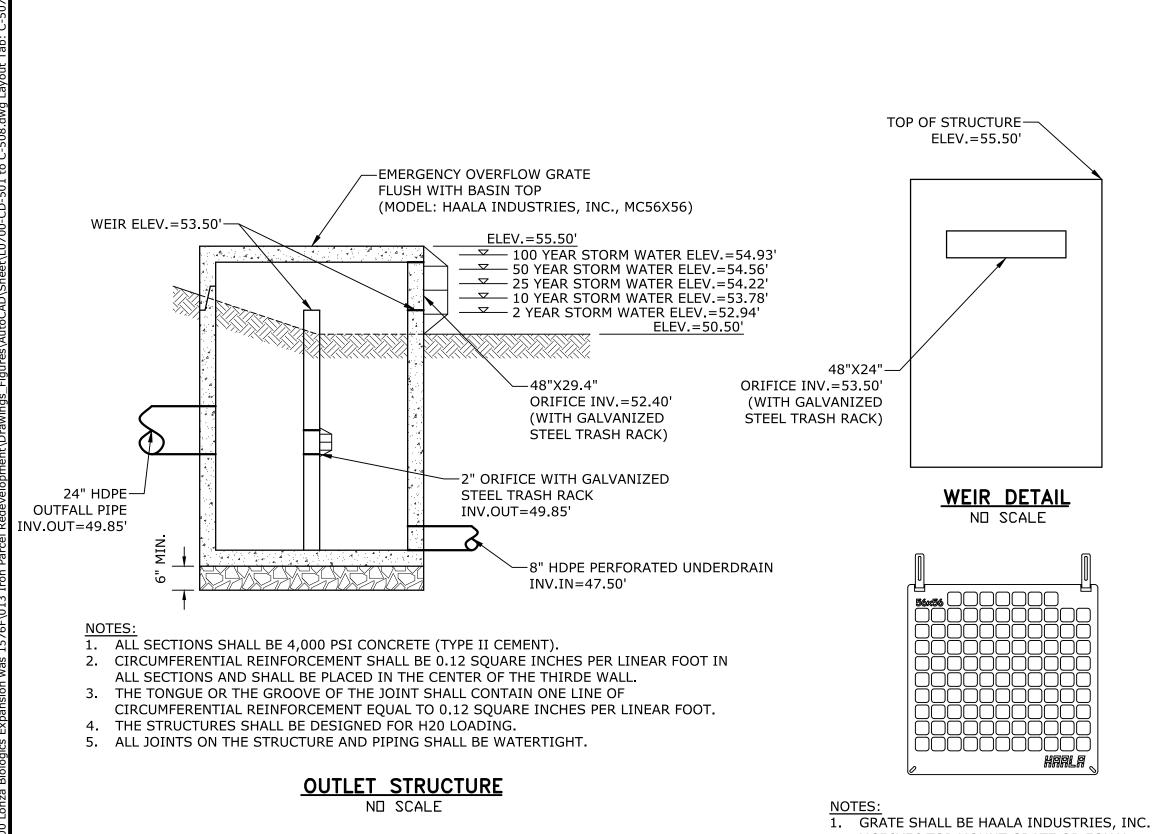
NO SCALE

2. GRATE TO BE SECURED TO CONCRETE

STRUCTURE.

- .. WETLAND SOIL SHALL BE A SANDY CLAY LOAM WITH A HYDRAULIC CONDUCTIVITY OF 0.1-0.01 FT/DAY.
 ORGANIC CONTENT SHALL BE GREATER THAN 15% BY VOLUME. CLAY CONTENT SHALL BE LESS THAN 15% BY VOLUME. THE MAXIMUM PARTICLE SIZE SHALL BE 3".
- 2. INFILTRATION TESTING OF THE NATIVE SOILS AT THE SUBGRADE OF THE PROPOSED GRAVEL WETLAND SHALL OCCUR PRIOR TO THE INSTALLATION OF THE GRAVEL WETLAND AND SHALL BE COORDINATED WITH THE ENGINEER. IF THE NATIVE SOILS EXCEED A PERMEABILITY RATE OF 0.03FT/DAY THE SOILS SHOULD AMENDED OR LINER ADDED AS DETERMINED BY THE ENGINEER.
- 3. PERFORATED RISERS SHALL HAVE VERTICAL SLOTS CUT INTO RISERS ABOVE GRADE MEASURING 3"x1/8".
- 4. SEE GRADING, DRAINAGE & EROSION CONTROL PLANS, SHEETS C-2A AND C-2B, FOR LOCATIONS AND ELEVATIONS.

GRAVEL WETLAND SECTION A-A



Inspect

GRAVEL WETLAND #3 PLANTING PLAN

SPECIES

SCALE: 1" = 20'

Industrial Development

Gravel Wetland Inspection/Maintenance Requirements
Frequency Action

Industrial Development

Lonza Biologics

MEZICLETA

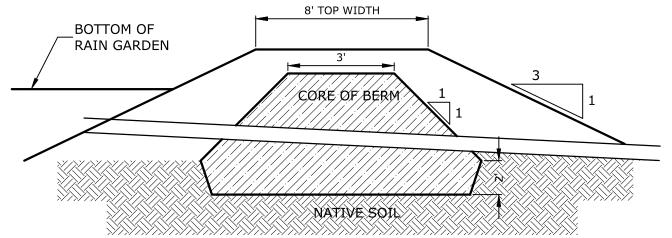
Proposed

Portsmouth,

New Hampshire

Maintenance	Trequency	Action
Monitor to ensure that Gravel Wetland functions effectively after storms	Four (4) times annually (quarterly) and after any rainfall event exceeding 2.5" in a 24-hr period	- Trash and debris to be removed - Any required maintenance shall be addressed - Inspect soil and repair eroded areas, especially on slopes Check inlets, outlets, and overflow spillway for blockage, structural integrity and evidence of erosion.
Inspect Vegetation	Annually	- Inspect the condition of all gravel wetland vegetation - Prune back overgrowth - Replace dead vegetation - Remove any invasive species -Coordinate with UNH Stormwater Center for further vegetation management guidelines
Inspect Drawdown Time - The system shall drawdown within 48- hours following a rainfall event.	Annually	- Hire qualified professional to assess the condition of the facility to determine measures required to restore the filtration function, including but not limited to removal of accumulated sediments or reconstruction of the filter.

		ll ll	reconstruction of the filter	·³		ļ	
		01	reconstruction of the filter.				
	GRAVEL W	VETLAND PLANTING F	ΡΙ ΔΝ	2	5/21/2018	TAC SUBMISSION	
			LAN	1	4/3/2018	TAC WS SUBMISSION	
	SPECIES	PLANT SIZE	QUANTITY/SPACING	MARK	DATE	DESCRIPTION	
\rightarrow	NEW ENGLAND EROSION			PROJE	CT NO:	L-0700-13	3
	CONTROL/RESTORATION MI	X	35LB/ACRE	DATE:		04/03/2018	
	OR EQUIVALENT			FILE:	L0700-CD-50	1 to C-508.dwg	
	"RED OSIER DOGWOOD"			DRAW	N BY:	NAH	
	CORNUS SERICEA	2'-3'	8'-10' ON CENTER	CHECK	ŒD:	PMC	
				APPRO	VED:	BLM	
	"SILKY DOGWOOD"						
	CORNUS AMMOMUM				DFTΔ1	ILS SHEET	
	AND	21.21	OL 10LON CENTER		DEIM	ILS STILLT	
	AND	2'-3'	8'-10' ON CENTER				
	"HIGHBUSH BLUEBERRY"			SCAI	LE:	AS SHOWN	
	VACCINUM CORYBOSSUSUM	1			_		
					C	-507	
					_	 -	



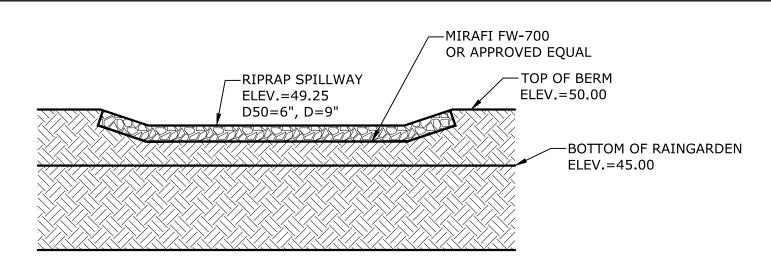
NOTES:

1. CORE MATERIAL SHALL MEET USGS CLASSIFICATION SC, SM, CL OR ML AND HAVE A MAXIMUM PARTICLE SIZE OF 3" AND A PERMEABILITY LESS THAN 0.000005 CM/S, AND MEET THE FOLLOWING GRADATION

SIEVE SIZE PERCENT FINER BY WEIGHT 3 INCH 100 50 -100. No. 200

2. PIPE SHALL BE FULLY EMBEDDED IN CORE TO ELIMINATE SEEPAGE

CLAY CORE BERM ND SCALE

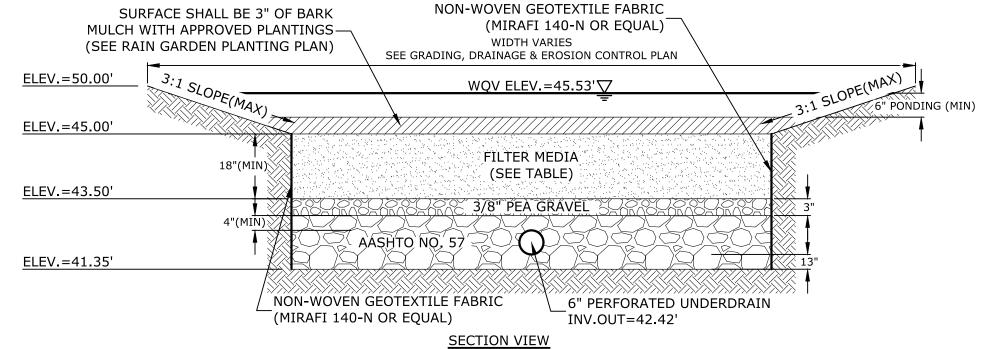


NOTE:
SEE GRADING, DRAINAGE & EROSION CONTROL PLANS, SHEET C-110, FOR LOCATIONS AND ELEVATIONS.

RIPRAP SPILLWAY

NO SCALE

	RAINGARDEN PLANT SCHEDULE					
CODE	BOTANICAL NAME	COMMON NAME	SIZE	REMARKS		
TREES				•		
BN	BETULA NIGRA	RIVER BIRCH	12 - 14' HT	B & B (CLUMP)		
AC	AMALANCHIER CANADENSIS	SHADBLOW SERVICEBERRY	6 - 7' HT	B & B (CLUMP)		
SHRUBS	5					
VD	VIBURNUM DENTATUM	ARROWWOOD VIBURNUM	5 GALLON	CONTAINER		
CA	CLETHERA ALNIFOLIA	SUMMERSWEET CLETHERA	5 GALLON	CONTAINER		
PERENN	IIALS					
PV	PANICUM VIRGATUM 'SHENANDOAH'	SHENANDOAH SWITCH GRASS	3 GALLON	CONTAINER		
EM	EUPATORIUM MACULATUM	JOE PYE WEED	2 GALLON	CONTAINER		
ΑI	ASCLEPIAS INCARNATA	MARSH MILKWEED	2 GALLON	CONTAINER		
RG	RUDBECKIA 'GOLDSTURM'	GOLDSTURM BLACKEYED SUSAN	1 GALLON	CONTAINER		
EP	ECHINACEA 'PURPUREA'	PURPLE CONEFLOWER	1 GALLON	CONTAINER		



	FILTER MEDIA COMPOSITION:				
COMPONENT MATERIAL	PERCENT OF MIXTURE	GRADATI	ON OF MATERIAL		
	BY VOLUME	SIEVE NO.	PERCENT PASSING		
ASTM C-33 CONCRETE SAND	50-55	SEE N	IOTE #5		
LOAMY SAND TOPSOIL	20-30	200	15-25		
MODERATELY FINE SHREDDED	20-30	200	5 MAX.		
BARK OR WOOD FIBER MULCH					

- NOTES:

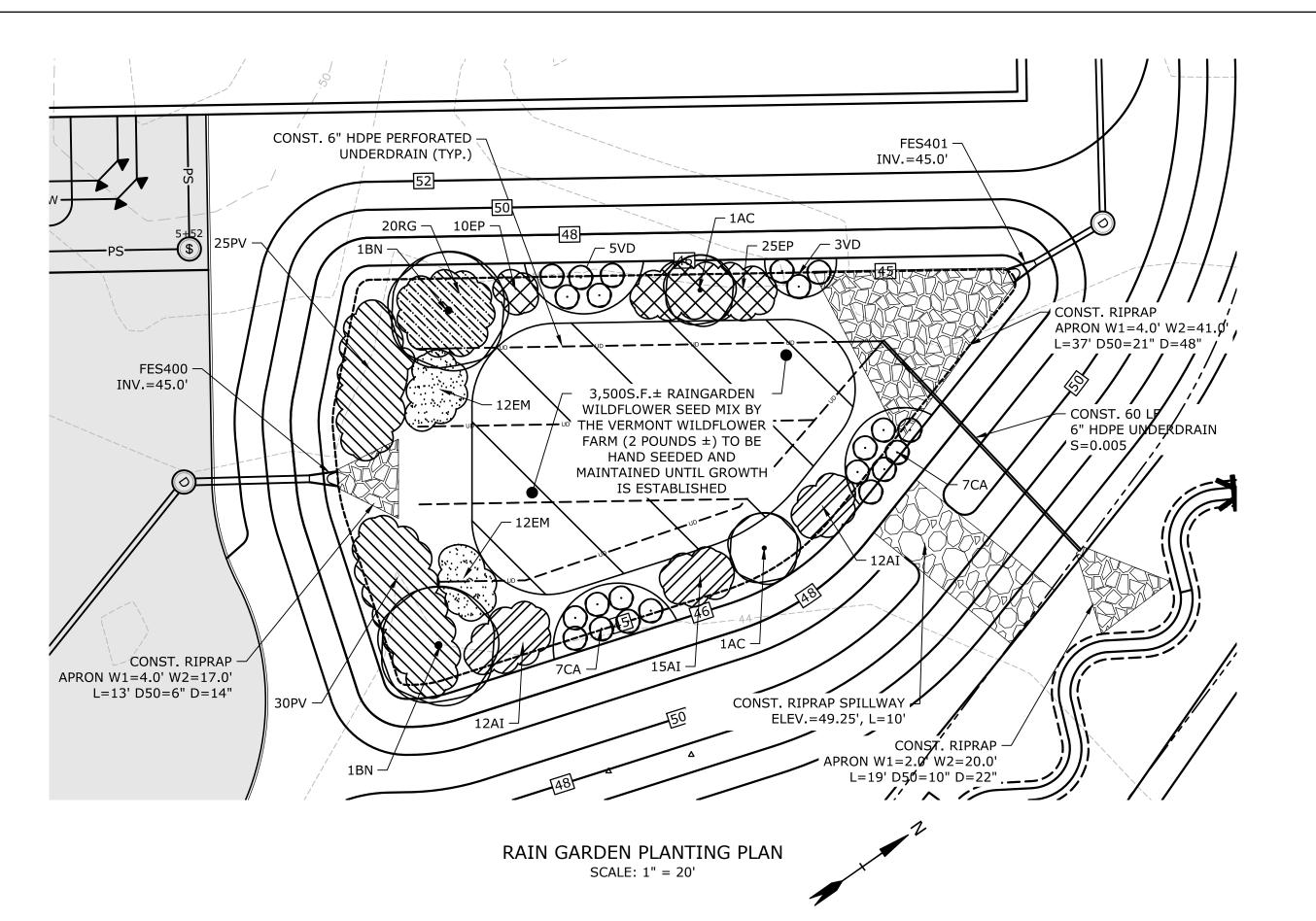
 1. BARK MULCH SHALL BE AGED A MINIMUM OF 12 MONTHS AND SHALL NOT FLOAT.
- 2. RAIN GARDENS SHALL NOT BE PLACED INTO SERVICE UNTIL THE PRACTICE HAS BEEN PLANTED AND ITS CONTRIBUTING AREAS HAVE BEEN FULLY STABILIZED.

0-10

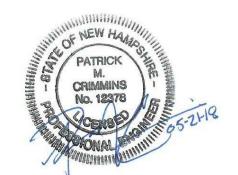
- 3. DO NOT TRAFFIC EXPOSED SOIL SURFACES WITH CONSTRUCTION EQUIPMENT. CONTRACTOR SHALL
- KEEP ALL EXCAVATION EQUIPMENT OUTSIDE OF THE LIMIT OF THE RAIN GARDEN.
 4. SEE GRADING, DRAINAGE & EROSION CONTROL PLAN FOR LOCATIONS, LAYOUTS, AND ELEVATIONS.
- 5. THE SAND PORTION OF THE FILTER MEDIA SHALL MEET THE FOLLOWING GRADATION (ASTM C-33): SIEVE SIZE PERCENT PASSING
- SIEVE SIZE #4 95-100 #8 80-100 #16 50-85 #30 25-60 #50 5-30

#100

RAIN GARDEN NO SCALE









Proposed Industrial Development

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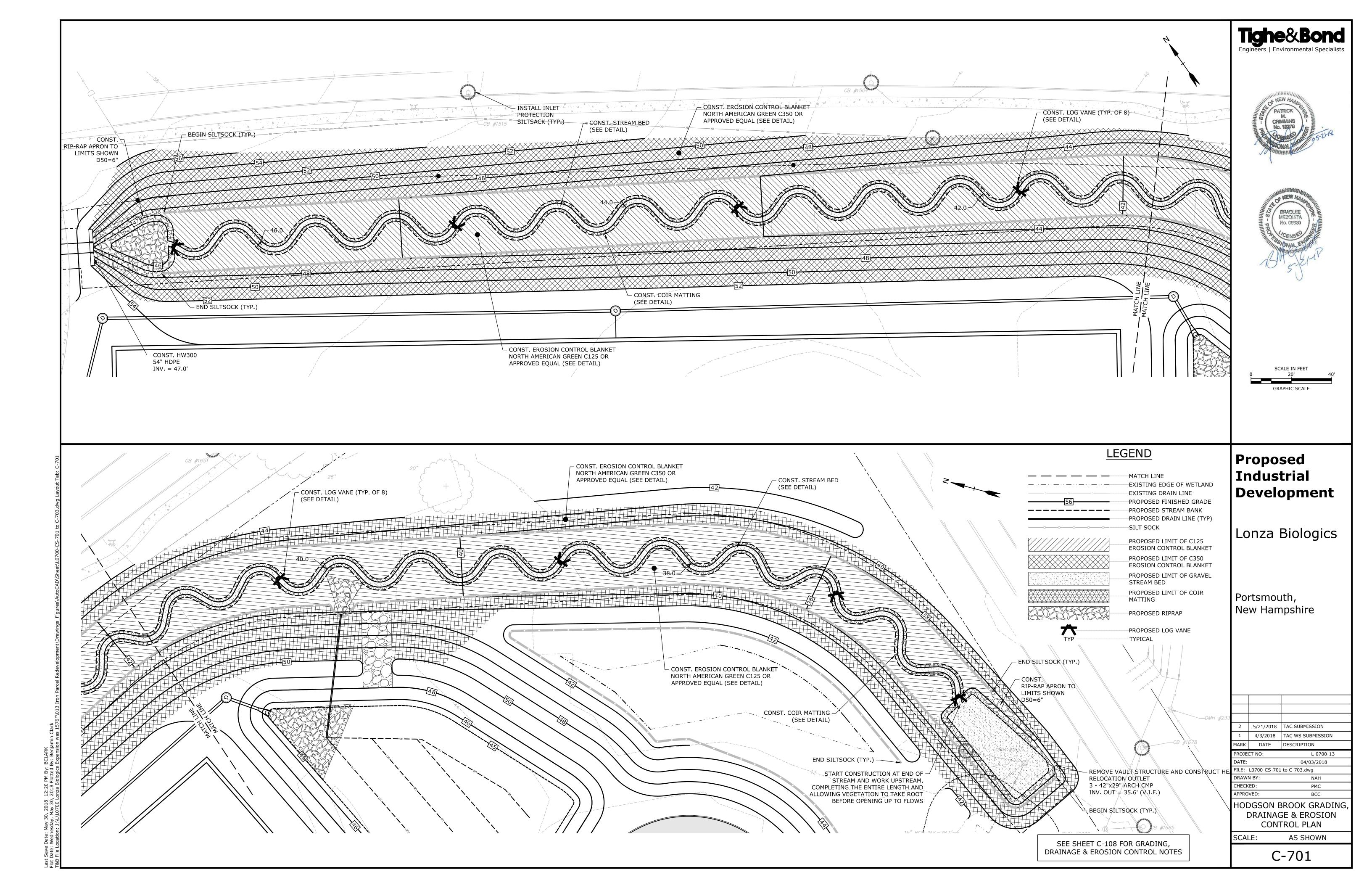
2	5/21/2018	TAC SUBMISSION	
1	4/3/2018	TAC WS SUBMISSION	
MARK	DATE	DESCRIPTION	
PROJECT NO:		L-0700-13	
DATE:		04/03/2018	
FILE: L0700-CD-501 to C-508.dwg			
DRAWN BY:		NAH	
CHECKED:		PMC	
A DDD O	VED:	51.14	

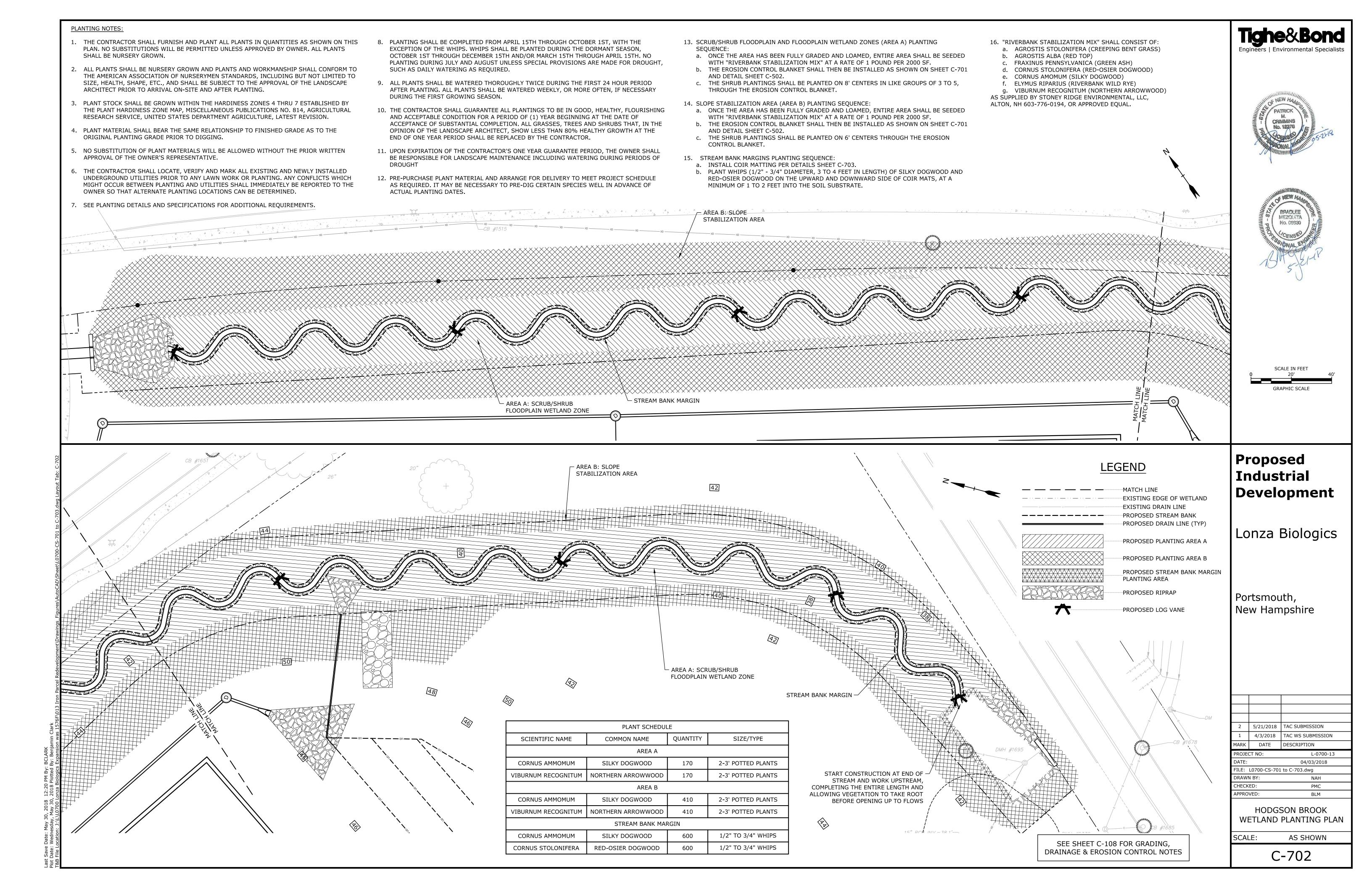
BLM

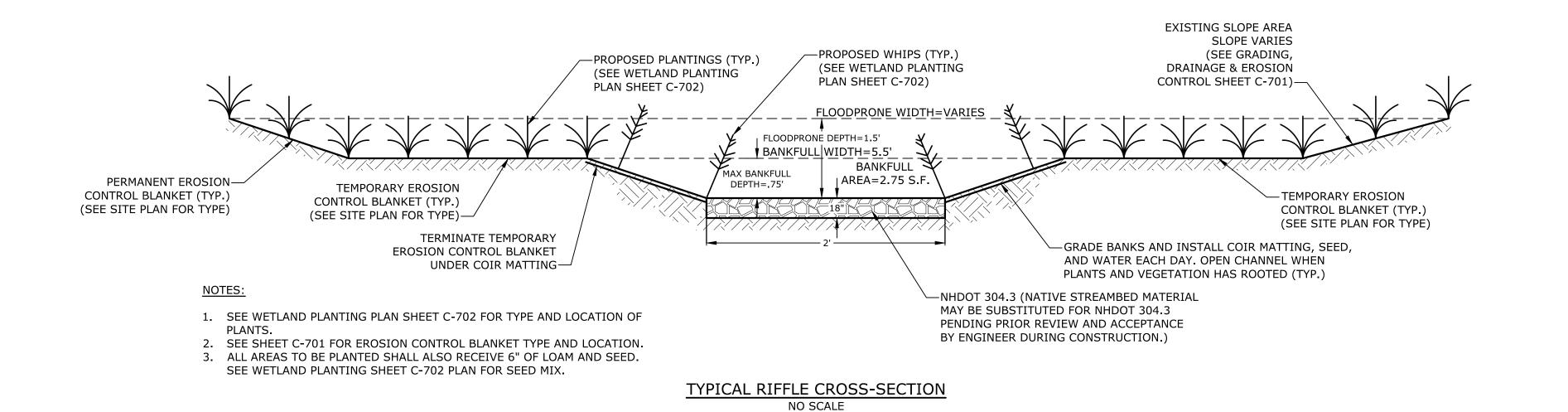
DETAILS SHEET

SCALE: AS SHOWN

APPROVED:







PLANTING SOIL MIX TO TOP OF CURB--WIDTH OF PIT SHALL BE 3 TIMES WIDTH OF ROOT BALL (5' MIN. IN CURB-LEDGE) (SCARIFY AND SLOPE SIDES **BITUMINOUS** OF PIT) CONCRETE ∕─3" EARTH SAUCER PAVEMENT--PLANTING SOIL MIX: DECIDUOUS -FOUR PARTS TOPSOIL & ONE PART MANURE, EVERGREEN - FOUR PARTS 6" MIN. IN EARTH TOPSOIL & ONE PART PEAT HUMUS 18" MIN. IN LEDGE COMPACTED SUBGRADE -TAMPED PLANTING MIX -UNTIE BURLAP & ROLL BACK 1/3 OF ROOT BALL. IF PLASTIC BURLAP IS USED, REMOVE COMPLETELY. CONTAINER GROWN NURSERY DUG REMOVE CONTAINER | BALL & BURLAP CURBED ISLAND CONDITION - LAWN CONDITION NOTE: PLANT AT SAME DEPTH AS PREVIOUSLY PLANTED, OR WITHIN 2" ABOVE. SHRUB PLANTING

NOTE: INITIAL CONSTRUCTION AND ANY CHANGES SHALL BE NOTCH SHALL BE CUT COORDINATED ON-SITE, DURING CONSTRUCTION, 2" WIDER THAN THE DIAMETER OF THE LOG WITH THE SITE ENGINEER. TO FIT IN THE NOTCH— -BACKFILL WITH GRAVEL MATCHING FILTER FABRIC-- BANKFULL -12" MIN. STREAMBED ANCHOR (TYP.)— 1/2 LOG DIA. CROSS LOG-SIDE VIEW OF NOTCH **→** 15-20 DEG —FILTER FABRIC 15-20 DEG -FOOTER LOG 3' MIN → FLOODPLAIN SILL, BURIED IN BANK--HEADER LOG RE-BAR PLAN VIEW OF NOTCH PLAN VIEW (TYP.)-BANKFULL ELEVATION <u>v</u> GRAVEL BACKFILL-BANKFULL ELEVATION

SINGLE LOG VANE CONSTRUCTION SEQUENCE:

EXCAVATE A TRENCH FOR THE VANE.

FASTENED AT THEIR CENTERS).

- 2. SET THE CROSS LOG
- 3. SET THE VANE LOG(S).
- 4. PIN THE LOG VANE ARMS WITH 4' LONG, ½" REBAR HAMMERED INTO PRE-DRILLED HOLES (2ft ON CENTER). HOLES ARE ANGLED OFF THE VERTICAL, ALTERNATING DIRECTION (UPSTREAM, DOWNSTREAM).
- 5. EXCAVATE A TRENCH FOR THE GEOTEXTILE FABRIC ON THE UPSTREAM SIDE OF THE VANE. THE TRENCH SHALL BE AT LEAST 1.5' DEEP.
- 6. ANCHORS SHALL BE CABLED TO THE LOGS BY > \frac{1}{7}" WIRE ROPE (CABLE), FASTENED WITH GRIPPLE CLIPS OR
- BOLTED CLAMPS. 7. ANCHORS SHALL BE EITHER LARGE (>100LB) ROCK OR REBAR CROSSES (TWO PIECES OF 2' LENTH, ½" REBAR
- 8. STAPLE OR NAIL THE GEOTEXTILE ON THE UPSTREAM SIDE OF THE LOG, JUST ABOVE MID-DIAMETER, FOR THE FULL LENGTH OF THE LOG. FOLD OVER THE GEOTEXTILE FABRIC ALONG NAIL LINE. THE STAPLES/NAILS SHALL BE AT LEAST 1' ON CENTERS OR CLOSER. THE STAPLE/ NAIL
- LENGTH SHOULD BE AT LEAST 1". 9. BACKFILL THE UPSTREAM SIDE OF THE VANE.
- 10. EXCAVATE A SILL TRENCH (MINIMUM LENGTH OF 3') AT THE BANK-END OF THE LOG; EITHER A STONE SILL WITH MINIMUM DEPTH OF 2' OR A GEOTEXTILE SILL - TWO
- PARALLEL TRENCHES WITH A MINIMUM DEPTH OF 2'. 11. CONSTRUCT THE SILL: PLACE >1' SIZE STONES IN TRENCH, COVER WITH GEOTEXTILE (MIRAFI N140 OR APPROVED EQUAL), BACKFILL; OR PLACE GEOTEXTILE IN PARALLEL TRENCHES, COVERING A MOUND BETWEEN THEM, AND BACKFILL.
- 12. WEAVE ONE CONTINUOUS GEOTEXTILE ALONG VANE AND SILL.

FILTER FABRIC—

HEADER LOG

FOOTER LOG

SECTION A-A

. CROSS LOGS SHALL BE A MINIMUM OF 8" IN DIAMETER. VANE ARM LOGS SHALL BE A MINIMUM OF 6" IN DIAMETER. ALL LOGS SHOULD BE RELATIVELY STRAIGHT AND, OF A HARDWOOD, HEMLOCK, OR LARCH SPECIES.

-RE-BAR

(TYP.)

2. CROSS LOGS SHALL BE A MINIMUM OF 8' IN LENGTH AND BE PINNED EVERY 2'. VANE ARM LOGS SHALL BE A MINIMUM OF 7', AND PINNED EVERY 2'.

SECTION B-B

3. VANE ARM LOGS SHALL BE BURIED INTO THE BANK A MINIMUM OF 2', WHERE THEY SHALL BE KEYED INTO THE BANK WITH A SILL OF A MINIMUM LENGTH OF 3'.

NO SCALE

- 4. NAIL FILTER FABRIC (MIRAFI 140N OR APPROVED EQUAL) ON TOP OF FOOTER LOG USING 3" 10d GALVANIZED COMMON NAIL OR SIMILAR AT 1' INTERVALS ALONG THE LOG. FOLD OVER THE FILTER FABRIC ALONG THE NAIL LINE.
- 5. SET THE ELEVATION OF THE TOP OF THE CROSS LOG TO THE DESIGNED THALWEG (CENTERLINE) ELEVATION OF THE STREAMBED. 6. THE CROSS NOTCH CAN BE FORMED BY MAKING CUTS 1"-2" APART WITH A CHAINSAW, THEN KNOCKING OUT THE SECTIONS WITH A CHISEL AND HAMMER.
- 7. THE ANGLE OF THE CROSS NOTCH SHALL MATCH THE ANGLE BETWEEN THE VANE ARMS AND THE STREAM BANK. 8. SCOUR POOLS SHALL BE OVER DUG BY ~1.4x THE RIFFLE DEPTH, OR ABOUT 1' - 1.25' DEEP.

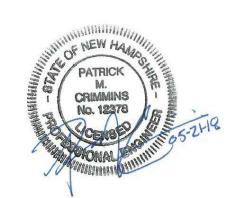
SCOUR POOL-

-ANCHOR

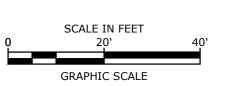
(TYP.)

LOG CROSS VANE









Proposed **Industrial Development**

Lonza Biologics

Portsmouth, New Hampshire

2	5/21/2018	TAC SUBMISSION	
1	4/3/2018	TAC WS SUBMISSION	
MARK	DATE	DESCRIPTION	
PROJECT NO:		L-0700-13	
DATE:		04/03/2018	
FILE: L0700-CS-701 to C-703.dwg			
DRAWN BY:		NAH	

HODGSON BROOK DETAILS SHEET

PMC

BLM

SCALE: AS SHOWN

CHECKED:

APPROVED:

C-703

PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING ANY NECESSARY

BEGIN AT THE TOP OF THE SLOPE, 36" OVER THE GRADE BREAK, BY ANCHORING

THE BLANKET IN A 6" DEEP X 6" WIDE TRENCH WITH APPROXIMATELY 12" OF

BLANKET EXTENDED BEYOND THE UPSLOPE PORTION OF THE TRENCH. ANCHOR

THE BLANKET WITH A ROW OF TAPLES/STAKES 12" APART IN THE BOTTOM OF

THE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING. APPLY

SEED TO COMPACTED SOIL AND FOLD REMAINING 12" PORTION OF BLANKET

BACK OVER SEED AND COMPACTED SOIL. SECURE BLANKET OVER COMPACTED

SOIL WITH A ROW OF STAPLES SPACED 12" APART ACROSS THE WIDTH OF THE

ROLL THE BLANKETS DOWN THE SLOPE. ALL BLANKETS MUST BE SECURELY

FASTENED TO THE SOIL SURFACE BY PLACING STAPLES IN APPROPRIATE

EROSION CONTROL BLANKET FOR SLOPE PROTECTION

LOCATIONS AS SHOWN ON THE STAPLE PATTERN GUIDE.

4. STAPLE LENGTHS SHALL BE A MINIMUM OF 8 INCHES.

APPLICATION OF LIME, FERTILIZER AND SEED.

BLANKET.

NO SCALE